FINAL REPORT SUBGRADE EXPLORATION REPORT CUY-490-00.00 CUYAHOGA COUNTY, OHIO PID: 107408

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NEAS PROJECT 21-0035

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EXECUTIVE SUMMARY

The Ohio Department of Transportation (ODOT) has proposed a roadway rehabilitation project CUY-490-00.00 (PID 107408) project along IR-490 in Cuyahoga County, Ohio. The project limits extend west to east from West 25th Street (St) to about a third of a mile west of East 55th St, but excludes the portion of IR-490 comprised of Bridge No. CUY-490-0100 which extends over various surface streets, railroads/railyards, and the Cuyahoga River. It is our understanding that the overall project objective is to rehabilitate the project portion of IR-490, which has degraded due to age and heavy traffic loading. As part of the proposed rehabilitation project, the proposed pavement replacement will maintain the existing pavement footprint (horizontal alignment) with vertical alignment changes up to about 2 ft. The associated ramps located within the project portion of I--490 will also be rehabbed with the IR-490 mainline pavement. These project ramps planned to undergo full depth pavement replacement include Lane E-S, Ramp C-7, Ramp 7-C, Ramp 7-7C, Ramp B-C, Ramp C-B, Ramp N-W, Ramp W-S, Ramp W-N, Ramp E-N and Ramp S-E.

National Engineering & Architectural Services, Inc. (NEAS) has been contracted to perform geotechnical engineering services for the project. The purpose of the geotechnical engineering services was to perform geotechnical explorations within the project limits to obtain information concerning the subsurface soil and groundwater conditions relevant to the design and construction of the project. Between June 9, 2021 and July 26, 2021, NEAS performed the site reconnaissance and exploration program for the project. The subsequent document presents the results of a subgrade exploration for the project portion of IR-490 to undergo full-depth pavement replacement. As part of the rehabilitation project, NEAS advanced a total of 53 borings to be utilized for subgrade characterization purposes.

The subgrade conditions within the project limits are relatively consistent and are generally comprised of either fill soils (i.e., embankment fill) or natural soils consisting of gravel, sand and silt, or low to moderately plastic sandy silt and silt/clay combinations. The subgrade soils encountered within the project limits are generally classified as either A-1-a, A-1-b, A-2-4, A-3, A-3a, A-4a, A-4b type soils. With respect to sulfate within the subgrade soil, based on the project laboratory testing program, each subgrade soil sample tested was determined to have a sulfate content of less than 5,000 parts per million (ppm) (i.e., lower than the level which ODOT considers high and may prevent the use of chemical stabilization).

Subgrade soils designated by ODOT's GDM as both "unstable" and "unsuitable" were present at various locations throughout the project. Subgrade soils designated as "unsuitable" consisted of soils classifying as A-4b (Silt) and were encountered within subgrade depths that require remediation in seven (7) borings (B-002-0-21, B-003-0-21, B-004-0-21, B-012-0-21, B-013-0-21, B-018-0-21 and B-020-0-21) performed along IR-490 Mainline, one (1) boring (B-012-0-21) performed on Ramp 7-7C, and one (1) boring (B-033-0-21) performed on Ramp C-7. Subgrade soils designated as "unstable" via high moisture content were encountered at the various locations identified in Section 4.1.3.1 of this report. In general, it is recommended that the subgrade soil of project interstates and associated ramps be globally (chemically) stabilized to a depth of 12 inches utilizing cement as the stabilization chemical. For areas where "unsuitable" A-4b (Silt) soils were encountered, it is recommended that either Excavate and Replace with geotextile (Item 204) be performed to a depth of 36 inches below the proposed top of subgrade, or chemical stabilization be performed to a depth of 14 inches. Our minimum recommended limits for the indicated project subgrade stabilization are provided in Table 7 of this report. Although, the minimum recommended limits are presented, due to the presence of A-4b soils, NEAS recommends that chemical stabilization be performed to a depth of 14 inches for the whole project portion of IR-490.



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1. INTRODUCTION

1.1. General

National Engineering & Architectural Services, Inc. (NEAS) presents our Subgrade Exploration Report for the interstate major rehabilitation project (CUY-490-00.00, PID 107408) along Interstate Route 490 (IR-490) and associated ramps within the City of Cleveland, Cuyahoga County, Ohio. It is our understanding that the objective of the proposed project is to rehabilitate and replace the existing IR-490 pavement extending from West 25th Street (St) to about a third of a mile west of East 55th St excluding the portion of IR-490 encompassed by existing Bridge No. CUY-490-0100 which extends over various surface streets, railroads/railyards, and the Cuyahoga River. We understand that the proposed pavement replacement will maintain the existing pavement footprint (horizontal alignment) with vertical alignment changes up to about 2 ft.. The associated ramps located within the project portion of IR-490 will also be rehabbed, these project ramps planned to undergo full depth pavement replacement include Lane E-S, Ramp C-7, Ramp 7-C, Ramp 7-7C, Ramp B-C, Ramp C-B, Ramp N-W, Ramp W-S, Ramp W-N, Ramp E-N and Ramp S-E. This report presents a summary of the project encountered surficial and subsurface conditions and our recommendations for subgrade stabilization and pavement design parameters. The roadway analysis performed as part of this report has been performed in accordance with ODOT's Geotechnical Design Manual (GDM) (ODOT, 2023) and *Pavement Design Manual* (PDM) (ODOT, 2020).

The exploration was conducted in general accordance with NEAS's proposal to GPD Group (GPD), dated April 22, 2021, and with the provisions of the January 2021 (ODOT, 2021) revisions of ODOT's *Specifications for Geotechnical Explorations* (SGE).

The scope of work performed by NEAS as part of the referenced project included: a review of published geotechnical information; performing 53 total test borings; laboratory testing of soil samples in accordance with the SGE; performing geotechnical engineering analysis to assess subgrade and recommended pavement design parameters; and development of this summary report.

2. GEOLOGY AND OBSERVATIONS OF THE PROJECT

2.1. Geology and Physiography

The majority of the project site is located within the Erie Lake Plain, part of the Huron-Erie Lake Plains. This area is characterized as the edge of the very low relief (10 ft), Ice-Age Lake basin separated from the modern Lake Erie by shoreline cliffs with major streams in deep gorges being characteristic. The geology in this region is described as Pleistocene-age lacustrine sand, silt, clay, and wave-planed glacial till over Devonian- and Mississippi-age shales and sandstones (ODGS, 1998).

The geology underlying the IR-90 and IR-490 interchange portion of the project site is mapped as an average of 20 ft of Wisconsinan-age sand underlain by an average of 230 ft of silt and clay thinning to an average of 80 ft of silt and clay at the western project limits all underlain by Devonian-age shale bedrock (ODGS, 2005). The geology underlying the IR-77 and IR-490 interchange portion of the project site is mapped as an average of 40 ft of Wisconsinan-age sand and gravel underlain by an average of 290 ft of silt and clay all underlain by Devonian-age age shale bedrock (ODGS, 2005).



The sands contain minor amounts of disseminated gravel or thin lenses of silt and is described as well to moderately sorted, moderately to well rounded, finely stratified to massive, may be cross bedded and may locally contain organics. Sand in deep buried valleys are noted as potentially being older than Wisconsinan. The sand and gravel soils are described as interbedded sand and gravel commonly containing thin, discontinuous layer of silt and clay and may locally contain organics. These sands and gravels are comprised of material that is moderately to well sorted, moderately to well-rounded and finely stratified to massive. Sand and gravel in buried valleys are noted as potentially being older than Wisconsinan. The silt and clay in this region can be found as thick lacustrine valley-fill deposits of high, proglacial predecessors of Lake Erie and is described as laminated to interbedded soils that may contain thin fine sand or gravel layers.

Based on the Bedrock Geologic Units Map of Ohio (USGS & ODGS, 2006), bedrock within the project area consists of shale of the Ohio Shale formation. This unit is comprised of Devonian-age shale with carbonate and/or siderite concretions in the lowermost 50 ft. This brownish black to greenish gray shale is carbonaceous to clayey, laminated to thin bedded and can have a petroliferous odor. The bedrock is anticipated to generally follow the natural topography of the site, sloping downward from west to east then increasing elevation moving east of the Cuyahoga River (ODGS, 2003). Based on the ODNR bedrock topography map of Ohio, bedrock elevations at the project site can be expected to be between elevations of 400 and 600 ft above sea level (amsl), putting bedrock at a depth ranging from about 50 ft to about 290 ft below ground surface (bgs).

The majority of soils directly underlying the project site have been mapped (Web Soil Survey) by the Natural Resources Conservation Service as being Udorthents and urban land complex. Udorthents are soils that have been disturbed by cutting or filling and are not rated for local roads. These soils as units are not classified according to the AASHTO method of soil classification, but it can be expected that these soils will largely consist of fill soils and often vary in composition. The exceptions to this are portions of the project near the West 7th St overpass where the soils are mapped as Ellsworth urban land complex, and near the Broadway Avenue (Ave) overpass where the soils are mapped as Elnora urban land complex. Soils in the Ellsworth series are characterized as very deep, moderately well drained soils formed in till on till plains. The Ellsworth series is comprised of primarily fine-grained soils and classifies as A-4, A-6 and A-7-6 type soils according to the AASHTO method of soil classification. Soils in the Elnora series are characterized as a very deep, moderately well drained soils formed in sandy glacial lake, eolian and deltaic sediments. The Elnora series is comprised of both coarse- and fine-grained soils and classifies as A-2 and A-4 type soils according to the AASHTO method of soil classification (USDA, 2015).

2.2. Hydrology/Hydrogeology

Groundwater at the project site can be expected at an elevation consistent with that of the Cuyahoga River as it is the most dominant hydraulic influence in the vicinity of the project's boundaries. The water level of the Cuyahoga River may be generally representative of the local groundwater table. However, it should be noted that perched groundwater systems may be existent in areas due to the presence of fine-grained soils making it difficult for groundwater to permeate to the phreatic surface.

The project site is not located within a special flood hazard area based on available mapping by the Federal Emergency Management Agency's (FEMA) National Flood Hazard mapping program (FEMA, 2016).



2.3. Mining and Oil/Gas Production

No abandoned mines are noted on ODNR's Abandoned Underground Mine Locator within the immediate vicinity of the project's boundaries (ODNR [1], 2016).

No oil or gas wells are noted on ODNR's Ohio Oil & Gas Locator within the immediate vicinity of the project's boundaries (ODNR [2], 2016).

2.4. Historical Records and Previous Phases of Project Exploration

A historic record search was performed through ODOT's Geotechnical Data Management System (GeoMS), and the following report/plans were available for review and evaluation for this report:

- Soil Profile Sheets as part of ODOT project CUY-490-0.27 pages 1-11, prepared by the Ohio State Highway Testing and Research Laboratory, dated May 6, 1998;
- Soil Profile Sheets as part of ODOT project CUY-21-254-(14.12-18.69), prepared by the State of Ohio Department of Highways Testing Laboratory, dated September 13, 1962;
- Project Boring Logs for CUY-71-19.25 prepared by the Ohio State Soil Testing Laboratory, dated April 17, 1964; and,
- Project Boring Logs for CUY-90-6.83 (PID 76779) and associated Subgrade Exploration Report prepared by S&ME, Inc., dated December 11, 2020.

Four historical soil borings (B-109-0-20, B-110-0-20, B-111-0-20, and B-112-0-20) that were drilled as part of the 2020 Subgrade Exploration for ODOT project CUY-90-6.83 were reviewed and are utilized in our report and analysis. A summary of the historic boring information (location, elevation, etc.) is provided in Table 1, and their locations are depicted on the Boring Location Plan provided in Appendix A. The historic boring logs of the borings utilized within this report are provided in Appendix B.

Table 1: Historic Boring Summary

Boring Number	Historical Location (Sta/Offset) ⁽¹⁾	Latitude ⁽²⁾	Longitude ⁽²⁾	Elevation ⁽²⁾ (NAVD 88) (ft)	Depth (ft)
B-109-0-20	930+69, 5' LT	41.474054	81.698962	656.0	7.5
B-110-0-20	931+91, 38' LT	41.474197	81.697498	648.1	7.5
B-111-0-20	935+97, 5' RT	41.474104	81.696012	639.8	7.5
B-112-0-20	937+90, 5' LT	41.474142	81.695311	635.8	7.5
Notes:					

Station and Offsets reference IR-90 alignment assoicated with ODOT Project CUY-90-6.83 (PID 76779).
 Location information based on data provided on refferenced boring logs assoicated with ODOT Project CUY-90-6.83 (PID 76779).

Additional historical soil borings associated with the above historical records, not listed in the table above, were reviewed, however, were not utilized for our analysis as historical borings are generally not representative of existing subgrade conditions. Therefore, are not referenced or presented within this report.

2.5. Field Reconnaissance

A field reconnaissance visit for the overall project area was conducted on June 9, 2021. The reconnaissance was performed along the project portions of IR-490 mainline and associated ramps (Lane E-S, Ramp C-7, Ramp 7-7C, Ramp B-C, Ramp C-B, Ramp N-W, Ramp W-N, Ramp E-N, and Ramp S-E). Site conditions, including the existing pavement conditions, were noted and photographed during the visit. Photographs of notable pavement distress and a summary of our observations by roadway segment are provided below.



2.5.1. Land Use and Cover

The land use of the project area consists of a combination of residential, commercial, industrial, and railroad properties as well as ODOT Right of Way (ROW).

2.5.2. IR-490 from West 25th St to West 11th St

In general, the pavement condition along this section of IR-490 was observed to be fair. Moderate severity longitudinal and transverse cracking was observed along this section as well as edge cracking and crack sealing deficiencies (Photograph 1). The roadway in this section is situated in a cut (i.e., at a lower grade than the surrounding area) with the observed cut slopes at an approximate 3 horizontal to 1 vertical (3H:1V) grade. The roadway was observed to be relatively well-drained along this segment though some signs of standing water were observed at the low point along this segment located near the center of the interchange. The area appeared to be stable with no signs of geotechnical instability observed during our visit.





2.5.3. IR-490 from West 11th St to Bridge No. CUY-490-0100

In general, the pavement condition along this section of the project was observed to be poor. High severity joint cracking, D-cracking, and settlement was observed along this section as well as moderate severity patching and crack sealing deficiencies (Photograph 2). The adjacent grading along this portion of IR-490 generally consists of slopes with the land to the south extending downslope of IR-490 and the land to the north extending upslope from IR-490. The referenced slopes on either side of the interstate were observed to be approximately 2H:1V. The roadway appeared to be well drained with no signs of standing water observed. The area appeared to be stable with no signs of geotechnical instability observed during our visit.



Photograph 2: Pavement condition of IR-490 between West 11th St and Bridge No. CUY-490-0100.



2.5.4. IR-490 from Bridge No. CUY-490-0100 to the Eastern Project Limits

In general, the pavement condition along this section of the project was observed to be poor. High severity joint cracking, D-cracking, and patching was observed along this section as well as moderate severity crack sealing deficiencies (Photograph 3). The interstate along this segment is situated in a cut (i.e., at a lower grade than surrounding area) with the adjacent cut slopes observed to be approximately 2H:1V. With respect to drainage, the roadway was observed to be relatively well-drained with signs of standing water such as cattails observed at the lowest point located near the IR-490 and IR-77 interchange (Photograph 4). The area appeared to be stable with no signs of geotechnical instability observed during our visit.

Photograph 3: Pavement Condition of IR-490 from Bridge No. CUY-490-0100 to the Eastern Project Limits





Photograph 4: Signs of standing water along IR-490



2.5.5. Ramp from IR-490 WB to IR-71 SB (Lane E-S)

In general, the pavement condition along Lane E-S was observed to be fair. Moderate severity transverse and longitudinal cracking was observed in addition to light severity settlement, map cracking and crack sealing deficiencies (Photograph 6). The deck of the bridge carrying this ramp over IR-490 appeared to be in excellent condition with very few signs of surface wear. On the northeast portion of Lane E-S, before the bridge, the ramp is constructed part way up an embankment east of IR-71 (north of IR-490). On the southwest portion of Lane E-S, following the bridge, the roadway is located downslope of IR-71's embankment and above IR-490 at grades approximately level with the surrounding property. The embankment slopes are roughly 2H:1V in the northeast and roughly 3H:1V in the southwest. The roadway drains to drainage ditches on the sides of the roadway while the bridge carrying the ramp over IR-490 drains to scuppers near the eastern end of the bridge. The area is moderately vegetated for the most part with no signs of standing water observed.







2.5.6. Ramp from West 7th St to IR-490 EB (Ramp 7-7C)

In general, the pavement condition along Ramp 7-7C was observed to be fair. High severity longitudinal joint cracking, D-cracking, and patching was observed as well as moderate crack sealing deficiencies (Photograph 6). Ramp 7-7C is a partial clover leaf ramp constructed atop an embankment above the surrounding land with the embankment slopes observed to be about 2H:1V. With respect to drainage, the roadway drains to the inside of the ramp towards two inlets spaced near the center of the ramp near where the ramp meets IR-490. The area is lightly vegetated for the most part with no signs of standing water observed. The area appeared to be stable with no signs of geotechnical instability during our visit.

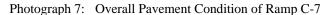


Photograph 6: Overall Pavement Condition of Ramp 7-7C

2.5.7. Ramp from IR-490 WB to West 7th St (Ramp C-7)

In general, the pavement condition along Ramp C-7 was observed to be poor. High severity longitudinal and transverse joint cracking, D-cracking, and patching was observed as well as moderate crack sealing deficiencies and bleeding of the asphalt patching (Photograph 7). The ramp extends downslope from West 7th St to IR-490 grades where the ramp appears to abut Bridge No. CUY-490-0100. The embankment slopes below the western portion of Ramp C-7 are roughly 2H:1V and in good condition. Ramp C-7 appears to drain west to east towards inlets located north of the ramp just prior to Bridge No. CUY-490-0100. The area is lightly vegetated for the most part with no signs of standing water observed. The area appeared to be stable with no signs of geotechnical instability during our visit.







2.5.8. Ramp from Rockefeller Ave to IR-490 WB (Ramp B-C)

In general, the pavement condition along Ramp B-C was observed to be fair. Moderate severity longitudinal and transverse joint cracking, D-cracking, and patching was observed as well as moderate crack sealing deficiencies (Photograph 8). The ramp extends downslope from Rockefeller Ave to IR-490 grades where the ramp appears to abut Bridge No. CUY-490-0100. The embankment slopes below the eastern portion of Ramp B-C are roughly 2H:1V and in good condition. Similar to Ramp C-7, Ramp B-C appears to drain towards inlets located north of the ramp just prior to Bridge No. CUY-490-0100. The area is lightly vegetated for the most part with no signs of standing water observed. The area appeared to be stable with no signs of geotechnical instability during our visit.



Photograph 8: Overall Pavement Condition of Ramp B-C

2.5.9. Ramp from IR-490 EB to Broadway Ave (Ramp C-B)

In general, the pavement condition along Ramp C-B was observed to be fair. Moderate severity longitudinal and transverse joint cracking and patching was observed as well as moderate crack sealing deficiencies and asphalt bleeding in the right turn lane (Photograph 9). This ramp generally consist of bridge deck with the exception of the eastern most approximate 250 ft of roadway located just west of Broadway Ave. The



portion of ramp supported by soil is constructed atop an embankment above the surrounding land roughly equal in grade with Broadway Ave. The roadway drains towards an inlet on the south side of the roadway. The area is lightly vegetated for the most part with no signs of standing water observed. The area appeared to be stable with no signs of geotechnical instability during our visit.



Photograph 9: Overall Pavement Condition of Ramp C-B

2.5.10. Ramp from IR-490 EB to IR-77 NB (Ramp S-E)

In general, the pavement condition along this section of the project was observed to be fair to poor. Moderate severity longitudinal and transverse joint cracking, D-cracking, joint spalling, and potholing was observed along this section as well as moderate crack sealing deficiencies and surface deterioration (Photograph 10). The roadway in this section is relatively level with the surrounding land. The embankment slope down to IR-490 is roughly 3H:1V to 4H:1V. The roadway slopes gradually upwards from west to east in this section. The roadway drains towards the north side of the road and off the shoulder as well as to a pair of inlets on the north side of the roadway just past where the ramp to IR-77 SB splits off. The area is lightly vegetated for the most part with no signs of standing water observed. The area appeared to be stable with no signs of geotechnical instability during our visit.



Photograph 10: Overall Pavement Condition of Ramp S-E



2.5.11. Ramp from IR-77 SB to IR-490 WB (Ramp N-W)

In general, the pavement condition along Ramp N-W was observed to be good to fair. Moderate severity longitudinal joint cracking, and patching was observed as well as light crack sealing deficiencies. The roadway in this section is situated in a cut below the surrounding land with the embankment slope up to the surrounding land observed to be about 2H:1V while the slope down to IR-490 was about 3H:1V. The roadway drains towards the north side of the road into a drainage ditch with several inlets spaced along the drainage ditch. The area is lightly vegetated for the most part with no signs of standing water observed. The area appeared to be stable with no signs of geotechnical instability during our visit.

2.5.12. Ramp from IR-490 WB to IR-77 NB (Ramp E-N)

In general, the pavement condition along Ramp E-N was observed to be fair in the northern portion and excellent in the southern portion. During our visit the northern portion of the ramp (about 500 ft) consisted of an asphalt pavement surface while the remaining southern portion consisted of a concrete surface. The asphalt portion was observed to show signs of surface wear such as moderate severity longitudinal and transverse cracking as well as moderate crack sealing deficiencies (Photograph 11). The concrete portion showed very little signs of wear at the surface. Ramp E-N is located upslope of IR-490 and downslope of an adjacent CSX railway. The embankment slopes which extended up to the adjacent CSX railway to the east are roughly 2H:1V while the slope down to IR-490 is roughly 3H:1V. With respect to drainage, the roadway drains towards the north/northeast side of the ramp into a ditches with several inlets spaced along the ditch. Standing water was observed near the location where the ramp passes underneath the CSX railroad bridge. The area appeared to be stable with no signs of geotechnical instability during our visit.



Photograph 11: Overall Pavement Condition of Ramp E-N

2.5.13. Ramp from IR-77 NB to IR-490 EB (Ramp W-N)

In general, the pavement condition along Ramp W-N was observed to be excellent at the entrance and exit portions of the ramp and fair in the central part of the ramp. The ramp has an asphalt surface at the entrance and through the central portion of the ramp with a concrete surface at the exit of the ramp. The asphalt in the central portion of the ramp was observed to show signs of surface wear consisting of moderate severity longitudinal and transverse cracking while the entrance portion appeared to be recently paved (Photograph 12). This ramp is situated above IR-490 grades and below IR-77 grades and the surrounding property in the area. The slopes up to the surrounding land to the south are roughly 2H:1V while the slope



down to IR-490 is about 3H:1V to 4H:1V. With respect to drainage, the roadway drains towards the south side of the road into drainage ditches. The area is moderately vegetated for the most part and signs of standing water were not observed. The area appeared to be stable with no signs of geotechnical instability during our visit.



Photograph 12: Pavement Condition Transition of Ramp W-N

GEOTECHNICAL EXPLORATION

2.6. Exploration Program

The subsurface exploration for the project was conducted by NEAS between July 13, 2021 and July 26, 2021 and included 53 borings each drilled to a depth of 7.5 ft bgs. The boring locations were selected by NEAS in general accordance with the guidelines contained in the SGE with the intent to evaluate subsurface soil and groundwater conditions. Borings were typically located either within existing pavement areas that are planned to undergo full-depth replacement or within areas where widening and/or realignment is planned. Target boring locations were located in the field by NEAS prior to drilling utilizing handheld GPS equipment and the boring locations were drilled in areas that were not restricted by underground utilities or dictated by terrain (i.e., steep embankment slopes). Each as-drilled project boring location and corresponding ground surface elevation was surveyed in the field following drilling. Each individual project boring log (included within Appendix B) includes the recorded boring latitude and longitude location (based on the surveyed Ohio State Plane North, NAD83, location) and the corresponding ground surface elevation. The boring locations are depicted within the boring location plan provided in Appendix A.

Borings were drilled using a CME 45B truck-mounted drilling rig utilizing 3.25-inch (inner diameter) hollow stem augers. Soil samples were typically recovered continuously to a depth of 7.5 ft bgs, using an 18-inch split spoon sampler (AASHTO T-206 "Standard Method for Penetration Test and Split Barrel Sampling of Soils."). The soil samples obtained from the exploration program were visually observed in the field by the NEAS field representative and preserved for review by a Geologist for possible laboratory testing. Standard penetration tests (SPT) were conducted using a CME auto hammer that has been calibrated on December 5, 2019 to be 81.7% efficient as indicated on the boring logs (Appendix B).

An exploration was performed to support a retaining wall which was subsequently removed from this project. This retaining wall exploration was conducted by NEAS on October 19, 2022 and included 4



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borings (B-001-1-21, B-001-2-21, B-002-1-21 and B-002-2-21) each drilled to a depth of 16.5 ft bgs. The noted boring logs are included in Appendix B.

Field boring logs were prepared by drilling personnel and included pavement description (where present), lithological description, SPT results recorded as blows per 6-inch increment of penetration and estimated unconfined shear strength values on specimens exhibiting cohesion (using a hand-penetrometer). Groundwater level observations were recorded both during and after the completion of drilling. These groundwater level observations are included on the individual boring logs (provided in Appendix B). After completing the borings, the boreholes were backfilled with either auger cuttings, bentonite chips, or a combination of these materials and patched accordingly with cold patch asphalt and/or cement when drilled through the roadway.

2.7. Laboratory Testing Program

The laboratory testing program consisted of classification testing, moisture content determinations, and sulfate content testing. Data from the laboratory testing program were incorporated onto the boring logs (Appendix B). Soil samples are retained at the laboratory for 60 days following report submittal, after which time they will be discarded.

2.7.1. Classification Testing

Representative soil samples were selected for index property (Atterberg Limits) and gradation testing for classification purposes on approximately forty percent (40%) of the samples. At each subgrade boring location, the upper two samples obtained below the proposed top of subgrade elevation were generally tested while additional samples were selected for testing with the intent of properly classifying the subsurface soil and groundwater conditions within the planned project limits. Soils not selected for testing were compared to laboratory tested samples/strata and classified visually. Moisture content testing was conducted on all samples. The laboratory testing was performed in general accordance with applicable AASHTO specifications and ODOT Supplements.

Final classification of soil strata in accordance with AASHTO M-145 "Classification of Soils and Soil-Aggregate Mixtures for Highway Construction Purposes," as modified by ODOT "Classification of Soils" was made once laboratory test results became available. The results of the soil classification are presented on the boring logs in Appendix B.

2.7.2. Standard Penetration Test Results

Standard Penetration Tests (SPT) and split-barrel (commonly known as split-spoon) sampling of soils were performed continuously in the project borings performed. To account for the high efficiency (automatic) hammers used during SPT sampling, field SPT N-values were converted based on the calibrated efficiency (energy ratio) of the specific drill rig's hammer. Field N-values were converted to an equivalent rod energy of 60% (N_{60}) for use in analysis or for correlation purposes. The resulting N_{60} values are shown on the boring logs provided in Appendix B.

2.7.3. Sulfate Testing

Sulfate testing was generally performed on one sample from each subgrade/roadway boring performed for pavement/subgrade design purposes. The selected samples were tested in accordance with ODOT Supplement 1122, "Determining Sulfate Content in Soils" dated July 17, 2015. In general, the upper most sample (within 3 ft of the proposed subgrade elevation) from each boring was tested when feasible. Testing



results are summarized in Table 2 below, provided in Appendix C and presented on the boring logs within Appendix B.

Average Sulfate Dilution Average Sulfate Boring ID **Boring ID** Sample Depth (ft) Sample Depth (ft) Ratio Content (ppm) Ratio Content (ppm) B-001-0-21 SS-1 1.5-3.0 20 1433 B-028-0-21 SS-1 1.5-3.0 93 20 B-002-0-21 SS-1 1.5-3.0 20 227 B-029-0-21 1.5-3.0 300 SS-1 20 B-003-0-21 SS-1A 1.5-2.2 20 647 B-030-0-21 SS-1 1.5-3.0 20 873 B-004-0-21 1.5-3.0 693 B-031-0-21 1.5-3.0 100 SS-1 20 SS-1 20 B-005-0-21 SS-1 1.5-3.0 20 487 B-032-0-21 SS-1 1.5-3.0 20 960 1.5-3.0 1187 B-033-0-21 1.5-3.0 B-006-0-21 SS-1 40 SS-1 20 733 1.5-3.0 B-034-0-21 B-007-0-21 1413 SS-1 20 193 SS-1 1.5-3.0 20 B-008-0-21 SS-1 1.5-3.0 40 1280 B-035-0-21 SS-1 1.5-3.0 20 153 B-009-0-21 SS-1 1.5-3.0 20 313 B-036-0-21 SS-1 1.5-3.0 20 367 B-010-0-21 1.5-3.0 B-037-0-21 20 553 SS-1 20 860 B-011-0-21 1.5-3.0 40 2120 B-038-0-21 SS-1 1.5-3.0 20 340 1.5-3.0 1.5-3.0 B-012-0-21 SS-1 20 733 B-039-0-21 SS-1 20 793 1.5-3.0 900 1.5-3.0 B-013-0-21 SS-1 20 B-040-0-21 SS-1 20 413 B-014-0-21 SS-1 1.5-3.0 40 2133 B-041-0-21 SS-1 1.5-3.0 100 2800 B-015-0-21 1.5-3.0 B-042-0-21 SS-1 100 2367 SS-1 1.5-3.0 1300 B-016-0-21 SS-1 1.5-3.0 20 973 B-043-0-21 SS-1 1.5-3.0 20 933 1.5-3.0 B-017-0-21 SS-1 20 0 B-044-0-21 SS-1 1.5-3.0 20 1080 B-018-0-21 SS-1 1.5-3.0 20 627 B-045-0-21 SS-1 1.5-3.0 20 340 B-019-0-21 1.5-3.0 20 SS-1 820 B-046-0-21 SS-1 1.5-3.0 20 253 B-020-0-21 SS-1A 1.5-2.7 40 2600 B-047-0-21 1.5-3.0 20 67 SS-1 B-021-0-21 SS-1 1.5-3.0 40 1400 B-048-0-21 SS-1 1.5-3.0 2387 1.5-3.0 20 400 B-049-0-21 B-022-0-21 SS-1

1573

133

560

73

240

SS-1

SS-1

SS-1

SS-1

B-050-0-21

B-051-0-21

B-052-0-21

B-053-0-21

1.5-3.0

1.5-3.0

1.5-3.0

1.5-3.0

20

100

20

20

1100

3000

40

347

Table 2: Sulfate Test Summary by Boring

3. FINDINGS

B-023-0-21

B-024-0-21

B-025-0-21

B-026-0-21

B-027-0-21

SS-1

SS-1

SS-1

SS-1

SS-1

1.5-3.0

1.5-3.0

1.5-3.0

1.5-3.0

1.5-3.0

40

20

20

20

20

The subsurface conditions encountered during NEAS's explorations are described in the following subsections and/or on each boring log presented in Appendix B. The boring logs represent NEAS's interpretation of the subsurface conditions encountered at each boring location based on our site observations, field logs, visual review of the soil samples by NEAS's geologist, and laboratory test results. The lines designating the interfaces between various soil strata on the boring logs represent the approximate interface location; the actual transition between strata may be gradual and indistinct. The subsurface soil and groundwater characterizations included herein, including summary test data, are based on the subsurface findings from the geotechnical explorations performed by NEAS as part of the referenced project. It should be noted that for the purposes of this report and our analysis the term 'subgrade' has been assumed to represent soils and/or soil conditions from 1.5 ft below proposed final pavement grades to a depth of 7.5 ft below the proposed pavement grades.

3.1. Existing Pavement

The pavement section thicknesses in terms of asphalt, concrete and granular base were measured at representative project subgrade borings during the subsurface exploration for the project and are recorded



on the test boring logs provided in Appendix B. A summary of these measurements is provided in Table 3 below.

Concrete Base Total **Asphalt** Concrete Base Total Drilled Drilled Proposed Proposed Thickness **Boring ID** Thickness Thickness Thickness **Boring ID** hickness Thickness Thickness Thickness Depth (ft) Depth (ft) Alignment Alignment (in) (in) (in) (in) (in) (in) (in) (in) B-001-0-21 IR-490 7.5 4.0 8.0 6.0 18.0 B-026-0-21 Lane E-S 7.5 6.0 7.0 0.0 13.0 B-002-0-21 IR-490 7.5 4.0 8.0 6.0 18.0 B-027-0-21 Lane E-S 7.5 4.0 6.0 0.0 10.0 B-003-0-21 IR-490 7.5 4.0 8.0 6.0 18.0 B-028-0-21 Lane E-S 4.0 0.0 12.0 7.5 8.0 B-004-0-21 IR-490 7.5 5.0 9.0 6.5 20.5 B-029-0-21 Ramp 7-7C 7.5 0.0 10.0 7.0 17.0 B-005-0-21 IR-490 7.5 4.0 8.0 6.0 18.0 B-030-0-21 Ramp 7-7C 7.5 0.0 10.0 7.0 17.0 B-033-0-21 B-006-0-21 IR-490 7.5 0.0 10.0 17.0 Ramp C-7 10.0 8.0 18.0 7.0 7.5 0.0 B-007-0-21 IR-490 7.5 6.0 6.0 0.0 12.0 B-034-0-21 Ramp C-7 7.5 0.0 8.0 9.0 17.0 B-008-0-21 IR-490 7.5 0.0 10.0 7.0 17.0 B-035-0-21 Ramp B-C 7.5 0.0 8.0 8.0 16.0 B-009-0-21 IR-490 5.0 0.0 13.0 B-036-0-21 Ramp B-C 14.0 8.0 0.0 6.0 8.0 B-010-0-21 IR-490 7.5 0.0 8.0 8.0 16.0 B-037-0-21 Ramp N-W 0.0 8.0 8.0 16.0 7.5 B-011-0-21 IR-490 7.5 6.5 0.0 14.0 B-038-0-21 Ramp N-W 7.5 0.0 8.0 8.0 16.0 B-012-0-21 IR-490 7.5 0.0 10.0 18.0 B-039-0-21 Ramp N-W 7.5 8.0 9.0 17.0 8.0 0.0 B-013-0-21 IR-490 7.5 8.0 6.0 0.0 14.0 B-040-0-21 Ramp N-W 7.5 0.0 6.0 8.0 14.0 17.0 B-042-0-21 Ramp W-N 17.0 B-014-0-21 IR-490 7.5 0.0 8.0 9.0 7.5 0.0 8.0 9.0 B-015-0-21 IR-490 7.5 0.0 8.0 9.0 17.0 B-043-0-21 Ramp W-N 7.5 0.0 8.0 8.0 16.0 IR-490 7.5 0.0 8.0 8.0 16.0 B-044-0-21 Ramp C-B 7.5 0.0 8.0 7.5 15.5 B-016-0-21 B-045-0-21 Ramp C-B B-017-0-21 IR-490 7.5 0.0 8.0 8.0 16.0 7.5 0.0 8.0 7.5 15.5 Ramp S-E B-018-0-21 IR-490 7.5 0.0 14.0 B-046-0-21 4.0 6.0 16.0 8.0 6.0 7.5 6.0 B-019-0-21 IR-490 7.5 0.0 8.0 8.0 16.0 B-047-0-21 Ramp S-E 7.5 4.0 8.0 6.0 18.0 B-020-0-21 IR-490 7.5 0.0 8.0 6.0 14.0 B-048-0-21 Ramp S-E 0.0 8.0 8.0 16.0 B-021-0-21 IR-490 0.0 8.0 8.0 16.0 B-049-0-21 0.0 8.0 7.5 15.5 Ramp S-E IR-490 7.5 4.0 0.0 12.0 B-050-0-21 Ramp E-N 7.5 8.0 7.5 15.5 B-022-0-21 8.0 0.0 B-023-0-21 7.5 4.0 0.0 0.0 10.0 7.0 17.0 Lane E-S 8.0 12.0 B-051-0-21 Ramp E-N 7.5 B-024-0-21 Lane E-S 7.5 4.0 7.0 0.0 11.0 B-052-0-21 Ramp E-N 7.5 4.0 8.0 6.0 18.0

Table 3: Measured Pavement Thickness at Boring Locations

3.2. Subgrade Conditions

7.5

4.0

8.0

0.0

B-025-0-21 Lane E-S

The subgrade conditions within the project limits are relatively consistent and are generally comprised of either fill soils (i.e., embankment fill) or natural soils consisting of gravel, sand and silt, or low to moderately plastic sandy silt and silt/clay combinations. The subgrade soils encountered within the project limits are generally classified as either A-1-a, A-1-b, A-2-4, A-3, A-3a, A-4a, A-4b type soils. With respect to sulfate within the subgrade soil, based on the project laboratory testing program, each subgrade soil sample tested was determined to have a sulfate content of less than 5,000 parts per million (ppm) (i.e., lower than the level which ODOT considers high and may prevent the use of chemical stabilization).

12.0

B-053-0-21 Ramp E-N

7.5

4.0

8.0

6.0

18.0

The following subsections present a brief summary of the subsurface conditions by ramp/roadway segment with problem areas highlighted where present.

3.2.1. *IR-490 Mainline*

The project portions of IR-490 are planned to undergo full depth pavement replacement. The borings performed along this portion of roadway included historical borings B-109-0-20 through B-112-0-20 as well as project borings B-001-0-21 through B-022-0-21.

Along IR-490, nineteen percent (19%) of the soil samples were identified as fine-grained soils and were comprised of cohesive Sandy Silt (A-4a, 11% of samples) and Silt (A-4b, 8% of samples). With respect to the consistency of the fine-grained soils, the descriptions varied from stiff to hard correlating to converted



SPT-N values (N_{60}) between 15 and 42 blows per foot (bpf). Natural moisture contents ranged from 10 to 19 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along the project portions of IR-490, the liquid and plastic limits ranged from 21 to 27 percent and from 16 to 21 percent, respectively.

Eighty-one percent (81%) of the samples taken along the proposed roadway were classified as coarse-grained, non-cohesive soils and were comprised of: 1) Gravel (A-1-a, 6% of samples); 2) Gravel with Sand (A-1-b, 8% of samples); 3) Gravel and Stone Fragments with Sand and Silt (A-2-4, 9% of samples); 4) Fine Sand (A-3, 4% of samples); 5) Coarse and fine sand (A-3a, 27% of samples); 6) non-cohesive Sandy Silt (A-4a, 12% of samples); and, 7) non-cohesive Silt (A-4b, 14% of samples). With respect to the relative density of the coarse-grained soils, the descriptions varied from medium dense to dense correlating to N_{60} values between 12 and 50 bpf. Natural moisture contents ranged from 4 to 26 percent.

