

# CUY-90-14.90

PID 77332/85531

# **APPENDIX UT-03**

# NEORSD Walworth Run Relocation (Reference Document)

State of Ohio
Department of Transportation
Jolene M. Molitoris, Director

Innerbelt Bridge
Construction Contract Group 1 (CCG1)

Revision Date: March 23, 2010



# NORTHEAST OHO REGIONAL SEWER DISTRICT WALWORTH RUN INTERCEPTOR REALIGNMENT (WRIR)

# WRIR

# NORTHEAST OHIO REGIONAL SEWER DISTRICT

**BOARD OF TRUSTEES** 

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JULIUS CIACCIA, JR., EXECUTIVE DIRECTOR

# ACCEPTED BY:

JULIUS CIACCIA, JR. EXECUTIVE DIRECTOR DATE

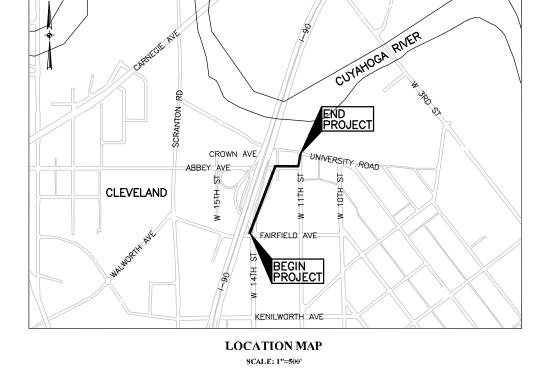
DATE

KELLIE C. ROTUNNO DIRECTOR OF ENGINEERING AND CONSTRUCTION

NORTHEAST OHIO REGIONAL SEWER DISTRICT

DLZ OHIO, INC.

DATE



ENGINEERS • ARCHITECTS • SCIENTISTS PLANNERS • SCR VEYORS

SUBMITTED BY:

DLZ OHIO, INC

50% SUBMITTAL MARCH 19, 2010



# <u>NOTES</u>

- 1. BASIS OF BEARING AND ELEVATION: HORIZONTAL AND VERTICAL CONTROL IS BASED ON THE OHIO NORTH ZONE STATE PLANE COORDINATE SYSTEM NAD 83 AND THE NAVD 88 VERTICAL DATUM.
- 2. EXISTING STRUCTURES, GRADES, PIPING ETC., ARE SHOWN IN APPROXIMATE LOCATIONS ON THE PLANS. THE INFORMATION SHOWN IS NOT GUARANTEED TO BE CORRECT OR COMPLETE. THE DATA SHALL BE VERIFIED IN THE FIELD BY THE CONTRACTOR.
- 3. THE CONTRACTOR SHALL COORDINATE HIS OPERATIONS WITH THE WORK OF THE UTILITY OWNERS OR OTHERS WHO MAY RELOCATE EXISTING UTILITIES, AND SHALL NOTIFY OWNERS OF THE UTILITIES OF HIS SCHEDULE SUFFICIENTLY IN ADVANCE TO PERMIT THEM TO MAKE THE NECESSARY
- 4. INFORMATION ON EXISTING UTILITIES AND OTHER SUB-STRUCTURES WAS OBTAINED FROM APPROPRIATE AGENCIES. EXISTING UTILITIES SHALL BE MAINTAINED IN PLACE BY THE CONTRACTOR UNLESS OTHERWISE SHOWN ON THE PLANS OR STATED IN THE SPECIFICATIONS. THE LOCATIONS OF EXISTING UTILITIES AND SUB-STRUCTURES SHOWN ON THE DRAWINGS ARE APPROXIMATE ONLY. THE CONTRACTOR SHALL VERIFY EXACT LOCATIONS, ELEVATIONS, AND DIMENSIONS IN THE FIELD PRIOR TO CONSTRUCTION IN THE AREA OF THE SPECIFIC SUB-STRUCTURE.
- 5. THE LENGTH OF PIPE SHOWN ON THE DRAWINGS IS GIVEN FROM CENTER—TO—CENTER OF STRUCTURE FOR STRUCTURES UP TO 6—FT INSIDE DIAMETER, AND TO THE INSIDE FACE OF STRUCTURE FOR STRUCTURES OVER 6-FT INSIDE DIAMETER.

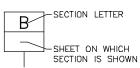
# LEGEND

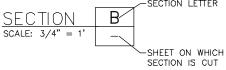
		LLOLI	<u> </u>		
0	_	EXISTING MANHOLE		_	POST (SQUARE)
	_	EXISTING CATCH BASIN	~^^	_	POST (ROUND)
Ω	_	EXISTING HYDRANT	8.5	_	TREE
ᡯ᠘ᡀᡐᡮᠿᡐᠿᡐ	-	EXISTING/PROPOSED VALVE LIGHT POLE	9	_	SHRUB
7	_	TELEPHONE POLE	0	_	BENCH MARK
₽ Æ	_	POWER POLE	X	_	CHISELED BENCH MARK
Ψ	_		M	_	EXISTING MONUMENT BOX
γ Æ	_	UTILITY POLE	0	_	IRON PIN/PIPE FOUND
Ψ_=	_	LIGHT & POWER POLE	0	_	IRON PIN/PIPE SET
φ	-	TELEPHONE & POWER POLE	•	_	TACKED HUB
	_	TELEPHONE & LIGHT POLE	0	_	DRILL HOLE
,	_	GUY ANCHOR	٠	_	PKNAIL
Q	-	SIGN (1 POST)	٥	_	RAILROAD SPIKE
-	_	SIGN (2 POST)	E	_	ELECTRICAL BOX
<b>(S)</b>	-	EXISTING SANITARY MANHOLE			
Ш	_	STORM INLET/ CATCH BASIN	(£) 	-	EXISTING ELECTRICAL MANHOLE
===	_	STORM INLET/ CATCH BASIN	<del>-    </del>	-	BORING LOCATION

CONCRETE

GROUT

DATE ISSUE





# **ABBREVIATIONS**

			ABBKI	<u>- VI</u>	ATIONS		
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA	=	ADHESIVE ANCHOR BOLT ADDITIONAL ALTERNATE ALUMINUM AND ASSEMBLY AT BITUMINOUS BOTTOM OF  BASE LINE BUILDING BLOCK BOTTOM BASE PLATE BEARING BENT PLATE CENTRIFUGALLY CAST FIBER—REINFORCED POLYMER MORTAR PIPE CENTER TO CENTER CONSTRUCTION JOINT CENTERLINE CIRCULAR CLEAR CONTROLED LOW—STRENGTH MATERIAL CONCRETE CONTINUOUS CONTROLE CONTINUOUS CONTROL CULVELAND PUBLIC POWER DEFLECTION DEPRESSION DETAIL DUCTILE IRON PIPE DIAMETER DIMETER DATE DEAD DETAIL DUCTILE IRON PIPE DIAMETER DIMETER DIMETE	EXPTENDING THE GARDEN PHENDEN FOR THE STATE OF THE STATE		EACH WAY EQUAL EXISTING EXPANSION EXTERIOR FOUNDATION FINISH FINISH LINE FLOOR FAR FACE FOOTING GAS GAGE GROUND HORIZONTAL HIGH POINT HIGH HIGH POINT HIGH HIGH POINT HIGH STRENGTH INSIDE FACE INTERIOR INSULATION INVERT JOINT KIP (1000 POUNDS) LIVE LOAD LONG LEG BACK—TO—BACK LONG LEG HORIZONTAL LONG LEG BACK—TO—BACK LONG LEG HORIZONTAL LONG LEG BACK—TO—BACK LONG LEG HORIZONTAL LONG LEG HORIZONTAL LONG LEG BACK—TO—BACK LONG LEG HORIZONTAL LONG LEG HORIZONTAL LONG LEG VERTICAL LONGITUDINAL LOW POINT LEFT LIGHT WEIGHT MASONRY MAXIMUM MANHOLE MINIMUM MANHOLE MINIMUM MASONRY OPENING NOT APPLICABLE NEAR FACE NUMBER ON CENTER OVERHEAD EXISTING OPPOSITE OPPOSIT	REQ'MT RO RT R/W SAN SCHED SECT SF SH SLBB SLV SPRD ST	 PROPERTY LINE/PLATE PROPOSED POUNDS PER SQUARE INCH POUNDS PER SQUARE FOOT POLYVINYL CHLORIDE RISER REINFORCED CONCRETE PIPE REINFORCING REQUIRED - REQUIREMENTS ROUGH OPENING RIGHT RIGHT—OF—WAY SANITARY SEWER SCHEDULE SECTION SOUARE FEET SHEET SIMILAR STEEL JOIST SHORT LEG BACK—TO—BACK SHORT LEG VERTICAL SPACES OR SPACING SPREAD — SQUARE STORM SEWER STATION STAINLESS STEEL STRUCTURAL SUPPORT STORMWATER OVERFLOW TREAD TOP OF TOP AND BOTTOM TEMPORARY THICK TOP OF MASONRY TYPICAL UNLESS OTHERWISE NOTED VITRIFIED CLAY PIPE VERTICAL WATER WITH WEST WATER MAIN WITHOUT WORK POINT WATERSTOP WELDED WIRE FABRIC

# SHEET INDEX

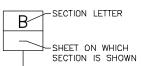
			SHEET INDEX
	SHEET NO	<u>).</u>	SHEET TITLE
			TITLE
	G-1	_	LEGEND, SHEET INDEX, AND GENERAL NOTES
	G-2	_	SURVEY CONTROL
E			MAINTENANCE OF TRAFFIC
			PLAN & PROFILE
	P-1	_	WALWORTH RUN INTERCEPTOR STA 1+00 TO STA 5+00
	P-2	_	WALWORTH RUN INTERCEPTOR STA 5+00 TO STA 10+00
	P-3	_	WALWORTH RUN INTERCEPTOR STA 10+00 TO STA 15+00
	P-4	-	WEST 15TH ST SEWER CONNECTION
			CIVIL
	C-1	_	NORTHERN SEWER ABANDONMENT PLAN
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	C-3	_	JUNCTION CHAMBER NO. 1 SITE PLAN
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	C-6	-	WATER MAIN RELOCATION PLAN AND NOTES
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	C-9		PRECAST CONCRETE MANHOLE DETAILS
	C-10		
			CIVIL DETAILS
	C-12	_	CITY OF CLEVELAND CATCH BASIN DETAIL
			THNNFI

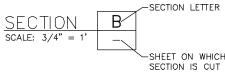
## <u>TUNNEL</u>

TU-1 - WORK SHAFT JUNCTION CHAMBER NO.1 INITIAL SUPPORTS TU-2 - JUNCTION CHAMBER NO.1 FINAL SUPPORTS TU-3 - WORK SHAFT JUNCTION CHAMBER NO.2 INITIAL SUPPORTS TU-4 - JUNCTION CHAMBER NO.2 FINAL SUPPORTS

TU-5 - WORK SHAFT MANHOLE NO.1 INITIAL SUPPORTS
TU-6 WORK SHAFT MANHOLE NO.2 INITIAL SUPPORTS TU-7 - BREAK-IN, BREAK-OUT, BACKSTOP AND SUMP DETAIL

SECTION CUTS





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PROJECT NO.:

SHEET: X

SCALE: 1"=10' SHEET NO.: G-1



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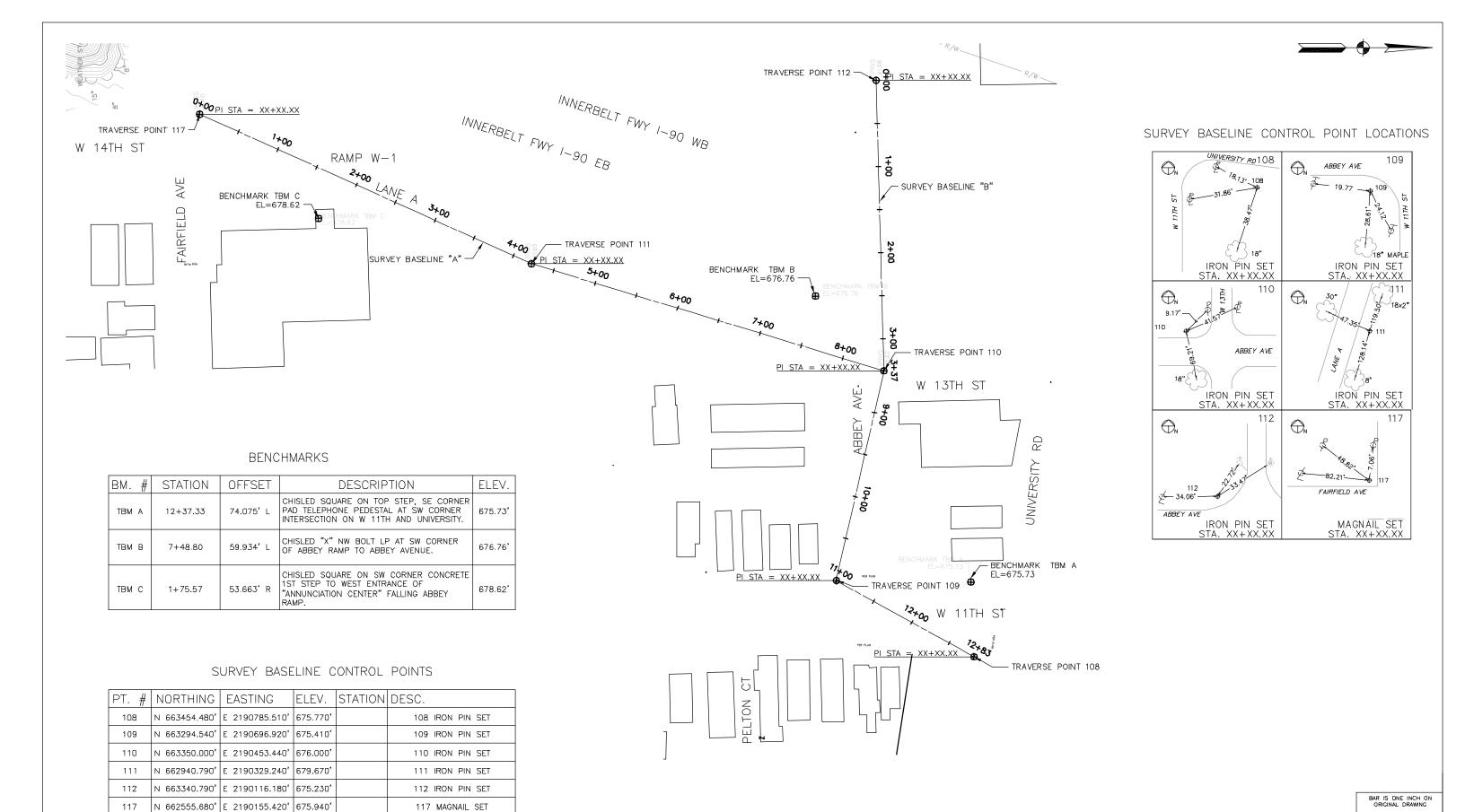
SCREENED GRAVEL

UNDISTURBED EARTH



This document was

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				DRAWN BY:
				SHEET CHK'D BY:
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				APPROVED BY:
REV.	DATE	ISSUE BY	REMARKS	DATE:





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WALWORTH RUN INTERCEPTOR REALIGNMENT

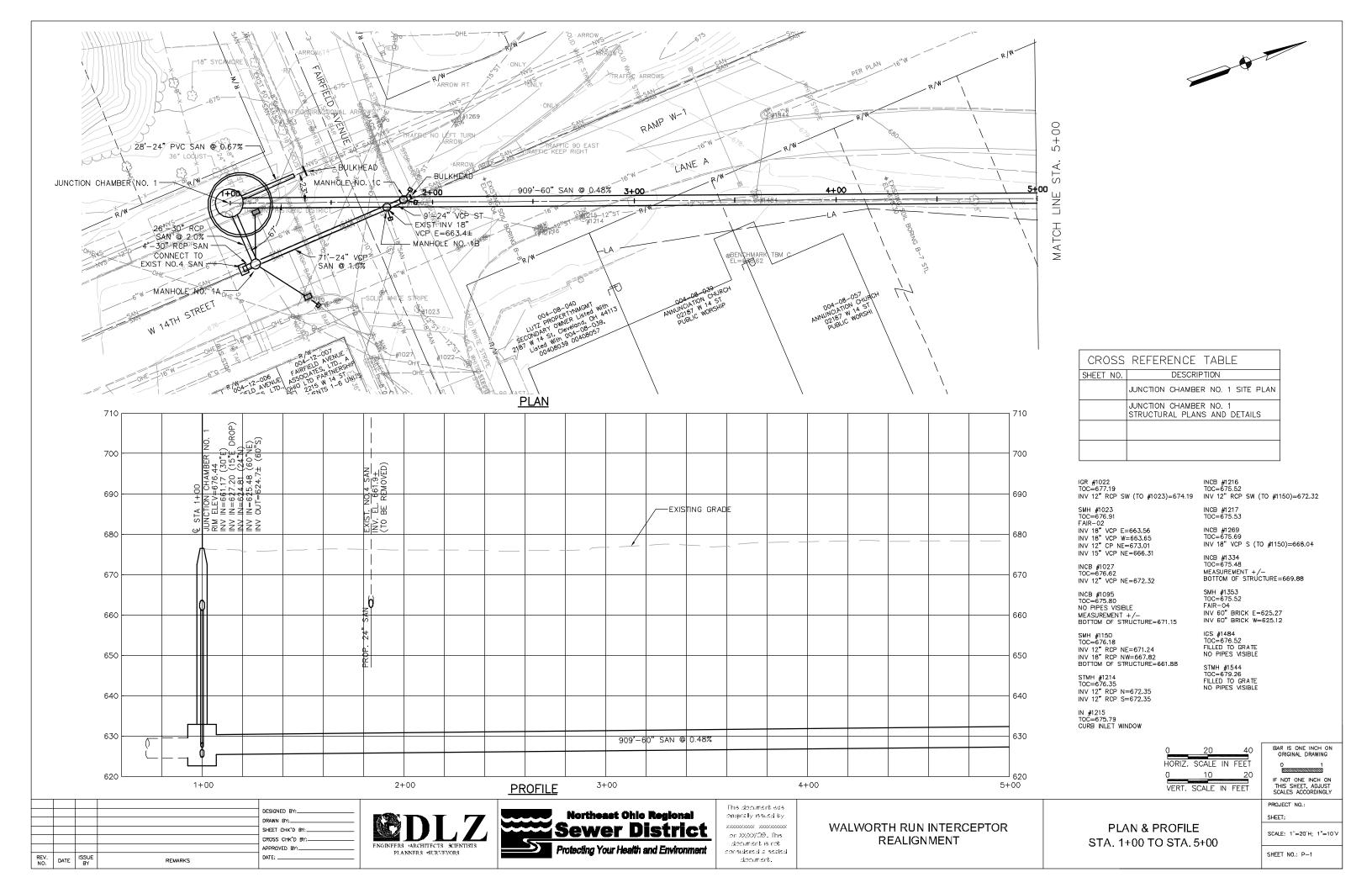
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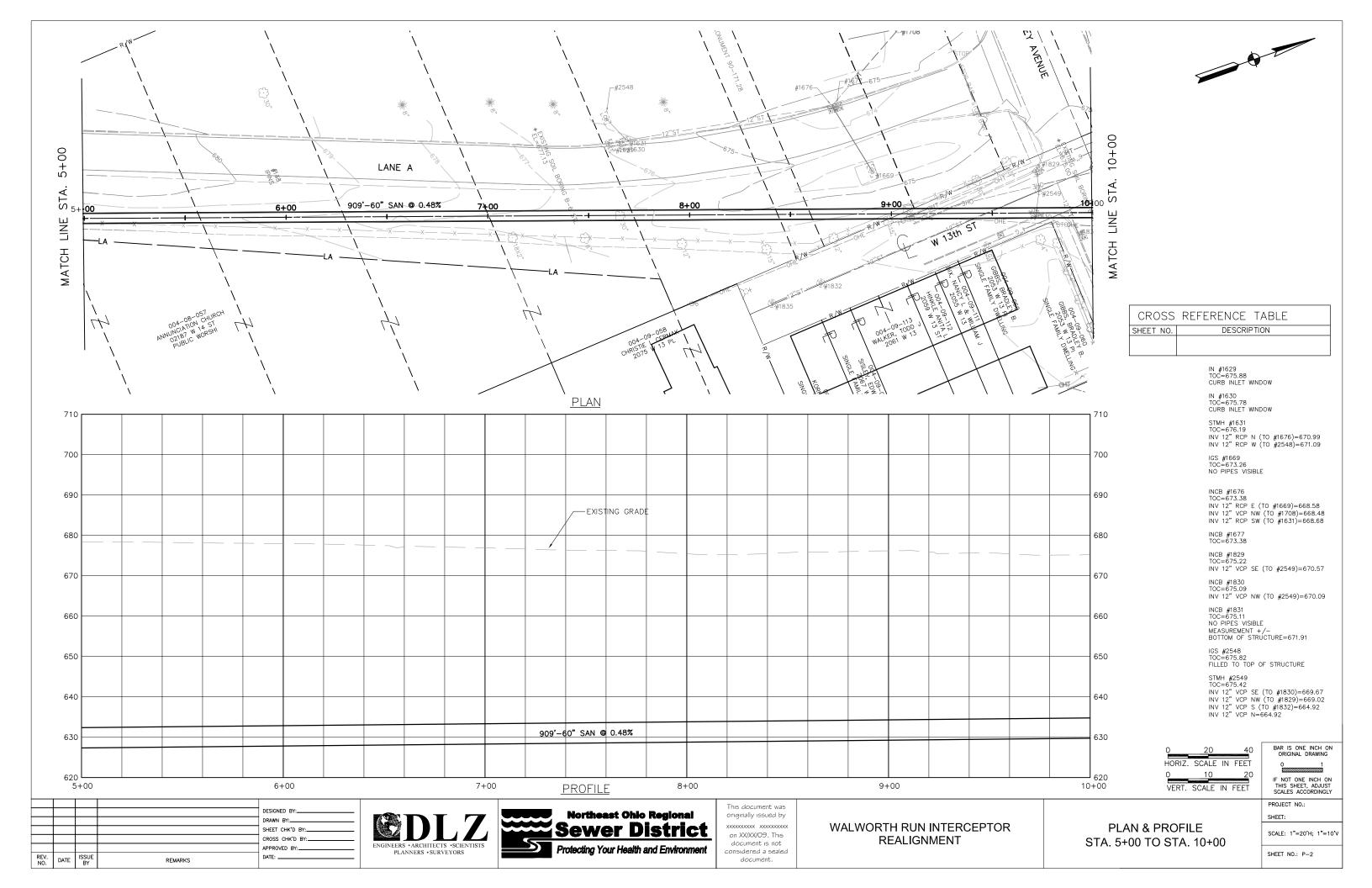
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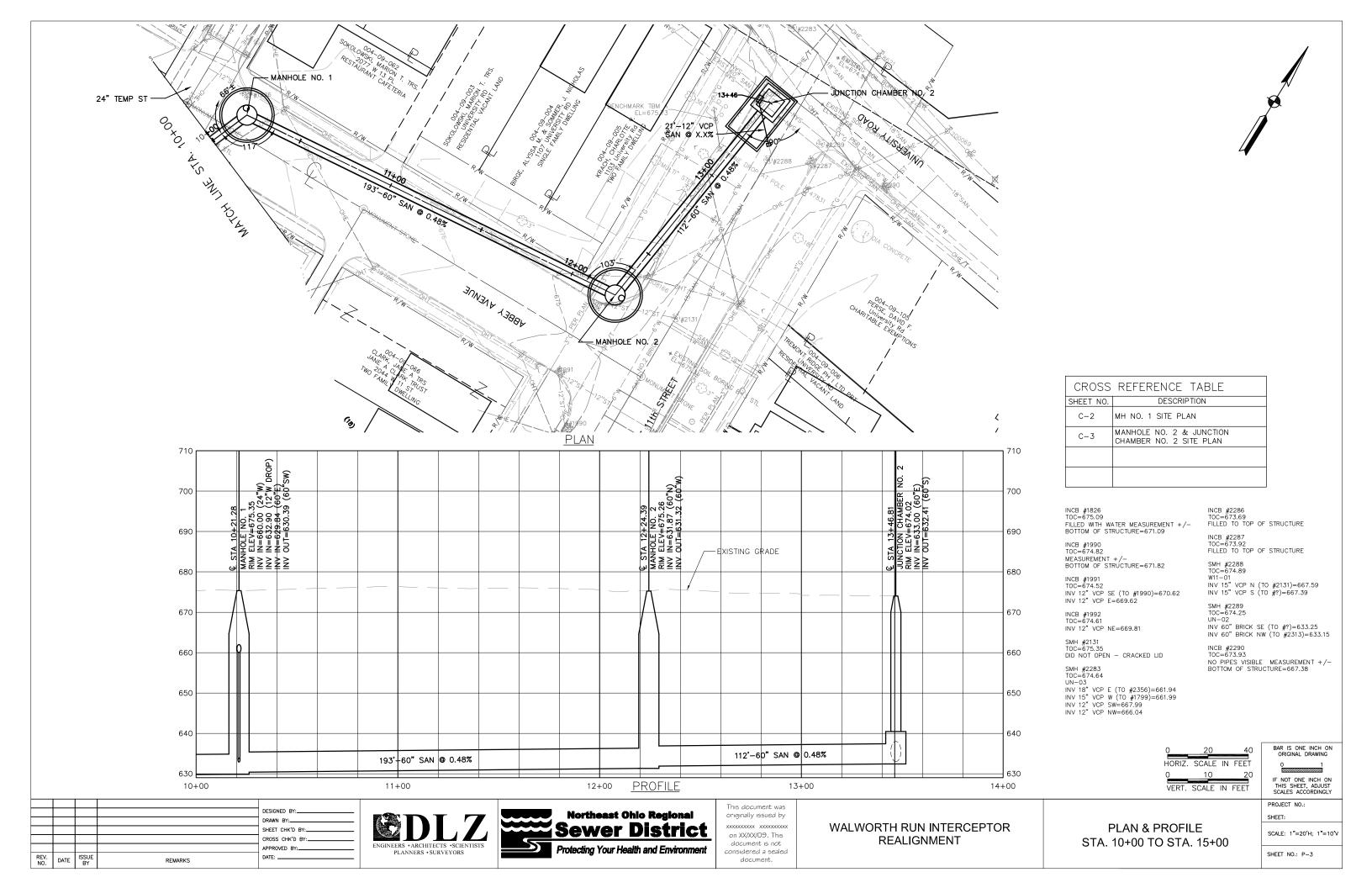
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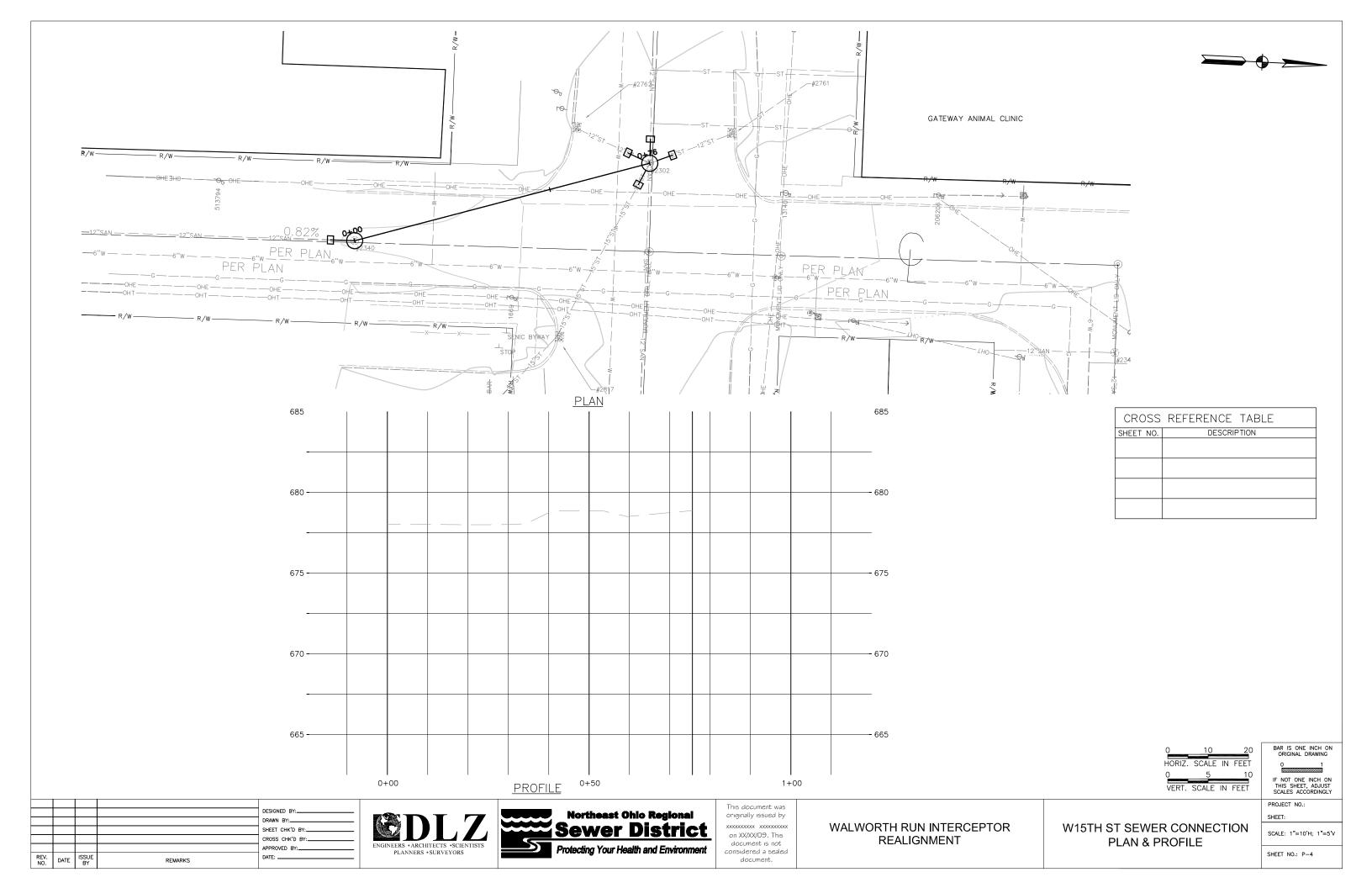
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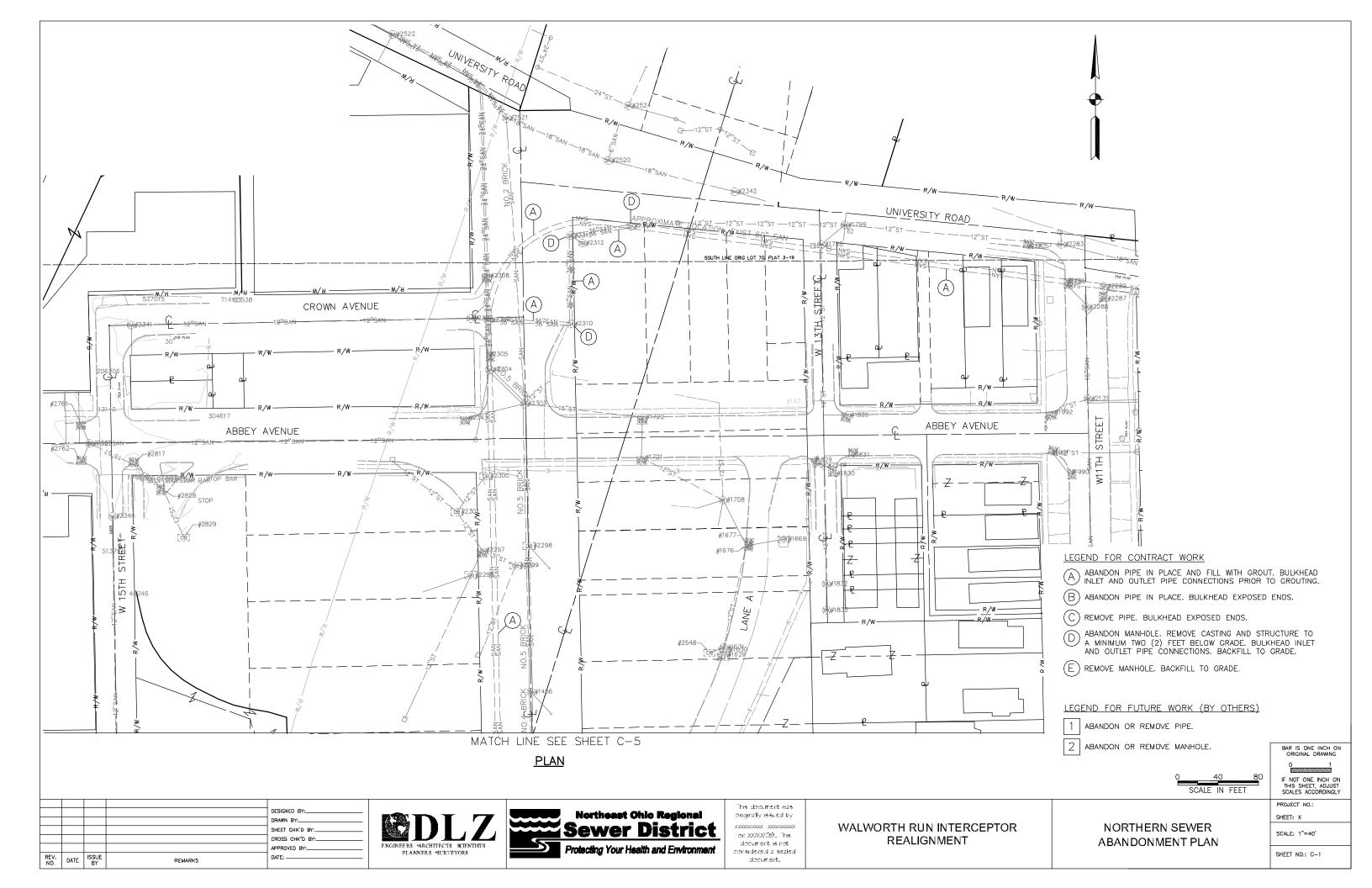
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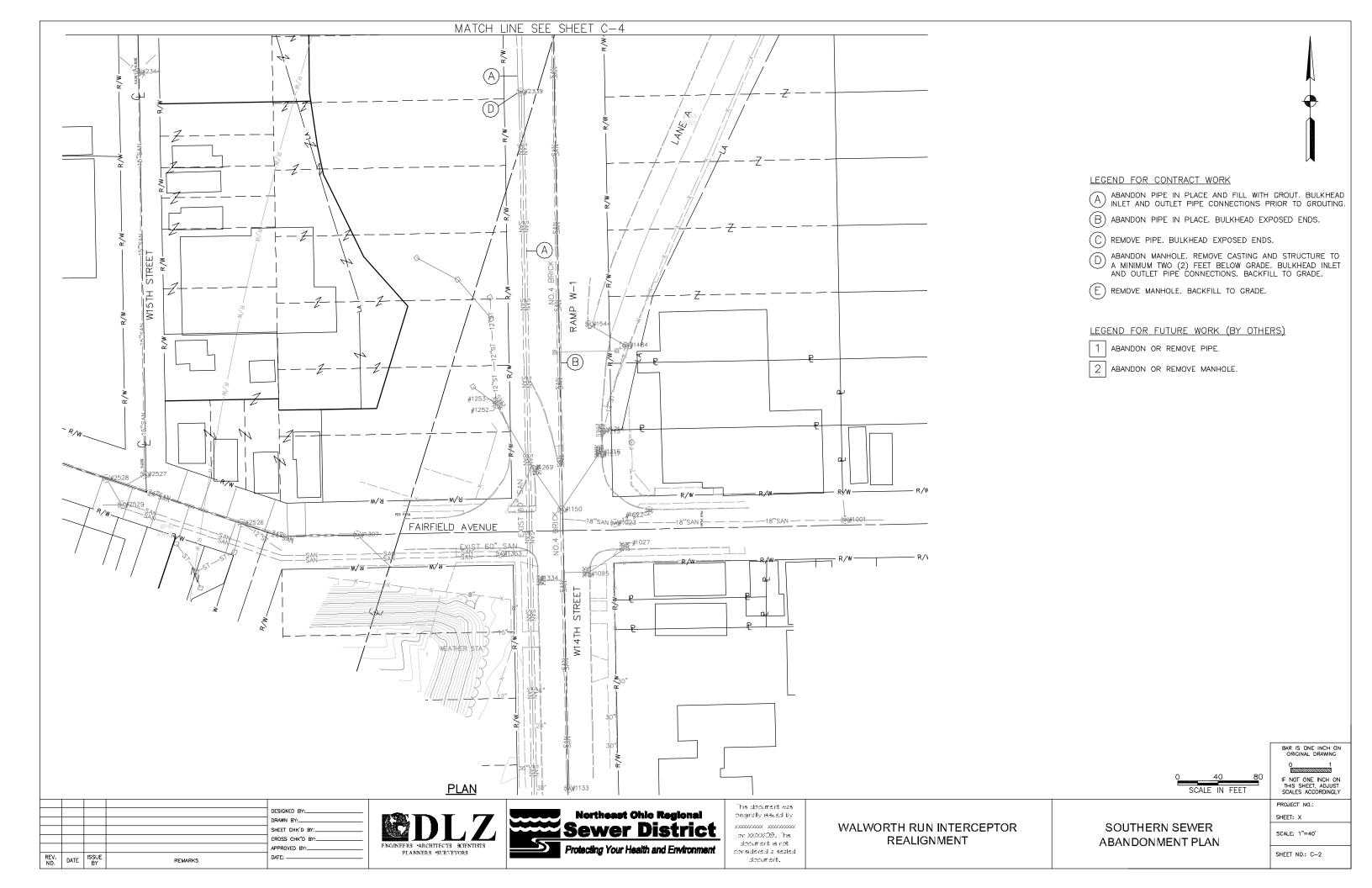


