



March 27, 2025

ODOT District 11  
2201 Reiser Avenue  
New Philadelphia, Ohio 44663

Attention: Ms. Adrienne N. Slanina, P.E.  
Consultant Contract Manager

Reference: Roadway Exploration – Final Submittal  
PID No. 119710  
Agreement No. 39773  
Task Order No. 11-D  
BEL-40-23.37, PID 114388  
Belmont County, Ohio  
CTL Project No. 24050050MOR

Dear Ms. Slanina

CTL Engineering, Inc. has completed the field and laboratory testing for the above referenced project. The following information is attached to this letter. We are also submitting spreadsheets with scour calculations separately.

- Typed Boring Log
- Mechanical Soil Classification Testing
- Rock Core Slake Durability
- Rock Core Uniaxial Compressive Strength
- Rock Core Photos
- Scour Data – Soil
- Scour Data - Bedrock

## Exploration

The test boring was drilled on December 30 and December 31, 2024, utilizing 3-¼ inch I.D. hollow-stem augers powered by a Mobile B-57 track-mounted drill rig. Split- spoon samples and Standard Penetration Tests (SPTs) were performed in the test borings using a 140-pound automatic hammer falling 30 inches to drive a 2-inch O.D. split barrel sampler for 18 inches. The automatic hammer was calibrated at an energy ratio of 79.3 percent on May 3, 2023.

Upon encountering auger refusal, the boring was further advanced into bedrock utilizing rock core sampling techniques and an NX size double tube core barrel with a diamond bit.

The test boring was staked in the field by ODOT Dist. 11 personnel. The test boring was drilled at the location shown in the following table.

Borehole	Location Description	Latitude	Longitude
B-001-0-24	East of bridge	40.066709	-80.820546

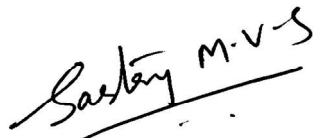
The recovered split spoon samples obtained during the drilling operations were preserved in glass jars, visually classified in the field and laboratory, and tested for moisture content. Representative samples were subjected to laboratory testing including Atterberg Limits, grain size distribution, and hand penetrometer.

The recovered rock core samples obtained during the drilling operations were preserved in core boxes, visually classified in the field and laboratory, and suitable representative rock core samples were tested for compressive strength and slake durability.

We appreciate the opportunity to be of service to you on this project. If you have any questions, please contact us.

Respectfully submitted,

**CTL Engineering, Inc.**



Sastry Malladi, P.E.  
Project Engineer



Joe Grani, P.E.  
Project Engineer

cc: Mr. Cody Notz, P.E. (via email)



PROJECT: BEL-40-23.37	DRILLING FIRM / OPERATOR: CTL / HB	DRILL RIG: MOBILE B-57 #513	STATION / OFFSET: 205+80, 1' LT.	EXPLORATION ID: B-001-0-24
TYPE: BRIDGE	SAMPLING FIRM / LOGGER: CTL / HB	HAMMER: MOBILE AUTOMATIC	ALIGNMENT:	
PID: 114388 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 5/3/23	ELEVATION: 716.7 (MSL) EOB: 46.0 ft.	PAGE: 1 OF 2
START: 12/30/24 END: 12/31/24	SAMPLING METHOD: SPT	ENERGY RATIO (%): 76.8	LAT / LONG: 40.066709, -80.820546	

MATERIAL DESCRIPTION AND NOTES	ELEV.	DEPTHS	SPT/RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	ABANDONED		
								GR	CS	FS	SI	CL	LL	PL	PI					
DENSE, GRAY, GRAVEL AND/OR STONE FRAGMENTS WITH SAND, LITTLE CLAY, TRACE SILT, FILL, DAMP @1.5'; MEDIUM DENSE, TRACE CLAY  @ 3.0'; CONTAINS PIECES OF CONCRETE  @ 4.5'; LITTLE CLAY	716.7		19																	
			16	40	100	SS-1	1.50	37	26	19	7	11	NP	NP	NP	13	A-1-b (0)			
			15																	
			12	29	100	SS-2	-	34	28	20	8	10	NP	NP	NP	12	A-1-b (0)			
			11																	
MEDIUM DENSE, GRAY, GRAVEL AND/OR STONE FRAGMENTS WITH SAND, LITTLE SILT, LITTLE CLAY, DAMP @ 7.5'; TRACE SILT, TRACE CLAY  @ 9.0'; LITTLE CLAY	710.7		7	19	100	SS-3	-	-	-	-	-	-	-	-	-	-	A-1-b (V)			
			7																	
			8	20	100	SS-4	-	41	21	16	10	12	NP	NP	NP	10	A-1-b (0)			
			9																	
			6	14	100	SS-5	1.00	28	22	26	12	12	NP	NP	NP	12	A-1-b (0)			
VERY STIFF, GRAY, SILT AND CLAY, SOME SAND, SOME GRAVEL, DAMP	706.2	▼	5	19	100	SS-6	2.00	51	17	13	10	9	NP	NP	NP	17	A-1-b (0)			
			6																	
			5	20	100	SS-7	-	53	13	13	9	12	NP	NP	NP	17	A-1-b (0)			
			6																	
			7	20	100	SS-8	-	53	13	13	9	12	NP	NP	NP	17	A-1-b (0)			
HARD, GRAY, SILTY CLAY, SOME SAND, SOME GRAVEL, DAMP	704.7	W 704.7	7	20	100	SS-8	3.00	27	19	16	17	21	32	20	12	16	A-6a (1)			
			7																	
DENSE, GRAY, GRAVEL AND/OR STONE FRAGMENTS WITH SAND, SILT, AND CLAY, DAMP	703.2		8	24	100	SS-9	4.50	24	12	15	19	30	40	20	20	13	A-6b (6)			
			8																	
MEDIUM DENSE, GRAY, SANDY SILT, LITTLE CLAY, LITTLE GRAVEL	701.7		10	33	100	SS-10	1.50	41	14	16	14	15	28	16	12	15	A-2-6 (0)			
			10																	
CLAYSTONE, BROWN, SEVERELY WEATHERED.	700.2	TR	8	27	100	SS-11	-	13	8	25	39	15	NP	NP	NP	7	A-4a (4)			
			9																	
			9	35	100	SS-12	1.50	-	-	-	-	-	-	-	-	-	-	10	Rock (V)	
			12																	
			12	41	100	SS-13	2.50	-	-	-	-	-	-	-	-	-	-	8	Rock (V)	
SHALE, GRAY, HIGHLY WEATHERED, SLIGHTLY STRONG; RQD 28%, REC 71%. @21.0' to 26.0'; I <sub>d2</sub> = 94.2%  @26.0' to 31.0'; I <sub>d2</sub> = 89.6%	695.7		12																	
			16																	
			16																	
			19																	
			19																	
			19		25	SS-14	-	-	-	-	-	-	-	-	-	10	Rock (V)			
			50/2"																	
			0		50	NQ2-1												CORE		
			0		55	NQ2-2												CORE		
			0																	

PID: 114388    SFN: \_\_\_\_\_    PROJECT: BEL-40-23.37    STATION / OFFSET: 205+80, 1' LT.    START: 12/30/24    END: 12/31/24    PG 2 OF 2    B-001-0-24

MATERIAL DESCRIPTION AND NOTES	ELEV. 686.7	DEPTHS	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			ODOT CLASS (GI)	ABAN- DONED
								GR	CS	FS	SI	CL	LL	PL	PI		
<b>SHALE, GRAY, HIGHLY WEATHERED, SLIGHTLY STRONG; RQD 28%, REC 71%. (continued)</b> @ 31.0'; Moderately Weathered @ 31.0' to 36.0'; I <sub>d2</sub> = 95.1% @ 32.3' to 32.8'; Q <sub>u</sub> = 2,380 psi  @ 36.4' to 36.9'; Q <sub>u</sub> = 2,790 psi	686.7	31															
		32															
		33	72	100	NQ2-3										CORE		
		34															
		35															
<b>CLAYSTONE, BROWN AND GRAY, HIGHLY WEATHERED, WEAK TO SLIGHTLY STRONG; RQD 31%, REC 100%.</b>  @ 44.1' to 44.5'; Q <sub>u</sub> = 1,620 psi	679.3	36															
	670.7	37															
		38	27	100	NQ2-4										CORE		
		39															
		40															
41																	
	670.7	42															
		43															
		44	47	100	NQ2-5										CORE		
		45															
		46															

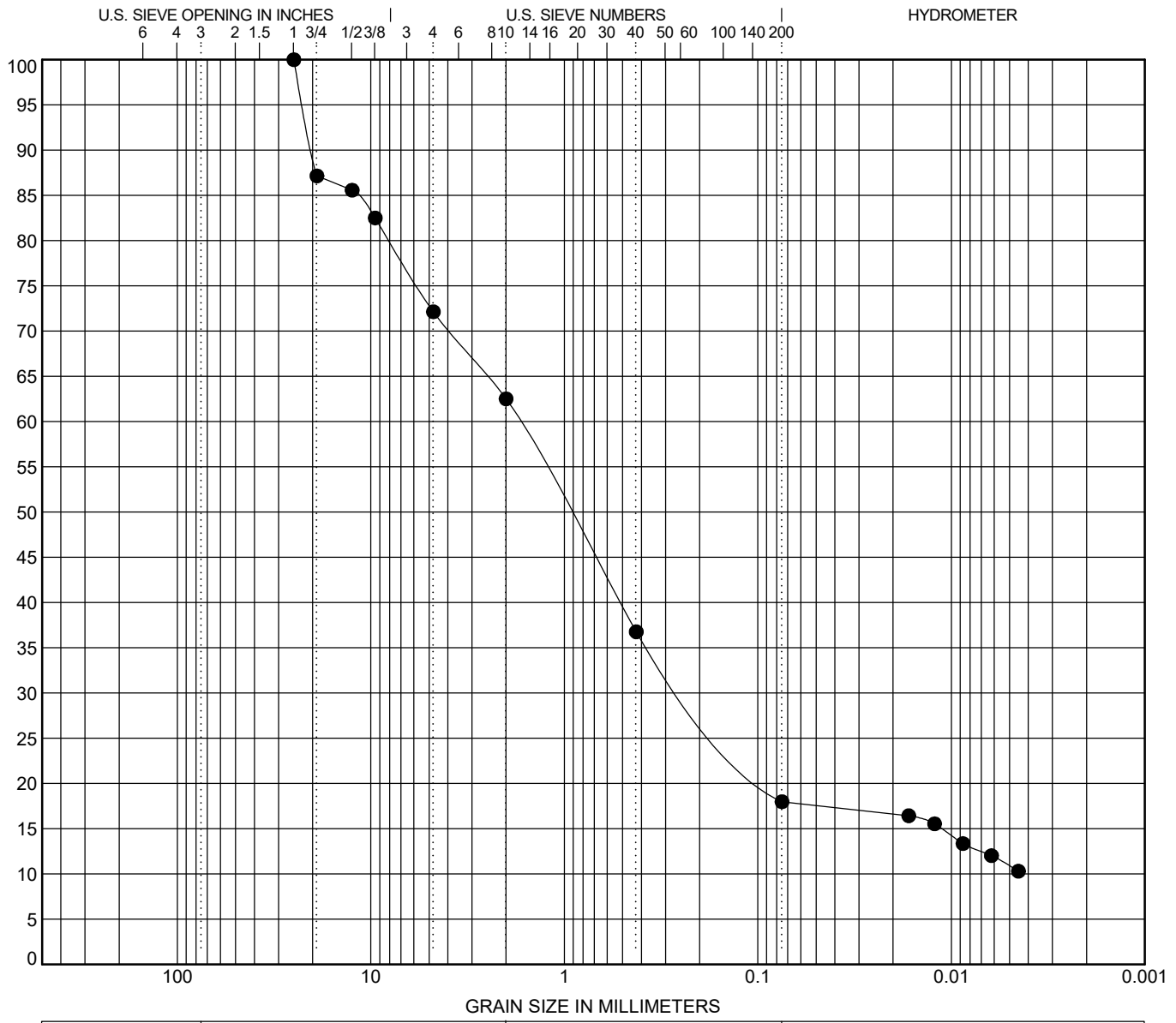
EOB

NOTES: CAVED AT 7'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: GROUT



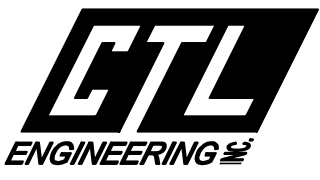
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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>0.0</b>	<b>A-1-b(0)</b>	<b>13</b>	<b>NP</b>	<b>NP</b>	<b>NP</b>		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>0.0</b>	<b>25</b>	<b>1.719</b>	<b>0.942</b>	<b>0.228</b>		<b>37</b>	<b>26</b>	<b>19</b>	<b>7</b>	<b>11</b>