3.2.2. Lane E-S

Lane E-S is the exit ramp from the IR-490 WB to IR-71 SB which is planned for full depth pavement replacement. The borings performed along lane E-S included borings B-023-0-21 through B-028-0-21.

Along Lane E-S, ninety-two percent (92%) of the soil samples were identified as coarse-grained, non-cohesive soils and were comprised of Gravel with Sand (A-1-b, 38% of samples) and Coarse and Fine Sand (A-3a, 54% of samples). With respect to the relative density of the coarse-grained soils, the descriptions varied from medium dense to very dense correlating to N_{60} values between 12 and 52 bpf. Natural moisture contents ranged from 5 to 17 percent.

Eight percent (8%) of the samples taken along the proposed roadway were classified as fine-grained soils and were comprised of Silt (A-4b, 2 samples). With respect to the consistency of the fine-grained soils, the soil can be described as very stiff correlating to N_{60} values between 18 and 29 bpf. Natural moisture contents ranged from 14 to 20 percent.

3.2.3. Ramp 7-7C

Ramp 7-7C is the exit ramp from West 7^{th} St to IR-490 EB which is planned for full depth pavement replacement. The borings performed along Ramp 7-7C included boring B-012-0-21 as well as borings B-029-0-21 through B-032-0-21.

Sixty percent (60%) of the samples taken along the ramp were classified as coarse-grained, non-cohesive soils and were comprised of Gravel and Stone Fragments with Sand and Silt (A-2-4, 20% of samples), Coarse and Fine Sand (A-3a, 20% of samples) and non-cohesive Silt (A-4b, 20% of samples). With respect to the relative density of the coarse-grained soils, the descriptions varied from medium dense to very dense correlating to N_{60} values of 15 and 63 bpf. Natural moisture contents ranged from 6 to 15 percent.

Forty percent (40%) of the soil samples taken along the proposed ramps were identified as fine-grained soils and were comprised of cohesive Sandy Silt (A-4a, 40% of samples). With respect to the consistency of the fine-grained soils, the descriptions varied from very stiff to hard correlating to N_{60} values between 23 and 56 bpf. Natural moisture contents ranged from 11 to 13 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along Ramps 7-7C, the liquid and plastic limits ranged from 23 to 29 percent and from 16 to 22 percent, respectively.



3.2.4. Ramp C-7

Ramp C-7 is the entrance ramp for West 7th St to IR-490 WB which is planned for full depth pavement replacement. The borings performed along Ramp C-7 included borings B-033-0-21 and B-034-0-21.

Sixty-three percent (63%) of the soil samples taken along the proposed ramps were identified as fine-grained soils and were comprised of cohesive Sandy Silt (A-4a, 13% of samples) and Silt (A-4b, 50% of samples). With respect to the consistency of the fine-grained soils, the descriptions varied from stiff to very stiff correlating to N₆₀ values between 14 and 18 bpf. Natural moisture contents ranged from 15 to 21 percent. Based on Atterberg Limit tests performed a representative sample of the fine-grained subgrade soils obtained along Ramp C-7, the liquid and plastic limits are 29 percent and 22 percent, respectively.

Thirty-seven percent (37%) of the samples taken along the ramp were classified as coarse-grained, non-cohesive soils and were comprised of Gravel with Sand (A-1-b, 12% of sample) and Gravel with Stone Fragments (A-1-a, 25% of samples). With respect to the relative density of the coarse-grained soils, the soils can be described as medium dense correlating to N_{60} values between 20 and 25 bpf. Natural moisture contents of the non-cohesive samples ranged from 7 to 9 percent.

3.2.5. Ramp B-C

Ramp B-C is the entrance ramp from Rockefeller Ave to IR-490 WB which is planned for full depth pavement replacement. The borings performed along Ramp B-C included borings B-035-0-21 and B-036-0-21.

One hundred percent (100%) of the samples taken along the ramp were classified as coarse-grained, non-cohesive soils and were comprised of Coarse and Fine Sand (A-3a, 63% of samples) and non-cohesive Sandy Silt (A-4a, 37% of samples). With respect to the relative density of the coarse-grained soils, the soil can be described as medium dense to dense correlating to N_{60} values between 11 and 31 bpf. Natural moisture contents of the non-cohesive samples ranged from 9 to 15 percent.

3.2.6. Ramp N-W

Ramp N-W is the IR-490 WB exit ramp from IR-71 SB which is planned for full depth pavement replacement. The borings performed along Ramps M and N included borings B-037-0-21 through B-040-0-21.

One hundred percent (100%) of the soil samples were identified as coarse-grained soils and were comprised of: 1) Gravel with Sand (A-1-b, 25% of sample); 2) Coarse and Fine Sand (A-3a, 50% of samples); and, 3) Fine Sand (A-3, 25% of samples). With respect to the consistency of the coarse-grained soils, the soils can be described as medium dense to dense correlating to N_{60} values between 11 and 41 bpf. Natural moisture contents ranged from 4 to 11 percent.

3.2.7. Ramps W-N

Ramps W-N is the IR-490 EB to IR-71 NB ramp which is planned for full depth pavement replacement. The borings performed along Ramp W-N included borings B-041-0-21 through B-043-0-21.

One hundred percent (100%) of the samples taken along the proposed ramps were classified as coarse-grained, non-cohesive soils and were comprised of Gravel with Sand (A-1-b, 42% of samples) and Coarse and Fine Sand (A-3a, 58% of samples). With respect to the relative density of the coarse-grained soils, descriptions ranged from medium dense to dense correlating to N_{60} values between 23 and 50 bpf. Natural moisture contents ranged from 4 to 30 percent.



3.2.8. Ramp C-B

Ramp C-B is the IR-490 EB exist ramp to Broadway Ave which is planned for full depth pavement replacement. The borings performed along Ramp C-B included borings B-044-0-21 and B-045-0-21.

One hundred percent (100%) of the samples taken along the ramp were classified as coarse-grained, non-cohesive soils and were comprised of: 1) Gravel with Sand (A-1-b, 50% of samples); 2) Coarse and Fine Sand (A-3a, 38% of samples); and, 3) Gravel with stone fragments (A-1-a, 12% of samples). With respect to the relative density of the coarse-grained soils can be described as medium dense correlating to N_{60} values between 11 and 18 bpf. Natural moisture contents ranged from 4 to 14 percent.

3.2.9. Ramp S-E

Ramp S-E is the IR-71 NB to IR-490 EB which is planned for full depth pavement replacement. The borings performed along Ramp S-E included borings B-046-0-21 through B-049-0-21.

Eighty-seven percent (87%) of the samples taken along the ramp were classified as coarse-grained, non-cohesive soils and were comprised of Gravel with Sand (A-1-b, 25% of samples) and Coarse and Fine Sand (A-3a, 62% of samples). With respect to the relative density of the coarse-grained soils, descriptions ranged from loose to dense correlating to N_{60} values between 10 and 38 bpf. Natural moisture contents ranged from 6 to 27 percent.

Thirteen percent (13%) of the soil samples taken along the proposed ramps were identified as fine-grained soils and were comprised of Silt (A-4b, 2 samples). With respect to the consistency of the fine-grained soils, the soil can be described as very stiff correlating to N_{60} values between 25 and 26 bpf. Natural moisture contents ranged from 15 to 16 percent. Based on Atterberg Limit tests performed on a representative sample of the fine-grained subgrade soils obtained along Ramp S-E, the liquid and plastic limits are 25 percent and 19 percent, respectively. Natural moisture contents ranged from 15 to 16 percent.

3.2.10. Ramp E-N

Ramp E-N is the IR-490 WB to IR-71 NB ramp from which is planned for full depth pavement replacement. The borings performed along Ramp E-N included borings B-050-0-21 through B-053-0-21.

Eighty-eight percent (88%) of the samples taken along the ramp were classified as coarse-grained, non-cohesive soils and were comprised of: 1) Gravel with Sand (A-1-b, 31% of samples); 2) Coarse and Fine Sand (A-3a, 38% of samples); and, 3) Sandy Silt (A-4a, 19% of samples). With respect to the relative density of the coarse-grained soils, descriptions ranged from medium dense to very dense correlating to N_{60} values between 14 and 56 bpf. Natural moisture contents ranged from 6 to 45 percent.

Twelve percent (12%) of the soil samples taken along the ramp were identified as fine-grained soils and were comprised of cohesive Sandy Silt (A-4a, 2 samples). With respect to the consistency of the fine-grained soils, the soil can be described as very stiff correlating to N_{60} values between 20 and 22 bpf. Natural moisture contents ranged from 10 to 12 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along Ramp E-N, the liquid and plastic limits are between 19 to 25 percent and 14 to 15 percent, respectively.

3.2.11. Groundwater

Groundwater was observed within proposed subgrade depths during drilling in four (4) of the borings (B-002-0-21, B-006-0-21, B-011-0-21, and B-024-0-21) performed as part of the exploration. Based on measurements at each boring location, groundwater was encountered at depths ranging from 3 ft to 5.5 ft



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(elevations ranging from 620.7 ft amsl to 647.3 ft amsl). It should be noted that groundwater is affected by many hydrologic characteristics in the area and may vary from those measured at the time of the exploration. The specific groundwater readings are included on the individual test boring logs located within Appendix В.

ANALYSES AND RECOMMENDATIONS

We understand that reconstruction of a portion of IR-490 mainline freeway as well as the reconstruction of various adjacent ramps are planned as part of the major rehabilitation project (CUY-490-0.00, PID 107408). In addition to the mainline freeway segment, full depth pavement replacement of the associated entrance/exit ramps (Lane E-S, Ramp C-7, Ramp 7-C, Ramp 7-7C, Ramp B-C, Ramp C-B, Ramp N-W, Ramp W-S, Ramp W-N, Ramp E-N and Ramp S-E) is also planned. For this purpose, a subgrade exploration and subsequent analysis was completed for the referenced project. The analysis completed for the proposed reconstruction included a subgrade analysis performed in accordance with ODOT's GDM criteria utilizing the ODOT provided GB1: Subgrade Analysis Spreadsheet (GB1 Subgrade Analysis.xls, Version 14.5 dated January 18, 2019). Input information for the spreadsheet was based on the soil characteristics gathered during both historical explorations and NEAS's subgrade exploration (i.e., SPT results, laboratory test results, etc.). A subgrade analysis was performed for the entire project as well as for each of the referenced mainline and ramp segments individually.

Based on our evaluation of the subsurface conditions and our geotechnical engineering analyses of the proposed reconstruction, it is our opinion that subgrade conditions are generally satisfactory, and pavement can be supported by the underlying subsurface material utilizing 12-inches of chemical stabilization (global stabilization) per ODOT's GDM, though certain segments of mainline IR-490 Ramp 7-7C and Ramp C-7 where unsuitable soils were encountered, may require additional stabilization beyond the recommended 12-inches. Further detail regarding our subgrade analysis and the recommended remediation are provided in Section 5.1 and Section 5.2 of this report, respectively.

4.1. **Subgrade Analysis**

A subgrade analysis was performed to identify the method, location, and dimensions (including depth) of required subgrade stabilization for the project. In addition to identifying stabilization recommendations, pavement design parameters are also determined to aid in pavement section design. The subsections below present the results of our subgrade analysis including pavement design parameters and unsuitable subgrade conditions identified within the project limits. Subgrade analysis spreadsheets are provided in Appendix D.

Again, it should be noted that for the purposes of this report and our analysis, the term 'proposed subgrade' has been assumed to represent soils and/or soil conditions from 1.5 ft below proposed final pavement grades to a depth of 7.5 ft below the proposed pavement grades.

4.1.1. Pavement Design Recommendations

It is our understanding that pavement analysis and design is to be performed to determine the proposed pavement sections for the segments within the project limits to undergo full depth replacement. A subgrade analysis was performed using the subgrade soil data obtained during our field exploration program to evaluate the soil characteristics and develop pavement parameters for use in pavement design. The subgrade parameters recommended for use in pavement design are presented in Table 4 below. Provided in the table are ranges of maximum, minimum and average N_{60L} values for the indicated segments as well as the design CBR value recommended for use in pavement design.



Table 4: Pavement Design Values

Segment	Maximum N _{60L}	Minimum N _{60L}	Average N _{60L}	Average PI Values	Design CBR
Mainline I-490	30	14	22	7	9
Lane E-S (WB-490 to SB-71)	27	12	20	NP	13
Ramp 7-7C (NB 7th St to EB-490)	30	15	25	7	8
Ramp C-7 (WB-490 to 7th St)	18	14	16	7	7
Ramp B-C (Rockefeller Ave to WB-490)	19	11	15	NP	9
Ramp N-W (SB-77 to WB-490)	22	11	16	NP	13
Ramp W-N (EB-490 to NB-77)	27	23	25	NP	13
Ramp C-B (EB-490 to Broadway Ave)	12	11	12	NP	13
Ramp S-E (NB-77 to EB-490)	25	10	15	6	12
Ramp E-N (WB-490 to NB-77)	25	14	21	6	11
Entire Project	30	10	20	7	10

4.1.2. Unsuitable Subgrade

Per ODOT's GDM, the presence of select subgrade conditions (i.e., unsuitable) are prohibited within the subgrade zone for new pavement construction. These unsuitable subgrade conditions generally include the presence of rock and specific soil types. With respect to the proposed pavement construction and realignment project these subgrade conditions are further discussed in the following subsections.

4.1.2.1. Unsuitable Soils

Unsuitable soil types per the GDM, which include A-4b, A-2-5, A-5, A-7-5, A-8a, A-8b, and soils with liquid limits greater than 65, were encountered within the subgrade of the referenced project roadway segments. Soil Type A-4b (Silt) was encountered within eight (8) borings performed along the project portion of IR-490 mainline, Ramp 7-7C, and Ramp C-7. A summary of the prohibited soils encountered and the associated GDM recommended remediation depths are shown in Table 5 below.

Table 5: Prohibited Soils Location Summary

	Prohibited	Donth Bolow	Remediation	Depth (inches)
Boring ID	Soil Type	Depth Below Subgrade (ft)	Excavate and Replace (Item 204 w/ Geotextile)	Chemical Stabilization (Item 206)
		Mai	nLine IR-490	
B-002-0-21	A-4b	2.0 - 2.5	36	14
B-003-0-21	A-4b	1.8 - 2.6	36	14
B-004-0-21	A-4b	1.5 - 3.5	36	14
B-012-0-21	A-4b	1.5 - 4.1	36	14
B-013-0-21	A-4b	3.0 - 9.0	36	14
B-018-0-21	A-4b	1.1 - 5.6	36	14
B-020-0-21	A-4b	1.2 - 2.2	36	14
		R	amp 7-7C	
B-012-0-21	A-4b	0.0-5.7	36	14
		F	Ramp C-7	
B-033-0-21	A-4b	0.0 - 6.4	36	14

4.1.3. Unstable Soils

The GDM recommends subgrade stabilization for soils considered unstable in which the N_{60} value of a particular soil sample (SS) at a referenced boring location is less than 12 bpf and in some cases less than 15 bpf (i.e., where moisture content is greater than optimum plus 3 percent). Based on the specific N_{60} value



at the subject boring, *Figure B - Subgrade Stabilization* within the GDM recommends a depth of subgrade stabilization for ODOT standard stabilization methods. It should be noted that *Figure B - Subgrade Stabilization* does not apply to soil types A-1-a, A-1-b, A-3, or A-3a, nor to soils with N_{60L} values of 15 or more. Per GDM guidance, *these soils should be reworked to stabilize the subgrade*. It should be noted that although a soil sample's N₆₀ value may meet the criteria to be considered an unstable soil, the depth in which the unstable soil is encountered in relation to the proposed subgrade is considered when each individual subgrade boring is analyzed. For example, if the GDM recommends an excavate and replace of 12 inches within a weak soil underlying 18 inches of stable material, it would be unreasonable to recommend the removal of both the stable and unstable material for a total of 30 inches of excavate and replace.

Within the subject project roadway no soil samples collected during our exploration met the N_{60} value criteria to be considered unstable with the exception of samples classified as soil types A-1-a, A-1-b, A-3, or A-3a for which *Figure B - Subgrade Stabilization* does not apply.

4.1.3.1. High Moisture Content Soils

High moisture content soils are defined by the GDM as soils that exceed the estimated optimum moisture content (per *Table 600-1: Optimum Moisture Content* within the GDM) for a given classification by 3 percent or more. Per the GDM, soils determined to be above the identified moisture content levels are a likely indication of the presence of an unstable subgrade and may require some form of subgrade stabilization. Similar to our analysis of unstable soils, although a soil sample's moisture content may meet the criteria to be considered high, the depth in which the high moisture soil is encountered in relation to the proposed subgrade is considered when each individual subgrade boring is analyzed for stabilization recommendations. Summaries of the boring locations where high moisture content conditions were encountered in the top 3 ft of subgrade within the limits of each proposed roadway segment are shown in Table 6 below.

Moisture Optimum Moisture Depth Below **Boring ID** Content (%) Content (%) Subgrade (ft) MainLine IR-490 B-109-0-20 0.0 - 2.9 B-004-0-21 10 1.5 - 2.0 14 B-012-0-21 14/15 10 0.0 - 2.6 B-013-0-21 17 10 3.0 - 9.0 B-018-0-21 14/20 10 0.0 - 2.6 B-019-0-21 16/19 10 0.0 - 2.7 B-020-0-21 14/19 1.2 - 2.2 10 Ramp 7-7C B-012-0-21 14/15 0.0 - 2.7

Table 6: High Moisture Content Soils Location Summary

4.2. Stabilization Recommendations

4.2.1. Subgrade Stabilization

Based on the results of our analysis, subgrade soils designated by ODOT's GDM as both "unstable" and "unsuitable" were present at various locations throughout the project. Subgrade soils designated as "unsuitable" consisted of soils classifying as A-4b (Silt) and were encountered within subgrade depths that require remediation in seven (7) borings (B-002-0-21, B-003-0-21, B-004-0-21, B-012-0-21, B-013-0-21, B-018-0-21 and B-020-0-21) performed along IR-490 Mainline, one (1) boring (B-012-0-21) performed on



PID: 107408

Ramp 7-7C, and one (1) boring (B-033-0-21) performed on Ramp C-7. Subgrade soils designated as "unstable" via high moisture content were encountered at the various locations identified in Section 4.1.3.1 of this report. Although these materials were encountered throughout the site, guidance from ODOT's GDM states that "For all Interstates and other divided highways with four or more lanes more than 1-mile in project length, the subgrade of the entire project shall be chemically stabilized (global stabilization), except where it is determined that soil is present where a majority of sulfate content values are found to be greater than 3,000 parts per million (ppm), or individual soil samples with sulfate contents greater than 5,000 ppm are present" and therefore global chemical stabilization is recommended for the proposed rehabilitation project except where otherwise indicated in this report.

The global chemical stabilization of the referenced mainline and ramp subgrade soils included within this project, should be performed to a minimum depth of 12 inches utilizing cement as the stabilizing chemical. The stabilization efforts should extend a minimum of 18-inches beyond the edge of the paved roadway, shoulder or median. The mix design should be conducted in accordance with ODOT's CMS Supplement 1120 (Mixture Design for Chemically Stabilized Soils). For design purposes it may be assumed that the cement addition will be 5% using the following formula.

Cement: $C = 0.75 \times T \times 115 \times 0.05$

Where:

C = amount of chemical in pounds / square yard and

T =thickness of the treatment zone in inches

A dry density of 115-pounds per cubic foot (pcf) is assumed.

For areas where "unsuitable" A-4b (Silt) soils were encountered, it is recommended that either Excavate and Replace with geotextile (Item 204) be performed to a depth of 36 inches below the proposed top of subgrade, or chemical stabilization be performed to a depth of 14 inches. Our minimum recommended limits for the indicated project subgrade stabilization are provided in Table 7 below. Although, the minimum recommended limits are presented below, NEAS recommends that chemical stabilization be performed to a depth of 14 inches for the *whole* project portion of IR-490. NEAS recommends chemical stabilization to 14 inches along IR-490 because: 1) approximately 40% of the project portion of IR-490 requires 14 inches of chemical stabilization due to A-4b soil and these soils are spread throughout; 2) due to the 400 ft boring spacing, the presence of A-4b could be more prevalent at the site then identified and as chemical stabilization is to be performed, construction field quality control will not be able to verify or disprove the presence of A-4b soils within 3 feet of the planned subgrade; 3) it is our opinion that a consistent pavement section (including subgrade improvements) along the IR-490 project limits will yield superior performance for the project especially with respect to drainage and frost susceptibility; and, 4) for ease of construction purposes.



Table 7: Stabilization Recommendations

Start Station	End Station	Excavate and Replace w/ Item 204 ⁽¹⁾ (inches)	Chemical Stabilization (inches)	Unsuitable Subgrade Conditions	Borings Considered
			IR-490 Mainli	ne	
Begin Work	940+74	12	12	-	Global Stabilization
940+74	952+00	36	14	A-4b (Silt)	B-002-0-21, B-003-0-21, B-004-0-21
952+00	977+76	12	12	-	Global Stabilization
977+76	984+05	36	14	A-4b (Silt)	B-012-0-21, B-013-0-21
984+05	1031+11	12	12	-	Global Stabilization
1031+11	End Work	36	14	A-4b (Silt)	B-018-0-21, B-020-0-21
		Ram	p 7-7 C (NB 7th S	to EB-490)	
Begin Work	End Work	36	14	A-4b (Silt)	B-012-0-21
		Ra	mp C-7 (WB-490	to 7th St)	
Begin Work	End Work	36	14	A-4b (Silt)	B-033-0-21
	Remainder	of Project (Lane E-S, Ramp	B-C, Ramp N-W,	Ramp W-N, Ramp C-B, F	Ramp S-E, Ramp E-N)
Begin Work	End Work	12	12	-	Global Stabilization
Notes:	Excavate and Rep	lace depths for areas where Che	emical Stabilization is	s not feasible.	

It should be noted that per ODOT's GDM, typical chemical stabilization equipment cannot stabilize areas less than 8 ft in width. If it is anticipated that the project will require multiple maintenance of traffic phases, it is recommended that the roadway work is coordinated with the maintenance of traffic schemes in such a way that an 8-ft minimum width for chemical stabilization exists. If areas of less than 8 ft in width are anticipated, subgrade soils may be excavated out, mixed with stabilization chemical, and compacted in place, though this method is not practical for large areas



5. QUALIFICATIONS

This investigation was performed in accordance with accepted geotechnical engineering practice for the purpose of characterizing the subsurface conditions along the referenced portions of roadways. This report has been prepared for GPD, ODOT and their design consultants to be used solely in evaluating the subgrade soils within the project limits and presenting geotechnical engineering recommendations specific to this project. The assessment of general site environmental conditions or the presence of pollutants in the soil, rock and groundwater of the site was beyond the scope of this geotechnical exploration. Our recommendations are based on the results of our field explorations, laboratory test results from representative soil samples, and geotechnical engineering analyses. The results of the field explorations and laboratory tests, which form the basis of our recommendations, are presented in the appendices as noted. This report does not reflect any variations that may occur between the borings or elsewhere on the site, or variations whose nature and extent may not become evident until a later stage of construction. In the event that any changes occur in the nature, design or location of the proposed interstate rehabilitation work, the conclusions and recommendations contained in this report should not be considered valid until they are reviewed and have been modified or verified in writing by a geotechnical engineer.

It has been a pleasure to be of service to GPD Group in performing this geotechnical exploration for the CUY-490-00.00 major rehabilitation project. Please call if there are any questions, or if we can be of further service.

Respectfully Submitted,

Brendan P. Andrews, P.E. *Project Geotechnical Engineer*

Derar Tarawneh, Ph.D., E.I. Geotechnical Staff Engineer

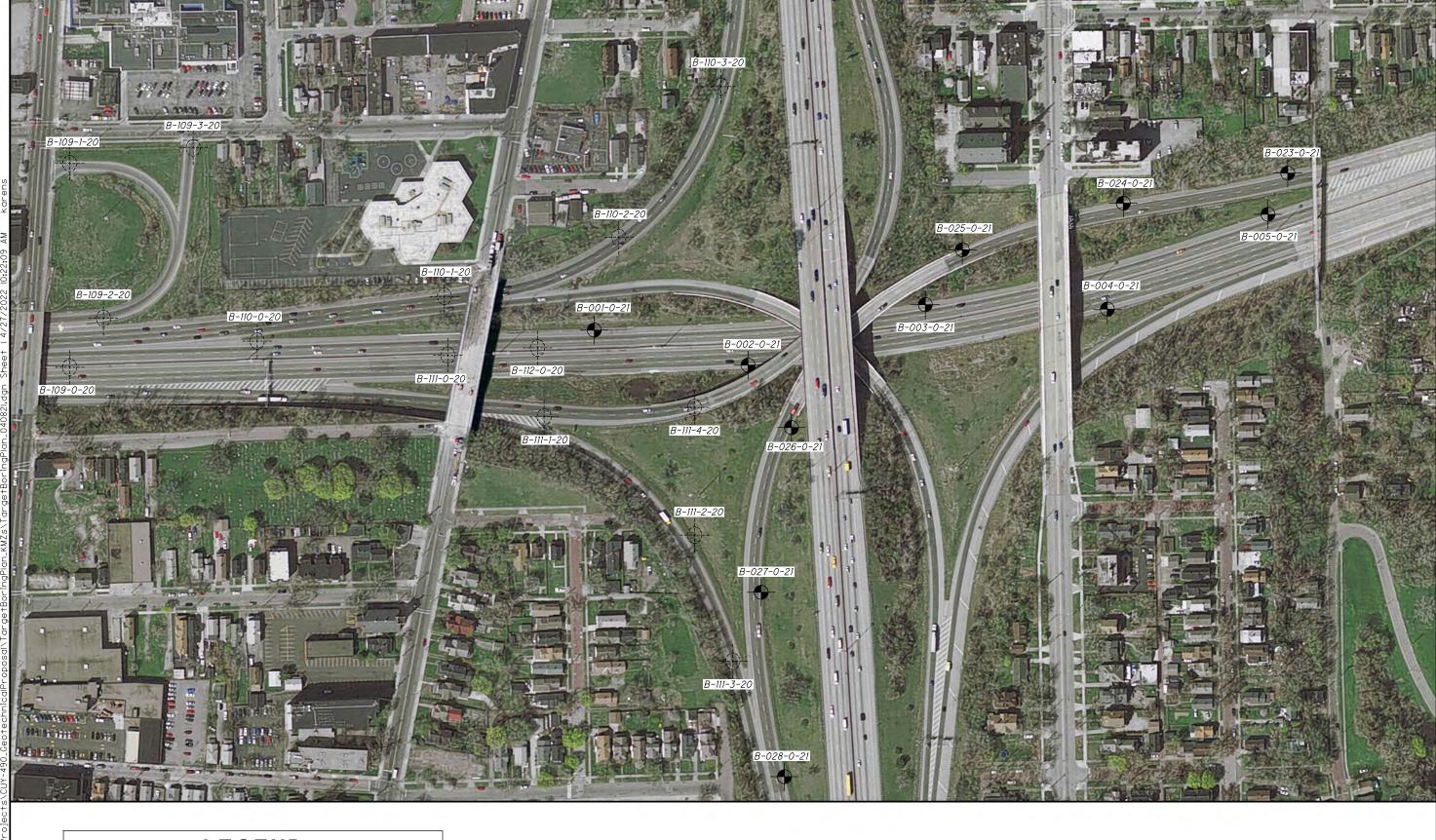


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APPENDIX A BORING LOCATION PLAN



LEGEND

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PROJECT BORING LOCATION

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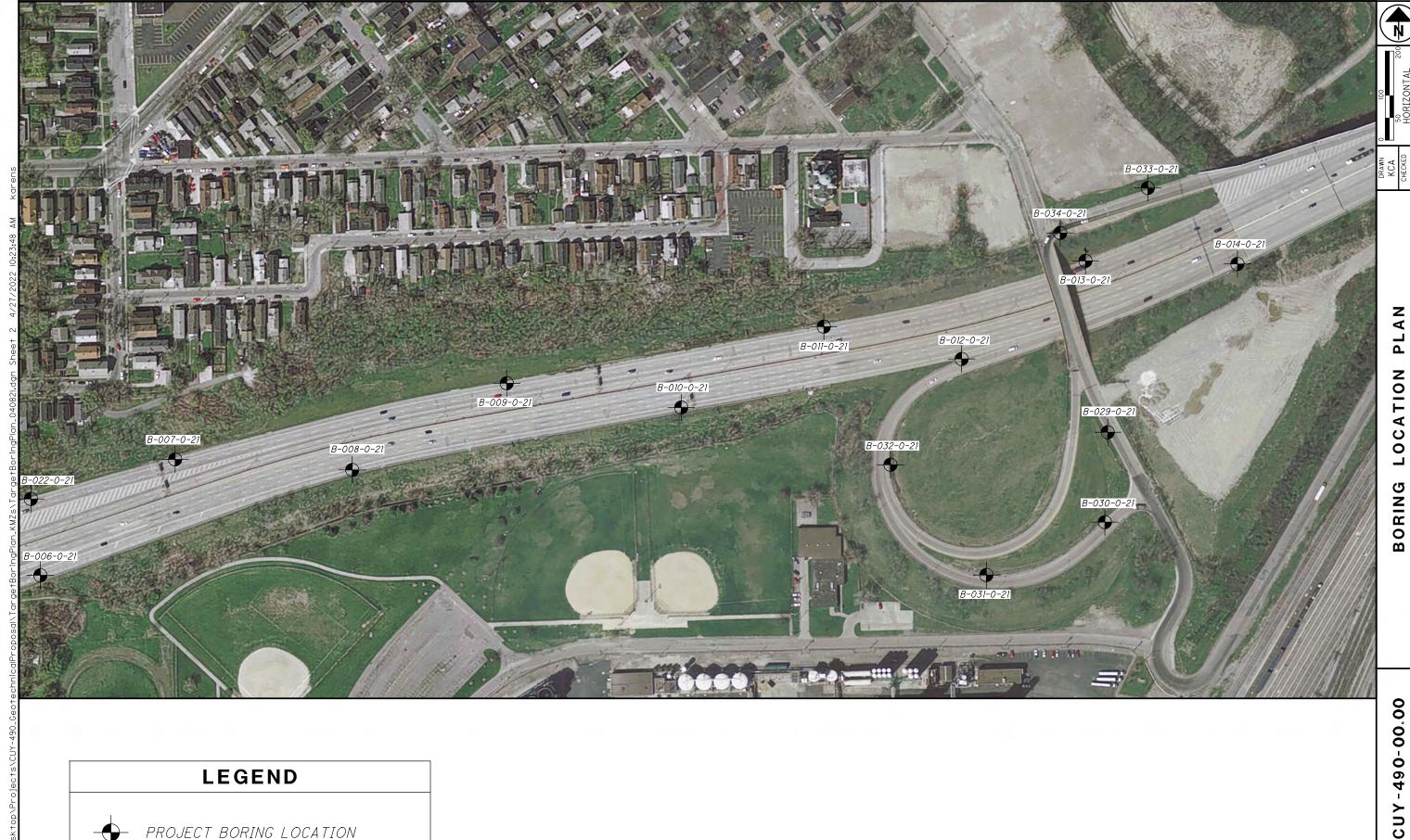
2020 HISTORIC BORING LOCATION

CUY-490-00.00

PLAN

LOCATION

BORING



PROJECT BORING LOCATION

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PROJECT BORING LOCATION



APPENDIX B BORING LOGS

TYPE: ROADWAY S	DRILLING FIRM / C SAMPLING FIRM /		ORS <u>&ME / C. BRU</u> R:S <u>&ME / C. BRUN</u>								ALIC	SNME	I / OF ENT:			IR-9	0		PLORA 3-109	-0-2
	DRILLING METHOL SAMPLING METHO		2.25" HSA SPT		l .		ION DATE (%)		90*	0		VATI / LOI	_					7.5 ft. .698962 W		PA(1 O
MATERIAL DESCRIPTION AND NOTES		ELEV. 656.0	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)			ATIO FS		_	ATTE	ERBI PL	ERG PI	WC	ODOT CLASS (GI)	SO4 ppm	
ASPHALT - 5 INCHES CONCRETE - 10 INCHES GRANULAR BASE - 3 INCHES		655.6	- 1 - - 1 -	23		(12)		(12)												× - 1
Medium-dense to dense gray SANDY SILT , tramoist.	ace clay,		W 653.3	19 14 4		100	SS-1	-	0	0	54	38				NP	21	A-4a (2)	443	7
			₩ 651.2 - 4 - 5 - 5 -	13 10 3 8 11	35 29	78 100	SS-2 SS-3	-	-	-	-	35	-	NP -	NP -	NP -	21	A-4a (V) A-4a (V)	-	
		648.5	- 6 - - 7 -	10 11 11	33	78	SS-4	-	-	-	-	-	-	-	-	-	20	A-4a (V)	-	- 17 × 1
NOTES: - Seepage noted at 2.7' during drilling. - Groundwater noted at 4.8' during drilling. - After removal of augers, boring caved at 4.2' observed to be dry.	' and was																			

NOTES: SEE ABOVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: ASPHALT PATCH; SOIL CUTTINGS

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	DRILLING FIRM / (SAMPLING FIRM /						S&ME CME A				STA		I / OFF ENT:	FSE ⁻	T:	931+9			LORA -110-
ID: 76779 BR ID: N/A	DRILLING METHO	D:	2.25" HSA SPT		CALI	BRAT	ON DATE	:6	/25/2 90*		ELE'		ON: _(NG:					7.5 ft. .697498 W	
MATERIAL DESCRIPTION AND NOTES		ELEV. 648.1	DEPTHS	SPT/ RQD	N	DEC	SAMPLE		_	RAD cs	ATIO) /	ATT	ERBE	ERG	wc	ODOT CLASS (GI)	SO4 ppm
ASPHALT - 2-1/4 INCHES CONCRETE - 10 INCHES		\647.9 647.1 646.6	_ 1	_		(70)	טו	(101)	O.C.	00		Oi	<u> </u>						
GRANULAR BASE - 5-3/4 INCHE Medium-dense to very-dense brown COARSI FINE SAND, little fine gravel, little silt, trace of	E AND		- 2 - 3	5 8 10	27	100	SS-1	-	17	22	45	13	3	NP	NP	NP	7	A-3a (0)	174
lamp.	lay,	643.6	4	11 42 12	80	100	SS-2	-	-	-	-	-	-	-	-	-	9	A-3a (V)	-
Dense to very-dense gray SANDY SILT , trace race fine gravel, moist.	e clay,		- 5 - - 6	17 19 20	54	100	SS-3	-	2	6	42	44	6 I	NP	NP	NP	17	A-4a (3)	-
		640.6	EOB - 7	13 14	41	100	SS-4	-	-	-	-	-	-	-	-	-	19	A-4a (V)	-
NOTES: No seepage or groundwater noted during dr After removal of augers, boring caved at 4.9 bserved to be dry.																			

NOTES: SEE ABOVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: ASPHALT PATCH; PLASTIC HOLE PLUG DEVICE; SOIL CUTTINGS

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411.6	

YPE: ROADWAY	SAMPLING FIRM		DRS <u>&ME / C. BF</u> R:S <u>&ME / C. BR</u>		· I						STA		I / OF	FSE	T: _	935+ IR-9			PLORA 3-111	-0-2
ID: <u>76779</u> BR ID: <u>N/A</u> TART: <u>8/13/20</u> END: <u>8/13/20</u>	DRILLING METHO SAMPLING METH		2.25" HSA SPT				ION DATE RATIO (%)		5/25/2 90*	20	ELE'		ON: _ NG: _					7.5 ft. .696012 W		PA 1 O
MATERIAL DESCRIPTION AND NOTES	V	ELEV. 639.8	DEPTHS	SPT/ RQD		REC (%)	SAMPLE ID	HP (tsf)			ATIO FS	N (% sı	_	ATTE	ERBI PL	ERG PI	WC	ODOT CLASS (GI)	SO4 ppm	
ASPHALT - 3-3/4 INCHES CONCRETE - 10 INCHES GRANULAR BASE - 4-1/4 INCH		639.5	- - 1	-				, ,												× 7
Very-dense brown COARSE AND FINE SAN silt, little fine gravel, trace clay, damp.	ND, little	T	- 2 - 3	19 50	-	100	SS-1	-	11	24	48	12	5	NP	NP	NP	11	A-3a (0)	248	7 4 7 7
/ery-dense GRAVEL , some fine to coarse silt, trace clay, damp.	sand, trace	000.0	- 4	33 50-4	-	88	SS-2	-	70	17	9	3	1	NP	NP	NP	6	A-1-a (0)	-	= \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
Hard gray SILT , some clay, trace fine to comoist.	arse sand,	+ + + +	- 5 - - 6	6	18	100	SS-3	4.0	0	1	5	60	34	25	17	8	20	A-4b (8)	-	
	+ + + + + + + + + + + + + + + + + + + +	632.3	- 7 EOB	7 8	23	78	SS-4	4.0	-	-	-	-	-	-	-	-	20	A-4b (V)	-	,
NOTES: No seepage or groundwater noted during After removal of augers, boring caved at 2 observed to be dry.																				

NOTES: SEE ABOVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: ASPHALT PATCH; SOIL CUTTINGS

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S&ME JOB: 1179-20-021																			\equiv	&
PROJECT: CUY-90-6.83 TYPE: ROADWAY PID: 76779 BR ID: N/A START: 8/17/20 END: 8/17/20	DRILLING FIRM / OF SAMPLING FIRM / L DRILLING METHOD SAMPLING METHOI	OGGER:			HAM CALI	MER: BRAT		UTON			STATALICATION	SNME VATI	ENT: ON:	635.	.8 (M	IR-9 SL)	EOB:		B-112	ATION II 2-0-20 PAGE 1 OF 1
MATERIAL DESCRIPTION AND NOTES	· ·	ELEV. 635.8	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	G GR	RAD cs	ATIO FS	N (% sı	CL	ATT LL	ERBE PL	ERG PI	wc	ODOT CLASS (GI)	SO4	
ASPHALT - 3-3/4 INCHES CONCRETE - 8-1/2 INCHES GRANULAR BASE - 5-3/4 INCH PROBABLE FILL: Very-dense black, brown GRAVEL, "and" fine to coarse sand, trace s clay, wet.	ES o and gray	635.5 634.8 634.3	- 2 - - 3 T	50-5"	-	40	SS-1 SS-2	-		23	15	5			NP NP			A-1-a (0) A-1-a (V)		× 1 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 ×
		629.3	- 5 -	50-5"	-	100	SS-3 SS-4	-	-	-	-	-	-	-	-	-	21	A-1-a (V)		77 V 7 V V

NOTES:
- Water noted at 1.1' during drilling.
- After removal of augers, boring caved at 3.0', and water was measured at 0.9'.