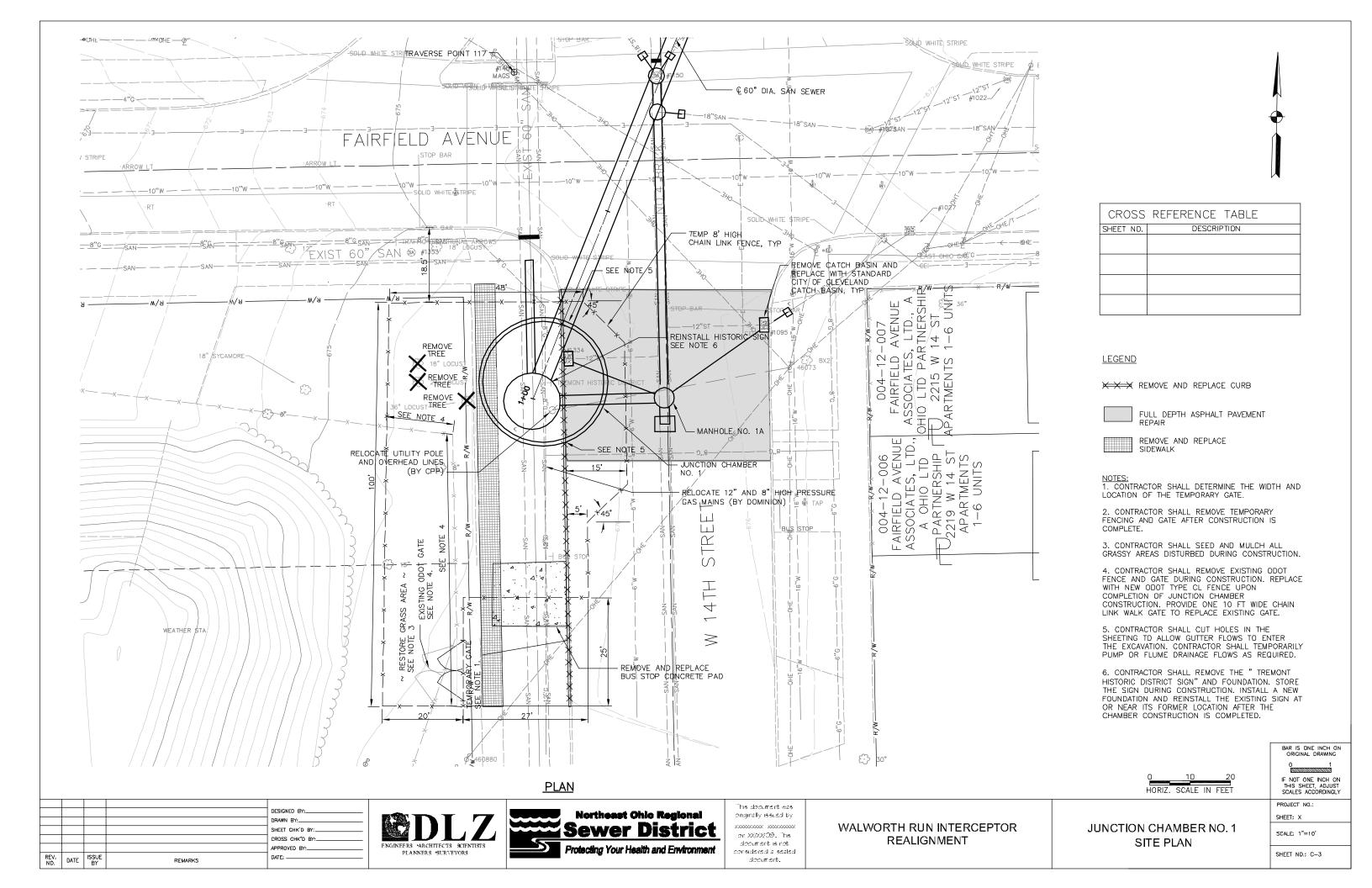


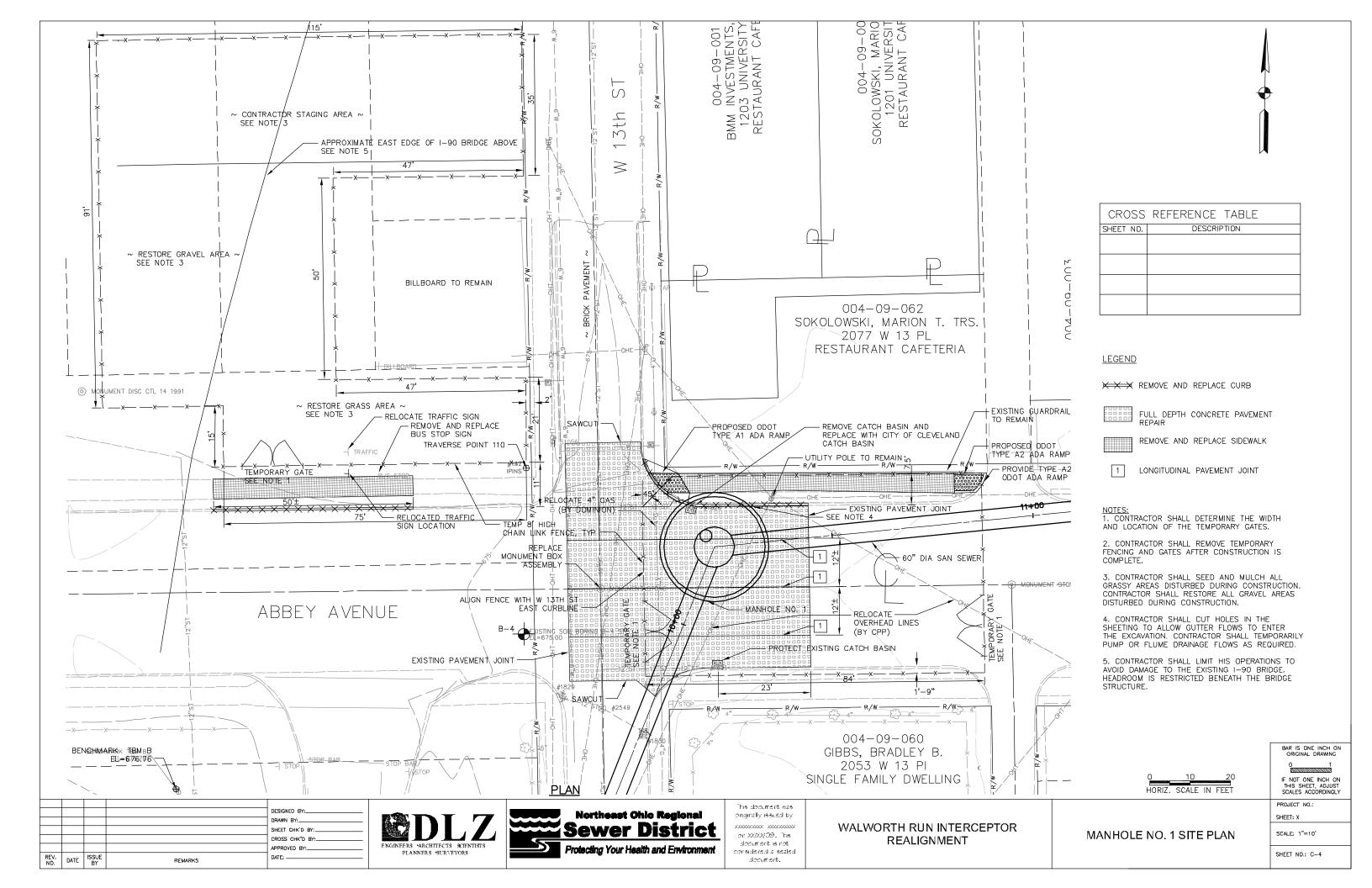


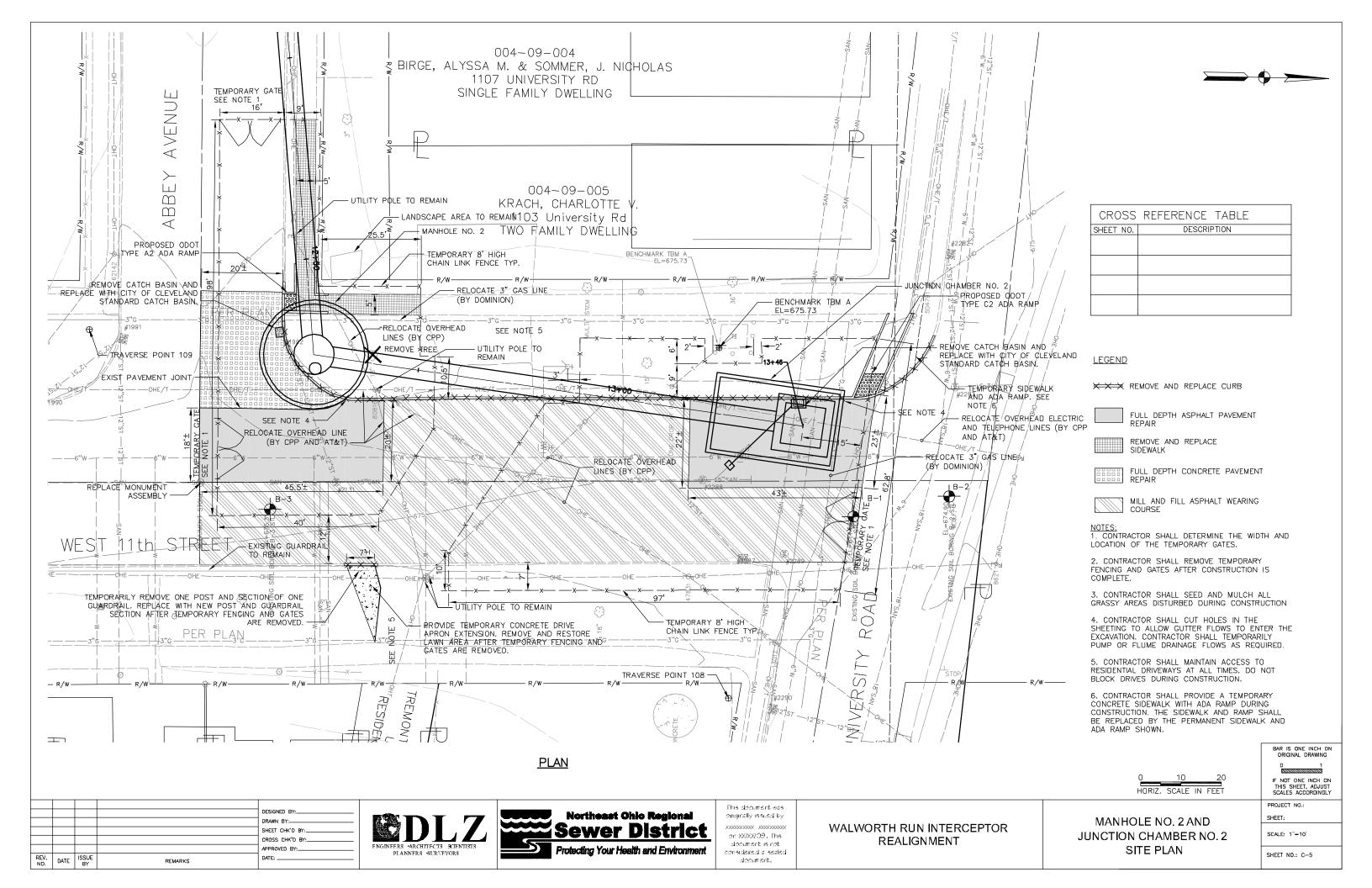












# CLEVELAND DIVISION OF WATER NOTES FOR NEW WATER MAIN INSTALLATION

CONTRACTOR IS TO ABIDE BY THE MOST CURRENT VERSION OF THE CLEVELAND, DIVISION OF WATER NOTES AND DETAILS. THE MOST UP-TO-DATE VERSION CAN BE FOUND AT WWW.CLEVELANDWATER.COM.

- THE INFORMATION SHOWN ON THE CLEVELAND DIVISION OF WATER'S SUMMARY OF WORK/CHARGE LETTER AND STRIP MAPS ARE TAKEN FROM EXISTING AVAILABLE RECORDS, AND THEIR ACCURACY IS NOT GUARANTEED.
- CALL THE INSPECTION AND ENFORCEMENT UNIT AT 216-664-2342 TO SCHEDULE A PRECONSTRUCTION MEETING. THE OPERATION OF ANY VALVE OR ALTERATION OF ANY PART OF THE WATER SYSTEM BY CONTRACTORS OR THEIR EMPLOYEES IS PROHIBITED THE SUPERVISION OF THE CLEVELAND DIVISION OF WATER INSPECTOR.
- THE MUNICIPALITY SHALL REQUIRE THAT THE PROJECT'S PROFESSIONAL ENGINEER OBTAIN ACTUAL FIFLD MEASUREMENTS OF THE MAIN DURING INSTALLATION AND SHALL FURNISH THE CWD INSPECTOR WITH RECORD PRINTS IN A FORM ACCEPTABLE TO THE DIVISION OF WATER. THE CLEVELAND DIVISION OF WATER WILL REQUIRE THE DELIVERY AND ACCEPTANCE OF TWO COPIES OF RECORD (AS BUILT) PRINTS. STAMPED BY A PROFESSIONAL ENGINEER, BEFORE THE PRESSURE TEST AND CHLORINATION OF THE MAIN
- . FOR THE PURPOSES OF CHIORINATION AND BACTERIOLOGICAL TESTING OF THE WATER MAINS THE CONTRACTOR SHALL PROVIDE AND INSTALL, AT EACH OF THE CHLORINATION PIT LOCATIONS SHOWN AND AT OTHER LOCATIONS DETERMINED BY THE DIVISION OF WATER, FLUSHING/SAMPLING TAPS OF SIZES TO BE DETERMINED BY THE DIVISION OF WATER. CHLORINATION PITS SHALL BE SIX (6) FOOT SQUARE MEETING OSHA STANDARDS. 15.
- 5. A TWO YEAR WARRANTY, COMMENCING FROM THE DATE OF ACCEPTANCE OF THE FINAL CHLORINATION OF THE WATER MAIN INSTALLATION, SHALL BE PROVIDED BY THE BUILDER/DEVELOPER AND/OR CONTRACTOR FOR ALL WATER MAINS AND SERVICE CONNECTION WORK PERFORMED BY THE CONTRACTOR, INCLUDING RETAPS, SHOULD LEAKS OCCUR AND REPAIRS BE REQUIRED DUE TO DEFECTIVE MATERIAL OR POOR SHOULD ANY WORKMANSHIP.
- . USE BACKFILL MATERIAL AS SPECIFIED AND COMPACT SUFFICIENTLY IN THOSE AREAS WHERE EXISTING MAINS AND WATER SERVICE CONNECTIONS ARE EXPOSED.
- ALL MATERIALS, INCLUDING BUT NOT LIMITED TO WATER MAINS, FIRE HYDRANTS, VALVES, CONNECTION MATERIALS AND OTHER WATER APPURTENANCES, SHALL BE NEW AND UNUSED AND SHALL CONFORM TO THE MOST CURRENT DIVISION OF WATER SPECIFICATIONS. ALL MATERIAL SHALL BE INSTALLED IN ACCORDANCE WITH DIVISION OF WATER'S STANDARDS.
- 3. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY DAMAGE TO EXISTING WATER MAINS AND APPURTENANCES THEREOF WHEN CONNECTING THE NEW WATER MAIN FOR THE HYDROSTATIC TEST. ALL REPAIRS TO DAMAGED EXISTING FACILITIES SHALL BE MADE BY THE CONTRACTOR, AT THE CONTRACTOR'S EXPENSE, TO THE SATISFACTION OF THE DIVISION OF WATER. (REFER TO THE THE ALTERNATE TEST DETAIL STD-002 AS NEEDED)
- ALL HYDROSTATIC PRESSURE TESTING SHALL BE DONE BY THE CONTRACTOR IN THE PRESENCE OF THE DIVISION OF WATER'S INSPECTOR. THE HYDROSTATIC TEST PRESSURE SHALL BE 75 PSI ABOVE THE STATIC PRESSURE PREVAILING AT THE SITE, BUT IN NO CASE LESS THAN 150 PSI. THE PRESSURE TEST SHALL BE FOR A DURATION OF TWO (2) HOURS WITH THE PRESSURE BEING MAINTAINED WITHIN 5 PSI OF THE REQUIRED TEST PRESSURE. SHOULD THE PRESSURE TEST FAIL THE CONTRACTOR SHALL FIND AND CORRECT THE DEFICIENCY(IES) TO THE SATISFACTION OF THE DIVISION OF WATER AND REPEAT THE TWO (2) HOUR PRESSURE TEST.
- OA. ALL PIPE, UNLESS OTHERWISE CALLED FOR, SHALL BE DUCTILE IRON, MINIMUM CLASS 52, CEMENT LINED HAVING PUSH-ON JOINTS WITH RADIALLY COMPRESSED RUBBER RING GASKET AND INSTALLED AS PER THE MOST CURRENT REVISION OF AWWA C600.
- UNLESS OTHERWISE CALLED FOR, SHALL BE APPROVED DUCTILE IRON CLASS 350, CEMENT LINED OR FUSION BONDED EPOXY COATED, ALL FITTINGS AND PIPE CONNECTED TO FITTINGS SHALL BE RESTRAINED USING A "RETAINED" MECHANICAL JOINT CONFORMING TO THE MATERIAL AND PERFORMANCE REQUIREMENTS OF ANSI/AWWA -110/A21.10 AND ANSI/AWWA C-111/A21.11, OR "COMPACT" FITTINGS IN ACCORDANCE WITH ANSI/AWWA C-153/A21.53 EXCEPT FOR ANCHOR TEES REDUCERS OR OTHER SPECIAL CIRCUMSTANCES WHEN DIRECTED BY CLEVELAND DIVISION OF WATER, ALL FITTINGS ARE TO HAVE BELL ENDS.
- OC. ALL BOLTS AND NUTS ON ALL "RETAINED" MECHANICAL JOINTS SHALL HAVE FIELD APPLIED ONE (1) COAT OF BITUMASTIC PAINTING FOLLOWED BY AN ENCASEMENT OF POLYETHYLENE WRAPPING IN ACCORDANCE WITH ANSI/AWWA C-105/A21.5-88, CLASS "C". METHOD "B"
- OD. WHERE SHOWN ON THE PLANS, OR WHEN OTHERWISE CALLED FOR, PIPE AND FITTINGS SHALL HAVE AN APPROVED "TYPE I" OR "TYPE II" BOLTLESS RESTRAINED PUSH-ON JOINTS TO THE LIMITS SHOWN ON THE DRAWINGS.
- DE. AT THE END OF EACH WORKDAY, THE CONTRACTOR SHALL PLUG ALL OPEN PIPE ENDS WITH WATER TIGHT PLUGS AS PER THE "PREVENTITIVE AND CORRECTIVE MEASURES DURING CONSTRUCTION" SECTION OF THE MOST CURRENT REVISION OF AWWA C-651 AS TO PREVENT THE INFILITRATION OR INTRUSION OF ANY FOREIGN OBJECTS OR MATERIALS.

  DATE STAMPED DIGITAL PHOTOS SHALL BE PROVIDED FOR EACH WORKDAY

  DEMONSTRATING THAT PROPER AWWA C-651 METHODS WERE USED TO PLUG ALL OPEN

  WATER MAIN ENDS. EACH PHOTO SHALL CLEARLY IDENTIFY THE STATION AT WHICH THE

  PIPE IS PLUGGED. THE STATIONING SHALL BE SHOWN BY THE USE OF A STATION

  MARKER PLACED AT THE PLUGGED PIPE END.

PHOTOS SHALL BE SUBMITTED ON A DAILY BASIS UNLESS OTHERWISE DEFINED BY THE CWD INSPECTOR OR ENGINEER. ALL PHOTOS TAKEN OVER THE COURSE OF THE PROJECT SHALL BE SUBMITTED BY THE CONTRACTOR AS PART OF THE AS-BUILT SUMITTAL. AS-BUILTS SHALL BE CONSIDERED INCOMPLETE WITHOUT SAID COLLECTION OF DIGITAL

# HYDRANTS:

- IN ALL HYDRANT INSTALLATIONS THE CONTRACTOR SHALL FACE ALL HYDRANT'S 4" (STEAMER) NOZZLE TOWARD THE PAVEMENT PRIOR TO TESTING AND CHLORINATION OF WATER MAINS. CONTRACTOR SHALL CONSULT WITH THE LOCAL MUNICIPALITY'S ENGINEERING OR SERVICE DEPARTMENT TO OBTAIN HYDRANT MODEL AND NOZZLE THREAD REQUIREMENTS IF NOT INDICATED ON THE APPROVED PLANS.
- 12. ALL VALVES SHALL BE AN APPROVED MODEL RESILIENT SEATED GATE VALVES AS PER THE MOST CURRENT VERSION OF AWWA C509 OR C515.

## CONNECTIONS:

- 13. WATER CONNECTIONS SHOWN ON THESE DRAWINGS ARE FOR REFERENCE ONLY AND ARE NOT PART OF THE WATER MAIN APPROVAL. ADDITIONAL PERMITS FOR SERVICE CONNECTIONS MUST BE OBTAINED FROM THE DIVISION OF WATER PRIOR TO INSTALLATION OF ANY PORTION OF THE SERVICE CONECTION(S). IT IS THE CONTRACTORS
  RESPONSIBILITY TO ARRANGE FOR PERMITS FOR ALL SIZE WATER SERVICE CONNECTIONS BEFORE PERFORMING ANY WORK, THE AMOUNT OF THE CHARGES CAN BE OBTAINED FROM THE DIVISION OF WATER, PERMITS AND SALES SECTION AT 216-664-2444 X5203.
- 14. ONE INCH SERVICE CONNECTIONS SHALL BE PERMITTED TO SERVICE HOMES BASED ON
- PEAK FLOW DEMANDS DO NOT EXCEED 25 GPM FOR AN INDIVIDUAL HOME/UNIT. INCLUSIVE OF ALL USAGE (FIRE, DOMESTIC AND/OR IRRIGATION) AND
- \* LENGTH OF ONE INCH CONNECTION DOES NOT EXCEED 75 FEET AS MEASURED FROM

THE MAIN TO THE POINT OF ENTRY INTO THE PROPOSED HOME/UNIT.

ANY SERVICE REQUESTS DIFFERING FROM THE STATED CRITERIA SHALL REQUIRE THE SUBMITTAL OF A COMPLETE WATER SERVICE APPLICATION. PEAK DEMANDS ARE TO BE ASSESSED ON APPLICATION AND SETBACKS ARE TO SHOWN ON AN ACCOMPANYING SITE PLAN SITE PLANS SHALL SHOW WATER METER VAULTS IN THE RIGHT OF WAY OR IN AN EASEMENT CONTIGUOUS TO THE RIGHT OF WAY FOR ANY HOMES/UNITS WITH SETBACKS GREATER THAN 150 FEET. EASEMENTS ARE TO BE PROVIDED WITH THE SERVICE CONNECTION APPLICATION SUBMITTAL.

ALL WATER MAIN CURB VALVE BOXES & METER VAULTS WILL BE INSTALL IN GRASS AREAS WHEN POSSIBLE.

# **EMERGENCIES:**

IF A WATER MAIN OR SERVICE CONNECTION BREAK OCCURS DURING CONSTRUCTION AND EMERGENCY ASSISTANCE IS REQUIRED, PLEASE NOTIFY THE DIVISION OF WATER AT 216-664-3060.

#### **UTILITIES:**

1. THE CONTRACTOR SHALL NOTIFY UTILITY COMPANIES AT LEAST TWO (2) WORKING DAYS THE CONTRACTOR SHALL NOTIFY UTILITY COMPANIES AT LEAST IWO (2) WORKING DAYS (NOT INCLUDING SATURDAYS AND LEGAL HOLIDAYS) PRIOR TO CONSTRUCTION TO HAVE UTILITIES STAKED, MARKED OR OTHERWISE DESIGNATED IN THE CONSTRUCTION AREA IN SUCH A MANNER AS TO INDICATE THEIR COURSE TOGETHER WITH THE APPROXIMATE DEPTH AT WHICH THEY WERE INSTALLED. THE MARKING OR LOCATION SHALL OCCUR APPROXIMATELY TWO DAYS AHEAD OF THE PLANNED CONSTRUCTION.

OHIO UTILITIES PROTECTION SERVICE
CITY OF SHAKER HEIGHTS SERVICE DEPARTMENT
CLEVELAND WATER - ROBERT SMITH
NORTHEAST OHIO REGIONAL SEWER DISTRICT
AT&T — ERIC WESTERBURG
DOMINION EAST OHIO GAS - JOE HINTON
TIME WARNER CABLE - LARRY BOCK
AMERICAN FIBER SYSTEMS - BRYCE BASISTA
THE ILLUMINATING COMPANY - JASON R. STEC
XO COMMUNICATIONS

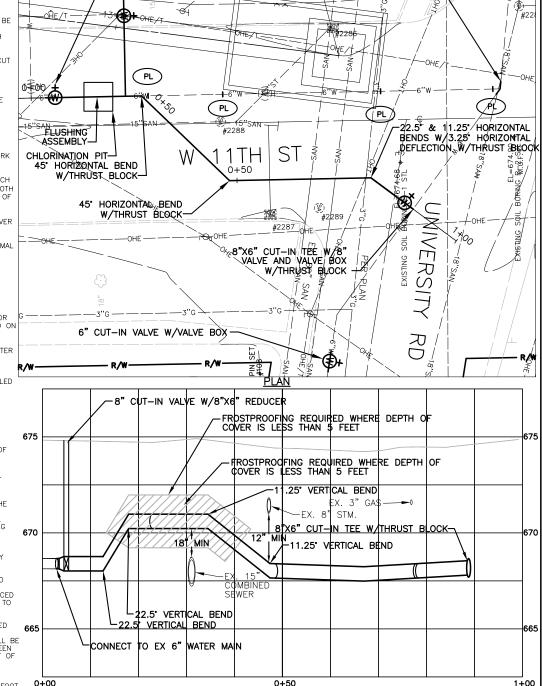
- 2. THE LOCATION OF THE EXISTING UNDERGROUND UTILITIES ARE SHOWN ON THE PLANS AND BELIEVED TO ESSENTIALLY CORRECT. THE LOCATIONS WERE OBTAINED FROM THE OWNERS OF THE UTILITIES AS REQUIRED BY SECTION 153.64 O.R.C. NO GUARANTEE IS MADE RELATIVE TO THE COMPLETENESS OR ACCURACY AND THE CONTRACTOR IS REQUIRED TO CONTACT THE REGISTERED UTILITY PROTECTION SERVICE AND THE OWNERS OF EACH UNDERGROUND UTILITY FACILITY SHOWN ON THE PLANS AT LEAST TWO WORKING DAYS PRIOR TO COMMENCING CONSTRUCTION IN ANY AREA.
- 3. ALL EXISTING UTILITIES, SERVICES, POLES AND CONNECTIONS SHALL BE PROTECTED AT THE CONTRACTOR'S EXPENSE. IF DAMAGE IS CAUSED BY CONSTRUCTION TO ANY EXISTING UTILITY, THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE REPAIR OR RESTORATION OF SAME AT HIS EXPENSE IN ACCORDANCE WITH DIRECTIONS OF THE ENGINEERS, AND FOR ANY RESULTING CONTINGENT DAMAGES. EXISTING UTILITIES INCLUDE, BUT ARE NOT LIMITED TO WATER MAINS, STORM SEWERS, SANITARY SEWERS, GAS, ELECTRICAL, TELEPHONE, FIBER OPTIC CABLE, TELEVISION CABLE, AND INDIVIDUAL
- 4. PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL EXPOSE ALL EXISTING UTILITIES SERVICES, OR STRUCTURES TO VERIFY THE VERTICAL AND HORIZONTAL LOCATION OF THE UTILITY, SERVICE, OR STRUCTURE AND ITS EFFECT ON THE PROPOSED CONSTRUCTION. THE CONTRACTOR SHALL COORDINATE HIS WORK WITH THE UTILITY OWNER.
- 5. INDIVIDUAL STORM, SANITARY, GAS, WATER, ELECTRICAL, TELEPHONE AND CABLE SERVICE CONNECTIONS MAY NOT BE SHOWN. THE CONTRACTOR SHALL LOCATE AND PROTECT SERVICE CONNECTIONS THROUGHOUT THE COURSE OF THE WORK. IN THE EVENT SERVICE CONNECTIONS INFOOGNOOF THE COURSE OF THE WORK. IN THE EVENT SERVICE CONNECTIONS ARE BROKEN OR DISTURBED, THE CONTRACTOR SHALL REPAIR OR REPLACE THE SERVICE CONNECTIONS TO THE SATISFACTION OF THE ENGINEER AT NO ADDITIONAL COST TO THE OWNER. THE CONTRACTOR SHALL EXPECT EACH RESIDENCE/COMMERCIAL PROPERTY ALONG THE ROUTE TO HAVE AT LEAST ONE SERVICE CONNECTION FOR EACH UTILITY.
- 6. EXISTING LATERAL CONNECTIONS SHOWN ARE APPROXIMATE. CONTRACTOR SHALL LOCATE TO DETERMINE LOCATION AND NUMBER OF LATERALS. NOT ALL LATERALS MAY BE SHOWN.
- 7. THE COST OF RELOCATION AND/OR SECURING ANY UTILITY POLES AS NECESSARY TO COMPLETE THE WORK SHALL BE INCLUDED IN THE BID PRICE PER LINEAL FOOT OF WATER MAIN. THE UTILITY MUST BE INFORMED BY THE CONTRACTOR OF THE PROPOSED METHODS BEFOREHAND TO VERIFY THE ADEQUACY OF SUCH SUPPORTS. NOTE THE OSHA REGULATIONS PROHIBIT CRANE/ BACKHOE OPERATIONS WITHIN TEN FEET OF THE ENERGIZED PRIMARY CONDUCTORS. CONTRACTOR MAY ELECT TO PAY THE UTILITY TO PERFORM THIS WORK AT NO ADDITIONAL COST TO OWNER.
- 8. STORM SEWER, SANITARY SEWER, AND CULVERT INVERTS SHOWN ON THE PLANS ARE APPROXIMATE. CONTRACTOR SHALL FIELD VERIFY DEPTHS AND LOCATIONS PRIOR TO CONSTRUCTION.
- 9. THE CONTRACTOR SHALL REPAIR AT HIS OWN COST ANY DAMAGE TO TRAFFIC SIGNAL LOOP DETECTORS. CONTRACTOR SHALL FIELD VERIFY ALL LOOP DETECTORS WITHIN PROJECT AREA.
- 10. THE CONTRACTOR MAY DAMAGE EXISTING CATCH BASINS WHILE INSTALLING THE WATER MAIN. THE CONTRACTOR SHALL REPAIR OR REPLACE DAMAGED CATCH BASINS TO THE SATISFACTION OF THE CITY OF SHAKER HEIGHTS.