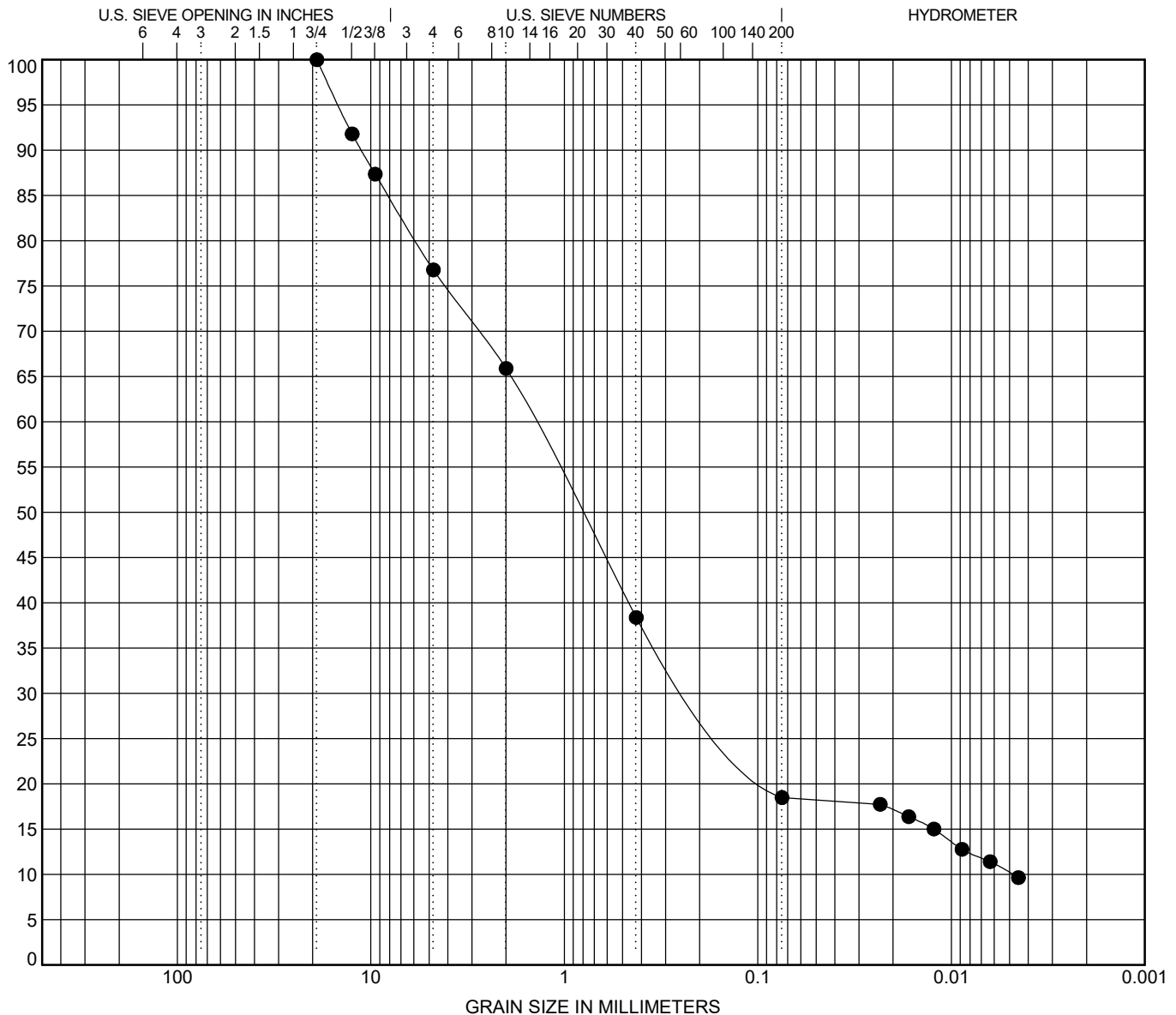


**CTL Engineering, Inc.**  
 2860 Fisher Road  
 Columbus, Ohio 43204  
 Telephone: 614-276-8123  
 Fax: 614-276-6377

### GRAIN SIZE DISTRIBUTION

Project: BEL-40-23.37  
 Location: BEL COUNTY  
 CTL Project Number:

CTL GRADATION - 2014 ODOT.GDT - 3/25/25 12:23 - O:\PROJECT\2024\MOR-05\24050050MOR\_OHIO DEPARTMENT OF TRANSPORTATION\_BEL-40-23-37 PID 114388LAB AND LOGS\GINT\24050050MOR.GPJ



COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>1.5</b>	<b>A-1-b(0)</b>	<b>12</b>	<b>NP</b>	<b>NP</b>	<b>NP</b>	<b>6.06</b>	<b>298.29</b>

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>1.5</b>	<b>19</b>	<b>1.435</b>	<b>0.817</b>	<b>0.205</b>	<b>0.005</b>	<b>34</b>	<b>28</b>	<b>20</b>	<b>8</b>	<b>10</b>

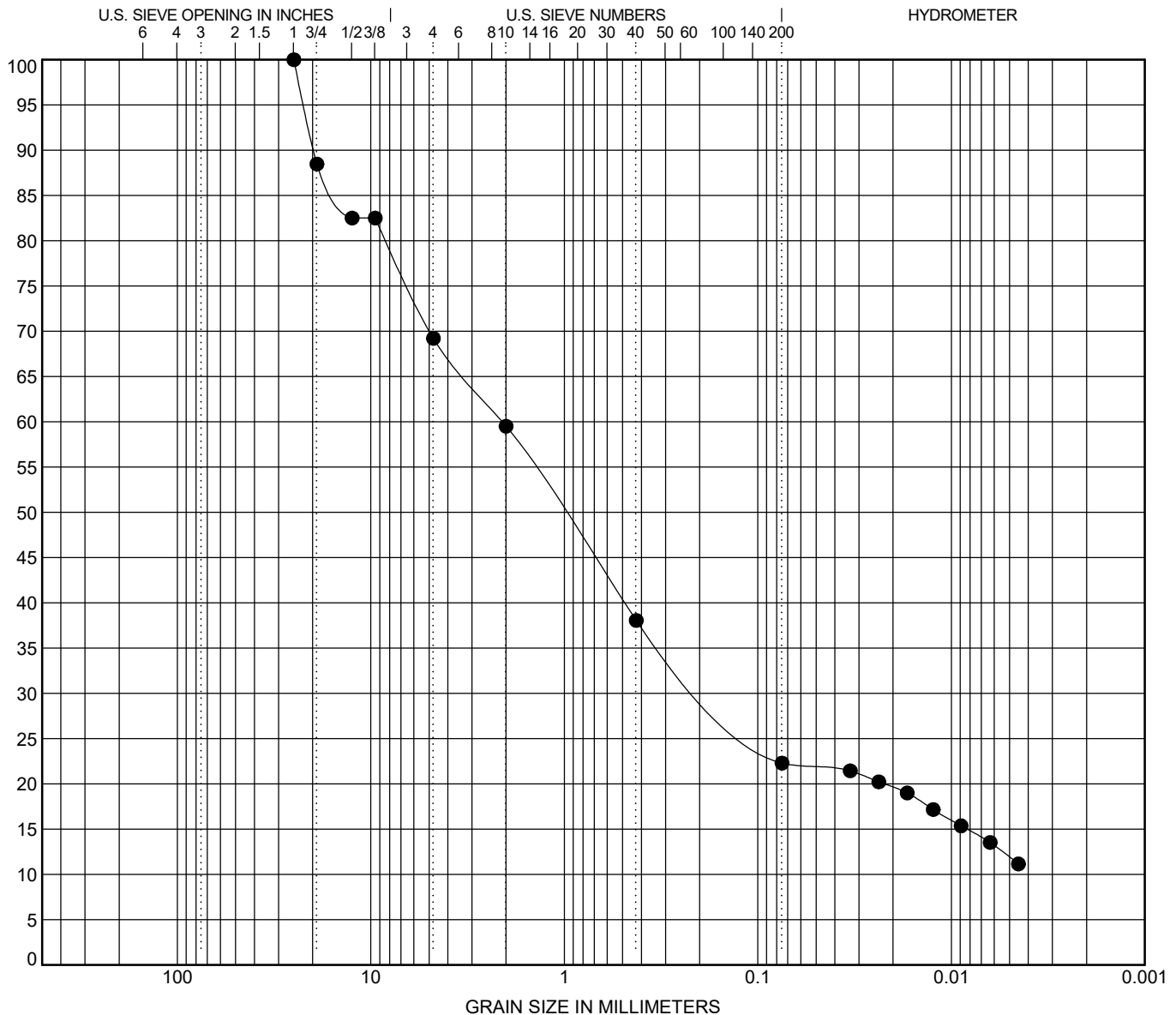


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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>4.5</b>	<b>A-1-b(0)</b>	<b>10</b>	<b>NP</b>	<b>NP</b>	<b>NP</b>		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>4.5</b>	<b>25</b>	<b>2.089</b>	<b>1.007</b>	<b>0.175</b>		<b>41</b>	<b>21</b>	<b>16</b>	<b>10</b>	<b>12</b>

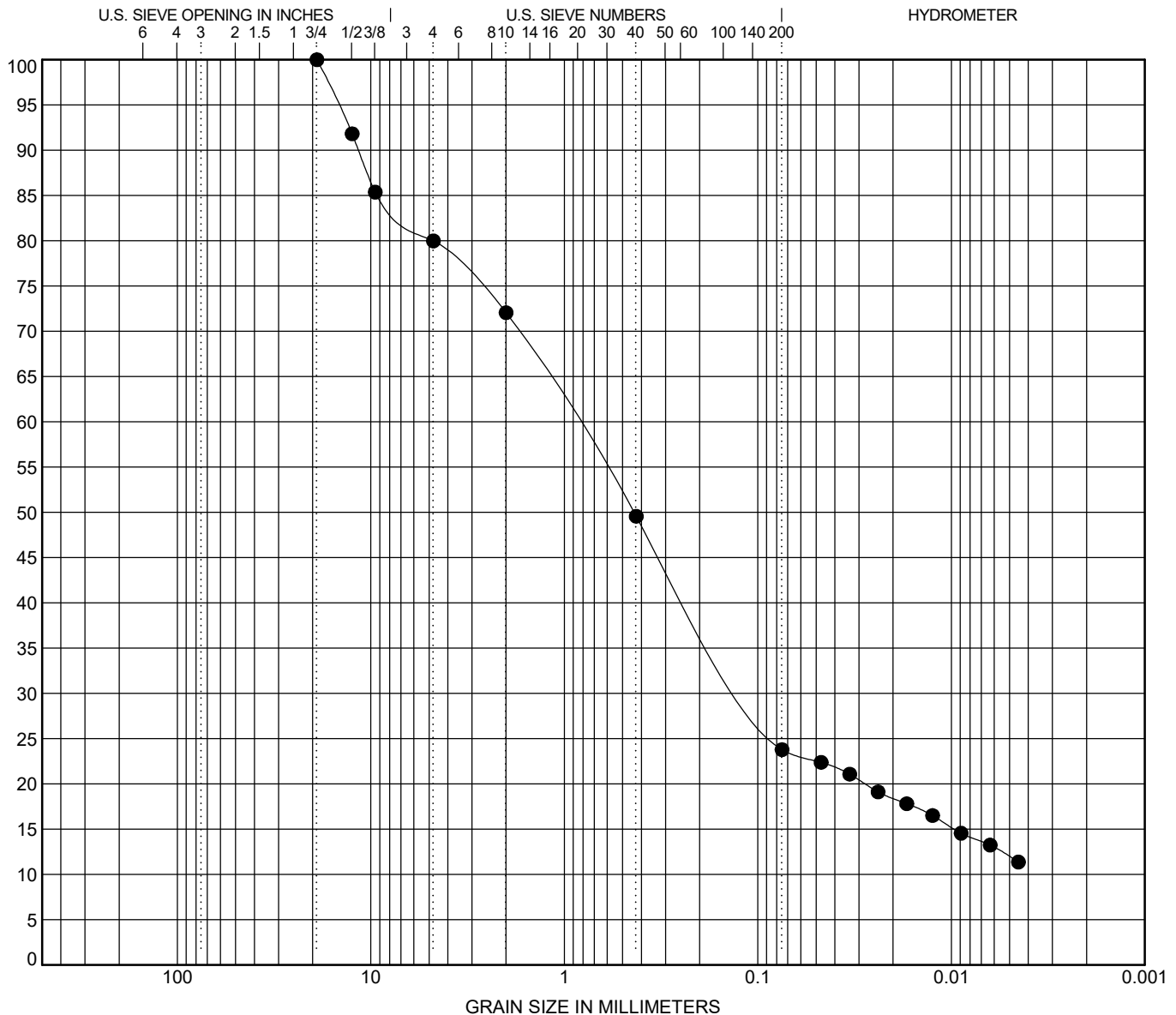


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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>6.0</b>	<b>A-1-b(0)</b>	<b>12</b>	<b>NP</b>	<b>NP</b>	<b>NP</b>		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>6.0</b>	<b>19</b>	<b>0.872</b>	<b>0.438</b>	<b>0.114</b>		<b>28</b>	<b>22</b>	<b>26</b>	<b>12</b>	<b>12</b>

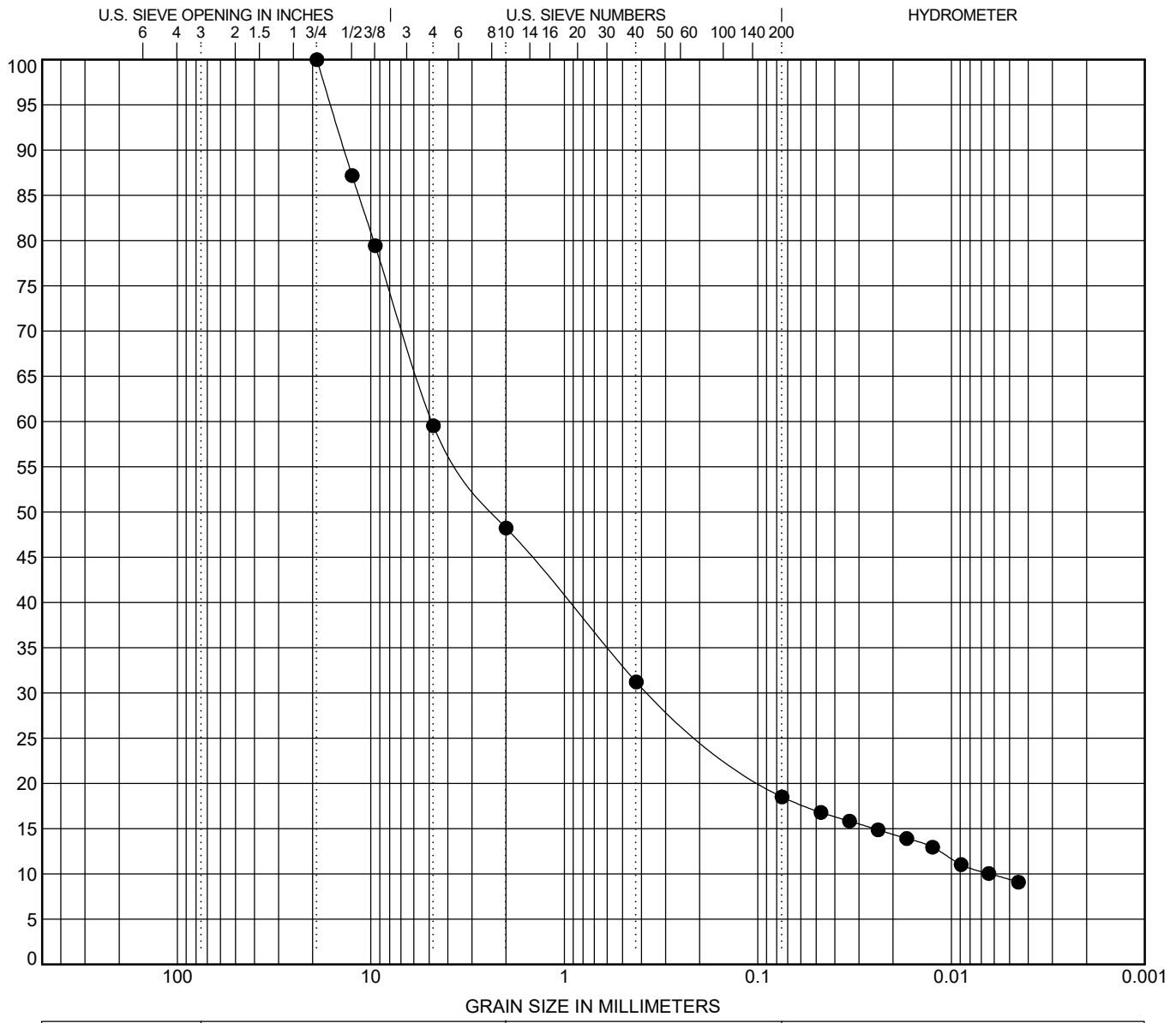


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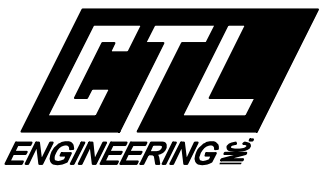
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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>7.5</b>	<b>A-1-b(0)</b>	<b>17</b>	<b>NP</b>	<b>NP</b>	<b>NP</b>	<b>4.27</b>	<b>767.73</b>