NOTES: SEE ABOVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: ASPHALT PATCH; SOIL CUTTINGS

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Ν̈́	PROJECT:	CUY-490-0.00	DRILLING FIRM / O	PERATOR:	NEAS / J. H	ODGES	DRIL	L RIG	C	ME 45	В		STA	TION /	OFFS	ET: _	939+	·11, 39	LT. EX		TION ID
000	TYPE:	SUBGRADE	SAMPLING FIRM / I	_OGGER:	NEAS / J. HO	DGES	HAM	MER:	CME A	UTON	1ATIC	;	ALIG	NMEN	IT:		IR-4	90	L	B-001-	0-21
0-0-	PID: 107408	SFN:	DRILLING METHOD): 	3.25" HSA		CALI	BRATI	ON DATE:	12	2/5/19)	ELE	/ATIO	N: 6	32.9 (MSL)	EOB:	7.5 ft.		PAGE
/-49(START: 7/14	1/21 END: 7/14/21	SAMPLING METHO	D:	SPT		ENE	RGY R	ATIO (%):		31.7		LAT	/ LON	3:	4	1.4742	243, - 81	.694868		1 OF 1
S		MATERIAL DESCRIPTION	v	ELEV.	DEPTHS	SPT/	N.	REC	SAMPLE	HP	C	SRAD	ATIO	N (%)	Α	TTER	BERG		ODOT	SO4	BACK
INE		AND NOTES		632.9	DEPTHS	RQD	N ₆₀	(%)	ID	(tsf)	GR	CS	FS	SI	CL L	L P	_ PI	wc	CLASS (GI)	ppm	FILL
1 ARCH	4.0" ASPHALT (DRILLERS DE	F AND 8.0" CONCRETE AND ESCRIPTION)		631.4	- - 1	_															
EAR\202	FINE SAND, L	SE TO DENSE, BROWN, COA ITTLE TO SOME GRAVEL AN LITTLE SILT. TRACE CLAY.	D STONE		_ 2	10 14 13	37	39	SS-1	-	21	23	38	15	3 N	P N	P NP	11	A-3a (0)	1433	7'1
VE BY Y	DAMP	EITTEE GIET, TIVIOE GEAT,	**************************************	628.4	_ 4	9 12 10	30	33	SS-2	-	-	-	-	-		-	-	9	A-3a (V)	-	1
1ARCHI		SE, BROWN, GRAVEL WITH FRACE CLAY, MOIST	SAND,	626.9	<u> </u>	10 12	30	61	SS-3	-	32	23	30	12	3 N	PN	P NP	12	A-1-b (0)	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
)JECTS		SE, GRAY, COARSE AND FIN TRACE CLAY, TRACE GRAVE		625.4	- 6 - 7	7 9 11	27	56	SS-4	-	-	-	-	-	-	. -	-	12	A-3a (V)	-	1 7 V V
\approx	The state of the s	·			EOP																

			_																			
PROJE		Y-490-0.00	DRILLING FIRM / OPER	_	NEAS /		- 1	L RIG		CME 5			STAT			FSET			10' F	RT.	EXPLOR	
TYPE:	RETAIN	IING WALL	SAMPLING FIRM / LOG	GER:	NEAS /	JL	HAM	IMER:	CN	IE AUTO	MATIC	:	ALIG	NME	NT:		٧	/ALL	1		B-00 ²	
PID:	SFN:		DRILLING METHOD:	3	.25" HSA		CALI	BRAT	ION D	ATE: 1	1/24/22	2	ELE\	/ATIC	ON:	631.6	(MS	L) E	OB:	16	6.5 ft.	PAGE
START	: 10/19/22 E	ND: 10/19/22	SAMPLING METHOD:		SPT		ENE	RGY F	RATIO	(%):	63.4		LAT /	LON	اG: -		41.4	74016	3, - 81	.6941	91	1 OF 1
5		ATERIAL DESCRIP	TION	ELEV.			SPT/		RFC	SAMPLE	HP		GRAD	ATIC	N (%	5)	ATT	ERBE	RG		ODOT	BACK
5		AND NOTES		631.6	DEPTI	HS	RQD	N ₆₀	(%)	ID	(tsf)		_		SI		LL		PI	wc	CLASS (GI)	
(DRILI	LERS DESCRIPT E, BROWN, CO	0" CONCRETE AND	ND, LITTLE	630.0		 - 1 - - 2 -			(**)		()					-						~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
(FILL)		, TRACE CLAY, MI				- 3 - 4	14 15 14	31	67	SS-1	-	15	25	41	13	6	NP	NP	NP	12	A-3a (0)	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
	STIFF, GRAY, \$ E GRAVEL, MOI	SILT, SOME CLAY, IST TO WET	TRACE SAND,	626.6		5 T	4 6 7	14	67	SS-2	2.25	-	-	-	-	-	-	-	-	21	A-4b (V)	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
Z Z Z Z			+ + + + + + + + + + + + + + + + + + +	+ + + + +		- 7 - - 8 -	4 3 6	10	61	SS-3	3.50	0	0	1	72	27	25	18	7	19	A-4b (8)	7
			+++ +++ +++ +++ +++ +++	+ + + + + + +		- 9 - - 10 - - 11 -	2 3 7	11	67	SS-4	3.00	-	-	-	-	-	-	-	-	26	A-4b (V)	7
			+++ +++ +++ +++ +++ +++			- 12 - - 13 -	0 0	2	67	SS-5	3.00	-	-	-	-	-	-	_	_	27	A-4b (V)	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
		TIFF, GRAY, SILT A E GRAVEL, WET	AND CLAY,	617.1			3 3	6	67	SS-6	1.00	0	0	1	54	45	30	19	11	28	A-6a (8)	1 > 1 > 1 > 1 > 1 > 1 > 1 > 1 > 1 > 1 >
			<i>\///</i>	615.1	EOB-	— 16 -	3		01	00-0	1.00			ı	J- 1	40	30	13	'']	20	A-0a (0)	1>11>

NOTES: GROUNWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE. DRILLED AS STAKED.

PRC TYP	DJECT PE:	Γ:	RE	CUY-			DRILLING FIRM SAMPLING FIR			NEAS /		-	L RIG: MER:		CME 55			STAT ALIG			SET:		2+66 VALL	i, 9' R 1	T.		ATION ID 1-2-21
PID:				FN: _			DRILLING MET			.25" HSA		- 1				/24/22		ELEV		_	632.0					6.5 ft.	PAGE
STA	NRT: _	10/1	19/22	_ EN			SAMPLING ME	THOD:		SPT / ST		_ ENE	RGY R			63.4	-	LAT /	-			_			.69370	08	1 OF 1
				MA		AL DESCRIPT ND NOTES	TION		ELEV. 632.0	DEP.	THS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID		GR	GRAD cs	ATIC FS) CL	ATT LL	ERBI PL	ERG PI	wc	ODOT CLASS (GI)	BACK FILL
(DF	RILLE	RS D	WN, O	RIPTIO	N)	VITH SAND, L			630.4		- 1 - - 2 -	-		,													7 L ^N 7 L 1 > N 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
(FIL	LL)							0.0	628.5		_ 3 -	14	31	56	SS-1	-	18	34	26	15	7	NP	NP	NP	8	A-1-b (0)	1>11>
	RD, G RAVEL			r, son	ЛЕ C	LAY, TRACE S	SAND, TRACE	++++			5 7	6															\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
								++++			- 6 - 7 -	5 10	16	61	SS-2	4.25	-	-	-	-	-	-	-	-	17	A-4b (V)	12V 12 12V 12 12V 12
								++++	622.5		_ 8 <u>_</u> _ 9 _	4 6	11	67	SS-3	4.50	0	0	4	71	25	23	18	5	17	A-4b (8)	1> \ 1 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
				GRAY, MOIST			Y, TRACE SAND,	++++ ++++ ++++ ++++ ++++ ++++			- 10 - - 11 - - 12			84	ST-1	-	0	0	7	75	18	NP	NP	NP	18	A-4b (8)	V V V V V V V V V V V V V V V V V V V
								+ + + + + + + + + + + + + + + + + + + +			13	6 9 12	22	72	SS-4	-	-	-	-	-	-	-	-	-	17	A-4b (V)	1> \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
								++++	615.5	EOB-	15 - - 16 -	4 10 13	24	67	SS-5	-	-	-	-	-	-	-	-	-	20	A-4b (V)	1>\ 1> \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \

NOTES: GROUNWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE. DRILLED AS STAKED.

PROJECTORY PROJECTORY PID: PID:	SUBGRADE 107408 SFN:	DRILLING FIRE SAMPLING FIRE DRILLING MET (15/21 SAMPLING MET	RM / LOGGE THOD:		ISA		HAM CALI	BRATI	CME AON DATE: ATIO (%):	12			ALIG	TION . SNME VATIC	NT: _)N: _		1 (MS	IR-49 SL)	EOB:		B-002-	TION ID 0-21 PAGE 1 OF 1
IVE/CUY	MATERIAL DES	SCRIPTION	ELEV 632.1			SPT/ RQD	N ₆₀		SAMPLE ID			GRAD CS	ATIO FS	_		ATT	ERBE PL		wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
MEDIU SAND,	SPHALT AND 8.0" CONCR LERS DESCRIPTION) IM DENSE TO DENSE, BRO LITTLE SILT, TRACE CLA' LT SEAM, DAMP	OWN, GRAVEL WITH	630.6	₩ 628.5	_ 2 _	8 8 9 7 6	23	67	SS-1 SS-2	-	21	36	25	13	5	NP -	NP -	NP -	9	A-1-b (0) A-1-b (V)	227	× × × × × × × × × × × × × × × × × × ×
	BROWNISH GRAY, SILT , TRACE GRAVEL, DAMP	SOME CLAY, TRACE	624.6		- 5 -	8 11 12 10 10 10	31	39 61	SS-3A SS-3B SS-4	- - <u>4.50</u> 4.50	- 3 -	- _1_ -	- 3 -	- 65 -	- 28 -	- 27 -	- _18 -	- 9 -	9 13 14	A-1-b (V) A-4b (8) A-4b (V)	- - -	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\

EXPLORATION ID PROJECT: CUY-490-0.00 DRILLING FIRM / OPERATOR: NEAS / JL DRILL RIG: CME 55T STATION / OFFSET: 1+44, 9' RT. B-002-1-21 **RETAINING WALL** SAMPLING FIRM / LOGGER: __ TYPE: NEAS / JL HAMMER: CME AUTOMATIC ALIGNMENT: WALL 1 PAGE PID: SFN: DRILLING METHOD: 3.25" HSA CALIBRATION DATE: 1/24/22 ELEVATION: 631.2 (MSL) EOB: 1 OF 1 START: 10/19/22 END: SAMPLING METHOD: SPT **ENERGY RATIO (%):** 10/19/22 63.4 LAT / LONG: 41.474044, -81.693267 **MATERIAL DESCRIPTION** ELEV. REC SAMPLE ΗP **GRADATION (%)** ATTERBERG SPT/ **BACK** ODOT **DEPTHS** N_{60} CLASS (GI) RQD (%) GR CS FS LL PL Ы FILL **AND NOTES** ID (tsf) SI CL WC 631.2 5.0" ASPHALT AND 7.0" CONCRETE AND 7.0" BASE (DRILLERS DESCRIPTION) 629.6 DENSE, BROWNISH GRAY, SANDY SILT, LITTLE CLAY. 2 LITTLE GRAVEL, DAMP 3 (FILL) 41 SS-1 NP NP NP 72 11 16 26 31 16 11 A-4a (2) 18 626.7 VERY STIFF, GRAY, SILT, SOME CLAY, TRACE SAND, 5 TRACE GRAVEL, CONTAINS NO INTACT SOIL FOR HP 1>1 50 SS-2 16 A-4b (V) 16 READINGS, DAMP 6 8 7 17 67 SS-3 0 0 3 71 26 24 17 A-4b (8) 7 16 9 10 1>1 16 50 SS-4 A-4b (V) 17 12 - 13 9 18 50 SS-5 16 A-4b (V) 15 9 17 44 SS-6 16 A-4b (V) 16 614 7 EOB-

NOTES: GROUNWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE. DRILLED AS STAKED.

STANDARD ODOT SOIL BORING LOG (8.5 X 11) - OH DOT GDT - 1/3/23 19:25 - X:ACTIVE PROJECTS/ACTIVE SOIL PROJECTS/CUV

EXPLORATION ID PROJECT: CUY-490-0.00 DRILLING FIRM / OPERATOR: NEAS / JL DRILL RIG: CME 55T STATION / OFFSET: 7' RT. B-002-2-21 SAMPLING FIRM / LOGGER: ___ **RETAINING WALL** HAMMER: CME AUTOMATIC WALL 1 TYPE: NEAS / JL ALIGNMENT: PAGE PID: SFN: DRILLING METHOD: 3.25" HSA CALIBRATION DATE: 1/24/22 ELEVATION: 633.2 (MSL) EOB: 1 OF 1 START: 10/19/22 END: 10/19/22 SAMPLING METHOD: SPT **ENERGY RATIO (%):** 41.474090, -81.692675 63.4 LAT / LONG: **MATERIAL DESCRIPTION** ELEV. REC SAMPLE ΗP **GRADATION (%)** ATTERBERG SPT/ **BACK** ODOT N₆₀ **DEPTHS** CLASS (GI) RQD (%) GR CS FS SI LL PL Ы FILL **AND NOTES** ID (tsf) CL WC 633.2 5.0" ASPHALT AND 7.0" CONCRETE AND 7.0" BASE (DRILLERS DESCRIPTION) 631.6 STIFF TO HARD, GRAY, SILT, SOME CLAY, TRACE 2 SAND, TRACE GRAVEL, CONTAINS NO INTACT SOIL FOR 3 HP READINGS, DAMP TO MOIST 35 SS-1 A-4b (V) 16 50 12 17 5 1>1 50 SS-2 2 29 24 6 15 0 68 18 6 17 A-4b (8) 6 8 12 56 SS-3 A-4b (V) 4 18 9 10 9 20 44 SS-4 A-4b (V) 18 - 12 - 13 8 15 50 SS-5 0 0 3 71 26 24 18 6 18 A-4b (8) 15 4 11 56 SS-6 22 A-4b (V) 16 616.7 EOB-

NOTES: GROUNWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE. DRILLED AS STAKED.

90-0-06	PROJECT: CUY-490-0.00 TYPE: SUBGRADE PID: 107408 SFN: START: 7/14/21 END: 7/14/2 ⁻	DRILLING FIRM / (SAMPLING FIRM / (DRILLING METHO SAMPLING METHO	LOGGER: D:	NEAS / J. HO NEAS / J. HO 3.25" HSA SPT		HAM CALI			12			ALIG	TION / C NMENT /ATION / LONG	631	.5 (M	IR-49 SL)	EOB:		B-003-	TION ID 0-21 PAGE 1 OF 1
IVE\CUY-	MATERIAL DESCRII AND NOTES		ELEV. 631.5	DEPTHS	SPT/ RQD	N ₆₀	_	SAMPLE ID	_	Ģ	RAD cs	ATIOI FS		AT	TERB		wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
21 ARCH	4.0" ASPHALT AND 8.0" CONCRETE (DRILLERS DESCRIPTION)	\bowtie	630.0	- - 1	-				·											- 1 LV 1
YEAR\20	MEDIUM DENSE, BROWN, COARSE A SOME SILT, LITTLE GRAVEL, TRACE NIRON STAINING, DAMP		629.3	- 2 - 3	13	42	72	SS-1A SS-1B	-	19	30 4	7	21 6 71 1	_	_	NP 4	7 13	A-3a (0) A-4b (8)	647	1
HIVE BY	DENSE, GRAYISH BROWN, SILT , LIT LITTLE SAND, TRACE GRAVEL, CONT IRON STAINING, DAMP	AINS TRÁCE		- - 4 	12 13	34	50	SS-2	-	13	16	16	44 1	24	20	4	10	A-4a (4)	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
CTS/1ARC	DENSE, BROWN AND GRAY, SANDY GRAVEL, LITTLE CLAY, CONTAINS IR		+ + + + + + + + + + + + + + + + + + + +	- 5 - 6	13 11 8	33	56	SS-3	-	-	-	-	- -	-	-	-	14	A-4b (V)	-	17 × 17 × 17 × 17 × 17 × 17 × 17 × 17 ×
핑		GRAVEL,		EOB 7	<u> </u>	19	67	SS-4	-	-	-	-	- -	<u> -</u>	-	-	18	A-4b (V)	-	\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\

TYPE: SUBGRADE PID: 107408 SFN:	DRILLING FIRM / OPER SAMPLING FIRM / LOC DRILLING METHOD: SAMPLING METHOD:	GGER: _	NEAS / ASHBA NEAS / ASHBA 3.25" HSA SPT		HAMI CALII	BRATI	CME A ON DATE: ATIO (%):	12			ALIC	TION / BNME! VATIO / LON	NT: _ N: _6	35.9	I (MS	IR-49 L)	EOB:	7.5 ft.	PLORA B-004-	ATION ID -0-21 PAGE 1 OF 1
MATERIAL DESCRIPTION AND NOTES		LEV. 35.9	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAD CS	ATIO FS	N (%)	CL /		RBE PL	RG PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
5.0" ASPHALT AND 9.0" CONCRETE AND 6. (DRILLERS DESCRIPTION) MEDIUM DENSE, BROWN, GRAVEL AND ST FRAGMENTS WITH SAND AND SILT, TRACE CONTAINS CONCRETE FRAGMENTS, DAMI HARD, BROWNISH GRAY, SILT, SOME CLASSAND, TRACE GRAVEL, DAMP	TONE CLAY, P CONTRACE	34.2	- 1 - 2 - 3 - 4 - 5 - 6 - 7 - FOB	8 9 11 10 12 9 5 9 10 6 8 11	27 29 26 26	67 56 89 56	-	-	29 - 0 -	25	19 - 4	22 - - 65	-	-	NP 19	NP - 6	8 8 14 15	A-2-4 (0) A-2-4 (V) A-4b (V) A-4b (8) A-4b (V)	693	7

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SINT	PROJECT: <u>CUY-490-0.00</u>	DRILLING FIRM / C	PERATOR:	NEAS / J. HOD	GES_	DRIL	L RIG	C	ME 45	В		STA	TION	/ OF	FSET	Г:	953+9	92, 41'	LT. EX		TION ID
00	TYPE: SUBGRADE	SAMPLING FIRM /	LOGGER:	NEAS / J. HOD	GES	HAM	MER:	CME A	NOTU	1ATIC)	ALIC	SNME	NT:			IR-49	90		B-005-	0-21
-0.0	PID: 107408 SFN:	DRILLING METHO	D:	3.25" HSA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE	VATIO	ON:	635.	3 (MS	SL)	EOB:	7.5 ft.		PAGE
/49(START: 7/19/21 END: 7/19/21	SAMPLING METHO	DD:	SPT		ENEF	RGY R	ATIO (%):		81.7		LAT	/ LOI	NG:		41.4	47488	36, - 81	.689604		1 OF 1
CO	MATERIAL DESCRIPTION	ı	ELEV.	DEPTHS	SPT/	NI.	REC	SAMPLE	HP	(GRAD	OITAC	N (%)	ATT	ERBI	ERG		ODOT	SO4	BACK
IIVE	AND NOTES		635.3	DEPTHS	RQD	N ₆₀	(%)	ID	(tsf)	GR	cs	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
1 ARCH	4" ASPHALT AND 8" CONCRETE AND 6" B (DRILLERS DESCRIPTION)	ASE	633.8	 - 1 -																	
/EAR\202	DENSE, BROWN, GRAVEL WITH SAND , LIT TRACE CLAY, CONTAINS CONCRETE FRAG CONTAINS IRON STAINING, DAMP		632.3	2 -	9 10 16	35	28	SS-1	-	28	23	28	16	5	NP	NP	NP	6	A-1-b (0)	487	77777
VE BY	(FILL) DENSE, BROWN, COARSE AND FINE SAND	D, SOME	3	_ 4 -	10 13	31	50	SS-2	-	14	22	36	22	6	NP	NP	NP	7	A-3a (0)	-	1 / 1 / 1 / 1 / 1 / 1 / 1 / 1 / 1 / 1 /
1ARCHI	SILT, LITTLE GRAVEL, TRACE CLAY, CONT STAINING, DAMP	AINS IRON	-i I	- 5 -	8 14 11	34	67	SS-3	-	-	-	-	-	-	-	-		10	A-3a (V)	-	< 1 7 × 7 × 7 × 7 × 7 × 7 × 7 × 7 × 7 × 7
ROJECTS	HARD, GRAYISH BROWN, SILT , LITTLE SA CLAY, TRACE GRAVEL, CONTAINS IRON S MOIST	ND, LITTLE ‡‡‡‡	‡	EOB 7	9 7 6	18	78	SS-4	4.25	-	-	-	-	-	-	-	-	16	A-4b (V)	-	1 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

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רי	PROJECT:	CUY-490-0.00	DRILLING FIRM / O				1	L RIG		ME 45				TION /		ET: _		33, 78'	RT. EX	PLORA B-006-	TION ID
8	TYPE:	SUBGRADE	SAMPLING FIRM / I	_OGGER	: <u>NEAS / J. HC</u>	DGES_	HAM	IMER:	CME A	NOTU	/ATIC	<u> </u>	ALIC	SNMEN	IT:		IR-4	90		D-000-	
9	PID:1074	408 SFN:	DRILLING METHOD):	3.25" HSA		CAL	IBRAT	ON DATE:	12	2/5/19	9	ELE	VATIO	N: <u>63</u>	2.7 (N	1SL)_	EOB:	7.5 ft.		PAGE
₹ 7 49	START:	7/19/21 END: 7/19/21	SAMPLING METHO	D:	SPT		ENE	RGY F	ATIO (%):	8	81.7		LAT	/ LON	3:	41	.4749	04, -81	.688112		1 OF 1
3		MATERIAL DESCRIPTIO	N	ELEV.	DEPTHS	SPT/	N ₆₀	REC	SAMPLE	HP	(GRAD	DATIC	N (%)	A	ITERE	BERG		ODOT	SO4	BACK
≅L		AND NOTES		632.7	DEFINS	RQD	11460	(%)	ID	(tsf)	GR	CS	FS	SI	CL L	. PL	PI	WC	CLASS (GI)	ppm	FILL
1 ARCH	10" CONCI DESCRIPT	RETE AND 7" BASE (DRILLERS 'ION)		631.3	- - 1	_															
EAR\202		DENSE, GRAY, GRAVEL , SOME : LT, TRACE CLAY, CONTAINS GF T	′ 1./\α	629.7	w 629.7	4 6	15	44	SS-1	-	55	20	14	9	2 N	P NP	NP	21	A-1-a (0)	1187	7 4 7
VE BY Y	VERY STIF	FF TO HARD, BROWN, SANDY S			- 3 - 4	4 4 7	15	67	SS-2	3.00	6	7	16	47	24 2	3 16	7	17	A-4a (7)	-	
1ARCHI	CLAY, TRA SEAMS, M	ACE TO LITTLE GRAVEL, CONTA OIST	AINS 1" SILT		<u> </u>	5 7	16	39	SS-3	4.25	-	-	-	-	- -	-	-	21	A-4a (V)	-	\\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
SJECTS				625.2	FOR - 7	5 6 8	19	50	SS-4	4.25	-	-	-	-	- -	-	-	21	A-4a (V)	-	1 / V / 1 / V / V / V / V / V / V / V /

TYF	10740	CUY-49 SUBGRA 08 SFN:		DRILLING FIRM / SAMPLING FIRM DRILLING METH	/ LOGGER		/ ASHBA / ASHBAU HSA		HAM CALI		CME A	12			ALIC	TION SNME VATIO	NT:			IR-49	53, 73' 90 EOB:	<u> </u>	B-007	PAGE
STA	RT: <u>7/</u>		AL DESCRIPTION	SAMPLING METH V	ELEV.	SF DEPT		SPT/	ENEI	REC	ATIO (%):	HP			ATIC)	ATT	ERBE	RG		.686998 ODOT CLASS (GI	SO4	1 OF 1 BACK FILL
ME SC	SCRIPTION DIUM DE	T AND 6" CONO DN) ENSE, BROWN,	ND NOTES CRETE (DRILLEI COARSE AND I LT, TRACE CLAY DAMP	FINE SAND,			- 1 - - 2 -	12 10 11	29	61	SS-1	(tsf)	GR 27	7	48	16	2	NP	PL NP	NP	7	A-3a (0)		7 LV 7
ME		, - ,	COARSE AND I	, 10.0	· • 1		- 4 - - 5 -	8 7 6 5	19 15	56 50	SS-2 SS-3	-	9	13	- 58	- 17	3	- NP	- NP	- NP	9	A-3a (V) A-3a (0)		7
					620.5	ЕОВ-	- 6 - - 7 -	5 5 7	16	56	SS-4	-	-	-	-	-	-	-	-	-	9	A-3a (V)	-	

PROJECT:	DRILLING FIRM / OPER, SAMPLING FIRM / LOGO DRILLING METHOD: SAMPLING METHOD:		NEAS / J. HODGE NEAS / J. HODGE 3.25" HSA SPT	S HA			12		A	STATIO ALIGNM ELEVAT	ENT: ION:		0 (MS	IR-49 SL)_	EOB:	RT. EX 7.5 ft.	B-008-	TION ID 0-21 PAGE 1 OF 1
MATERIAL DESCRIPTION AND NOTES	I ELE	.EV.	DEDTHS S	SPT/ RQD N	DEC	SAMPLE ID		G	RADA	TION (ATT	ERBE		wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
10.0" CONCRETE AND 7.0" BASE (DRILLEI DESCRIPTION) MEDIUM DENSE, BROWN MOTTLED WITH ORANGISH BROWN AND GRAY, SANDY SI GRAVEL, TRACE CLAY, CONTAINS IRON SAND GLASS FRAGMENTS, DAMP (FILL) HARD, BROWN MOTTLED WITH ORANGISH AND GRAY, SANDY SILT, LITTLE CLAY, TRACE CLAY, T	LT, SOME 615 TAINING 614 H BROWN ACE	15.6 14.0 19.5	3 4 - 4 - 7	10 9 2 1 1 1 1 3 1 1 1 3 1 1 1 1 5	6 67 0 78	SS-1 SS-2 SS-3 SS-4	- 4.50 4.50 4.50	22 - 6	-	21 28 20 46 	-	NP - 24 -	NP - 17 -	NP - 7 -	9 11 12 14	A-4a (1) A-4a (V) A-4a (6) A-4a (V)	1280	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

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ΞĮ	PROJECT:	CUY-490-0.00	DRILLING FIRM / O	PERATOR:	NEAS / ASHB	AUGH_	DRIL	L RIG	C	ME 45	В		STA	TION /	OFFS	ET: _	969+	07, 61	LT. EX		TION ID
00	TYPE:	SUBGRADE	SAMPLING FIRM / L	OGGER: _	NEAS / ASHBA	AUGH_	HAM	IMER:	CME A	NOTU	/ATIC		ALIC	SNMEN	IT:		IR-4	90	L	B-009-	
0-0	PID: 107408	SFN:	DRILLING METHOD):	3.25" HSA		CAL	IBRATI	ON DATE:	12	2/5/19	9	ELE	VATIO	N: 6	3.6 (I	MSL)	EOB:	7.5 ft.		PAGE
۲-49	START:7/14/	21 END: 7/14/21	SAMPLING METHO	D:	SPT		ENE	RGY R	ATIO (%):	;	81.7		LAT	/ LON	3:	4	1.4760	61, - 81	.684277		1 OF 1
\C		MATERIAL DESCRIPTION	V	ELEV.	DEPTHS	SPT/	N ₆₀	REC	SAMPLE	HP	(GRAD	OITAC	N (%)	А	TTER	BERG		ODOT	SO4	BACK
IIVE		AND NOTES		613.6	DEFINS	RQD	1460	(%)	ID	(tsf)	GR	CS	FS	SI	CL L	_ PI	- PI	WC	CLASS (GI)	ppm	FILL
1 ARCH	DESCRIPTION)			612.5	- 1 -	-															***
EAR\202		IISH GRAY AND BROWN, S FRACE TO LITTLE GRAVEL,			_ 2 -	13 12 9	29	67	SS-1	4.50	10	18	28	32	12 2	1 10	5 5	10	A-4a (2)	313	7 4 7
VE BY Y					3 - 4 -	7 9 8	23	89	SS-2	4.50	15	15	17	36	17 2	7 18	3 9	15	A-4a (4)	-	1 > 1 > 1 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1
1ARCHI					<u> </u>	8 7 10	23	83	SS-3	4.50	-	-	-	-	- .	-	-	14	A-4a (V)	-	\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\
)JECTS				606.1	- 6 - - 7 -	6 8 10	25	78	SS-4	4.50	-	-	-	-	-	-	-	13	A-4a (V)	-	1 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

ŗ[PROJECT	T: CUY-49	90-0 00	DRILLING FIRM /	OPERATOR	· NFAS	/ J. HOD	GES	DRII	L RIG:	C	ME 45	iB.		STA	TION	/ OFF	SFT	· <u>c</u>	72+8	35. 62'	RT EX	PLORA	ATION ID
ריו	TYPE: _	SUBGRA		SAMPLING FIRM						MER:						SNME		0_,		IR-49			B-010-	-0-21
		07408 SFN:		DRILLING METHO	D:	3.25" H	ISA		1		ON DATE:		2/5/19	9	ELE,	VATIC)N: _	616.	8 (MS	SL)_	EOB:	7.5 ft.		PAGE
₹	START: _	7/19/21 END:	7/19/21	SAMPLING METH	OD:	SP [*]	Т		ENE	RGY R	ATIO (%):		81.7		LAT	/ LON	IG: _		41.4	17590)1, -81	.682845	<u></u>	1 OF 1
5			AL DESCRIPTION	N	ELEV.	DEPTI	HS	SPT/	N ₆₀	_	SAMPLE			ī -	OITAC	-	_	ATT	ERBE			ODOT	SO4	BACK FILL
⋛			ND NOTES		616.8		1	RQD	60	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	XXXXXXX
I ARC	8.0" COI DESCRI	NCRETE AND 8.0" PTION)	BASE (DRILLEF	RS	615.5		- - 1 -	-																
EAR\202	GRAVEL	M DENSE TO DENS L AND STONE FRA RACE CLAY, CONT.	GMENTS WITH	SAND AND ∤			2	10 11 9	27	67	SS-1	-	29	19	19	23	10	NP	NP	NP	12	A-2-4 (0)	553	7'1
IVE BY Y	DAMP (FILL)				 		4	10 12 15	37	72	SS-2	-	-	-	-	-	-	-	-	-	11	A-2-4 (V)	-	1 > \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1
\1ARCH							5 - - 6 -	11 11 14	34	67	SS-3	-	23	20	22	26	9	NP	NP	NP	12	A-2-4 (0)	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
OJECTS	@6.0' BE	ECOMES GRAY			609.3	— ЕОВ —	- 7 -	12 10 11	29	67	SS-4	-	-	-	-	-	-	-	-	-	11	A-2-4 (V)	-	1 / V / V

EXPLORATION ID PROJECT: CUY-490-0.00 DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH DRILL RIG: CME 45B STATION / OFFSET: 976+32, 61' LT. B-011-0-21 TYPE: **SUBGRADE** SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH HAMMER: CME AUTOMATIC ALIGNMENT: IR-490 **PAGE** PID: 107408 SFN: DRILLING METHOD: 3.25" HSA CALIBRATION DATE: 12/5/19 ELEVATION: 622.9 (MSL) EOB: 7.5 ft. 1 OF 1 **ENERGY RATIO (%):** START: 7/14/21 END: 7/14/21 SAMPLING METHOD: SPT 81.7 LAT / LONG: 41.476390, -81.681670 ELEV. REC SAMPLE HP **GRADATION (%) ATTERBERG MATERIAL DESCRIPTION** SPT/ ODOT SO4 BACK **DEPTHS** CLASS (GI) FILL RQD ppm (%) GR CS FS SI CL LL PL PΙ WC **AND NOTES** ID (tsf) 622.9 7.5" ASPHALT AND 6.5" CONCRETE (DRILLERS 621.7 DESCRIPTION) MEDIUM DENSE TO DENSE, GRAY, GRAVEL WITH 1>1 2 SAND, TRACE SILT, TRACE CLAY, WET 41 2 NP NP 18 78 SS-1 35 33 20 10 NP 18 A-1-b (0) 2120 **w** 620.1 12 3 SS-2A 15 A-1-b (V) 18 67 618.7 1 > 1 SS-2B 4.50 58 21 27 19_ A-4b (8) 618.4 6 8 21 \ 6 HARD, DARK GRAY, SILT, SOME CLAY, LITTLE SAND. TRACE GRAVEL, SLIGHTLY ORGANIC, DAMP 16 SS-3 56 21 A-1-b (V) 1>1 MEDIUM DENSE. GRAY. GRAVEL WITH SAND. LITTLE SILT, TRACE CLAY, WET 1>1 22 SS-4 44 21 A-1-b (V) <, ∨ 615.4

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\GINT	PROJECT	T: <u>CUY-490-0.00</u> SUBGRADE		DRILLING FIR				J. HOD			L RIG:		ME 45				TION		SET		979+2 IR-49	20, 72'	RT. EX	PLORA B-012-	ATION ID -0-21
				SAMPLING FI				J. HODO	JEO		MER:					1	SNME	-						$\overline{}$	DAGE
0-0	PID:10	07408 SFN:		DRILLING ME	THOD	D:	3.25"	HSA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE'	VATIC)N: _	631.	9 (MS	<u>SL)</u>	EOB:	7.5 ft.		PAGE
Y-49	START: _	7/19/21 END:7/	ETHO	D:	SF	PΤ		ENE	RGY R	ATIO (%):		81.7		LAT	/ LON	IG: _		41.4	17618	32, -81	.680543		1 OF 1		
∃\CU		MATERIAL DES			ELEV.	DEPT	HS	SPT/	N ₆₀	_	SAMPLE				OITA		_		ERBE			ODOT	SO4	BACK	
Ĭ.		AND NO	TES			631.9			RQD	. •60	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
321 ARCH	DESCRI	- ,		A/A L OU T		630.4		- 1 -	0																- 1 LV 1
/EAR\2(LITTLE (/I DENSE TO DENSE, GR/ CLAY, TRACE TO LITTLE _, CONTAINS IRON STAIN	SAND, TRAC	CE	+ + + + + + + + + + + +			_ 2 _	13 14	37	78	SS-1	-	0	0	6	78	16	NP	NP	NP	14	A-4b (8)	733	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
IVE BY `		- ,			+ + + + + + + + + + + + + + + +			_ 4 -	8 11 10	29	61	SS-2	-	1	3	10	74	12	NP	NP	NP	15	A-4b (8)	-	1 4 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
11ARCH					++++			- 5 - - 6 -	8 10 11	29	72	SS-3	-	-	-	-	-	-	-	-	-	15	A-4b (V)	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
OJECTS					++++	624.4	— ЕОВ —	- 7 -	6 12 11	31	67	SS-4	-	-	-	-	-	-	-	-	-	14	A-4b (V)	-	1 / / / / / / / / / / / / / / / / / / /

	PROJECT: TYPE: PID:107408	CUY-490-0.00 SUBGRADE SFN:	DRILLING FIRM / C SAMPLING FIRM / DRILLING METHO	LOGGER:	: NEAS / ASHBA NEAS / ASHBA 3.25" HSA		HAM CALI		CME A	12			ALIC	SNME	NT:			IR-49	19, 63' 90 EOB:	LT. E)	B-013	PAGE
IVE\CUY-49	START:	21 END: 7/14/21 MATERIAL DESCRIPTION AND NOTES	SAMPLING METHON N	DD: ELEV. 635.5	SPT DEPTHS	SPT/ RQD	_		SAMPLE ID		81.7 GR	GRAD cs	LAT DATIO FS	/ LON N (% SI		ATT LL	41.4 ERBE PL	_	30, -81 wc	.679520 ODOT CLASS (GI	SO4 ppm	1 OF 1 BACK FILL
ARCHIVE BY YEAR\2021 ARCH	VERY STIFF TO SILT, TRACE TO	AND 6.0" CONCRETE (DRIL D HARD, GRAY AND BROWI D SOME SAND, TRACE TO E CLAY, MOIST TO WET	NISH GRAY,	634.3	- 1 - 2 - 1 - 3 4 - 5 - 5 5 1 1 - 1 - 1 - 1 -	15 11 6 7 7	23 19 23	44 67 78	SS-1 SS-2 SS-3	3.75 4.50 3.00	17 0	8 0	19 8	50 83	6 9 -	NP NP	NP NP		17 22 19	A-4b (4) A-4b (8) A-4b (V)	-	X
OJECTS/1	HARD, BROWN CLAY, TRACE (I AND GRAY, SANDY SILT , I GRAVEL, DAMP	LITTLE	628.0	- 6 - - 7 - EOB	7 9 11	27	100	SS-4	4.50	-	-	-	-	-	-	-	-	16	A-4a (V)	-	1 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4

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(J)	PROJEC	CT: CUY-490-0.00 SUBGRADE	_ DRILLING FIRM / C		R: <u>NEAS / J. HO</u> NEAS / J. HOD			L RIG		ME 45				TION /		SET:		85+6 IR-49	2, 74'	RT. EX	PLORA B-014	ATION ID -0-21
	TYPE: _		—			IGES_			CME A						_						$\overline{}$	DAGE
3	PID:1	107408 SFN:	_ DRILLING METHOI	D:	3.25" HSA		CALI	IBRATI	ON DATE:	1:	2/5/19	9	ELE	VATIO	N: _6	48.4	1 (MS	L)_	EOB:	7.5 ft.		PAGE
749	START:		_ SAMPLING METHO	D:	SPT		ENE	RGY F	ATIO (%):		81.7		LAT	/ LON	G:		41.4	7675	2, -81	.678275		1 OF 1
5		MATERIAL DESCRIPT	ON	ELEV.	DEPTHS	SPT/	N _{eo}		SAMPLE					N (%)	-		ERBE			ODOT	SO4	BACK
₹		AND NOTES		648.4		RQD	. 460	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
S\1ARCHIVE BY YEAR\2021 ARCH	DESCR MEDIUM	ONCRETE AND 9.0" BASE (DRILL RIPTION) M DENSE, BROWN, COARSE AN SILT, LITTLE GRAVEL, TRACE C	D FINE SAND, LAY, DAMP		- 1 2 3 4 5 6 - 6	14 13 8 12 10 8 6 7	29 25 16	67 33 67	SS-1 SS-2 SS-3	-	18 17 -	20 12 -	38 57	19 12 -	_	-		NP NP	7 5 8	A-3a (0) A-3a (0) A-3a (V)	2133	3
OJECT			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	640.9	- 7 - EOB	6	14	39	SS-4	-	-	-	-	-	-	-	-	-	7	A-3a (V)	-	7 > 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