# PAVEMENTS AND WALKS:

- ROADWAYS, DRIVES, AND PAVEMENTS DISTURBED BY CONSTRUCTION SHALL BE REPLACED. SEE DETAILS ON PLANS AND SPECIFICATIONS. TEMPORARY PAVEMENT SHALL BE USED WHEN HOT MIX ASPHALT IS NOT AVAILABLE OR WHEN WEATHER FOR PAVEMENT IS UNACCEPTABLE. SIDEWALKS AND DRIVEWAY APRONS SHALL BE
- 2 THE CONTRACTOR MAY DAMAGE EXISTING ROADWAY CURRING WHILE INSTALLING THE WATER MAIN. THE CONTRACTOR SHALL REPLACE ANY DAMAGED CURBING ALONG ALL ROADS WITH ODOT 609 CURBING. CURB REPLACEMENT SHALL MATCH EXISTIN CURB, AND LIMITS OF REPLACEMENT SHALL BE TO THE NEAREST CONTROL JOINT ON EITHER SIDE OF THE AREA DAMAGED.
- 3. THE CONTRACTOR MAY DAMAGE EXISTING DRIVE APRONS WHILE INSTALLING THE WATER MAIN, DRIVE APRONS SHALL BE REMOVED AND REPLACED TO THE NEAREST JOINT. PAVEMENT TYPE AND THICKNESS SHALL MATCH EXISTING.
- 4. EXISTING SANDSTONE WALKS THAT MAY BE AFFECTED BY CONSTRUCTION SHALL BE SALVAGED AND RESET IF STONE WALKS ARE DAMAGED DURING CONSTRUCTION THEY SHALL BE REMOVED TO THE NEAREST JOINT AND REPLACED IN KIND WITH
- 5. WHERE NECESSARY TO DISTURB PAVEMENTS OR DRIVES, PAVEMENT SHALL BE CUT

### SUPPLEMENTAL WATER MAIN NOTES:

- 1. ALL NEW VALVES SHALL OPEN BY TURNING CLOCKWISE. VALVES SHALL BE SAME SIZE AS THE WATER MAIN. ALL VALVE BOXES SHALL BE INSTALLED FLUSH TO GRADE.
- THE MAXIMUM TRENCH OPENING SHALL NOT EXCEED 100 LINEAL FEET. WHERE ACCESS TO DRIVES AND PARKING LOTS IS HINDERED OR BLOCKED FOR AN EXTENDED PERIOD OF TIME, THE CONTRACTOR SHALL PROVIDE TEMPORARY BITUMINOUS PAVEMENT TO MAINTAIN ACCESS. CONTRACTOR SHALL KEEP ALL WORK WITHIN THE RIGHT-OF-WAY.
- 3. THE CONTRACTOR SHALL INSTALL DETECTABLE TRACER TAPE IN THE SAME TRENCH WITH ALL WATER MAINS. TAPE SHALL BE 3" WIDE, BLUE CODED POTABLE ON BOTH-SIDES, TRACER TAPE SHALL BE INCLUDED IN THE PRICE BID PER LINEAL FOOT OF
- 4. UNLESS OTHERWISE NOTED. THE NEW WATER MAIN SHALL HAVE 6' MINIMUM COVER OVER THE TOP OF PIPE.
- 5. A MINIMUM OF 35 PSI SHALL BE MAINTAINED TO THE CURB STOP DURING NORMAL OPERATING CONDITIONS.
- 6. BOOSTER PUMPS ARE NOT PERMITTED ON SERVICE CONNECTIONS
- 7 PIPE JOINTS SHALL BE DEFLECTED TO MAINTAIN HORIZONTAL ALIGNMENT AND VERTICAL ELEVATIONS UNLESS OTHERWISE INDICATED. DEFLECTIONS SHALL NOT EXCEED THE PIPE MANUFACTURERS RECOMMENDATIONS.
- 8. CONTRACTOR SHALL ESTABLISH AND STAKE OUT THE WATER MAIN ALIGNMENT FOR CONSTRUCTION FROM THE HORIZONTAL AND VERTICAL CONTROL AS REFERENCED ON THE DRAWINGS.
- ALL COSTS ASSOCIATED WITH ABANDONING AND/OR REMOVING THE EXISTING WATER MAIN, LINE VALVES, OR SERVICE CONNECTIONS SHALL BE INCLUDED IN THE BID PRICE PER LINEAL FOOT OF WATER MAIN.
- 10. NEW FIRE HYDRANTS SHALL BE BAGGED UNTIL THE NEW WATER MAIN IS INSTALLED
- 11. THE WATER MAIN SHALL BE PRESSURE TESTED AND DISINFECTED PRIOR TO PERFORMING CORPORATION STOP TAPS.
- 12. FIRE HYDRANT PLACEMENT SHALL BE ESTABLISHED BY GOVERNING FIRE
- 13. CONTRACTOR SHALL PRESSURE TEST AND DISINFECTION TEST WITHIN 15 DAYS OF WATER MAIN INSTALLATION.
- 14. ANY EXISTING UTILITIES OR APPURTENANCES INSIDE OR OUTSIDE OF THI CONSTRUCTION LIMITS DAMAGED DURING CONSTRUCTION SHALL BE REPLACED AT THE CONTRACTOR'S EXPENSE.
- 15. GROUNDWATER CONTROL MEASURES SHALL BE IN PLACE PRIOR TO THE TIME THE EXCAVATION REACHES THE GROUNDWATER LEVEL TO MAINTAIN INTEGRITY OF THE IN—SITU MATERIALS. WHILE THE EXCAVATION IS OPEN, THE GROUNDWATER LEVEL SHALL BE MAINTAINED CONTINUOUSLY AT 2 FEET OR MORE BELOW THE WORKING
- 16 UNSTABLE OR UNSUITABLE PIPE FOUNDATION CONDITIONS THAT RESULT FROM INADEQUATE OR INAPPROPRIATE DEWATERING METHODS SHALL BE CORRECTED BY THE CONTRACTOR AT NO COST TO THE OWNER.
- THE CONTRACTOR SHALL REMOVE ALL GUARDRAIL AND FENCE AS NECESSARY TO FACILITATE CONSTRUCTION OF THE PROPOSED WATER MAIN, ANY GUARDRAIL OR FENCE DAMAGED DURING CONSTRUCTION BY THE CONTRACTOR SHALL BE REPLACED IN COMPLETE LENGTH AND KIND BY THE CONTRACTOR AT NO ADDITIONAL COST TO
- 18. ANY EXISTING PROPERTY CORNER PINS OR MONUMENTS DAMAGED OR DESTROYED BY THE CONSTRUCTION SHALL BE RESET BY A REGISTERED SURVEYOR UPON COMPLETION OF THE PROJECT PRIOR TO FINAL PAYMENT. A CERTIFICATION SHALL BI FURNISHED BY A REGISTERED SURVEYOR, STATING THAT SAID DAMAGES HAVE BEEN RESTORED. THE COST SHALL BE INCLUDED IN THE PRICE BID PER LINEAL FOOT OF
- 19. CONTRACTOR SHALL GRADE AND RESLOPE ALL DITCHES DISTURBED DURING CONSTRUCTION. THE COST SHALL BE INCLUDED IN THE PRICE BID PER LINEAL FOOT OF WATER MAIN.
- 20. ACCESS TO ADJOINING PROPERTIES SHALL BE MAINTAINED AT ALL TIMES.
- 21. UNLESS MARKED FOR REMOVAL, SPECIAL CARE SHALL BE TAKEN TO AVOID DAMAGE TO TREES AND THEIR ROOT SYSTEMS. IN GENERAL, WHERE THE TRENCH FALLS WITHIN THE LIMITS OF THE LIMB SPREAD, THE LEAVING OF HEADERS ACROSS TO PROTECT ROOTS WILL BE REQUIRED. THE OPERATION OF ALL EQUIPMENT, PARTICULARLY WHEN EMPLOYING BOOMS, THE STORAGE OF MATERIALS, AND DEPOSITION OF EXCAVATION SHALL BE CONDUCTED IN A MANNER WHICH WILL NOT INJURE TREE TRUNKS, BRANCHES, OR ROOTS UNLESS SUCH TREES ARE DESIGNATED BY THE MUNICIPALITY'S CHEENINGTON OF CREETING FOR PROVING BY THE MUNICIPALITY'S SUPERINTENDENT OF FORESTRY FOR REMOVAL.



6" CUT-IN VALVE W/VALVE BOX -

REMOVE EX. 6"X6" TEE\_AND/

12.51

INSTALL 6" \$POOL PIECES
W/22.5" BEND W/THRUST BLOCK

TO CONNECT TO EX 6" WATER MAIN

CR-1 REPLACE EXISTING CONNECTION, SHORT SIDE, (1" AND UNDER) WITH 1" COPPER CONNECTION, INCLUDING CURB VALVE AND VALVE BOX

(CR-1)

ADDRESS #1103 UNIVERSITY

I'CUT−IN VALVE W∕VALVÉ

BDX W/8"X6" REDUCER

RETAP AND RECONNECT

' WSC #4775

PL PLUG EXISTING WATER MAIN END

BAR IS ONE INCH ON IF NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY PROJECT NO.

DESIGNED BY: RAWN BY HEET CHK'D BY CROSS CHK'D BY:\_ PPROVED BY:\_\_\_ DATE: \_ DATE REMARKS





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(216) 491-1490 (216) 664-2444

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WALWORTH RUN INTERCEPTOR REALIGNMENT

WATER MAIN RELOCATION PLAN AND NOTES

PROFILE ALONG WATER MAIN/ W 11TH ST

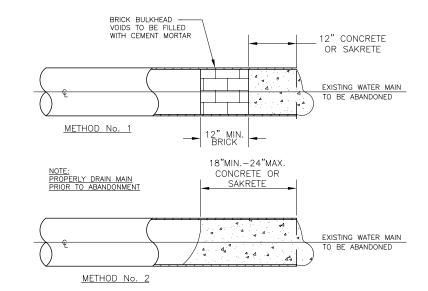
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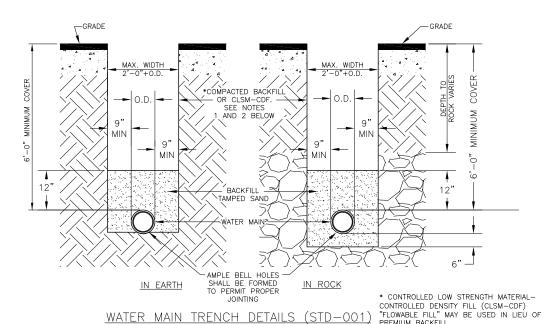
# SUPPLEMENTAL WATER MAIN NOTES: (CONTINUED)

- 22. THE CONTRACTOR SHALL BE RESPONSIBLE FOR MAINTAINING MAIL SERVICE IN THE CONSTRUCTION AREA. PRIOR TO DISTURBING ANY MAIL BOXES, THE CONTRACTOR SHALL CONTRACT THE POSTAL AUTHORITIES AND SHALL TEMPORARILY RELOCATE MAIL BOXES IN ACCORDANCE WITH THEIR REQUIREMENTS. THE CONTRACTOR SHALL RESTORE MAIL BOXES TO THEIR ORIGINAL CONDITION AND LOCATION. COST OF SAME SHALL BE INCLUDED IN THE UNIT PRICE PER LINEAL FOOT OF WATER MAIN.
- 23. RIGHT-OF-WAY AND PROPERTY LINES SHOWN WERE PREPARED FROM RECORD INFORMATION AND DO NOT REPRESENT A BOUNDARY SURVEY.
- 24. THE BIDDER SHALL MAKE HIS OWN INVESTIGATIONS OF THE SITE CONDITIONS PRIOR TO SUBMITTING HIS PROPOSAL. IF THE BIDDER DESIRES TO OBTAIN ADDITIONAL INFORMATION AS TO SOIL CONDITIONS, HE MUST DO SO AT HIS OWN EXPENSE AND SECURE ALL APPLICABLE APPROVALS AND PERMITS.
- 25. CONTRACTOR SHALL KEEP ALL WORK WITHIN THE RIGHT-OF-WAYS AND EASEMENTS.
- 26. THE CONTRACTOR IS RESPONSIBLE FOR DISPOSAL OF ALL CONSTRUCTION DEBRIS INCLUDING BUT NOT LIMITED TO EXCESS SOIL, ROCK, OR ANY OTHER TYPE OF MATERIALS. THE CONTRACTOR SHALL NOT FILL ANY WETLANDS, LOWLANDS, FLOOD PLAINS, OR DRAINAGE WAYS WITH SAID DEBRIS.
- 27. THE CONTRACTOR SHALL REMOVE AND REINSTALL CULVERT AND/OR DRAINAGE PIPE AS NECESSARY TO FACILITATE CONSTRUCTION OF THE PROPOSED WATER MAIN. PROPER DRAINAGE MUST BE MAINTAINED AT ALL TIMES. ANY CULVERT OR DRAINAGE PIPE DAMAGED OR BROKEN DURING THE CONSTRUCTION BY THE CONTRACTOR SHALL BE REPLACED, COMPLETE IN LENGTH AND KIND BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
- 28. CONTRACTOR SHALL CLEAN THE ROADWAY AT THE END OF EACH DAY OF OPERATION OR EVERY 500 FEET OF INSTALLED WATER MAIN. CLEANING SHALL BE PERFORMED USING A POWER BROOM OR HYDROSPRAYER, OR AS DIRECTED BY THE ENGINEER.
- 29. THE CONTRACTOR SHALL OBTAIN ALL PERMITS REQUIRED FOR CONSTRUCTION, INCLUDING BUT NOT LIMITED TO EXCAVATION AND ROAD OPENINGS. PERMITS SHALL BE OBTAINED FROM THE CITY ENGINEER AND FROM ANY LOCAL GOVERNMENTAL OFFICIALS IN WHICH THE WORK IS BEING PERFORMED.
- 30. CONTRACTOR SHALL PERFORM ALL CLEAN—UP, ROCK REMOVAL, FINAL GRADING, AND SEEDING TO AREAS DISTURBED BY WORK ASSOCIATED WITH INSTALLATION OF NEW WATER MAIN.
- 31. CONTRACTOR SHALL PROPERLY NOTIFY PROPERTY OWNERS OF CONSTRUCTION ACTIVITIES THAT WILL IMPACT THEM.
- 32. CONTRACTOR SHALL NOT BE PERMITTED TO STORE MATERIALS, EQUIPMENT, OR VEHICLES ON PRIVATE PROPERTY.
- 33. THE CONTRACTOR SHALL BE RESPONSIBLE FOR REMOVING LANDSCAPE ITEMS SUCH AS SHRUBBERY, RAILROAD TIES, ETC. IN A MANNER SUITABLE FOR REPLANTING OR RELOCATION BY THE CONTRACTOR, OR AT THE OPTION OF THE PROPERTY OWNER, SHALL REMOVE AND DISPOSE OF THE LANDSCAPE ITEMS. THE COST FOR THE ABOVE RESTORATION SHALL BE INCLUDED IN THE BID PRICE PER LINEAL FOOT OF WATER MAIN.
- 34. THE CONTRACTOR SHALL PROVIDE TEMPORARY WATER MAINS AND SERVICE CONNECTIONS PER SPECIFICATION SECTION D-45. TEMPORARY MAINS SHALL BE LAID IN THE GUTTERLINES AND SHALL CROSS THE STREETS AT INTERSECTIONS. TEMPORARY MAINS SHALL NOT BE LAID ON TREELAWNS.

# CONSTRUCTION SEQUENCE



PLUGGING ABANDONED WATER MAIN ENDS (STD-004)

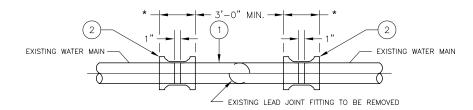


# NOTES:

PREMIUM BACKFILL CONSISTING OF CONTROLLED LOW STRENGTH MATERIAL — CONTROLLED DENSITY FILL (CLSM—CDF) "FLOWABLE FILL" IS BEGUIRED.

- NOT TO SCALE -

- A) UNDER ALL EXISTING OR FUTURE PAVEMENTS, SIDEWALKS AND DRIVES
- B) AT ALL LOCATIONS WITHIN THE CITY OF CLEVELAND CORPORATION LIMITS
  C) AS SPECIFIED IN LOCAL MUNICIPALITIES SERVED BY CWD (SEE LOCAL REQUIREMENTS)
- 2) WHEN PREMIUM BACKFILL IS REQUIRED BY THE LOCAL MUNICIPALITY FOR CASES OTHER THAN THOSE LISTED IN NOTE 1 ABOVE, IT SHALL BE LIMESTONE GRADED PER ODOT 304.02 OR ODOT 411. NO SLAG IS PERMITTED.\*
- 3) CONTRACTOR SHALL USE SPECIAL CARE IN PLACING THE SAND BEDDING, SO AS TO AVOID SCRAPING OF THE EXTERIOR COATING, INJURING THE PIPE, DISTORTING OR MOVING THE PIPE WHEN COMPACTING THE SAME. THE SAND BEDDING BACKFILL SHALL BE TAMPED IN SIX (6) INCH LAYERS, SIMULTANEOUSLY ON EACH SIDE OF THE PIPE, AND THOROUGHLY COMPACTED SO AS TO PROVIDE A SOLID BACKING AGAINST THE EXTERNAL SURFACE OF THE PIPE.
- 4) MINIMUM COMPACTION FOR ALL SAND BEDDING, BACKFILL AND PREMIUM BACKFILL SHALL BE 95% STANDARD PROCTOR.
- 5) PAVEMENT, SIDEWALK OR DRIVES TO BE INSTALLED IN ACCORDANCE WITH LOCAL MUNICIPALITY'S SPECIFICATIONS.



- 1) PLAIN END x PLAIN END DUCTILE IRON PIPE AS SPECIFIED (CUT TO SUIT).
- 2) \*CONNECTION SHALL BE MADE WITH RETAINED MECHANICAL JOINT SOLID SLEEVES (SHORT OR LONG PATTERN) DUCTILE IRON CLASS 350 OR CAST IRON CLASS 250 OR COMPRESSION COUPLINGS.

COMPRESSION COUPLINGS SHALL BE OF A GASKETED, SLEEVE TYPE WITH DIAMETERS TO PROPERLY FIT PLAIN END IRON PIPE. EACH COUPLING SHALL CONSIST OF ONE (1) MIDDLE RING, WITHOUT STOPS; TWO (2) FOLLOWER GLANDS; TWO (2) RUBBER-COMPOUND BUNA-N BLEND, WEDGE SECTION GASKETS; AND SUFFICIENT TRACKHEAD STAINLESS STEEL BOLTS AND NUTS (ASTM A276/A193/194, TYPE 304, EXTRA HEAVY HEX) TO PROPERLY COMPRESS THE GASKETS.

MIDDLE RING AND FOLLOWER GLANDS SHALL BE OF FITHER STEEL OR DUCTHE IRON (ASTM-A5.36).

THE COMPRESSION COUPLING SHALL BE WITHOUT STOPS AND BE RATED FOR A MINIMUM WORKING PRESSURE OF 250 PSI AND SHALL BE EQUAL TO THE DRESSER STYLE No's 38, 138 OR 162 (TRANSITION TYPE), OR SMITH—BLAIR 441 STRAIGHT AND TRANSITION COUPLINGS.

3) ALL BOLTS AND NUTS ON ALL MECHANICAL JOINTS, INCLUDING THOSE ON THE "RETAINED" TYPE, SHALL HAVE FIELD APPLIED ONE (1) COAT OF BITUMASTIC PAINTING FOLLOWED BY AN ENCASEMENT OF POLYETHYLENE WRAPPING IN ACCORDANCE WITH ANSI/AWWA C-105/A21.5-88, CLASS "C", METHOD "B".

# SPOOL PIECE INSTALLATION DETAIL (STD-008)

\*CONNECTION SHALL BE MADE WITH RETAINED MECHANICAL JOINT SOLID SLEEVES (SHORT OR LONG PATTERN) DUCTILE IRON CLASS 350 OR CAST IRON CLASS 250 OR COMPRESSION COUPLINGS.

COMPRESSION COUPLINGS SHALL BE OF A GASKETED, SLEEVE TYPE WITH DIAMETERS TO PROPERLY FIT PLAIN END IRON PIPE. EACH COUPLING SHALL CONSIST OF ONE (1) MIDDLE RING, WITHOUT STOPS: TWO (2) FOLLOWER GLANDS; TWO (2) RUBBER-COMPOUND BUNA-N BLEND, WEDGE SECTION GASKETS; AND SUFFICIENT TRACKHEAD STAINLESS STEEL BOLTS AND NUTS (ASTM A276/A193/194, TYPE 304, EXTRA HEAVY HEX) TO PROPERLY COMPRESS THE GASKETS.

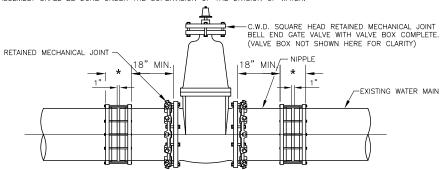
MIDDLE RING AND FOLLOWER GLANDS SHALL BE OF EITHER STEEL OR DUCTILE IRON (ASTM-A536).

THE COMPRESSION COUPLING SHALL BE WITHOUT STOPS AND BE RATED FOR A MINIMUM WORKING PRESSURE OF 250 PSI AND SHALL BE EQUAL TO THE DRESSER STYLE No'S 38, 138 OR 162 (TRANSITION TYPE), OR SMITH-BLAIR 441 STRAIGHT AND TRANSITION COURS INC.

ALL BOLTS AND NUTS ON ALL MECHANICAL JOINTS, INCLUDING THOSE ON THE "RETAINED" TYPE, SHALL HAVE FIELD APPLIED ONE (1) COAT OF BITUMASTIC PAINTING FOLLOWED BY AN ENCASEMENT OF POLYETHYLENE WRAPPING IN ACCORDANCE WITH ANSI/AWWA C-105/A21.5-88, CLASS "C", METHOD "E".

THE DIVISION OF WATER WILL DETERMINE THE FIELD LOCATION OF THE CUT-IN-VALVE ASSEMBLY. THE DIVISION OF WATER WILL ALSO SET THE TIME OF INSTALLATION OF THE CUT-IN-VALVE ASSEMBLY.

THE CONTRACTOR SHALL DO ALL PIPE CUTTING AND INSTALLATION. HOWEVER, THE INSTALLATION OF THE CUT-IN-VALVE ASSEMBLY SHALL BE DONE UNDER THE SUPERVISION OF THE DIVISION OF WATER.



NOTE: BEFORE CUTTING EXISTING WATER MAIN, THE NIPPLES SHALL BE CONNECTED TO THE MECHANICAL JOINT BELL END GATE VALVE. AFTER CUTTING PIPE, FINAL CONNECTIONS SHALL BE MADE WITH COUPLINGS/SOLID SLEEVES AS

CUT-IN-VALVE DETAIL (STD-005)







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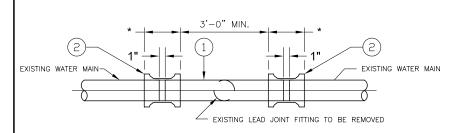
WALWORTH RUN INTERCEPTOR REALIGNMENT

WATER MAIN NOTES AND DETAILS

PROJECT NO.: SHEET:

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SCALE: NTS



- 1) PLAIN END x PLAIN END DUCTILE IRON PIPE AS SPECIFIED (CUT TO SUIT).
- 2) \*CONNECTION SHALL BE MADE WITH RETAINED MECHANICAL JOINT SOLID SLEEVES (SHORT OR LONG PATTERN) DÚCTILE IRON CLASS 350 OR CAST IRON CLASS 250 OR COMPRESSION COUPLINGS

COMPRESSION COUPLINGS SHALL BE OF A GASKETED, SLEEVE TYPE WITH DIAMETERS TO PROPERLY FIT PLAIN END IRON PIPE. EACH COUPLING SHALL CONSIST OF ONE (1) MIDDLE RING, WITHOUT STOPS; TWO (2) FOLLOWER GLANDS; TWO (2) RUBBER-COMPOUND BUNA-N BLEND, WEDGE SECTION GASKETS; AND SUFFICIENT TRACKHEAD STAINLESS STEEL BOLTS AND NUTS (ASTM A276/A193/194, TYPE 304, EXTRA HEAVY HEX) TO PROPERLY COMPRESS THE GASKETS.

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CITY OF CLEVELAND STANDARD 4" OR 6" HYDRANT. 6" WITH 1 - 4" STEAMER NOZZLE WITH HOSE ADAPTER SHOWN.

-4" I.D STEAMER NOZZLE ADAPTER

(PENTAGON NUT POINT TO FLAT 1-1/8", HEIGHT 1", FLAT 3/4" WIDE)

4" TEMPORARY WATER MAIN (BY PASS) FOR DOMESTIC AND

TEMPORARY FIRE HYDRANT SUPPLY OR 2" TEMPORARY WATER MAIN FOR DOMESTIC SUPPLY ONLY.

4" VALVE FOR FIRE HYDRANT CONTROL WITH

TEMPORARY WATER MAIN & HYDRANT CONNECTION ASSEMBLY-A

TO PROVIDE SIMULTANEOUS SERVICE IN EXISTING HYDRANT AND TEMPORARY BYPASS MAIN (STD-H14)

- NOT TO SCALE -

1/4 TURN "ON-OFF" STOPS. OPERATING NUT SHALL BE CLEVELAND FIRE HYDRANT STANDARD.

4" STEAMER NOZZLE

2-1/2" MATCHING HOSE NOZZLE CAP

NOTE: THREAD PATTERN FOR STEAMER AND

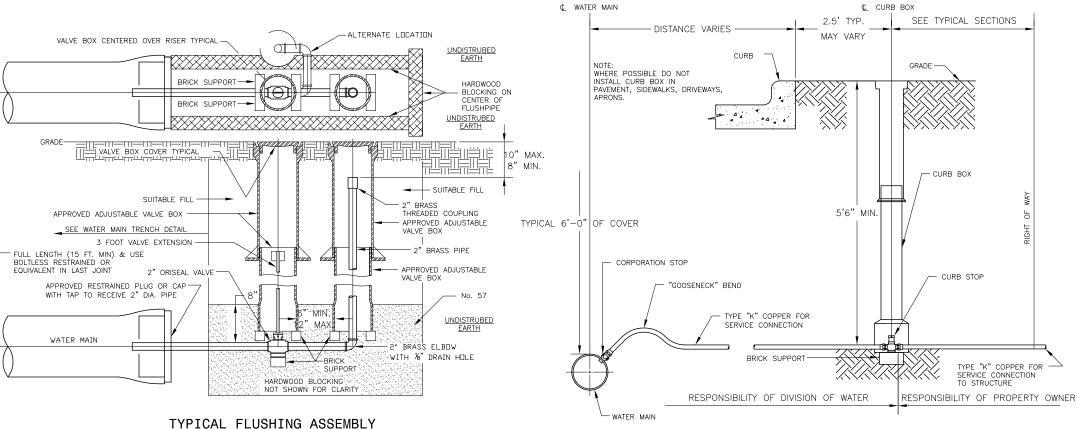
HOSE NOZZLES IS EITHER CLEVELAND STANDARD OR NATIONAL STANDARD THREAD (NST)

-4" LD. STFAMER NO77LF OR

"VICTAULIC" JOINT COUPLINGS ARE SHOWN FOR ASSEMBLY

2-1/2" HOSE NOZZLE ADAPTER

SPOOL PIECE INSTALLATION DETAIL (STD-008) -NOT TO SCALE-



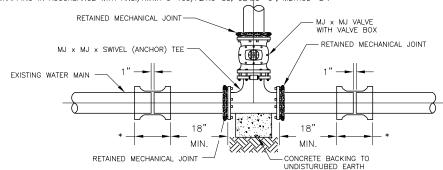
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COMPRESSION COUPLINGS SHALL BE OF A GASKETED, SLEEVE TYPE WITH DIAMETERS TO PROPERLY FIT PLAIN END IRON PIPE. EACH COUPLING SHALL CONSIST OF ONE (1) MIDDLE RING, WITHOUT STOPS; TWO (2) FOLLOWER GLANDS; TWO (2) RUBBER-COMPOUND BUNA-N BLEND, WEDGE SECTION GASKETS; AND SUFFICIENT TRACKHEAD STAINLESS STEEL BOLTS AND NUTS (ASTM A276/A193/A194, TYPE 304, EXTRA HEAVY HEX) TO PROPERLY COMPRESS THE GASKETS.

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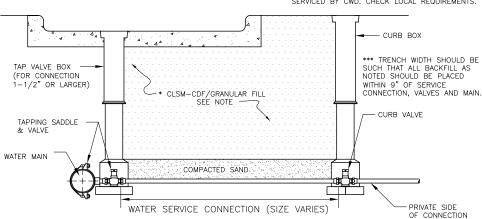


CUT-IN TEE DETAIL METHOD No.1 STD-T01 NOT TO SCALE

NEW 1" SERVICE CONNECTION DETAIL IN PUBLIC RIGHT OF WAY (STD-CO4)

\*\* CLEVELAND REQUIRED MIX DESIGN -CEMENT - 50 LBS. PER CUBIC YARD SAND - 2850 LBS. PER CUBIC YARD 50 GALLONS PER CUBIC YARD RHEOCELL 30MB - 3 OZ, PER CUBIC YARD

\* CONTROLLED LOW STRENGTH MATERIAL-CONTROLLED DENSITY FILL (CLSM-CDF) "FLOWARLE FILL" IS REQUIRED WITHIN THE CITY OF CLEVELAND CORPORATION LIMITS
AND PERMITTED IN ALL COMMUNITIES
SERVICED BY CWD. CHECK LOCAL REQUIREMENTS.



- 1) CONTRACTOR SHALL USE SPECIAL CARE IN PLACING THE SAND BEDDING BACKFILL, SO AS TO AVOID SCRAPING OF THE EXTERIOR COATING, INJURING THE PIPE, DISTORTING OR MOVING THE PIPE WHEN COMPACTING THE SAME. THE SAND BEDDING BACKFILL, SHALL BE TAMPED IN SIX (6) INCH LAYERS, SIMULTANEOUSLY ON EACH SIDE OF THE PIPE, AND THOROUGHLY COMPACTED SO AS TO PROVIDE A SOLID BACKING AGAINST THE EXTERNAL SURFACE OF THE PIPE.
- 2) MINIMUM COMPACTION FOR ALL SAND BEDDING BACKFILL, BACKFILL AND PREMIUM BACKFILL SHALL BE 95% STANDARD PROCTOR.

SERVICE CONNECTION BACKFILL DETAIL (STD-023) - NOT TO SCALE -

DESIGNED BY RAWN BY HEET CHK'D BY CROSS CHK'D BY: PPROVED BY:\_\_ DATE: DATE REMARKS





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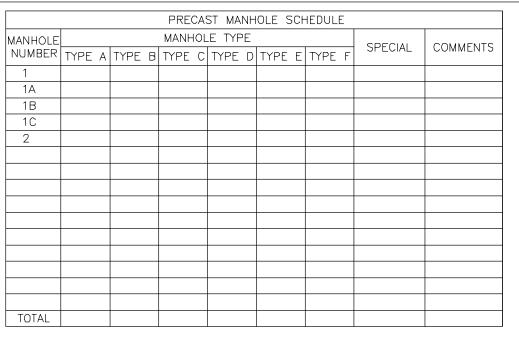
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WATER MAIN RELOCATION DETAILS

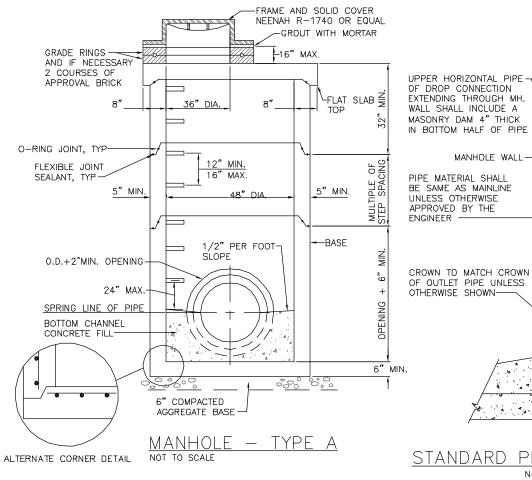
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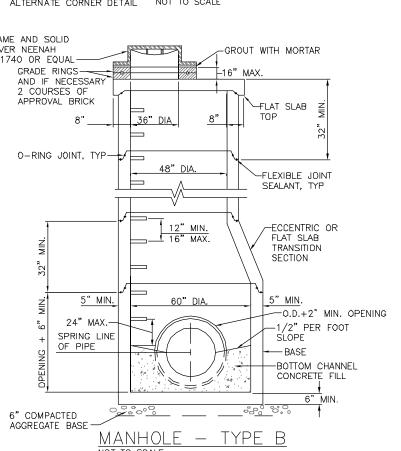
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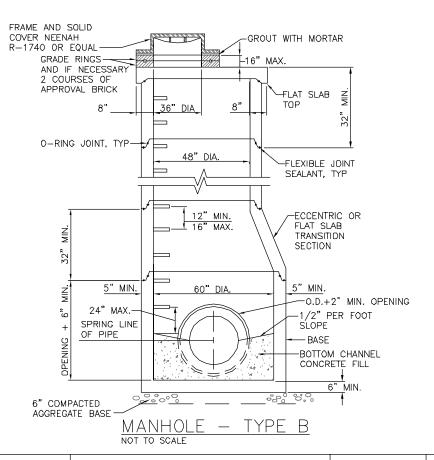


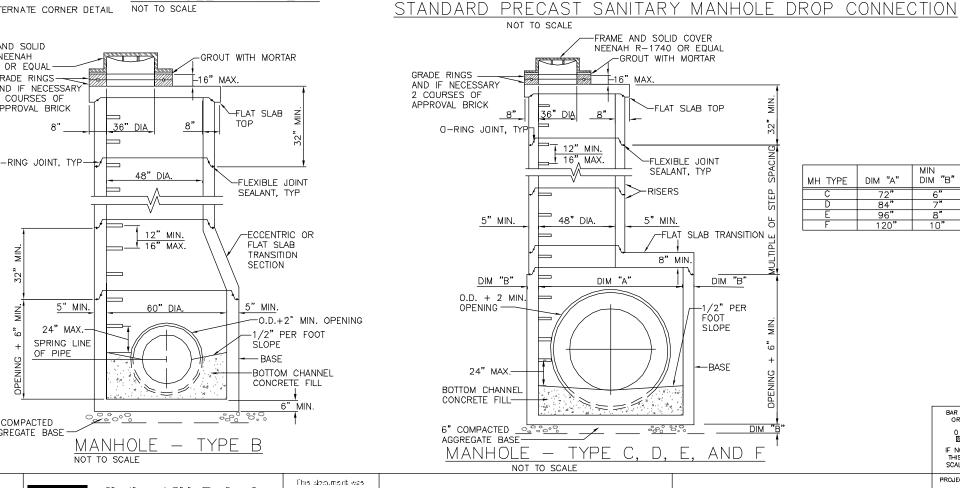
# **NOTES**

- SECTIONS OF THE PRECAST MANHOLE SHALL BE CAST AND ASSEMBLED WITH EITHER ALL TONGUE OR ALL GROOVE ENDS UP. LIFT HOLES MAY BE PROVIDED IN EACH SECTION FOR HANDLING.
- 2. BASES FOR MANHOLES ARE SHOWN WITH MONOLITHIC FLOOR AND RISERS WHICH MAY BE CAST IN ONE OR TWO OPERATIONS, A PERMISSIBLE ALTERNATE IS TO CAST AND SHIP THE FLOOR AND BARREL SEPARATELY. OPENINGS FOR INLET AND OUTLET PIPES SHALL BE PROVIDED, EITHER WHEN THE UNIT IS CAST OR LATER TO MEET PROJECT REQUIREMENTS, BOTTOM CHANNELS MAY BE FORMED OF CONRETE PRECAST IN THE BASE OR INSTALLED BY FIELD CONSTRUCTION. FLOORS MAY ALSO BE POURED IN PLACE.
- 3. OPENINGS IN RISER SECTIONS SHALL BE PREFABRICATED. FLEXIBLE CONNECTIONS SHALL BE PROVIDED FOR SANITARY AND STORM SEWERS. PREMIUM SEALS SHALL MEET ASTM C-923.
- JOINT SEALS BETWEEN PRECAST MANHOLE SECTIONS SHALL BE RESILENT AND FLEXIBLE GASKET JOINTS. JOINTS SHALL MEET ASTM C-443, FEDERAL SPECIFICATION SS-S-00210 (210 A), AND AASHTO
- MANHOLE JOINTS SHALL BE SEALED BY A FLEXIBLE SEALANT, CONSEAL CS-202 AS MANUFACTURED BY 5. CONSEAL CONCRETE SEALANTS, INC., OR APPROVED
- 6. MANHOLE GRADE RINGS SHALL BE SEALED EXTERNALLY AND BETWEEN GRADE RINGS WITH A LAYER OF MASTIC COMPOUND SUCH AS FABERLITE, KENT SEAL, OR EQUAL
- 7. PRECAST MANHOLES SHALL CONFORM TO THE REQUIREMENTS OF ASTM C-478.
- 8. SEAL ALL LIFT HOLES WITH APPROVED CONCRETE PLUGS
- 9. SEE PLANS FOR FRAME AND COVER ELEVATIONS.
- 10. TOP MANHOLE STEP SHALL BE INSTALLED NOT MORE THAN 2' BELOW TOP OF FRAME.
- 11. APPLY "THOROSEAL" BY THORO SYSTEM PRODUCTS, OR APPROVED EQUAL TO THE INSIDE EXPOSED SURFACES OF ALL MANHOLES.















