

LUC-23 - BrR Load Rating Background Calcs

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Date: 8/24/2022

Checker: F. Getz

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This sheet is give the load rating assumptions and inputs.

This sheet is in accordance with AISC Manual for Steel Construction, 15th Ed.

User inputs are highlighted in - Yellow Sheet assumption are highlighted in - Blue

Sheet checks are highlighted in - Green Inputs from other files are highlighted in purple - Purple

Diaphragm Weights

1958 Interior Diaphragm

$$\text{Angle}_{wt} := 6.1 \cdot \text{plf}$$

$$\text{Angle}_{Length} := (7 \cdot \text{ft} + 3 \cdot \text{in}) + 2 \cdot \left[(36 \cdot \text{in})^2 + (7 \cdot \text{ft} + 3 \cdot \text{in})^2 \right]^{0.5} = 22.942 \text{ ft}$$

$$\text{Int}_{1958_wt} := \text{Angle}_{wt} \cdot \text{Angle}_{Length} = 0.14 \cdot \text{kip}$$

1958 End Diaphragm

$$\text{Angle}_{wt} := 8.2 \cdot \text{plf}$$

$$\text{Angle}_{Length} := \left(\frac{7 \cdot \text{ft} + 3 \cdot \text{in}}{\cos(3.175 \cdot \text{deg})} \right) + 2 \cdot \left[(36 \cdot \text{in})^2 + \left(\frac{1}{2} \cdot \frac{7 \cdot \text{ft} + 3 \cdot \text{in}}{\cos(3.175 \cdot \text{deg})} \right)^2 \right]^{0.5} = 16.681 \text{ ft}$$

$$\text{End}_{1958_wt} := \text{Angle}_{wt} \cdot \text{Angle}_{Length} + \left(\frac{3}{8} \cdot \text{in} \right) \cdot (8 \cdot \text{in}) \cdot (12 \cdot \text{in}) \cdot 490 \cdot \text{pcf} = 0.147 \cdot \text{kip}$$

2022 End Diaphragm

$$\text{Channel}_{wt} := 42.7 \cdot \text{plf}$$

$$\text{Channel}_{Length} := \frac{7 \cdot \text{ft} + 3 \cdot \text{in}}{\cos(3.175 \cdot \text{deg})} = 7.261 \text{ ft}$$

$$\text{Stiffener_vol} := \left(\frac{1}{2} \cdot \text{in} \right) \cdot \left(8 \frac{1}{4} \cdot \text{in} \right) \cdot (34 \cdot \text{in})$$

$$\text{End}_{2022_wt} := \text{Channel}_{wt} \cdot \text{Channel}_{Length} + 2 \cdot \text{Stiffener_vol} \cdot 490 \cdot \text{pcf} = 0.39 \cdot \text{kip}$$

2022 Interior Diaphragm

$$\text{Angle}_{wt} := 8.5 \cdot \text{plf}$$

$$\text{Angle}_{Length} := (6 \cdot \text{ft} + 0 \cdot \text{in}) + 2 \cdot \left[(36 \cdot \text{in})^2 + (6 \cdot \text{ft} + 0 \cdot \text{in})^2 \right]^{0.5} = 19.416 \text{ ft}$$

$$\text{Stiffener_vol} := \left(\frac{3}{8} \cdot \text{in} \right) \cdot (7.87 \cdot \text{in}) \cdot (34 \cdot \text{in})$$

$$\text{Filler_PL_Vol} := \left(\frac{3}{8} \cdot \text{in} \right) \cdot (12 \cdot \text{in}) \cdot (4 \cdot \text{in})$$

$$\text{Int}_{2022_wt} := \text{Angle}_{wt} \cdot \text{Angle}_{Length} + (2 \cdot \text{Stiffener_vol} + \text{Filler_PL_Vol}) \cdot 490 \cdot \text{pcf} = 0.227 \cdot \text{kip}$$

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Checker: R. Brinkman

Date: 6/29/2023

$$\gamma_{\text{conc}} := 150 \cdot \text{pcf}$$

$$\gamma_{\text{steel}} := 490 \cdot \text{pcf}$$

$$\text{Total_Span_Length} := 2 \cdot (52 \cdot \text{ft} + 86.5 \cdot \text{ft}) = 277 \text{ ft}$$