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\GINT	PROJEC	CT:	CUY-490-0		DRILLING FI							L RIG:		ME 45				TION		SET			43, 40	RT. EX	PLORA B-015-	TION ID -0-21
00	TYPE: _		SUBGRADE		SAMPLING F			NEAS / J		3EO_		MER:						SNME	-			IR-49	-		$\overline{}$	DAGE
0-0	PID:	107408	SFN:		DRILLING MI	ETHOD	:	3.25" HS	SA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE'	VATIO)N: _	647.	3 (MS	SL)_	EOB:	7.5 ft.		PAGE
Y-49	START:	:7/26/21	END:	7/26/21	SAMPLING N	ИЕТНО	D:	SPT			ENE	RGY R	ATIO (%):		81.7		LAT	/ LON	IG: _		41.4	7977	72, -81	.666011		1 OF 1
CU			MATERIAL D	DESCRIPTION	V		ELEV.	DEPTH:	S	SPT/	N _{eo}	REC	SAMPLE	HP		GRAD	OITA	N (%)		ATT	ERBE	RG		ODOT	SO4	BACK
IIVE			AND I	VOTES			647.3	DEI III	0	RQD	1 160	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
R\2021 ARCH	DESC	RIPTION) JM DENSE,	BROWN, CO	OARSE AND F	FINE SAND,		645.9		- 1 - - 2 -	16	29	61	SS-1		11	15	46	21	7	NP	NP	NP	9	A-3a (0)	2367	-
/E BY YEAF	SOME	: SIL1, LI111	LE GRAVEL,	TRACE CLAY	, DAMP		242.5		- 3 -	10 10 11 10	29	39	SS-2	-	-	-	-	-	-	-	-	-	7	A-3a (V)	-	V 1 7 V 1 7
11ARCHIN	MEDIU	JM DENSE,		ARSE AND F		,	_642.5_		5 - 6 -	4 5 4	12	67	SS-3A SS-3B	-	2	15	71	10	2	- NP	- NP	 NP	19 8	A-3a (V) A-3a (0)	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
OJECTS	IIVACE	L OILT, TIVE	OL OLAT, IN	VIOL GIVIVE	L, DAME		639.8	EOB	7 -	4 4 4	11	56	SS-4	-	-	-	-	-	-	-	-	-	6	A-3a (V)	-	7 > 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

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Į.	PROJECT	Γ:(CUY-490-0	0.00	DRILLING FIF	RM / O	PERATOR	: NEAS	/ J. HOD	GES_	DRIL	L RIG	C	ME 45	В		STA	TION	/ OFI	FSET	ī: <u>1</u>	025+	70, 40	LT. EX		ATION ID
ĕ	TYPE:	SI	UBGRADE	<u> </u>	SAMPLING FI	IRM / I	LOGGER:	NEAS.	J. HOD	GES	HAM	MER:	CME A	NOTU	1ATIC)	ALIC	SNME	NT:			IR-49	90		B-016-	-0-21
)7408 SF	N:		DRILLING ME	ETHOD) :	3.25" I	HSA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE	VATIO	DN:	640.	3 (MS	SL)	EOB:	7.5 ft.		PAGE
7-490	START: _		END:	7/23/21	SAMPLING M	IETHO	D:	SF			ENE	RGY R	ATIO (%):		81.7			/ LON	_					.664827		1 OF 1
Ś		M	ATERIAL	DESCRIPTIO	N		ELEV.	DEDT	110	SPT/		REC	SAMPLE	HP	(GRAD	OITA	N (%)		ATT	ERBE	ERG		ODOT	SO4	BACK
NE			AND	NOTES			640.3	DEPT	HS	RQD	N ₆₀	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	wc	CLASS (GI)		
ARCH	8" CONC		8" BASE	(DRILLERS			639.0		 - 1 -																	
EAR\2021		,	- ,	OARSE AND I	- ,				2	10 8 10	25	67	SS-1	-	15	32	39	11	3	NP	NP	NP	10	A-3a (0)	973	11 1
VE BY Y		E SAND, TRA	- ,	NE SAND , "AI TRACE GRA	ND" VEL, TRACE				E 4 =	9 11 7	25	56	SS-2		-	-	-	-	-	-	-	-	5	A-3 (V)	-	7>L1
1ARCH	OL (1, D)	, uvii				.F:3.			5 -	8 10 7	23	72	SS-3	-	7	37	46	8	2	NP	NP	NP	5	A-3 (0)	-	17 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 ×
(OJECTS)							632.8	— ЕОВ —	- 7 -	7 7 8	20	67	SS-4	-	-	-	-	-	-	-	-	-	4	A-3 (V)	-	1 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

90-0 ⁻ 06	PROJECT: TYPE: PID:10740 START:7/2	CUY-490-0.00 SUBGRADE 8 SFN:	DRILLING FIRM / C SAMPLING FIRM / DRILLING METHO SAMPLING METHO	LOGGER: _ D:	NEAS / J. HO NEAS / J. HOI 3.25" HSA SPT		HAM CALI		CME A ON DATE: ATIO (%):	12			ALIC ELE	TION SNME VATIO	:NT: DN: _		8 (MS	IR-49 SL)	EOB:		B-017	ATION ID -0-21 PAGE 1 OF 1
VE/CU		MATERIAL DESCRIPT AND NOTES	ION	ELEV. 629.8	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAE cs	DATIC FS	N (%)) CL	ATT LL	ERBE PL	PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
IS\1ARCHIVE BY YEAR\2021 ARCHI	MEDIUM DEI COARSE AN GRAVEL, TR (FILL)	TE AND 8" BASE (DRILLER IN) NSE, BROWN AND ORANG ID FINE SAND, SOME SILT, ACE CLAY, DAMP TO MOIS	SH BROWN, TRACE T		- 1 - 2 - 3 - 4 - 5 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6	7 9 10 9 7 8	26 20 27	44 39 50	SS-1 SS-2 SS-3		0 9 -	11 10 -	59 50	25 24 -			NP NP	NP NP	9 12 9	A-3a (0) A-3a (0) A-3a (V)	0 -	V1 1 V 1 1 V 1 7 V 1 V 1 V 1 V 1 V 1 V 1
OJECT	TRACE GRA		++++ +++ +++	622.3	EOB - 7 -	9 13	30	44	SS-4	4.50	-	-	-	-	-	-	-	-	18	A-4b (V)	-	1>L1

SINT	PROJECT	: CUY-490	-0.00	DRILLING FIF	RM / O	PERATOR	: NEAS	/ J. HOD	GES	DRIL	L RIG:	C	ME 45	В		STA	TION	/ OFF	SET	: <u>1</u>	032+	80, 42	<u>' LT.</u> EX		TION ID
00	TYPE:	SUBGRAD	E	SAMPLING F	IRM / L	LOGGER:	NEAS /	J. HODO	GES	HAM	MER:	CME A	NOTU	MATIC)	ALIC	SNME	NT:			IR-49	90		B-018-	0-21
		7408 SFN:		DRILLING ME	ETHOD):	3.25" H	-ISA		CALI	BRATI	ON DATE:	1:	2/5/19	9	ELE	VATIC	N: -	624.	6 (MS	SL)	EOB:	7.5 ft.		PAGE
6	START: _	7/23/21 END: _	7/23/21	SAMPLING M			SP					ATIO (%):		81.7			/ LON	_					.662227		1 OF 1
Ś		MATERIAL	DESCRIPTION	N		ELEV.	DEDT		SPT/		REC	SAMPLE	HP		GRAD	OITA	N (%)		ATT	ERBE	RG		ODOT	SO4	BACK
IIVE		AND	NOTES			624.6	DEPT	HS	RQD	N ₆₀	(%)	ID	(tsf)	GR	cs	FS	SI	CL	LL	PL	PI	wc	CLASS (GI)		FILL
ARCH	8" CONC DESCRIP	RETE AND 6" BASE PTION)	(DRILLERS			623.4		 - 1 -																	
EAR\2021		DENSE, BROWN, S , TRACE CLAY, DAM		RACE		621.6		2	9 10 12	30	67	SS-1	-	8	8	36	44	4	NP	NP	NP	14	A-4a (3)	627	7 4 7
VE BY Y		DENSE TO DENSE, SAND, TRACE CLAY,			+ + + + + + + + + + + + + + + +			- 3 - - 4 -	10 10 13	31	67	SS-2	-	0	1	10	80	9	NP	NP	NP	20	A-4b (8)	-	1 > \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1 \ 1
1ARCH					++++				8 6 7	18	56	SS-3	-	-	-	-	-	-	-	-	1	21	A-4b (V)	-	~
DJECTS					++++	617.1	— FOB—	- 6 - 7 -	6 7 6	18	67	SS-4	-	-	-	-	-	-	-	-	-	26	A-4b (V)	-	1 > L 1

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SINT	PROJECT	:C	UY-490-0	.00	DRILLING F	IRM / C	PERATOR	: NEAS	/ J. HOD	GES_	DRIL	L RIG:	C	ME 45	В		STA	TION	/ OF	FSET	ī: <u>1</u>	036+	77, 37	' RT EX		ATION ID
ğ	TYPE:	SL	JBGRADE		SAMPLING	FIRM /	LOGGER:	NEAS /	J. HOD	GES	HAM	MER:	CME A	UTON	1ATIC	;	ALIC	SNME	NT:			IR-49	90		B-019-	-0-21
		7408 SFN	N:		DRILLING M	/ETHO	D:	3.25" I	HSA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE	VATIO	ON:	624.	2 (MS	SL)	EOB:	7.5 ft	.	PAGE
7-490	START: _	7/23/21	END:	7/23/21	METHO	DD:	SP	Т		ENE	RGY R	ATIO (%):		31.7		LAT	/ LON	ا اG: _		41.4	47970	8, -81	.660794		1 OF 1	
Ś		MA	TERIAL D	DESCRIPTION		ELEV.	DEDT	T.I.C	SPT/	N	REC	SAMPLE	HP	(SRAD	ATIC	N (%)	ATT	ERBE	RG		ODOT	SO4	BACK	
Ĭ.			AND I	NOTES			624.2	DEPT	по	RQD	N ₆₀	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
ARCH	8" CONC DESCRIP	RETE AND P	8" BASE (DRILLERS			622.9		- 1 -																	
EAR\2021		ANDY SILT,		GRAYISH BR GRAVEL, TRA					2	8 11 12	31	44	SS-1	-	8	8	34	44	6	NP	NP	NP	16	A-4a (3)	820	1 1 1
IVE BY Y									- 4 -	7 9 11	27	67	SS-2		1	•	1	-		-	-	-	19	A-4a (V)	-	
1ARCH							618.2		5 -	7 8 8	22	56	SS-3	-	2	2	45	44	7	NP	NP	NP	20	A-4a (3)	-	
SUECTS		DENSE, GR RACE GRAV		LITTLE CLA T	Y, LITTLE	++++	616.7	EOB	- 6 - 7	9 10 10	27	67	SS-4	-	1	1	-	-	-	-	-	1	18	A-4b (V)	-	1 / V / V
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2	PROJECT:	CUY-490	0.00	DRILLING FIRM	1 / OP	PERATOR:	NEAS	/ J. HOD	GES_	DRIL	L RIG:	C	ME 45	В		STAT	ION /	OFFSE	T:	1040+	62, 48	<u>'LT.</u> EX		TION ID
٤	TYPE:	SUBGRAD	DE	SAMPLING FIR	M/LC	OGGER:	NEAS /	J. HOD	GES	HAM	MER:	CME A	NOTU	MATIC	;	ALIG	NMEN	T:		IR-49	90		B-020-	0-21
į	PID: 1074	108 SFN:		DRILLING MET	HOD:	_	3.25" I	HSA		CALI	BRATI	ON DATE:	12	2/5/19		ELEV	OITA	I: 63	.2 (M	ISL)	EOB:	7.5 ft.		PAGE
¥ 8	START:7	7/23/21 END:	7/23/21	SAMPLING ME	THOD	D:	SP	т		ENEF	RGY R	ATIO (%):		81.7		LAT /						.659372		1 OF 1
3		MATERIAL	DESCRIPTION	Ň		ELEV.	DEPT	LIC	SPT/	NI.	REC	SAMPLE	HP		GRAD	OITA	l (%)	AT	TERB	ERG		ODOT	SO4	BACK
		ANI	D NOTES			631.2	DEPT	по	RQD	N ₆₀	(%)	ID	(tsf)	GR	CS	FS	SI (L LL	PL	PI	wc	CLASS (GI)	ppm	FILL
1 ARC	8" CONCRI DESCRIPT	ETE AND 6" BASI ION)	E (DRILLERS		\boxtimes	630.0		 - 1 -																
ARIZUZ	FRAGMEN	ROWN AND GRAY TS WITH SAND , S GRANULAR BAS	SOME SILT, TR	ACE CLAY,		628.5		_ 2 -	6 13	33	44	SS-1A	-	37	21	17	21	1 NF	NP	NP	13	A-1-b (0)	2600	1 / / / / / / / / / / / / / / / / / / /
1		ENSE TO DENSE		/ l+	+++	627.7		3 +	7			SS-1B SS-2A	<u> </u>	1	<u>-</u>	14	- 73 1	- 2 NF	NP	NP	14 19	A-4b (V) A-4b (8)	-	1>11
		ND, LITTLE CLAY		EL, WET	F.S.	626.7		⊢ 4 +	11 9	27	67	SS-2B	-	-	-	-	-	- -	-	-	18	A-3 (V)	-	7/2/1
בול בול בול בול בול בול בול בול בול בול		ENSE, BROWN, F AY, TRACE GRAV		OME SILT,	+++			5	6	29	72	SS-3	-	0	0	23	69	3 NF	NP	NP	19	A-4b (8)	-	1 × 1 × 1
JJECIOI.		ENSE TO DENSE ID, TRACE CLAY,	,	GRAY, SILT , ‡ EL, WET ‡	+++	623.7	- FOB	- 6 - - 7 -	5 4 4	11	89	SS-4	-	-	-	-	-		-	-	19	A-4b (V)	-	1 × 1 × 1 × 1 × 1

(FILL)

正																									
Ĭ	PROJECT:	CUY-490-	-0.00	DRILLING FIRM	M / OPEF	RATOR:	NEAS	/ J. HOD	GES	DRIL	L RIG:	С	ME 45	В		STA	TION	/ OF	FSET	: _1	045+2	27, 40	'RT. EX		TION ID
ĕ	TYPE:	SUBGRAD	E	SAMPLING FIF	RM / LOG	GER:	NEAS /	J. HODO	GES	HAM	MER:	CME A	NOTUA	1ATIC	;	ALIG	SNME	NT:			IR-49	90		B-021-	0-21
		408 SFN:		DRILLING MET	HOD:	_	3.25" H	HSA		CALI	BRATI	ON DATE:	1:	2/5/19	9	ELE'	VATIO	ON:	641.	1 (MS	SL)	EOB:	7.5 ft.		PAGE
\approx		7/23/21 END:	7/23/21	SAMPLING ME	THOD:		SP	Т		ENE	RGY R	ATIO (%):		81.7			/ LON	_				'1, - 81	.657699		1 OF 1
Ş		MATERIAL	DESCRIPTION	v	EL	EV.	DEDT		SPT/	N.	REC	SAMPLE	HP	(SRAE	OITAC	N (%))	ATT	ERBE	RG		ODOT	SO4	BACK
ΝĒ		AND	NOTES		64	11.1	DEPT	H5	RQD	N ₆₀	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
1 ARCH	8" CONCR DESCRIPT	ETE AND 8" BASE ION)	(DRILLERS		63	39.8		 - 1 -																	***
'EAR\202	GRAVEL A	DENSE TO DENSE, AND STONE FRAG CE CLAY, CONTAI	MENTS WITH	SAND AND				2 - 2	12 8 10	25	44	SS-1	-	28	13	34	20	5	NP	NP	NP	10	A-2-4 (0)	1400	1 1 7
IVE BY \	STAINING (FILL)	, DAMP TO WET			63	36.6		_ 4 _	12 14 13	37	44	SS-2	-	-	-	-	-	-	-	-	-	15	A-2-4 (V)	-	1 > \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
\1ARCH	SAND, SO	DENSE, DARK BRC ME SILT, LITTLE G S GLASS FRAGME	RAVEL, TRAC	E CLAY,	63	35.1		- 5 - - 6	11 10 8	25	56	SS-3	-	19	17	36	22	6	NP	NP	NP	14	A-3a (0)	-	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
JECTS	∖(FILL)	ARK BROWN, GRA		ONE /	63	33.6	FOR	- 7 -	12 13 13	35	50	SS-4	-	-	-	-	-	-	-	-	-	14	A-2-4 (V)	-	1 / V / V
OIL PRC	FRAGMEN	ITS WITH SAND A I GGLASS FRAGME	ND SILT, TRAC			•	—EOB—										·	•	•						

490-0.00	PROJECT: CUY-490-0.00 TYPE: SUBGRADE PID: 107408 SFN: START: 7/16/21 END: 7/	SAMPL DRILLI	LING FIRM / OP PLING FIRM / LO LING METHOD: PLING METHOD	OGGER:	NEAS / NE	SA		HAM CALI		CME A ON DATE: ATIO (%):	12		_	ALIG ELE\	NMEN	l: <u>63</u>	 2.1 (M	ANE SL)	EOB:		B-022-0	TION ID 0-21 PAGE 1 OF 1
HIVE\CUY	MATERIAL DES AND NO	SCRIPTION		ELEV. 632.1	DEPTH		SPT/ RQD	N ₆₀		SAMPLE ID			CS	OITA		ΑT	TERB		WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
ECTS/1ARCHIVE BY YEAR\2021 ARC	4.0" ASPHALT AND 8.0" CONCRIDESCRIPTION) MEDIUM DENSE, BROWN, COARLITTLE GRAVEL, LITTLE SILT, TR MEDIUM DENSE, BROWN, FINE STRACE COARSE SAND, TRACE COWET	RSE AND FINE SAI RACE CLAY, DAMF	AND, IP ILT, RAVEL,	631.1 629.1 624.9		1 - 1 - 2 - 3 - 3 - 4 - 5 - 5 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6	18 11 8 6 7 8 5 7 7	26 20 16	89 61 100	SS-1 SS-2 SS-3 SS-4A		17 0 -	10 5 -	57 87 -	13 7 -	3 NF 1 NF	1		10 24 22 23	A-3a (0) A-3 (0) A-3 (V) A-3 (V)	400 - -	**************************************
IIL PRO,	MEDIUM DENSE, GRAY, SILT , LI [*] CLAY, TRACE GRAVEL, WET	TTLE SAND, LITTL	TLE JHILL	624.6	—EOB—	_ / _	7			SS-4B					-		_ -	<u>. </u>	22	_A-4b (V)_	-	

490-0.00\GIN	PROJECT: CUY-490-0.00 TYPE: SUBGRADE PID: 107408 SFN:	DRILLING FIRM / OP SAMPLING FIRM / LO DRILLING METHOD:	OGGER: _	NEAS / ASHB 3.25" HSA		HAM! CAL!!		CME A	12	1ATIC 2/5/19	; 9	ALIC		NT: DN:		 L 5 (MS	ANE	EOB:	7.5 ft	B-023	ATION ID -0-21 PAGE 1 OF 1
HIVE\CUY-	START: 7/15/21 END: 7/15/21 MATERIAL DESCRIPTION AND NOTES		ELEV. 638.5	SPT DEPTHS	SPT/ RQD			SAMPLE ID		81.7 GR	GRAD CS		/ LON N (%) SI	_	ATT LL	ERBE	_	27, -81 wc	.689447 ODOT CLASS (GI)	SO4 ppm	BACK
ARCHIVE BY YEAR\2021 ARC	4.0" ASPHALT AND 8.0" CONCRETE (DRIL DESCRIPTION) MEDIUM DENSE, BROWN AND GRAY, GRA STONE FRAGMENTS WITH SAND, TRACE TRACE CLAY, DAMP TO MOIST	AVEL AND SILT,	637.5	- 1 - 2 - 3 - 4 - 5	11 9 10 5 5 4	26 12 18	22 39 56	SS-1 SS-2 SS-3	-	51 51	17 16	21 21 -	9 10 -	2 2		NP NP	NP NP	11 11 16	A-1-b (0) A-1-b (V)	-	3
KOJECI SVI	VERY STIFF, GRAY, SILT , LITTLE CLAY, TF SAND, TRACE GRAVEL, MOIST	RACE ++++	631.0	- 6 - 7	6 6 7	18	67	SS-4	2.75	-	-	-	-	-	-	-	-	20	A-4b (V)	-	1

{	ROJECT	T: CUY-490-0.00 SUBGRADE	DRILLING FIRM / O SAMPLING FIRM / I					L RIG: MER:	CME A	ME 45		 ;		TION		FSE1		3050- ANE	+96, 5' E-S	LT. EX	PLORA B-024	ATION ID -0-21
"I	ID: <u>10</u> TART: _	07408 SFN:	DRILLING METHOD SAMPLING METHO		3.25" HSA SPT		_		ON DATE: ATIO (%):		2/5/19 81.7	9		VATION /	-	652.			EOB: 60, -81	7.5 ft.		PAGE 1 OF 1
) \ 		MATERIAL DESCRIPTION AND NOTES	٧	ELEV. 652.7	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAD CS	ATIO FS	N (%)) CL	ATT LL	ERBI PL	ERG PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
:\!	DESCRI	- 1		651.8	 - 1 -																	***
{	SOME S	M DENSE, BROWN, COARSE AND F BILT, LITTLE GRAVEL, TRACE CLAY IRON STAINING, MOIST		649.7	_ 2 -	9 11 10	29	78	SS-1	-	11	15	39	27	8	NΡ	NP	NP	11	A-3a (0)	133	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
		DENSE, BROWN, GRAVEL WITH SILT, TRACE CLAY, WET			_ 4 -	8 7 7	19	67	SS-2	-	18	33	29	16	4	NP	NP	NP	15	A-1-b (0)	-	1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 ×
				646.7	W 647.3 - 5	7 9 10	26	78	SS-3	-	-	1	-	-	-	ı	-	-	17	A-1-b (V)	-	1 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
		BROWNISH GRAY, SILT , LITTLE CL TRACE GRAVEL, DAMP	AY, LITTLE	645.2	EOB 7 -	10 10 11	29	72	SS-4	4.50	-	-	-	-	-	-	-	-	14	A-4b (V)	-	1 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

START:	-0.00\GIN	PROJECT: CUY-490-0.00 TYPE: SUBGRADE	DRILLING FIRM / OI SAMPLING FIRM / L	OGGER:	NEAS / ASHB		НАМ	L RIG:	CME A		/ATIC	;	STA [*]	SNME	NT:		L	ANE			B-025	ATION ID -0-21 PAGE
MATERIAL DESCRIPTION AND NOTES G67.3 DEPTHS SPT/ RQD R	-490		-				_								_	667.						-
## ASPHALT AND 8" CONCRETE (DRILLERS DESCRIPTION) MEDIUM DENSE, BROWN AND GRAY, GRAVEL AND STONE FRAGMENTS WITH SAND, LITTLE SILT, TRACE CLAY, CONTAINS GRANULAR BASE MATERIAL AND CONCRETE FRAGMENTS, DAMP (FILL) MEDIUM DENSE, BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, CONTAINS GRANULAR BASE MATERIAL AND CONCRETE FRAGMENTS, DAMP (FILL) MEDIUM DENSE TO DENSE, BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, DAMP 10 26 39 SS-2 5 A-1-b (V) - 7 LV SAND, LITTLE SILT, TRACE CLAY, DAMP	11 VEICUY	MATERIAL DESCRIPTION		ELEV.				REC	SAMPLE	HP	(GRAD	ATIO	N (%))	ATT	ERBI	ERG	,	ODOT		BACK
MEDIUM DENSE TO DENSE, BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, DAMP SAND, LITTLE SILT, TRACE CLAY, DAMP 15 15 16 16 17 18 32 31 15 4 NP NP NP NP 6 A-1-b (0) - 7 17 17 17 17 17 17 17 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	E BY YEAKIZUZI ARUL	DESCRIPTION) MEDIUM DENSE, BROWN AND GRAY, GRAY STONE FRAGMENTS WITH SAND, LITTLE TRACE CLAY, CONTAINS GRANULAR BAS AND CONCRETE FRAGMENTS, DAMP	AVEL AND	666.3	- 1 - 2 - 3	10 12 8		56		-	21	29	29	16	5	NP -	NP -	NP -		,		1 2 2 1 1 2 1 1 2 1 1 2 1 1 1 1 1 1 1 1
単	CI S\1ARCHIVI	MEDIÚM DENSE TO DENSE, BROWN, GRA	VEL WITH		- 4 - 5 - 6	15 16		72 89	SS-3 SS-4	-	18	32	31	15	4	NP	NP	NP		,		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

PROJECT: TYPE: PID: 1074 START:		DRILLING FIRM / C SAMPLING FIRM / I DRILLING METHOD SAMPLING METHO	LOGGER:):			HAM CALI			12			ALIC	TION SNME VATION	NT: _ DN: _		8 (MS	ANE SL)	EOB:	RT. E	B-026	ATION ID -0-21 PAGE 1 OF 1
	MATERIAL DESCRIPTION AND NOTES	V	ELEV. 677.8	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAD CS	ATIO FS	N (%)	CL	ATT LL	ERBE PL	RG PI	wc	ODOT CLASS (GI	SO4 ppm	
MEDIUM D	LT AND 7" CONCRETE (DRILLEF TION) DENSE TO DENSE, BROWN, COA D, SOME GRAVEL, LITTLE SILT, NTAINS TRACE IRON STAINING,	ARSE AND TRACE	676.7	- 1 - 1 - 2 - 1 - 3 - 1 - 4 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	18 13 14 10 12 11	37 31	56 56	SS-1 SS-2	-	23 25	25 24	31 32	16 15		NP NP	NP NP	NP NP	7	A-3a (0)		17 × 17 × 17 × 17 × 17 × 17 × 17 × 17 ×
@6.0'; SS-4	4 BECOMES TRACE GRAVEL		670.3	- 5 - - 6 - - 7 -	10 10 10 12 13	27 34	44 67	SS-3 SS-4	-	-	-	-	-	-	-	-	-	7 8	A-3a (V) A-3a (V)		V

F																			
PROJECT: <u>CUY-490-0.00</u>						L RIG	C	ME 45	В			TION /		_		16, 27	" RT. EX	PLORA B-027-	ATION ID
SUBGRADE	SAMPLING FIRM /	LOGGER:	NEAS / ASHBA	JGH_	HAM	MER:	CME A	NOTU	1ATIC	<u> </u>	ALIC	SNMEN	T:	L	_ANE	E-S		D-027-	-
ର୍ଚ୍ଚ PID: <u>107408</u> SFN:	DRILLING METHO	D:	3.25" HSA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE'	OITAV	l: <u>67</u> 4	I.5 (M	ISL)_	EOB:	7.5 ft.		PAGE
START: <u>7/13/21</u> END: <u>7/</u>	13/21 SAMPLING METHO	D:	SPT		ENE	RGY F	ATIO (%):	8	81.7		LAT	/ LONG	i:	41.	4726	95, - 81	.693585		1 OF 1
MATERIAL DES	CRIPTION	ELEV.	DEPTHS	SPT/	N ₆₀	REC	SAMPLE	HP	(GRAD	OITAC	N (%)	AT	TERB	ERG		ODOT	SO4	BACK
₹ AND NO	TES	674.5	DEFINS	RQD	1460	(%)	ID	(tsf)	GR	CS	FS	SI C	L LL	PL	PI	WC	CLASS (GI)	ppm	FILL
4" ASPHALT AND 6" CONCRETE DESCRIPTION) MEDIUM DENSE, BROWN BECOI GRAY, COARSE AND FINE SAND CLAY, TRACE GRAVEL, SS-1 ANI STAINING, DAMP TO MOIST	MING BROWN AND , SOME SILT, TRACE	673.7	- 1 - 1 - 2 - 1 - 3 - 1 - 3 - 1 - 1 - 1 - 1 - 1 - 1	11 11 10 10 8 11 4 4 8 8	29 26 16	50 67 28 39	SS-1 SS-2 SS-3 SS-4	-	5 - 7 -	10 - 20 -	54 - 39 -	-	6 NP NP	-	-	10 9 8	A-3a (0) A-3a (V) A-3a (0) A-3a (V)	240	

EXPLORATION ID PROJECT: CUY-490-0.00 DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH DRILL RIG: CME 45B STATION / OFFSET: 3034+13, 26' RT. B-028-0-21 TYPE: SUBGRADE SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH HAMMER: CME AUTOMATIC ALIGNMENT: LANE E-S **PAGE** 12/5/19 PID: 107408 SFN: DRILLING METHOD: 3.25" HSA CALIBRATION DATE: ELEVATION: 669.4 (MSL) EOB: 7.5 ft. 1 OF 1 SAMPLING METHOD: SPT **ENERGY RATIO (%):** 41.471613, -81.693416 START: 7/13/21 END: 7/13/21 81.7 LAT / LONG: **MATERIAL DESCRIPTION** ELEV. REC SAMPLE HP **GRADATION (%)** ATTERBERG SPT/ ODOT SO4 BACK **DEPTHS** CLASS (GI) FILL RQD ppm (%) (tsf) GR CS FS SI CL LL PL PΙ WC **AND NOTES** ID 669.4 8" ASPHALT AND 4" CONCRETE (DRILLERS 668.4 DESCRIPTION) MEDIUM DENSE TO VERY DENSE, BROWN, COARSE 1>1 2 AND FINE SAND, LITTLE SILT, LITTLE GRAVEL, 26 33 17 NP NP 10 78 SS-1 11 35 4 NP 9 A-3a (0) 93 TRACE CLAY, SS-2 CONTAINS ASPHALT FRAGMENTS 3 AND IRON STAINING, DAMP 8 22 67 SS-2 7 A-3a (V) 1>1 29 67 SS-3 7 8 A-3a (V) 1>1 1>1 52 56 18 SS-4 6 A-3a (V) 661.9 < , ∨

FILES/CUY-4																						
(')	PROJECT: CUY-490-0.00	DRILLING FIRM / O						L RIG:		ME 45				TION /		SET:				RT. EX		TION ID
	TYPE: SUBGRADE	SAMPLING FIRM / I	_			GES_			CME A					NMEN				MP 7			B-029-	PAGE
0-061	PID:107408	DRILLING METHOD		3.25" H					ON DATE:		2/5/19			VATIO						7.5 ft.		1 OF 1
٦	START: 7/20/21 END: 7/20/21	SAMPLING METHO		SP	1	0.000			ATIO (%):		81.7			/ LONG					1, -81	.679351		
/E/C	MATERIAL DESCRIPTION AND NOTES	V	ELEV.	DEPT	HS	SPT/ RQD	N ₆₀	(%)	SAMPLE ID	HP (tsf)		GRAD/ cs			_	ATTE	PL		wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
I ARCHIVE∖CU	10" CONCRETE AND 7" BASE (DRILLERS DESCRIPTION)		643.8		 - 1 -	- NGD		(70)	ID.	(tsi)	OIX	00	10	OI ,		LL			WO	· · ·		
YEAR\2021	MEDIUM DENSE TO DENSE, BROWN AND BROWN, COARSE AND FINE SAND , SOME TRACE TO LITTLE GRAVEL, TRACE CLAY,	SILT,			_ 2 _ _ 3 _	9 10 15	34	72	SS-1	-	10	23	34	26	7	NP	NP	NP	9	A-3a (0)	300	17 6 7
Β	CONTAINS TRACE IRON STAINING, DAMP		639.8		_ 4 -	9 5 6	15	50	SS-2A SS-2B	-	14	28	30		5	NP -	NP -	NP -	8 11	A-3a (0) A-3a (V)	-	7 V 7 V 7 V 7 V 7 V 7 V 7 V 7 V 7 V 7 V
\1ARCHI	MEDIUM DENSE, GRAY AND BROWN, COA FINE SAND , SOME SILT, LITTLE GRAVEL, L CLAY, DAMP				- 5 - - - 6 -	7 6 7	18	61	SS-3	-	-	-	-	-	-	-	-	-	6	A-3a (V)	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
OJECTS	, 		636.3	–EOB—	- - 7 -	5 4 4	11	67	SS-4	-	-	-	-	-	-	-	-	-	9	A-3a (V)	-	1 / / / / / / / / / / / / / / / / / / /
STANDARD ODOT LOG W/ SULFATES (8.5 X 11) - OH DOT.GDT - 8/28/23 17:14 - X'ACTIVE PROJECTSIACTIVE SOIL PROJECTS\1ARCHIVE																						

00\GIN I	PROJECT: TYPE:	CUY-490 SUBGRAD		DRILLING FIRM SAMPLING FIRM			/ J. HOD / J. HOD(L RIG: MER:	C	ME 45		<u></u>	STA			FSE1		68+99 NMP 7	9, 19' l 7-7C	RT. EX	PLORA B-030-	
490-0	PID: <u>107408</u> START: 7/20		7/20/21	DRILLING METH SAMPLING MET		3.25" I SF			_		ON DATE: ATIO (%):		<u>2/5/19</u> 81.7	9	ELE LAT		-	624.			EOB:	7.5 ft. .679382		PAGE 1 OF 1
VE\CUY.		MATERIAL	L DESCRIPTION D NOTES	_	ELEV. 624.2	DEPT		SPT/ RQD	N ₆₀		SAMPLE ID	_	_	GRAD cs	ATIO FS	_		ATT	ERBE	_	WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
21 ARCH	DESCRIPTION	l)	SE (DRILLERS	X	622.8		- 1 -			,		,												- 5 LV 3
/EAR\202	LITTLÉ CLAY,	LITTLE GRAV	GRAY, SANDY (EL, CONTAINS AINING, DAMP	BRICK	621.2		- 2 - - 3 -	14 20 21	56	50	SS-1	4.50	13	12	11	47	17	29	22	7	12	A-4a (6)	873	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
VE BY			, GRAVEL AND		619.7		_ 4 _	16 22 24	63	33	SS-2	-	26	27	21	21	5	NP	NP	NP	8	A-2-4 (0)	-	7 × 1 7 × 1 7 × 1 7 × 1 7
1ARCH	DAMP		ND SILT, TRAC				- 5 - - 6 -	9 12 16	38	67	SS-3	4.50	-	-	-	-	-	-	-	-	12	A-4a (V)	-	<pre></pre>
SISS	GRAVEL, DAN		.i, cirrice oca	I, IIVOL	616.7	— FOB —	- 7 -	9 11 13	33	56	SS-4	4.50	-	-	-	-	-	-	-	-	13	A-4a (V)	-	1 L 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

PROJECT:CUY-490-0.00 TYPE:SUBGRADE PID:107408	DRILLING FIRM / OP SAMPLING FIRM / LO DRILLING METHOD: SAMPLING METHOD	OGGER: _	NEAS / J. HOD NEAS / J. HOD 3.25" HSA SPT		HAMI CALII			12			ALIC	TION . SNME VATIC / LON	NT: _ N: _(RA 3 (MS	MP 7 SL)	EOB:		B-031-	TION ID 0-21 PAGE 1 OF 1
MATERIAL DESCRIPTION AND NOTES		ELEV. 623.3	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAD CS	ATIO FS	N (%) SI	CL	ATTI LL	ERBE PL	RG PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
HARD, BROWN, SANDY SILT, LITTLE GRAY LITTLE CLAY, DAMP (FILL) MEDIUM DENSE TO DENSE, BROWN AND BROWN, GRAVEL AND STONE FRAGMENT SAND AND SILT, TRACE CLAY, CONTAINS STAINING AND TRACE BRICK FRAGMENTS (FILL)	ORANGISH FS WITH IRON S, DAMP	620.3	- 1 - 2 - 1 - 3 - 1 - 3 - 1 - 1 - 1 - 1 - 1 - 1	8 8 10 10 12 14 11 8 12 15	23 27 34 37	72 50 56 61	SS-1 SS-2 SS-3 SS-4	4.50	18 27 -	18 26 -	18 18 -	31 22 -	-	24 NP -	17 NP -	7 NP -	11 9 10	A-4a (2) A-2-4 (0) A-2-4 (V) A-2-4 (V)	100	7

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ני	PROJECT: CUY-490-0.00 TYPE: SUBGRADE	DRILLING FIRM / C		NEAS / J. HOD			L RIG: MER:		ME 45				TION /	OFFS	_	76+1 RAMP	2, 11' l		PLORA B-032-	TION ID 0-21
90-0	PID: 107408 SFN: START: 7/20/21 END: 7/20/21	DRILLING METHOD SAMPLING METHOD	D:	3.25" HSA SPT		CALI	BRATI	ON DATE: ATIO (%):	12	2/5/19 31.7		ELE/		N: 62	21.4 (N	1SL)_	EOB:	7.5 ft.		PAGE 1 OF 1
VE/CUY-	MATERIAL DESCRIPTION AND NOTES		ELEV. 621.4	DEPTHS	SPT/ RQD	N ₆₀		SAMPLE ID	$\overline{}$		RAD cs		N (%)		TTERE	BERG	WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
21 ARCHI	HARD, GRAYISH BROWN, SANDY SILT , L TRACE GRAVEL, CONTAINS TRACE IRON DAMP		021.4	 _ 1 _			(11)		(121)											\$ \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
/EAR\202	DAMP			_ 2 _	6 11 14	34	72	SS-1	4.50	9	12	13	48	18 2	5 18	7	11	A-4a (6)	960	7
IVE BY				_ 4 _	6 10 14	33	61	SS-2	4.50	10	12	19	44	15 2	3 16	7	11	A-4a (5)	-	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
11ARCH				- 5 - - 6 -	6 16 12	38	67	SS-3	4.50	-	-	-	-	-	-	-	12	A-4a (V)	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
JECTS)			613.0	- 7 -	10 16	45	78	SS-4	4.50	-	-	-	-	-	-	-	12	A-4a (V)	-	1 2 7 7