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>7.5</b>	<b>19</b>	<b>4.827</b>	<b>2.29</b>	<b>0.36</b>	<b>0.006</b>	<b>51</b>	<b>17</b>	<b>13</b>	<b>10</b>	<b>9</b>

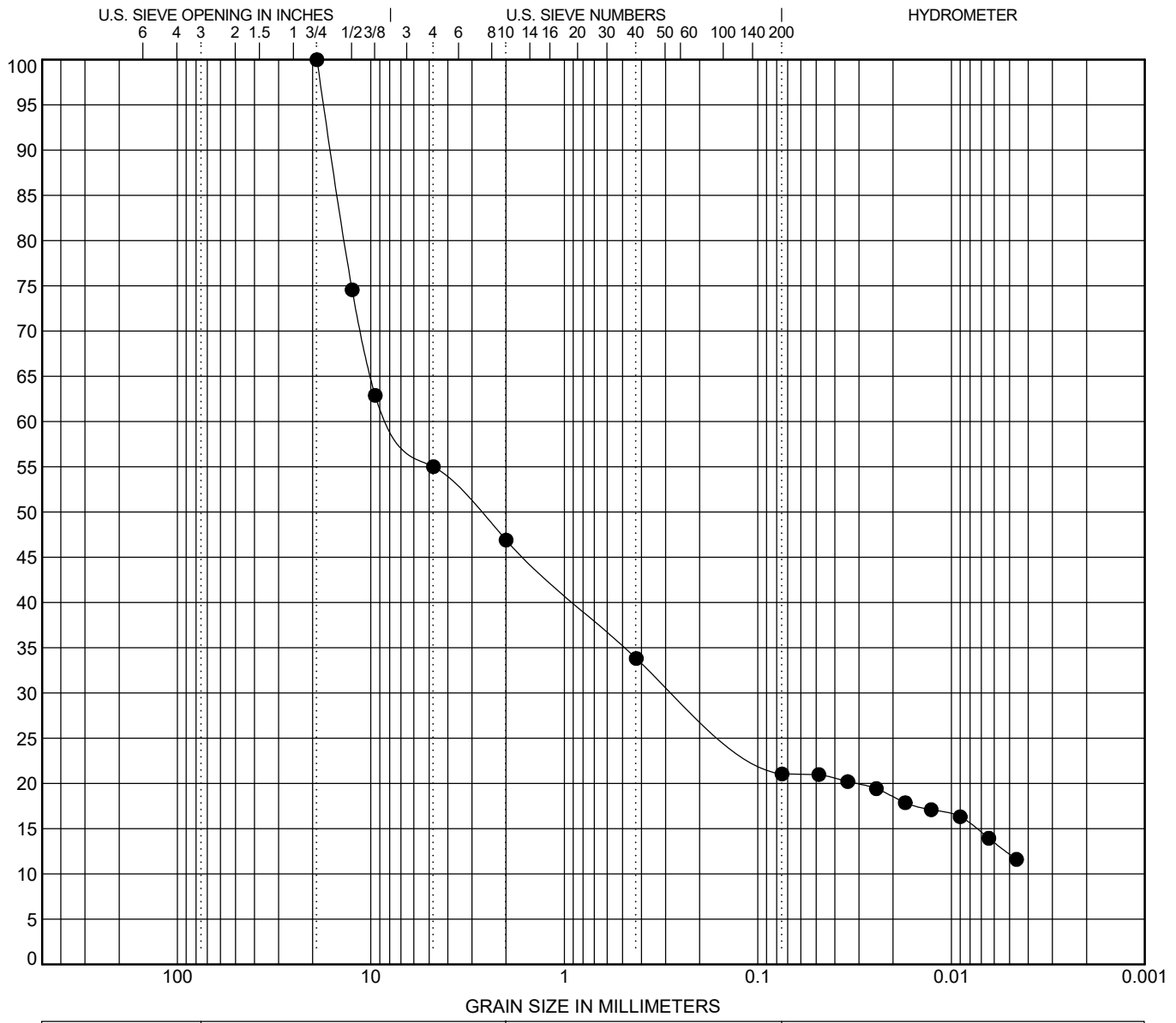


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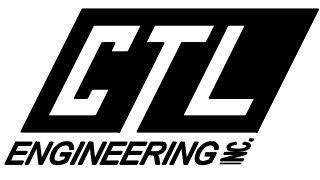
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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>9.0</b>	<b>A-1-b(0)</b>	<b>17</b>	<b>NP</b>	<b>NP</b>	<b>NP</b>		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>9.0</b>	<b>19</b>	<b>7.367</b>	<b>2.783</b>	<b>0.253</b>		<b>53</b>	<b>13</b>	<b>13</b>	<b>9</b>	<b>12</b>

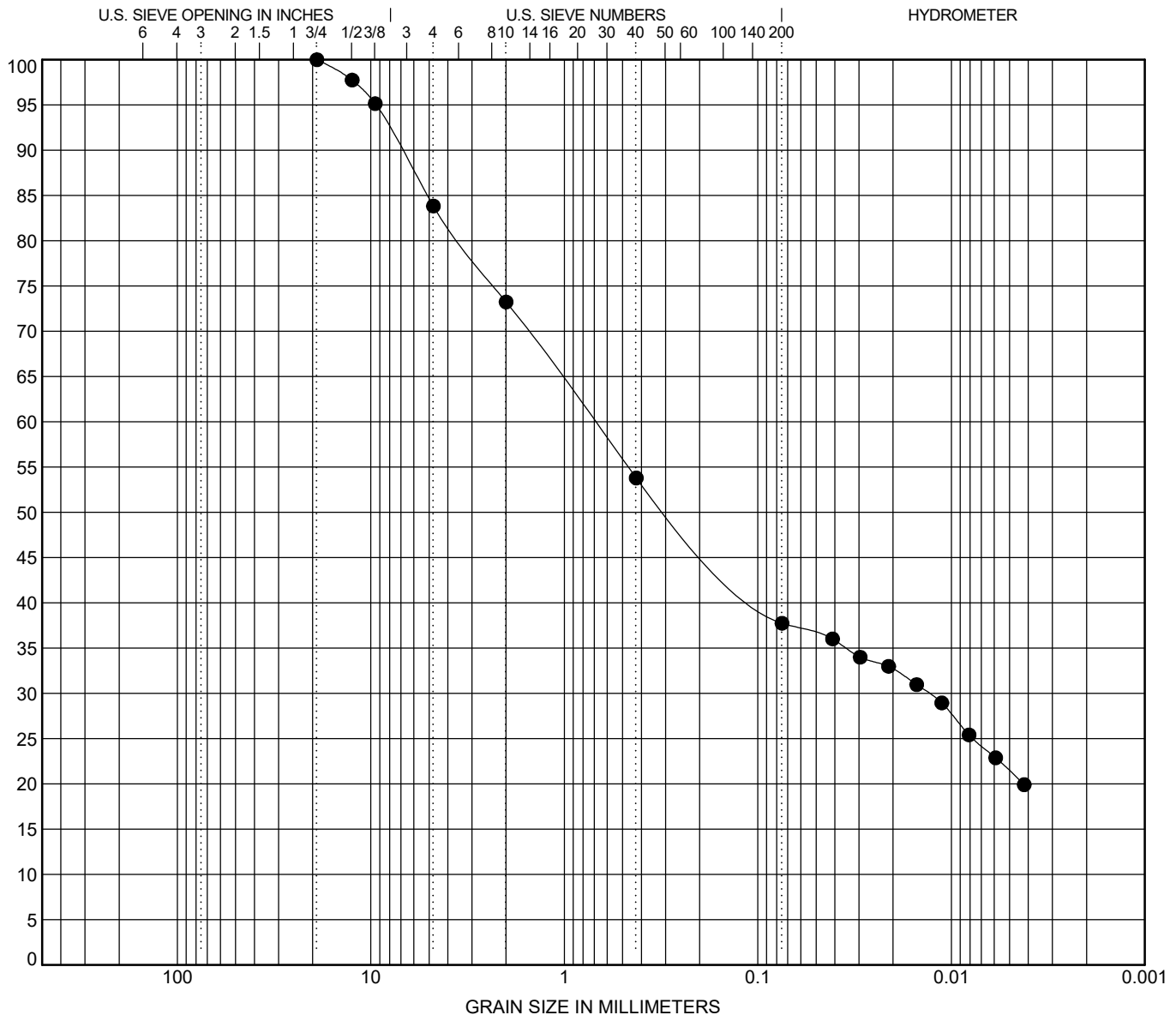


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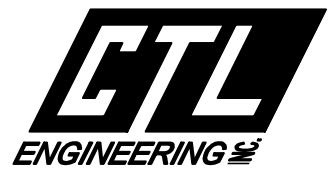
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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>10.5</b>	<b>A-6a(1)</b>	<b>16</b>	<b>32</b>	<b>20</b>	<b>12</b>		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>10.5</b>	<b>19</b>	<b>0.697</b>	<b>0.282</b>	<b>0.013</b>		<b>27</b>	<b>19</b>	<b>16</b>	<b>17</b>	<b>21</b>

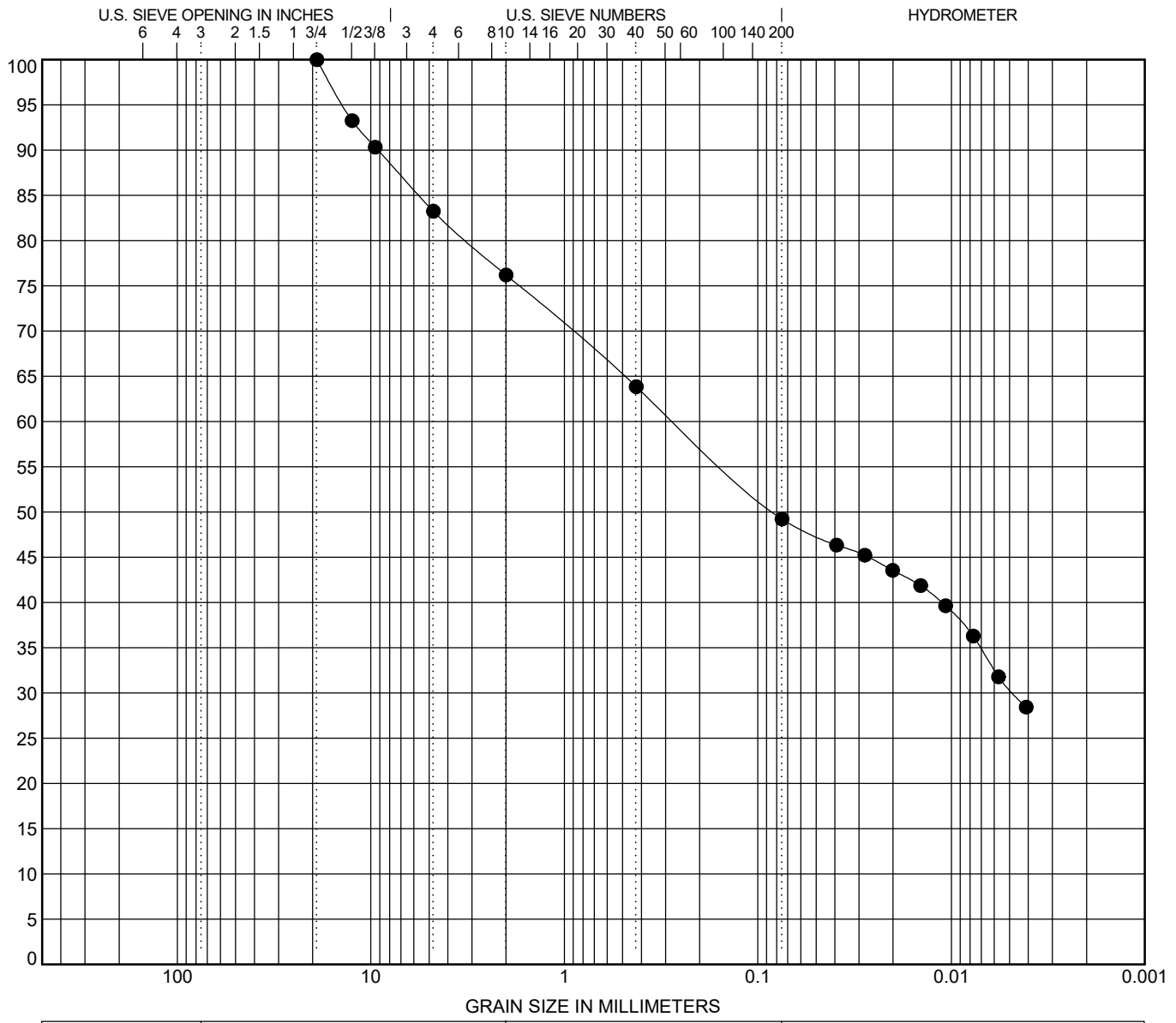


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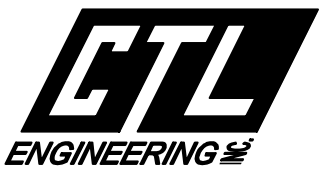
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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>12.0</b>	<b>A-6b(6)</b>	<b>13</b>	<b>40</b>	<b>20</b>	<b>20</b>		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>12.0</b>	<b>19</b>	<b>0.269</b>	<b>0.082</b>	<b>0.005</b>		<b>24</b>	<b>12</b>	<b>15</b>	<b>19</b>	<b>30</b>