*Program defines the loads from CL to CL of Bearings
So use this for determine loads*

BR-2-15

ODOT Standard Drawing - BR-2-15

$$\text{HSS4x3x0_25}_{\text{wt}} := 10.48 \cdot \text{plf}$$

$$\text{HSS4x4x0_188}_{\text{wt}} := 9.40 \cdot \text{plf}$$

$$\text{Post}_{\text{height}} := 1 \cdot \text{ft} + 6 \cdot \text{in} - 0.75 \cdot \text{in} = 17.25 \cdot \text{in}$$

$$\text{BR_Base_Plate}_{\text{wt}} := (10.5 \cdot \text{in} \cdot 10.5 \cdot \text{in} \cdot 0.75 \cdot \text{in}) \cdot \gamma_{\text{steel}} = 0.023 \cdot \text{kip}$$

$$\text{Hardware_Increase} := 105 \cdot \%$$

*Increase by 5% to account for
bolts splice plates, etc.*

$$\text{Total_Posts_South} := (24) \cdot 2 = 48$$

$$\text{South_BR}_{\text{wt_total}} := \left[2 \cdot \text{HSS4x3x0_25}_{\text{wt}} \dots + \left(\text{HSS4x4x0_188}_{\text{wt}} \cdot \text{Post}_{\text{height}} \dots + \text{BR_Base_Plate}_{\text{wt}} \right) \cdot \frac{\text{Total_Posts_South}}{\text{Total_Span_Length}} \right] \cdot \text{Hardware_Increase} = 0.029 \cdot \text{klf}$$

BR-2-15 - Modified

The middle barrier has tubes on both sides

$$\text{Backing_Plate}_{\text{wt}} := (8 \cdot \text{in} \cdot 3 \cdot \text{in} \cdot 0.25 \cdot \text{in}) \cdot \gamma_{\text{steel}} = 0.002 \cdot \text{kip}$$

$$\text{Total_Posts_Middle} := (22) \cdot 2 = 44$$

$$\text{Middle_BR}_{\text{wt_total}} := \left[4 \cdot \text{HSS4x3x0_25}_{\text{wt}} \dots + \left(\text{HSS4x4x0_188}_{\text{wt}} \cdot \text{Post}_{\text{height}} \dots + \text{BR_Base_Plate}_{\text{wt}} + 2 \cdot \text{Backing_Plate}_{\text{wt}} \right) \cdot \frac{\text{Total_Posts_South}}{\text{Total_Span_Length}} \right] \cdot \text{Hardware_Increase} = 0.051 \cdot \text{klf}$$

Fence

$$\text{Rail}_{\text{wt}} := 7.93 \cdot \text{plf}$$

HSS 3.5 x 2 x 1/4

$$\text{Post}_{\text{wt}} := 17.20 \cdot \text{plf}$$

HSS 3.5 x 2 x 3/8

$$\text{Post}_{\text{Ht}} := 6 \cdot \text{ft} - 0.625 \cdot \text{in} = 5.948 \text{ ft}$$

$$\text{Picket}_{\text{wt}} := 1 \cdot \text{in} \cdot 1 \cdot \text{in} \cdot \gamma_{\text{steel}} = 3.403 \cdot \text{plf}$$

$$\text{Picket}_{\text{ht}} := 4 \text{ ft} + 6 \text{ in}$$

$$\text{Pickets}_{\text{Max}_{\text{Space}}} := 4 \cdot \text{in}$$

$$\text{No}_{\text{Pickets}} := \text{round}(\text{Total}_{\text{Span}_{\text{Length}}} \div \text{Pickets}_{\text{Max}_{\text{Space}}}, 0) = 831$$

Approximate by dividing the max spacing by the total span length. Some pickets will be closer spaced, and there are pilasters but this is a good approximation

$$\text{No}_{\text{Fence}_{\text{Posts}}} := (20) \cdot 2 = 40$$

$$\text{Fence}_{\text{Base}_{\text{Plate}}_{\text{wt}}} := (8 \cdot \text{in} \cdot 9 \cdot \text{in} \cdot 0.625 \cdot \text{in}) \cdot \gamma_{\text{steel}}$$