щ.																						
רי	PROJECT: _	CUY-490-0.00	DRILLING FIRM / C	PERATOR	: NEAS / J. HOD	OGES_	DRIL	L RIG	C	ME 45	БВ		STA	TION	OFF	SET	:8	34+4	6, 21'			TION ID
00	TYPE:	SUBGRADE	SAMPLING FIRM /	LOGGER:	NEAS / J. HOD	GES_	HAM	MER:	CME A	NOTU	/ATIC		ALIC	SNME	NT: _		R/	AMP	C-7		B-033-	
	PID: 10740	08 SFN:	DRILLING METHOD):	3.25" HSA		CALI	BRATI	ON DATE:	1:	2/5/19	9	ELE	VATIC	N: _	656.	6 (MS	L)_	EOB:	7.5 ft.		PAGE
Y-49	START:7/2	20/21 END: 7/20/21	_ SAMPLING METHO	D:	SPT		ENE	RGY R	ATIO (%):		81.7		LAT	/ LON	G: _		41.4	7722	26, -81	.679002		1 OF 1
CU		MATERIAL DESCRIPTION	ON	ELEV.	DEPTHS	SPT/	N _{eo}	REC	SAMPLE	HP	(GRAD	DATIC	N (%)		ATT	ERBE	RG		ODOT	SO4	BACK
₽ 		AND NOTES		656.6	DEFILIS	RQD	11460	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
21 ARCH	10" CONCRI DESCRIPTIO	ETE AND 8" BASE (DRILLER: DN)		655.1	- 1 -																	- 5 LV 1
EAR\20	AND GRAY,	WN MOTTLED WITH ORANG SILT , LITTLE TO SOME CLAY CE GRAVEL, CONTAINS IRON	, LITTLE		- 2 - - 2 -	9 6 7	18	72	SS-1	4.50	6	7	7	60	20	29	22	7	17	A-4b (8)	733	1>V 1
VE BY \	DAMP	SE GIV (VEE, GOIVI) III OI	++++ ++++ ++++		_ 4 -	5 5 6	15	67	SS-2	4.50	7	7	8	58	20	29	22	7	16	A-4b (8)	-	7
1ARCHI			+ + + + + + + + + + + +		- 5 -	5 6 4	14	67	SS-3	4.50	-	-	-	-	-	-	-	-	21	A-4b (V)	-	\(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1}{1} \) \(\frac{1} \) \(\frac{1} \) \(\frac{1} \) \(\frac{1} \) \(\f
JECTS			+ + + + + + + + + + + + + + + +	649.1	EOB 7 -	4 6 4	14	61	SS-4	4.50	-	-	-	-	-	-	-	-	17	A-4b (V)	-	1>V 1

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90-0.00/6	TYPE: SUBGRADE PID: 107408 SFN:	DRILLING FIRM / C SAMPLING FIRM / DRILLING METHOD	LOGGER: D:	NEAS / J. I 3.25" HSA		HAM		CME A	12	1ATIC 2/5/19		ALIG ELE\	NMEI ATIO	N: _6	63.4 (RAMF (MSL)	EOB:	7.5 ft.	B-034-	TION ID 0-21 PAGE 1 OF 1
IIVE\CUY-4	START: 7/20/21 END: 7/20/21 MATERIAL DESCRIPTION AND NOTES	SAMPLING METHO	DD: ELEV. 663.4	SPT DEPTHS	SPT RQE	/ N		SAMPLE ID	_	31.7 GR	GRAD cs	LAT / DATION FS	۱ (%)	A	TTEF	H1.4769 RBERG PL PI		0DOT CLASS (GI)	SO4 ppm	BACK FILL
321 ARCH	8" CONCRETE AND 9" BASE (DRILLERS DESCRIPTION) MEDIUM DENSE, BROWN AND GRAY, STOR	NE Ö'-	662.0	- - -	1 -															- 1 L ^N 1
3Y YEAR\2(FRAGMENTS WITH SAND, LITTLE SILT, TRACONTAINS BRICK FRAGMENTS, DAMP (FILL)	T- / T-C	660.4	 - - -	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	23	39	SS-1 SS-2	-	41 51	21	17	15			IP NP		A-1-b (0)	1413	1
IARCHIVE	MEDIUM DENSE, GRAY, STONE FRAGMEN SAND, TRACE SILT, TRACE CLAY, CONTAIN FRAGMENTS, DAMP ((FILL)	TS, SOME	658.9 657.4	- - - -	4 - ' 5 - 6 ₇	18	39	SS-3	4.50	-	-	-	-	-	-		15	A-1-a (0) A-4a (V)	-	- 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1 × 1
DJECTS	HARD, GRAY, SANDY SILT , LITTLE CLAY, T GRAVEL, MOIST		655.9	- FOB	6 7 7 8 1	25	22	SS-4	-	-	•	-	-	-	-	- -	7	A-1-a (V)	-	1 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
OIL PR(MEDIUM DENSE, GRAY, STONE FRAGMEN SAND, TRACE SILT, TRACE CLAY, DAMP	TS, SOME		LOD																

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רי	PROJECT:	CUY-490-0.00	DRILLING FIRM / O				l	L RIG:		ME 45				TION		FSET			9, 31'		PLORA B-035-	TION ID
00	TYPE:	SUBGRADE	SAMPLING FIRM / I	LOGGER: _.	NEAS / J. HOD	GES_	HAM	MER:	CME A	NOTU	1ATIC	;	ALIC	SNME	NT: _		R.	AMP	B-C			-
	PID: 107408	SFN:	DRILLING METHOD):	3.25" HSA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE	VATIC	N: _	667.	4 (MS	SL)_	EOB:	7.5 ft.		PAGE
۲-49	START:7/22/	/21 END:7/22/21	SAMPLING METHO	D:	SPT		ENE	RGY R	ATIO (%):	8	81.7		LAT	/ LON	IG: _		41.4	48034	17, -81	.667621		1 OF 1
CU		MATERIAL DESCRIPTION	N	ELEV.	DEPTHS	SPT/	N ₆₀	REC	SAMPLE	HP	(GRAD	DATIC	N (%)		ATT	ERBE	ERG		ODOT	SO4	BACK
₽		AND NOTES		667.4	DEFINS	RQD	1460	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
HIVE BY YEAR\2021 ARCH	MEDIUM DENS AND FINE SAN	TE AND 8.0" BASE (DRILLEF) SE, DARK BROWN AND GRAID, LITTLE TO SOME SILT, L CE CLAY, WET TO MOIST	AY, COARSE	666.1	- 1 - 2 3 4	3 5 4 3 5	12 11	67	SS-1 SS-2	-	13 15	19 20	43	20 24		NP NP		NP NP	15 11	A-3a (0) A-3a (0)	153	
\1ARCF					- 5 - - - 6 -	5 3	11	39	SS-3	-	-	-	-	-	-	-	-	-	11	A-3a (V)	-	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
JECTS				659.9	- 7 -	6 4 5	12	50	SS-4	-	-	-	-	-	-	-	-	-	11	A-3a (V)	-	17 \ 7
\approx					-EOB		•	•											•			

EXPLORATION ID PROJECT: CUY-490-0.00 DRILLING FIRM / OPERATOR: NEAS / J. HODGES DRILL RIG: CME 45B STATION / OFFSET: 15+10, 2' LT. B-036-0-21 TYPE: **SUBGRADE** SAMPLING FIRM / LOGGER: NEAS / J. HODGES HAMMER: CME AUTOMATIC ALIGNMENT: RAMP B-C **PAGE** PID: 107408 SFN: DRILLING METHOD: 3.25" HSA CALIBRATION DATE: 12/5/19 ELEVATION: 665.1 (MSL) EOB: 7.5 ft. 1 OF 1 START: 7/21/21 END: 7/21/21 SAMPLING METHOD: SPT **ENERGY RATIO (%):** 81.7 LAT / LONG: 41.479942, -81.668381 REC SAMPLE HP **GRADATION (%) ATTERBERG MATERIAL DESCRIPTION** ELEV. SPT/ ODOT SO4 BACK **DEPTHS** CLASS (GI) FILL RQD ppm GR CS FS SI CL LL PL PΙ WC **AND NOTES** (%)ID (tsf) 665.1 6" CONCRETE AND 8" BASE (DRILLERS 663.9 **DESCRIPTION)** MEDIUM DENSE, BROWN, SANDY SILT, LITTLE 1>1 2 GRAVEL, TRACE CLAY, CONTAINS IRON STAINING, 25 56 SS-1 16 21 24 29 10 NP NP NP 9 A-4a (1) 367 662.1 DAMP 10 3 (FILL) 7 19 44 SS-2 12 20 35 26 NP NP NP 9 A-3a (0) MEDIUM DENSE, BROWN, COARSE AND FINE SAND, 660.6 1>1 SOME SILT, LITTLE GRAVEL, TRACE CLAY, CONTAINS IRON STAINING, DAMP SS-3 9 29 78 9 A-4a (V) 1>1 (FILL) MEDIUM DENSE TO DENSE, BROWN, SANDY SILT, 1>1 31 10 67 SS-4 10 A-4a (V) TRACE TO LITTLE GRAVEL, TRACE CLAY, CONTAINS 657.6 < . v IRON STAINING, SS-4 CONTAINS BRICK FRAGMENTS, DAMP (FILL)

PROJECT:CUY-49 TYPE:SUBGR/ PID:107408	ADE	DRILLING FIRM / C SAMPLING FIRM / DRILLING METHO SAMPLING METHO	LOGGER: _ D:	NEAS / J. H NEAS / J. H 3.25" HSA	HODGES	HAM CALI		CME A ON DATE: ATIO (%):	12			ALIC ELE	TION / SNMEN VATIO / LONG	IT: N: _6	1.4 (N	RAMP (ISL)	EOB:	L	B-037	ATION ID -0-21 PAGE 1 OF 1
٣	AL DESCRIPTION ND NOTES	Ň	ELEV. 651.4	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAE cs	ATIO FS	N (%)	A CL L	ITERI	BERG . PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
8" CONCRETE AND 8" BA DESCRIPTION) MEDIUM DENSE, BROWN LITTLE TO SOME GRAVEL DAMP	COARSE AND I		650.1	- - - - - - - - - - - - - - - - - - -	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	27 22 23 23	56 39 44 61	SS-1 SS-2 SS-3 SS-4		26 16 -	24 26 -	26 35 -	+	6 N 6 N	-			A-3a (0) A-3a (0) A-3a (V) A-3a (V)	-	7

PROJECT: CUY-490-0.00 TYPE: SUBGRADE PID: 107408 SFN: START: 7/21/21 END: 7/21/21	DRILLING FIRM / OPERAT SAMPLING FIRM / LOGGE DRILLING METHOD: SAMPLING METHOD:		S F			12)	ALIG	FION / O INMENT: /ATION: / LONG:	649	R. .1 (M	AMP SL)	EOB:		B-038-	TION ID -0-21 PAGE 1 OF 1
MATERIAL DESCRIPTION AND NOTES	V ELEV 649.	I DEPTHS I	RQD 1	N ₆₀ REC (%)	SAMPLE ID	HP (tsf)		cs	ATIOI FS	N (%) SI CL	AT LL	PL	ERG PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
8" CONCRETE AND 8" BASE (DRILLERS DESCRIPTION) MEDIUM DENSE, BROWN, COARSE AND FLITTLE SILT, TRACE TO LITTLE GRAVEL, TMOIST	647.8	3	6 5 6 4 6	15 67 15 67 14 44 20 50	SS-1 SS-2 SS-3 SS-4		17 8 -	23 18 -	41 50 -	14 5 19 5 	NP NP -	NP NP -	NP NP -	11 11 11	A-3a (0) A-3a (0) A-3a (V) A-3a (V)	340	X

<u>.</u>			-																		
	PROJECT:	CUY-490-0.00	DRILLING FIRM / O				1	L RIG		ME 45			l		OFFS	_		+74, 4'	LT. EX	PLORA B-039-	ATION ID -0-21
8	TYPE:	SUBGRADE	SAMPLING FIRM / L	.OGGER: _	NEAS / J. HOD	GES_	HAIV	1MER:	CME A	UTON	IATIC	<u>; </u>	ALIC	SNME	NI:		RAMP	N-VV			-
9	PID: <u>107408</u>	_ SFN:	DRILLING METHOD	:	3.25" HSA		CAL	IBRATI	ON DATE:	12	2/5/19	9	ELE	VATIO	N: <u>65</u>	7.9 (1	/ISL)_	EOB:	7.5 ft.		PAGE
7₹	START:	21 END: 7/21/21	SAMPLING METHO	D:	SPT		ENE	RGY F	ATIO (%):		81.7		LAT	/ LON	G:	41	.4805	70, -8´	1.663858		1 OF 1
		MATERIAL DESCRIPTION	N	ELEV.	DEPTHS	SPT/	N	REC	SAMPLE	HP		GRAD	DATIC	N (%)	A	ITERI	BERG		ODOT	SO4	BACK
ΞI		AND NOTES		657.9	DEPINS	RQD	N ₆₀	(%)	ID	(tsf)	GR	CS	FS	SI	CL L	. PL	PI	WC	CLASS (GI)	ppm	FILL
/ YEAR\2021 ARC	MEDIUM DENS TRACE SILT, TI FRAGMENTS, I	E, BROWN, GRAVEL WITH RACE CLAY, CONTAINS CO		656.5	- 1 - - 1 - - 2 - - 3 -	6 8	22	56	SS-1		27	44	21	7	1 N	P NF	P NP	7	A-1-b (0)	793	× 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
IIVE B)	(FILL)				_ 4 -	0 7 8	20	50	SS-2	-	16	49	26	7	2 N	P NF	NP	4	A-1-b (0)	-	7 × × 7 × × 7 × × 7 × 7
3/1ARCF					<u> </u>	6 6 7	18	44	SS-3		ı	-	-	-	- -	-	-	5	A-1-b (V)	-	<17 × × × × × × × × × × × × × × × × × × ×
OJECT				650.4	- 6 7 - 7 -	5 6 6	16	39	SS-4	-	1	-	-	-	- -	-	-	4	A-1-b (V)	-	1 / / / / / / / / / / / / / / / / / / /

PROJECT:	DRILLING FIRM / OI SAMPLING FIRM / L DRILLING METHOD SAMPLING METHOI	OGGER: _	NEAS / J. H NEAS / J. HO 3.25" HSA SPT		HAM CALI			12			ALIC ELE	TION SNME VATIO	NT: DN: _		R/ 4 (MS	AMP SL)	EOB:	7.5 ft.	B-040-	ATION ID -0-21 PAGE 1 OF 1
MATERIAL DESCRIPTION ≩ AND NOTES	V	ELEV. 669.4	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAE cs	ATIO FS	N (%)	CL	ATT LL	ERBE PL	PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
6" CONCRETE AND 8" BASE (DRILLERS DESCRIPTION) DENSE, BROWN, FINE SAND, SOME COAR LITTLE GRAVEL, TRACE SILT, TRACE CLAY MEDIUM DENSE, BROWN, FINE SAND, SOI COARSE SAND, TRACE SILT, TRACE CLAY GRAVEL, DAMP	Y, DAMP	668.2 666.4 661.9	- 1 - 2 - 3 - 4 - 5 - 6 - 7	10 18 12 6 4 4 4 5 5	41 11 14 14	56 56 56 78	SS-1 SS-2 SS-3 SS-4		13 0 -	28 28 -	51 66 -	6 5 -		NP NP -	NP NP -	NP NP -	9 5 7 4	A-3 (0) A-3 (0) A-3 (V) A-3 (V)	413	**************************************

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/GIN	PROJECT: CUY-490-0.00	DRILLING FIRM / C	PERATOR	NEAS / J. H	ODGES	DRIL	L RIG	C	ME 45	В		STAT	TION /	OFFS	ET: _	623+	88, 12	LT. EX		TION ID
.00.	TYPE: SUBGRADE	SAMPLING FIRM /	LOGGER:	NEAS / J. HO	DDGES	HAM	MER:	CME A	UTON	/ATIC		ALIG	NME	NT:		RAMP	W-N		B-041-	-
30 - C	PID: 107408 SFN:	DRILLING METHOD):	3.25" HSA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE\	/ATIO	N: 6	10.6 (MSL)	EOB:	7.5 ft.		PAGE
γ4	START: 7/21/21 END: 7/21/21	SAMPLING METHO	D:	SPT		ENE	RGY R	ATIO (%):		81.7		LAT	LON	G:	4	1.4797	16, - 81	.665074		1 OF 1
E/CL	MATERIAL DESCRIPTIO	N	ELEV.	DEPTHS	SPT/	N ₆₀	REC	SAMPLE	HP	(GRAD	ATIO	V (%)	Д	TTER	BERG		ODOT	SO4	BACK
₽	AND NOTES		640.6	DEFINS	RQD	1460	(%)	ID	(tsf)	GR	CS	FS	SI	CL L	L P	- PI	WC	CLASS (GI)	ppm	FILL
021 ARC	MEDIUM DENSE TO DENSE, BROWN, CO FINE SAND, LITTLE SILT, TRACE TO LITTI TRACE CLAY. CONTAINS TRACE IRON ST	E GRAVEL,		- - 1	_															- 1 LV 1
YEAR\2	DAMP TO WET	AINING,		- 2 - 3	6 9 11	27	50	SS-1	-	10	32	31	19	8 1	P N	P NP	10	A-3a (0)	2800	17'1
IIVE BY				_ 4	7 10 10	27	61	SS-2	-	18	31	28	17	6 N	P N	P NP	30	A-3a (0)	-	1 > V 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
3/1ARCF				5	⁷ 11 12	31	56	SS-3	-	-	-	-	-	-	. -	-	6	A-3a (V)	-	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
OJECIS			633.1	- 6 - 7	8 12 11	31	67	SS-4		-	-	-	-	-	. -	-	5	A-3a (V)	-	1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVELED SOIL CUTTINGS

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5	PROJECT: CUY-490-0.00	DRILLING FIRM / OI	PERATOR	R: NEAS / J. HOD	GES	DRIL	L RIG:	C	ME 45	В		STA	TION	/ OF	FSE1	Г:	627	+30, R	TE		ATION ID
3	TYPE: SUBGRADE	SAMPLING FIRM / L	OGGER:	NEAS / J. HODO	SES	HAM	MER:	CME A	UTON	1ATIC	;	ALIC	SNME	NT:		R	AMP	W-N		B-042	_
	PID: 107408 SFN:	DRILLING METHOD	:	3.25" HSA		CALI	BRATI	ON DATE:	12	2/5/19)	ELE	VATIO	ON:	639.	4 (MS	SL)_	EOB:	7.5 ft		PAGE
	START: END:	SAMPLING METHO	D:	SPT		ENE	RGY R	ATIO (%):	8	31.7		LAT	/ LON	NG: _		41.4	47950	05, -81	.663858		1 OF 1
í	MATERIAL DESCRIPTION	V	ELEV.	DEPTHS	SPT/	N ₆₀	REC	SAMPLE	HP	C	SRAD	OITA	N (%))	ATT	ERBE	ERG		ODOT	SO4	BACK
į	AND NOTES		639.4	DEFINS	RQD	11460	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
VII 17	8" CONCRETE AND 9" BASE (DRILLERS DESCRIPTION)		638.0	 - 1 -																	
	MEDIUM DENSE, LIGHT BROWN AND GRA AND STONE FRAGMENTS WITH SAND, TR LITTLE SILT. TRACE CLAY, CONTAINS CO	ACE TO		_ 2 _	10 11 _ 10_	29	44	SS-1	-	31	32	24	11	2	NP	NP	NP	8	A-1-b (0)	1300) / / / / / / / / / / / / / / / / / / /
- N	FRAGMENTS AND TRACE IRON STAINING (FILL)	- C - L		_ 4 _	7 9 10	26	50	SS-2	-	23	40	25	10	2	NP	NP	NP	10	A-1-b (0)	-	7
				5 -	7 8 13	29	44	SS-3	-	•	-	•	-	-	-	-	-	5	A-1-b (V)	-	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
COSEC			631.9	- 0 - - 7 -	9 12 10	30	39	SS-4	-	-	-	-	-	-	-	-	-	4	A-1-b (V)	-	1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7

PROJECT: CUY-490-0.00 TYPE: SUBGRADE PID: 107408 SFN: START: 7/21/21 END: 7/21/21	DRILLING FIRM / O SAMPLING FIRM / I DRILLING METHOD SAMPLING METHO	LOGGER:	NEAS / J. HO NEAS / J. HOI 3.25" HSA SPT		HAM CALI	BRATI	CME A ON DATE: ATIO (%):	12			ALIC ELE	TION . SNME VATIO / LON	NT: _)N: _		R/ 4 (MS	AMP (EOB:		B-043-	PAGE 1 OF 1
MATERIAL DESCRIPTION AND NOTES	V	ELEV. 641.4	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAE cs	ATIO FS	N (%) sı	CL	ATT LL	ERBE PL	RG PI	WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
8" CONCRETE AND 8" BASE (DRILLERS DESCRIPTION) DENSE, BROWN AND GRAY, GRAVEL WIT LITTLE SILT, TRACE CLAY, DAMP MEDIUM DENSE TO DENSE, BROWN, COAFINE SAND, LITTLE SILT, LITTLE GRAVEL, CLAY, DAMP TO MOIST	ARSE AND	640.1	- 1 - 2 - 3 - 4 - 5 - 6 - 7 - EOB	6 13 24 7 18 12 7 9 8 8 7	50 41 23 23	56 44 67 61	SS-1 SS-2 SS-3 SS-4		23 18 -	28 30 -	27 29 -	17 18 -		NP NP -		NP NP -	10 11 12 10	A-1-b (0) A-3a (0) A-3a (V) A-3a (V)	933	1

AND NOTES 670.6 Septimor Fill	匝.																					
PID: 107408 SFN: DRILLING METHOD: 3.25" HSA CALIBRATION DATE: 12/5/19 ELEVATION: 670.6 (MSL) EOB: 7.5 ft. DRILLING METHOD: SPT ENERGY RATIO (%): 81.7 LAT / LONG: 41.479059, -81.664584 1 OF 1 MATERIAL DESCRIPTION AND NOTES SAMPLING METHOD: SPT SA	(1)	_															_		-,			-
START:					-		GES_															DACE
MATERIAL DESCRIPTION AND NOTES SPT/ RQD No. REC SAMPLE HP GRADATION (%) ATTERBERG ODOT CLASS (GI) Ppm FILL	0-0	PID: <u>1074</u>	l <u>08 </u>	DRILLING METHOD):	3.25" HSA		CALI	BRATI	ON DATE:	12	2/5/19	9	ELE	VATIO	N: <u>67</u>	0.6 (N	<u> </u>	EOB:	7.5 ft.		
AND NOTES 670.6 DEPTHS RQD N ₆₀ (%) ID (tsf) GR CS FS SI CL LL PL PI WC CLASS (GI) PPM FILL	Y-49	START: 7	7/23/21 END: 7/23/21	SAMPLING METHO	D:	SPT		ENE	RGY R	ATIO (%):	;	81.7		LAT	/ LONG	3:	41	.4790	59, -81	.664584		1 OF 1
AND NOTES 670.6 RQD 60 (%) ID (tsf) GR CS FS SI CL LL PL PL PL WC CLASS (B) PPIN PLL 8.0" CONCRETE AND 7.5" BASE (DRILLERS DESCRIPTION) MEDIUM DENSE, GRAY AND BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, DAMP TO MOIST (FILL)	∃\CU			N	ELEV.	DEPTHS		N	REC	SAMPLE	HP				N (%)	Α		_				BACK
DESCRIPTION	M		AND NOTES		670.6	DEI IIIO	RQD	• •60	(%)	ID	(tsf)	GR	CS	FS	SI	CL LI	PL	PI	WC	CLASS (GI)	ppm	FILL
	TS\1ARCHIVE BY YEAR\2021 ARCHI	MEDIUM DI SAND, LITT	ION) ENSE, GRAY AND BROWN, GR	AVEL WITH		- 1 - 2 - 1 - 3 - 1 - 4 - 1 - 5 - 1 - 6 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	3 6 5	12	33	SS-2 SS-3		-	-	-	-		-	-	8	A-1-b (V) A-1-b (0)	1080	7

щ,																								
Ϋ́	PROJECT:	CUY-490	-0.00	DRILLING FIRM /	OPERATOR	R: NEAS / J.	HODGE	<u>s</u> [DRILL	RIG:	C	ME 45	В		STA	TION	/ OFI	FSET	ī:	16+5	50, 5' F	RT. EX		TION ID
ĕ	TYPE:	SUBGRAD	E	SAMPLING FIRM	/ LOGGER:	NEAS / J. I	HODGES	s H	HAMM	ER:	CME A	NOTU	1ATIC)	ALIC	SNME	NT:		R	AMP	C-B		B-045-	0-21
		7408 SFN:		DRILLING METHO	DD:	3.25" HSA	١		CALIBE	RATIO	ON DATE:	12	2/5/19	9	ELE'	VATIO	DN:	674.	0 (MS	SL)	EOB:	7.5 ft.		PAGE
۲-49	START:	7/23/21 END: _	7/23/21	SAMPLING METH	IOD:	SPT		E	ENERO	GY R	ATIO (%):		81.7		LAT	/ LON	IG: _		41.4	47896	64, - 81	.664220		1 OF 1
3		MATERIAL	DESCRIPTION	N	ELEV.	DEPTHS	SI	PT/	N ₆₀ F	REC	SAMPLE	HP	(GRAD	OITA	N (%)		ATT	ERBE	ERG		ODOT	SO4	BACK
₹		ANE	NOTES		674.0	DEFINS	R	QD	1460	(%)	ID	(tsf)	GR	CS	FS	SI	CL	LL	PL	PI	WC	CLASS (GI)	ppm	FILL
1 ARCH	8.0" CONO	CRETE AND 7.5" B. TION)	ASE (DRILLER	RS X	672.7	-	1 —																	
/EAR\202		DENSE, GRAY, GR ILT, TRACE CLAY, I			671.0	_	2 5	6 5	15	56	SS-1	-	54	20	14	9	3	NP	NP	NP	4	A-1-a (0)	340	17 × 17 × 17 × 17 × 17 × 17 × 17 × 17 ×
VE BY	SOME SIL	DENSE, BROWN, C LT, TRACE CLAY, T				E	4	4 4	11	39	SS-2	-	5	7	60	21	7	NP	NP	NP	14	A-3a (0)	-	7
1ARCHI	DAMP					<u>-</u>		5 5	14	44	SS-3	-	-	-	-	-	-	-	1	1	12	A-3a (V)	-	<177 177 177
OJECTS\					666.5	EOB-	6 7 - 6	5 4	12	72	SS-4		-	-	-	-	-	-	-	-	9	A-3a (V)	-	1777

TYPE: SUBGRADE PID: 107408 SFN:	DRILLING FIRM / OI SAMPLING FIRM / L DRILLING METHOD SAMPLING METHO	OGGER: _			HAM CALI	BRATI	CME A ON DATE: ATIO (%):	12			ALIC	TION SNME VATIO / LON	NT: DN: _		R 9 (M	AMP SL)	EOB:	7.5 ft.	B-046	ATION ID -0-21 PAGE 1 OF 1
MATERIAL DESCRIPTION ≩ AND NOTES		ELEV. 658.9	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	CS	ATIO FS	N (%) sı	CL	ATT LL	ERBI PL	PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
4" ASPHALT AND 6" CONCRETE AND 6" B/ (DRILLERS DESCRIPTION) MEDIUM DENSE TO DENSE, BROWN, GRA' SAND, LITTLE SILT, TRACE CLAY, DAMP HARD, GRAY, SILT, SOME CLAY, TRACE S/ TRACE GRAVEL, DAMP	VEL WITH	657.6 655.2 651.4	- 1 - 2 - 3 - 4 - 5 - 6 - 7	10 13 15 10 8 10 9 10 9	38 25 26 29	56 50 67 67		- 4.50 4.50 4.50	20 - 0	34 - 1	27 - 3	14 - 67 -	5 - 29 -	NP - 25 -	NP - 19 -	NP - 6	6 6 15 16	A-1-b (0) A-1-b (V) A-4b (8) A-4b (V) A-4b (V)	253	1

PROJECT: CUY-490-0.00 TYPE: SUBGRADE PID: 107408 SFN: START: 7/22/21 END: 7/22/21	DRILLING FIRM / OP SAMPLING FIRM / LO DRILLING METHOD: SAMPLING METHOD	OGGER: _	NEAS / J. HO NEAS / J. HOI 3.25" HSA SPT		HAM CALI			12			ALIC ELE	TION / SNMEN VATIO / LON	NT: N: _6	19.5 (RAM MSL)	P S-E _ EO		_ 	B-047-0	TION ID 0-21 PAGE 1 OF 1
MATERIAL DESCRIPTION ∃ AND NOTES		ELEV. 649.5	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAD CS	ATIO FS	N (%)	CL I		RBERG		1 01 4	OOT SS (GI)	SO4 ppm	BACK FILL
4" ASPHALT AND 8" CONCRETE AND 6" BY (DRILLERS DESCRIPTION) MEDIUM DENSE, BROWN, COARSE AND FILITILE TO SOME SILT, TRACE CLAY, TRACE MOIST	INE SAND, CE GRAVEL,	648.0	- 1 - 2 - 3 3 5 6 - 7 - 7 7 7 7 7 7 7 7 7 7 7 7 7	6 9 10 5 6 8 4 6 5	26 19 15	56 67 56	SS-1 SS-2 SS-3 SS-4	-	8 6 -	23	51 46 -	13 21 -	5 N 10 N		IP NIIP NI	2 1	1 A-3	a (0) a (0) a (V) a (V)	67 - -	X

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVELED SOIL CUTTINGS

PROJ TYPE PID:	107408	CUY-490 SUBGRAD SFN: 21 END:		DRILLING FIR SAMPLING FII DRILLING ME SAMPLING ME	RM / L	_OGGER: _):				HAMI CALII		CME A ON DATE: ATIO (%):	12			ALIG	TION SNME VATIO	NT: _ DN: _		- R 4 (MS	AMP SL)	EOB:	· · ·	B-048-0	TION ID 0-21 PAGE 1 OF 1
		MATERIAL ANI	V		ELEV. 640.4	DEPT		SPT/ RQD	N ₆₀	_	SAMPLE ID	HP (tsf)		GRAD cs				ATT LL	ERBE PL	_	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
DES	CRIPTION)		SE (DRILLERS			639.1		_ 1 _																	- 5 LN 3
	GMENTS W		GRAVEL AND S LITTLE SILT, TF			637.4		- 2 - - 3 -	14 12 10	30	56	SS-1	-	35	22	28	12	3	NP	NP	NP	9	A-1-b (0)	2387	1> \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
			COARSE AND F L, TRACE CLAY			635.9		_ 4 -	7 7 8	20	67	SS-2	-	14	17	40	23	6	NP	NP	NP	10	A-3a (0)	-	1 × 1 × 1
		E, GRAY, GR RACE CLAY,	MOIST	AND,		634.4		- 5 - - 6 -	5 6 9	20	61	SS-3	-	-	-	-	-	-	-	-	-	12	A-1-b (V)	-	1 / / / / / / / / / / / / / / / / / / /
			COARSE AND F L, TRACE CLAY			632.9	– EOB –	- 7 - 7	5 4 5	12	56	SS-4	-	-	-	-	-	-	-	-	-	10	A-3a (V)	-	1 / / / / / / / / / / / / / / / / / / /

ři —	CT:CUY-490-0.00 SUBGRADE 107408 SFN: 7/23/21 END:7/23/21	DRILLING FIRM / C SAMPLING FIRM / DRILLING METHO SAMPLING METHO	LOGGER: _ D:	NEAS / J. HO NEAS / J. HO 3.25" HSA SPT		HAM CALI			1		9	ALIGN ELEV	ON / O MENT: ATION: ONG:		R .2 (MS	AMP SL)	EOB:		B-049-	TION ID -0-21 PAGE 1 OF 1
	MATERIAL DESCRIPTIO AND NOTES	N	ELEV. 643.2	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR		ATION FS S	(%) SI CL	ATT	ERBE PL	ERG PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
LOOSE FINE SA	ONCRETE AND 7.5" BASE (DRILLEI RIPTION) E TO MEDIUM DENSE, BROWN, CO AND, LITTLE TO SOME SILT, TRAC E GRAVEL, WET	ARSE AND	641.9	- 1 - 2 - 3 - 4	4 6 5 3 4 3 4 3	15	67	SS-1 SS-2	-	0			4 2 6 2	NP NP	NP NP	NP NP	23	A-3a (0) A-3a (0)	20	X
@6.0';	SS-4 CONTAINS A 2.0" CONCRETE	FRAGMENT	635.7	- 6 - 7	3 3 3 4	10	78	SS-3 SS-4	-	-	-	-		-	-	-	27	A-3a (V) A-3a (V)	-	- 1

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVELED SOIL CUTTINGS

TYPE: <u>SU</u> PID: <u>107408</u> SFN	JY-490-0.00 BGRADE : END: 7/23/21	DRILLING FIRM / C SAMPLING FIRM / DRILLING METHO SAMPLING METHO	LOGGER: _ D:	NEAS / J. H NEAS / J. H 3.25" HSA SPT		HAM CALI			1		; 9	ALIG ELE\	NMEN	N: 64	0.2 (M	RAMP ISL)	EOB:	T. EX 7.5 ft.	PLORA B-050-	TION ID 0-21 PAGE 1 OF 1
MA`	TERIAL DESCRIPTION AND NOTES	N	ELEV. 640.2	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAD CS	ATIOI FS		A.	TERB	_	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
8.0" CONCRETE AND DESCRIPTION) MEDIUM DENSE, BROFFRAGMENTS WITH S CONTAINS SLAG, WE (FILL)	OWN, GRAVEL AND : AND , LITTLE SILT, TR	STONE	638.9	- 2	7 2 - 7 9 3 - 8 4 - 7 11	29 25	56 56	SS-1 SS-2	-	45 -	19	23	12	1 N	P NP	NP -	16 14	A-1-b (0) A-1-b (V)	1100	17 × 17 × 17 × 17 × 17 × 17 × 17 × 17 ×
MEDIUM DENSE TO I GRAVEL WITH SAND CONTAINS SLAG, WE (FILL)	, LITTLÉ SILT, TRACE		632.7	- ! - ! - ! - :	5 12 14 5 10 7 11 10	33	39 44	SS-3 SS-4	-	40 -	28	20	11	1 N	NP	NP -	45 41	A-1-b (0) A-1-b (V)	-	- 1

PROJECT:	DRILLING FIRM / OPE SAMPLING FIRM / LO DRILLING METHOD: SAMPLING METHOD:	GGER: _	NEAS / J. HODO NEAS / J. HODO 3.25" HSA SPT		HAM CALI	BRATI	CME A ON DATE: ATIO (%):	12			ALIG	TION / INMEN /ATIO / LON(IT: N: _6	- 86.2 (I	RAMF (ISL)	EOB:		B-051-	O-21 PAGE 1 OF 1
MATERIAL DESCRIPTION → AND NOTES		ELEV. 636.2	DEPTHS	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAD CS	ATIO FS	N (%)	A CL L	TTER L PI	BERG . PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
10.0" CONCRETE AND 7.0" BASE (DRILLEF DESCRIPTION) DENSE, BROWN AND GRAY, STONE FRAG WITH SAND, TRACE SILT, TRACE CLAY, DA (FILL) MEDIUM DENSE TO DENSE, BROWN, SANI TRACE CLAY, TRACE GRAVEL, DAMP TO N DENSE, BROWN, SILT, LITTLE SAND, TRACE GRAVEL, MOIST	MENTS AMP DY SILT, MOIST	634.8 633.2 629.2 628.7	- 4 - - 5 -	12 16 10 10 7 9 11 8 10 13 15	39 23 26 38	50 72 56 78	SS-1 SS-2 SS-3 SS-4A SS-4B		37 5 -	20 9 -	26 49 - -	14 30 - -	3 N 7 N				A-1-b (0) A-4a (0) A-4a (V) A-4a (V) A-4b (V)	3000	1

PROJECT: CUY-490-0.00 TYPE: SUBGRADE PID: 107408 SFN: START: 7/23/21 END: 7/23/21	DRILLING FIRM / OPER SAMPLING FIRM / LOG DRILLING METHOD: _ SAMPLING METHOD: _		NEAS / J. HODG NEAS / J. HODG 3.25" HSA SPT		HAMI			12			ALIC ELE	TION SNME VATIO	NT: _)N: _		R/ 4 (MS	AMP SL)	EOB:		PLORA B-052-	TION ID 0-21 PAGE 1 OF 1
MATERIAL DESCRIPTION AND NOTES	-	LEV. 43.4	LIEDIAS I	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GR	GRAD CS	FS FS	N (%)	CL	ATT LL	ERBE PL	RG PI	wc	ODOT CLASS (GI)	SO4 ppm	BACK FILL
4" ASPHALT AND 8" CONCRETE AND 6" E (DRILLERS DESCRIPTION) MEDIUM DENSE TO DENSE, BROWN, COAFINE SAND, TRACE TO LITTLE SILT, TRACE TRACE GRAVEL, DAMP TO MOIST	ARSE AND E CLAY,	41.9	- 1 - 7 - 1 - 7 - 7 - 1 - 7 - 7 - 1 - 7 - 7	7 11 12 3 10 9 5 6 6 6 4 4	31 26 16	50 44 44 56	SS-1 SS-2 SS-3 SS-4		0 1 -	13 21 -	75 61 -	9 12 -		NP NP -		NP NP -	6 13 7	A-3a (0) A-3a (0) A-3a (V) A-3a (V)	40 - -	X

-0.00\GIN	PROJECT:	CUY-490-0.00 SUBGRADE	DRILLING FIRM / C SAMPLING FIRM /	LOGGER: _	NEAS / J. H		HAM	L RIG: MER:	CME A		/ATIC	<u>; </u>	STA	SNME	NT:		R	AMP			B-053	-
4 9 9	PID: <u>107408</u> START: 7/23/2	SFN: 1 END: 7/23/21	DRILLING METHOR SAMPLING METHOR		3.25" HSA SPT		_		ON DATE: ATIO (%):		<u>2/5/19</u> 81.7	9	ELE'		_	657.			EOB:	7.5 ft.		PAGE 1 OF 1
IIVE/CUY	31AR1	MATERIAL DESCRIPTION AND NOTES		ELEV. 657.0	DEPTHS	SPT/ RQD	N ₆₀		SAMPLE ID	_	_	GRAD cs		_	_	ATT	ERBE	_	WC	ODOT CLASS (GI)	SO4 ppm	
ZI ARUL	4" ASPHALT AN (DRILLERS DES	ID 8" CONCRETE AND 6" E	BASE	655.5	- - 1	_		(70)		(10.)												***
TEARIZO	CLAY, TRACE TO	HARD, BROWN, SANDY S O LITTLE GRAVEL, CONTA NTS, SS-2 CONTAINS NO	INS TRACE		_ 2	10 6	22	50	SS-1	4.50	14	18	30	25	13	22	15	7	12	A-4a (1)	347	12 7
IIVE DY	FOR HP READIN (FILL)			652.5	- 3 - 4	10 8 7	20	56	SS-2	-	6	20	33	27	14	19	14	5	10	A-4a (1)	-	
DI ARCI	LITTLE TO SOM	ROWN, COARSE AND FIN E SILT, TRACE TO LITTLE ONTAINS TRACE IRON ST.	GRAVEĹ,		<u> </u>	16 18 21	53	72	SS-3	-	-	-	-	-	-	-	-	-	8	A-3a (V)	-	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
(O)ECI	DAMP	ONTAINS TRACE INON ST	00000000000000000000000000000000000000	649.5	FOB - 7	17 21 20	56	78	SS-4	-	-	-	-	-	-	-	-	-	8	A-3a (V)	-	1 / / / / / / / / / / / / / / / / / / /