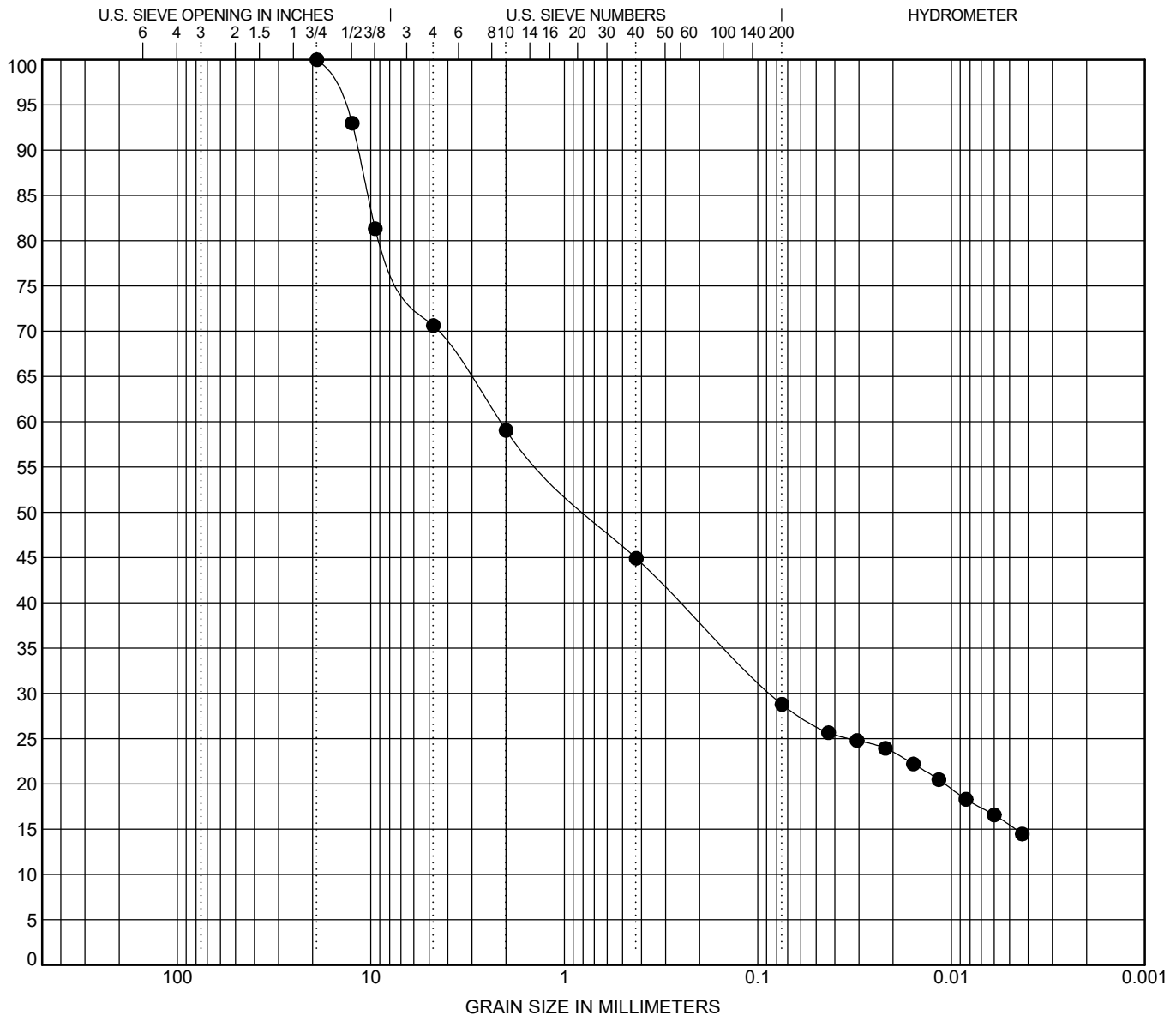
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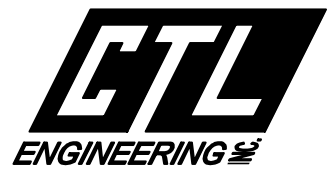
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COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>13.5</b>	<b>A-2-6(0)</b>	<b>15</b>	<b>28</b>	<b>16</b>	<b>12</b>		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>13.5</b>	<b>19</b>	<b>2.148</b>	<b>0.742</b>	<b>0.085</b>		<b>41</b>	<b>14</b>	<b>16</b>	<b>14</b>	<b>15</b>

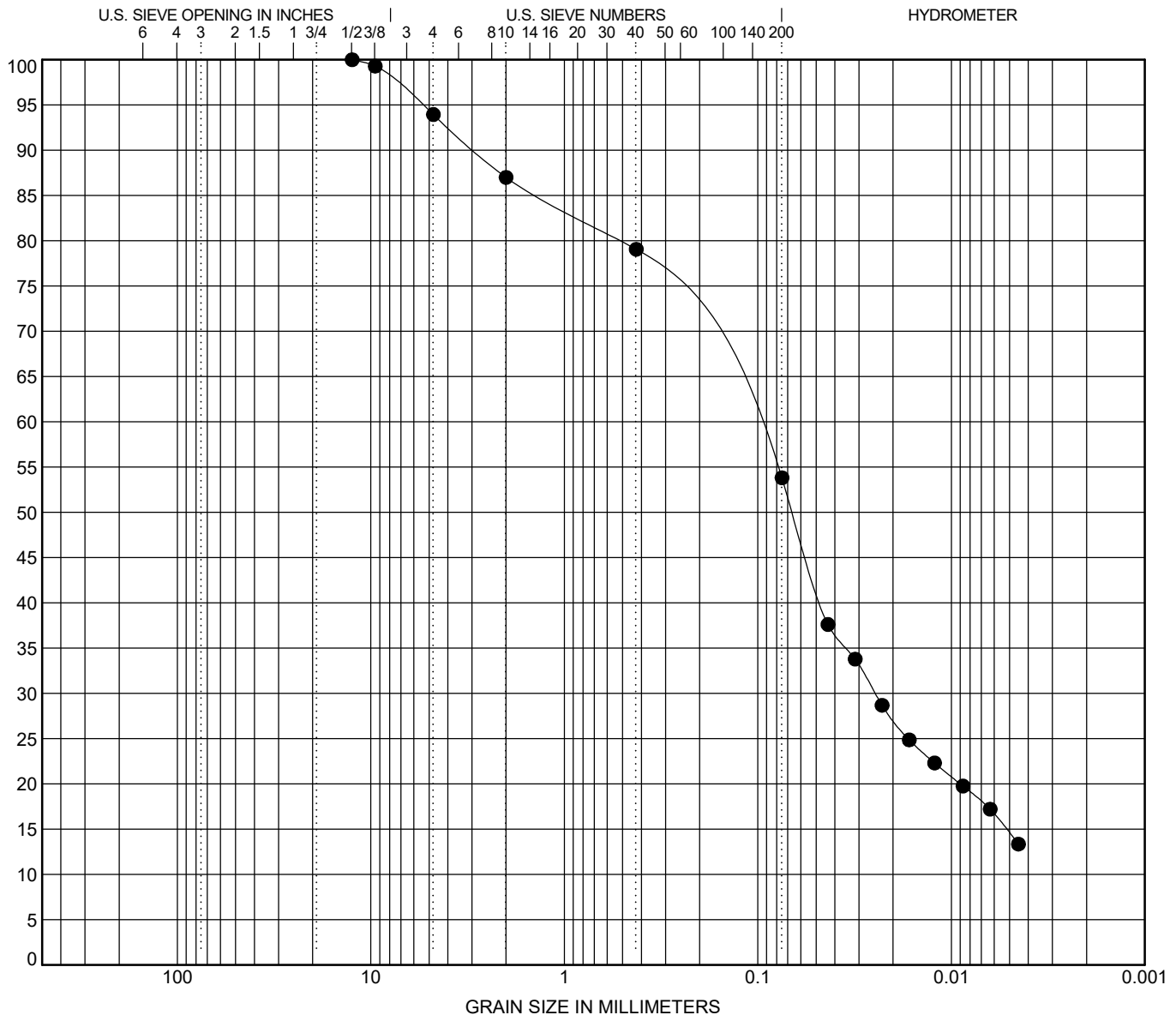


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 Columbus, Ohio 43204  
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 Fax: 614-276-6377

### GRAIN SIZE DISTRIBUTION

Project: BEL-40-23.37  
 Location: BEL COUNTY  
 CTL Project Number:

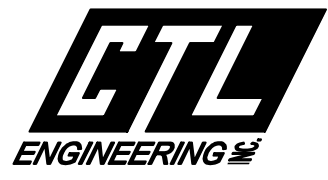
CTL GRADATION - 2014 ODOT.GDT - 3/25/25 12:23 - O:\PROJECT\2024\IMOR-05\24050050MOR\_05\DEPARTMENT OF TRANSPORTATION\_BEL-40-23-37 PID 114388\LAB AND LOGS\GINT\24050050MOR.GPJ



COBBLES	GRAVEL		SAND		SILT OR CLAY
	coarse	fine	coarse	fine	

Specimen Identification	Depth	Classification	MC	LL	PL	PI	Cc	Cu
<b>B-001-0-24</b>	<b>15.0</b>	<b>A-4a(0)</b>	<b>7</b>	<b>NP</b>	<b>NP</b>	<b>NP</b>		

Specimen Identification	Depth	D100	D60	D50	D30	D10	%Gravel	%Coarse Sand	%Fine Sand	%Silt	%Clay
<b>B-001-0-24</b>	<b>15.0</b>	<b>12.5</b>	<b>0.115</b>	<b>0.066</b>	<b>0.025</b>		<b>13</b>	<b>8</b>	<b>25</b>	<b>39</b>	<b>15</b>



**CTL Engineering, Inc.**  
 2860 Fisher Road  
 Columbus, Ohio 43204  
 Telephone: 614-276-8123  
 Fax: 614-276-6377

### GRAIN SIZE DISTRIBUTION

Project: BEL-40-23.37  
 Location: BEL COUNTY  
 CTL Project Number:

**Slake Durability of Shales and Similar Weak Rocks  
ASTM D 4644**

**CTL ENGINEERING, INC.**  
2860 Fisher Road Columbus, Ohio 43204

Sample ID: B-001-0-24, NQ2-1, 21.0'-26.0'

Sample Description: Shale, Gray

Slake Durability Index (%): 94.2  
(second cycle)  
Moisture Content (%): 1.8  
Temperature Range (°C): 18.4-20.8  
Temperature Average (°C): 19.6

Client: Ohio Department of Transportation  
Project: BEL-40-23.37, PID 114388

Project No. 24050050MOR  
Lab Code. 25050700COL  
Date Tested: 1/23/2025  
Reviewed by: JG



Pre-Test Sample



Post Test Sample

Remarks:

Post Test Sample Description : Type II—Retained specimen consist of large and small fragments.

**Slake Durability of Shales and Similar Weak Rocks  
ASTM D 4644**

**CTL ENGINEERING, INC.**  
2860 Fisher Road Columbus, Ohio 43204

Sample ID: B-001-0-24, NQ2-2, 26.0'-31.0'

Sample Description: Shale, Gray

Slake Durability Index (%): 89.6  
(second cycle)  
Moisture Content (%): 2.2  
Temperature Range (°C): 18.3-18.7  
Temperature Average (°C): 18.5

Client: Ohio Department of Transportation  
Project: BEL-40-23.37, PID 114388

Project No. 24050050MOR  
Lab Code. 25050700COL  
Date Tested: 1/23/2025  
Reviewed by: JG



Pre-Test Sample



Post Test Sample

Remarks:

Post Test Sample Description : Type II—Retained specimen consist of large and small fragments.

**Slake Durability of Shales and Similar Weak Rocks  
ASTM D 4644**

**CTL ENGINEERING, INC.**  
2860 Fisher Road Columbus, Ohio 43204

Sample ID: B-001-0-24, NQ2-3, 31.0'-36.0'

Sample Description: Shale, Gray

Slake Durability Index (%): 95.1  
(second cycle)  
Moisture Content (%): 2.2  
Temperature Range (°C): 18.9-20.7  
Temperature Average (°C): 19.8

Client: Ohio Department of Transportation  
Project: BEL-40-23.37, PID 114388

Project No. 24050050MOR  
Lab Code. 25050700COL  
Date Tested: 1/23/2025  
Reviewed by: JG



Pre-Test Sample



Post Test Sample

Remarks:

Post Test Sample Description : Type II—Retained specimen consist of large and small fragments.