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WALWORTH RUN INTERCEPTOR REALIGNMENT

TABLE OF DIMENSIONS

-TEE

PLAN

MANHOLE WALL

PIPE MATERIAL ADAPTER

-PIPE

RFAM

2'-0" SET ON

UNDISTURBED

STIRRUPS

@ 12" CENTERS-

#6 BAR

GROUND

COMPACTED GRANGULAR

BACKFILL UNDER PIPE SUPPORT BEAM

CLASS "A" CONCRETE

90° ELBOW

SUPPORT

**→** B

**⊸** В

(IF REQUIRED)

PRECAST CONCRETE MANHOLE DETAILS

IF NOT ONE INCH ON THIS SHEET, ADJUST SCALES ACCORDINGLY PROJECT NO.: SHEET:

DIM "B"

-RAMSET THREADER STUD

-CLASS "A" CONCRETE

#4 BARS

@ 12" CENTERS

END SMOOTH

REINFORCING

STEEL @ 12"

CENTERS

NO. 3440 A HEX. STRAIGHT THROUGH

NO. 1223 OR EQUAL

COUPLING

6 (AD) 1

SECTION A-A

SECTION B-B

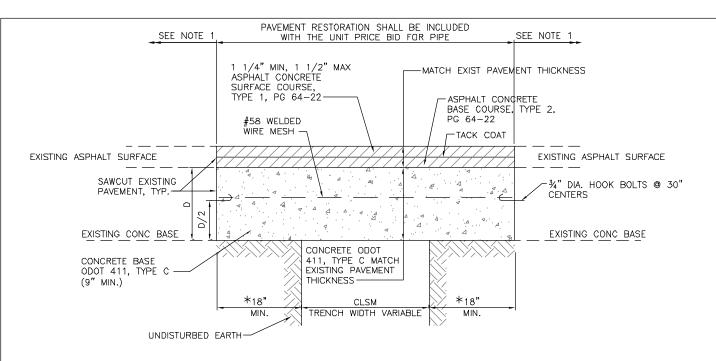
DIM "A"

MH TYPE

SCALE: NONE

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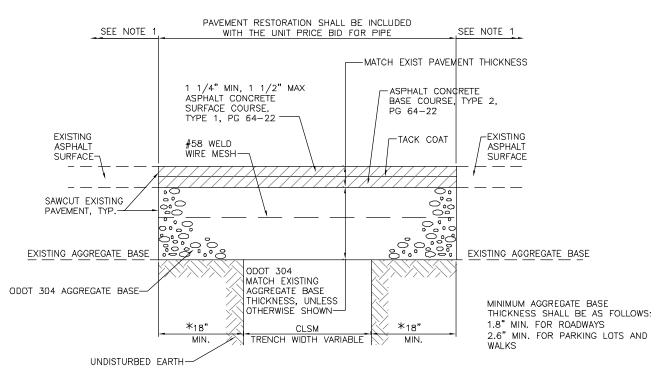
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\*CONTINUE PAVEMENT REPLACEMENT TO CURB WHERE SAWCUT OCCURS LESS THAN 3' FROM FACE OF CURB

# TYPICAL TRENCH DETAIL FOR ASPHALT PAVEMENT WITH CONCRETE BASE

NOT TO SCALE



\*CONTINUE PAVEMENT REPLACEMENT TO CURB WHERE SAWCUT OCCURS LESS THAN 3' FROM FACE OF CURB

# TYPICAL TRENCH DETAIL FOR ASPHALT PAVEMENT WITH AGGREGATE BASE

NOT TO SCALE

DESIGNED BY: DRAWN BY:\_ SHEET CHK'D BY: CROSS CHK'D BY APPROVED BY: REV. DATE ISSUE BY





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NOT TO SCALE

REMOVE EXISTING CONCRETE

SIDEWALK AND REINFORCING

REMOVAL

EXISTING 4" TO 6"

THICK CONCRETE

WALWORTH RUN INTERCEPTOR REALIGNMENT

PAVEMENT WITH BRICK BASE

TYPICAL TRENCH DETAIL FOR ASPHALT

# TRENCH REPAIR DETAILS

PROJECT NO.: SHEET:

INCLUDED WITH THE UNIT PRICE BID

FOR PAVEMENT MILLING AND

RESURFACING

SCALE: NONE SHEET NO.: C-10

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LEVELING COURSE DEPTH AS

REQUIRED TO ESTABLISH

-COMPACTED SUBGRADE

SAWCUT OCCURS LESS THAN 3' FROM FACE OF CURB

GRADES

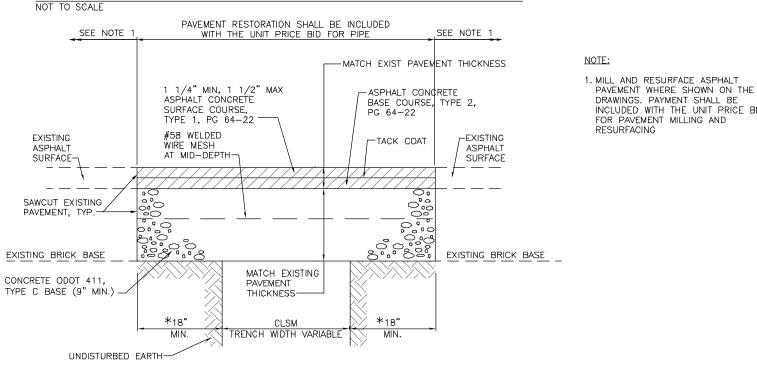
REPLACEMENT

SIDEWALK SIDEWALK REMOVAL AND REPLACEMENT -CONCRETE ODOT 411, TYPE C MATCH EXIST. MIN. D/4" DEEP X 1/4" PAVEMENT THICKNESS -IF 5'-0" OR LESS WIDE JOINT TO BE SÉALED UNLESS OTHERWISE SHOWN REMOVE TO PAVEMENT JOINT W/ODOT ITEM 705.04 OR TO EXISTING CURB SÉALANT, TYP.-#58 WFLDED WIRE MESH-EXIST. CONCRETE EXIST. CONCRETE PAVEMENT PAVEMENT SAWCUT EXIST. 3/4" DIA. HOOK BOLTS @ 30" CENTERS. PAVEMENT, TYP. OMIT HOOK BOLTS FOR SIDEWALKS WHERE "D" IS 6" OR LESS. UNDISTURBED EARTH MINIMUM PAVEMENT THICKNESS SHALL BE AS FOLLOWS: \*18" 1. 9" MIN. FOR ROADWAY MIN. RENCH WIDTH MIN 6" MIN. FOR DRIVEWAYS OR PARKING AREAS VARIABLE 4" MIN. FOR SIDEWALKS \*CONTINUE PAVEMENT REPLACEMENT TO CURB WHERE

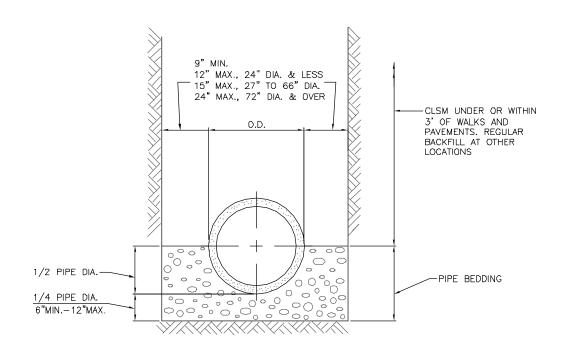
4" FIBER REINFORCED

CONCRETE

# TYPICAL TRENCH DETAIL FOR CONCRETE PAVEMENT



\*CONTINUE PAVEMENT REPLACEMENT TO CURB WHERE SAWCUT OCCURS LESS THAN 3' FROM FACE OF CURB



TYPICAL SEWER TRENCH FOR RCP AND VCP

NOT TO SCALE

DESIGNED BY:\_\_ DRAWN BY:\_\_\_ SHEET CHK'D BY:-CROSS CHK'D BY:\_ APPROVED BY:\_ REV. DATE ISSUE BY DATE: \_\_\_





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WALWORTH RUN INTERCEPTOR REALIGNMENT

**CIVIL DETAILS** 

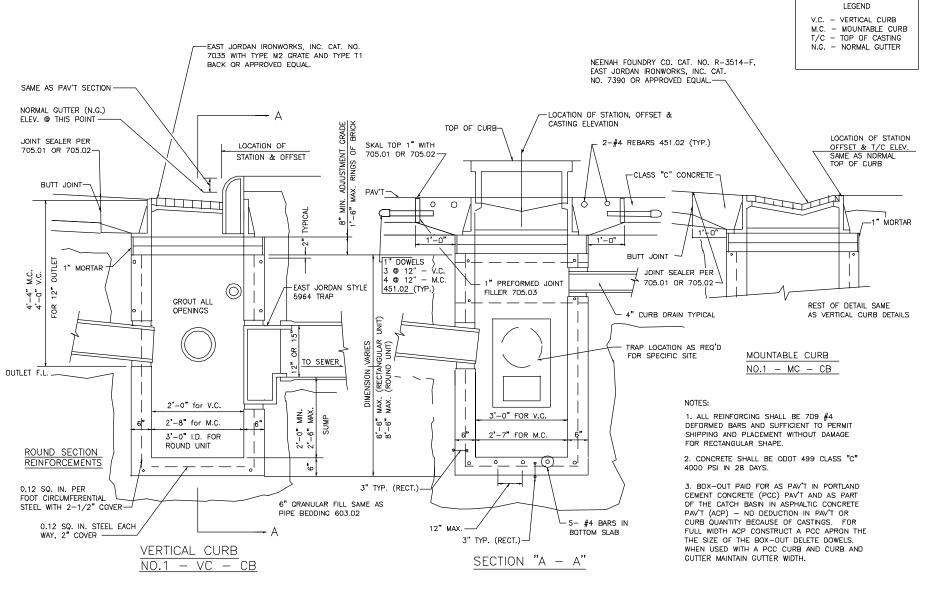
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SHEET NO.: C-11



# ALTERNATE BASIN SHAPE

A ROUND PRECAST CONCRETE UNIT MAY BE USED IN LIEU OF RECTANGULAR UNIT. THE ROUND SECTION SHALL BE A 36" I.D. UNIT WITH INTEGRAL BASE AND PRECAST TOP TRANSITION (ROUND TO RECTANGULAR) SECTION TO FIT CASTING BEING USED. TRANSITION UNIT REQUIRES A #5 REBAR AT CORNERS OF RECTANGULAR SHAPED SECTION AND 3 x 8 W6 X X W5 WELDED WIRE FABRIC IN VERTICAL SECTION.

CITY OF CLEVELAND STANDARD CATCH BASIN NOT TO SCALE





considered a sealed

WALWORTH RUN INTERCEPTOR REALIGNMENT CITY OF CLEVELAND CATCH BASIN DETAIL

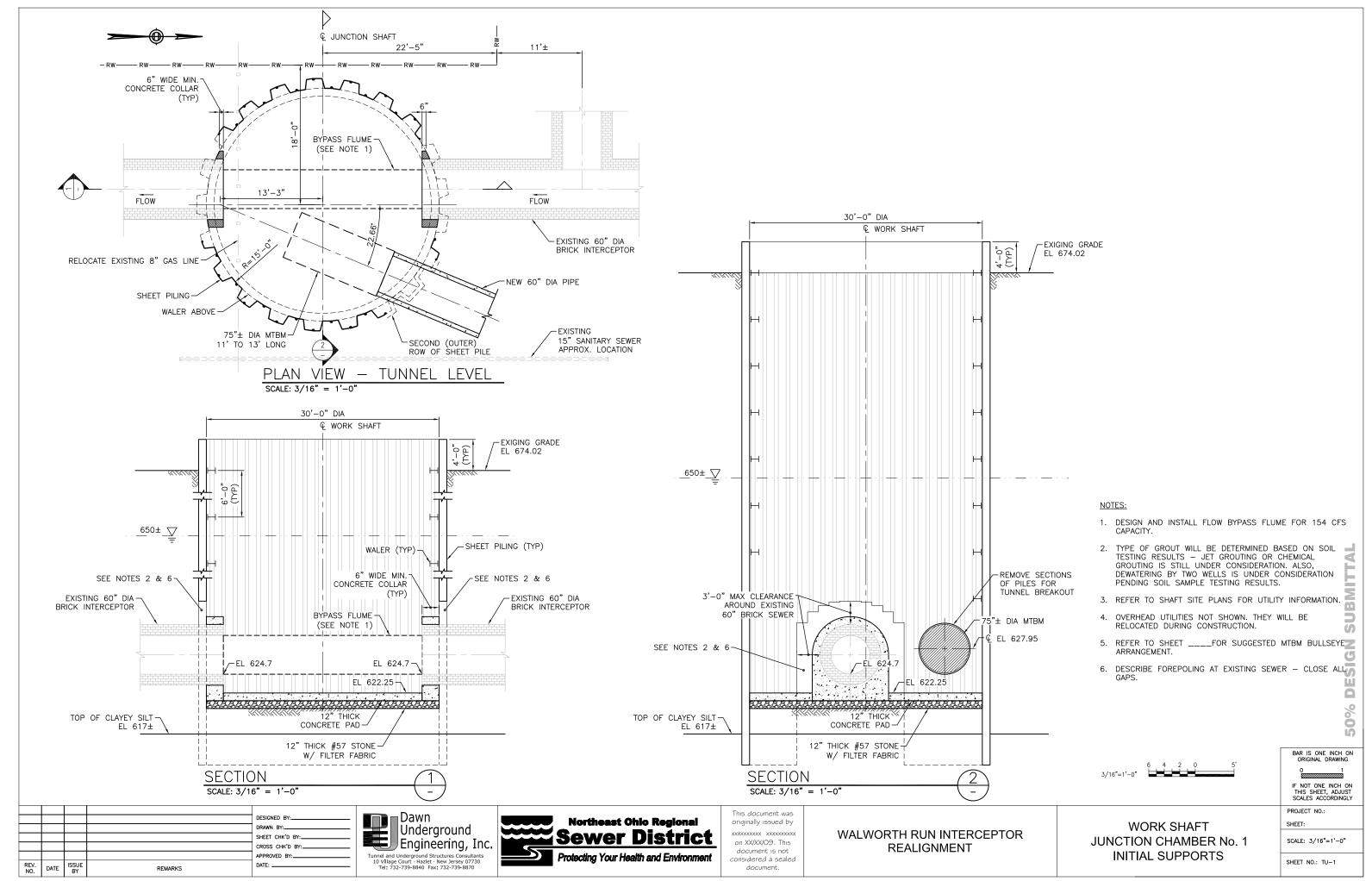
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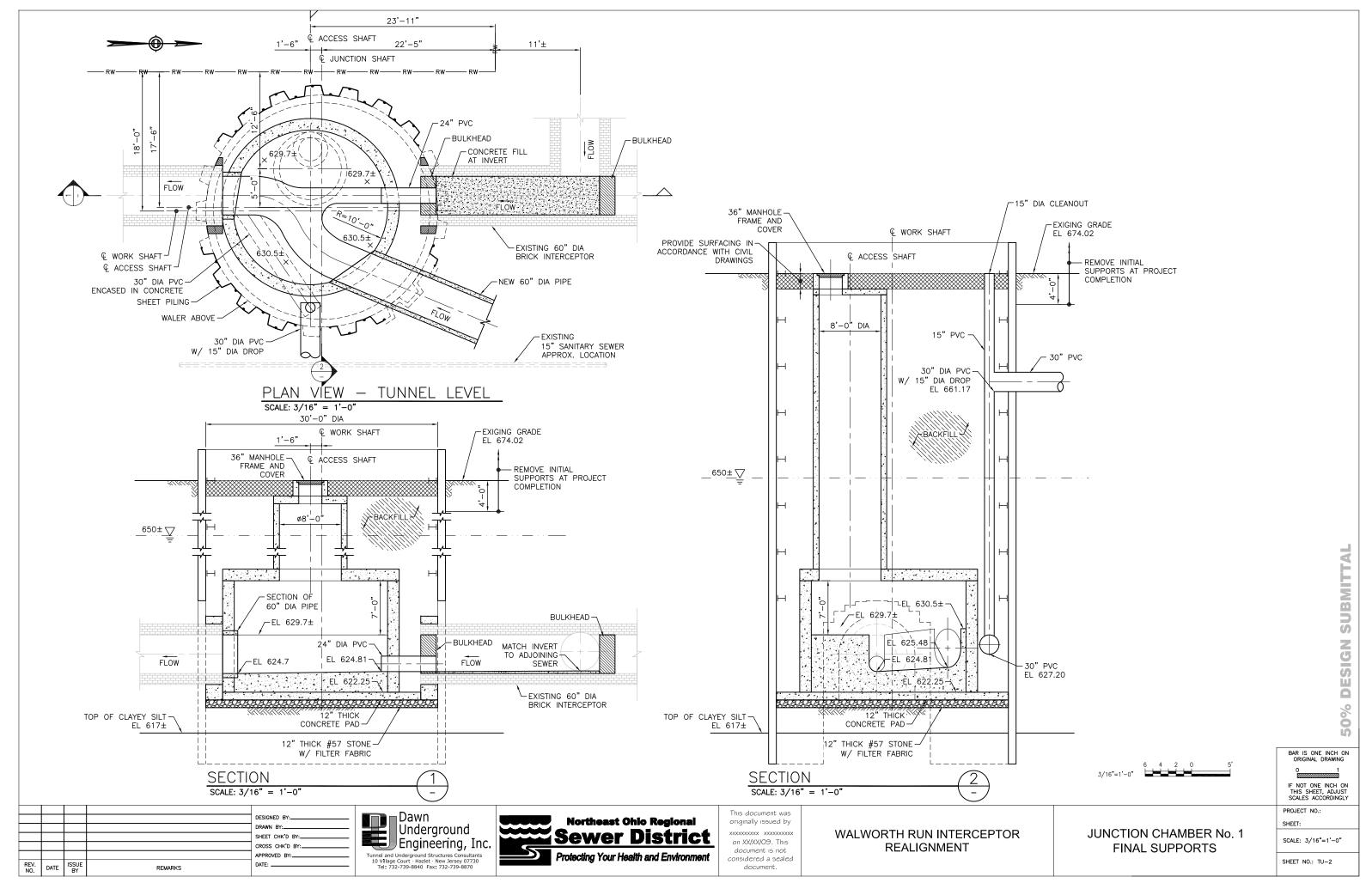
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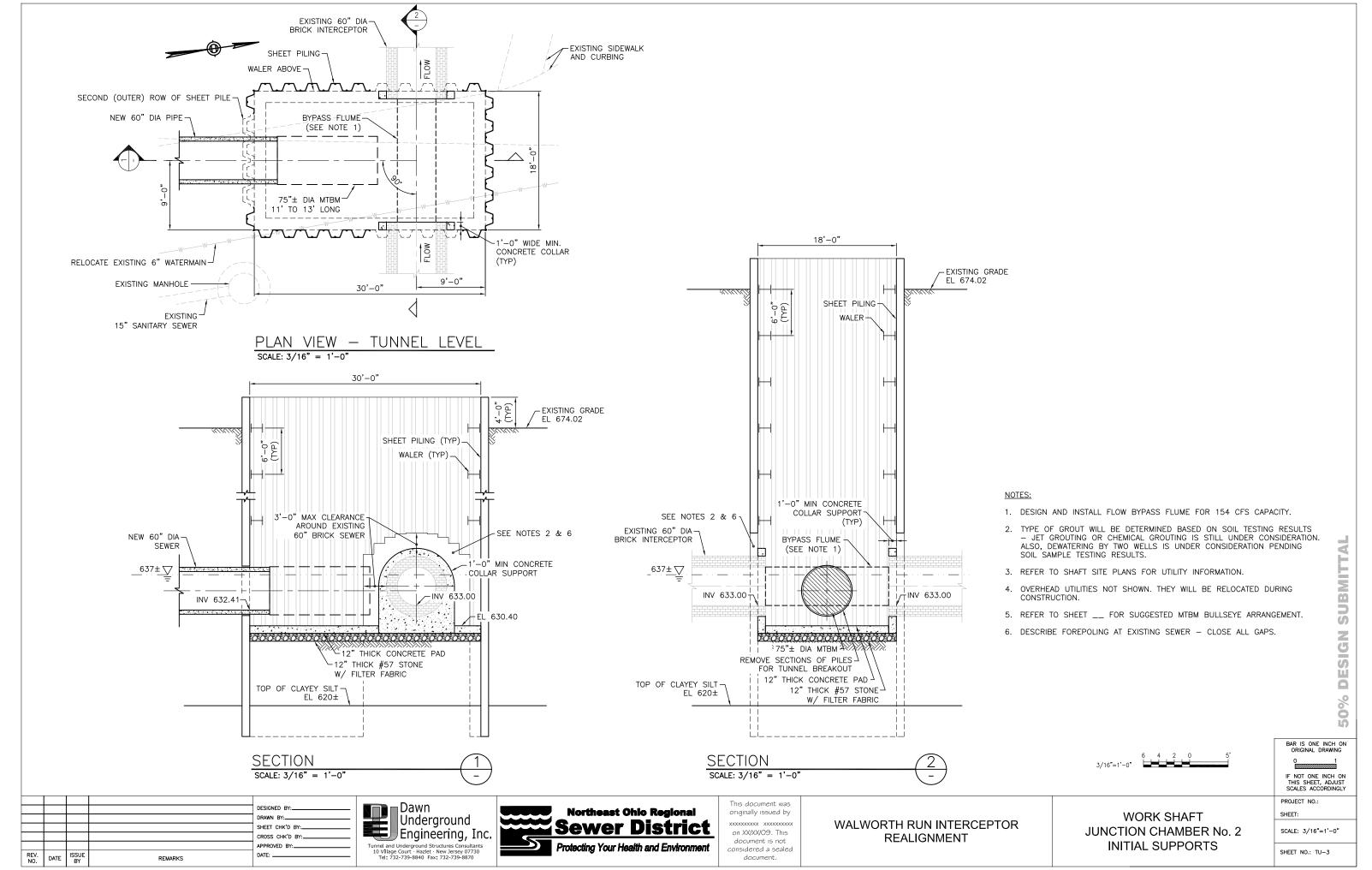
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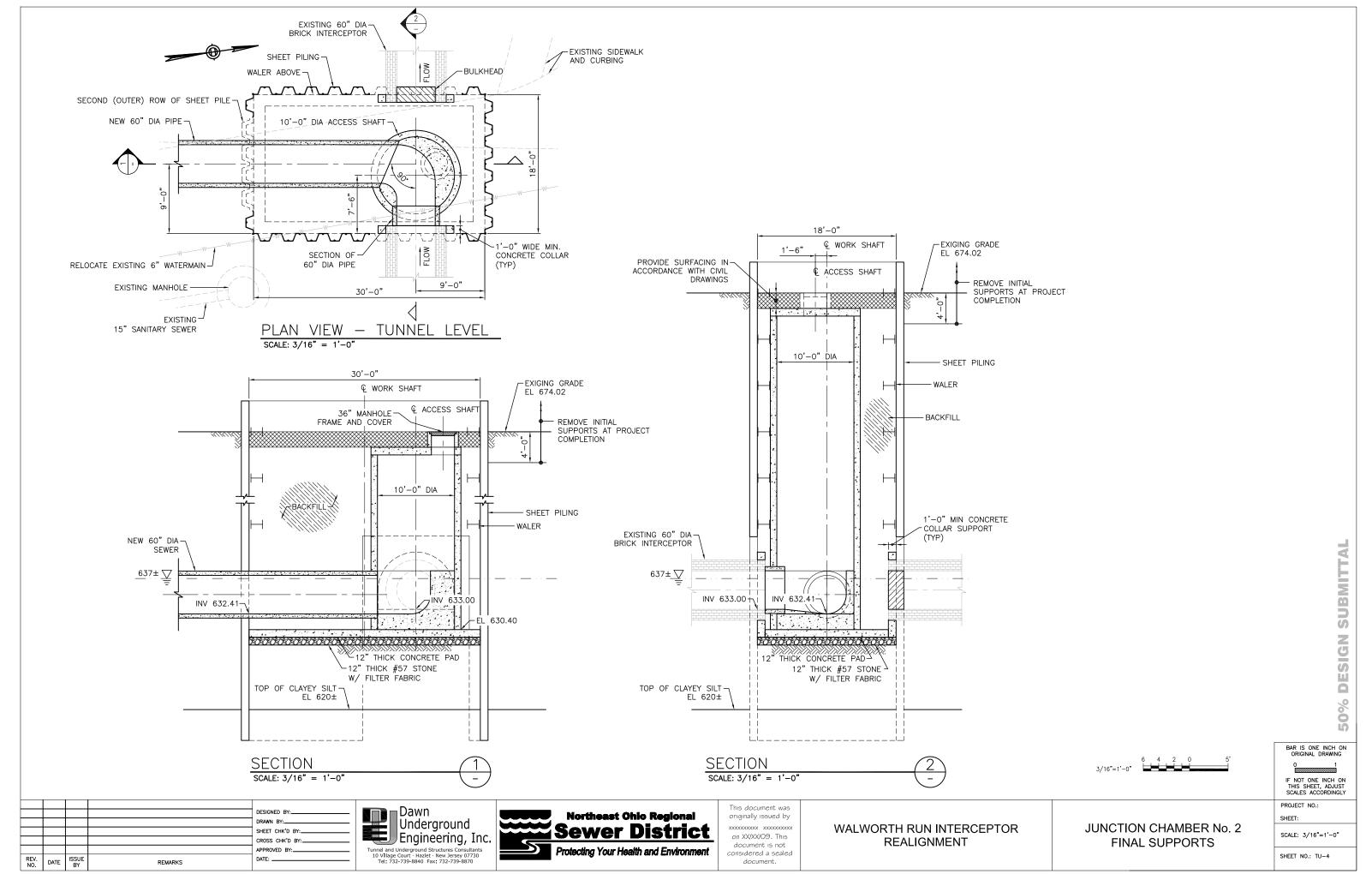
Z-IDUEIDUE Projects/2009/D2920 - WRIR/Current/JUNCTION CHAMBER No 1.dwg, 3/16/2010 3:01:11 PM, Th



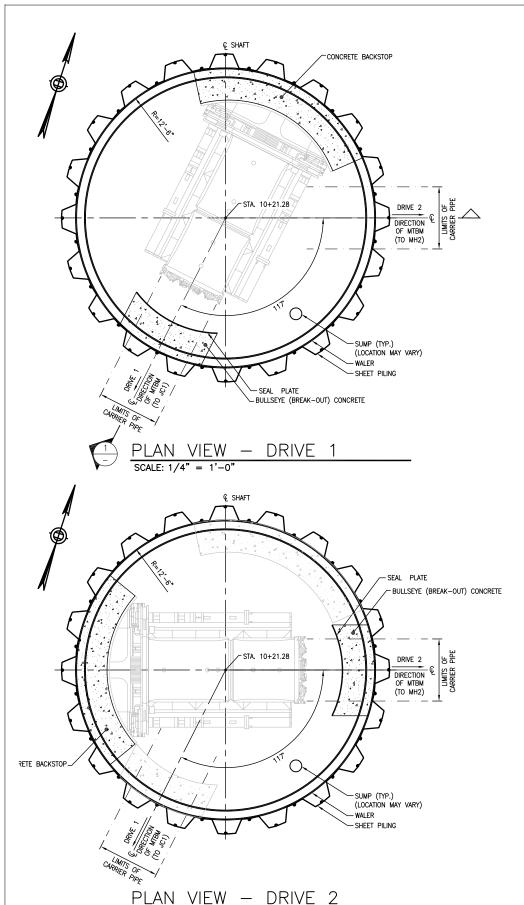
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2:IDUEIDUE Projects/2009/D2920 - WRIRICurrent/JUNCTION CHAMBER No 2.dwg, 3/16/2010 2:51:56 PM, Thomas



2:IDUEIDUE Projects/2009/D2920 - WRIR/Current/UNCTION CHAMBER No 2.dwg, 3/16/2010 2:53:13 PM



SCALE: 1/4" = 1'-0"

REMARKS

DESIGNED BY:.

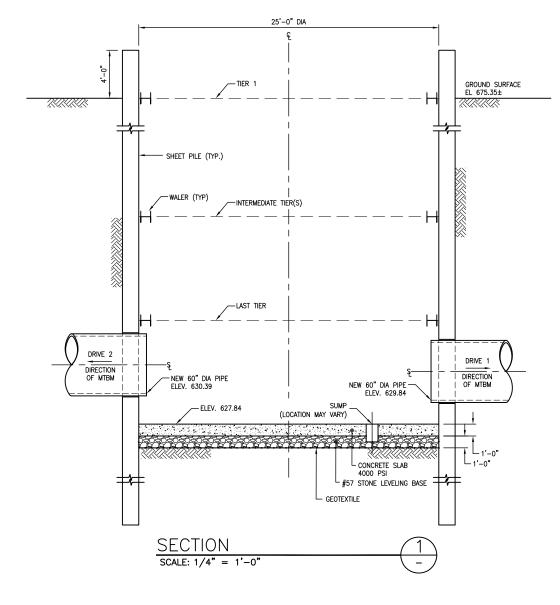
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CROSS CHK'D BY:\_

APPROVED BY:\_\_

DRAWN BY

DATE: \_



document.

GENERAL NOTES:

1. ALL STRUCTURAL STEEL MEMBERS ARE FY = 50 KSI.

2. STEEL SHEETING IS PZ27 OR EQUAL (FY = 50 KSI))
3. USE E70XX ELECTRODES FOR ALL WELDS.
4. THE MAX. THRUST LOAD FROM MTBM ON TUNNEL BREAK-IN CONCRETE SHALL NOT EXCEED 50 TONS.

SEQUENCE OF CONSTRUCTION FOR WORK SHAFT AT MANHOLE NO. 1 (MH1)
THE FOLLOWING SEQUENCE OF CONSTRUCTION FOR WORK SHAFT AT MH1 IS PREPARED CONSIDERING THAT MICROTUNNEL DRIVE 1 WILL BE COMPLETED FIRST AND THEN DRIVE 2 WILL BE COMPLETED.

TO MAINTAIN THE EXCAVATION AND SUPPORT STABILITY, THE FOLLOWING SEQUENCE OF CONSTRUCTION FOR THE WORK SHAFT

TO MAINTAIN THE EXCAVATION AND SUPPORT STABILITY, THE FOLLOWING SEQUENCE OF CONSTRUCTION FOR THE WORK SHAFT SHALL SECOND (OUTER) ROW OF SHEET PILES AT TUNNEL BREAK-OUT LOCATIONS WITHIN LIMITS INDICATED.

3. EXCAVATE PIT "IN DRY" TO MAXIMUM OF 2 FEET DEPTH BELOW TIER 1 LEVEL AND INSTALL TIER 1 STEEL SUPPORTS.

4. CONTINUE TO EXCAVATE PIT "IN DRY" IN STEPS TO MAXIMUM OF 2 FEET DEPTH FOR EACH OF THE REMAINING TIER LEVEL AND INSTALL REMAINING TIER TIES SUPPORTS.

5. AFTER INSTALLATION OF THE LAST TIER, CONTINUE TO EXCAVATE THE PIT "IN DRY" DOWN TO THE BOTTOM OF FYCAVATION.

EXCAVATION.

EXAMATION.

C. CLEAN THE BOTTOM OF EXCAVATION AND PLACE GEOTEXTILE FABRIC, CRUSHED STONE BASE AND CONCRETE SLAB. PROVIDE SUMP PIT AS SHOWN ON THE DRAWINGS. ALLOW THE CONCRETE SLAB TO GAIN THE DESIGN STRENGTH.

J. IF GROUND WATER IS IN-FILTERING INTO THE SUMP PIT, CONTINUOUSLY PUMP OUT THE WATER FROM THE SUMP PIT. FOR THE ENTIRE DURATION OF WORK.

PREPARATION FOR BREAK-OUT FOR DRIVE 1 AND DRIVE 2

8. PLACE SUITABLE GROUT BETWEEN TWO ROWS OF SHEETING AT TUNNEL BREAK-OUT LOCATIONS TO PREVENT GROUNDWATER OR SOIL INFILTRATION WHEN MAIN SHEET PILES ARE CUT FOR MICROTUNNEL BORING MACHINE (MTBM) BULLS EYE.

CUT THE SHEET PILES (INSTALLED FOR THE SHAFT) IN THE MICROTUNNEL BREAK-OUT AREAS (BULLSEYE). IF DURING CUTTING OF SHEET PILES, GROUNDWATER OR SOIL INFILTRATION IS OBSERVED, PROVIDE SECONDARY GROUT TO COMPLETELY SEAL BULLSEYE ZONE AS NECESSARY. APPLY A BOND BREAKER AGAINST SHEET PILES IN THE BULLSEYE

PROCEDURE FOR BREAK-OUT FOR DRIVE1 AND DRIVE 2

10. INSTALL STEEL BULLSEYE SEAL PLATE AND PLACE CONCRETE FOR THE TUNNEL BREAK-OUT BETWEEN SEAL PLATE AND SHEET PILES FOR DRIVE 1. ALLOW THE CONCRETE TO GAIN THE DESIGN STRENGTH. PULL UP THE SECOND (OUTER) ROW OF SHEET PILES JUST ENOUGH TO CLEAR THE MICRO TUNNEL BORING MACHINE (MTBM) FOR DRIVE 1.

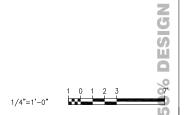
11. ON COMPLETION OF DRIVE1, INSTALL BREAK-OUT FOR DRIVE 2 SIMILAR TO THE BREAK-OUT PROCEDURE FOR DRIVE 1.

ALLOW THE CONCRETE TO GAIN THE DESIGN STRENGTH. PULL UP THE SECOND (OUTER) ROW OF SHEET PILES JUST ENOUGH TO CLEAR THE MICROTUNNEL BORING MACHINE (MTBM) FOR DRIVE 2.

CONCRETE BACKSTOP CONSTRUCTION FOR DRIVE 1 AND DRIVE 2

12. CONSTRUCT THE CONCRETE BACK STOP AS SHOWN ON THE DRAWING FOR DRIVE 1.

13. ON COMPLETION OF DRIVE1, CONSTRUCT THE CONCRETE BACK STOP FOR DRIVE 2.



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PROJECT NO .:

SHEET:

SUBMIT

SCALE: AS NOTED

WALWORTH RUN INTERCEPTOR REALIGNMENT

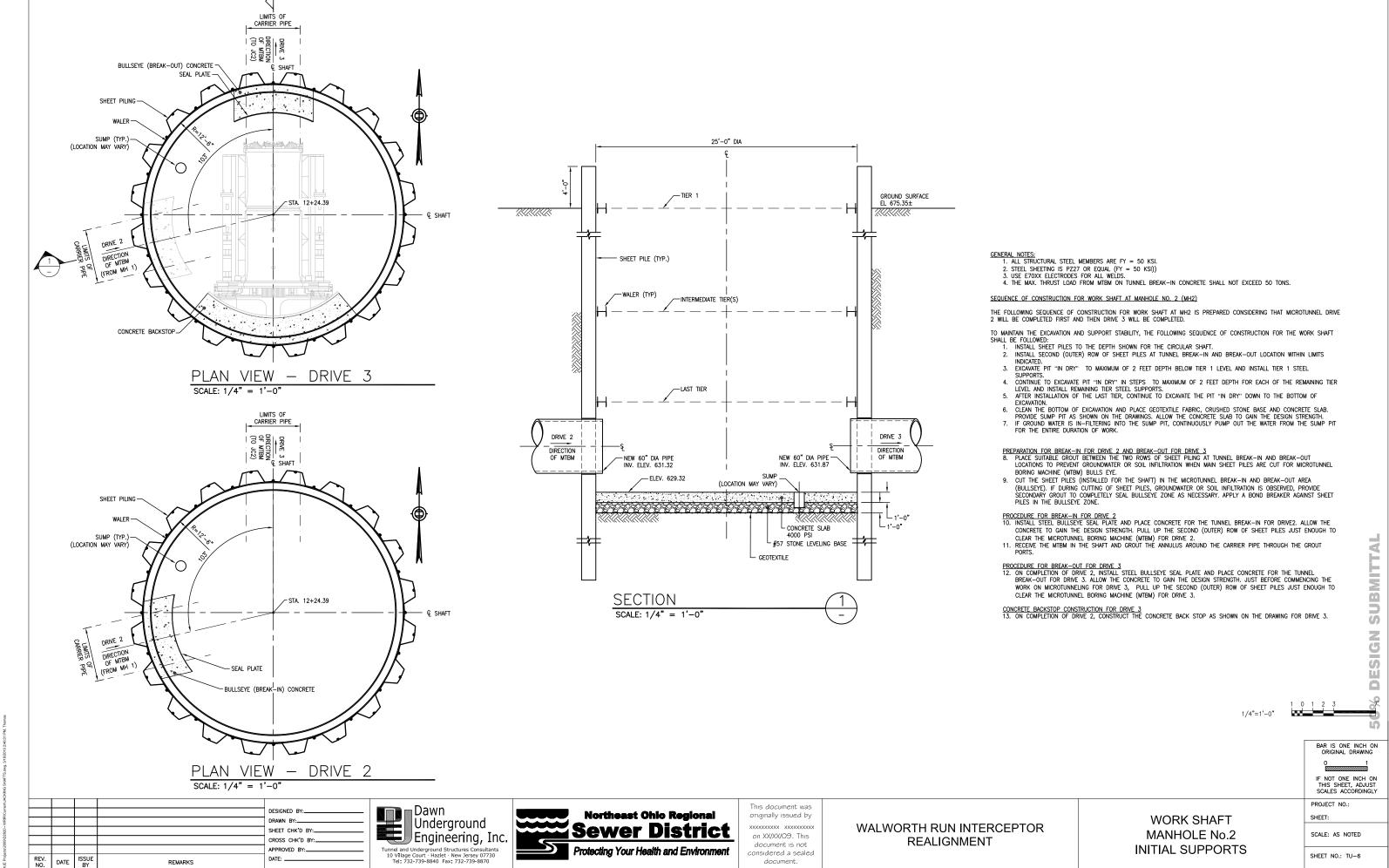
**WORK SHAFT** MANHOLE No.1 **INITIAL SUPPORTS** 

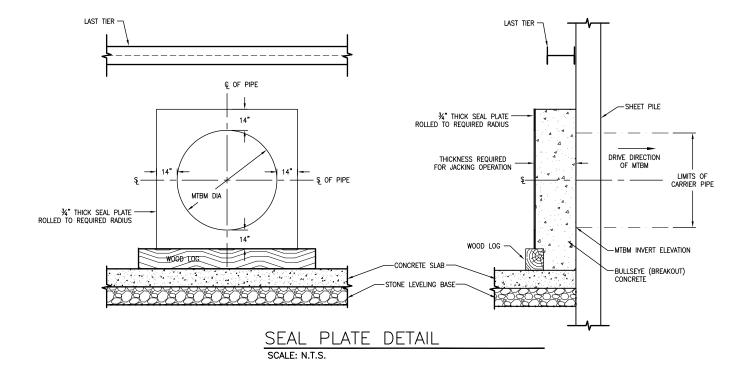
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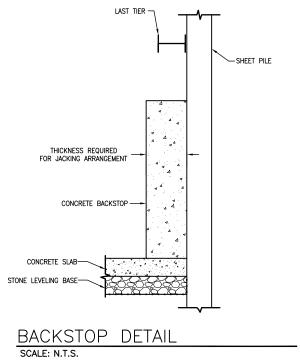
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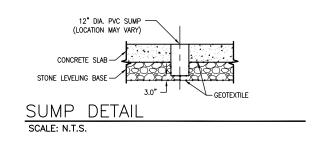
Dawn Underground Engineering, Inc.