Same for both North and South

$$\text{Mesh}_{\text{wt}} := 2 \cdot \text{psf}$$

$$\text{Mesh}_{\text{ht}} := \text{Picket}_{\text{ht}} = 4.5 \text{ ft}$$

$$\text{Total}_{\text{Fence}_{\text{wt}_{\text{total}}}} := \left[3 \cdot \text{Rail}_{\text{wt}} + \left(\text{Post}_{\text{wt}} \cdot \text{Post}_{\text{Ht}} + \text{Fence}_{\text{Base}_{\text{Plate}}_{\text{wt}}} \right) \cdot \frac{\text{No}_{\text{Fence}_{\text{Posts}}}}{\text{Total}_{\text{Span}_{\text{Length}}}} + \left(\text{Picket}_{\text{wt}} \cdot \text{Picket}_{\text{ht}} \right) \cdot \frac{\text{No}_{\text{Pickets}}}{\text{Total}_{\text{Span}_{\text{Length}}}} + \text{Mesh}_{\text{wt}} \cdot \text{Mesh}_{\text{ht}} \right] \cdot \text{Hardware}_{\text{Increase}} = 0.1 \cdot \text{klf}$$

Total South Barrier

$$\text{South}_{\text{Conc}_{\text{Barrier}}_{\text{wt}}} := [(1.5 \cdot \text{ft} \cdot 1.5 \cdot \text{ft}) + 6 \cdot \text{in} \cdot (1 \cdot \text{ft} + 8 \cdot \text{in})] \cdot \gamma_{\text{conc}} = 0.462 \cdot \text{klf}$$

$$\text{South}_{\text{Total}_{\text{Barrier}}_{\text{wt}}} := \text{South}_{\text{Conc}_{\text{Barrier}}_{\text{wt}}} + \text{South}_{\text{BR}_{\text{wt}_{\text{total}}}} + \text{Total}_{\text{Fence}_{\text{wt}_{\text{total}}}} = 0.591 \cdot \text{klf}$$

$$\text{South}_{\text{Program}_{\text{Conc}}_{\text{wt}}} := 0.450 \cdot \text{klf}$$

There are limitations in the program as to how to input the loads, take the program load for the concrete and then adjust the superimposed load as needed to get the total load calculated above

$$\text{South}_{\text{Add}_{\text{Load}_{\text{Program}_{\text{Input}}}_{\text{wt}}}} := \text{South}_{\text{Total}_{\text{Barrier}}_{\text{wt}}} - \text{South}_{\text{Program}_{\text{Conc}}_{\text{wt}}} = 0.141 \cdot \text{klf}$$

Total Middle Barrier

$$\text{Middle_Conc_Barrier}_{\text{wt}} := [2 \cdot \text{ft} \cdot (1 \cdot \text{ft} + 1.5 \cdot \text{in})] \cdot \gamma_{\text{conc}} = 0.337 \cdot \text{klf}$$

$$\text{Middle_Total_Barrier}_{\text{wt}} := \text{Middle_Conc_Barrier}_{\text{wt}} + \text{Middle_BR}_{\text{wt_total}} = 0.389 \cdot \text{klf}$$

Total North Barrier

$$\text{North_Conc_Barrier}_{\text{wt}} := [[1.5 \cdot \text{ft} \cdot (1 \cdot \text{ft} + 1.5 \cdot \text{in})] + 6 \cdot \text{in} \cdot (1 \cdot \text{ft} + 3.5 \cdot \text{in})] \cdot \gamma_{\text{conc}} = 0.35 \cdot \text{klf}$$

$$\text{North_Total_Barrier}_{\text{wt}} := \text{North_Conc_Barrier}_{\text{wt}} + \text{Total_Fence}_{\text{wt_total}} = 0.45 \cdot \text{klf}$$

$$\text{North_Program_Conc}_{\text{wt}} := 0.338 \cdot \text{klf}$$

There are limitations in the program as to how to input the loads, take the program load for the concrete and then adjust the superimposed load as needed to get the total load calculated above

$$\text{North_Add_Load_Program_Input}_{\text{wt}} := \text{North_Total_Barrier}_{\text{wt}} - \text{North_Program_Conc}_{\text{wt}} = 0.112 \cdot \text{klf}$$