APPENDIX B SULFATE TEST DATA REPORT



OHIO DEPARTMENT OF TRANSPORTATION DETERMINING SULFATE CONTENT IN SOILS SUPPLEMENT 1122

Project C-R-S:	CUY-490-0.00	
PID No:	107408	
Report Date:	9/21/2021	
Consultant:	NEAS Inc.	
Technician:	L. Rosenbeck	

								Re	olicate Sar	nple Readi	ngs		Sulfate
Boring ID & Sample	Station	Offset	Latitude & Long	•	Elevation	Soaking		1		2		3	Content
#			Plane Coo	ordinates		Time (hr)	Dilution	Reading	Dilution	Reading	Dilution	Reading	(ppm)
B-001-0-21 SS-1			41.474243	-81.694868	632.9	17.7	20	76	20	68	20	71	1433
B-002-0-21 SS-1			41.474030	-81.693671	632.1	18.8	20	15	20	7	20	12	227
B-003-0-21 SS-1A			41.474375	-81.692283	631.5	18.4	20	34	20	31	20	32	647
B-004-0-21 SS-1			41.474338	-81.690864	635.9	18.8	20	34	20	33	20	37	693
B-005-0-21 SS-1			41.474886	-81.689604	635.3	18.4	20	26	20	26	20	21	487
B-006-0-21 SS-1			41.474904	-81.688112	632.7	18.4	40	30	40	30	40	29	1187
B-007-0-21 SS-1			41.475610	-81.686998	628	17.7	20	10	20	9	20	10	193
B-008-0-21 SS-1			41.475534	-81.685547	617	17.3	40	32	40	30	40	34	1280
B-009-0-21 SS-1			41.476061	-81.684277	613.6	18.8	20	15	20	17	20	15	313
B-010-0-21 SS-1			41.475901	-81.682845	616.8	17.3	20	27	20	28	20	28	553
B-011-0-21 SS-1			41.476390	-81.681670	622.9	18.8	40	47	40	53	40	59	2120
B-012-0-21 SS-1			41.476182	-81.680543	631.9	18.4	20	37	20	35	20	38	733
B-013-0-21 SS-1			41.476780	-81.679520	635.5	18.8	20	44	20	50	20	41	900
B-014-0-21 SS-1			41.476752	-81.678275	648.4	17.4	40	55	40	53	40	52	2133
B-015-0-21 SS-1			41.479772	-81.666011	647.3	17.4	100	25	100	19	100	27	2367
B-016-0-21 SS-1			41.480032	-81.664827	640.3	16.9	20	50	20	48	20	48	973
B-017-0-21 SS-1			41.479807	-81.663473	629.8	17.2	20	0	20	0	20	0	0
B-018-0-21 SS-1			41.479983	-81.662227	624.6	17.7	20	30	20	31	20	33	627

B-019-0-21 SS-1	41.479708	-81.660794	624.2	17.2	20	48	20	39	20	36	820
B-020-0-21 SS-1	41.479881	-81.659372	631.2	17.8	40	66	40	66	40	63	2600
B-021-0-21 SS-1	41.479571	-81.657699	641.1	16.9	40	33	40	38	40	34	1400
B-022-0-21 SS-1	41.475375	-81.688184	632.1	17.4	20	19	20	22	20	19	400
B-023-0-21 SS-1	41.475127	-81.689447	638.5	17.4	40	39	40	37	40	42	1573
B-024-0-21 SS-1	41.474960	-81.690732	652.7	17.4	20	7	20	6	20	7	133
B-025-0-21 SS-1	41.474695	-81.691991	667.3	17.9	20	30	20	29	20	25	560
B-026-0-21 SS-1	41.473661	-81.693337	677.8	17.8	20	4	20	3	20	4	73
B-027-0-21 SS-1	41.472695	-81.693585	674.5	17.9	20	13	20	12	20	11	240
B-028-0-21 SS-1	41.471613	-81.693416	669.4	18.0	20	5	20	5	20	4	93
B-029-0-21 SS-1	41.475721	-81.679351	643.8	17.9	20	15	20	15	20	15	300
B-030-0-21 SS-1	41.475167	-81.679382	624.2	17.9	20	45	20	41	20	45	873
B-031-0-21 SS-1	41.474849	-81.680357	623.3	18.2	20	5	20	5	20	5	100
B-032-0-21 SS-1	41.475534	-81.681133	621.4	16.9	20	47	20	46	20	51	960
B-033-0-21 SS-1	41.477226	-81.679002	656.6	16.8	20	33	20	39	20	38	733
B-034-0-21 SS-1	41.476953	-81.679724	663.4	17.1	20	65	20	72	20	75	1413
B-035-0-21 SS-1	41.480347	-81.667621	667.4	17.4	20	8	20	7	20	8	153
B-036-0-21 SS-1	41.479942	-81.668381	665.1	16.9	20	18	20	18	20	19	367
B-037-0-21 SS-1	41.480121	-81.666407	651.4	18.0	20	44	20	41	20	44	860
B-038-0-21 SS-1	41.480298	-81.665064	649.1	18.0	20	17	20	17	20	17	340
B-039-0-21 SS-1	41.480570	-81.663858	657.9	16.9	20	40	20	39	20	40	793
B-040-0-21 SS-1	41.481275	-81.663067	669.4	17.0	20	24	20	19	20	19	413
B-041-0-21 SS-1	41.479716	-81.665074	640.6	17.1	100	23	100	33	100	28	2800
B-042-0-21 SS-1	41.479505	-81.663858	639.4	16.9	20	67	20	67	20	61	1300
B-043-0-21 SS-1	41.479481	-81.662745	641.4	18.0	20	48	20	44	20	48	933
B-044-0-21 SS-1	41.479059	-81.664584	670.6	16.8	20	52	20	52	20	58	1080
B-045-0-21 SS-1	41.478964	-81.664220	674	17.3	20	18	20	16	20	17	340
B-046-0-21 SS-1	41.477904	-81.660282	658.9	16.8	20	13	20	13	20	12	253
B-047-0-21 SS-1	41.478742	-81.659701	649.5	16.9	20	4	20	3	20	3	67
B-048-0-21 SS-1	41.479209	-81.658594	640.4	16.8	40	61	40	58	40	60	2387
B-049-0-21 SS-1	41.479298	-81.657315	643.2	18.2	20	1	20	1	20	1	20
B-050-0-21 SS-1	41.480037	-81.657981	640.2	17.9	20	56	20	53	20	56	1100
B-051-0-21 SS-1	41.480218	-81.659276	636.2	17.9	100	30	100	28	100	32	3000

B-052-0-21 SS-1	41.480654	-81.660386	643.4	18.1	20	2	20	2	20	2	40
B-053-0-21 SS-1	41.481367	-81.661138	657	17.9	20	18	20	17	20	17	347
полити											0

APPENDIX D

GEOTECHNICAL BULLETIN 1 (GB1) ANALYSIS SPREADSHEETS

ENTIRE PROJECT



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By:

Derar M. Tarawneh

Date prepared: Wednesday, August 30, 2023

Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

brendan.andrews@neasinc.com

NO. OF BORINGS:

57



#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-109-0-20	IR-90	930+69	5	RT	S&ME TRK 55 (R52)	90	656.0	654.4	1.6 C
2	B-110-0-20	IR-90	931+91	38	LT	S&ME TRK 55 (R52)	90	648.1	645.9	2.2 C
3	B-111-0-20	IR-90	935+97	5	RT	S&ME TRK 55 (R52)	90	639.8	638.3	1.5 C
4	B-112-0-20	IR-90	937+90	5	LT	S&ME TRK 55 (R52)	90	635.8	634.5	1.3 C
5	B-001-0-21	IR-490	939+11	39	LT	CME 45B	82	632.9	632.0	0.9 C
6	B-002-0-21	IR-490	942+36	47	RT	CME 45B	82	632.1	628.6	3.5 C
7	B-003-0-21	IR-490	946+27	40	LT	CME 45B	82	631.5	631.1	0.4 C
8	B-004-0-21	IR-490	950+05	51	RT	CME 45B	82	635.9	633.4	2.5 C
9	B-005-0-21	IR-490	953+92	41	LT	CME 45B	82	635.3	634.5	0.8 C
10	B-006-0-21	IR-490	957+83	78	RT	CME 45B	82	632.7	631.9	0.8 C
11	B-007-0-21	IR-490	961+53	73	LT	CME 45B	82	628.0	626.3	1.7 C
12	B-008-0-21	IR-490	965+28	63	RT	CME 45B	82	617.0	617.2	0.2 F
13	B-009-0-21	IR-490	969+07	61	LT	CME 45B	82	613.6	613.0	0.6 C
14	B-010-0-21	IR-490	972+85	62	RT	CME 45B	82	616.8	614.0	2.9 C
15	B-011-0-21	IR-490	976+32	61	LT	CME 45B	82	622.9	623.1	0.3 F
16	B-012-0-21	IR-490	979+20	72	RT	CME 45B	82	631.9	628.5	3.4 C
17	B-013-0-21	IR-490	982+49	63	LT	CME 45B	82	635.5	637.0	1.5 F
18	B-014-0-21	IR-490	985+62	74	RT	CME 45B	82	648.4	645.5	2.9 C
19	B-015-0-21	IR-490	1021+43	40	RT	CME 45B	82	647.3	649.4	2.2 F
20	B-016-0-21	IR-490	1025+70	40	LT	CME 45B	82	640.3	638.7	1.7 C
21	B-017-0-21	IR-490	1029+41	39	RT	CME 45B	82	629.8	628.7	1.0 C
22	B-018-0-21	IR-490	1032+80	42	LT	CME 45B	82	624.6	622.7	1.9 C
23	B-019-0-21	IR-490	1036+77	37	RT	CME 45B	82	624.2	622.4	1.8 C
24	B-020-0-21	IR-490	1040+62	48	LT	CME 45B	82	631.2	629.9	1.3 C
25	B-021-0-21	IR-490	1045+27	40	RT	CME 45B	82	641.1	642.4	1.2 F
26	B-022-0-21	IR-490	3058+12	5	LT	CME 45B	82	632.1	632.0	0.1 C
27	B-023-0-21	LANE E-S	3054+54	6	LT	CME 45B	82	638.5	638.1	0.4 C
28	B-024-0-21	LANE E-S	3050+96	5	LT	CME 45B	82	652.7	651.6	1.0 C
29	B-025-0-21	LANE E-S	3047+38	2	LT	CME 45B	82	667.3	666.2	1.1 C
30	B-026-0-21	LANE E-S	3041+89	27	RT	CME 45B	82	677.8	678.7	0.9 F
31	B-027-0-21	LANE E-S	3038+16	27	RT	CME 45B	82	674.5	674.7	0.2 F
32	B-028-0-21	LANE E-S	3034+13	26	RT	CME 45B	82	669.4	667.9	1.5 C
33	B-029-0-21	Ramp 7-7C	67+99	145	RT	CME 45B	82	643.8	642.3	1.5 C
34	B-030-0-21	Ramp 7-7C	68+99	19	RT	CME 45B	82	624.2	622.7	1.6 C
35	B-031-0-21	Ramp 7-7C	72+21	23	RT	CME 45B	82	623.8	622.5	1.2 C
36	B-032-0-21	Ramp 7-7C	76+12	11	RT	CME 45B	82	622.0	622.0	0.0 C
37	B-033-0-21	Ramp C-7	84+46	21	LT	CME 45B	82	656.6	655.5	1.1 C
38	B-034-0-21	Ramp C-7	82+28	16	RT	CME 45B	82	663.4	662.4	1.0 C
39	B-035-0-21	Ramp B-C	17+69	31	LT	CME 45B	82	667.4	666.1	1.3 C
40	B-036-0-21	Ramp B-C	15+10	2	LT	CME 45B	82	665.1	663.9	1.2 C
41	B-037-0-21	Ramp N-W	120+53	8	LT	CME 45B	82	651.4	650.3	1.0 C
42	B-038-0-21	Ramp N-W	124+26	1	LT	CME 45B	82	649.1	647.5	1.6 C
43	B-039-0-21	Ramp N-W	127+74	4	LT	CME 45B	82	657.9	657.0	0.9 C
44	B-040-0-21	Ramp N-W	131+20	7	LT	CME 45B	82	669.4	668.7	0.7 C
45	B-041-0-21	Ramp W-N	623+88	12	LT	CME 45B	82	640.6	638.4	2.2 C



#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
46	B-042-0-21	Ramp W-N	627+30	0	RT	CME 45B	82	639.4	638.8	0.6 C
47	B-043-0-21	Ramp W-N	630+38	4	LT	CME 45B	82	641.4	640.5	0.9 C
48	B-044-0-21	Ramp C-B	15+45	1	RT	CME 45B	82	670.6	669.9	0.8 C
49	B-045-0-21	Ramp C-B	16+50	5	RT	CME 45B	82	674.0	673.3	0.7 C
50	B-046-0-21	Ramp S-E	335+69	7	RT	CME 45B	82	658.9	657.3	1.6 C
51	B-047-0-21	Ramp S-E	339+21	4	RT	CME 45B	82	649.5	647.9	1.5 C
52	B-048-0-21	Ramp S-E	342+76	3	RT	CME 45B	82	640.4	637.7	2.8 C
53	B-049-0-21	Ramp S-E	346+29	6	RT	CME 45B	82	643.2	643.5	0.3 F
54	B-050-0-21	Ramp E-N	744+41	4	LT	CME 45B	82	640.2	638.8	1.4 C
55	B-051-0-21	Ramp E-N	740+80	2	RT	CME 45B	82	636.2	634.3	1.8 C
56	B-052-0-21	Ramp E-N	737+33	4	LT	CME 45B	82	643.4	642.6	0.8 C
57	B-053-0-21	Ramp E-N	733+99	4	LT	CME 45B	82	657.0	655.9	1.1 C



			Sam	nle	Subg	rade	Stan	dard															Excavate ar	d Renlace	
#	Boring	Sample	De	•	De			ration	НР		Pl	nysica	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate	Proble	m	(Item	•	Recommendation
#			From		From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	Mc	M _{OPT}	Class	GI	Content (ppm)	Unsuitable	Unstable	Unsuitable	Unstable	(Enter depth in inches)
1	В	SS-1	1.5	3.0	-0.1	1.4	50						38	8	46	21	10	A-4a	8	443		Mc			
	109-0	SS-2	3.0	4.5	1.4	2.9	35						35	3	38	21	10	A-4a	5			Mc			
	20	SS-3	4.5	6.0	2.9	4.4	29									20	10	A-4a	8						
		SS-4	6.0	7.5	4.4	5.9	33	29								20	10	A-4a	8						
2	В	SS-1	1.5	3.0	-0.7	0.8	27						13	3	16	7	8	A-3a	0	174					
	110-0	SS-2	3.0	4.5	0.8	2.3	80									9	8	A-3a	0						
	20	SS-3	4.5	6.0	2.3	3.8	54						44	6	50	17	10	A-4a	8						
		SS-4	6.0	7.5	3.8	5.3	41	27								19	10	A-4a	8						
3	В	SS-1	1.5	3.0	0.0	1.5	50						12	5	17	11	8	A-3a	0	248					
	111-0	SS-2	3.0	4.5	1.5	3.0	50						3	1	4	6	6	A-1-a	0						
	20	SS-3	4.5	6.0	3.0	4.5	18			25	17	8	60	34	94	20	12	A-4b	8						
		SS-4	6.0	7.5	4.5	6.0	23	18								20	10	A-4b	8						
4	В	SS-1	1.5	1.9	0.2	0.6	50						5	2	7	16	6	A-1-a	0	197					
	112-0	SS-2	3.0	3.4	1.7	2.1	50						8	3	11	17	6	A-1-a	0						
	20	SS-3	4.5	4.9	3.2	3.6	50									21	6	A-1-a	0						
		SS-4	6.0	6.5	4.7	5.2	50	30								15	6	A-1-a	0						
5	В	SS-1	1.5	3.0	0.6	2.1	37						15	3	18	11	8	A-3a	0	1433					
	001-0	SS-2	3.0	4.5	2.1	3.6	30									9	8	A-3a	0						
	21	SS-3	4.5	6.0	3.6	5.1	30						12	3	15	12	6	A-1-b	0						
		SS-4	6.0	7.5	5.1	6.6	27	27								12	8	A-3a							
6	В	SS-1	1.5	3.0	-2.0	-0.5	23						13	5	18	9	6	A-1-b	0	227					
	002-0	SS-2	3.0	4.5	-0.5	1.0	19									11	6	A-1-b	0						
	21	SS-3A	4.5	5.5	1.0	2.0	31	1								9	6	A-1-b	0						
		SS-3B	5.5	6.0	2.0	2.5	31	19	4.5	27	18	9	65	28	93	13	13	A-4b	8		A-4b		30"		
7	В	SS-1A	1.5	2.2	1.1	1.8	42						21	6	27	7	8	A-3a	0	647					
	003-0	SS-1B	2.2	3.0	1.8	2.6	42			22	18	4	71	16	87	13	13	A-4b	8		A-4b				
	21	SS-2	3.0	4.5	2.6	4.1	34			24	20	4	44	11	55	10	15	A-4a	4						
	}	SS-3	4.5	6.0	4.1	5.6	33	30								14	10	A-4b	8						
8	В	SS-1	1.5	3.0	-1.0	0.5	27						22	5	27	8	10	A-2-4	0	693					
	004-0	SS-2A	3.0	4.0	0.5	1.5	29									8	10	A-2-4	0				·		
	21	SS-2B	4.0	4.5	1.5	2.0	29		4.5							14	10	A-4b	8		A-4b	Мс			
		SS-3	4.5	6.0	2.0	3.5	26	26	4.5	25	19	6	65	29	94	15	14	A-4b	8		A-4b	.,,,0	42''		
9	В	SS-1	1.5		0.7	2.2	35						16	5	21	6	6	A-1-b	0	487					
	005-0	SS-2	3.0	4.5	2.2	3.7	31						22	6	28	7	8	A-3a	0						
	21	SS-3	4.5	6.0	3.7	5.2	34									10	8	A-3a	0						
		SS-4	6.0	7.5	5.2	6.7	18	18	4.25							16	10	A-4b				<u> </u>			



#	Boring	Sample	Sam De _l	•	1 -	rade pth		dard ration	НР		Pl	hysica	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate ar	•	Recommendation (Enter depth in
п			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
10	В	SS-1	1.5	3.0	0.7	2.2	15						9	2	11	21	6	A-1-a	0	1187					
	006-0	SS-2	3.0	4.5	2.2	3.7	15		3	23	16	7	47	24	71	17	11	A-4a	7						
	21	SS-3	4.5	6.0	3.7	5.2	16		4.25							21	10	A-4a	8						
		SS-4	6.0	7.5	5.2	6.7	19	15	4.25							21	10	A-4a							
11	В	SS-1	1.5	3.0	-0.2	1.3	29						16	2	18	7	8	A-3a	0	193					
	007-0	SS-2	3.0	4.5	1.3	2.8	19									9	8	A-3a	0						
	21	SS-3	4.5	6.0	2.8	4.3	15						17	3	20	11	8	A-3a	0						
,		SS-4	6.0	7.5	4.3	5.8	16	15								9	8	A-3a	0						
12	В	SS-1	1.5	3.0	1.7	3.2	26						28	10	38	9	10	A-4a	5	1280					
	008-0	SS-2	3.0	4.5	3.2	4.7	16		4.5							11	10	A-4a	8						
	21	SS-3	4.5	6.0	4.7	6.2	30		4.5	24	17	7	46	18	64	12	12	A-4a	6						
,		SS-4	6.0	7.5	6.2	7.7	35	16	4.5							14	10	A-4a							
13	В	SS-1	1.5	3.0	0.9	2.4	29		4.5	21	16	5	32	12	44	10	11	A-4a	2	313					
	009-0	SS-2	3.0	4.5	2.4	3.9	23		4.5	27	18	9	36	17	53	15	13	A-4a	4						
	21	SS-3	4.5	6.0	3.9	5.4	23		4.5							14	10	A-4a	8						
		SS-4	6.0	7.5	5.4	6.9	25	23	4.5							13	10	A-4a							
14	В	SS-1	1.5	3.0	-1.4	0.1	27						23	10	33	12	10	A-2-4	0	553					
	010-0	SS-2	3.0	4.5	0.1	1.6	37									11	10	A-2-4	0						
	21	SS-3	4.5	6.0	1.6	3.1	34						26	9	35	12	10	A-2-4	0						
		SS-4	6.0	7.5	3.1	4.6	29	27								11	10	A-2-4	0						
15	В	SS-1	1.5	3.0	1.8	3.3	41						10	2	12	18	6	A-1-b	0	2120					
	011-0	SS-2A	3.0	4.0	3.3	4.3	18									15	6	A-1-b	0						
	21	SS-2B	4.0	4.5	4.3	4.8	18		4.5	27	21	6	58	21	79	19	16	A-4b	8						
		SS-3	4.5	6.0	4.8	6.3	16	16								21	6	A-1-b	0						
16	В	SS-1	1.5	3.0	-1.9	-0.4	37						78	16	94	14	10	A-4b	8	733					
	012-0	SS-2	3.0	4.5	-0.4	1.1	29						74	12	86	15	10	A-4b	8		A-4b	Мс			
	21	SS-3	4.5	6.0	1.1	2.6	29									15	10	A-4b	8		A-4b	Mc	31"		
		SS-4	6.0	7.5	2.6	4.1	31	29								14	10	A-4b	8						
17	В	SS-1	1.5	3.0	3.0	4.5	23		3.75				50	6	56	17	10	A-4b	8	900					
	013-0	SS-2	3.0	4.5	4.5	6.0	19		4.5				83	9	92	22	10	A-4b	8						
	21	SS-3	4.5	6.0	6.0	7.5	23		3							19	10	A-4b							
		SS-4	6.0	7.5	7.5	9.0	27	19	4.5							16	10	A-4b							
18	В	SS-1	1.5	3.0	-1.4	0.1	29						19	5	24	7	8	A-3a	0	2133					
	014-0	SS-2	3.0	4.5	0.1	1.6	25						12	2	14	5	8	A-3a	0						
	21	SS-3	4.5	6.0	1.6	3.1	16									8	8	A-3a	0						
		SS-4	6.0	7.5	3.1	4.6	14	14								7	8	A-3a	0						



1	Во	oring	Sample	Sam De _l	•	Subg De	rade pth		ndard tration	НР		P	hysic	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate	Proble	m	Excavate ar		Recommendation (Enter depth in
				From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable	inches)
)	В	SS-1	1.5	3.0	3.7	5.2	29						21	7	28	9	8	A-3a	0	2367					
Note	0	015-0	SS-2	3.0	4.5	5.2	6.7	29									7	8	A-3a							
20		21	SS-3A	4.5	5.0	6.7	7.2	12									19	8	A-3a							
1			SS-3B	5.0	6.0	7.2	8.2	12	29					10	2	12	8	8	A-3a							
Section Sect)	В	SS-1	1.5	3.0	-0.2	1.3	25						11	3	14	10	8	A-3a	0	973					
SS-4 60 7.5 4.3 5.8 5.0 2.0	0	016-0	SS-2	3.0	4.5	1.3	2.8	25									5	8	A-3	0						
1		21	SS-3	4.5	6.0	2.8	4.3	23						8	2	10	5	8	A-3	0						
11-0 11-0		Ī	SS-4	6.0	7.5	4.3	5.8	20	20								4	8	A-3	0						
1	L	В	SS-1	1.5	3.0	0.5	2.0	26						25	5	30	9	8	A-3a	0	0					
Section Sect	0	017-0	SS-2	3.0	4.5	2.0	3.5	20						24	7	31	12	8	A-3a	0						
Section Sect		21	SS-3	4.5	6.0	3.5	5.0	27									9	8	A-3a	0						
Name			SS-4				6.5	30	20	4.5							18	10	A-4b	8						
1	2	В	SS-1	1.5	3.0	-0.4	1.1	30						44	4	48	14	10	A-4a	8	627		Mc			
SS-4	0	018-0	SS-2	3.0	4.5	1.1	2.6	31						80	9	89	20	10	A-4b	8		A-4b	Мс			
SS-4 6.0 7.5 4.1 5.6 18 18 18 19 10 10 10 10 10 10 10		21	SS-3	4.5	6.0	2.6	4.1	18									21	10	A-4b	8						
11 12 13 14 15 15 15 15 15 15 15		Ì	SS-4	6.0	7.5		5.6	18	18								26	10	A-4b	8						
21 SS-3 4.5 6.0 7.5 4.2 7.7	3	В	SS-1	1.5	3.0	-0.3	1.2	31						44	6	50	16	10	A-4a	8	820		Mc			
SS-4 6.0 7.5 4.2 5.7 27 22 8 8 8 10 10 10 10 10 10 10 10 10 10 10 10 10	0	019-0	SS-2	3.0	4.5	1.2	2.7	27									19	10	A-4a	8			Мс			
SS-4 6.0 7.5 4.2 5.7 2.7 2.2 2.1 3.1		21	SS-3	4.5	6.0	2.7	4.2	22						44	7	51	20	10	A-4a	8						
0200		ŀ		_				27	22								_		!	8						
21	1	В	SS-1A	1.5	2.5	0.2	1.2	33						21	4	25	13	6	A-1-b	0	2600					
SS-28 SS-2	0	020-0	SS-1B	2.5	3.0	1.2	1.7	33									14	10	A-4b	8		A-4b	Mc			
SS-28 SS-1 1.5 3.0 2.7 4.2 2.5 2.7 3.7 3.7 3.7 3.7 3.7 3.7 3.7 3.8 3		21	SS-2A	3.0	3.5	1.7	2.2	27						73	12	85	19	10	A-4b	8		A-4b	Mc	26''		
021-0								27	27									1		0						
21 SS-3 4.5 6.0 5.7 7.2 25 25 2	5	В	SS-1	1.5	3.0	2.7	4.2	25						20	5	25	10	10	A-2-4	0	1400					
SS-4 6.0 7.5 7.2 8.7 35 25	0	021-0	SS-2	3.0	4.5	4.2	5.7	37									15	10	A-2-4	0						
SS-4 6.0 7.5 7.2 8.7 35 25		21	SS-3	4.5	6.0		7.2	25						22	6	28	14	8	A-3a							
26 B SS-1 1.5 3.0 1.4 2.9 26 7 1 8 22 8 A-3 0 400		ļ		_					25								_									
21 SS-3 4.5 6.0 4.4 5.9 16 8 8 8 A-3 0 8 8 A-3 0 8 8 A-3 0 0 8 A-3 0 0 A-3 0	5	В	SS-1	1.5			2.9	26						13	3	16	10	8	A-3a	0	400					
SS-4A 6.0 7.0 5.9 6.9 19 16 9 9 2 11 11 6 A-1-b 0 1573 9 1573 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0	022-0	SS-2	3.0	4.5	2.9	4.4	20						7	1	8	24	8	A-3	0						
SS-4A 6.0 7.0 5.9 6.9 19 16 9 9 2 11 11 6 A-1-b 0 1573 9 1573 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		21	SS-3	4.5	6.0	4.4	5.9	16									22	8	A-3	0						
27 B SS-1 1.5 3.0 1.1 2.6 26 9 2 11 11 6 A-1-b 0 1573								1	16										4							
023-0 SS-2 3.0 4.5 2.6 4.1 12 10 2 12 11 6 A-1-b 0 1 16 A-1-b 0 1 1 16 A-1-b 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	, 	В						!						9	2	11	_		1	0	1573					
21 SS-3 4.5 6.0 4.1 5.6 18 16 6 A-1-b 0	0	023-0						12						10	2	12	11	6	A-1-b	0						
		ŀ																		0						
SS-4 6.0 7.5 5.6 7.1 18 12 2.75 20 10 A-4b			SS-4	6.0	7.5	5.6	7.1	18	12	2.75							20	10	A-4b							



	Boring	Sample	Sam De _l		Subg De			dard	НР		P	hysica	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate	Proble	m	Excavate ar	-	Recommendation
#			From		From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	Content (ppm)	Unsuitable	Unstable	Unsuitable	Unstable	(Enter depth in inches)
28	В	SS-1	1.5	3.0	0.5	2.0	29						27	8	35	11	8	A-3a	0	133					
	024-0	SS-2	3.0	4.5	2.0	3.5	19						16	4	20	15	6	A-1-b	0						
	21	SS-3	4.5	6.0	3.5	5.0	26									17	6	A-1-b	0						
		SS-4	6.0	7.5	5.0	6.5	29	19	4.5							14	10	A-4b	8						
29	В	SS-1	1.5	3.0	0.4	1.9	30						16	5	21	5	6	A-1-b	0	560					
	025-0	SS-2	3.0	4.5	1.9	3.4	26									5	6	A-1-b	0						
	21	SS-3	4.5	6.0	3.4	4.9	42						15	4	19	6	6	A-1-b	0						
		SS-4	6.0	7.5	4.9	6.4	38	26								6	6	A-1-b	0						
30	В	SS-1	1.5	3.0	2.4	3.9	37						16	5	21	7	8	A-3a	0	73					
	026-0	SS-2	3.0	4.5	3.9	5.4	31						15	4	19	6	8	A-3a	0						
	21	SS-3	4.5	6.0	5.4	6.9	27									7	8	A-3a							
		SS-4	6.0	7.5	6.9	8.4	34	27								8	8	A-3a							
31	В	SS-1	1.5	3.0	1.7	3.2	29						25	6	31	10	8	A-3a	0	240					
	027-0	SS-2	3.0	4.5	3.2	4.7	26									9	8	A-3a	0						
	21	SS-3	4.5	6.0	4.7	6.2	16						26	8	34	8	8	A-3a	0						
		SS-4	6.0	7.5	6.2	7.7	18	16								12	8	A-3a							
32	В	SS-1	1.5	3.0	0.0	1.5	26						17	4	21	9	8	A-3a	0	93					
	028-0	SS-2	3.0	4.5	1.5	3.0	22									7	8	A-3a	0						
	21	SS-3	4.5	6.0	3.0	4.5	29									7	8	A-3a	0						
		SS-4	6.0	7.5	4.5	6.0	52	22								6	8	A-3a	0						
33	В	SS-1	1.5	3.0	0.0	1.5	34						26	7	33	9	8	A-3a	0	300					
	029-0	SS-2A	3.0	4.0	1.5	2.5	15						23	5	28	8	8	A-3a	0						
	21	SS-2B	4.0	4.5	2.5	3.0	15									11	8	A-3a	0						
		SS-3	4.5	6.0	3.0	4.5	18	15								6	8	A-3a	0						
34	В	SS-1	1.5	3.0	-0.1	1.4	56		4.5	29	22	7	47	17	64	12	17	A-4a	6	873					
	030-0	SS-2	3.0	4.5	1.4	2.9	63						21	5	26	8	10	A-2-4	0						
	21	SS-3	4.5	6.0	2.9	4.4	38		4.5							12	10	A-4a	8						
		SS-4	6.0	7.5	4.4	5.9	33	30	4.5							13	10	A-4a	8						
35	В	SS-1	1.5	3.0	0.3	1.8	23		4.5	24	17	7	31	15	46	11	12	A-4a	2	100					
	031-0	SS-2	3.0	4.5	1.8	3.3	27						22	7	29	9	10	A-2-4	0						
	21	SS-3	4.5	6.0	3.3	4.8	34									10	10	A-2-4	0						
		SS-4	6.0	7.5	4.8	6.3	37	23								11	10	A-2-4	0						
36	В	SS-1	1.5	3.0	1.5	3.0	34		4.5	25	18	7	48	18	66	11	13	A-4a	6	960					
	032-0	SS-2	3.0	4.5	3.0	4.5	33		4.5	23	16	7	44	15	59	11	11	A-4a	5						
	21	SS-3	4.5	6.0	4.5	6.0	38	1	4.5							12	10	A-4a	8						
		SS-4	6.0	7.5	6.0	7.5	45	30	4.5							12	10	A-4a							



#	Boring	Sample	Sam De	nple pth	1	grade pth	Stan Penet	dard ration	НР		P	hysic	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate and Replace (Item 204)		Recommendation (Enter depth in
#			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
37	В	SS-1	1.5	3.0	0.4	1.9	18		4.5	29	22	7	60	20	80	17	17	A-4b	8	733	A-4b				
	033-0	SS-2	3.0	4.5	1.9	3.4	15		4.5	29	22	7	58	20	78	16	17	A-4b	8		A-4b		40''		
	21	SS-3	4.5	6.0	3.4	4.9	14		4.5							21	10	A-4b	8						
		SS-4	6.0	7.5	4.9	6.4	14	14	4.5							17	10	A-4b	8						
38	В	SS-1	1.5	3.0	0.5	2.0	23						15	6	21	9	6	A-1-b	0	1413					
	034-0	SS-2	3.0	4.5	2.0	3.5	20						10	4	14	8	6	A-1-a	0						
	21	SS-3	4.5	6.0	3.5	5.0	18		4.5							15	10	A-4a	8						
		SS-4	6.0	7.5	5.0	6.5	25	18								7	6	A-1-a							
39	В	SS-1	1.5	3.0	0.2	1.7	12						20	5	25	15	8	A-3a	0	153					
	035-0	SS-2	3.0	4.5	1.7	3.2	11						24	5	29	11	8	A-3a	0						
	21	SS-3	4.5	6.0	3.2	4.7	11									11	8	A-3a	0						
		SS-4	6.0	7.5	4.7	6.2	12	11								11	8	A-3a	0						
40	В	SS-1	1.5	3.0	0.3	1.8	25						29	10	39	9	10	A-4a	6	367					
	036-0	SS-2	3.0	4.5	1.8	3.3	19						26	7	33	9	8	A-3a	0						
	21	SS-3	4.5	6.0	3.3	4.8	29									9	10	A-4a	8						
		SS-4	6.0	7.5	4.8	6.3	31	19								10	10	A-4a	8						
41	В	SS-1	1.5	3.0	0.5	2.0	27						18	6	24	6	8	A-3a	0	860					
	037-0	SS-2	3.0	4.5	2.0	3.5	22						17	6	23	7	8	A-3a	0						
	21	SS-3	4.5	6.0	3.5	5.0	23									5	8	A-3a	0						
		SS-4	6.0	7.5	5.0	6.5	23	22								6	8	A-3a	0						
42	В	SS-1	1.5	3.0	-0.1	1.4	15						14	5	19	11	8	A-3a	0	340					
	038-0	SS-2	3.0	4.5	1.4	2.9	15						19	5	24	11	8	A-3a	0						
	21	SS-3	4.5	6.0	2.9	4.4	14									11	8	A-3a	0						
		SS-4	6.0	7.5	4.4	5.9	20	14								11	8	A-3a	0						
43	В	SS-1	1.5	3.0	0.6	2.1	22						7	1	8	7	6	A-1-b	0	793					
	039-0	SS-2	3.0	4.5	2.1	3.6	20						7	2	9	4	6	A-1-b	0						
	21	SS-3	4.5	6.0	3.6	5.1	18									5	6	A-1-b	0						
		SS-4	6.0	7.5	5.1	6.6	16	16								4	6	A-1-b							
44	В	SS-1	1.5	3.0	0.8	2.3	41						6	2	8	9	8	A-3	0	413					
	040-0	SS-2	3.0	4.5	2.3	3.8	11						5	1	6	5	8	A-3	0						
	21	SS-3	4.5	6.0	3.8	5.3	14									7	8	A-3	0						
		SS-4	_	7.5	5.3	6.8	14	11								4	8	A-3							
45	В	SS-1	1.5		-0.7	0.8	29						11	2	13	8	6	A-1-b	0	1300					
	041-0	SS-2	3.0	4.5	0.8	2.3	26						10	2	12	10	6	A-1-b	0						
	21	SS-3	4.5	6.0	2.3	3.8	29									5	6	A-1-b	0						
		SS-4	6.0	7.5	3.8	5.3	30	26								4	6	A-1-b	0						



	Boring	Sample	Sam	-	Subg De	rade pth	Stan Penet	dard ration	НР		P	hysica	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate	Proble	m	Excavate ar	Recommendation
#			From		From	То		N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	Mc	M _{OPT}	Class	GI	Content (ppm)	Unsuitable	Unstable	Unsuitable	(Enter depth in inches)
46	В	SS-1	1.5	3.0	0.9	2.4	50						17	5	22	10	6	A-1-b	0	933				
	042-0	SS-2	3.0	4.5	2.4	3.9	41						18	5	23	11	8	A-3a	0					
	21	SS-3	4.5	6.0	3.9	5.4	23									12	8	A-3a	0					
		SS-4	6.0	7.5	5.4	6.9	23	23								10	8	A-3a						
47	В	SS-1	1.5	3.0	0.6	2.1	27						19	8	27	10	8	A-3a	0	2800				
	043-0	SS-2	3.0	4.5	2.1	3.6	27						17	6	23	30	8	A-3a	0					
	21	SS-3	4.5	6.0	3.6	5.1	31									6	8	A-3a	0					
		SS-4	6.0	7.5	5.1	6.6	31	27								5	8	A-3a						
48	В	SS-1	1.5	3.0	0.8	2.3	14						14	5	19	6	6	A-1-b	0	1080				
	044-0	SS-2	3.0	4.5	2.3	3.8	12									8	6	A-1-b	0					
	21	SS-3	4.5	6.0	3.8	5.3	18						13	5	18	8	6	A-1-b	0					
	ľ	SS-4	6.0	7.5	5.3	6.8	14	12								9	6	A-1-b						
49	В	SS-1	1.5	3.0	0.8	2.3	15						9	3	12	4	6	A-1-a	0	340				
	045-0	SS-2	3.0	4.5	2.3	3.8	11						21	7	28	14	8	A-3a	0					
	21	SS-3	4.5	6.0	3.8	5.3	14									12	8	A-3a	0					
	ľ	SS-4	6.0	7.5	5.3	6.8	12	11								9	8	A-3a						
50	В	SS-1	1.5	3.0	-0.1	1.4	38						14	5	19	6	6	A-1-b	0	253				
	046-0	SS-2A	3.0	4.5	1.4	2.9	25									6	6	A-1-b	0					
	21	SS-2B	4.5	6.0	2.9	4.4	25		4.5	25	19	6	67	29	96	15	14	A-4b	8					
	•	SS-3	6.0	7.5	4.4	5.9	26	25	4.5							16	10	A-4b	8					
51	В	SS-1	1.5	3.0	0.0	1.5	26						13	5	18	12	8	A-3a	0	67				
	047-0	SS-2	3.0	4.5	1.5	3.0	19						21	10	31	11	8	A-3a	0					
	21	SS-3	4.5	6.0	3.0	4.5	15									13	8	A-3a	0					
	ľ	SS-4	6.0	7.5	4.5	6.0	12	12								13	8	A-3a	0					
52	В	SS-1	1.5	3.0	-1.3	0.3	30						12	3	15	9	6	A-1-b	0	2387				
	048-0	SS-2	3.0	4.5	0.3	1.8	20						23	6	29	10	8	A-3a	0					
	21	SS-3	4.5	6.0	1.8	3.3	20									12	6	A-1-b	0					
		SS-4	6.0	7.5	3.3	4.8	12	12								10	8	A-3a	0					
53	В	SS-1	1.5	3.0	1.8	3.3	15						14	2	16	23	8	A-3a	0	20				
	049-0	SS-2	3.0	4.5	3.3	4.8	10						26	2	28	20	8	A-3a	0					
	21	SS-3	4.5	6.0	4.8	6.3	10									27	8	A-3a	0					
		SS-4	6.0	7.5	6.3	7.8	10	10								20	8	A-3a						
54	В	SS-1	-	3.0	0.1	1.6	29						12	1	13	16	6	A-1-b	0	1100				
	050-0	SS-2	3.0	4.5	1.6	3.1	25									14	6	A-1-b	0					
	21	SS-3	4.5	6.0	3.1	4.6	33						11	1	12	45	6	A-1-b	0					
		SS-4	6.0	7.5	4.6	6.1	29	25						-	12	41	6	A-1-b	0					