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Dawn Underground Engineering, Inc.



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WALWORTH RUN INTERCEPTOR REALIGNMENT

BREAK-IN, BREAK-OUT, BACKSTOP AND SUMP DETAIL

PROJECT NO.: SHEET:

SCALE: AS NOTED

SHEET NO.: TU-7

# WALWORTH RUN INTERCEPTOR REALIGNMENT PROJECT - CONTRACT WRIR



MAR 1 6 2010
PRODUCTION DEPT.

# DRAFT BASIS OF DESIGN REPORT

February 4, 2010

Prepared for

Northeast Ohio Regional Sewer District

Prepared by

DLZ Ohio, Inc. in Conjunction with Dawn Underground Engineering, Inc.



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# 1.0 Background

#### 1.1 General

This Basis of Design Report summarizes the features of the Walworth Run Interceptor Realignment (WRIR) Project. This project involves the relocation of the Walworth Run Interceptor (WRI) to accommodate the future Interstate 90 Innerbelt Bridge Project by the Ohio Department of Transportation (ODOT). The affected segment of the WRI commences at Regulator WR-27A at the intersection of University Road and West 10<sup>th</sup> Street. The section to be realigned is from Regulator WR-27A to Regulator WR-24 at Fairfield Avenue. The relocated WRI will be constructed entirely within the City of Cleveland.

#### 1.2 **Background Information**

The Interstate 90 Innerbelt Bridge Project provides for the phased replacement of the existing Central Viaduct (Innerbelt Bridge) through the construction of a new westbound bridge to the north of the existing bridge, followed by the construction of a new eastbound bridge on essentially the same alignment as the existing bridge. The project requires the relocation of the 5 ft diameter Walworth Run Interceptor (WRI) and several local sewer utilities in the area of the new I-90 bridge replacement. Figure 1 shows the general location of the WRI relocation.

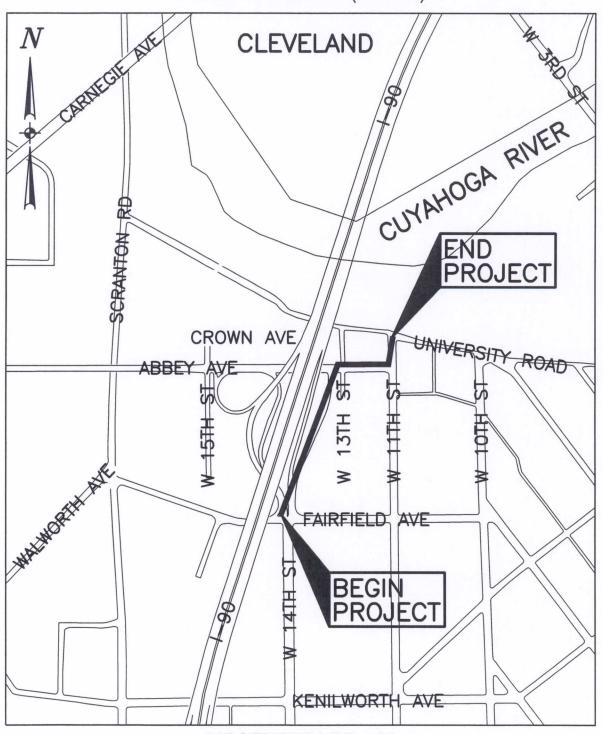
The area where the I-90 bridge replacement will impact the NEORSD utilities is located at the west bank of the Cuyahoga River under the existing Innerbelt Bridge, approximately north of Fairfield Avenue between West 15<sup>th</sup> and West 11<sup>th</sup> Streets.

In general, the new I-90 Innerbelt Bridge is to be located approximately 210 ft west of the existing I-90 bridge at the west bank of the Cuyahoga River. ODOT anticipates one of the first construction activities being the slope stabilization of the west bank of the Cuyahoga River. The stabilization consists of cutting and benching the existing slope starting just north of Abbey Avenue between West 13<sup>th</sup> and West 15<sup>th</sup> Streets.

Figure 2 depicts the proposed re-grading plan of the west bank of the Cuyahoga River at the I-90 Bridge.



# BASIS OF DESIGN FOR THE WALWORTH RUN INTERCEPTOR REALIGNMENT (WRIR)



VICINITY PLAN

SCALE: 1"=500'



FIGURE 1





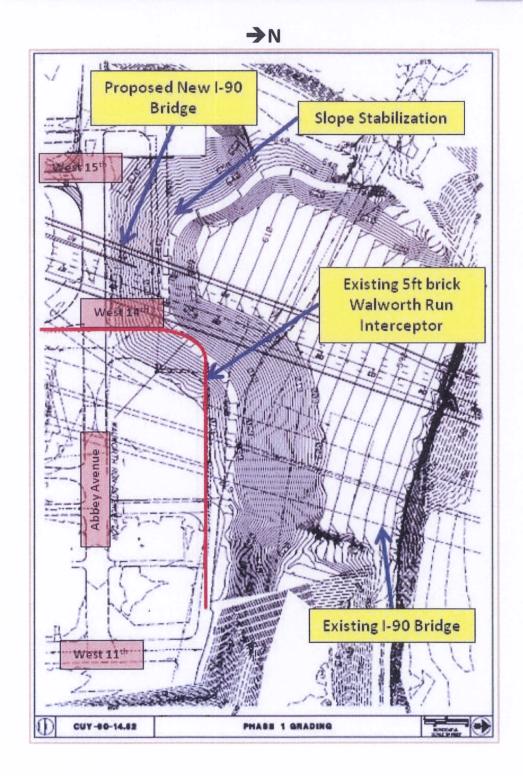


FIGURE 2 PROPOSED FUTURE WORK AT WEST BANK OF CUYAHOGA RIVER AT THE I-90 BRIDGE





#### 1.3 Existing Walworth Run Interceptor (WRI)

# 1.3.1 Alignment

Most of the combined sewer overflow during both dry and wet weather goes to the WRI. The WRI is the oldest of the four interceptors in the Westerly District. The initial purpose of the interceptor was to collect the combined sewer overflow from the local sewers and transport that flow to the Cuyahoga River.

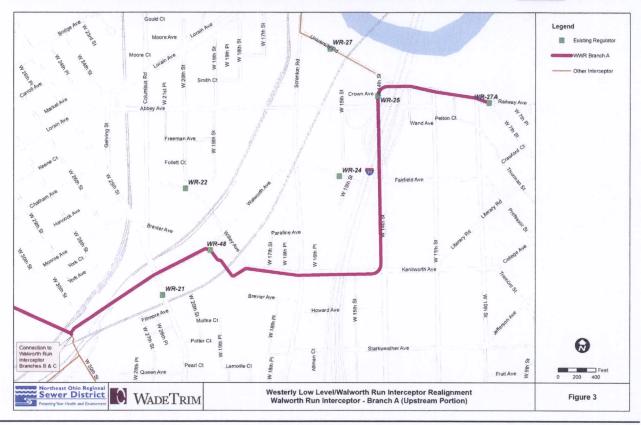
The affected WRI segment begins at the dry weather outlet Regulator WR-27A. The regulator directs flow from the Tremont Bluff area to either the head of the WRI or CSO 81. The interceptor runs down University Road as a 5 ft tunnel to West 14th Street. After turning south on West 14th Street, flow from the local sewer drops in at Crown Avenue through the leaping weir regulator WR-25. The interceptor continues on West 14th Street to Kenilworth Avenue. WRI then turns west onto Kenilworth Avenue, crosses Scranton Avenue, where Kenilworth Avenue becomes Willey Avenue and heads down the hill. Near the Animal Protective League facility, the interceptor turns south and then west along the route that used to be Shay Court and Brevier Avenue. The interceptor then turns west continuing to Train Avenue.

WRI reaches the bottom of the hill and turns southwest, crossing over the larger Walworth Run Overflow sewer (CSO 080). A 24 inch pipe connects the interceptor and the overflow pipe at the turn. The connection was constructed to relieve surcharging in the interceptor.

Once on Train Avenue, the interceptor decreases from a 5 ft circular sewer to a No 4 egg-shaped sewer and accepts dry weather flow from the regulator WR-22. The WRI continues on a southerly path, picking up flow from regulator WR-21 on West 25th Street. The interceptor stays on Train Avenue until turning north at West 30th Street. WRI enters the intersection of Train Avenue and West 30th Street and combines with dry weather flows from other sewer branches. Figure 3 shows the alignment of the WRI within Branch A of the sewer system.







# FIGURE 3

# **WALWORTH RUN INTERCEPTOR - BRANCH A**

Table 1.3.1 summarizes existing design criteria for the Walworth Run Interceptor.

Table 1.3.1 – Existing WRI Design Criteria

Interior Diameter	5 ft		
Maximum Flow (manning's full pipe capacity)	185 cfs flowing full		
10-yr, 6-hr flow <sup>(1)</sup>	109 cfs		
Dry Weather Flow (DWF) flow <sup>(1)</sup>	6.85 cfs		
Slope	0.43%		
Pipe Material	Brick		
Average Invert Depth at the Project Area	Approx. 45 ft		

Estimates based on Westerly CSO Phase II Facilities Plan models (Feb 2000)





#### Walworth Run Interceptor Realignment (WRIR) 1.4

#### 1.4.1 **Option Evaluation**

Five (5) conceptual relocation options for a portion of the WRIR were considered to accommodate the future design of the Interstate 90 Innerbelt Bridge. Options 1 and 2 were presented by NEORSD during the proposal stage. Options 3 through 5 were developed by DLZ as potential alternates and included in the proposal submission. Based on project goals, cost and schedule, DLZ concurred with the original NEORSD recommendation that Option 2 be selected as the preferred alternate for the WRIR. The updated WRIR Draft Technical Memorandum dated January 11, 2010 and February 4, 2010 (Revision No. 1), prepared by DLZ, is included as Appendix A.

# 1.4.2 Alignment

The WRIR begins by connecting to the existing WRI at the intersection of University Road and West 11<sup>th</sup> Street. Approximately 140' of 60" tunneled pipe runs southbound from the connection point along West 11th Street to an installed manhole at the intersection of Abbey Avenue. The alignment of the 60" tunneled pipe then runs westbound approximately 275' along Abbey Avenue to an installed manhole at the West 14<sup>th</sup> Street intersection. From this point, the alignment of the 60" tunneled pipe proceeds along the West 14th connector ramp within the ODOT limited access (LA) for approximately 900' to the intersection of West 14th Street and Fairfield Avenue. At this point, the 60" tunneled pipe connects to the existing WRI with a connecting structure.







# FIGURE 4 WRIR GENERAL ROUTE

# 1.4.3 Interceptor and Regulator Structures

The WRIR design includes four (4) major interceptor structures to be constructed within tunnel/work shafts. Two of the structures will be cast in place concrete junction chambers constructed to temporarily bypass flow from WRI. The junction chambers will be located at University Road and West 11<sup>th</sup> Street and Fairfield Avenue and West 14<sup>th</sup> Street. The two remaining structures at the turning points will be manholes and will be located at Abbey Avenue & West 11<sup>th</sup> Street and at Abbey Avenue & West 14<sup>th</sup> Street. DLZ will determine if the manholes will be entirely pre-cast or have cast-in-place components. Additionally, Regulator WR-25 at Crown Avenue & West 14<sup>th</sup> Street will be abandoned and Regulator WR-24 on Fairfield Avenue will be rebuilt.

Table 1.4.3 shows the proposed design summary for the Walworth Run Interceptor Realignment Project.





Table 1.4.3 – Proposed WRIR Design Summary

Interior Diameter <sup>(1)</sup>	60 inches
Full Flow Capacity <sup>(2)</sup>	187 cfs
Design Slope <sup>(3)</sup>	0.51%
Pipe Material	To be determined
Average Invert Depth at the Project Area	Approximately 45 ft

<sup>(1)</sup> Interior diameter may need to increase if surveyed inverts are different than what has been presented in the RFP.

<sup>&</sup>lt;sup>(2)</sup> Full Flow Capacity is based on  $60^{\prime\prime}$  diameter pipe with a Manning's n=0.013, and 0.51%

<sup>(3)</sup> Design Slope is based on inverts determined by field investigation and record data. Additional field information is necessary at the WRI downstream connection point for verification of all design assumptions.





# 2.0 Permits

#### 2.1 General

The WRIR alignment will require significant permitting coordination. Construction permits will be required from the City of Cleveland for work located within city street right-of-way such as University Road, West 11<sup>th</sup> Street, Abbey Avenue, Crown Avenue, West 14<sup>th</sup> Street, and Fairfield Avenue. These construction permits will require considerations for traffic control and other potential construction disturbances.

In addition to permitting coordination normally associated with the City of Cleveland, there will be activity associated with acquiring a permit from ODOT. All portions of the WRIR in the Interstate 90 LA will require the acquisition of an ODOT MR 509 Permit for permission to perform the necessary work.

Additional permitting will be necessary to meet the Ohio EPA regulations for the Permit to Install, and it may become necessary to apply for coverage under a National Pollutant Discharge Elimination System (NPDES) general permit if one or more acres of land is disturbed. Additional agencies may become involved as the work is better defined.





# 3.0 Local Sewers and Hydraulics

#### 3.1 **Local Sewers**

Local sewers are impacted by the proposed Innerbelt work. Table 3.1 lists the impacted sewers and their disposition. DLZ will contact the appropriate agencies to coordinate the necessary work on the impacted sewers. This work will require the re-direction of flows at MH No. 5 and at the Crown Avenue Animal Hospital, and the assessment of pipe capacities.

Table 3.1 – WRIR Sewer Impacts

Identification	Impacted Section
No 4 - No 5 existing 48" diameter brick combined sewer running north along West 14th Street.	Remove or Abandon from MH 5 located at the intersection West 14th Street and Fairfield Avenue to regulator WR 27 located at intersection of University Road and the Walworth Run overflow sewer (CSO 080).
12" diameter existing combined sewer running east along Abbey Avenue from approximately West 15th to West 14th Street.	The complete sewer line is to be abandoned.
12" diameter existing combined sewer running east along Crown Avenue from approximately West 15th to West 14th Street.	The complete sewer line is to be abandoned.
36" diameter existing combined sewer - Running west along University Road.	Remove or abandoned from MH located at the intersection of West 13th and University Road. to regulator WR-25 located at the intersection of West 14th Street and Crown Avenue.
Existing Storm sewer draining into MH 5 located at the intersection of West 14th Street and Fairfield Avenue.	Abandon or remove all of this sewer line. This storm sewer runs in a southeast direction and ends at MH 5.
Existing 12" storm sewer draining into MH 3. This storm sewer runs in a northwest direction and ends at MH 3.	Abandon or remove the complete sewer line.
Existing storm sewers running east and draining into MH 2.	Abandon or remove all the storm sewers connected to MH 2.





Table 3.1 – WRIR Sewer Impacts (Continued)

Identification	Impacted Section
Existing 12" storm sewer running west and draining into MH 2.	Abandon or remove all the storm sewers connected to MH 2.
Existing 15" storm sewer running west along Abbey Avenue and draining into MH 1.	Abandon or remove all of this sewer line.
Existing 18" storm sewer running west along University Road. This 18" storm line connects to the 24" combined sewer at the intersection of West 14th Street and University Road.	To be removed by the stabilization works of the east bank slope.
Existing storm sewers north of the intersection between West 14th Street and University Road discharging on the Cuyahoga River.	These sewers v. will be removed during the stabilization of the Cuyahoga River west bank.
Dry weather outlet from WR-24 to West 14th Street.	May need to be upsized.
Combined sewer on Fairfield Avenue connecting to Regulator WR-24.	May need to be upsized.

#### 3.2 **Local Sewer Regulators**

There are two regulators in the project area that are impacted by the Innerbelt Bridge project.

Table 3.2 – WRI Regulator Impacts

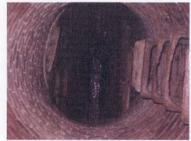
Regulator ID	Location	DWO Destination	Wet Weather Destination	Regulator Type	Proposed Dispensation
WR-24	West 15 <sup>th</sup> Place – 1515 Fairfield Avenue	WRI – Branch A	Regulator WR-27	Leaping Weir	Modify and Rebuild
WR-25	Crown Ave at West 14 <sup>th</sup> Street	WRI – Branch A	Westerly Low Level Interceptor	Leaping Weir	Abandon







Regulator WR-24



**Regulator WR-25** 

#### 3.3 **Flow Characteristics**

The relocated segment of Walworth Run Interceptor is required to convey the flows contained in Table 1.2 of the RFP including the maximum flow of 185 cfs. The surveying work has been completed, and the inverts and slopes of the existing Walworth Run Interceptor have been confirmed, except at the proposed downstream connection point. Apparently, there is no existing structure at the connection of the 60" overflow from WR-24 at the Interceptor. Based on the confirmed inverts, a conservative approximation of the invert of the proposed connection point using existing drawings, and an anticipated length of 1,315 lineal feet, it has been determined that the relocated segment of Walworth Run Interceptor can be designed at a slope of 0.51% (6.81 feet of drop over 1,315 lineal feet), which is greater than the slope of 0.47% that was listed in the RFP. The full-flow capacity of the relocated segment using a Manning's nfactor of 0.013 would be approximately 187 cfs, which is greater than the maximum design flow of 185 cfs. Once the proposed connection point invert is confirmed, the design slope will be updated accordingly.





# 4.0 Geotechnical Considerations

#### 4.1 **Project Geologic Setting**

The Walworth Interceptor Realignment Project (WRIR) is within the northern section of the Cuyahoga River Valley. Geologically, most of this area is classified as "made land" composed of fill materials of variable source, composition and depth.

A total of eight (8) soil borings have been taken along the Option 2 alignment at this writing. Figure 5 shows the locations of the borings. The draft boring logs are included as Appendix "B." The borings reveal that the fill layer varies from a couple of feet to as much as 19 feet (Boring B -7). Brick pieces were recovered while sampling the fill layer in this boring. Beneath the fill materials, alluvium deposits extend consisting mostly of very loose to medium dense sands and silts; and medium stiff silty clay lenses (Boring B-3 and B-8). Most of the deposits show a stratified or inter-layered structure containing fine sands and silts. The alluvium materials were deposited prior to the Cuyahoga River. Beneath the alluvium deposits, lacustrine deposits start approximately 55 feet below the surface and consist mostly of medium stiff to very stiff silty clays stratified with silt layers.

Based on preliminary information, the ground water table has been estimated to be between 30 to 35 feet below ground surface.

#### 4.2 **Subsurface Conditions Along the Tunnel**

The proposed tunnel construction will be below ground water and through sandy and silty soils. In the past, these soil deposits were most troublesome for tunneling projects in Cleveland. In the WRIR case, soils within the tunnel zone will be dense to very dense and below ground water. This setting will make the soil susceptible to uncontrollable flow unless proper tunnel techniques for supporting the tunnel



Microtunneling from a caisson

face are employed. Slurry shields with one-pass concrete segmental linings or microtunneling





with pipe jacking will be evaluated given the subsurface conditions anticipated at the site. Based on the short length of the project and the 90 degree turns required to negotiate the alignment, it appears that microtunneling will be the most cost effective solution.

Shafts for the WRIR will be constructed through all of the soil deposits mentioned above. Shafts at Borings B-1, B-3 and B-4 will terminate in silt deposits and the Shaft at B-8 (the down stream connection) will terminate in silty clay or clay. Excavating shafts below the water table through the upper deposits of lose sands and silts may present unstable side and bottom conditions unless water tight supports are employed. These supports must be pre-installed ahead of the shaft excavations and extend deep enough to prevent boiling and bottom heave. Currently, the design team is investigating the use of pre-driven steel sheet piles, secant piles, precast concrete caissons, slurry walls and jet grouting as methods for excavating the shafts.

A soil profile of the WRIR is shown on Sheets 1-6 of 6 following Section 4.5 of this report. A jacking pit concept plan is also included following Section 4.5.

#### 4.3 **Tunnel Support**

Based on microtunneling appearing to be the most effective tunneling method for the replacement sewer installation, reinforced concrete pipe, centrifugally cast fiberglass reinforced polymer mortar pipe (CCFRPM) such as produced by HOBAS, and clay pipe can be suitable candidates for this project since they are all specifically designed and produced for installation by jacking. Microtunneling methods of tunneling provide immediate initial support for the tunnel since the final carrier pipes are jacked behind a TBM or MTBM.



**CCFRPM** Pipe



Reinf. Conc. Jacking Pipe



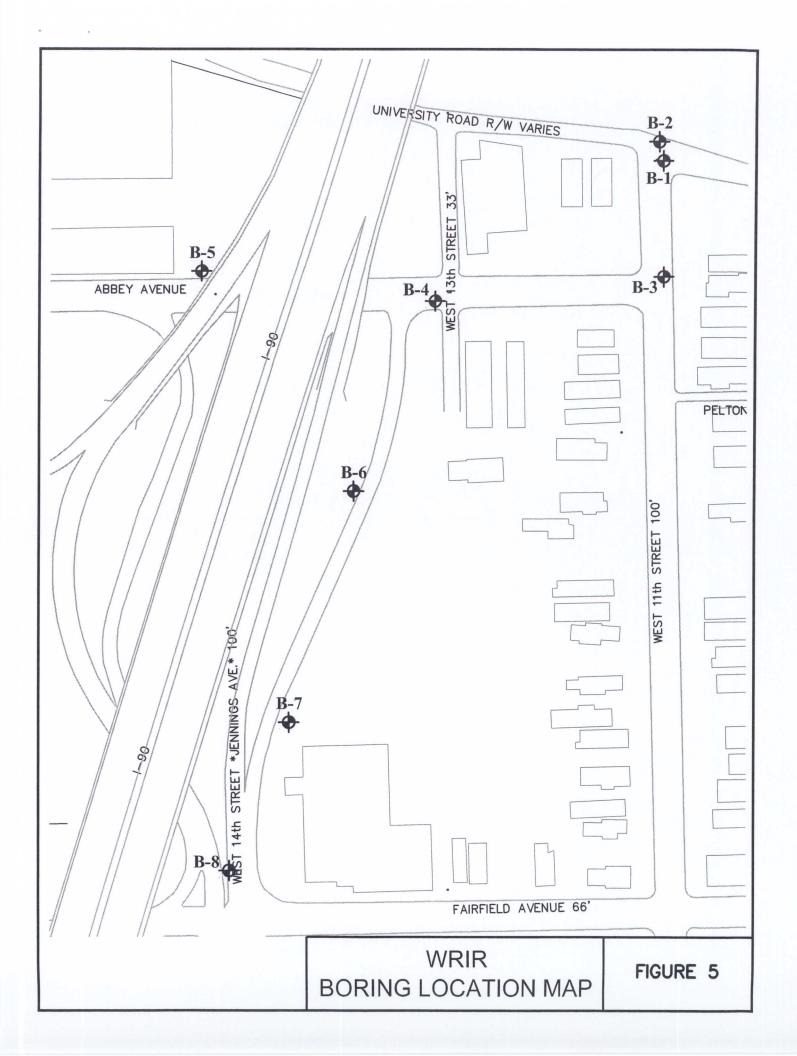


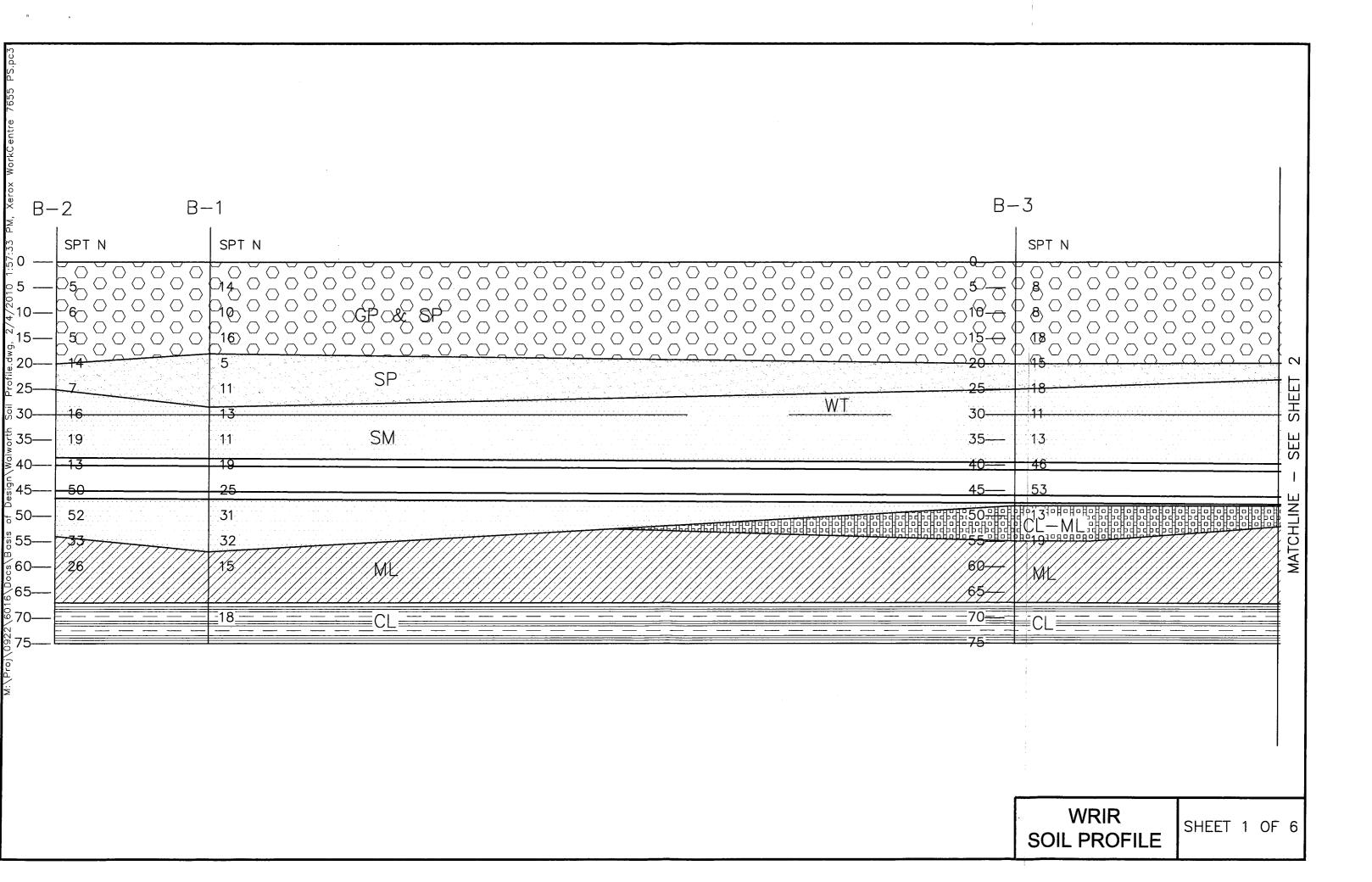
# 4.4 Additional Borings

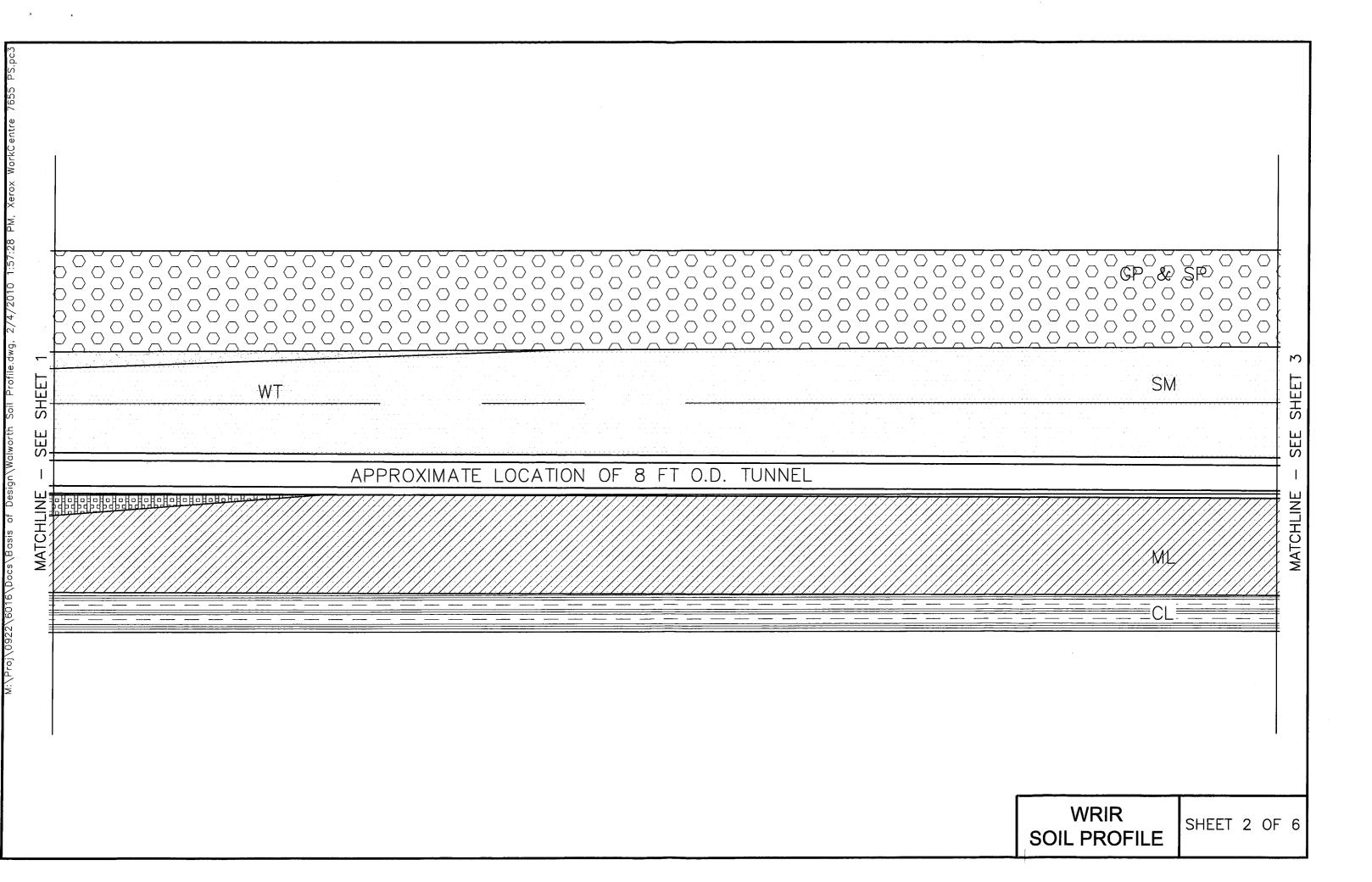
Boring B-7 shows 19 feet of fill. Two adjacent borings (B-6 and B-8) show only a couple feet of fill. This indicates that the fill depth may vary greatly within the project area. Currently it is contemplated that the downstream connection may be moved to the south-west corner of the Fairfield Avenue and West 14<sup>th</sup> Street intersection. This will require the shaft construction to place a connection structure and also to retrieve the MTBM or TBM. If the connection point is moved, DUE recommends that an additional boring be taken near the new location. Sampling in this boring may only extend to the bottom of fill or the first 25 feet (whichever is greater) and the remainder of the boring extended only for placement of the piezometer.