PROJECT NO:	24050050MOR
DATE:	2/11/2025

**UNIAXIAL COMPRESSIVE STRENGTH OF  
INTACT ROCK CORE - ASTM D 7012**



Method C

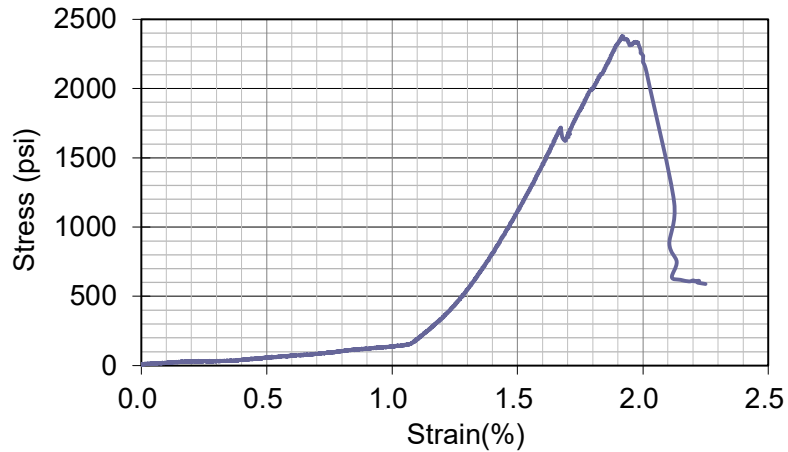
BORING NUMBER	B-001-0-24	TOP DEPTH(FT)	32.3	BOTTOM DEPTH(FT)	32.8
SAMPLE NUMBER	NQ2-3	DISTRICT	11	PID NO.	114388
COUNTY	BEL	ROUTE	40	SECTION	23.37



FORMATION	Conemaugh Group
DESCRIPTION	Shale, Gray, Moderately Weathered, Slightly Strong
MOISTURE CONDITION	As Received

MEASUREMENT	LENGTH(INCHES)	DIAMETER(INCHES)
1	4.026	1.975
2	4.033	1.975
3	4.025	1.976
AVERAGE	4.028	1.975

LENGTH/DIAMETER	2.0
CORRECTION FACTOR	1
AREA(IN <sup>2</sup> )	3.1
MASS (GRAMS)	535.6
UNIT WEIGHT(LBS/FT <sup>3</sup> )	165.3

RATE OF LOADING (in/min)	0.11
COMPRESSIVE STRENGTH (PSI)	2,380
Equip. ID - 68897	
NON-CONFORMANCES - None	
TIME OF TEST (MINUTES)	0.87
LOADING DIRECTION	PERP. TO BEDDING
TECHNICIAN - MW	
TEMPERATURE - Room	



 <p>BEFORE TESTING</p>	 <p>AFTER TESTING</p>
<p align="center">Physical Appearance after Test - Sample sheared through middle portion - No signs of cracking, spalling or shearing at the platen-specimen interface</p>	

PROJECT NO:	24050050MOR
DATE:	2/11/2025

## UNIAXIAL COMPRESSIVE STRENGTH OF INTACT ROCK CORE - ASTM D 7012



Method C

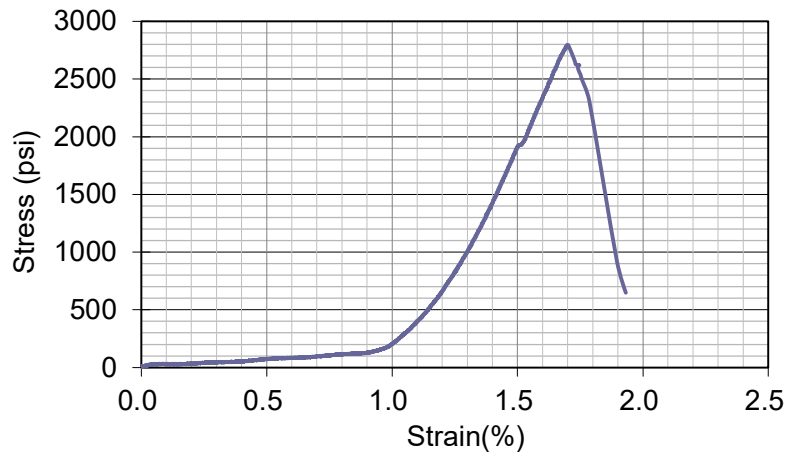
BORING NUMBER	B-001-0-24	TOP DEPTH(FT)	36.4	BOTTOM DEPTH(FT)	36.9
SAMPLE NUMBER	NQ2-4	DISTRICT	11	PID NO.	114388
COUNTY	BEL	ROUTE	40	SECTION	23.37



FORMATION	Conemaugh Group
DESCRIPTION	Shale, Gray, Moderately Weathered, Slightly Strong
MOISTURE CONDITION	As Received

MEASUREMENT	LENGTH(INCHES)	DIAMETER(INCHES)
1	4.010	1.984
2	4.007	1.983
3	4.004	1.984
AVERAGE	4.007	1.984

LENGTH/DIAMETER	2.0
CORRECTION FACTOR	1
AREA(IN <sup>2</sup> )	3.1
MASS (GRAMS)	524.3
UNIT WEIGHT(LBS/FT <sup>3</sup> )	161.3

RATE OF LOADING (in/min)	0.10
COMPRESSIVE STRENGTH (PSI)	2,790
Equip. ID - 68897	
NON-CONFORMANCES - None	
TIME OF TEST (MINUTES)	0.85
LOADING DIRECTION	PERP. TO BEDDING
TECHNICIAN - MW	
TEMPERATURE - Room	



	
BEFORE TESTING	AFTER TESTING
Physical Appearance after Test - Sample sheared through middle portion - No signs of cracking, spalling or shearing at the platen-specimen interface	

PROJECT NO:	24050050MOR
DATE:	2/11/2025

## UNIAXIAL COMPRESSIVE STRENGTH OF INTACT ROCK CORE - ASTM D 7012



Method C

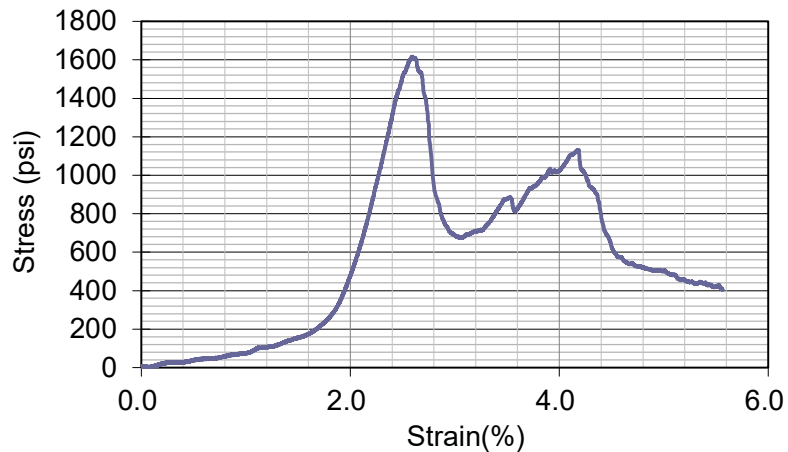
BORING NUMBER	B-001-0-24	TOP DEPTH(FT)	44.1	BOTTOM DEPTH(FT)	44.5
SAMPLE NUMBER	NQ2-5	DISTRICT	11	PID NO.	114388
COUNTY	BEL	ROUTE	40	SECTION	23.37

FORMATION	Conemaugh Group
DESCRIPTION	Claystone, Brown & Gray, Highly Weathered, Slightly Strong
MOISTURE CONDITION	As Received

MEASUREMENT	LENGTH(INCHES)	DIAMETER(INCHES)
1	4.029	1.963
2	4.024	1.968
3	4.025	1.965
AVERAGE	4.026	1.965

LENGTH/DIAMETER	2.0
CORRECTION FACTOR	1
AREA(IN <sup>2</sup> )	3.0
MASS (GRAMS)	505.8
UNIT WEIGHT(LBS/FT <sup>3</sup> )	157.8

RATE OF LOADING (in/min)	0.12
COMPRESSIVE STRENGTH (PSI)	1,620
Equip. ID - 68897	
NON-CONFORMANCES - None	
TIME OF TEST (MINUTES)	1.94
LOADING DIRECTION	PERP. TO BEDDING
TECHNICIAN - MW	
TEMPERATURE - Room	



		
BEFORE TESTING		AFTER TESTING
Physical Appearance after Test - Sample sheared through middle portion - No signs of cracking, spalling or shearing at the platen-specimen interface		



**B-001-0-24    Box # 1**



Run #:	Depth:		Recovery		RQD	
NQ2-1	21.0'	26.0'	2.5/5.0	50%	0/5.0	0%
NQ2-2	26.0'	31.0'	2.75/5.0	55%	0/5.0	0%

24050050MOR – BEL-40-23.27

**B-001-0-24    Box # 2**



Run #:	Depth:		Recovery		RQD	
NQ2-3	31.0'	36.0'	5.0/5.0	100%	3.58/5.0	72%
NQ2-4	36.0'	41.0'	5.0/5.0	100%	1.33/5.0	27%

24050050MOR – BEL-40-23.27



**B-001-0-24    Box # 3**



Run #:	Depth:		Recovery		RQD	
NQ2-5	41.0'	46.0'	5.0/5.0	100%	2.33/5.0	47%

24050050MOR – BEL-40-23.27

### Summary of Soil Scour Data

#### BEL-40-23.37 Bridge - Scour Analysis

Boring No.	Sample	Elevation (ft)	D <sub>50</sub> (mm)	τ <sub>c</sub> (psf)	D <sub>50, equiv</sub> (mm)	Erosion Category (EC)
B-001-0-24	SS-1	715.2-716.7	0.942	0.0197	0.9420	2.1689
	SS-2	713.7-715.2	0.817	0.0171	0.8170	2.0947
	SS-4	710.7-712.2	1.007	0.0210	1.0070	2.2036
	SS-5	709.2-710.7	0.438	0.0091	0.4380	1.7698
	SS-6	707.7-709.2	2.29	0.0478	2.2900	2.6318
	SS-7	706.2-707.7	2.783	0.0581	2.7830	2.7334
	SS-8	704.7-706.2	0.282	0.0804	3.8504	3.1680
	SS-9	703.2-704.7	0.082	0.4233	20.2654	3.7247
	SS-10	701.7-703.2	0.742	0.0573	2.7445	2.0445
	SS-11	700.2-701.7	0.2	0.2293	10.9810	1.3612



**Summary of Bedrock Scour Data**

Boring ID	Sample ID	Sample Elevation (Ft)	Erodibility Index (K)	$\tau_c$ Value (psf)	$D_{50, equiv}$ (mm)	Erosion Category
B-001-0-24	SS-12 to SS-14	695.7-700.2	0.01	0.6	30.9	3.77
B-001-0-24	NQ2-1&2	685.7-695.7	1.03	5.4	257.4	3.77
B-001-0-24	NQ2-3&4	679.3-685.7	678.26	137.7	6591.9	3.98
B-001-0-24	NQ2-4&5	670.7-679.3	115.42	56.8	2719.2	3.77

## DESIGN MEMORANDUM

To: OODT Dist 11  
 Copy:  
 From: CTL Engineering, Inc.  
 Date: March 25, 2025  
 Subject: BEL-40-23.37 PID 114388; Rock Scour Assessment

At your request, CTL Engineering, Inc. has completed drilling and sampling operations for the referenced project. It is our understanding that the near surface bedrock will be interacting with the proposed foundational elements and rock scour is a concern. The following is the assessment of the encountered bedrock conditions relative to the geotechnical explorations:

Boring Evaluated:	B-001-0-24
Boring Location:	Adjacent to Pier, Sta. 205+80, 1' Lt.
Ground Elevation (ft):	716.7
Bedrock Elevation (ft):	700.2
Bedrock Age:	Pennsylvanian
Bedrock Description:	Claystone, Severely Weathered (Augered)

Testing Characteristics	BDM Threshold Value	Result	Scour Resistant Property
Unconfined Compressive Strength (ASTM D 7012C) (ASTM D 7012C)	$Q_u \geq 2,500$ psi	76.51 psi 0.53 MPa	NO
Slake Durability Index [Id <sub>2</sub> ]: (ASTM D4644)	SDI $\geq 90\%$	0.0 %	NO
Rock Quality Designation: (SGE Section 6)	RQD $\geq 65\%$	0	NO
Total Unit Weight (pcf):	$\gamma_{tot} \geq 150$ pcf	135 pcf	NO
Rock Mass Rating:	RMR $\geq 75$	32	NO
Geological Strength Index (GSI):	GSI $\geq 75$	20	NO
GSI Structure:	Massive or Blocky	Laminated	NO
GSI Surface Conditions:	Very Good or Good	Fair	NO
Erodibility Index [K]: FHWA-HIF-12-003 (HEC18)	K $\geq 100$	0.01	NO
Rock Joint Set Number [J <sub>n</sub> ]:	J <sub>n</sub> $\leq 5$	1.5	YES
Joint Roughness Number [J <sub>r</sub> ]:	J <sub>r</sub> $\geq 1$	1.5	YES
Joint Alteration Number [J <sub>a</sub> ]:	J <sub>a</sub> $\leq 5$	4	YES
Relative Joint Orientation [J <sub>s</sub> ]:	J <sub>s</sub> $\geq 0.4$	1	YES
Does bedrock meet criteria of scour resistant per BDM:		<b>NO</b>	

Critical Shear Stress ( $\tau_c$ ) \* =  $\rho (1000 K^{0.75} / 7.853 \rho)^{2/3}$

30.9	Pa
0.6	psf

## DESIGN MEMORANDUM

$$\text{Calculated } D_{50} \text{ equivalent} = \boxed{30.9} \text{ mm } \boxed{1.218} \text{ in}$$

$$\text{Calculated Erosion Category (EC)} = \boxed{3.77}$$

### CALCULATIONS

$$K = (M_s)(K_b)(K_d)(J_s) \quad K = \boxed{0.01}$$

Where:  $M_s$  = Intact Rock Strength Parameter

$$\text{From Testing: } Q_u = \boxed{\phantom{000}} \text{ psi}$$

$$Q_u = \boxed{\phantom{000}} \text{ MPa}$$

$$M_s = Q_u \text{ for } Q_u \geq 10 \text{ MPa}$$

$$(0.78) Q_u^{1.05} \text{ for } Q_u < 10 \text{ MPa}$$

See Last sheet for  $Q_u$  Determination

$$Q_u = \boxed{76.51} \text{ psi}$$

$$Q_u = \boxed{0.53} \text{ MPa}$$

$$M_s = \boxed{0.40}$$

Where:  $K_b$  = Block Size Parameter

$$K_b = RQD/J_n \geq 0.10$$

$$RQD = \boxed{0}$$

$$J_n = \boxed{1.5} \leq 5.0$$

$$K_b = \boxed{0.10} \geq 0.1$$

Where:  $K_d$  = Shear Strength Parameter

$$K_d = J_r/J_a$$

$$J_r = \boxed{1.5} \geq 1.0$$

$$J_a = \boxed{4} \leq 5.0$$

$$K_d = \boxed{0.38} \geq 0.2$$

Where:  $J_s$  = Relative Orientation Parameter

$$J_s = \boxed{1.00} \geq 0.4$$

$$\text{Average Joint Spacing} = \boxed{2} \text{ inches } \boxed{50.8} \text{ mm}$$

**Re-arrange HEC-18 Equations 7.38 for 'Critical Stream Power' and 7.39 'Approach Flow Stream Power' to derive the critical shear stress for non-scour resistant bedrock as follows:**

$$\text{Critical Shear Stress } (\tau_c)^* = \rho (1000 K^{0.75} / 7853 \rho)^{2/3} \boxed{30.9} \text{ Pa}$$

# DESIGN MEMORANDUM

Where:  $\tau_c$  = Critical shear stress (Pa)  
 $\rho$  = Mass density of water (1000 kg/m<sup>3</sup>)  
 K = Erodibility Index (dim.)