#	Boring	Sample	San De	nple pth	1 ~	grade pth		dard ration	НР		P	hysic	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate ar (Item	•	Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inchas)
55	В	SS-1	1.5	3.0	-0.3	1.2	39						14	3	17	9	6	A-1-b	0	3000					
	051-0	SS-2	3.0	4.5	1.2	2.7	23						30	7	37	10	10	A-4a	5						
	21	SS-3	4.5	6.0	2.7	4.2	26									7	10	A-4a	8						
		SS-4A	6.0	7.0	4.2	5.2	38	23								14	10	A-4a	8						
56	В	SS-1	1.5	3.0	0.7	2.2	31						9	3	12	6	8	A-3a	0	40					
	052-0	SS-2	3.0	4.5	2.2	3.7	26						12	5	17	13	8	A-3a	0						
	21	SS-3	4.5	6.0	3.7	5.2	16									7	8	A-3a	0						
		SS-4	6.0	7.5	5.2	6.7	14	14								7	8	A-3a							
57	В	SS-1	1.5	3.0	0.4	1.9	22		4.5	22	15	7	25	13	38	12	10	A-4a	1	347					
	053-0	SS-2	3.0	4.5	1.9	3.4	20			19	14	5	27	14	41	10	10	A-4a	1						
	21	SS-3	4.5	6.0	3.4	4.9	53									8	8	A-3a	0						
		SS-4	6.0	7.5	4.9	6.4	56	20								8	8	A-3a	0						



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 57

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 8/30/2023

C	Chemical Stabilization Option	าร
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	NA

Excavate and Repl Stabilization Option	
Global Geotextile	J.1.5
Average(N60L):	0''
Average(HP):	0''
Global Geogrid	
Average(N60L):	0''
Average(HP):	0"

Design CBR	10
---------------	----

% Samples within 6 feet of subgrade									
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%						
N ₆₀ < 12	3%	0.5 < HP ≤ 1	0%						
12 ≤ N ₆₀ < 15	8%	1 < HP ≤ 2	0%						
N ₆₀ ≥ 20	71%	HP > 2	17%						
M+	5%								
Rock	0%								
Unsuitable	14%								

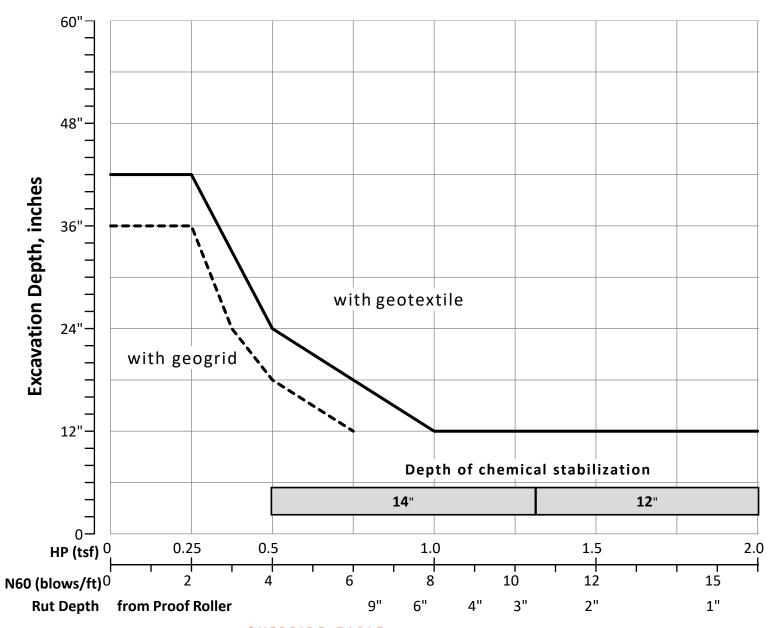
Excavate and Replace	ace
Average	0"
Maximum	0"
Minimum	0"

% Proposed Subgrade Su	ırface
Unstable & Unsuitable	18%
Unstable	9%
Unsuitable	9%

	N ₆₀	N _{60L}	НР	LL	PL	PI	Silt	Clay	P 200	M _c	M _{OPT}	GI
Average	27	20	4.34	25	18	7	26	7	33	12	9	2
Maximum	80	30	4.50	29	22	9	83	34	96	45	17	8
Minimum	10	10	2.75	19	14	4	3	1	4	4	6	0

	Classification Counts by Sample																		
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	9	40	13	0	0	0	11	83	39	31	0	0	0	0	0	0	0	226
Percent	0%	4%	18%	6%	0%	0%	0%	5%	37%	17%	14%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%					86%								14	1%				100%
Surface Class Count	0	6	27	8	0	0	0	4	41	20	14	0	0	0	0	0	0	0	120
Surface Class Percent	0%	5%	23%	7%	0%	0%	0%	3%	34%	17%	12%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
4.34	0.50	НР
20.35	6.00	N60L

Average HP Average N_{60L}

MAINLINE IR-490	
MAINLINE IN-490	



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

IR-490 Mainline -Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By:

Derar M. Tarawneh

Date prepared: Wednesday, August 30, 2023

Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

brendan.andrews@neasinc.com

NO. OF BORINGS:

25





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-109-0-20	IR-90	930+69	5	RT	S&ME TRK 55 (R52)	90	656.0	654.4	1.6 C
2	B-110-0-20	IR-90	931+91	38	LT	S&ME TRK 55 (R52)	90	648.1	645.9	2.2 C
3	B-111-0-20	IR-90	935+97	5	RT	S&ME TRK 55 (R52)	90	639.8	638.3	1.5 C
4	B-112-0-20	IR-90	937+90	5	LT	S&ME TRK 55 (R52)	90	635.8	634.5	1.3 C
5	B-001-0-21	IR-490	939+11	39	LT	CME 45B	82	632.9	632.0	0.9 C
6	B-002-0-21	IR-490	942+36	47	RT	CME 45B	82	632.1	628.6	3.5 C
7	B-003-0-21	IR-490	946+27	40	LT	CME 45B	82	631.5	631.1	0.4 C
8	B-004-0-21	IR-490	950+05	51	RT	CME 45B	82	635.9	633.4	2.5 C
9	B-005-0-21	IR-490	953+92	41	LT	CME 45B	82	635.3	634.5	0.8 C
10	B-006-0-21	IR-490	957+83	78	RT	CME 45B	82	632.7	631.9	0.8 C
11	B-007-0-21	IR-490	961+53	73	LT	CME 45B	82	628.0	626.3	1.7 C
12	B-008-0-21	IR-490	965+28	63	RT	CME 45B	82	617.0	617.2	0.2 F
13	B-009-0-21	IR-490	969+07	61	LT	CME 45B	82	613.6	613.0	0.6 C
14	B-010-0-21	IR-490	972+85	62	RT	CME 45B	82	616.8	614.0	2.9 C
15	B-011-0-21	IR-490	976+32	61	LT	CME 45B	82	622.9	623.1	0.3 F
16	B-012-0-21	IR-490	979+20	72	RT	CME 45B	82	631.9	628.5	3.4 C
17	B-013-0-21	IR-490	982+49	63	LT	CME 45B	82	635.5	637.0	1.5 F
18	B-014-021	IR-490	985+62	74	RT	CME 45B	82	648.4	645.5	2.9 C
19	B-015-0-21	IR-490	1021+43	40	RT	CME 45B	82	647.3	649.4	2.2 F
20	B-016-0-21	IR-490	1025+70	40	LT	CME 45B	82	640.3	638.7	1.7 C
21	B-017-0-21	IR-490	1029+41	39	RT	CME 45B	82	629.8	628.7	1.0 C
22	B-018-0-21	IR-490	1032+80	42	LT	CME 45B	82	624.6	622.7	1.9 C
23	B-019-0-21	IR-490	1036+77	37	RT	CME 45B	82	624.2	622.4	1.8 C
24	B-020-0-21	IR-490	1040+62	48	LT	CME 45B	82	631.2	629.9	1.3 C
25	B-021-0-21	IR-490	1045+27	40	RT	CME 45B	82	641.1	642.4	1.2 F



			Sam	nle	Subg	rade	Stan	dard															Excavate ar	d Renlace	
#	Boring	Sample	De	•	De			ration	НР		Pl	nysica	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate	Proble	m	(Item	•	Recommendation
#			From		From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	Mc	M _{OPT}	Class	GI	Content (ppm)	Unsuitable	Unstable	Unsuitable	Unstable	(Enter depth in inches)
1	В	SS-1	1.5	3.0	-0.1	1.4	50						38	8	46	21	10	A-4a	8	443		Mc			
	109-0	SS-2	3.0	4.5	1.4	2.9	35						35	3	38	21	10	A-4a	5			Mc			
	20	SS-3	4.5	6.0	2.9	4.4	29									20	10	A-4a	8						
		SS-4	6.0	7.5	4.4	5.9	33	29								20	10	A-4a	8						
2	В	SS-1	1.5	3.0	-0.7	0.8	27						13	3	16	7	8	A-3a	0	174					
	110-0	SS-2	3.0	4.5	0.8	2.3	80									9	8	A-3a	0						
	20	SS-3	4.5	6.0	2.3	3.8	54						44	6	50	17	10	A-4a	8						
		SS-4	6.0	7.5	3.8	5.3	41	27								19	10	A-4a	8						
3	В	SS-1	1.5	3.0	0.0	1.5	50						12	5	17	11	8	A-3a	0	248					
	111-0	SS-2	3.0	4.5	1.5	3.0	50						3	1	4	6	6	A-1-a	0						
	20	SS-3	4.5	6.0	3.0	4.5	18			25	17	8	60	34	94	20	12	A-4b	8						
		SS-4	6.0	7.5	4.5	6.0	23	18								20	10	A-4b	8						
4	В	SS-1	1.5	1.9	0.2	0.6	50						5	2	7	16	6	A-1-a	0	197					
	112-0	SS-2	3.0	3.4	1.7	2.1	50						8	3	11	17	6	A-1-a	0						
	20	SS-3	4.5	4.9	3.2	3.6	50									21	6	A-1-a	0						
		SS-4	6.0	6.5	4.7	5.2	50	30								15	6	A-1-a	0						
5	В	SS-1	1.5	3.0	0.6	2.1	37						15	3	18	11	8	A-3a	0	1433					
	001-0	SS-2	3.0	4.5	2.1	3.6	30									9	8	A-3a	0						
	21	SS-3	4.5	6.0	3.6	5.1	30						12	3	15	12	6	A-1-b	0						
		SS-4	6.0	7.5	5.1	6.6	27	27								12	8	A-3a							
6	В	SS-1	1.5	3.0	-2.0	-0.5	23						13	5	18	9	6	A-1-b	0	227					
	002-0	SS-2	3.0	4.5	-0.5	1.0	19									11	6	A-1-b	0						
	21	SS-3A	4.5	5.5	1.0	2.0	31									9	6	A-1-b	0						
	•	SS-3B	5.5	6.0	2.0	2.5	31	19	4.5	27	18	9	65	28	93	13	13	A-4b	8		A-4b		30"		
7	В	SS-1A	1.5	2.2	1.1	1.8	42						21	6	27	7	8	A-3a	0	647					
	003-0	SS-1B	2.2	3.0	1.8	2.6	42			22	18	4	71	16	87	13	13	A-4b	8		A-4b				
	21	SS-2	3.0	4.5	2.6	4.1	34	1		24	20	4	44	11	55	10	15	A-4a	4						
		SS-3	4.5	6.0	4.1	5.6	33	30								14	10	A-4b	8						
8	В	SS-1	1.5	3.0	-1.0	0.5	27						22	5	27	8	10	A-2-4	0	693					
	004-0	SS-2A	3.0	4.0	0.5	1.5	29									8	10	A-2-4	0				·		
	21	SS-2B	4.0	4.5	1.5	2.0	29	1	4.5							14	10	A-4b	8		A-4b	Мс			
		SS-3	4.5	6.0	2.0	3.5	26	26	4.5	25	19	6	65	29	94	15	14	A-4b	8		A-4b	.,,,	42''		
9	В	SS-1	1.5			2.2	35						16	5	21	6	6	A-1-b	0	487					
	005-0	SS-2	3.0	4.5	2.2	3.7	31						22	6	28	7	8	A-3a	0						
	21	SS-3	4.5	6.0	3.7	5.2	34	1								10	8	A-3a	0						
		SS-4	6.0	7.5	5.2	6.7	18	18	4.25							16	10	A-4b							



	Boring	Sample	Sam Dei	•	Subg	rade pth	Stan	dard ration	НР	' <u> </u>			isture	Ohio DOT		Sulfate	Problem		Excavate and Replace (Item 204)		Recommendation				
#			From		From	То		N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	Content (ppm)	Unsuitable	Unstable	Unsuitable	,	(Enter depth in inches)
10	В	SS-1	1.5	3.0	0.7	2.2	15						9	2	11	21	6	A-1-a	0	1187					
	006-0	SS-2	3.0	4.5	2.2	3.7	15		3	23	16	7	47	24	71	17	11	A-4a	7						
	21	SS-3	4.5	6.0	3.7	5.2	16		4.25							21	10	A-4a	8						
	Ī	SS-4	6.0	7.5	5.2	6.7	19	15	4.25							21	10	A-4a							
11	В	SS-1	1.5	3.0	-0.2	1.3	29						16	2	18	7	8	A-3a	0	193					
	007-0	SS-2	3.0	4.5	1.3	2.8	19									9	8	A-3a	0						
	21	SS-3	4.5	6.0	2.8	4.3	15						17	3	20	11	8	A-3a	0						
	Ī	SS-4	6.0	7.5	4.3	5.8	16	15								9	8	A-3a	0						
12	В	SS-1	1.5	3.0	1.7	3.2	26						28	10	38	9	10	A-4a	5	1280					
	008-0	SS-2	3.0	4.5	3.2	4.7	16		4.5							11	10	A-4a	8						
	21	SS-3	4.5	6.0	4.7	6.2	30		4.5	24	17	7	46	18	64	12	12	A-4a	6						
	ľ	SS-4	6.0	7.5	6.2	7.7	35	16	4.5							14	10	A-4a							
13	В	SS-1	1.5	3.0	0.9	2.4	29		4.5	21	16	5	32	12	44	10	11	A-4a	2	313					
	009-0	SS-2	3.0	4.5	2.4	3.9	23		4.5	27	18	9	36	17	53	15	13	A-4a	4						
	21	SS-3	4.5	6.0	3.9	5.4	23		4.5							14	10	A-4a	8						
	ľ	SS-4	6.0	7.5	5.4	6.9	25	23	4.5							13	10	A-4a							
14	В	SS-1	1.5	3.0	-1.4	0.1	27						23	10	33	12	10	A-2-4	0	553					
	010-0	SS-2	3.0	4.5	0.1	1.6	37									11	10	A-2-4	0						
	21	SS-3	4.5	6.0	1.6	3.1	34						26	9	35	12	10	A-2-4	0						
	ľ	SS-4	6.0	7.5	3.1	4.6	29	27								11	10	A-2-4	0						
15	В	SS-1	1.5	3.0	1.8	3.3	41						10	2	12	18	6	A-1-b	0	2120					
	011-0	SS-2A	3.0	4.0	3.3	4.3	18									15	6	A-1-b	0						
	21	SS-2B	4.0	4.5	4.3	4.8	18		4.5	27	21	6	58	21	79	19	16	A-4b	8						
	ľ	SS-3	4.5	6.0	4.8	6.3	16	16								21	6	A-1-b	0						
16	В	SS-1	1.5	3.0	-1.9	-0.4	37			NP	NP	NP	78	16	94	14	11	A-4b	8						
	012-0	SS-2	3.0	4.5	-0.4	1.1	29			NP	NP	NP	74	12	86	15	11	A-4b	8		A-4b	Mc			
	21	SS-3	4.5	6.0	1.1	2.6	29									15	10	A-4b	8		A-4b	Мс	31"		
	ľ	SS-4	6.0	7.5	2.6	4.1	31	29								14	10	A-4b	8						
17	В	SS-1	1.5	3.0	3.0	4.5	23		3.75				50	6	56	17	10	A-4b	8	900					
	013-0	SS-2	3.0	4.5	4.5	6.0	19		4.5				83	9	92	22	10	A-4b	8						
	21	SS-3	4.5	6.0	6.0	7.5	23		3							19	10	A-4b							
		SS-4	6.0	7.5	7.5	9.0	27	19	4.5							16	10	A-4b							
18	В	SS-1	1.5		-1.4	0.1	29						19	5	24	7	8	A-3a	0	2133					
	014-0	SS-2	3.0	4.5	0.1	1.6	25						12	2	14	5	8	A-3a	0						
	1	SS-3	4.5	6.0	1.6	3.1	16									8	8	A-3a	0						
		SS-4	6.0	7.5	3.1	4.6	14	14								7	8	A-3a	0						



#	Boring	Sample	Sam De _l	•	Subg De			dard	НР		P	hysic	al Chara	cteristics		Мо	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate an	-	Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M_{c}	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
19	В	SS-1	1.5	3.0	3.7	5.2	29						21	7	28	9	8	A-3a	0	2367					
	015-0	SS-2	3.0	4.5	5.2	6.7	29									7	8	A-3a							
	21	SS-3A	4.5	5.0	6.7	7.2	12									19	8	A-3a							
		SS-3B	5.0	6.0	7.2	8.2	12	29					10	2	12	8	8	A-3a							
20	В	SS-1	1.5	3.0	-0.2	1.3	25						11	3	14	10	8	A-3a	0	973					
	016-0	SS-2	3.0	4.5	1.3	2.8	25									5	8	A-3	0						
	21	SS-3	4.5	6.0	2.8	4.3	23						8	2	10	5	8	A-3	0						
		SS-4	6.0	7.5	4.3	5.8	20	20								4	8	A-3	0						
21	В	SS-1	1.5	3.0	0.5	2.0	26						25	5	30	9	8	A-3a	0	0					
	017-0	SS-2	3.0	4.5	2.0	3.5	20						24	7	31	12	8	A-3a	0						
	21	SS-3	4.5	6.0	3.5	5.0	27									9	8	A-3a	0						
		SS-4	6.0	7.5	5.0	6.5	30	20	4.5							18	10	A-4b	8						
22	В	SS-1	1.5	3.0	-0.4	1.1	30						44	4	48	14	10	A-4a	8	627		Mc			
	018-0	SS-2	3.0	4.5	1.1	2.6	31						80	9	89	20	10	A-4b	8		A-4b	Mc			
	21	SS-3	4.5	6.0	2.6	4.1	18									21	10	A-4b	8						
		SS-4	6.0	7.5	4.1	5.6	18	18								26	10	A-4b	8						
23	В	SS-1	1.5	3.0	-0.3	1.2	31						44	6	50	16	10	A-4a	8	820		Mc			
	019-0	SS-2	3.0	4.5	1.2	2.7	27									19	10	A-4a	8			Mc			
	21	SS-3	4.5	6.0	2.7	4.2	22						44	7	51	20	10	A-4a	8						
		SS-4	6.0	7.5	4.2	5.7	27	22								18	10	A-4b	8						
24	В	SS-1A	1.5	2.5	0.2	1.2	33						21	4	25	13	6	A-1-b	0	2600					
	020-0	SS-1B	2.5	3.0	1.2	1.7	33									14	10	A-4b	8		A-4b	Mc			
	21	SS-2A	3.0	3.5	1.7	2.2	27						73	12	85	19	10	A-4b	8		A-4b	Mc	26"		
		SS-2B	3.5	4.5	2.2	3.2	27	27								18	8	A-3	0						
25	В	SS-1	1.5	3.0	2.7	4.2	25						20	5	25	10	10	A-2-4	0	1400					
	021-0	SS-2	3.0	4.5	4.2	5.7	37									15	10	A-2-4	0						
	21	SS-3	4.5	6.0	5.7	7.2	25						22	6	28	14	8	A-3a							
		SS-4	6.0	7.5	7.2	8.7	35	25								14	10	A-2-4							



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 25

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 8/30/2023

C	Chemical Stabilization Option	ns
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	NA

Excavate and Repl	ace
Stabilization Option	ons
Global Geotextile	
Average(N60L):	0"
Average(HP):	0''
Global Geogrid	
Average(N60L):	0"
Average(HP):	0''

Design CBR	9
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% Sampl	es within	6 feet of subgi	rade
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%
N ₆₀ < 12	0%	0.5 < HP ≤ 1	0%
12 ≤ N ₆₀ < 15	1%	1 < HP ≤ 2	0%
N ₆₀ ≥ 20	80%	HP > 2	19%
M+	12%		
Rock	0%		
Unsuitable	23%		

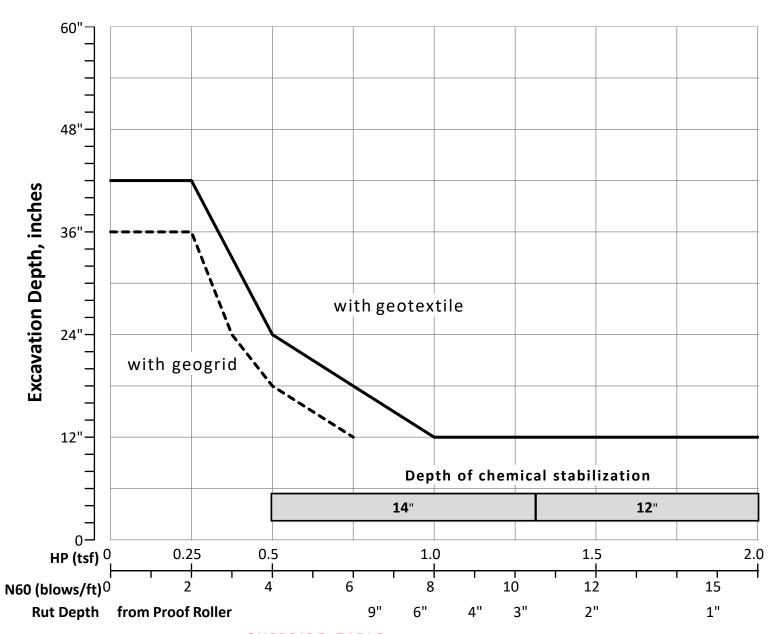
Excavate and Replant Surface	ace
Average	0"
Maximum	0"
Minimum	0"

% Proposed Subgrade Su	ırface
Unstable & Unsuitable	35%
Unstable	19%
Unsuitable	16%

	N ₆₀	N _{60L}	НР	LL	PL	PI	Silt	Clay	P 200	M_{c}	M _{OPT}	GI
Average	29	22	4.28	25	18	7	32	8	40	14	9	3
Maximum	80	30	4.50	27	21	9	83	34	94	26	16	8
Minimum	12	14	3.00	21	16	4	3	1	4	4	6	0

Classification Counts by Sample																			
ODOT Class	Rock	ock A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-3 A-3a A-4a A-4b A-5 A-6a A-6b A-7-5 A-7-6 A-8a A-8b													Totals				
Count	0	6	8	9	0	0	0	4	26	22	23	0	0	0	0	0	0	0	98
Percent	0%	6%	8%	9%	0%	0%	0%	4%	27%	22%	23%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%					77%								23	3%				100%
Surface Class Count	0	4	6	6	0	0	0	2	15	12	12	0	0	0	0	0	0	0	57
Surface Class Percent	0%	7%	11%	11%	0%	0%	0%	4%	26%	21%	21%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
4.28	0.50	НР
22.36	6.00	N60L

Average HP Average N_{60L}

Lane E-S (WB-490 to SB-71)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Lane E-S (WB-490 to SB-71) -Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By: Date prepared:

Derar M. Tarawneh Friday, March 3, 2023

Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

brendan.andrews@neasinc.com

NO. OF BORINGS:

6





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-023-0-21	LANE E-S	3054+54	6	LT	CME 45B	82	638.5	638.1	0.4 C
2	B-024-0-21	LANE E-S	3050+96	5	LT	CME 45B	82	652.7	651.6	1.0 C
3	B-025-0-21	LANE E-S	3047+38	2	LT	CME 45B	82	667.3	666.2	1.1 C
4	B-026-0-21	LANE E-S	3041+89	27	RT	CME 45B	82	677.8	678.7	0.9 F
5	B-027-0-21	LANE E-S	3038+16	27	RT	CME 45B	82	674.5	674.7	0.2 F
6	B-028-0-21	LANE E-S	3034+13	26	RT	CME 45B	82	669.4	667.9	1.5 C

V. 14.5

#	Boring	Sample	San De	nple pth	_	rade pth	Stan Penet		НР		P	hysic	al Chara	cteristics		Mo	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate an	-	Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M_{c}	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	1.1	2.6	26						9	2	11	11	6	A-1-b	0	1573					
	023-0	SS-2	3.0	4.5	2.6	4.1	12						10	2	12	11	6	A-1-b	0						
	21	SS-3	4.5	6.0	4.1	5.6	18									16	6	A-1-b	0						
		SS-4	6.0	7.5	5.6	7.1	18	12	2.75							20	10	A-4b							
2	В	SS-1	1.5	3.0	0.5	2.0	29						27	8	35	11	8	A-3a	0	133					
	024-0	SS-2	3.0	4.5	2.0	3.5	19						16	4	20	15	6	A-1-b	0						
	21	SS-3	4.5	6.0	3.5	5.0	26									17	6	A-1-b	0						
		SS-4	6.0	7.5	5.0	6.5	29	19	4.5							14	10	A-4b	8						
3	В	SS-1	1.5	3.0	0.4	1.9	30						16	5	21	5	6	A-1-b	0	560					
	025-0	SS-2	3.0	4.5	1.9	3.4	26									5	6	A-1-b	0						
	21	SS-3	4.5	6.0	3.4	4.9	42						15	4	19	6	6	A-1-b	0						
		SS-4	6.0	7.5	4.9	6.4	38	26								6	6	A-1-b	0						
4	В	SS-1	1.5	3.0	2.4	3.9	37						16	5	21	7	8	A-3a	0	73					
	026-0	SS-2	3.0	4.5	3.9	5.4	31						15	4	19	6	8	A-3a	0						
	21	SS-3	4.5	6.0	5.4	6.9	27									7	8	A-3a							
		SS-4	6.0	7.5	6.9	8.4	34	27								8	8	A-3a							
5	В	SS-1	1.5	3.0	1.7	3.2	29						25	6	31	10	8	A-3a	0	240					
	027-0	SS-2	3.0	4.5	3.2	4.7	26									9	8	A-3a	0						
	21	SS-3	4.5	6.0	4.7	6.2	16	1					26	8	34	8	8	A-3a	0						
		SS-4	6.0	7.5	6.2	7.7	18	16							-	12	8	A-3a							
6	В	SS-1	1.5	3.0	0.0	1.5	26						17	4	21	9	8	A-3a	0	93					
	028-0	SS-2	3.0	4.5	1.5	3.0	22	1								7	8	A-3a	0						
	21	SS-3	4.5	6.0	3.0	4.5	29	1								7	8	A-3a	0						
		SS-4	6.0	7.5	4.5	6.0	52	22								6	8	A-3a	0						



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 6

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

(Chemical Stabilization Option	ıs									
320	320 Rubblize & Roll Option										
206	Cement Stabilization	No									
	Lime Stabilization	Option									
206	Depth	NA									

Excavate and Repl	ace
Stabilization Option	ons
Global Geotextile	
Average(N60L):	0"
Average(HP):	0"
Global Geogrid	
Average(N60L):	0"
Average(HP):	0"

Design CBR	13
---------------	----

% Sampl	es within	6 feet of subgr	ade
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%
N ₆₀ < 12	0%	0.5 < HP ≤ 1	0%
12 ≤ N ₆₀ < 15	5%	1 < HP ≤ 2	0%
N ₆₀ ≥ 20	77%	HP > 2	9%
M+	0%		
Rock	0%		
Unsuitable	8%		

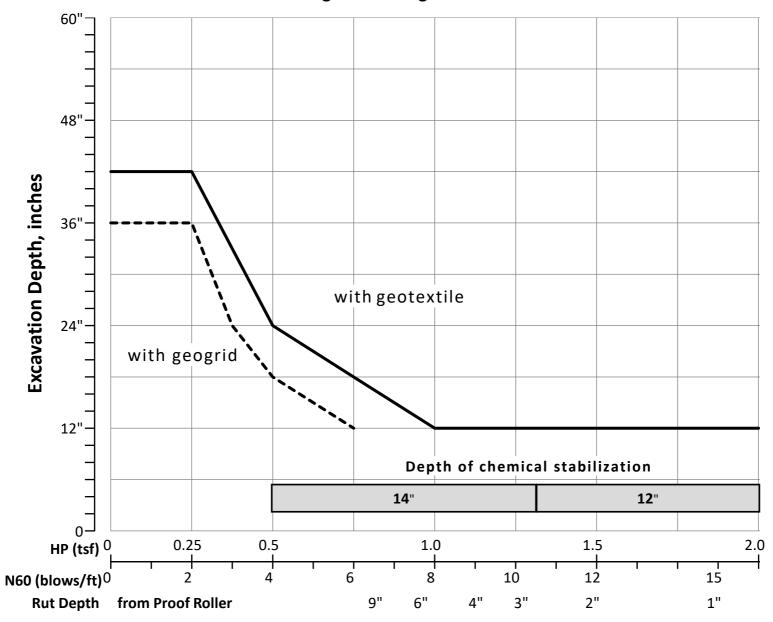
Excavate and Replace at Surface										
Average	0"									
Maximum	0"									
Minimum	0"									

% Proposed Subgrade Su	rface
Unstable & Unsuitable	0%
Unstable	0%
Unsuitable	0%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{OPT}	GI
Average	28	20	3.63				17	5	22	10	7	0
Maximum	52	27	4.50	0	0	0	27	8	35	20	10	8
Minimum	12	12	2.75	0	0	0	9	2	11	5	6	0

					Class	ificat	ion C	ount	s by	Sam	ple								
ODOT Class	Rock	ck A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-3 A-3a A-4a A-4b A-5 A-6a A-6b A-7-5 A-7-6 A-8a A-8b													Totals				
Count	0	0	9	0	0	0	0	0	13	0	2	0	0	0	0	0	0	0	24
Percent	0%	0%	38%	0%	0%	0%	0%	0%	54%	0%	8%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%					92%								8	%				100%
Surface Class Count	0	0	5	0	0	0	0	0	5	0	0	0	0	0	0	0	0	0	10
Surface Class Percent	0%	0%	50%	0%	0%	0%	0%	0%	50%	0%	0%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
3.63	0.50	HР
20.33	6.00	N60L

Average HP Average N_{60L}

RAMP 7-7C (NB 7th St to EB-490)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Ramp 7-7C (NB 7th St. to EB-490) Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By: Date prepared:

Derar M. Tarawneh Friday, March 3, 2023

Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

brendan.andrews@neasinc.com

NO. OF BORINGS:

5





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-029-0-21	Ramp 7-7C	67+99	145	RT	CME 45B	82	643.8	642.3	1.5 C
2	B-030-0-21	Ramp 7-7C	68+99	19	RT	CME 45B	82	624.2	622.7	1.6 C
3	B-031-0-21	Ramp 7-7C	72+21	23	RT	CME 45B	82	623.8	622.5	1.2 C
4	B-032-0-21	Ramp 7-7C	76+12	11	RT	CME 45B	82	622.0	622.0	0.0 C
5	B-012-0-21	Ramp 7-7C	79+20	20	LT	CME 45B	82	631.9	630.1	1.8 C

V. 14.5 1/18/2019

#	Boring	Sample	Sam De _l	•	Subg De	rade pth	Stan Penet	dard ration	НР		Pl	nysica	al Chara	cteristics		Moi	isture	Ohio	DOT	Sulfate Content	Sulfate Problem		Excavate ar (Item	•	Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	0.0	1.5	34						26	7	33	9	8	A-3a	0	300					
	029-0	SS-2A	3.0	4.0	1.5	2.5	15						23	5	28	8	8	A-3a	0						
	21	SS-2B	4.0	4.5	2.5	3.0	15									11	8	A-3a	0						
		SS-3	4.5	6.0	3.0	4.5	18	15								6	8	A-3a	0						
2	В	SS-1	1.5	3.0	-0.1	1.4	56		4.5	29	22	7	47	17	64	12	17	A-4a	6	873					
	030-0	SS-2	3.0	4.5	1.4	2.9	63						21	5	26	8	10	A-2-4	0						
	21	SS-3	4.5	6.0	2.9	4.4	38		4.5							12	10	A-4a	8						
		SS-4	6.0	7.5	4.4	5.9	33	30	4.5							13	10	A-4a	8						
3	В	SS-1	1.5	3.0	0.3	1.8	23		4.5	24	17	7	31	15	46	11	12	A-4a	2	100					
	031-0	SS-2	3.0	4.5	1.8	3.3	27						22	7	29	9	10	A-2-4	0						
	21	SS-3	4.5	6.0	3.3	4.8	34									10	10	A-2-4	0						
		SS-4	6.0	7.5	4.8	6.3	37	23								11	10	A-2-4	0						
4	В	SS-1	1.5	3.0	1.5	3.0	34		4.5	25	18	7	48	18	66	11	13	A-4a	6	960					
	032-0	SS-2	3.0	4.5	3.0	4.5	33		4.5	23	16	7	44	15	59	11	11	A-4a	5						
	21	SS-3	4.5	6.0	4.5	6.0	38		4.5							12	10	A-4a	8						
		SS-4	6.0	7.5	6.0	7.5	45	30	4.5							12	10	A-4a							
5	В	SS-1	1.5	3.0	-0.3	1.2	37						78	16	94	14	10	A-4b	8	733	A-4b	Mc			
	012-0	SS-2	3.0	4.5	1.2	2.7	29						74	12	86	15	10	A-4b	8		A-4b	Мс	33"		
	21	SS-3	4.5	6.0	2.7	4.2	29									15	10	A-4b	8						
		SS-4	6.0	7.5	4.2	5.7	31	29								14	10	A-4b	8						



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 5

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

C	Chemical Stabilization Options								
320	Rubblize & Roll	Option							
206	06 Cement Stabilization								
	Lime Stabilization	No							
206	Depth	NA							

Excavate and Replace							
Stabilization Option	Stabilization Options						
Global Geotextile							
Average(N60L):	0''						
Average(HP):	0"						
Global Geogrid							
Average(N60L):	0"						
Average(HP):	0"						

Design CBR	8
---------------	---

% Sampl	% Samples within 6 feet of subgrade									
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%							
N ₆₀ < 12	0%	0.5 < HP ≤ 1	0%							
12 ≤ N ₆₀ < 15	0%	1 < HP ≤ 2	0%							
N ₆₀ ≥ 20	85%	HP > 2	40%							
M+	10%									
Rock	0%									
Unsuitable	20%									

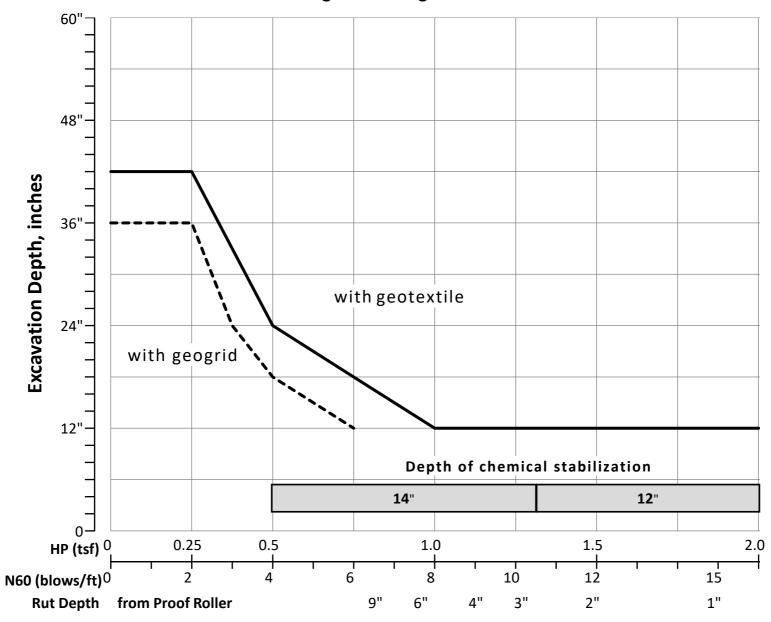
Excavate and Replace at Surface							
Average	0"						
Maximum	0"						
Minimum	0"						

% Proposed Subgrade Surface							
Unstable & Unsuitable	36%						
Unstable	18%						
Unsuitable	18%						

	N ₆₀	N _{60L}	НР	LL	PL	PI	Silt	Clay	P 200	M_{c}	M _{OPT}	GI
Average	33	25	4.50	25	18	7	41	12	53	11	10	4
Maximum	63	30	4.50	29	22	7	78	18	94	15	17	8
Minimum	15	15	4.50	23	16	7	21	5	26	6	8	0