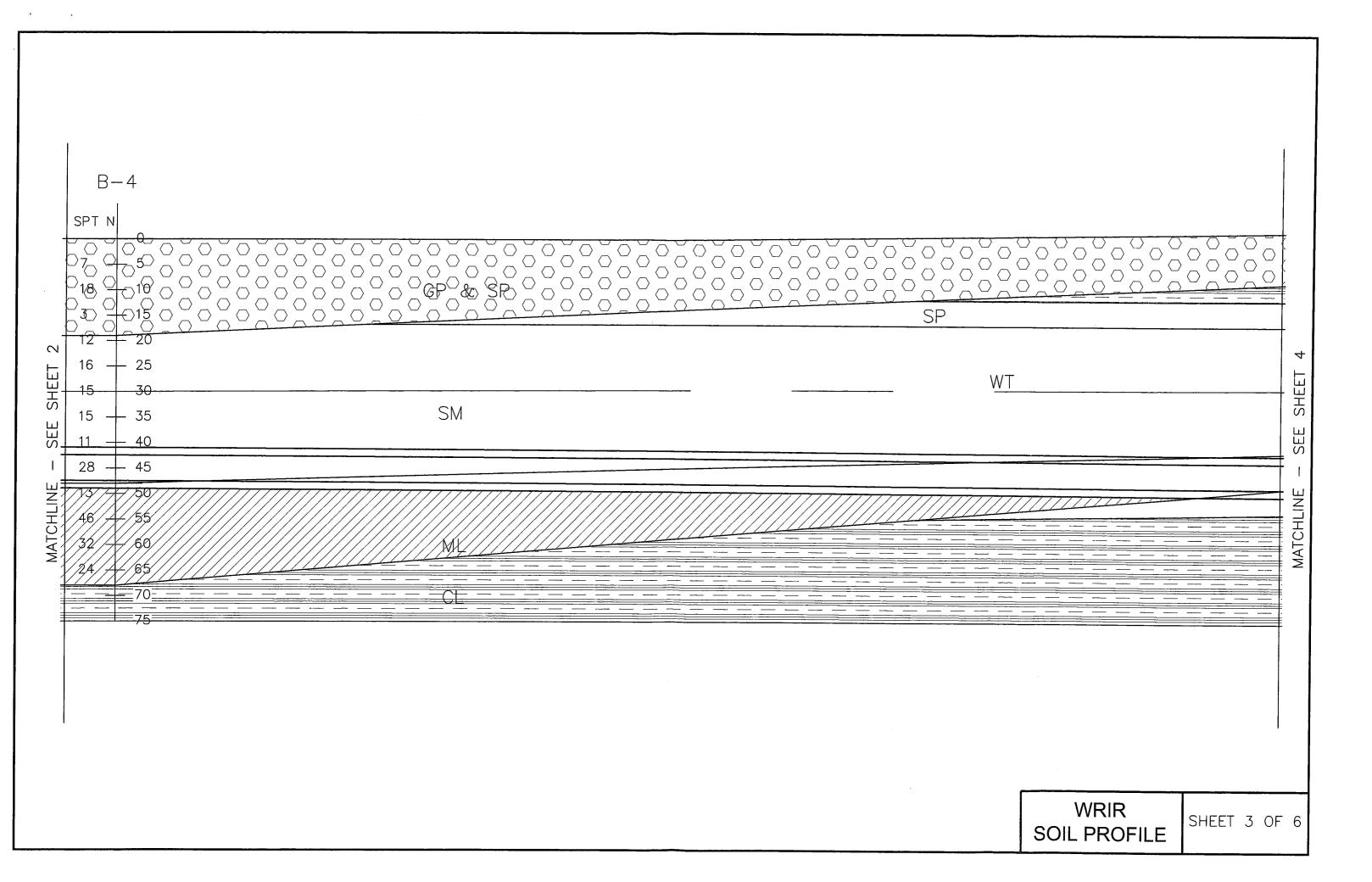
# 4.5 Long-Term Ground Water Observation

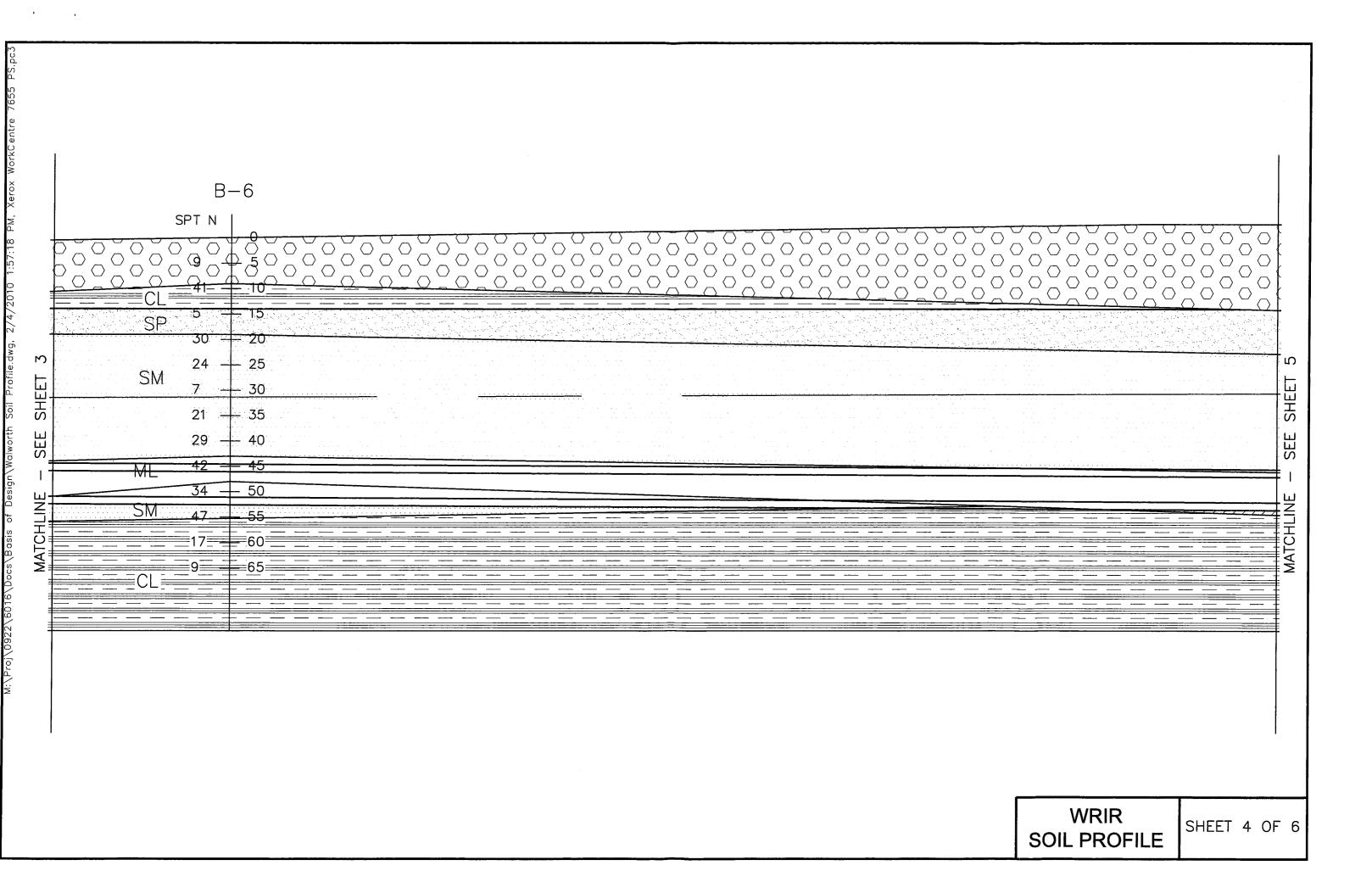
The Design Team recommends that long term observation of ground water levels be conducted at each shaft location. Currently there are only two piezometers at the site – one near boring B-3 marked W-1 and one near boring B-5 marked W-2. Additional piezometers should be installed near the planned connection point on University Road, near Boring B-4 and near the connection point downstream at Fairfield Avenue and W 14<sup>th</sup> Street (three additional piezometers). The piezometers should be located where they will not be damaged later by construction. This will allow the Design Team to monitor the ground water during construction should the need arise to confirm design assumptions. Water levels should be monitored on a monthly basis until the project bidding period. The Design Team will coordinate the location of the piezometer tip elevations and location of the screens.

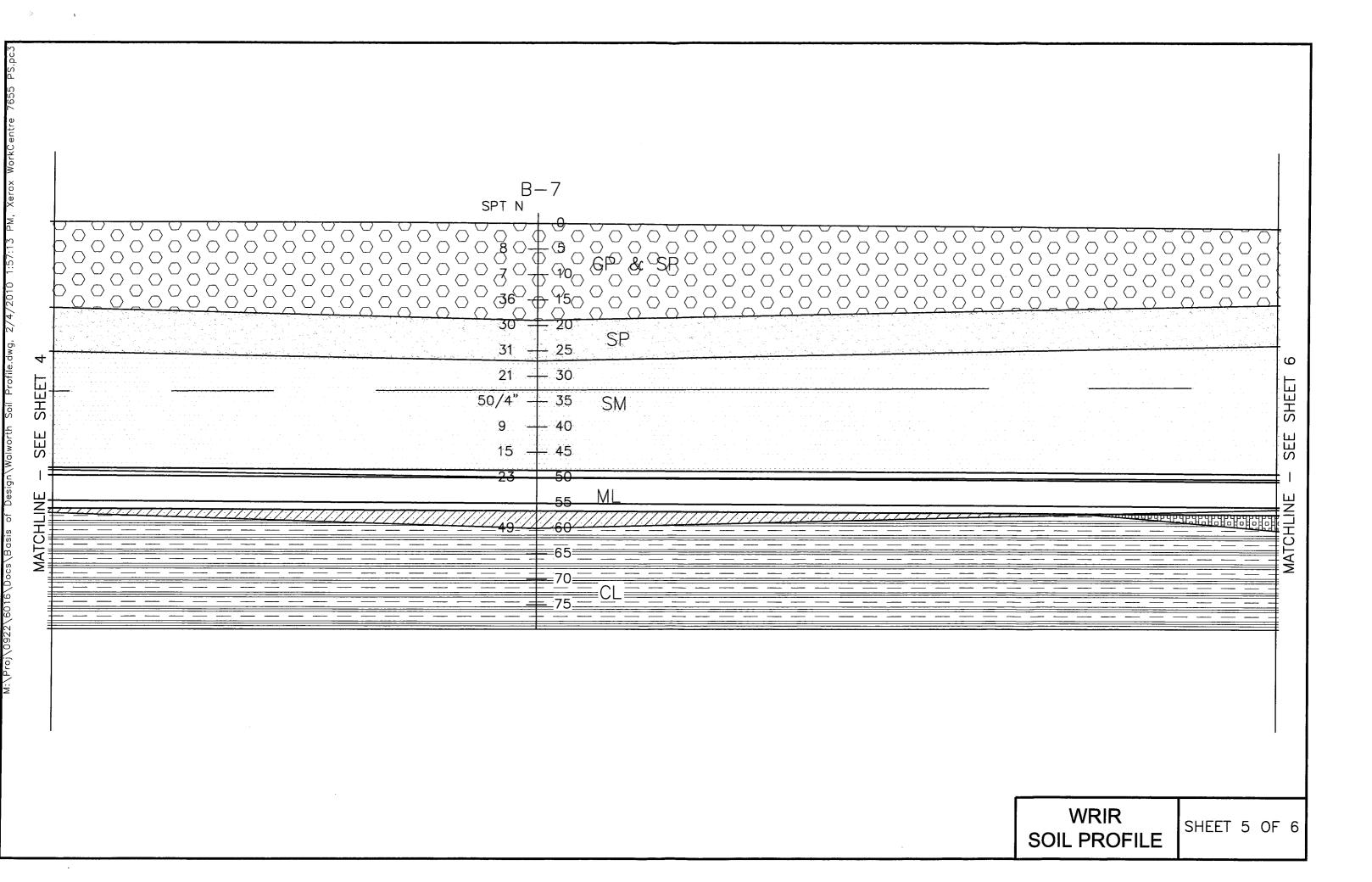


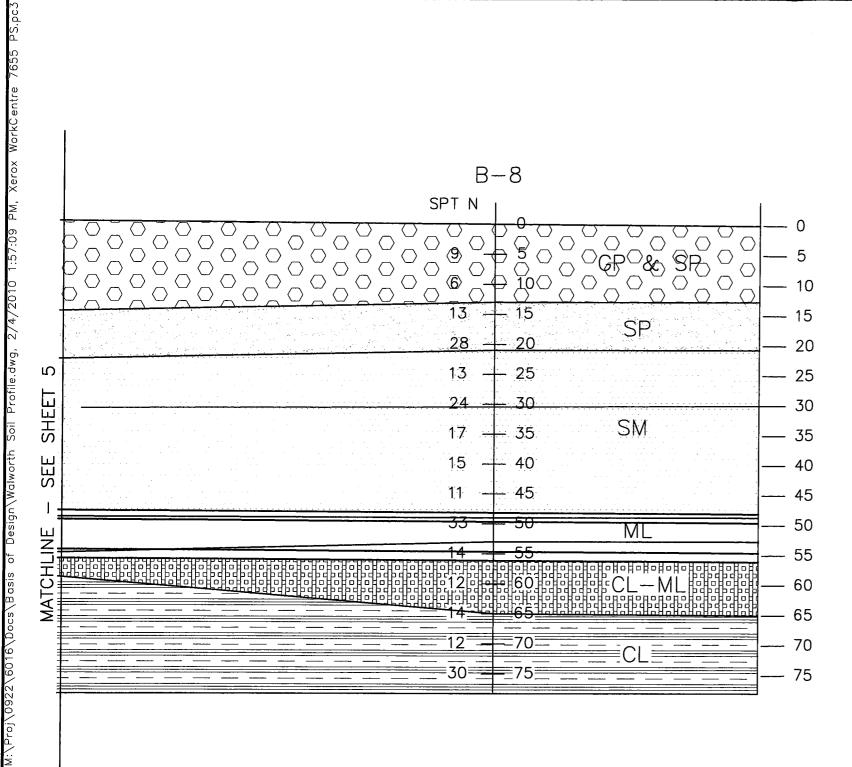






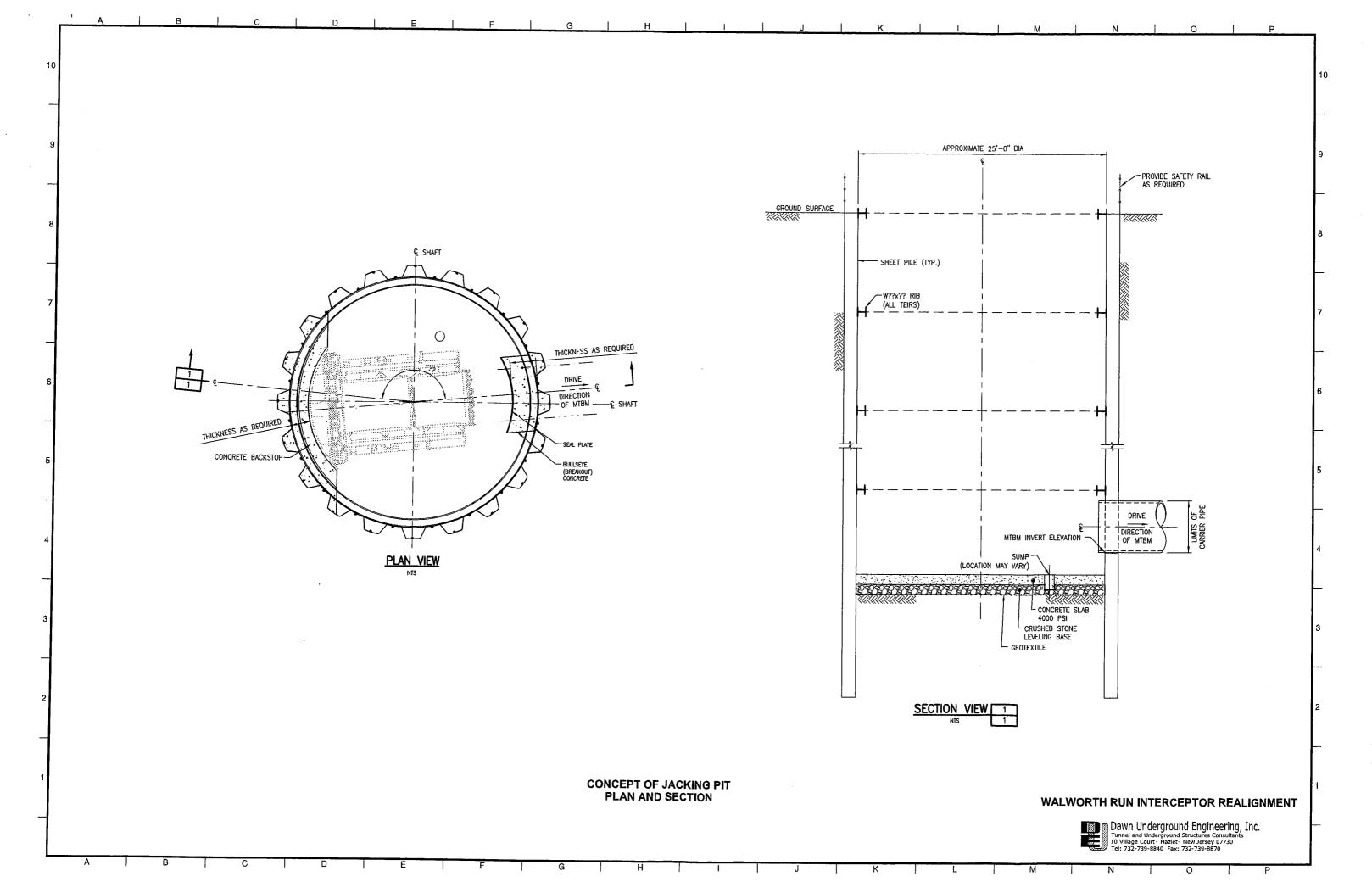






WRIR SOIL PROFILE

SHEET 6 OF 6



APPENDIX "A"

**Draft Technical Memorandum** 



# **DRAFT TECHNICAL MEMORANDUM**

To:

Mr. Brian Page, PE

From:

Mr. Thomas Hessler, PE, PS

Date:

January 11, 2010 (1st Issue)

February 4, 2010 (Revision No. 1)

Subject:

Walworth Run Interceptor Relocation Alignment Option Evaluation

### Section 1 - Project Description

The Ohio Department of Transportation (ODOT) is designing the future Interstate 90 Innerbelt Bridge Project. The design of the new westbound structure adversely impacts the existing Walworth Run Interceptor (WRI) and several local storm and sanitary sewers in the project area. The new Innerbelt Bridge will require the regrading of the west bank of the Cuyahoga River. This regrading work requires the relocation of the WRI. ODOT is also evaluating several options with respect to the existing Innerbelt Bridge that will impact the WRI relocation.

The WRI is divided into three (3) branches; A, B, and C. This project involves the relocation of a section of Branch A. Branch A commences at Regulator WR-27A at the intersection of University Road and West 10<sup>th</sup> Street. The area to be evaluated is from Regulator WR-27A to Regulator WR-24 at Fairfield Avenue.

# **Section 2 - Option Evaluations**

The relocation options for a portion of the WRI Branch A must consider the future design of the Interstate 90 Innerbelt Bridge. Five (5) conceptual options are discussed in this section. Options 1 and 2 were presented by NEORSD during the proposal stage. Options 3 through 5 were developed by DLZ as potential alternates and included in our proposal submission.



## 2.1 Option 1

Conceptual Option 1, shown in Figure A, consists of approximately 900' of 60" diameter tunneled pipe and three (3) major interceptor structures. This option would begin at a connection to the existing WRI at the intersection of University Road and West 11<sup>th</sup> Street. Approximately 200' of 60" tunneled pipe would run southbound from the connection point along West 11<sup>th</sup> Street to the intersection of Abbey Avenue where a manhole would be installed. The 60" tunneled pipe alignment would then run westbound for a distance of approximately 700' along Abbey Avenue to the West 14<sup>th</sup> Street intersection. At this point, it would tap into the existing WRI alignment with a connecting structure.

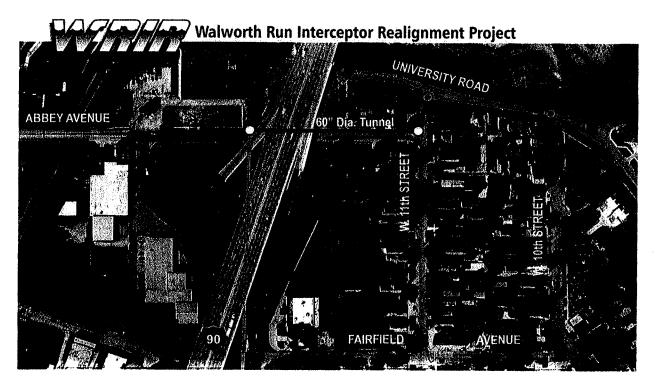


Figure A - Conceptual Option 1

Several local sewers will be removed or abandoned with this option. Additionally, Regulator WR-25 at Crown Avenue and West 14<sup>th</sup> Street would be abandoned and Regulator WR-24 on Fairfield Avenue would be rebuilt. The existing 190' run of 12" sanitary sewer on Crown



Avenue for the Animal Hospital will be relocated. Also, the combined sewer on Fairfield Avenue connecting to Regulator WR-24 may need to be upsized. The dry weather outlet from Regulator WR-24 to West 14<sup>th</sup> Street may also need to be upsized.

Option 1 removes the WRI from the westbound Innerbelt bridge slope regrading area, and provides a relatively short relocation run of tunnel to the connection at Abbey Avenue and West 14<sup>th</sup> Street. However, a significant portion of the relocated WRI is still in the footprint of the eastbound Innerbelt Bridge and passes under the current Innerbelt alignment. This alignment maintains a section of existing WRI along West 14<sup>th</sup> Street under the current Innerbelt Bridge and therefore limits options regarding the potential alignment or subsurface needs of a future eastbound bridge.

### 2.2 **Option 2**

Conceptual Option 2 is shown in Figure B. This option consists of approximately 1,400′ of 60″ diameter tunneled pipe and four (4) major interceptor structures. This option would begin by connecting to the existing WRI at the intersection of University Road and West 11<sup>th</sup> Street. Approximately 140′ of 60″ tunneled pipe would run southbound from the connection point along West 11<sup>th</sup> Street to the intersection of Abbey Avenue where a manhole would be installed. The alignment of the 60″ tunneled pipe would then run westbound approximately 275′ along Abbey Avenue to the West 14<sup>th</sup> Street intersection where a manhole would be installed. From this point, the alignment of the 60″ tunneled pipe would proceed along the West 14<sup>th</sup> connector ramp within the ODOT limited access for approximately 900′ to the intersection of West 14<sup>th</sup> Street and Fairfield Avenue. At this point, the 60″ tunneled pipe would connect to the existing WRI at a connecting structure.

As with Option 1, several local sewers will be removed or abandoned. Additionally, Regulator WR-25 at Crown Avenue and West 14<sup>th</sup> Street would be abandoned and Regulator WR-24 on Fairfield Avenue would be rebuilt. The existing 190' run of 12" sanitary sewer on Crown



Avenue for the Animal Hospital will be relocated. Also, the combined sewer on Fairfield Avenue connecting to Regulator WR-24 may need to be upsized. The dry weather outlet from Regulator WR-24 to West 14<sup>th</sup> Street may also need to be upsized.

Option 2 provides for the complete removal of the WRI from the Innerbelt project footprint. The relocated WRI will not be in conflict with any slope modifications that may be necessary for the existing eastbound Innerbelt Bridge along Abbey Avenue or West 13<sup>th</sup> Street. This Option meets the objectives of the WRI relocation.

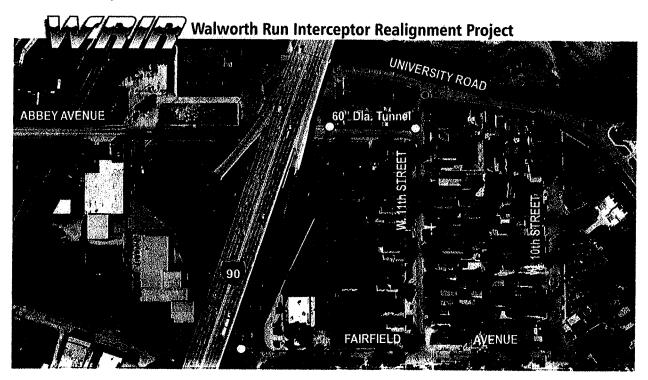


Figure B - Conceptual Option 2

### 2.3 Option 3

Figure C shows Conceptual Option 3, which is a variation of Option 2. This option consists of approximately 1,000' of 60" diameter tunneled pipe and three (3) major interceptor structures. It would begin at a connection to the existing WRI on University Road near West 13<sup>th</sup> Street. The alignment of the 60" tunneled pipe would then run south approximately 200' to the



intersection of Abbey Avenue and West 14<sup>th</sup> Street where a work shaft and a manhole would be installed. The 60" tunneled pipe would then run southwest along the West 14<sup>th</sup> St. / Abbey Avenue access ramp for a distance of approximately 800' to the intersection of Fairfield Avenue and West 14<sup>th</sup> Street where it would connect to the existing WRI with a connecting structure.

As with Options 1 and 2, several sewer pipes would be removed or abandoned with this option. Additionally, Regulator WR-25 at Crown Avenue and West 14<sup>th</sup> Street would be abandoned and Regulator WR-24 on Fairfield Avenue would be rebuilt. The existing 190' run of 12" sanitary sewer on Crown Avenue for the Animal Hospital will be relocated. Also, the combined sewer on

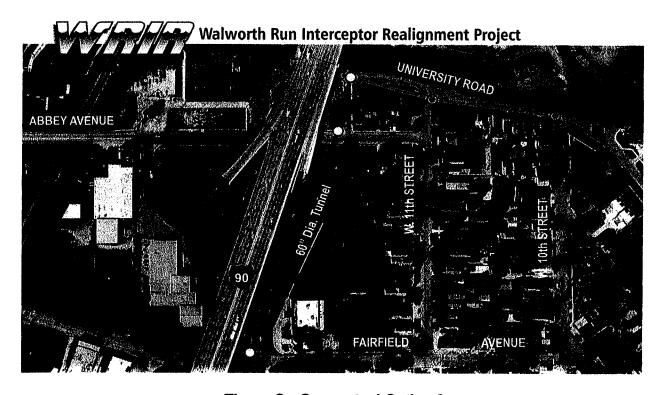


Figure C - Conceptual Option 3

Fairfield Avenue connecting to Regulator WR-24 may need to be upsized. The dry weather outlet from Regulator WR-24 to West 14<sup>th</sup> Street may also need to be upsized.

The major advantage of Option 3 is only one shaft is needed as the drive shaft for the microtunnel (tunnel) operation. This shaft would be located at Abbey Avenue. Also, this option



only has two (2) tunnel shafts, therefore reducing the number of tunnel shafts necessary for the run when compared to the other options. Option 3 meets the requirement to remove the WRI from the future Innerbelt Project area. This alternative also has less traffic conflicts.

However, there are some disadvantages with Conceptual Option 3. The existing WRI would remain along a longer portion of University Road, which may be a concern regarding future slope failures or movements. Another disadvantage is that the starting point of Option 3 is very close to the final Innerbelt grading at the corner of University Road and West 13<sup>th</sup> Street and may conflict with the future grading plan for the eastbound bridge.

### 2.4 Option 4

Conceptual Option 4 is shown in Figure D, and is a variation of Option 1. Conceptual Option 4 consists of 500' of 60" diameter tunneled pipe and three (3) structures. The 60" tunneled pipe would begin by connecting to the existing WRI at University Road and West 13<sup>th</sup> Street and run south approximately 200' to Abbey Avenue near West 13<sup>th</sup> Street in to a manhole. The alignment would then travel westbound along Abbey Avenue for a distance of approximately 300' to the intersection of Abbey Avenue and West 14<sup>th</sup> Street. At this point, the 60" tunneled pipe would connect to the existing WRI with a connecting structure.

As with the other options, several sewer pipes would be removed or abandoned with this option. Additionally, Regulator WR-25 at Crown Avenue and West 14<sup>th</sup> Street would be abandoned and Regulator WR-24 on Fairfield Avenue would be rebuilt. The existing 190' run of 12" sanitary sewer on Crown Avenue for the Animal Hospital will be relocated. Also, the combined sewer on Fairfield Avenue connecting to Regulator WR-24 may need to be upsized. The dry weather outlet from Regulator WR-24 to West 14<sup>th</sup> Street may also need to be upsized.

Option 4 removes the WRI from the westbound Innerbelt Bridge slope regrading area, and similar to Option 1 provides a relatively short relocation run of tunnel to the connection at Abbey Avenue and West 14<sup>th</sup> Street. However, a significant portion of the relocated WRI is still



in the footprint of the eastbound Innerbelt Bridge and passes under the current Innerbelt alignment. This alignment maintains a section of existing WRI along West 14<sup>th</sup> Street under the current Innerbelt Bridge and therefore limits options regarding the potential alignment or subsurface needs of a future eastbound bridge. The existing WRI would remain along a longer portion of University Road, which may be a concern regarding future slope failures or movements. Another disadvantage is that the starting point of Option 4 is very close to the final Innerbelt grading at the corner of University Road and West 13<sup>th</sup> Street and may conflict with the future grading plan for the eastbound bridge.

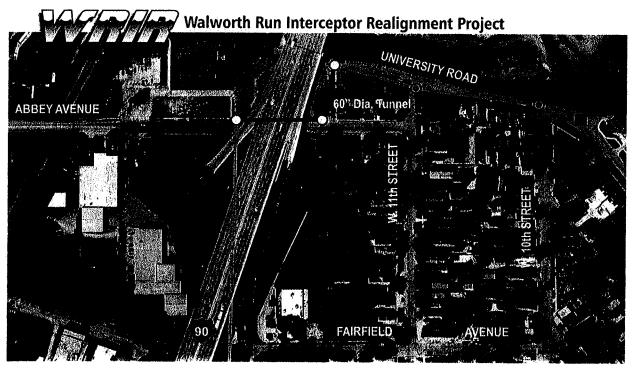


Figure D - Conceptual Option 4

### 2.5 **Option 5**

Conceptual Option 5 is shown in Figure E. This option consists of approximately 1,900' of 60" diameter tunneled pipe and four (4) major interceptor structures. The 60" tunneled pipe would begin by connecting to the existing WRI near Regulator WR-27A located on University Road, close to West 10<sup>th</sup> Street. From this point, the alignment would run southwest for



approximately 200' in to a manhole located on West 10<sup>th</sup> Street. From this point, the 60" tunneled pipe alignment would run southward along West 10<sup>th</sup> Street for a distance of approximately 600' to the intersection of West 10<sup>th</sup> Street and Fairfield Avenue. At this intersection, a manhole would be installed. From this structure, the alignment would run westbound for approximately 1,100' along Fairfield Avenue to the connection point at the intersection of Fairfield Avenue and West 14<sup>th</sup> Street. At this point, the 60" tunneled pipe would connect to the existing WRI with a connecting structure. As with the other options, several sewer pipes would be removed or abandoned with this option. Additionally, Regulator WR-25 at Crown Avenue and West 14<sup>th</sup> Street would be abandoned and Regulator WR-24 on Fairfield Avenue would be rebuilt. The existing 190' run of 12" sanitary sewer on Crown Avenue for the Animal Hospital will be relocated. Also, the combined sewer on Fairfield Avenue connecting to Regulator WR-24 may need to be upsized. The dry weather outlet from Regulator WR-24 to West 14<sup>th</sup> Street may also need to be upsized.

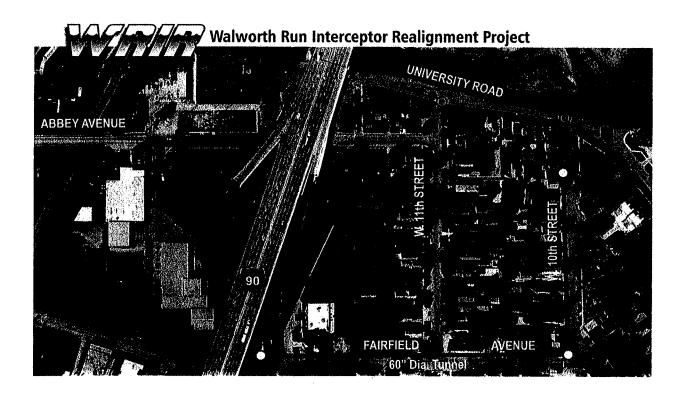


Figure E - Conceptual Option 5



Option 5 completely removes the WRI from the University Road area, which may be a long term slope failure concern. There could also be a possible reduction in flow to CSO-081, near the Cuyahoga River, based on favorable hydraulic evaluations. In addition, Option 5 meets the requirement to remove the WRI from the future Innerbelt Project area.

Option 5 is estimated to be the most costly option. It has a total length of 1,900 feet. Because the beginning and ending inverts are controlled by the existing WRI sewer, the proposed pipe may need to be larger than 60" diameter due to a lesser slope. The proposed diameter of the pipe would need to be evaluated. Additional soil borings would be required, adding to the total design cost. Also, two of the work shafts for Option 5 would be located in the Tremont neighborhood and may have stakeholder concerns. This option exceeds the original intent of the WRI relocation project.

## Section 3 – Table 3.1 - Estimate of Probable Construction Cost (2010 Dollars)

Table 3.1 on the following pages lists estimated probable construction costs for the proposed WRI construction options. These costs are preliminary budgetary estimates based on comparison with recently completed projects. They do not include design engineering, construction administration, field inspection, legal review, easement acquisition, or property procurements costs that may be associated with the construction project.



Option 1	Qty.	Unit	Unit Cost	Total
Mobilization	1	LS	\$200,000	\$200,000
Tunnel Shaft w/Junction Chamber No. 1	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/ Manhole	1	Ea.	\$400,000	\$400,000
Tunnel Shaft w/Junction Chamber No. 2	1	Ea.	\$750,000	\$750,000
60" Tunneled Pipe	900	LF	\$2,500	\$2,250,000
Utility Relocations	1	LS	\$250,000	\$250,000
Remove / Abandon Sewer Pipes 24" & Smaller	3,400	LF	\$100	\$340,000
Remove / Abandon Sewer Pipes 30" & Larger	1,100	LF	\$200	\$220,000
Remove / Abandon Exist. 64" WRI	800	LF	\$500	\$400,000
Abandon Regulator WR-25	1	Ea.	\$20,000	\$20,000
Rebuild Existing Regulator WR-24	1	Ea.	\$30,000	\$30,000
Upsize WR-24 DWO Alignment	450	LF	\$200	\$90,000
Relocate Exist. 12" Sanitary to Animal Hospital	190	LF	\$150	\$28,500
Upsize Combined Sewer to WR-24	260	LF	\$200	\$52,000
Subtotal				\$5,780,500
Contingency (30%)				\$1,734,150
Option 1 Total				\$7,514,650
			USE	\$7.5 M

Option 2	Qty.	Unit	Unit Cost	Total
Mobilization	1	LS	\$200,000	\$200,000
Tunnel Shaft w/Junction Chamber No. 1	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/Junction Chamber No. 2	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/ Manhole No. 1	1	Ea.	\$400,000	\$400,000
Tunnel Shaft w/ Manhole No. 2	1	Ea.	\$400,000	\$400,000
60" Tunneled Pipe	1,400	LF	\$2,500	\$3,500,000
Utility Relocations	1	LS	\$250,000	\$250,000
Remove / Abandon Sewer Pipes 24" & Smaller	3,400	LF	\$100	\$340,000
Remove / Abandon Sewer Pipes 30" & Larger	1,100	LF	\$200	\$220,000
Remove / Abandon Exist. 64" WRI	1,500	LF	\$500	\$750,000
Abandon Regulator WR-25	1	Ea.	\$20,000	\$20,000
Rebuild Existing Regulator WR-24	1	Ea.	\$30,000	\$30,000
Upsize WR-24 DWO Alignment	450	LF	\$200	\$90,000
Relocate Exist. 12" Sanitary to Animal Hospital	190	LF	\$150	\$28,500
Upsize Combined Sewer to WR-24	260	LF	\$200	\$52,000
Subtotal				\$7,780,500
Contingency (30%)				\$2,334,150
Option 2 Total				\$10,114,650
			USE	\$10.1 M



Option 3	Qty.	Unit	Unit Cost	Total
Mobilization	1	LS	\$200,000	\$200,000
Tunnel Shaft w/Junction Chamber No. 1	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/Junction Chamber No. 2	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/ Manhole	1	Ea.	\$400,000	\$400,000
60" Tunneled Pipe	1,000	LF	\$2,500	\$2,500,000
Utility Relocations	1	LS	\$250,000	\$250,000
Remove / Abandon Sewer Pipes 24" & Smaller	3,400	LF	\$100	\$340,000
Remove / Abandon Sewer Pipes 30" & Larger	1,100	LF	\$200	\$220,000
Remove / Abandon Exist. 64" WRI	1,200	LF	\$500	\$600,000
Abandon Regulator WR-25	1	Ea.	\$20,000	\$20,000
Rebuild Existing Regulator WR-24	1	Ea.	\$30,000	\$30,000
Upsize WR-24 DWO Alignment	450	LF	\$200	\$90,000
Relocate Exist. 12" Sanitary to Animal Hospital	190	LF	\$150	\$28,500
Upsize Combined Sewer to WR-24	260	LF	\$200	\$52,000
Subtotal				\$6,230,500
Contingency (30%)				\$1,869,150
Option 3 Total				\$8,099,650
			USE	\$8.1 M

Option 4	Qty.	Unit	<b>Unit Cost</b>	Total
Mobilization	1	LS	\$200,000	\$200,000
Tunnel Shaft w/Junction Chamber No. 1	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/Junction Chamber No. 2	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/ Manhole	1	Ea.	\$400,000	\$400,000
60" Tunneled Pipe	500	LF	\$2,500	\$1,250,000
Utility Relocations	1	LS	\$250,000	\$250,000
Remove / Abandon Sewer Pipes 24" & Smaller	3,400	LF	\$100	\$340,000
Remove / Abandon Sewer Pipes 30" & Larger	1,100	LF	\$200	\$220,000
Remove / Abandon Exist. 64" WRI	400	LF	\$500	\$200,000
Abandon Regulator WR-25	1	Ea.	\$20,000	\$20,000
Rebuild Existing Regulator WR-24	1	Ea.	\$30,000	\$30,000
Upsize WR-24 DWO Alignment	450	LF	\$200	\$90,000
Relocate Exist. 12" Sanitary to Animal Hospital	190	LF	\$150	\$28,500
Upsize Combined Sewer to WR-24	260	LF	\$200	\$52,000
Subtotal				\$4,580,500
Contingency (30%)				\$1,374,150
Option 4 Total				\$5,954,650
		to don't commence to the company of the com-	USE	\$6.0 M



Option 5	Qty.	Unit	Unit Cost	Total
Mobilization	1	LS	\$200,000	\$200,000
Tunnel Shaft w/Junction Chamber No. 1	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/Junction Chamber No. 2	1	Ea.	\$750,000	\$750,000
Tunnel Shaft w/ Manhole No. 1	1	Ea.	\$400,000	\$400,000
Tunnel Shaft w/ Manhole No. 2	1	Ea.	\$400,000	\$400,000
60" Tunneled Pipe	1,900	LF	\$2,500	\$4,750,000
Utility Relocations	1	LS	\$250,000	\$250,000
Remove / Abandon Sewer Pipes 24" & Smaller	3,400	LF	\$100	\$340,000
Remove / Abandon Sewer Pipes 30" & Larger	1,100	Ŀ	\$200	\$220,000
Remove / Abandon Exist. 64" WRI	2,000	LF	\$500	\$1,000,000
Abandon Regulator WR-25	1	Ea.	\$20,000	\$20,000
Rebuild Existing Regulator WR-24	1	Ea.	\$30,000	\$30,000
Upsize WR-24 DWO Alignment	450	LF	\$200	\$90,000
Relocate Exist. 12" Sanitary to Animal Hospital	190	LF	\$150	\$28,500
Upsize Combined Sewer to WR-24	260	LF	\$200	\$52,000
Subtotal				\$9,280,500
Contingency (30%)				\$2,784,150
Option 5 Total				\$12,064,650
			USE	\$12.1 M

# **Section 4 – Comparison of Sewer Construction Options**

Five (5) general WRI construction options were described and evaluated. Table 4.1 summarizes these options and presents estimated probable construction costs, advantages, and disadvantages associated with each option.