Erosion Category (EC) =  $1.2(1.83333 + \text{Log}(S_v/2.5))$

EC = 3.77

## REFERENCES

Table 4.20: Geomechanics Rating Adjustment for Joint Orientations (after AASHTO 2010)

Orientation of Joints		Very Favorable	Favorable	Fair	Unfavorable	Very Unfavorable
Rating	Tunnels	0	-2	-5	-10	-12
	Foundations	0	-2	-7	-15	-25
	Slopes	0	-5	-25	-50	-60

Table 4.21: Geomechanics Rock Mass Classes Determined From Total Ratings (AASHTO 2010)

RMR (Note 1)	100 to 81	80 to 61	69 to 41	41 to 21	≤20
Class No.	I	II	III	IV	V
Description	Very Good Rock	Good Rock	Fair Rock	Poor Rock	Very Poor Rock

Table 4.23. Rock Joint Set Number  $J_n$

Number of Joint Sets	Joint Set Number ( $J_n$ )
Intact, no or few joints/fissures	1.00
One joint/fissure set	1.22
One joint/fissure set plus random	1.50
Two joint/fissure sets	1.83
Two joint/fissure sets plus random	2.24
Three joint/fissure sets	2.74
Three joint/fissure sets plus random	3.34
Multiple joint/fissure sets	4.09
Multiple joint/fissure sets	5.00

Table 4.24. Joint Roughness Number  $J_r$

Table 4.25. Joint Alteration Number  $J_a$

Condition of Joint	Joint Roughness Number ( $J_r$ )	Description of Gouge	Alteration Number ( $J_a$ )		
			1.0 <sup>{1}</sup>	2.0 - 5.0 <sup>{2}</sup>	5.0 <sup>{3}</sup>
Stepped Joint/fissures	4.0	Tightly healed, hard, non-softening impermeable	0.75	---	---
Rough or irregular, undulating	3.0	Unaltered joint walls, surface staining only	1.0	---	---
Smooth undulating	2.0	Slightly altered, non-softening, non-cohesive rock mineral or crushed rock infilling	2.0	2.0	4.0
Slickensided undulating	1.5	Non-softening, slightly clayey non-cohesive filling	3.0	6.0	10.0
Smooth planar	1.0	Non-softening, strongly over-consolidated clay mineral filling, with or without crushed rock	3.0	6.0 **	10.0
Slickensided planar	0.5	Softening or low friction clay mineral coatings and small quantities of swelling clays	4.0	8.0	13.0



## DESIGN MEMORANDUM

Joint/fissures either open or containing relatively soft gouge of sufficient thickness to prevent joint/fissure wall contact upon excavation	1.0	Softening moderately over-consolidated clay mineral filling, with or without crushed rock	4.0	8.0 **	13.0
		Shattered or micro-shattered (swelling) clay gouge, with or without crushed rock	5.0	10.0	18.0
Shattered or micro-shattered clay	1.0	{1} Joint walls effectively in contact {2} Joint walls come into contact after approximately 100-mm of shear {3} Joint walls do not come into contact at all upon shear ** Also applies when crushed rock occurs in clay gouge without rock wall contact			

### AASHTO LRFD Bridge Design Specifications, 6th Ed. (AASHTO 2012)

Table 10.4.6.4-1: Geomechanics Classification of Rock Masses (AASHTO 2012)

Parameter		Range of Values							Score	
1	Strength of intact rock material	Point Load Strength Index	> 175 ksf	85-175 ksf	45-85 ksf	20-45 ksf	For this low range, uniaxial compressive strength is preferred			0
		Uniaxial Compressive Strength	> 4320 ksf	2160-4320 ksf	1080-2160 ksf	520-1080 ksf	215-520 ksf	70-215 ksf	20-7 ksf	
	Relative Rating	15	12	7	4	2	1	0		
2	Drill core quality (RQD)	90-100%	75-90%	50-75%	25-50%	<25%			3	
	Relative Rating	20	17	13	8	3				
3	Spacing of Joints	>10 ft.	3-10 ft.	1-3 ft.	2 in - 1 ft.	<2in.			10	
	Relative Rating	30	25	20	10	5				
4	Conditions of Joints	<ul style="list-style-type: none"> <li>• Very rough surfaces</li> <li>• Not continuous</li> <li>• No Separation</li> <li>• Hard joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slightly rough surfaces</li> <li>• Separation &lt;0.05 in.</li> <li>• Hard joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slightly rough surface</li> <li>• Separation &lt;0.05 in.</li> <li>• Soft joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slickenside surface</li> <li>• Gouge &lt;0.2in thick</li> <li>• Joints open 0.05 - 0.2 in.</li> <li>• Continuous Joints</li> </ul>	<ul style="list-style-type: none"> <li>• Soft gouge &gt;0.2 in.</li> <li>• Joints open &gt;0.2 in.</li> <li>• Continuous Joints</li> </ul>			12	
		Relative Rating	25	20	12	6				0
5	Groundwater conditions (for scour only use the General Conditions and either Moist or Completely Dry)	Completely Dry	Moist only (interstitial water)		Water under moderate pressure	Severe water problems		7		
	Relative Rating	10	7		4	0				
Note: 1 MPa = 145 psi 1 psi = 0.00689 Mpa 1 psi = 0.144 ksf		<b>Rock Mass Rating</b>							<b>32</b>	



## DESIGN MEMORANDUM

Bedrock Scour Samples						
Boring ID	Sample ID	Sample Elevation (Ft)	Erodibility Index (K)	$\tau_c$ Value (psf)	$D_{50,equiv}$ (mm)	Erosion Category
B-001-0-24	SS-12to14	695.7-700.2	0.01	0.6	30.9	3.77

Slake Durability Index [ $Id_2$ ] = 0% - Estimated from GDM Table 400-5

Total Unit Weight = 135 pcf - Estimated from GDM Table 400-5

### Qu Determination

Sample	$N_{60}$	Nrate	Qu (ksf)	Qu (psi)
SS-12	35		4.375	30.38
SS-13	41		5.125	35.59
SS-14	50/2"	300	23.55	163.56
			Qu Avg =	76.51 psi
			Qu Avg =	0.53

For SS-12 & SS-13,  $Qu = N_{60} * 125 / 1000$

For SS-14, Qu Based on SPT (Stark et. al. 2017)

Nrate            300.0

ER =              76.8

$N_{90}$  =           256.0 bpf

Qu =              23.55 ksf

Qu =              163.56 psi

## DESIGN MEMORANDUM

To: OODT Dist 11  
 Copy:  
 From: CTL Engineering, Inc.  
 Date: March 25, 2025  
 Subject: BEL-40-23.37 PID 114388; Rock Scour Assessment

At your request, CTL Engineering, Inc. has completed drilling and sampling operations for the referenced project. It is our understanding that the near surface bedrock will be interacting with the proposed foundational elements and rock scour is a concern. The following is the assessment of the encountered bedrock conditions relative to the geotechnical explorations:

Boring Evaluated:	B-001-0-24
Boring Location:	Adjacent to Pier, Sta. 205+80, 1' Lt.
Ground Elevation (ft):	716.7
Bedrock Elevation (ft):	695.7
Bedrock Age:	Pennsylvanian
Bedrock Description:	Shale, Highly Weathered, Slightly Strong

Testing Characteristics	BDM Threshold Value	Result	Scour Resistant Property
Unconfined Compressive Strength (ASTM D 7012C) (ASTM D 7012C)	$Q_u \geq 2,500$ psi	1500 psi 10.34 MPa	NO
Slake Durability Index [ $I_{d2}$ ]: (ASTM D4644)	SDI $\geq 90\%$	89.6 -94.20%	NO
Rock Quality Designation: (SGE Section 6)	RQD $\geq 65\%$	0	NO
Total Unit Weight (pcf):	$\gamma_{tot} \geq 150$ pcf	155 pcf	YES
Rock Mass Rating:	RMR $\geq 75$	34	NO
Geological Strength Index (GSI):	GSI $\geq 75$	35	NO
GSI Structure:	Massive or Blocky	Blocky Disturbed	NO
GSI Surface Conditions:	Very Good or Good	Fair	NO
Erodibility Index [K]: FHWA-HIF-12-003 (HEC18)	$K \geq 100$	1.03	NO
Rock Joint Set Number [ $J_n$ ]:	$J_n \leq 5$	1.5	YES
Joint Roughness Number [ $J_r$ ]:	$J_r \geq 1$	2	YES
Joint Alteration Number [ $J_a$ ]:	$J_a \leq 5$	2	YES
Relative Joint Orientation [ $J_s$ ]:	$J_s \geq 0.4$	1	YES
Does bedrock meet criteria of scour resistant per BDM:		<b>NO</b>	

Critical Shear Stress ( $\tau_c$ ) \* =  $\rho (1000 K^{0.75} / 7.853 \rho)^{2/3}$

257.4	Pa psf
5.4	

## DESIGN MEMORANDUM

$$\text{Calculated } D_{50} \text{ equivalent} = \boxed{257.4} \text{ mm } \boxed{10.13} \text{ in}$$

$$\text{Calculated Erosion Category (EC)} = \boxed{3.77}$$

### CALCULATIONS

$$K = (M_s)(K_b)(K_d)(J_s) \quad K = \boxed{1.03}$$

Where:  $M_s$  = Intact Rock Strength Parameter

Est. GDM Table 400-6 :  $Q_u = \boxed{1500}$  psi  
 $Q_u = \boxed{10.34}$  MPa

$$M_s = \begin{cases} Q_u & \text{for } Q_u \geq 10 \text{ MPa} \\ (0.78) Q_u^{1.05} & \text{for } Q_u < 10 \text{ MPa} \end{cases}$$

Based on SPT (Stark et. al. 2017)

Where:  $Q_u$  (ksf) =  $0.092 \times N_{90}$

$$Q_u = \boxed{0.00} \text{ psi}$$

$$Q_u = \boxed{0.00} \text{ MPa}$$

$$N_{90} = \boxed{\phantom{000}}$$

$$M_s = \boxed{10.34}$$

Where:  $K_b$  = Block Size Parameter

$$K_b = RQD/J_n \geq 0.10$$

$$RQD = \boxed{0}$$

$$J_n = \boxed{1.5} \leq 5.0$$

$$K_b = \boxed{0.10} \geq 0.1$$

Where:  $K_d$  = Shear Strength Parameter

$$K_d = J_r/J_a$$

$$J_r = \boxed{2} \geq 1.0$$

$$J_a = \boxed{2} \leq 5.0$$

$$K_d = \boxed{1.00} \geq 0.2$$

Where:  $J_s$  = Relative Orientation Parameter

$$J_s = \boxed{1.00} \geq 0.4$$

$$\text{Average Joint Spacing} = \boxed{2} \text{ inches } \boxed{50.8} \text{ mm}$$

**Re-arrange HEC-18 Equations 7.38 for 'Critical Stream Power' and 7.39 'Approach Flow Stream Power' to derive the critical shear stress for non-scour resistant bedrock as follows:**

$$\text{Critical Shear Stress } (\tau_c)^* = \rho (1000 K^{0.75} / 7853 \rho)^{2/3} \boxed{257.4} \text{ Pa}$$

## DESIGN MEMORANDUM

Where:  $\tau_c$  = Critical shear stress (Pa)  
 $\rho$  = Mass density of water (1000 kg/m<sup>3</sup>)  
 K = Erodibility Index (dim.)