	Classification Counts by Sample																		
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	0	4	0	0	0	0	4	8	4	0	0	0	0	0	0	0	20
Percent	0%	0%	0%	20%	0%	0%	0%	0%	20%	40%	20%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%					80%					20%								100%
Surface Class Count	0	0	0	2	0	0	0	0	3	3	3	0	0	0	0	0	0	0	11
Surface Class Percent	0%	0%	0%	18%	0%	0%	0%	0%	27%	27%	27%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
4.50	0.50	НР
25.40	6.00	N60L

Average HP Average N_{60L}

RAMP C-7 (WB-490 to 7th St)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Ramp C-7 (WB-490 to 7th St) -Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By: Date prepared:

Derar M. Tarawneh Friday, March 3, 2023

Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

brendan.andrews@neasinc.com

NO. OF BORINGS:

2





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-033-0-21	Ramp C-7	84+46	21	LT	CME 45B	82	656.6	655.5	1.1 C
2	B-034-0-21	Ramp C-7	82+28	16	RT	CME 45B	82	663.4	662.4	1.0 C

V. 14.5

#	Boring	ing Sample		nple pth	_	grade pth		dard tration	НР		Pl	hysica	al Chara	cteristics		Mo	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate ar (Item	•	Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	0.4	1.9	18		4.5	29	22	7	60	20	80	17	17	A-4b	8	733	A-4b				
	033-0	SS-2	3.0	4.5	1.9	3.4	15		4.5	29	22	7	58	20	78	16	17	A-4b	8		A-4b		40''		
	21	SS-3	4.5	6.0	3.4	4.9	14		4.5							21	10	A-4b	8						
		SS-4	6.0	7.5	4.9	6.4	14	14	4.5							17	10	A-4b	8						
2	В	SS-1	1.5	3.0	0.5	2.0	23						15	6	21	9	6	A-1-b	0	1413					
	034-0	SS-2	3.0	4.5	2.0	3.5	20						10	4	14	8	6	A-1-a	0						
	21	SS-3	4.5	6.0	3.5	5.0	18		4.5							15	10	A-4a	8						
		SS-4	6.0	7.5	5.0	6.5	25	18								7	6	A-1-a							



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 2

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

C	Chemical Stabilization Optio	ns
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	NA

Excavate and Repl	ace								
Stabilization Options									
Global Geotextile									
Average(N60L):	12"								
Average(HP):	0''								
Global Geogrid									
Average(N60L):	0''								
Average(HP): 0"									

Design CBR	7
---------------	---

% Sampl	es within	6 feet of subgr	ade
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%
N ₆₀ < 12	0%	0.5 < HP ≤ 1	0%
12 ≤ N ₆₀ < 15	25%	1 < HP ≤ 2	0%
N ₆₀ ≥ 20	38%	HP > 2	63%
M+	0%		
Rock	0%		
Unsuitable	50%		

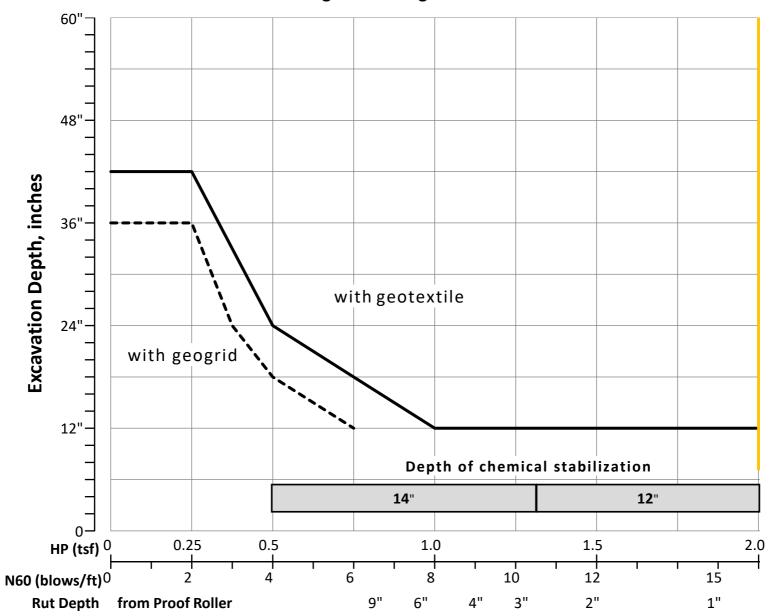
Excavate and Replace at Surface										
Average	0''									
Maximum	0"									
Minimum	0"									

% Proposed Subgrade Su	rface
Unstable & Unsuitable	50%
Unstable	0%
Unsuitable	50%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{OPT}	GI
Average	18	16	4.50	29	22	7	36	13	48	14	10	6
Maximum	25	18	4.50	29	22	7	60	20	80	21	17	8
Minimum	14	14	4.50	29	22	7	10	4	14	7	6	0

	Classification Counts by Sample																		
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	2	1	0	0	0	0	0	0	1	4	0	0	0	0	0	0	0	8
Percent	0%	25%	13%	0%	0%	0%	0%	0%	0%	13%	50%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%		50%								50%								100%
Surface Class Count	0	1	1	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	4
Surface Class Percent	0%	25%	25%	0%	0%	0%	0%	0%	0%	0%	50%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
4.50	0.50	HР
16.00	6.00	N60L

Average HP Average N_{60L}

RAMP B-C (Rockefeller Ave to WB-490)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Ramp B-C (Rockefeller Ave to WB-490) -Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By: Date prepared:

Derar M. Tarawneh Friday, March 3, 2023

Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

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NO. OF BORINGS:

2



#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-035-0-21	Ramp B-C	17+69	31	LT	CME 45B	82	667.4	666.1	1.3 C
2	B-036-0-21	Ramp B-C	15+10	2	LT	CME 45B	82	665.1	663.9	1.2 C

V. 14.5

#	Boring	Sample		nple pth	1 -	grade pth		dard tration	НР		Pl	hysica	al Chara	cteristics		Mo	isture	Ohio	DOT	Sulfate Content	Proble	Problem		id Replace 204)	Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	ы	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	0.2	1.7	12						20	5	25	15	8	A-3a	0	153					
	035-0	SS-2	3.0	4.5	1.7	3.2	11						24	5	29	11	8	A-3a	0						
	21	SS-3	4.5	6.0	3.2	4.7	11									11	8	A-3a	0						
		SS-4	6.0	7.5	4.7	6.2	12	11								11	8	A-3a	0						
2	В	SS-1	1.5	3.0	0.3	1.8	25						29	10	39	9	10	A-4a	6	367					
	036-0	SS-2	3.0	4.5	1.8	3.3	19						26	7	33	9	8	A-3a	0						
	21	SS-3	4.5	6.0	3.3	4.8	29									9	10	A-4a	8						
		SS-4	6.0	7.5	4.8	6.3	31	19								10	10	A-4a	8						



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 2

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

(Chemical Stabilization Options										
320	320 Rubblize & Roll										
206	206 Cement Stabilization										
	Lime Stabilization	Option									
206	Depth	12"									

ace
ons
12"
0''
0''
0''

Design CBR	9
---------------	---

% Sampl	% Samples within 6 feet of subgrade													
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%											
N ₆₀ < 12	25%	0.5 < HP ≤ 1	0%											
12 ≤ N ₆₀ < 15	25%	1 < HP ≤ 2	0%											
N ₆₀ ≥ 20	38%	HP > 2	0%											
M+	0%													
Rock	0%													
Unsuitable	0%													

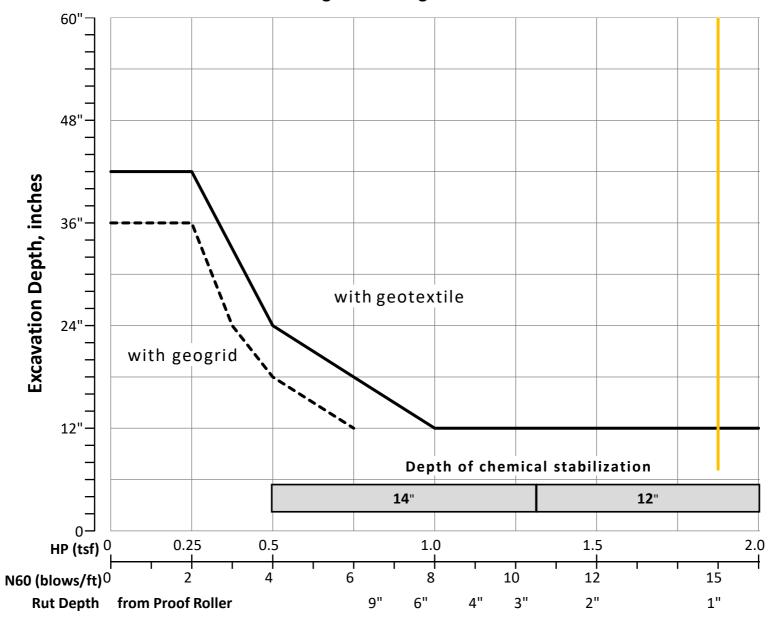
Excavate and Replace at Surface										
Average	0"									
Maximum	0"									
Minimum	0"									

% Proposed Subgrade Surface										
Unstable & Unsuitable	0%									
Unstable	0%									
Unsuitable	0%									

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{OPT}	GI
Average	19	15					25	7	32	11	9	3
Maximum	31	19	0.00	0	0	0	29	10	39	15	10	8
Minimum	11	11	0.00	0	0	0	20	5	25	9	8	0

					Class	ificat	ion C	ount	s by	Sam	ple								
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	0	0	0	0	0	0	5	3	0	0	0	0	0	0	0	0	8
Percent	0%	0%	0%	0%	0%	0%	0%	0%	63%	38%	0%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%		100% 0%											100%					
Surface Class Count	0	0	0	0	0	0	0	0	3	1	0	0	0	0	0	0	0	0	4
Surface Class Percent	0%	0%	0%	0%	0%	0%	0%	0%	75%	25%	0%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
	20.00	✓ HP
15.00	6.00	N60L

RAMP N-W (SB-77 to WB-490)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Ramp N-W (SB-77 to WB-490) -Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By: Date prepared:

Derar M. Tarawneh Friday, March 3, 2023

Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

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NO. OF BORINGS:

4





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-037-0-21	Ramp N-W	120+53	8	LT	CME 45B	82	651.4	650.3	1.0 C
2	B-038-0-21	Ramp N-W	124+26	1	LT	CME 45B	82	649.1	647.5	1.6 C
3	B-039-0-21	Ramp N-W	127+74	4	LT	CME 45B	82	657.9	657.0	0.9 C
4	B-040-0-21	Ramp N-W	131+20	7	LT	CME 45B	82	669.4	668.7	0.7 C

V. 14.5

1/18/2019

#	Boring	Sample	Sam Dej	-		grade pth		dard ration	НР		Pl	hysic	al Chara	cteristics		Mo	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate ar		Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	0.5	2.0	27						18	6	24	6	8	A-3a	0	860					
	037-0	SS-2	3.0	4.5	2.0	3.5	22						17	6	23	7	8	A-3a	0						
	21	SS-3	4.5	6.0	3.5	5.0	23									5	8	A-3a	0						
		SS-4	6.0	7.5	5.0	6.5	23	22								6	8	A-3a	0						
2	В	SS-1	1.5	3.0	-0.1	1.4	15						14	5	19	11	8	A-3a	0	340					
	038-0	SS-2	3.0	4.5	1.4	2.9	15						19	5	24	11	8	A-3a	0						
	21	SS-3	4.5	6.0	2.9	4.4	14									11	8	A-3a	0						
		SS-4	6.0	7.5	4.4	5.9	20	14								11	8	A-3a	0						
3	В	SS-1	1.5	3.0	0.6	2.1	22						7	1	8	7	6	A-1-b	0	793					
	039-0	SS-2	3.0	4.5	2.1	3.6	20						7	2	9	4	6	A-1-b	0						
	21	SS-3	4.5	6.0	3.6	5.1	18									5	6	A-1-b	0						
		SS-4	6.0	7.5	5.1	6.6	16	16								4	6	A-1-b							
4	В	SS-1	1.5	3.0	0.8	2.3	41						6	2	8	9	8	A-3	0	413					
	040-0	SS-2	3.0	4.5	2.3	3.8	11						5	1	6	5	8	A-3	0						
	21	SS-3	4.5	6.0	3.8	5.3	14									7	8	A-3	0						
		SS-4	6.0	7.5	5.3	6.8	14	11								4	8	A-3							



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 4

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

(Chemical Stabilization Options								
320	320 Rubblize & Roll Optic								
206	Cement Stabilization	No							
	Lime Stabilization	Option							
206	Depth	12"							

Excavate and Repl	ace							
Stabilization Option	Stabilization Options							
Global Geotextile								
Average(N60L):	12"							
Override(HP):	0"							
Global Geogrid								
Average(N60L):	0''							
Override(HP):	0"							

Design CBR	13
---------------	----

% Sampl	% Samples within 6 feet of subgrade									
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%							
N ₆₀ < 12	6%	0.5 < HP ≤ 1	0%							
12 ≤ N ₆₀ < 15	19%	1 < HP ≤ 2	0%							
N ₆₀ ≥ 20	50%	HP > 2	0%							
M+	0%									
Rock	0%									
Unsuitable	0%									

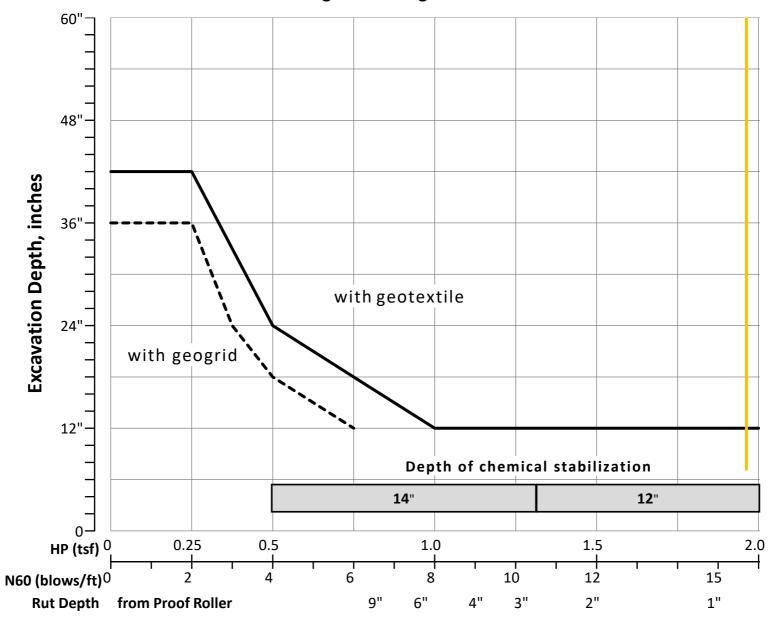
Excavate and Replace at Surface							
Average	0''						
Maximum	0"						
Minimum 0"							

% Proposed Subgrade Surface							
Unstable & Unsuitable	0%						
Unstable	0%						
Unsuitable	0%						

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{OPT}	GI
Average	20	16					12	4	15	7	8	0
Maximum	41	22	0.00	0	0	0	19	6	24	11	8	0
Minimum	11	11	0.00	0	0	0	5	1	6	4	6	0

	Classification Counts by Sample																		
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	4	0	0	0	0	4	8	0	0	0	0	0	0	0	0	0	16
Percent	0%	0%	25%	0%	0%	0%	0%	25%	50%	0%	0%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%					100%					0%								100%
Surface Class Count	0	0	2	0	0	0	0	2	4	0	0	0	0	0	0	0	0	0	8
Surface Class Percent	0%	0%	25%	0%	0%	0%	0%	25%	50%	0%	0%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
	20.00	✓ HP
15.75	6.00	N60L

RAMP W-N (EB-490 to NB-77)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Ramp W-N (EB-490 to NB-77) -Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By: Date prepared:

Derar M. Tarawneh Friday, March 3, 2023

Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

brendan.andrews@neasinc.com

NO. OF BORINGS:

3





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-041-0-21	Ramp W-N	623+88	12	LT	CME 45B	82	640.6	638.4	2.2 C
2	B-042-0-21	Ramp W-N	627+30	0	RT	CME 45B	82	639.4	638.8	0.6 C
3	B-043-0-21	Ramp W-N	630+38	4	LT	CME 45B	82	641.4	640.5	0.9 C

V. 14.5

1/18/2019

#	Boring	Sample		iple pth	_	grade pth	Stan Penet	dard ration	НР		Pl	hysic	al Chara	cteristics		Mo	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate ar (Item	•	Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	-0.7	0.8	29						11	2	13	8	6	A-1-b	0	1300					
	041-0	SS-2	3.0	4.5	0.8	2.3	26						10	2	12	10	6	A-1-b	0						
	21	SS-3	4.5	6.0	2.3	3.8	29									5	6	A-1-b	0						
		SS-4	6.0	7.5	3.8	5.3	30	26								4	6	A-1-b	0						
2	В	SS-1	1.5	3.0	0.9	2.4	50						17	5	22	10	6	A-1-b	0	933					
	042-0	SS-2	3.0	4.5	2.4	3.9	41						18	5	23	11	8	A-3a	0						
	21	SS-3	4.5	6.0	3.9	5.4	23									12	8	A-3a	0						
		SS-4	6.0	7.5	5.4	6.9	23	23								10	8	A-3a							
3	В	SS-1	1.5	3.0	0.6	2.1	27						19	8	27	10	8	A-3a	0	2800					
	043-0	SS-2	3.0	4.5	2.1	3.6	27						17	6	23	30	8	A-3a	0						
	21	SS-3	4.5	6.0	3.6	5.1	31									6	8	A-3a	0						
		SS-4	6.0	7.5	5.1	6.6	31	27								5	8	A-3a							



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 3

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

(Chemical Stabilization Option	ıs
320	Rubblize & Roll	Option
206	Cement Stabilization	No
	Lime Stabilization	Option
206	Depth	NA

Excavate and Repla	ace								
Stabilization Options									
Global Geotextile									
Average(N60L):	0"								
Override(HP):	0"								
Global Geogrid									
Average(N60L):	0"								
Override(HP):	0''								

Design CBR	13
---------------	----

% Sampl	es within	6 feet of subgr	ade
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%
N ₆₀ < 12	0%	0.5 < HP ≤ 1	0%
12 ≤ N ₆₀ < 15	0%	1 < HP ≤ 2	0%
N ₆₀ ≥ 20	100%	HP > 2	0%
M+	0%		
Rock	0%		
Unsuitable	0%		

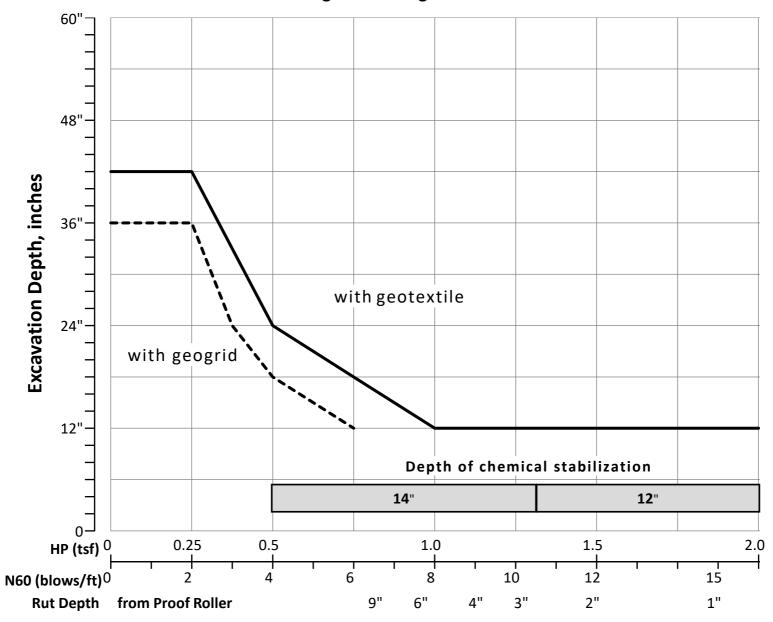
Excavate and Repl at Surface	ace
Average	0"
Maximum	0"
Minimum	0"

% Proposed Subgrade Su	rface
Unstable & Unsuitable	0%
Unstable	0%
Unsuitable	0%

	N ₆₀	N _{60L}	НР	LL	PL	PI	Silt	Clay	P 200	M _c	M _{OPT}	GI
Average	31	25					15	5	20	10	7	0
Maximum	50	27	0.00	0	0	0	19	8	27	30	8	0
Minimum	23	23	0.00	0	0	0	10	2	12	4	6	0

	Classification Counts by Sample																		
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	5	0	0	0	0	0	7	0	0	0	0	0	0	0	0	0	12
Percent	0%	0%	42%	0%	0%	0%	0%	0%	58%	0%	0%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%					100%								0	%				100%
Surface Class Count	0	0	4	0	0	0	0	0	3	0	0	0	0	0	0	0	0	0	7
Surface Class Percent	0%	0%	57%	0%	0%	0%	0%	0%	43%	0%	0%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
	20.00	✓ HP
25.33	6.00	N60L

RAMP C-B (EB-490 to Broadway Ave)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Ramp C-B (EB-490 to Broadway Ave) -Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By: Date prepared:

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Brendan P. Andrews 2868 East Kemper Rd. Cincinnati, OH 45241

(920) 427-0671

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NO. OF BORINGS:

2





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-044-0-21	Ramp C-B	15+45	1	RT	CME 45B	82	670.6	669.9	0.8 C
2	B-045-0-21	Ramp C-B	16+50	5	RT	CME 45B	82	674.0	673.3	0.7 C

V. 14.5

1/18/2019

#	Boring	Sample	Sam De _l	•	Subg De _l		Stan Penet		НР		P	hysic	sical Characteristics Moisture Ohio DOT		DOT	Sulfate Content	Problem		Excavate an	•	Recommendation (Enter depth in				
"			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	0.8	2.3	14						14	5	19	6	6	A-1-b	0	1080					
	044-0	SS-2	3.0	4.5	2.3	3.8	12									8	6	A-1-b	0						
	21	SS-3	4.5	6.0	3.8	5.3	18						13	5	18	8	6	A-1-b	0						
		SS-4	6.0	7.5	5.3	6.8	14	12								9	6	A-1-b							
2	В	SS-1	1.5	3.0	0.8	2.3	15						9	3	12	4	6	A-1-a	0	340					
	045-0	SS-2	3.0	4.5	2.3	3.8	11						21	7	28	14	8	A-3a	0						
	21	SS-3	4.5	6.0	3.8	5.3	14									12	8	A-3a	0						
		SS-4	6.0	7.5	5.3	6.8	12	11								9	8	A-3a							



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 2

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

(Chemical Stabilization Option	ıs												
320	320 Rubblize & Roll No													
206	206 Cement Stabilization													
	Lime Stabilization	Option												
206	Depth	12"												

ace
ons
12"
0''
0''
0''

Design CBR	13
---------------	----

% Sampl	% Samples within 6 feet of subgrade														
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%												
N ₆₀ < 12	13%	0.5 < HP ≤ 1	0%												
12 ≤ N ₆₀ < 15	63%	1 < HP ≤ 2	0%												
N ₆₀ ≥ 20	0%	HP > 2	0%												
M+	0%														
Rock	0%														
Unsuitable	0%														

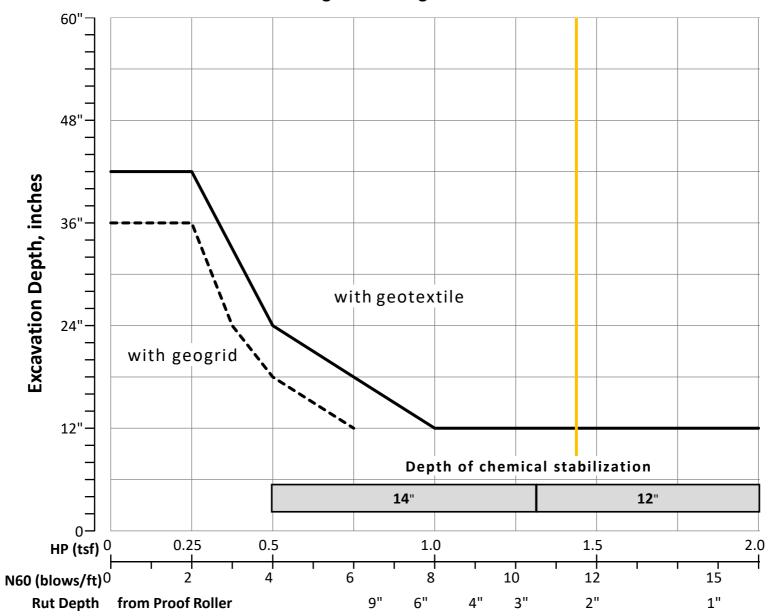
Excavate and Repl at Surface	ace
Average	0"
Maximum	0"
Minimum	0"

% Proposed Subgrade Su	rface
Unstable & Unsuitable	0%
Unstable	0%
Unsuitable	0%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{OPT}	GI
Average	14	12					14	5	19	9	7	0
Maximum	18	12	0.00	0	0	0	21	7	28	14	8	0
Minimum	11	11	0.00	0	0	0	9	3	12	4	6	0

					Class	ificat	ion C	ount	s by	Sam	ple								
ODOT Class	ODOT Class Rock A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-3 A-3a A-4a A-4b A-5 A-6a A-6b A-7-5 A-7-6 A-8a A-8b															Totals			
Count	0	1	4	0	0	0	0	0	3	0	0	0	0	0	0	0	0	0	8
Percent		13%	50%	0%	0%	0%	0%	0%	38%	0%	0%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%		100% 0%														100%		
Surface Class Count	0	1	2	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	4
Surface Class Percent	0%	25%	50%	0%	0%	0%	0%	0%	25%	0%	0%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
	20.00	✓ HP
11.50	6.00	N60L

RAMP S-E (NB-77 to EB-490)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Ramp S-E (NB-77 to EB-490) -Interstate Route 490 Major Rehabilitation

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NO. OF BORINGS:

4





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-046-0-21	Ramp S-E	335+69	7	RT	CME 45B	82	658.9	657.3	1.6 C
2	B-047-0-21	Ramp S-E	339+21	4	RT	CME 45B	82	649.5	647.9	1.5 C
3	B-048-0-21	Ramp S-E	342+76	3	RT	CME 45B	82	640.4	637.7	2.8 C
4	B-049-0-21	Ramp S-E	346+29	6	RT	CME 45B	82	643.2	643.5	0.3 F

V. 14.5

1/18/2019

#	Boring	Sample	San De	-	1	grade pth		dard ration	НР		Pl	hysic	al Chara	cteristics		Mo	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate ar		Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	-0.1	1.4	38						14	5	19	6	6	A-1-b	0	253					
	046-0	SS-2A	3.0	4.5	1.4	2.9	25									6	6	A-1-b	0						
	21	SS-2B	4.5	6.0	2.9	4.4	25		4.5	25	19	6	67	29	96	15	14	A-4b	8						
		SS-3	6.0	7.5	4.4	5.9	26	25	4.5							16	10	A-4b	8						
2	В	SS-1	1.5	3.0	0.0	1.5	26						13	5	18	12	8	A-3a	0	67					
	047-0	SS-2	3.0	4.5	1.5	3.0	19						21	10	31	11	8	A-3a	0						
	21	SS-3	4.5	6.0	3.0	4.5	15									13	8	A-3a	0						
		SS-4	6.0	7.5	4.5	6.0	12	12								13	8	A-3a	0						
3	В	SS-1	1.5	3.0	-1.3	0.3	30						12	3	15	9	6	A-1-b	0	2387					
	048-0	SS-2	3.0	4.5	0.3	1.8	20						23	6	29	10	8	A-3a	0						
	21	SS-3	4.5	6.0	1.8	3.3	20									12	6	A-1-b	0						
		SS-4	6.0	7.5	3.3	4.8	12	12								10	8	A-3a	0						
4	В	SS-1	1.5	3.0	1.8	3.3	15						14	2	16	23	8	A-3a	0	20					
	049-0	SS-2	3.0	4.5	3.3	4.8	10						26	2	28	20	8	A-3a	0						
	21	SS-3	4.5	6.0	4.8	6.3	10									27	8	A-3a	0						
		SS-4	6.0	7.5	6.3	7.8	10	10								20	8	A-3a							



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 4

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

(Chemical Stabilization Options									
320	Rubblize & Roll	Option								
206	Cement Stabilization	Option								
	Lime Stabilization	No								
206	Depth	12"								

Excavate and Replace Stabilization Options							
Global Geotextile Average(N60L): Average(HP):	12" 0"						
Global Geogrid Average(N60L): Average(HP):	0" 0"						

Design CBR	12
---------------	----

% Samples within 6 feet of subgrade									
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%						
N ₆₀ < 12	13%	0.5 < HP ≤ 1	0%						
12 ≤ N ₆₀ < 15	13%	1 < HP ≤ 2	0%						
N ₆₀ ≥ 20	53%	HP > 2	13%						
M+	0%								
Rock	0%								
Unsuitable	13%								

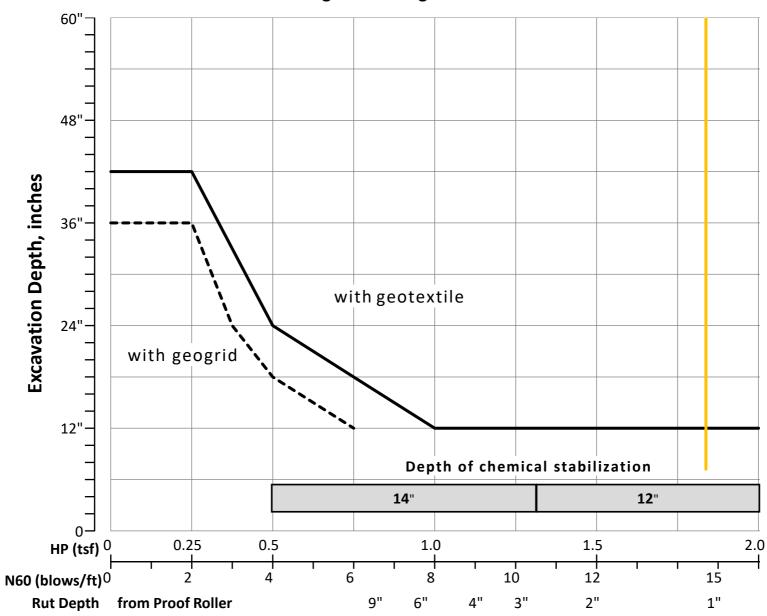
Excavate and Replace at Surface							
Average	0"						
Maximum	0"						
Minimum	0"						

% Proposed Subgrade Surface							
Unstable & Unsuitable	0%						
Unstable	0%						
Unsuitable	0%						

	N ₆₀	N _{60L}	НР	LL	PL	PI	Silt	Clay	P 200	M_{c}	M _{OPT}	GI
Average	20	15	4.50	25	19	6	24	8	32	14	8	1
Maximum	38	25	4.50	25	19	6	67	29	96	27	14	8
Minimum	10	10	4.50	25	19	6	12	2	15	6	6	0

	Classification Counts by Sample																		
ODOT Class	ODOT Class Rock A-1-a A-1-b A-2-4 A-2-5 A-2-6 A-2-7 A-3 A-3a A-4a A-4b A-5 A-6a A-6b A-7-5 A-7-6 A-8a A-8b														Totals				
Count	0	0	4	0	0	0	0	0	10	0	2	0	0	0	0	0	0	0	16
Percent	0%	0%	25%	0%	0%	0%	0%	0%	63%	0%	13%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%					88%								13	3%				100%
Surface Class Count	0	0	4	0	0	0	0	0	4	0	0	0	0	0	0	0	0	0	8
Surface Class Percent	0%	0%	50%	0%	0%	0%	0%	0%	50%	0%	0%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
4.50	0.50	HР
14.75	6.00	N60L

RAMP E-N (WB-490 to NB-77)



OHIO DEPARTMENT OF TRANSPORTATION

OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES Geotechnical Bulletin GB1

CUY-490-0.00 PID 107408

Ramp E-N (WB-490 to NB-77) -Interstate Route 490 Major Rehabilitation

NEAS, Inc.

Prepared By: Date prepared:

Derar M. Tarawneh Friday, March 3, 2023

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NO. OF BORINGS:

4





#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-050-0-21	Ramp E-N	744+41	4	LT	CME 45B	82	640.2	638.8	1.4 C
2	B-051-0-21	Ramp E-N	740+80	2	RT	CME 45B	82	636.2	634.3	1.8 C
3	B-052-0-21	Ramp E-N	737+33	4	LT	CME 45B	82	643.4	642.6	0.8 C
4	B-053-0-21	Ramp E-N	733+99	4	LT	CME 45B	82	657.0	655.9	1.1 C

V. 14.5

1/18/2019

#	Boring	Sample	Sam De _l	-	_	grade pth	Stan Penet	dard ration	НР		Р	hysic	al Chara	cteristics		Mo	isture	Ohio	DOT	Sulfate Content	Proble	m	Excavate an		Recommendation (Enter depth in
			From	То	From	То	N ₆₀	N _{60L}	(tsf)	LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI	(ppm)	Unsuitable	Unstable	Unsuitable	Unstable	inches)
1	В	SS-1	1.5	3.0	0.1	1.6	29						12	1	13	16	6	A-1-b	0	1100					
	050-0	SS-2	3.0	4.5	1.6	3.1	25									14	6	A-1-b	0						
	21	SS-3	4.5	6.0	3.1	4.6	33						11	1	12	45	6	A-1-b	0						
		SS-4	6.0	7.5	4.6	6.1	29	25								41	6	A-1-b	0						
2	В	SS-1	1.5	3.0	-0.3	1.2	39						14	3	17	9	6	A-1-b	0	3000					
	051-0	SS-2	3.0	4.5	1.2	2.7	23						30	7	37	10	10	A-4a	5						
	21	SS-3	4.5	6.0	2.7	4.2	26									7	10	A-4a	8						
		SS-4A	6.0	7.0	4.2	5.2	38	23								14	10	A-4a	8						
3	В	SS-1	1.5	3.0	0.7	2.2	31						9	3	12	6	8	A-3a	0	40					
	052-0	SS-2	3.0	4.5	2.2	3.7	26						12	5	17	13	8	A-3a	0						
	21	SS-3	4.5	6.0	3.7	5.2	16									7	8	A-3a	0						
		SS-4	6.0	7.5	5.2	6.7	14	14								7	8	A-3a							
4	В	SS-1	1.5	3.0	0.4	1.9	22		4.5	22	15	7	25	13	38	12	10	A-4a	1	347					
	053-0	SS-2	3.0	4.5	1.9	3.4	20			19	14	5	27	14	41	10	10	A-4a	1						
	21	SS-3	4.5	6.0	3.4	4.9	53									8	8	A-3a	0						
		SS-4	6.0	7.5	4.9	6.4	56	20								8	8	A-3a	0						



PID: PID 107408

County-Route-Section: CUY-490-0.00

No. of Borings: 4

Geotechnical Consultant: NEAS, Inc.

Prepared By: Derar M. Tarawneh

Date prepared: 3/3/2023

C	Chemical Stabilization Options									
320	320 Rubblize & Roll Opt									
206	Cement Stabilization	Option								
	Lime Stabilization	No								
206	Depth	NA								

Excavate and Replace							
Stabilization Option	Stabilization Options						
Global Geotextile							
Average(N60L): 0"							
Average(HP): 0"							
Global Geogrid							
Average(N60L): 0"							
Average(HP): 0"							

Design CBR	11
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% Samples within 6 feet of subgrade											
N ₆₀ ≤ 5	N ₆₀ ≤ 5 0% HP ≤ 0.5 09										
N ₆₀ < 12	0%	0.5 < HP ≤ 1	0%								
12 ≤ N ₆₀ < 15	6%	1 < HP ≤ 2	0%								
N ₆₀ ≥ 20	88%	HP > 2	6%								
M+	0%										
Rock	0%		·								
Unsuitable	0%										

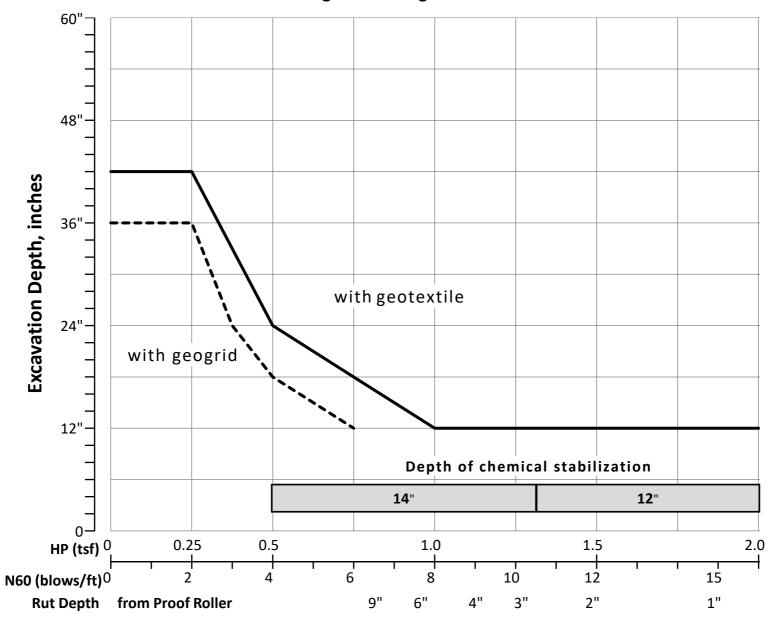
Excavate and Replace at Surface					
Average	0"				
Maximum	0"				
Minimum	0"				

% Proposed Subgrade Surface						
Unstable & Unsuitable	0%					
Unstable	0%					
Unsuitable	0%					

	N ₆₀	N _{60L}	НР	LL	PL	PI	Silt	Clay	P 200	M _c	M _{OPT}	GI
Average	30	21	4.50	21	15	6	18	6	23	14	8	2
Maximum	56	25	4.50	22	15	7	30	14	41	45	10	8
Minimum	14	14	4.50	19	14	5	9	1	12	6	6	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	5	0	0	0	0	0	6	5	0	0	0	0	0	0	0	0	16
Percent	0%	0%	31%	0%	0%	0%	0%	0%	38%	31%	0%	0%	0%	0%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%		100% 0%									100%							
Surface Class Count	0	0	3	0	0	0	0	0	2	4	0	0	0	0	0	0	0	0	9
Surface Class Percent	0%	0%	33%	0%	0%	0%	0%	0%	22%	44%	0%	0%	0%	0%	0%	0%	0%	0%	100%

GB1 Figure B – Subgrade Stabilization



OVERRIDE TABLE

Calculated Average	New Values	Check to Override
4.50	0.50	HР
20.50	6.00	N60L