# **Table 4.1 – Summary of WRI Construction Options**

Description	Estimated Probable Construction Cost (2010 Dollars)	Advantages	Disadvantages
Option 1	\$7.5 Million	<ul> <li>Removes WRI from westbound bridge grading area.</li> <li>Relatively short tunnel run</li> <li>Meets required schedule</li> </ul>	Relocated WRI is in the eastbound Innerbelt Bridge footprint and may conflict with future eastbound bridge needs.
Option 2	\$10.1 Million	<ul> <li>Relocated WRI is completely removed from the Innerbelt footprint</li> <li>Meets required schedule</li> </ul>	Longer project length with respect to other options (except Option 5)
Option 3	\$8.1 Million	<ul> <li>Relocated WRI is completely removed from the Innerbelt footprint.</li> <li>Only 2 tunnel shafts necessary</li> <li>Only 1 drive shaft needed</li> <li>Minimal traffic conflicts</li> <li>Meets required schedule</li> </ul>	<ul> <li>Long length of existing WRI run on University Rd. may be future concern for slope failures</li> <li>Connection point very close to final Innerbelt grading at University Rd. and West 13<sup>th</sup> St.</li> </ul>
Option 4	\$6.0 Million	<ul> <li>Removes WRI from westbound bridge grading area.</li> <li>Minimal traffic conflicts</li> <li>Meets required schedule</li> </ul>	<ul> <li>Long length of existing WRI run on University Rd. may be future concern for slope failures</li> <li>Connection point very close to final Innerbelt grading at University Rd. and West 13<sup>th</sup> St.</li> </ul>
Option 5	\$12.0 Million	<ul> <li>WRI not in conflict with future Innerbelt Project area</li> <li>Completely removes WRI from University Rd. area, thus easing future slope failure concern</li> <li>Possible reduction in flow to CSO-081 based on favorable hydraulic evaluation</li> <li>Most likely will have schedule implications</li> </ul>	<ul> <li>2 work shafts located in Tremont neighborhood may have Stakeholder concerns</li> <li>May need larger diameter pipe than 60" due to long length of run and pipe grades.</li> <li>Additional soil borings required</li> <li>Most costly option</li> </ul>



#### Section 5 – ODOT's Comments and Concerns

ODOT reviewed DLZ's Technical Memorandum dated Jan 11, 2010 and provided comments. DLZ's responses are as follows:

ODOT District 12 Comments (By David Lastovka): Comments Dated 1/20/2010

# 1. Alignment Recommendation

<u>Comment 1A:</u> ODOT concurs with the recommended Option #2 alignment (University-W11th-Abbey-frontage road between Abbey & Fairfield)

DLZ Response: Comment Noted.

### 2. Phasing

<u>Comment 2A:</u> During detail design, ODOT requests consideration for project phasing that considers earlier abandonment/removal of the Westerly Low Level Interceptor between Abbey and the NS overpass in the project construction schedule. If the Westerly Low Level Interceptor can be abandoned early, then the ODOT project can begin removal of the Cold Storage building, along with initial slope excavation, in advance of completion of the Walworth Run Interceptor relocation. This strategy would allow some overlap in both ODOT's and NEORSD's construction schedules.

<u>DLZ Response:</u> DLZ will investigate the hydraulic impacts of abandoning or removing the Westerly Low Level Interceptor between Abbey Avenue and the NS overpass as an early phase of construction. Please note that earlier abandonment/removal would require an elaborate bypass pumping plan.

#### 3. Right of Way

<u>Comment 3A:</u> As previously discussed, early identification of any needed project right of way is critical to maintaining the project schedule.

<u>DLZ Response</u>: DLZ understands that early identification of any needed project right-of-way is critical to maintaining the project schedule. As of this report, it appears that the main sewer tunnel will be constructed without the need of right-



of-way. However, it should be noted that as the project progresses it may become necessary to obtain additional right-of-way for construction staging areas or other reasons.

<u>Comment 3B:</u> Additionally, since this relocation is within the Tremont Historic District, any additional RW needs may require additional Environmental coordination with the Federal Highway Administration (FHWA). If at all possible, the relocation work should be designed within the existing public right of way.

**DLZ Response:** Comment Noted.

<u>Comment 3C:</u> ODOT's record right of way plans were emailed to DLZ on 1-15-2010.

**DLZ Response:** DLZ has received ODOT's record right of way plans.

#### 4. Access Shaft Locations

<u>Comment 4A:</u> Maintenance of Traffic (MOT) - During detail design, consideration should be given to minimizing local traffic impacts.

<u>DLZ Response:</u> DLZ will investigate ways to minimize local traffic impacts. One example is the relocation of the downstream connection away from the Fairfield Avenue/West 14<sup>th</sup> Street intersection to a location in the ODOT property on the southwest corner.

<u>Comment 4B</u>: W14th/Fairfield Shaft Location - ODOT's record information for the existing 60" Walworth run interceptor reflects that the sewer is east of the location shown on the Conceptual Plan graphic. Depending on the exact location of the existing sewer, consideration should be given to moving the access shaft either north or south of the Fairfield/W14th intersection, in order to minimize the work area's impact on traffic. See attached screen capture from the project's DGN basemap file.

<u>DLZ Response:</u> The field survey recently completed by DLZ shows the WRI on the west side of West 14<sup>th</sup> Street in the tree lawn. Currently it is contemplated that the downstream connection may be moved to the southwest corner of the Fairfield Avenue and West 14<sup>th</sup> Street intersection.



### 5. City of Cleveland Coordination

<u>Comment 5A:</u> The Innerbelt project has had significant coordination with Cleveland Engineering & Construction (Rob Mavec), Traffic (Andy Cross), and Water Pollution Control (Rachid Zoghaib). These offices should be coordinated with during project development.

<u>DLZ Response:</u> Coordinating with the aforementioned offices is standard operating procedure. DLZ is very familiar with the City of Cleveland and will coordinate as necessary.

#### 6. Interim Condition

Comment 6A: There is a need to coordinate the existing I90 and local storm drainage (mainly west of W13th and north of Fairfield) with the proposed work. As you progress in detail design we will need to determine the disposition of this storm water, both in the interim condition and permanently.

<u>DLZ Response:</u> DLZ will address this issue during the design phase and work with ODOT.

#### 7. Survey Control

<u>Comment 7A:</u> Confirmation that both projects are on the same survey control and all questions related to this topic are resolved.

<u>DLZ Response:</u> DLZ's survey will show elevations and horizontal coordinates referenced to the Ohio State Plane North Zone NAD 83 and NAVD 88 Datums as the primary system with the Cleveland Regional Geodetic Survey (CRGS) Datum as the secondary system.

#### 8. As-Built Plans

<u>Comment 8A:</u> Does NEORSD have as-built plans created for projects? Coordination between the as-constructed NEORSD project and the ODOT design-build team will be very important.

<u>DLZ Response:</u> Yes, the design team will provide ODOT with all available as-builts at the completion of the project.



### 9. Haul Roads for NEORSD Project

<u>Comment 9A:</u> In coordination with Cleveland, our Design-Build project is not allowing Scranton or West 14<sup>th</sup> to be project haul roads. These same restrictions should be in place for the NEORSD project.

<u>DLZ Response</u>: DLZ will take these restrictions into account.

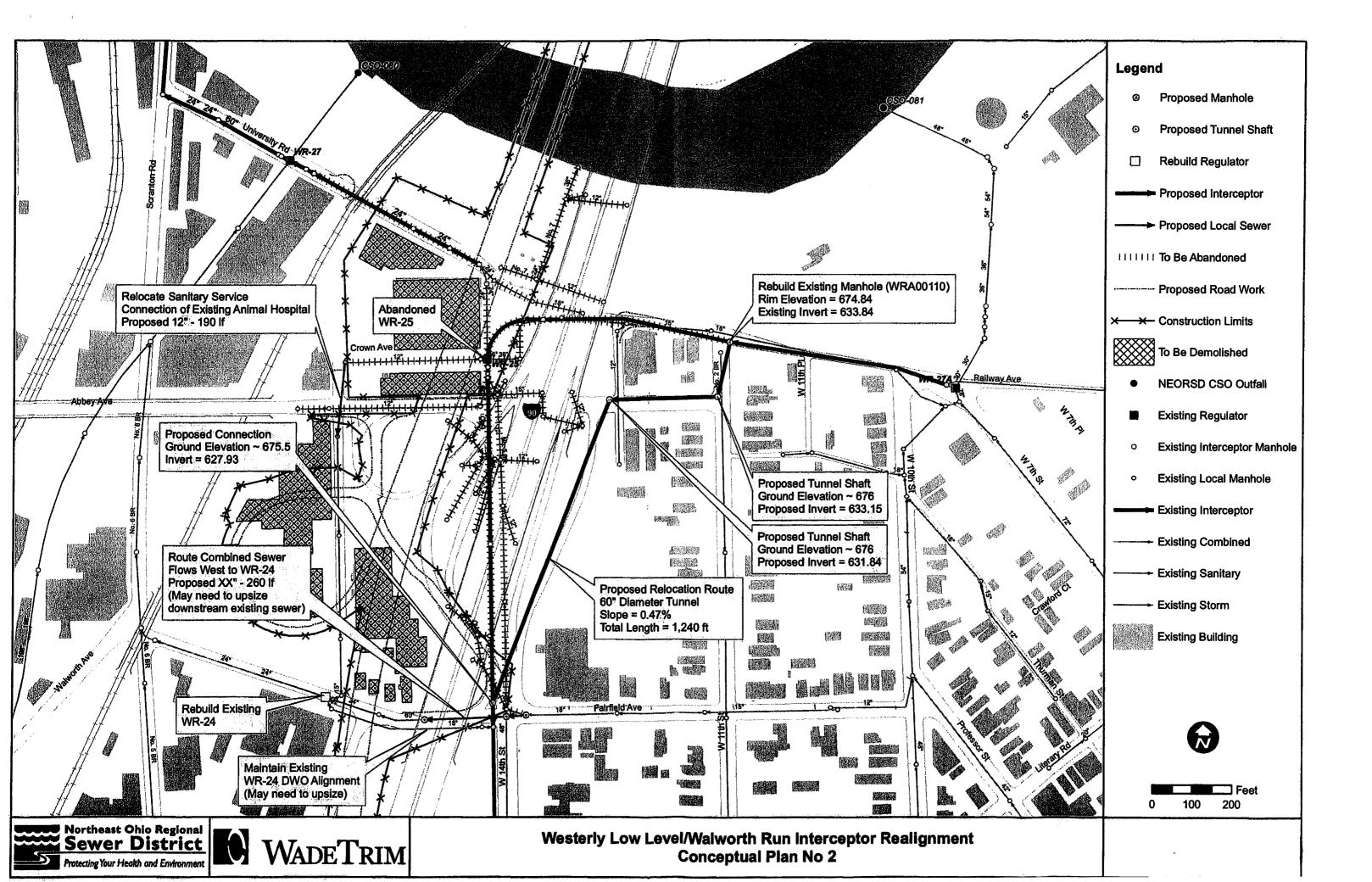
#### 10. Vibration Monitoring

<u>Comment 10A:</u> We recommend requiring vibration monitoring of properties adjacent to the NEORSD work locations. Section 9.3.4 of the Design-Build scope addresses ODOT's approach to Vibration Monitoring and Control. This scope language can be provided upon request.

<u>DLZ Response:</u> DLZ will investigate vibration monitoring of properties adjacent to the NEORSD work locations.

### Section 6 – Recommendation

Based on the evaluation of the above options, considering the project goals, cost and schedule, DLZ concurs with the original NEORSD recommendation that **Option 2** be selected as the preferred alternate for the WRIR. The estimated probable construction cost for the recommended sewer construction plan is \$10,100,000 (2010 Dollars). This plan is shown on the attached plan view exhibit previously prepared by NEORSD and Wade Trim. This estimate should be regarded as a budgetary planning estimate. The estimate will be revised and updated throughout the project's design as more detailed design information becomes available.



APPENDIX "B"

**Draft Soil Boring Logs** 

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Solar Testing Laboratories, Inc. 1126 Valley Belt Road Brooklyn Heights, Ohio 44131 Telephone: 216-741-7007

#### **BORING NUMBER B-1**

PAGE 1 OF 2

PROJECT NAME   Walkworth Real Interceptor Realignment (WRIRI) Project			_			16-741-7011	-1001							PAG	7E 1 '	UF 2	
DATE STARTED 11/18/09 COMPLETED 11/18/09 GROUND ELEVATION BORNIS CONTRACTOR Seles Testina Laboratories, Inc.  DRILLING METHOD. Indices Size August LOGGED BY R. Spellary  DRILLER J. Degranek  VATER ON ENCOUNTER 38.8 ft  VATER O	CLIE	NT _	North	east	Ohi	o Regional S	ewer District	PROJECT NAME Wal	worth Run is	ntercep	tor Re	alignn	ent (V	VRIR)	Projec	t	
DRILLING CONTRACTOR   Scient Testing Laboratories, Inc.   DRINGE COLATION   W. 11th & University	PRO.	JEÇT	NUN	BEF	<u> </u>	09570x10		_ PROJECT LOCATION	W 11th, Ab	bey, V	/ 14th	Street	s, Clev	eland,	Ohio		
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### BORING NUMBER B-1 PAGE 1 OF 2

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					R Solar Testing Laboratories, Inc. BORING LOCATION V			<u>/</u>					
DRILI	LING MI	ETH	OD	_H	llow Stem Auger GROUND WATER LEVI	ELS:							
LOGO	SED BY	<u>R.</u>	Sp	ella	DRILLER J. Deranek VATER ON ENC								
NOTE	:s				¥WATER ON COM		38.8 ft						
HOLE	SIZE		_		AUGER SIZE 4.25 I.D. WATER AFTER	HRS:	<del></del>						
O DEPTH	SAMPLE TYPE		U.S.C.S.	<b>GRAPHIC LOG</b>	MATERIAL DESCRIPTION	BLOW COUNTS (N VALUE)	RECOVERY % (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIMIT	PLASTICITY WE INDEX	
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_	ss				Loose to medium dense brown medium to fine SAND, little (Moist)	2-3-4-4 (7)							
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SS

Solar Testing Laboratories, Inc. 1125 Valley Belt Road Brooklyn Heights, Ohio 44131 Telephone: 216-741-7007

#### **BORING NUMBER B-1**

Telephone: 216-741-7007 PAGE 2 OF 2 Fax: 216-741-7011 PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project CLIENT Northeast Ohio Regional Sewer District PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio PROJECT NUMBER A09570x10 **ATTERBERG** UN. COMP.
STRENGTH (tsf)
DRY UNIT WT.
(pcf) MOISTURE CONTENT (%) SAMPLE TYPE GRAPHIC LOG LIMITS U.S.C.S. PLASTICITY INDEX DEPTH (ft) MATERIAL DESCRIPTION aure ytuic 35 Medium dense brown FINE SAND, some silt, few sandy (Moist) 6-8-9-10 silt layers. (continued) SS ям 🕽 (17)Medium dense brown medium to fine, SAND, trace silt. 7-5-6-7 (Wet) SS **CUAINED** (11)39.0 ¥ Medium dense to dense gray SILTY FINE SAND. (Moist) 9-9-10-11 40 20.7 SS (19)10-15-21 SILTY SAND. SS SM 27 (36)10-12-13recomes medium daose with 16 SS (25)45 (Moist) 7-10-11-15 interlayers. SS (21)166 gray FINE SAND, little sill 16-23-27 (Moist) SS 29 BE COMES DEUSE (50)12-14-17 Medium dense to dense gray SILTY FINE SAND, clayey silt interlayers (stratified). 21 (31) SS 3-7-9-11 A SILTY SAND TO SILT. 31 SS (16)10-14-18 20 (32) (Moist) SS 55 12-18-20 (Wet) SS Medium dense graf SILT little sand, trace clay, few silty clay interfavers (stratified). 7-8-9-11 SS (17) 4-6-9-10 60 24.9 25 5 20 SS (15)4-5-7-9 (Wet) SS MŁ (12)8-9-10-12 SS (19)65 27 POSHTH6 19 ST Stiff to very stiff gray SILTY CLAY, little sand, few silt 6-9-9-11 interlayers (laminated) 23 SS (18)8-11-12-14 70 SS Lean Clay (23)6-7-7-9 31 11 20 SS 25.7 (14) 5-6-7-9

Bottom of hole at 75.0 feet,

(13)



#### **BORING NUMBER B-1**

PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10

PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

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	SS		SM		37.0	Medium dense brown FINE SAND, some silt, few sandy silt layers. (continued)	(Moist)	6-8-9-10 (17)						
-	SS		SP		39.0 ₹	Medium dense brown medium to fine SAND, trace silt.	(Wet)	7-5-6-7 (11)						
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_	ss		SM					10-15-21- 27 (36)						
 45 _	ss				45.0			10-12-13- 16 (25)						
	SS		SM		47.0	Medium dense gray SILTY FINE SAND, few silt interlayers.	(Moist)	7-10-11-15 (21)						
	SS		SM			Dense gray FINE SAND, little silt.	(Moist)	16-23-27- 29 (50)						
50	ss				49.5	Medium dense to dense gray SILTY FINE SAND, silt and clayey silt interlayers (stratified).	(Wet)	12-14-17- 21 (31)						
	ss		SM					3-7-9-11 (16)						
- <b>-</b> _55	ss		SM- ML				(Moist)	(32)						
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	ss					Medium dense gray SILT, little sand, trace clay, few silty clay interlayers (stratified).	(Moist)	7-8-9-11 (17)						
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	ss							6-7-7-9 (14)		25.7				
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CLIENT North	reas
PROJECT NUM	/BE

olar Testing Laboratories, Inc. 125 Valley Belt Road

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CLIE	NT N	orthe	east	Ohio	Regional Sewer District	PROJECT NAME Walk	vorth Run Ir	tercep	tor Re	alignm	ent (V	/RIR) f	<sup>2</sup> roject	
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DATE	STAI	RTEI	) 1	1/19	/09 COMPLETED 11/19/09	GROUND ELEVATION _								
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					ter DRILLER J. Deranek	· ·		7.0 ft						
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					Loose brown SAND, little gravel, trace sil interlayers.	t, few silty clay (Moist)	(11)	}						
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	i I							ľ						
	<u> </u>		И		18.5 Medium dense brewn SAND, trace silt.		5-6-8							
20	SS				Woodalli delise metri delise, il dece sinti	TRACESILT (Moist)	(14)		5.5					
			SP		BECOMES									
			or.											
_			41		Loose brown 5, little gravel, trace sill	, few sifty clay	2-3-4							
25	SS				interlayers.	(Moist)	(7)		11.9					-
			SP		da a									
_			-		BECOMES.									
					00.5									
					28.5 Medium dense brown FINE SAND little s	filtr (Moist)	5-7-9							
30	SS					- (IXIOISI)	(16)							
													:	
			SM		SILTYS	HVD.								
- <b>-</b>		Y	_			-								
	SS				· •		7-8-11							



### BORING NUMBER B-2 PAGE 1 OF 2

					Regional Sewer District PROJECT NAME W									
					09570x10 PROJECT LOCATION				/ 14th	Streets	s, Clev	<u>eland,</u>	Ohio	
					/09 COMPLETED 11/19/09 GROUND ELEVATION									
					R Solar Testing Laboratories, Inc. BORING LOCATION			iversity	<u>/</u>					
					Illow Stem Auger GROUND WATER LE									
					ter DRILLER J. Deranek YWATER ON EN									
					¥ WATER ON CO		_							
HOLE	SIZE	<del></del> -	_	_	AUGER SIZE 2.25 l.D. WATER AFTER	₹ 	HRS:	<del></del>			<del></del>		TERBE	.00
o DEPTH	SAMPLE TYPE	808		GRAPHIC LOG	MATERIAL DESCRIPTION		BLOW COUNTS (N VALUE)	RECOVERY % (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIQUID	LIMITS	
<u></u> _					5" ASPHALT, 4¾" BRICK PAVER, 3" BASE, 6" CONCRETE.	$\exists$								
 	SS	-	X	X	1.6  2.5  FILL: CINDERS & SAND.  Loose brown SAND, little gravel, trace silt, few silty clay interlayers. (Moi	ist)	9-6-5 (11)							
5	SS						4-2-3 (5)							
· -	SS						4-4-4 (8)							
10	ss	SF					3-3-3 (6)		7.7					
15	SS	;				-	3-3-2 (5)		6.8					
20	SS	SF			18.5 Medium dense brown SAND, trace silt. (Moi:	ist)	5-6-8 (14)		5.5					
25	SS	SF			23.5 Loose brown SAND, little gravel, trace silt, few silty clay interlayers. (Moi	ist)	2-3-4 (7)		11.9					
30	SS	-			28.5 Medium dense brown FINE SAND, little silt. (Moi.	ist)	5-7-9 (16)					•		
· -	SS	SM	4 100				7-8-11 (19)							



#### **BORING NUMBER B-2**

PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project
PROJECT NUMBER A09570x10 PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

	ш			ø			ł	8		સ્	نے	AT	TERBE LIMITS	
	SAMPLE TYPE		S.S.	GRAPHIC LOG		WEEDIN DESCRIPTION	BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (t	DRY UNIT WT (pcf)	0.		Г
€	AP.E.		U.S.C.S.	APHI		MATERIAL DESCRIPTION SILTY SAND	N VSUS	88	OIS	ENG ENG	(pd)	LIQUID	PLASTICITY INDEX	PLASTIC
5	AS AS		. ا	GR.		3121 7 37102		뿐	≥છ	STR	絽		₽₽	딥
		7	SM			Medium dense brown (INE SAND, little silt. (continued) (Moist								
4		Ч		XI.	37 <u>.0</u> 🕎	Medium dense brown FINE-SAND, trace silt.								
4						-GRAINED								
,	ss					-6(A)DED	3-5-8 (13)							
			SP											
-														
-				71.	43.5	Dense to very dense gray SILTY FIME SAND. (Maint	45.00.00							
;	SS					Moist	15-22-28 (50)		23.3					
4						SILTY SAND.								
+		ł				3101   011.2							•	
1			SM			·	16-22-30	ł						
	SS				·		(52)							
4														
+			•											Ì
]				1	54.0		11-16-17							
<u>;    </u>	SS					Medium dense to dense gray SILT, some sand, few thin silty clay interlayers. (Moist	(33)							
1														
	ļ		ML											
+	SS		·				10-15-11		19.8			NP	NP	١.,
	-			Ш	60.0	Bottom of hole at 60.0 feet.	(26)	1						
					1									
								ŀ						
					•									



### BORING NUMBER B-2 PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District	PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project
PROJECT NUMBER A09570x10	PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio
	ATTERBERG

	ца	1		90			(	%,	E (%)	i. (tsf)	VT.		ERBE	
(H) (H)	HAVE BYPE	מאווו דר	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%	UN. COMP. STRENGTH (t	DRY UNIT WT (pcf)	LIQUID LIMIT	PLASTICITY INDEX	PLASTIC LIMIT
			SM		Medium dense brown FINE SAND, little silt. (continued) (Me	oist)								
					37.0 ▼ Medium dense brown FINE SAND, trace silt.	 Vet)								
-	SS						3-5-8							
40			SP				(13)							
				TT.	Dense to very dense gray SILTY FINE SAND.  (Mc		15-22-28		23.3					
_ 45 _	SS				(NA)	JISIJ	(50)		23.3					
			SM				16-22-30							
50	SS						(52)							
-					54.0		44 40 47							
 55	SS				Medium dense to dense gray SILT some sand few thin	oist)	11-16-17 (33)							
-			ML											
-			IVIL											
 60	SS			Ш	0.0		10-15-11 (26)		19.8					ļ
					Bottom of hole at 60.0 feet.									
1	1	1	ı					I	l	l	1	L	L	L

#### ADD PP - WHERE APPLICABLE.

Solar Testing Laboratories, Inc. 1125 Valley Belt Road Brooklyn Heights, Ohio 44131 Telephone: 216-741-7007

### BORING NUMBER B-3 PAGE 1 OF 2

		ı	Eax:	216	3-741-	-7011													
CLIEN	IT <u>N</u>	orthe	ast	<u>Ohio</u>	Regi	ional S				PROJECT NAME									
PROJ	ECT N	IUME	3ER	A	09570	0x10				PROJECT LOCA	TION _	W 11th, Abl	ey, W	14th 8	Streets	, Cleve	eland, (	<u>Ohio</u>	
										GROUND ELEVA									
										BORING LOCAT			ey						
DRILL	ING N	/ETH	IOD	Ho	llow S	Stem /	Auger		<del></del>	GROUND WATE									j
LOGG	ED B	Y <u>R</u>	. Sp	ellaç	<u>y</u>		DRILLER _	J. Deranek	·	V WATER O									—I
NOTE	s							<del> </del>		WATER O	N COMP	LETION _6	0.0 ft						
HOLE	SIZE						AUGER SIZE	4.25 I.D.		WATER A	FTER _	HRS:	=						
о ОЕРТН	SAMPLE TYPE		U.S.C.S.	GRAPHIC LOG				MATERIAL [				BLOW COUNTS (N VALUE)	RECOVERY % (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pd)	ļ	PLASTICITY WE INDEX STIRE	
- 1	SS			o •//	1.0	1	SILT.			GRAVEL trace	(Moist)	4-4-4-3 (8)							
	ss		SI C		_	OH	ECK.					3-4-4-6 (8)							
	ss			6. ( 0.	7.0							7-9-12-10 (21)		4.4					
	SS						Loose to mediu gravel, trace sili				(Moist)	3-3-3-5 (6)							
10	SS		SP							0(=)(: = 1)		2-3-5-5 (8)							
; ;	SS				13.0						(Wet)	3-6-6-10 (12)							
 15	SS			• (			Medium dense	brown SANL	3 & GRAVE	L) trace silt.	(Moist)	7-7-11-8 (18)			'				
	ss	(	SP GP	000	-	CH	Eeve.					5-8-9-9 (17)							
 	SS			, , ,								6-7-8-10 (15)		4.8					
<u>20</u> 	SS		_	0	20.3	· · · · · · · · · · · · · · · · · · ·	Medium dense	brown FINE	SAND, trac	æ gravel, silt.	(Moist)					-			
- 	SS		SP					**	-biain	ed		8-9-11-12 (20)							
25	SS				25.0		Medium dense	harres CII TO	V FIME CAN	ID four thin		7-9-9-10 (18) 10-11-12-							
	SS					•	interlayers of sa		PNE SAI	vo, iew umi	(Moist)	13 (23)							
-	SS		SM						SILT	y sand		8-8-8-10 (16)							
30	SS				31.0	)			01125	(OII T. by)		5-5-6-11 (11)							
	ss	(	ML SP	#		ӯ	Medium dense of FINE SAND	to dense bro trace silt, st	own SAND)	/ SILT, intertayers	(Wet)	6-8-9-11 (17)							
ļ	SS	\	٦	1		_	OHECK					4-5-8-9 (13)							



#### **BORING NUMBER B-3**

PAGE 1 OF 2

CLIEN	1T _1	<b>Northe</b>	east	Ohio	Regional Sewer District PROJECT NAME Walk	vorth Run Ir	ntercep	tor Re	alignm	ient (V	/RIR) [	Project	
PROJ	ECT	NUMI	BER	. <u>A</u>	.09570x10 PROJECT LOCATION	W 11th, Ab	bey, V	/ 14th	Street	s, Clev	eland,	Ohio	
DATE	STA	RTEI	<b>o</b> <u>1</u>	1/20	0/09 COMPLETED 11/23/09 GROUND ELEVATION								
					OR Solar Testing Laboratories, Inc.  BORING LOCATION W								
DRILL	.ING	METH	1OD	Ho	ollow Stem Auger GROUND WATER LEVE	LS:							
LOGG	ED E	3Y <u>R</u>	<u>≀. S</u> p	ellac	cy DRILLER J. Deranek	OUNTER 3	2.5 ft						
NOTE	s				¥ WATER ON COMF	PLETION _	60.0 ft						
HOLE	SIZE	=			AUGER SIZE 4.25 I.D. WATER AFTER	HRS:							
	بإ	ή		၂ဗ္ဂ			%	  @	[g.	F.	AT	TERBE LIMITS	
E_	SAMDI E TVDE	=	2.S.	GRAPHIC LOG		BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)			
<b>DEPTH</b> (ft)		<u>F</u>	U.S.C.	Į.	MATERIAL DESCRIPTION	ÄÿŠ¥	Š8	SES	ENG C	S &	LIQUID	E.E.	PLASTIC LIMIT
	100	NAN I	7	GR4		ے ا	REC	ĕÖ	SE E	DR.	55	PLASTICITY INDEX	7 =
0			$\vdash$		2¾" ASPHALT, 4¾" BRICK PAVER, 4" Gray CLAYEY		$\vdash\vdash$	<b> </b> -	<u> </u>	<del> </del>	<b></b>	<u>"</u>	
-			$\vdash$	<b>0</b>	1.0 SILT. Loose to medium dense brown SAND & GRAVEL, trace (Moist)	1112			'	'			
	SS			۰.(	Loose to medium dense brown SAND & GRAVEL, trace (Moist)	4-4-4-3 (8)			'	<b>'</b>			
- +			SP.	0		3-4-4-6			'	'			
5	SS		SP- GP	ه: <sup>ز</sup>		(8)							
	SS			. o. (		7-9-12-10		4.4		'			
_		]		ø	7.0	(21)	] !	~~		1			
_	ss				Loose to medium dense brown MEDIUM SAND, little gravel, trace silt, few silty clay interlayers. (Moist)					'			
_						(6)	!	!	'	'			
10	ss		SP			2-3-5-5 (8)	!			'			
	$\vdash$									'			
	ss				(Wet)	3-6-6-10 (12)				'			
			$\vdash$	0	13.0  Medium dense brown SAND & GRAVEL, trace silt.  (Moist)	7-7-11-8				'			
 15	SS			o (	(MOSC)	(18)				'			
				o.		5-8-9-9							
]	SS		SP- GP	ه ۲		(17)				'			
_ ]	ss			): •: (		6-7-8-10		4.8		/			
				Ø		(15)		"-		!			
20	ss			٥. · · ·	20.3	7-7-8-11 (15)				!			
			$\lceil \cdot \rceil$		Medium dense brown FINE SAND, trace gravel, silt. (Moist)					!			
	ss					8-9-11-12 (20)				!			
- +			SP							!			
 -	ss				05.0	7-9-9-10 (18)				!			
25			$  \cdot  $	11	25.0  Medium dense brown SILTY FINE SAND, few thin interlayers of sandy silt (Moist)	10-11-12-			!	!			
- 1	SS				interlayers of sandy silt.	13 (23)				!			
	00		24			8-8-8-10				!			
_ ]	SS		SM			(16)			!	!			
30	ss					5-5-6-11				'			
_					31.0	(11)			!				
	ss				Medium dense to dense brown SANDY SILT, interlayers of FINE SAND, trace silt, stratified. (Wet)	6-8-9-11 (17)							
			ML- SP		<del>7</del>								
	SS					4-5-8-9 (13)							



#### **BORING NUMBER B-3**

PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10 PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

								r		· · · · · ·	A-T	TERBE	DC.
<b>-</b>	YPE	:	s)	106		V TS JE)	RY %	JRE T (%)	UN. COMP. STRENGTH (tsf)	T WT.	A11	LIMITS	-
DEPTH (ft)	SAMPLE TYPE	}	U.S.C.	GRAPHIC LOG	MATERIAL DESCRIPTION	BLOW COUNTS (N VALUE)	RECOVERY ( (RQD)	MOISTURE CONTENT (%)	N. CO ENGT	DRY UNIT WT. (pcf)	LIQUID LIMIT	PLASTICITY INDEX	PLASTIC LIMIT
35	SAN	; ;		GR/		)) )	BE	⊻ე	STS	K K	57	A €	7
	SS	(	ML- SP	J	Medium dense to dense brown SANDY SILT, interlayers of FINE SAND, trace silt, stratified (continued)  37.0	7-8-23-27 (31)							
_	SS			1	Dense gray SILTY FINE SAND, few silt interlayers. (Moist)	12-20-29- 38							
 40			SM		SILTY SALD	(49) 13-20-26-					to		-ر-
40	SS			1	41.0	32 (46)		/			18	BTIN	<b>1</b> 0
	SS	(	(g)	¥	Very dense gray MERIPMISAND, trace silt. (Moist)	9-24-32-39 (56)		18.4		)	ΝP	ΝP	NP
	ss				Medium dense to very dense gray SILT, some sand, with SILTY SAND interlayers. (Moist)	20-25-28- 31	٠				~~~		
45						(53) 17-25-31-							
	SS		ML- SM	*		34 (56)							
	SS					10-14-16- 22 (30)							
 50	\$S				Medium dense to dense gray SILT, little clay, sand. (Moist)	5-6-7-9 (13)		22			24	5	19
	ss		٠		SNMCLAY	5-6-8-9 (14)							
	ss					4-6-13-14 (19)							
55				#	- Deline Massing	,					NP	NP	NP
		ST	ML		-> pashing pressures						IVI	ME	INF
	ss					10-9-11-14 (20)							
60	SS				₹.	10-15-17- 20 (32)		17					
  - 	ss				63.0	9-12-16-19 (28)							
	ss		SP	<b>++</b> +	Dense gray SAND, trace silt. (Moist)	20-19-28- 34 (47)		:					
65	şs		ML	Ш	Dense gray SANDY SILT. SILT (Moist)	15-20-23- 30							
-			<u> </u>		67.0 Stiff to very stiff gray SILTY CLAY, little sand, stratified, (Moist)	(43) 6-7-8-9		23					
<u> </u>	SS				few silt interlayers.	(15)		23					
70	ss		CL		LEAN CLAY (Wet)	7-9-12-14 (21)							
<u> </u>	SS					6-9 <b>-</b> 11-12 (20)							
75	SS				75.0	6-7-11-13 (18)		25.6					
13	l	L	4	V././.	Bottom of hole at 75.0 feet.	·	-		************				



#### **BORING NUMBER B-3**

PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10

PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

										,	,				
	Ę	T.		90				~ @	%,	ய <u></u> %	(tst)	Å.		TERBE LIMITS	
HTH DEPTH (#)	TOXE TI	SAMPLE	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIQUID	PLASTICITY INDEX	PLASTIC LIMIT
	ss		ML- SP		3	Medium dense to dense brown SANDY SILT, interlayers of FINE SAND, trace silt, stratified. (continued) (W.7.0	et)	7-8-23-27 (31)							
	ss		SM			Dense gray SILTY FINE SAND, few silt interlayers. (Mo	ist)	12-20-29- 38 (49)							
40	ss		Sivi		4	1.0		13-20-26- 32 (46)							
	ss		SP	1111	4	3.0	ist)	9-24-32-39 (56)		18.4			,		
45	ss					Medium dense to very dense gray SILT, some sand, with SILTY SAND interlayers. (Mo	ist)	20-25-28- 31 (53)							
- -	SS		ML- SM					17-25-31- 34 (56) 10-14-16-			:				
- 	SS				4	9.0  Medium dense to dense gray SILT, little clay, sand.		22 (30)							
<u>50</u>	SS		i i			(Mo	st)	5-6-7-9 (13) 5-6-8-9		22					
	SS							(14) 4-6-13-14							
55	SS	<u> </u>						(19)							
	ss	ST	ML					10-9-11-14							
 60	ss					<b>T</b>		(20) 10-15-17- 20		17					
	ss			i				(32) 9-12-16-19 (28)			:				
	ss		SP	Ш		3.0  Dense gray SAND, trace silt. (Moi	st)	20-19-28- 34							
_ 65 	ss		ML			5.0 Dense gray SANDY SILT. (Moi	st)	(47) 15-20-23- 30 (43)			,				
	ss				<u>  -</u>	Stiff to very stiff gray SILTY CLAY, little sand, stratified, few silt interlayers. (Moi	st)	6-7-8-9 (15)		23					
70	ss		CL			(W	et)	7-9-12-14 (21)							
	SS		<u>о</u> г					6-9-11-12 (20)							
 75	SS				7:	5.0  Rottom of hole at 75.0 feet		6-7-11-13 (18)		25.6					

Bottom of hole at 75.0 feet.