Erosion Category (EC) =  $1.2(1.83333 + \text{Log}(S_v/2.5))$

EC = 3.77

### REFERENCES

Table 4.20: Geomechanics Rating Adjustment for Joint Orientations (after AASHTO 2010)

Orientation of Joints		Very Favorable	Favorable	Fair	Unfavorable	Very Unfavorable
Rating	Tunnels	0	-2	-5	-10	-12
	Foundations	0	-2	-7	-15	-25
	Slopes	0	-5	-25	-50	-60

Table 4.21: Geomechanics Rock Mass Classes Determined From Total Ratings (AASHTO 2010)

RMR (Note 1)	100 to 81	80 to 61	69 to 41	41 to 21	≤20
Class No.	I	II	III	IV	V
Description	Very Good Rock	Good Rock	Fair Rock	Poor Rock	Very Poor Rock

Table 4.23. Rock Joint Set Number  $J_n$

Number of Joint Sets	Joint Set Number ( $J_n$ )
Intact, no or few joints/fissures	1.00
One joint/fissure set	1.22
One joint/fissure set plus random	1.50
Two joint/fissure sets	1.83
Two joint/fissure sets plus random	2.24
Three joint/fissure sets	2.74
Three joint/fissure sets plus random	3.34
Multiple joint/fissure sets	4.09
Multiple joint/fissure sets	5.00

Table 4.24. Joint Roughness Number  $J_r$

Condition of Joint	Joint Roughness Number ( $J_r$ )
Stepped Joint/fissures	4.0
Rough or irregular, undulating	3.0
Smooth undulating	2.0
Slickensided undulating	1.5
Smooth planar	1.0
Slickensided planar	0.5

Table 4.25. Joint Alteration Number  $J_a$

Description of Gouge	1.0 <sup>{1}</sup>	2.0 - 5.0 <sup>{2}</sup>	5.0 <sup>{3}</sup>
Tightly healed, hard, non-softening impermeable	0.75	---	---
Unaltered joint walls, surface staining only	1.0	---	---
Slightly altered, non-softening, non-cohesive rock mineral or crushed rock infilling	2.0	2.0	4.0
Non-softening, slightly clayey non-cohesive filling	3.0	6.0	10.0
Non-softening, strongly over-consolidated clay mineral filling, with or without crushed rock	3.0	6.0 **	10.0
Softening or low friction clay mineral coatings and small quantities of swelling clays	4.0	8.0	13.0

## DESIGN MEMORANDUM

Joint/fissures either open or containing relatively soft gouge of sufficient thickness to prevent joint/fissure wall contact upon excavation	1.0	Softening moderately over-consolidated clay mineral filling, with or without crushed rock	4.0	8.0 **	13.0
		Shattered or micro-shattered (swelling) clay gouge, with or without crushed rock	5.0	10.0	18.0
Shattered or micro-shattered clay	1.0	{1} Joint walls effectively in contact {2} Joint walls come into contact after approximately 100-mm of shear {3} Joint walls do not come into contact at all upon shear ** Also applies when crushed rock occurs in clay gouge without rock wall contact			

### AASHTO LRFD Bridge Design Specifications, 6th Ed. (AASHTO 2012)

Table 10.4.6.4-1: Geomechanics Classification of Rock Masses (AASHTO 2012)







Parameter		Range of Values							Score	
1	Strength of intact rock material	Point Load Strength Index	> 175 ksf	85-175 ksf	45-85 ksf	20-45 ksf	For this low range, uniaxial compressive strength is preferred			2
		Uniaxial Compressive Strength	> 4320 ksf	2160-4320 ksf	1080-2160 ksf	520-1080 ksf	215-520 ksf	70-215 ksf	20-7 ksf	
	Relative Rating	15	12	7	4	2	1	0		
2	Drill core quality (RQD)		90-100%	75-90%	50-75%	25-50%	<25%			3
	Relative Rating		20	17	13	8	3			
3	Spacing of Joints		>10 ft.	3-10 ft.	1-3 ft.	2 in - 1 ft.	<2in.			10
	Relative Rating		30	25	20	10	5			
4	Conditions of Joints	<ul style="list-style-type: none"> <li>• Very rough surfaces</li> <li>• Not continuous</li> <li>• No Separation</li> <li>• Hard joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slightly rough surfaces</li> <li>• Separation &lt;0.05 in.</li> <li>• Hard joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slightly rough surface</li> <li>• Separation &lt;0.05 in.</li> <li>• Soft joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slickenside surface</li> <li>• Gouge &lt;0.2in thick</li> <li>• Joints open 0.05 - 0.2 in.</li> <li>• Continuous Joints</li> </ul>	<ul style="list-style-type: none"> <li>• Soft gouge &gt;0.2 in.</li> <li>• Joints open &gt;0.2 in.</li> <li>• Continuous Joints</li> </ul>	12			
		Relative Rating	25	20	12	6		0		
5	Groundwater conditions (for scour only use the General Conditions and either Moist or Completely Dry)		Completely Dry	Moist only (interstitial water)		Water under moderate pressure	Severe water problems		7	
	Relative Rating		10	7		4	0			
Note: 1 MPa = 145 psi 1 psi = 0.00689 Mpa 1 psi = 0.144 ksf		<b>Rock Mass Rating</b>					<b>34</b>			



# DESIGN MEMORANDUM

## AASHTO LRFD Bridge Design Specifications, 9th Ed. (AASHTO 2020)

Table 10.4.6.4-1: Determination of GSI for Jointed Rock Mass (AASHTO 2020)

<p><b>GEOLOGICAL STRENGTH INDEX FOR JOINTED ROCKS</b></p> <p>From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavourable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis</p> <p style="text-align: center;"><b>STRUCTURE</b></p>		<p><b>SURFACE CONDITIONS</b></p>	<p><b>VERY GOOD</b> Very rough, fresh, unweathered surfaces</p>	<p><b>GOOD</b> Rough, slightly weathered, iron stained surfaces</p>	<p><b>FAIR</b> Smooth, moderately weathered and altered surfaces</p>	<p><b>POOR</b> Slickensided, highly weathered surfaces with compact coating or fillings of angular fragments</p>	<p><b>VERY POOR</b> Slickensided, highly weathered surfaces with soft clay coatings or fillings</p>
		<p>DECREASING SURFACE QUALITY <span style="font-size: 2em;">➔</span></p>					
 <p>INTACT OR MASSIVE- Intact rock specimens or massive in-situ rock with few widely spaced discontinuities</p>	90	/					N/A
 <p>BLOCKY - Well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets</p>	80	70	/				/
 <p>VERY BLOCKY - Interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets</p>	60	50	/				/
 <p>BLOCKY/DISTURBED/SEAMY - Folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity</p>	40	30	/				/
 <p>DISINTEGRATED - Poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces</p>	20	/					/
 <p>LAMINATED/SHEARED - Lack of blockiness due to close spacing of the weak schistosity or shear planes</p>	N/A	N/A	/				10



## DESIGN MEMORANDUM

Bedrock Scour Samples						
Boring ID	Sample ID	Sample Elevation (Ft)	Erodibility Index (K)	$\tau_c$ Value (psf)	$D_{50,equiv}$ (mm)	Erosion Category
B-001-0-24	NQ2-1/2	685.7-695.7	1.03	5.4	257.4	3.77

Qu = 1,500 psi Estimated from GDM Table 400-6 (Slightly Strong)

Total Unit Weight = 155 pcf Estimated from GDM Table 400-5

## DESIGN MEMORANDUM

To: OODT Dist 11  
 Copy:  
 From: CTL Engineering, Inc.  
 Date: March 25, 2025  
 Subject: BEL-40-23.37 PID 114388; Rock Scour Assessment

At your request, CTL Engineering, Inc. has completed drilling and sampling operations for the referenced project. It is our understanding that the near surface bedrock will be interacting with the proposed foundational elements and rock scour is a concern. The following is the assessment of the encountered bedrock conditions relative to the geotechnical explorations:

Boring Evaluated:	B-001-0-24
Boring Location:	Adjacent to Pier, Sta. 205+80, 1' Lt.
Ground Elevation (ft):	716.7
Bedrock Elevation (ft):	685.7
Bedrock Age:	Pennsylvanian
Bedrock Description:	Shale, Moderately Weathered, Slightly Strong

Testing Characteristics	BDM Threshold Value	Result	Scour Resistant Property
Unconfined Compressive Strength [Q <sub>u</sub> ] (ASTM D 7012C) (ASTM D 7012C)	Q <sub>u</sub> ≥ 2,500 psi	2380 -2790 psi 16.4-19.2 MPa	NO
Slake Durability Index [Id <sub>2</sub> ]: (ASTM D4644)	SDI ≥ 90%	95.1 %	YES
Rock Quality Designation: (SGE Section 6)	RQD ≥ 65%	62	NO
Total Unit Weight (pcf):	γ <sub>tot</sub> ≥ 150 pcf	165.3 pcf	YES
Rock Mass Rating:	RMR ≥ 75	44	NO
Geological Strength Index (GSI):	GSI ≥ 75	35	NO
GSI Structure:	Massive or Blocky	Blocky/Disturbed	NO
GSI Surface Conditions:	Very Good or Good	Fair	NO
Erodibility Index [K]: FHWA-HIF-12-003 (HEC18)	K ≥ 100	678.26	YES
Rock Joint Set Number [J <sub>n</sub> ]:	J <sub>n</sub> ≤ 5	1.5	YES
Joint Roughness Number [J <sub>r</sub> ]:	J <sub>r</sub> ≥ 1	2	YES
Joint Alteration Number [J <sub>a</sub> ]:	J <sub>a</sub> ≤ 5	2	YES
Relative Joint Orientation [J <sub>s</sub> ]:	J <sub>s</sub> ≥ 0.4	1	YES
Does bedrock meet criteria of scour resistant per BDM:		<b>NO</b>	

Critical Shear Stress (τ<sub>c</sub>) \* = ρ (1000 K<sup>0.75</sup> / 7.853 ρ)<sup>2/3</sup>

6591.9	Pa psf
137.7	

## DESIGN MEMORANDUM

$$\text{Calculated } D_{50} \text{ equivalent} = 6591.9 \text{ mm } 259.5 \text{ in}$$

$$\text{Calculated Erosion Category (EC)} = 3.98$$

### CALCULATIONS

$$K = (M_s)(K_b)(K_d)(J_s) \quad K = 678.26$$

Where:  $M_s$  = Intact Rock Strength Parameter

$$\text{From Testing: } Q_u = 2380 \text{ psi}$$
$$Q_u = 16.41 \text{ MPa}$$

$$M_s = Q_u \text{ for } Q_u \geq 10 \text{ MPa}$$
$$(0.78) Q_u^{1.05} \text{ for } Q_u < 10 \text{ MPa}$$

Based on SPT (Stark et. al. 2017)

Where:  $Q_u$  (ksf) =  $0.092 \times N_{90}$

$$Q_u = 0.00 \text{ psi}$$

$$N_{90} =$$

$$Q_u = 0.00 \text{ MPa}$$

$$M_s = 16.41$$

Where:  $K_b$  = Block Size Parameter

$$K_b = RQD/J_n \geq 0.10$$

$$RQD = 62$$
$$J_n = 1.5 \leq 5.0$$

$$K_b = 41.33 \geq 0.1$$

Where:  $K_d$  = Shear Strength Parameter

$$K_d = J_r/J_a$$

$$J_r = 2 \geq 1.0$$

$$J_a = 2 \leq 5.0$$

$$K_d = 1.00 \geq 0.2$$

Where:  $J_s$  = Relative Orientation Parameter

$$J_s = 1.00 \geq 0.4$$

$$\text{Average Joint Spacing} = 3 \text{ inches } 76.2 \text{ mm}$$

**Re-arrange HEC-18 Equations 7.38 for 'Critical Stream Power' and 7.39 'Approach Flow Stream Power' to derive the critical shear stress for non-scour resistant bedrock as follows:**

$$\text{Critical Shear Stress } (\tau_c)^* = \rho (1000 K^{0.75} / 7853 \rho)^{2/3} 6591.9 \text{ Pa}$$

## DESIGN MEMORANDUM

Where:  $\tau_c$  = Critical shear stress (Pa)  
 $\rho$  = Mass density of water (1000 kg/m<sup>3</sup>)  
 K = Erodibility Index (dim.)

Erosion Category (EC) =  $1.2(1.83333 + \text{Log}(S_v/2.5))$

EC = 3.98

### REFERENCES

Table 4.20: Geomechanics Rating Adjustment for Joint Orientations (after AASHTO 2010)

Orientation of Joints		Very Favorable	Favorable	Fair	Unfavorable	Very Unfavorable
Rating	Tunnels	0	-2	-5	-10	-12
	Foundations	0	-2	-7	-15	-25
	Slopes	0	-5	-25	-50	-60

Table 4.21: Geomechanics Rock Mass Classes Determined From Total Ratings (AASHTO 2010)

RMR (Note 1)	100 to 81	80 to 61	69 to 41	41 to 21	≤20
Class No.	I	II	III	IV	V
Description	Very Good Rock	Good Rock	Fair Rock	Poor Rock	Very Poor Rock

Table 4.23. Rock Joint Set Number  $J_n$

Number of Joint Sets	Joint Set Number ( $J_n$ )
Intact, no or few joints/fissures	1.00
One joint/fissure set	1.22
One joint/fissure set plus random	1.50
Two joint/fissure sets	1.83
Two joint/fissure sets plus random	2.24
Three joint/fissure sets	2.74
Three joint/fissure sets plus random	3.34
Multiple joint/fissure sets	4.09
Multiple joint/fissure sets	5.00

Table 4.24. Joint Roughness Number  $J_r$

Condition of Joint	Joint Roughness Number ( $J_r$ )
Stepped Joint/fissures	4.0
Rough or irregular, undulating	3.0
Smooth undulating	2.0
Slickensided undulating	1.5
Smooth planar	1.0
Slickensided planar	0.5

Table 4.25. Joint Alteration Number  $J_a$

Description of Gouge	1.0 <sup>{1}</sup>	2.0 - 5.0 <sup>{2}</sup>	5.0 <sup>{3}</sup>
Tightly healed, hard, non-softening impermeable	0.75	---	---
Unaltered joint walls, surface staining only	1.0	---	---
Slightly altered, non-softening, non-cohesive rock mineral or crushed rock infilling	2.0	2.0	4.0
Non-softening, slightly clayey non-cohesive filling	3.0	6.0	10.0
Non-softening, strongly over-consolidated clay mineral filling, with or without crushed rock	3.0	6.0 **	10.0
Softening or low friction clay mineral coatings and small quantities of swelling clays	4.0	8.0	13.0

## DESIGN MEMORANDUM

Joint/fissures either open or containing relatively soft gouge of sufficient thickness to prevent joint/fissure wall contact upon excavation	1.0	Softening moderately over-consolidated clay mineral filling, with or without crushed rock	4.0	8.0 **	13.0
		Shattered or micro-shattered (swelling) clay gouge, with or without crushed rock	5.0	10.0	18.0
Shattered or micro-shattered clay	1.0	{1} Joint walls effectively in contact {2} Joint walls come into contact after approximately 100-mm of shear {3} Joint walls do not come into contact at all upon shear ** Also applies when crushed rock occurs in clay gouge without rock wall contact			

### AASHTO LRFD Bridge Design Specifications, 6th Ed. (AASHTO 2012)

Table 10.4.6.4-1: Geomechanics Classification of Rock Masses (AASHTO 2012)