Pilaster Loads

$$\text{Abutment_Pilaster_Length} := 5 \cdot \text{ft} + 5 \cdot \text{in}$$

$$\text{Interior_Pilaster_Length} := 3 \cdot \text{ft}$$

$$\text{South_Pilaster_Width} := 1 \cdot \text{ft} + 3.5 \cdot \text{in}$$

$$\begin{aligned} \text{South_Abut_Pilaster_Load} := & \text{Abutment_Pilaster_Length} \cdot [(6 \cdot \text{ft} + 1 \cdot \text{in}) \text{South_Pilaster_Width} \gamma_{\text{conc}}] \dots = 9.314 \cdot \text{kip} \\ & + (\text{Abutment_Pilaster_Length} + 4 \cdot \text{in}) \cdot [(7.5 \cdot \text{in}) \cdot (\text{South_Pilaster_Width} + 3 \cdot \text{in}) \cdot \gamma_{\text{conc}}] \dots \\ & + \text{Abutment_Pilaster_Length} \cdot (1 \cdot \text{ft} + 3.5 \cdot \text{in}) \cdot (2 \cdot \text{ft}) \cdot \gamma_{\text{conc}} \end{aligned}$$

$$\begin{aligned} \text{South_Interior_Pilaster_Load} := & \text{Interior_Pilaster_Length} \cdot [(6 \cdot \text{ft} + 1 \cdot \text{in}) \text{South_Pilaster_Width} \gamma_{\text{conc}}] \dots = 6.466 \cdot \text{kip} \\ & + (\text{Abutment_Pilaster_Length} + 4 \cdot \text{in}) \cdot (7.5 \cdot \text{in}) \cdot (\text{South_Pilaster_Width} + 3 \cdot \text{in}) \cdot \gamma_{\text{conc}} \dots \\ & + \text{Abutment_Pilaster_Length} \cdot (1 \cdot \text{ft} + 3.5 \cdot \text{in}) \cdot (2 \cdot \text{ft}) \cdot \gamma_{\text{conc}} \end{aligned}$$

$$\text{North_Pilaster_Width} := 1 \cdot \text{ft}$$

$$\begin{aligned} \text{North_Abut_Pilaster_Load} := & \text{Abutment_Pilaster_Length} \cdot [(6 \cdot \text{ft} + 1 \cdot \text{in}) \text{North_Pilaster_Width} \gamma_{\text{conc}}] \dots = 8.325 \cdot \text{kip} \\ & + (\text{Abutment_Pilaster_Length} + 4 \cdot \text{in}) \cdot [(7.5 \cdot \text{in}) \cdot (\text{North_Pilaster_Width} + 3 \cdot \text{in}) \cdot \gamma_{\text{conc}}] \dots \\ & + \text{Abutment_Pilaster_Length} \cdot (1 \cdot \text{ft} + 8 \cdot \text{in}) \cdot (2 \cdot \text{ft}) \cdot \gamma_{\text{conc}} \end{aligned}$$

$$\begin{aligned} \text{North_Interior_Pilaster_Load} := & \text{Interior_Pilaster_Length} \cdot [(6 \cdot \text{ft} + 1 \cdot \text{in}) \text{North_Pilaster_Width} \gamma_{\text{conc}}] \dots = 6.12 \cdot \text{kip} \\ & + (\text{Abutment_Pilaster_Length} + 4 \cdot \text{in}) \cdot (7.5 \cdot \text{in}) \cdot (\text{North_Pilaster_Width} + 3 \cdot \text{in}) \cdot \gamma_{\text{conc}} \dots \\ & + \text{Abutment_Pilaster_Length} \cdot (1 \cdot \text{ft} + 8 \cdot \text{in}) \cdot (2 \cdot \text{ft}) \cdot \gamma_{\text{conc}} \end{aligned}$$

Note that the barrier load MUST be defined the full length. The The pilaster weight calculated was the total weight. Therefore subtract off the barrier weight to be used to pinput into the BrR Program

G14

$$\text{BrR_South_Abut_Pilaster_Load} := \text{South_Abut_Pilaster_Load} - \text{South_Total_Barrier}_{\text{wt}} \cdot \text{Abutment_Pilaster_Length} = 6.111 \cdot \text{kip}$$

$$\text{BrR_South_Interior_Pilaster_Load} := \text{South_Interior_Pilaster_Load} - \text{South_Total_Barrier}_{\text{wt}} \cdot \text{Abutment_Pilaster_Length} = 3.263 \cdot \text{kip}$$

G1

$$\text{BrR_North_Abut_Pilaster_Load} := \text{North_Abut_Pilaster_Load} - \text{North_Total_Barrier}_{\text{wt}} \cdot \text{Abutment_Pilaster_Length} = 5.887 \cdot \text{kip}$$

$$\text{BrR_North_Interior_Pilaster_Load} := \text{North_Interior_Pilaster_Load} - \text{North_Total_Barrier}_{\text{wt}} \cdot \text{Abutment_Pilaster_Length} = 3.682 \cdot \text{kip}$$

$$\text{Abut_Pil_Loc}_1 := \text{Abutment_Pilaster_Length} \div 2 - (2 \cdot \text{ft} + 9 \cdot \text{in} - 6 \cdot \text{in}) = 0.458 \cdot \text{ft}$$

$$\text{Abut_Pil_Loc}_2 := \text{Total_Span_Length} - \text{Abut_Pil_Loc}_1 = 276.542 \text{ ft}$$

$$\text{Int_Pil_Loc}_1 := 52 \cdot \text{ft}$$

$$\text{Int_Pil_Loc}_2 := \text{Int_Pil_Loc}_1 + 57 \cdot \text{ft} + 8 \cdot \text{in} = 109.667 \text{ ft}$$

$$\text{Int_Pil_Loc}_3 := \text{Total_Span_Length} - \text{Int_Pil_Loc}_2 = 167.333 \text{ ft}$$

$$\text{Int_Pil_Loc}_4 := \text{Total_Span_Length} - \text{Int_Pil_Loc}_1 = 225 \text{ ft}$$

Lighting Load

$$\text{Lighting_Bump_Out}_{\text{wt}} := \left[1.5 \cdot \text{ft} \cdot (1 \cdot \text{ft} + 7 \cdot \text{in}) \dots \right] \cdot 1.5 \cdot \text{ft} \cdot \gamma_{\text{conc}} = 1.544 \cdot \text{kip}$$

$$\text{Light_Pole}_{\text{wt}} := 150 \cdot \text{lbf}$$

$$\text{Total_Light}_{\text{wt}} := \text{Lighting_Bump_Out}_{\text{wt}} + \text{Light_Pole}_{\text{wt}} = 1.694 \cdot \text{kip}$$

$$\text{Light_Loc}_1 := 26 \cdot \text{ft} + 10 \cdot \text{in} = 26.833 \text{ ft}$$

$$\text{Light_Loc}_2 := 79 \cdot \text{ft} + 4 \cdot \text{in} = 79.333 \text{ ft}$$

$$\text{Light_Loc}_3 := 138 \cdot \text{ft} + 6 \cdot \text{in} = 138.50 \text{ ft}$$

$$\text{Light_Loc}_4 := \text{Total_Span_Length} - \text{Light_Loc}_2 = 197.667 \text{ ft}$$

$$\text{Light_Loc}_5 := \text{Total_Span_Length} - \text{Light_Loc}_1 = 250.167 \text{ ft}$$

Bar Deck Offset Location

$$\text{Bot_Bar_Dist} := 1.5\text{in} + \frac{5}{8} \cdot \text{in} + \frac{1}{2} \cdot \frac{5}{8} \text{in} = 2.438 \cdot \text{in}$$

$$\text{Top_Bar_Dist} := 2.5 \cdot \text{in} + \frac{1}{2} \cdot \frac{4}{8} \cdot \text{in} = 2.750 \cdot \text{in}$$

$$\text{Pier_Bar_Dist} := 2.5 \cdot \text{in} + \frac{1}{2} \cdot \frac{5}{8} \cdot \text{in} = 2.813 \cdot \text{in}$$