Parameter		Range of Values							Score	
1	Strength of intact rock material	Point Load Strength Index	> 175 ksf	85-175 ksf	45-85 ksf	20-45 ksf	For this low range, uniaxial compressive strength is preferred			2
		Uniaxial Compressive Strength	> 4320 ksf	2160-4320 ksf	1080-2160 ksf	520-1080 ksf	215-520 ksf	70-215 ksf	20-7 ksf	
	Relative Rating	15	12	7	4	2	1	0		
2	Drill core quality (RQD)	90-100%	75-90%	50-75%	25-50%	<25%				13
	Relative Rating	20	17	13	8	3				
3	Spacing of Joints	>10 ft.	3-10 ft.	1-3 ft.	2 in - 1 ft.	<2in.				10
	Relative Rating	30	25	20	10	5				
4	Conditions of Joints	<ul style="list-style-type: none"> <li>• Very rough surfaces</li> <li>• Not continuous</li> <li>• No Separation</li> <li>• Hard joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slightly rough surfaces</li> <li>• Separation &lt;0.05 in.</li> <li>• Hard joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slightly rough surface</li> <li>• Separation &lt;0.05 in.</li> <li>• Soft joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slickenside surface</li> <li>• Gouge &lt;0.2in thick</li> <li>• Joints open 0.05 - 0.2 in.</li> <li>• Continuous Joints</li> </ul>	<ul style="list-style-type: none"> <li>• Soft gouge &gt;0.2 in.</li> <li>• Joints open &gt;0.2 in.</li> <li>• Continuous Joints</li> </ul>				12
		Relative Rating	25	20	12	6				
5	Groundwater conditions (for scour only use the General Conditions and either Moist or Completely Dry)	Completely Dry	Moist only (interstitial water)		Water under moderate pressure	Severe water problems			7	
	Relative Rating	10	7		4	0				
Note: 1 MPa = 145 psi 1 psi = 0.00689 Mpa 1 psi = 0.144 ksf		<b>Rock Mass Rating</b>								<b>44</b>



## DESIGN MEMORANDUM

Bedrock Scour Samples						
Boring ID	Sample ID	Sample Elevation (Ft)	Erodibility Index (K)	$\tau_c$ Value (psf)	$D_{50,equiv}$ (mm)	Erosion Category
B-001-0-24	NQ2-3/4	679.3-685.7	678.26	137.7	6591.9	3.98

## DESIGN MEMORANDUM

To: OODT Dist 11  
 Copy:  
 From: CTL Engineering, Inc.  
 Date: March 25, 2025  
 Subject: BEL-40-23.37 PID 114388; Rock Scour Assessment

At your request, CTL Engineering, Inc. has completed drilling and sampling operations for the referenced project. It is our understanding that the near surface bedrock will be interacting with the proposed foundational elements and rock scour is a concern. The following is the assessment of the encountered bedrock conditions relative to the geotechnical explorations:

Boring Evaluated:	B-001-0-24
Boring Location:	Adjacent to Pier, Sta. 205+80, 1' Lt.
Ground Elevation (ft):	716.7
Bedrock Elevation (ft):	679.3
Bedrock Age:	Pennsylvanian
Bedrock Description:	Claystone, Highly Weathered, Weak to Slightly Strong

Testing Characteristics	BDM Threshold Value	Result	Scour Resistant Property
Unconfined Compressive Strength [Q <sub>u</sub> ] (ASTM D 7012C) (ASTM D 7012C)	Q <sub>u</sub> ≥ 2,500 psi	1620 psi 11.17 MPa	NO
Slake Durability Index [Id <sub>2</sub> ]: (ASTM D4644) GDM Table 400-5	SDI ≥ 90%	30.0 %	NO
Rock Quality Designation: (SGE Section 6)	RQD ≥ 65%	31	NO
Total Unit Weight (pcf):	γ <sub>tot</sub> ≥ 150 pcf	157.8 pcf	YES
Rock Mass Rating:	RMR ≥ 75	38	NO
Geological Strength Index (GSI):	GSI ≥ 75	30	NO
GSI Structure:	Massive or Blocky	Blocky/Disturbed	NO
GSI Surface Conditions:	Very Good or Good	Fair	NO
Erodibility Index [K]: FHWA-HIF-12-003 (HEC18)	K ≥ 100	115.42	YES
Rock Joint Set Number [J <sub>n</sub> ]:	J <sub>n</sub> ≤ 5	1.5	YES
Joint Roughness Number [J <sub>r</sub> ]:	J <sub>r</sub> ≥ 1	2	YES
Joint Alteration Number [J <sub>a</sub> ]:	J <sub>a</sub> ≤ 5	4	YES
Relative Joint Orientation [J <sub>s</sub> ]:	J <sub>s</sub> ≥ 0.4	1	YES
Does bedrock meet criteria of scour resistant per BDM:		<b>NO</b>	

$$\text{Critical Shear Stress } (\tau_c)^* = \rho (1000 K^{0.75} / 7.853 \rho)^{2/3}$$

2719.2	Pa
56.8	psf



## DESIGN MEMORANDUM

$$\text{Calculated } D_{50} \text{ equivalent} = 2719.2 \text{ mm } 107.1 \text{ in}$$

$$\text{Calculated Erosion Category (EC)} = 3.77$$

### CALCULATIONS

$$K = (M_s)(K_b)(K_d)(J_s) \quad K = 115.42$$

Where:  $M_s$  = Intact Rock Strength Parameter

$$\begin{aligned} \text{From Testing : } Q_u &= 1620 \text{ psi} \\ Q_u &= 11.17 \text{ MPa} \end{aligned}$$

$$\begin{aligned} M_s &= Q_u \text{ for } Q_u \geq 10 \text{ MPa} \\ &= (0.78) Q_u^{1.05} \text{ for } Q_u < 10 \text{ MPa} \end{aligned}$$

Based on SPT (Stark et. al. 2017)

Where:  $Q_u$  (ksf) =  $0.092 \times N_{90}$

$$\begin{aligned} Q_u &= 0.00 \text{ psi} \\ Q_u &= 0.00 \text{ MPa} \end{aligned}$$

$$N_{90} = \text{[ ]}$$

$$M_s = 11.17$$

Where:  $K_b$  = Block Size Parameter

$$K_b = RQD/J_n \geq 0.10$$

$$\begin{aligned} RQD &= 31 \\ J_n &= 1.5 \leq 5.0 \end{aligned}$$

$$K_b = 20.67 \geq 0.1$$

Where:  $K_d$  = Shear Strength Parameter

$$K_d = J_r/J_a$$

$$\begin{aligned} J_r &= 2 \geq 1.0 \\ J_a &= 4 \leq 5.0 \end{aligned}$$

$$K_d = 0.50 \geq 0.2$$

Where:  $J_s$  = Relative Orientation Parameter

$$J_s = 1.00 \geq 0.4$$

$$\text{Average Joint Spacing} = 2 \text{ inches } 50.8 \text{ mm}$$

**Re-arrange HEC-18 Equations 7.38 for 'Critical Stream Power' and 7.39 'Approach Flow Stream Power' to derive the critical shear stress for non-scour resistant bedrock as follows:**

$$\text{Critical Shear Stress } (\tau_c)^* = \rho (1000 K^{0.75} / 7853 \rho)^{2/3} 2719.2 \text{ Pa}$$

## DESIGN MEMORANDUM

Where:  $\tau_c$  = Critical shear stress (Pa)  
 $\rho$  = Mass density of water (1000 kg/m<sup>3</sup>)  
 K = Erodibility Index (dim.)

Erosion Category (EC) =  $1.2(1.83333 + \text{Log}(S_v/2.5))$

EC = 3.77

### REFERENCES

Table 4.20: Geomechanics Rating Adjustment for Joint Orientations (after AASHTO 2010)

Orientation of Joints		Very Favorable	Favorable	Fair	Unfavorable	Very Unfavorable
Rating	Tunnels	0	-2	-5	-10	-12
	Foundations	0	-2	-7	-15	-25
	Slopes	0	-5	-25	-50	-60

Table 4.21: Geomechanics Rock Mass Classes Determined From Total Ratings (AASHTO 2010)

RMR (Note 1)	100 to 81	80 to 61	69 to 41	41 to 21	≤20
Class No.	I	II	III	IV	V
Description	Very Good Rock	Good Rock	Fair Rock	Poor Rock	Very Poor Rock

Table 4.23. Rock Joint Set Number  $J_n$

Number of Joint Sets	Joint Set Number ( $J_n$ )
Intact, no or few joints/fissures	1.00
One joint/fissure set	1.22
One joint/fissure set plus random	1.50
Two joint/fissure sets	1.83
Two joint/fissure sets plus random	2.24
Three joint/fissure sets	2.74
Three joint/fissure sets plus random	3.34
Multiple joint/fissure sets	4.09
Multiple joint/fissure sets	5.00

Table 4.24. Joint Roughness Number  $J_r$

Condition of Joint	Joint Roughness Number ( $J_r$ )
Stepped Joint/fissures	4.0
Rough or irregular, undulating	3.0
Smooth undulating	2.0
Slickensided undulating	1.5
Smooth planar	1.0
Slickensided planar	0.5

Table 4.25. Joint Alteration Number  $J_a$

Description of Gouge	1.0 <sup>{1}</sup>	2.0 - 5.0 <sup>{2}</sup>	5.0 <sup>{3}</sup>
Tightly healed, hard, non-softening impermeable	0.75	---	---
Unaltered joint walls, surface staining only	1.0	---	---
Slightly altered, non-softening, non-cohesive rock mineral or crushed rock infilling	2.0	2.0	4.0
Non-softening, slightly clayey non-cohesive filling	3.0	6.0	10.0
Non-softening, strongly over-consolidated clay mineral filling, with or without crushed rock	3.0	6.0 **	10.0
Softening or low friction clay mineral coatings and small quantities of swelling clays	4.0	8.0	13.0

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Joint/fissures either open or containing relatively soft gouge of sufficient thickness to prevent joint/fissure wall contact upon excavation	1.0	Softening moderately over-consolidated clay mineral filling, with or without crushed rock	4.0	8.0 **	13.0
		Shattered or micro-shattered (swelling) clay gouge, with or without crushed rock	5.0	10.0	18.0
Shattered or micro-shattered clay	1.0	{1} Joint walls effectively in contact {2} Joint walls come into contact after approximately 100-mm of shear {3} Joint walls do not come into contact at all upon shear ** Also applies when crushed rock occurs in clay gouge without rock wall contact			

### AASHTO LRFD Bridge Design Specifications, 6th Ed. (AASHTO 2012)







Table 10.4.6.4-1: Geomechanics Classification of Rock Masses (AASHTO 2012)

Parameter		Range of Values							Score	
1	Strength of intact rock material	Point Load Strength Index	> 175 ksf	85-175 ksf	45-85 ksf	20-45 ksf	For this low range, uniaxial compressive strength is preferred			1
		Uniaxial Compressive Strength	> 4320 ksf	2160-4320 ksf	1080-2160 ksf	520-1080 ksf	215-520 ksf	70-215 ksf	20-7 ksf	
	Relative Rating	15	12	7	4	2	1	0		
2	Drill core quality (RQD)		90-100%	75-90%	50-75%	25-50%	<25%			8
	Relative Rating		20	17	13	8	3			
3	Spacing of Joints		>10 ft.	3-10 ft.	1-3 ft.	2 in - 1 ft.	<2in.			10
	Relative Rating		30	25	20	10	5			
4	Conditions of Joints	<ul style="list-style-type: none"> <li>• Very rough surfaces</li> <li>• Not continuous</li> <li>• No Separation</li> <li>• Hard joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slightly rough surfaces</li> <li>• Separation &lt;0.05 in.</li> <li>• Hard joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slightly rough surface</li> <li>• Separation &lt;0.05 in.</li> <li>• Soft joint wall rock</li> </ul>	<ul style="list-style-type: none"> <li>• Slickenside surface</li> <li>• Gouge &lt;0.2in thick</li> <li>• Joints open 0.05 - 0.2 in.</li> <li>• Continuous Joints</li> </ul>	<ul style="list-style-type: none"> <li>• Soft gouge &gt;0.2 in.</li> <li>• Joints open &gt;0.2 in.</li> <li>• Continuous Joints</li> </ul>			12	
		Relative Rating		25	20	12				6
5	Groundwater conditions (for scour only use the General Conditions and either Moist or Completely Dry)		Completely Dry	Moist only (interstitial water)		Water under moderate pressure	Severe water problems		7	
	Relative Rating		10	7		4	0			
Note: 1 MPa = 145 psi 1 psi = 0.00689 Mpa 1 psi = 0.144 ksf		<b>Rock Mass Rating</b>					<b>38</b>			

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## AASHTO LRFD Bridge Design Specifications, 9th Ed. (AASHTO 2020)

Table 10.4.6.4-1: Determination of GSI for Jointed Rock Mass (AASHTO 2020)

GEOLOGICAL STRENGTH INDEX FOR JOINTED ROCKS From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavourable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis		SURFACE CONDITIONS				
STRUCTURE		VERY GOOD Very rough, fresh, unweathered surfaces	GOOD Rough, slightly weathered, iron stained surfaces	FAIR Smooth, moderately weathered and altered surfaces	POOR Slickensided, highly weathered surfaces with compact coating or fillings of angular fragments	VERY POOR Slickensided, highly weathered surfaces with soft clay coatings or fillings
		DECREASING SURFACE QUALITY				
	INTACT OR MASSIVE- Intact rock specimens or massive in-situ rock with few widely spaced discontinuities	90	80	N/A	N/A	N/A
	BLOCKY - Well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets	70	60	N/A	N/A	N/A
	VERY BLOCKY - Interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets	50	40	N/A	N/A	N/A
	BLOCKY/DISTURBED/SEAMY - Folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity	30	20	N/A	N/A	N/A
	DISINTEGRATED - Poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces	10	N/A	N/A	N/A	N/A
	LAMINATED/SHEARED - Lack of blockiness due to close spacing of the weak schistosity or shear planes	N/A	N/A	N/A	N/A	N/A

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Bedrock Scour Samples						
Boring ID	Sample ID	Sample Elevation (Ft)	Erodibility Index (K)	$\tau_c$ Value (psf)	$D_{50,equiv}$ (mm)	Erosion Category
B-001-0-24	NQ2-4/5	670.7-679.3	115.42	56.8	2719.2	3.77

Slake Durability Index [ $Id_2$ ] From GDM Table 400-5