## ADD PP WHERE APPLICABLE

	Sola
	1125
	Broo
The state of the s	Tala

ar Testing Laboratories, Inc. 5 Valley Belt Road oklyn Heights, Ohio 44131 aphone: 216-741-7007

### BORING NUMBER B-4 PAGE 1 OF 2

			Fax:	21	-741-7011								
CLIEN	NT _ <u>N</u>	lorthe	east	Ohio	Regional Sewer District PROJECT NAME W	alworth Run I	ntercer	otor Re	alignm	ent (V	(RIR) I	roject	
PROJ	ECT I	NUM	BER	_A	9570x10 PROJECT LOCATION	W 11th, A	bbey, V	V 14th	Streets	, Clev	eland,	Ohio	
DATE	STA	RTEI	· _1	1/30	09 COMPLETED 11/30/09 GROUND ELEVATION								
DRILL	.ING (	CON.	TRA	СТС	R Solar Testing Laboratories, Inc. BORING LOCATION	Abbey at W.	14th R	amp					
DRILL	ING I	VETI	1OD	Н	llow Stem Auger GROUND WATER LE	/ELS:							
LOGG	ED B	Υ <u>· F</u>	≀. Sp	ella	y DRILLER J. Deranek	COUNTER _	34.0 ft						
NOTE	s				¥ WATER ON CO	MPLETION _	34.0 ft						
HOLE	SIZE				AUGER SIZE 4.25 l.D. WATER AFTER	HRS:							
	ш	1	Ī	o			8	3	G.	<u>,_</u>	AT	TERBE LIMITS	
DEPTH (ft)	SAMPI E TYPE	<u>-</u> }	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	N. COMP. ENGTH (t	DRY UNIT WT. (pcf)	LIQUID		PLASTIC
	V V	5	_	GP.		ا ا	₩.	≥8	STR	DR	בבן	₹€	걸기
0					0.8 9%" CONCRETE.	+	+	<del> </del>				<del></del>	
				XX	1.5 FILL: Brown SAND, little gravel (BASE).		1						
	ss		_ ا	0	POSSIBLE FILL: Loose to medium dense brown SAND & (Moi GRAVEL, trace silt.	4-7-8-7 st) (15)							
	SS		SP- GP	oy.	- OHEERS	3-4-3-4	1						
5		(		٠.<	C1)cc \$2	(7)	-						
				9.1 ]:1	6.0 POSSIBLE FILL: Medium dense brown SAND little	+	4.	l					
	SS		SM.		gravel, silt, trace clay.	5-7-9 (16)							
			ر	1.7	85 SILTY SAND		1.						
- 10	SS			0.	Very loose to medium dense brown medium to coarse > SAND & GRAVEL, trace silt, organics, thin silty clay layer. (Moi	6-8-10 (18)		6.4					
-				0	ુલ્લામાર્સ્	"							
 - J		/		0.	_ CHEEK								
<u>-</u>	SS		SP- GP	X.		2-1-2		7.6					
15		(		6		(0)							
_				). Ø	•		i						
-				o C	, ,								
- 20	ss		ML	: • : 1 TIT	19.2 20.0 Medium dense brown SILT, little sand, clay. (Moi	5-5-7 (12)		21.8					
				11	Medium dense brown The silt. (Moi		1						
					7610mED								
. ]					/ "								
						5-6-10	1	10.1	ما	/	ميسن سدد		
25	SS				_ SILTY SAND	(16)	4	10.1			DE	1	
					· 0(0) 1 3 1 WL)			<del></del>	M	ATC	廿	80	16
			SM	$\mathbb{N}$	SOIL DISTRIBUTION		1		t	27	(N)	_	
				1	B-4 235 0 25 70 GRAVEL Q 4 70 SAND 79.1	**	]						
	ss				Yo CO DUSC!	7-7-8			W	111	B:	DR1	20
30					1° 5ANO 70	100	10	<b>√</b> ~					
					71.1	(SA)	ر ره	)					
			1	1.1.1		1		1 .	i				
- 					- Otelle								
			ML SM	<b>.</b>	33.8 Medium dense brown SILT, little sand, interlayers of silty	5-6-9							



### BORING NUMBER B-4 PAGE 1 OF 2

CLIEN	<b>IT</b> _N	lorthe	ast	Ohio	Regional Sewer District PROJECT NAME W						_			
PROJ	ECT N	NUME	3ER	Α	09570x10 PROJECT LOCATION	N <u>W</u>	11th, Ab	bey, W	/ 14th	Streets	s, Clev	eland,	Ohio	
					//09 COMPLETED 11/30/09 GROUND ELEVATIO									
DRILL	ING (	CONT	ra.	СТС	R Solar Testing Laboratories, Inc. BORING LOCATION	Abb	ey at W. 1	14th Ra	amp					
					ollow Stem Auger GROUND WATER LE									
LOGG	ED B	Y _R	t. Sp	ella	DRILLER J. Deranek WATER ON EN									
NOTE	s				¥ WATER ON CO									
HOLE	SIZE	_			AUGER SIZE 4.25 I.D. WATER AFTER	R	_ HRS:		,					
	ц	J		၂ဗ္				%		UN. COMP. STRENGTH (tsf)	ļ <u>;</u>	AT	ERBE	
Ξ	Σ.	•	ις	5			BLOW COUNTS (N VALUE)		15 P	ŽE ŽE	}_∈		Σ	o
DEPTH (ft)	<u> </u>	!	U.S.C.	붚	MATERIAL DESCRIPTION		일을	58	SE	28	<u>5</u> 8	LIQUID	든X	STE
	SAMPI F TYPF		ב	GRAPHIC LOG			-0Z	RECOVERY (RQD)	MOISTURE CONTENT (%)		DRY UNIT WT. (pcf)	을들	PLASTICITY INDEX	PLASTIC LIMIT
0	0,	,						<u> </u>		ίO.			<u>a</u>	
				$\propto$	0.8 93/4" CONCRETE.  1.5 FILL: Brown SAND, little gravel (BASE).									
	ss		-	××	1.5 FILL: Brown SAND, little gravel (BASE).  POSSIBLE FILL: Loose to medium dense brown SAND & (Mc		4-7-8-7							
				a.	GRAVEL, trace silt.	DIST)	(15)							
_	ss		SP- GP	);;			3-4-3-4							
5			-	<u>:</u> ز			(7)							
				0.	6.0									
_	ss				POSSIBLE FILL: Medium dense brown SAND, little gravel, silt, trace clay.	oist)	5-7-9 (16)							
	$\dashv$		SM		8.5	-	(10)	1						
				0	Van loose to medium dense brown medium to coarse	- +	6-8-10		6.4					
10	SS			0.	SAND & GRAVEL, trace silt, organics, thin silty clay layer.	DIST	(18)		6.4					
				٥										
_				0 (										
				0.						İ				
			SP- GP	)		$\vdash$	2-1-2							
15	SS		GF	(			(3)		7.6					
_				0.										
				٥						1				
				6							Ì		:	
		:		0	19.2	F	5-5-7		04.0	ŀ				
20	SS		ML.		20.0 Medium dense brown SILT, little sand, clay. (Mo	oist)	(12)		21.8		ļ	İ		
_					Medium dense brown FINE SAND, little silt. (Mo	oist)								
_														
						-	5-6-10	1	40.4		i			
25	SS						(16)		10.1		ŀ			
			SM						•					
						-	7-7-8	1						
30	SS						(15)	]						
_														
			<u> </u>		33.8 — Madium dages brown SUT little and interlovers of silb.	_	5-6-9	1						
35	SS		ML- SM	111	Medium dense brown SILT, little sand, interlayers of silty	Net)	(15)		İ					



**BORING NUMBER B-4** 

PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Watworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10

PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

												,		
	μ̈	J		ပ္ခ			_	%		tsf)	<u>-</u>	AT	TERBE LIMITS	RG
프	Ž		S.	20			NTS EBJ	DERY DERY	15 K	OMP TH (	후	ο.	È	ე.
DЕРТН (ft)	SAMP! F TYPE	i :	U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	BLOW	COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf	DRY UNIT WT. (pcf)	LIQUID	PLASTICIT INDEX	PLASTIC LIMIT
	NA.		_	용	CHEEK		~ <del>C</del>	뿞	≥ઇ	STS	뚭	3-	A =	۲_
35			ML- SM	H	Medium dense brown SILT, little sand, interlayers of silty fine sand. (continued) (We	t)								
- -					Medium dense gray SILTY FINE SAND, few silt (We interlayers.	t)								
40	SS						?-4-7 (11)		29.3					
-			SM			8-	12-16							
45	SS				·	H	(28)							
					48.0		•							
-	SS				Medium dense to dense gray SILT, little sand, trace clay, some clayey silt interlayers.		5-5-8 (13)							
50							(10)							
-														
55		ÎST										NP	NP	NP
	SS						-19-27 (46)		18.6					
  -														
60	SS		ML			13	-15-17 (32)		19					
<u> </u>														
-						13	-14-10		400					
65	ss		-				(24)	-	16.9					
					ACCORDING TO TESTING @ GBF	۲۱-								
		ŠТ	-	$\parallel \parallel$	R	- \$	H&L	13-1	pus	1/1	6	28	9	19
70		-	-			,	HEL PRE	ร่รับ	pe	8.				
ļ .	-				72.0 Very stiff gray SILTY. CLAY, little sand.	et)								
75	SS	-	CL		TLEAN CLAY	7	-11-14 (25)		22.6					
<u></u>				V.//	Bottom of hole at 75.0 feet.									



### BORING NUMBER B-4 PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District	PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project
PROJECT NUMBER A09570x10	PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

					T								A 7	repor	P.C
25 DEPTH (ff)	SAMPLE TYPE		U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		BLOW COUNTS (N VALUE)	RECOVERY % (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	TIMIT CIOUID	PLASTICITY WINDEX	PLASTIC Z
	SS				37.0	Medium dense brown SILT, little sand, interlayers of silty fine sand. (continued)  Medium dense gray SILTY FINE SAND, few silt interlayers.	(Wet)			29.3					
45	SS		SM		<u> 48.0</u>		. —	8-12-16 (28)							
50	SS					Medium dense to dense gray SILT, little sand, trace clay some clayey silt interlayers.	, (Wet)	5-5-8 (13)							
55	SS	ST						17-19-27 (46)		18.6					
60	SS		ML					13-15-17 (32)		19					
65	SS	ST						13-14-10 (24)		16.9					
70	00	31	CL		72,0	Very stiff gray SILTY CLAY, little sand.	(Wet)	7-11-14		22.6					
75	SS		<u> </u>		75.0	Bottom of hole at 75.0 feet.		(25)	<u> </u>		L		l		



### BORING NUMBER B-5

l						ROJECT NAME Walv			-						
l						ROJECT LOCATION	W 11th, Ab	bey, W	/ 14th	Streets	, Clev	eland,	Ohio	<del></del>	
DATE						ROUND ELEVATION _									
						ORING LOCATION W		bey			· · · · · · · · · · · · · · · · · · ·			—	
DRILL	ING I	METH	HOD	_H		ROUND WATER LEVE									
1		Y F	₹. Sp	ellac	DRILLER J. Deranek	¥ WATER ON ENCO									
NOTE	\$					▼ WATER ON COM									
HOLE	SIZE			-	AUGER SIZE 4.25 I.D.	WATER AFTER	HRS:		<del></del>		r===		TEODE		
1	L L	ı		ဗ္ဂ	·	•		%	ш̂	(F)	Ϋ́.		TERBE LIMITS		
F_	AMAPI E TYPE	-	S.	GRAPHIC LOG			BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%	UN. COMP. STRENGTH (13	يئ ⊒	ا ا	PLASTICITY INDEX	U	
DEPTH (ft)	ā	i :	U.S.C.	품	MATERIAL DESCRIPTION		282≥	58	泛류	28	<b>[5</b> 8	LIMIT	등짓	E TE	
~	M A		~	[8			OS	E E	ĭĕĝ	52	DRY UNIT (pcf)	울리	Ş≅	PLASTIC LIMIT	
0			<u> </u>	Ŭ	OI AODUALT AUDDIOIC DAVED		<u> </u>			S.			<u>~</u>	$\vdash \vdash \vdash$	
-			$\vdash$	XX	0.6 3" ASPHALT, 4" BRICK PAVER.  FILL: Brown SAND, little silt, trace gravel, or	coal, few thin (Moist)	1			,					
				₩	silty clay layers.	(IVIOIST)	11-9-8								
ļ	SS			₩		•	(17)								İ
5	ss			▩	4.5': STORM SEWER at edge of hole. Cou past. Moved hole 2 feet east.	ld not auger	4-3-4-4 (7)								
				₩	FILL Brown SAND & GRAVEL, trace silt, for	ew thin silty (Moist)	4-3-3-3								
-	SS			₩	clay layers.	(	(6)								
-				₩			1-1-1-50/2"								
-	SS			₩	9.0 8.5': Abandoned METAL PIPE.		1-1-1-50/2								
- 40				XX	Loose to medium dense brown medium to	coarse SAND, (Moist)	5-7-4-3					ĺ			
10	SS				some gravel, trace silt.		(11)								
					44 OLO Strate Mark January of Ollows OLON	- eldined	0.4.6.7							,	
	SS		SP	1	11.3': 8-inch-thick layer of SILTY CLAY.	MANESON	3-4-6-7 (10)	.							
		_			- V	THE SOLL OF	2000								
-	SS				C+1-7115 307	al ou ams	3-6-9-9 (15)		5.9				1 1	. ]	
15			34		150 Leose to medium dense brown line to med	um SAND.									
	SS			:::	Trace-off DECOMES MEDIUM	DEEDSE TOORS	7-7-9-13 (16)								
			SP			7 Minkesi								. 1	
	ss				BECOTES LOOSE		7-5-4-4 (9)					. 1			
					19.0 Loose brown SILTY SAND, trace gravel.										
20	SS		SM	11	20.0 Lease to will our dense brown fine to medi	(Moist)	6-5-5-6 (10)							İ	
-		,	ļ		trace silt.	(Moist)									
-	ss	(	SP.	)			6-8-8-9 (16)					.		.	
		ì	ı		23.0 Loose brown fine to medium SAND, little gr		ļ					. 1		.	
_	SS		SP		Loose brown line to friedlight SAND, little g	(Moist)	4-3-4-4					. 1	i		
25			<u> </u>		25.0	N 1911 296 - 4	<u> </u>				ادسم	_			
L _	SS				Loose to medium dense brown FINE SANI	Moist)			-7:4		S	1	acc	CRD	ilde Istria
						-	(8)				4	اس ا		لمدا	
_	ss		SM	H.	\\ \Cu	ty saud	3-4-6-6				,	20 P	43 EV	<i>-</i> 4	SIXIG
	-00		بر کا	M	310	1 0000	(10)				128	T 2			
30	00						6-9-10-12					. 1	i		
	SS				31.0		(19)							, [	
_					Loose to medium dense brown FINE SAND	), trace silt. (Moist)	3-2-3-5							. [	
_	SS				<del>*</del>	(Wet)									
-			SP		·	26.8.4.4	8-10-12-15 (22)								
35	SS			`		(MOIST)	(22)								, I



### BORING NUMBER B-5 PAGE 1 OF 2

CLIEN	NT Nort	heast	Ohi	io I	Regional Sewer District PROJECT NAME	Valv	vorth Run In	tercep	tor Re	alignm	ent (V	RIR) F	roject	
PROJ	ECT NU	MBEF	? _£	٩0	9570x10 PROJECT LOCATIO	N _	W 11th, Ab	bey, V	/ 14th	Streets	s, Clev	eland,	Ohio	
DATE	START	ED _	11/2	3/(	9 COMPLETED 11/27/09 GROUND ELEVATION	ON _								
DRILL	ING CO	NTRA	CTO	OF	Solar Testing Laboratories, Inc. BORING LOCATION	<u> W</u>	. 14th & Abl	bey						
DRILL	ING ME	THOE	<u>H</u>	loi	ow Stem Auger GROUND WATER L									
LOGG	SED BY	R. S	oella	СУ	DRILLER J. Deranek ————————————————————————————————————									
NOTE	s				WATER ON C	OMI	PLETION _4	18.0 ft						
HOLE	SIZE		<del></del> -	<del></del>	AUGER SIZE _4.25 I.D. WATER AFTE	R_	HRS:							
	Щ		99					%	ଛ	tst)	Ŀ	AT	TERBE	
DEPTH (ft)	SAMPLE TYPE	U.S.C.S.	GRAPHIC LO		MATERIAL DESCRIPTION		BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIQUID	TICITY DEX	PLASTIC LIMIT
0	SAM	٦	GRA				_0 <u>S</u>	REC	≅ģ	STRE	PR√	음크	PLAS IN[	PLA
		$\blacksquare$	XX	X	.6 3" ASPHALT, 4" BRICK PAVER.		1							
	$\blacksquare$	İ	$\otimes$	X	FILL: Brown SAND, little silt, trace gravel, coal, few thin silty clay layers.	loist)	11-9-8				:			
	SS		$\otimes$	8			(17)							
 5	ss				4.5': STORM SEWER at edge of hole. Could not auger past. Moved hole 2 feet east.		4-3-4-4 (7)		:					
	ss		▓		FILL Brown SAND & GRAVEL, trace silt, few thin silty clay layers.	loist)	4-3-3-3 (6)							
	SS				.0 8.5': Abandoned METAL PIPE.		1-1-1-50/2"							
10	ss				Loose to modium dense brown medium to coarse SAND	loist)	5-7-4-3 (11)							
 	ss	SP			11.3': 8-inch-thick layer of SILTY CLAY.		3-4-6-7 (10)							
  15	ss				5.0		3-6-9-9 (15)		5.9		:			
	ss				Lease to madium dense brown fine to madium SAND	oist)	7-7-9-13 (16)							
	ss	SP			9.0		7-5-4-4 (9)							
 20		SM		1	L CULTY CALID (	oist)	6-5-5-6							
	SS				Loose to medium dense brown fine to medium SAND	oist)	(10)							
	ss	SP			3.0		6-8-8-9 (16)							
  25	ss	SP			Loose brown fine to medium SAND, little gravel, trace silt. (M	oist)	(7)							
	ss				Loose to medium dense brown FINE SAND, little silt, trace (M	oist)	4-3-5-6 (8)		7.4					
	ss	SM					3-4-6-6 (10)							
30	SS				10		6-9-10-12 (19)							
- 	SS				- <del>V</del> -	loist) Vet)								
35	SS	SP			(М	loist)	8-10-12-15 (22)							



#### **BORING NUMBER B-5**

PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10

PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

								<del></del>				4.77		
	Щ	ı		၅				%	Е (%)	i. (tsf)	۷Ŧ.		ERBE	
S DEPTH	SAMPI E TYPE		U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION		BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIQUID	PLASTICITY INDEX	PLASTIC LIMIT
	ss		SP		Loose to medium dense brown FINE SAND, trace silt. (Moi	st)	5-8-10-11 (18)							
	SS			11	38': Heaving SAND.  38.2  Medium dense gray SILT, some sand, interlayers of wet FINE SAND, trace sit, stratified.  (Moi	_	4-7-9-12 (16)							
40	SS	,	بمصوبه	*	FINE SAND, trace sit, stratified.	1	5-7-11-13 (18)							
	\$\$		SM- ML	7	Is THIS ONE??		6-9-10-11 (19)							
45	SS				45.0		3-6-8-9 (14)							
-	SS		SM		Medium dense gray SILTY FINE SAND. (Mol	st) S	9-12-14-17 (26)							
	SS				48.0 ▼  Medium dense gray SILT, some sand, few silty sand interlayers. (Moi	st)	4-6-9-11 (15)	,						
50		,s <u>T</u>		$\prod$								22	3	19
	SS		ML		Posting pressures	ļ	8-9-15-19 (24)							
. 55·	SS		A		55.97		12-15-19- 23 (34)							
	ss				Dense gray SILT, little sand, clay. (Moi	st)	11-16-19- 26 (35)		20.1					
- <b>-</b>		ST	ML	╫	_ boahing diseasones		16-19-21-					NP	NP	ΝP
60 -	SS						26 (40) 14-17-20-							
	SS				63.0 Stiff to very stiff gray \$ILTY CLAY) little sand, interlayers	$\downarrow$	25 (37) 14-11-15-		17.6					
- 65	SS				of SILT, stratified. (Moi	st)	16 (26)							
	SS				(we	et)	5-6-8-10 (14)							
	SS.		CL- ML		69-71 - LEAN CLAY			0						
70		ŚŤ	-		The							29	9	20
 	SS					-	8-11-14-18 (25)		22					
- <b>-</b> 75	SS		<u> </u>		75.0 Bottom of hole at 75.0 feet.		7-9-12-14 (21)	ļ	22.5			ļ		



**BORING NUMBER B-5** 

PAGE 2 OF 2

CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10

PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

	Ш	1		90					%	ш <sup>©</sup>	i. (tsf)	Υ.	ATI	ERBE	RG
ж DEРТН (ft)	SAMPLETYPE		U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIQUID LIMIT	PLASTICITY INDEX	PLASTIC LIMIT
-	SS		SP			e to medium dense brown FINE SAND, trace silt. inued)	(Moist)	5-8-10-11 (18)							
1	ss			.11	38.2	leaving SAND. um dense gray SILT, some sand, interlayers of wet	(Wet)	4-7-9-12 (16)							
40	ss				FINE	SAND, trace silt, stratified.	(Moist)	5-7 <b>-</b> 11-13 (18)							
-	SS		SM- ML					6-9-10-11 (19)							
-	ss							3-6-8-9 (14)	:						
45 -	ss		SM		45.0 Medi	um dense gray SILTY FINE SAND.	(Moist)	9-12-14-17 (26)							
-	ss				48.0 ▼ Medi	um dense gray SILT, some sand, few silty sand	(Moist)	4-6-9-11 (15)						ı	
50		ST		•	incom	ayoro.									
1	ss		ML					8-9-15-19 (24)						ı	
- 55	SS				55.0			12-15-19- 23 (34)							
	ss				Dens	e gray SILT, little sand, clay.	(Moist)	11-16-19- 26 (35)		20.1					
-		ST	MŁ												
60	SS							16-19-21- 26 (40)		!					
-	SS				63.0			14-17-20- 25 (37)		17.6					
- 65	SS				Stiff	to very stiff gray SILTY CLAY, little sand, interlayers LT, stratified.	(Moist)	14-11-15- 16 (26)						'	
	ss						(Wet)	5-6-8-10 (14)							
1	ss		CL- ML						0						
70		ST	ML												
-	SS							8-11-14-18 (25)		22					
75	ss				75.0			7-9-12-14 (21)		22.5					!



### BORING NUMBER B-6 PAGE 1 OF 2

ı						Sewer District			-									
l					409570x10				_	CATION _	W 11th, Ab	bey, V	/ 14th	Streets	s, Clev	eland,	Ohio	
						COMPLE				_								
DRILI	LING	CON	TRA	CT	OR Solar T	esting Laborat	tories, Inc.		_ BORING LOCA	ATION W	. 14th Ram	p to Ab	bey (s	outh e	nd)			
DRILI	LING	MET	HOD	<u>+</u>	lollow Stem	Auger												
LOGG	SED I	BY F	R. Sp	ella	icy	DRILLER	J. Derane	ek	_									
NOTE	:s _								_ ¥ WATER		LETION _	54.0 ft						
HOLE	SIZE	Ē	T	_	<del></del>	AUGER SE	ZE <u>4.25 l.C</u>	) <u>.</u>	WATER	AFTER _	HRS:			·		· · · · · ·		
	}	T.		g	: <b> </b>							%	⊊	(tsf)	ΜŢ.		ERBE IMITS	
Ŧ_	}	<u>-</u>	οj.	120	<b>.</b> .				•		BLOW COUNTS (N VALUE)	X 6	35	ŽE.	\ E_		7	^
DEPTH (ft)		7	U.S.C.	표			MATERI	AL DESCRIP	TION		│ 있중▼	SQ S	ISE TSE	ၓၑၟ	38	LIQUID	EXE.	ĭĭ
<u></u>		SAMPLE IYPE	7	GRAPHIC LOG							205	RECOVERY (RQD)	MOISTURE CONTENT (9	UN. COMP. STRENGTH (t	DRY UNIT (pof)	g S	PLASTICIT INDEX	PLAST LIMIT
0		,, 		L									Ŭ	S			귭	
ļ <u>-</u>	SS			X	803	4" TOPSOIL FILL: Brown		silt	·	(Moist)	2-1-2-3							
				▩	8,,					<b>,</b> ,	(3)					٠.		
	ļ	}	<b>=</b> =	X	28.7	FILL: Gray S	SILTY FINE	SAND, trace of	organics.	(Moist)								•
_	ss	ŀ	SP-	·	1	Loose brown	SAND & G	RAVEL, trace	silt.	(Moist)	3-4-5							
5	00		GP	D.:	5.5				•		(9)							
			-	Š			ise brown fin	e to medium,	SAND, trace silt,	(Moist)								
	SS		SP		3	gravel.		. 2	GRAINED	(WOISI)	6-8-7 (15)		7.2		i			
			35							·	(/							
					9.0						11-18-23							
10	SS					Hard brown	SILTY CLAY	, little sand, t	race CaCO <sub>3</sub> ,	2 7 (Moist)	(41)							
- 4					<b>]</b>		1 CA 1/	NAV										
			CL		7		LEAN	7 7										
					<b>.</b>									l				
	3			<i>!!!!</i>	13.6	Loose brown	MEDIUM S	AND, some o	ravel, trace silt.		3-2-3							
15	SS						3	GRAINED	,	(Moist)	(5)					l		
- 4					1											l		
			SP													İ		
. 4										:						- 1	- 1	
	00			11	19.0						11-16-14		40.0	ł			l	i
20	SS			11		Medium den: lenses, trace	se brown Fill gravel.	NE SAND	le silt, few silty cla	y (Moist)	(30)		10.9	j	1	I	ļ	
-				1				1					İ			.		
				1			(	1 ~ A	W.				1	ľ		İ		İ
					1		$\Rightarrow \iota$	TY SAI					I		1		1	
	-		SM							ŀ	13-10-14		ŀ					
25	SS			:11						1	(24)				Ī		ı	
													Ì		Ì			ļ
. 4														l				
				#	:		•	, and the same of										
_	긁				29.0 ▽	<del></del>					12-3-4		_					
30	SS					Loose to med of SAND,	dium dense l	brown SAND'	Y SILT, interlayers	(Wet)	(7)		30					
. ]					]						<u> </u>	Į	21	امرده	This	10	05.	
_			ML- SP						-			- \$	THE	er	10	124	ا (د	
			٦٢		]													1
. 」				111	.]					f	3-8-13				-			
35	SS		_ }	Ш	1						(21)						-	



### BORING NUMBER B-6 PAGE 1 OF 2

CLIEN	1T <u>N</u>	lorthe	east (	<u>Ohi</u>	Regional Sewer District PROJECT NAME Wa	worth Run I	ntercer	tor Re	alignm	ent (V	/RIR) [	Project	
PROJ	ECT N	NUME	BER	A	09570x10 PROJECT LOCATION	W 11th, At	bey, V	V 14th	Streets	s, Clev	eland,	Ohio	
DATE	STAF	RTEC	1_1	1/28	8/09 COMPLETED 11/28/09 GROUND ELEVATION								
					OR Solar Testing Laboratories, Inc.  BORING LOCATION 1	V. 14th Ram	p to At	bey (s	outh e	nd)			
DRILL	.ing N	VETH	IOD	_H	ollow Stem Auger GROUND WATER LEV								
LOGG	ED B	Y <u>R</u>	. Sp	ella	DRILLER J. Deranek WATER ON ENC								
NOTE	s												
HOLE	SIZE	_			AUGER SIZE 4.25 I.D. WATER AFTER	HRS:	<del></del>	<del></del>	1				
, DEРТН (ft)	SAMPLE TYPE		U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	BLOW COUNTS (N VALUE)	RECOVERY % (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIMIT	PLASTICITY WE BE INDEX	
0			_	₹ \$\$\$	0.3_, 4" TOPSOIL.	2-1-2-3	$\vdash$					-	
	SS			₩	FILL: Brown SAND, little silt. (Mois	(3)							
- 1			_=	₩	2.5	7	1						
			en.	o : `	Loose brown SAND & GRAVEL trace sitt	ــــــــــــــــــــــــــــــــــــــ	-						
5	SS		SP- GP	): : 1	(Moist	) 3-4-5 (9)							
			-4	O	5.5 Medium dense brown fine to medium SAND, trace silt,								
_ ]	SS				gravel. (Moist	′  0-0- <i>/</i>		7.2					
_			SP			(15)	-						
					9.0	11-18-23	1						l
10	SS				Hard brown SILTY CLAY, little sand, trace CaCO <sub>3</sub> . (Moist	1445	]						
								İ					
			CL										
_ ]							İ					•	
_ ]			_		13.6 Loose brown MEDIUM SAND, some gravel, trace silt.	3-2-3	┨		1				Ī
15	SS	- [			(Moist	(5)							
_													l
			SP										ł
_							]						
_ ]		ļ			19.0	11-16-14	1	40.0					
20	SS				Medium dense brown FINE SAND, little silt, few silty clay lenses, trace gravel. (Moist	(30)	1	10.9					
_ ]													
_			Ì										
			Ì										
_			ям (			13-10-14	1						
25	SS					(24)	1						
_													[
_			}										
_		ļ		111.	29.0 ▽	12-3-4	1	20					
30	SS				Loose to medium dense brown SANDY SILT, interlayers of SAND. (Wet		-	30					
			ML- SP										
			ا										
	SS		-			3-8-13	1						
35	33		i	11		(21)	<u> </u>						



# BORING NUMBER B-6 PAGE 2 OF 2

i					Regional Sewer District PROJECT NAME Walk									-
PROJ	ECT I	NUM	BEK	_A(	09570x10 PROJECT LOCATION	vv mm, An	bey, v	14m 3	Sileers	, Cleve	elano,	Office		
	į.	ـــــــــــــــــــــــــــــــــــــ		စ္ပ		, n n	%	ы (%)	(fsf)	WT		TERBI		
35 DEPTH	SAMPI E TVDE		U.S.C.S.	GRAPHIC LOG	MATERIAL DESCRIPTION	BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%	UN. COMP STRENGTH (	DRY UNIT ( (pd)	LIQUID LIMIT	PLASTICITY INDEX	PLASTIC LIMIT	
		7	ML-	1	Loose to medium dense brown SANDY SILT interlayers of SAND. (continued) (Wet)									
<b>-</b>					37.0 Medium dense to dense gray SILTY FINE SAND. (Wet)									
40	SS				silty sand	7-13-16 (29)		22.6						
			SM		·							ستمحر	·	
45	SS				# SILT (ML)	7-16-26 (42)		21.2		7	NP	NP	NР	
												) /		
				11	48.0 Dense gray FINE SAND, trace silt (Moist)	8-10-24				$\gamma$				\
50	SS	,	~	V.	(SM) SILTY SAND!	(34)		22.3		\	NP	NP	NP	
		(	Ś₽	1	<1			- 1						
55	ss				54.0 ▼  Dense gray SILT, little sand. (Moist)	13-19-28 (47)		18						
- 3			ML		57.0									
					Very stiff gray CLAYEY SILT, little sand. (Moist)									•
60	SS		ML			7-8-9 (17)		21.1			24	5	19	)
												,,		
65	SS		CL		63.5 Stiff gray SILTY CLAY, little sand, few silt interlayers. (Moist)	4-4-5 (9)		28.6	¢	j 	/- 44	ाइ <sub>व</sub>	- L	
- 55			R		Bettom of hole at 65.0 feet.	<u></u>			٠		- 1		U A	- 1
													7	_
					LEAN CLAY DEVISE THIS BURING G	6								
					BUNNE									
			,											



#### **BORING NUMBER B-6**

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CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10

PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

		 		9570X10		PROJECT LOCA		vv i iui, Ab	UCY, VV	14413	ou ce is	, Cievi	elaliu,	Onio	
	ű		90					(c)	%	E %)	o (tsf)	VT.	AT	ERBE	RG
S DEPTH (ft)	SAMPI E TVPE	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRI	PTION		BLOW COUNTS (N VALUE)	RECOVERY 9 (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIQUID	PLASTICITY INDEX	PLASTIC LIMIT
		ML- SP		of SAN 37.0	to medium dense brown SAN ND. (continued)		(Wet)								
				Mediu	m dense to dense gray SILTY	FINE SAND.	(Wet)	7-13-16							
40	SS							(29)		22.6					
45	SS	SM						7-16-26 (42)		21.2					
	SS		11.	48.0 Dense	gray FINE SAND, trace silt.		 (Moist)	8-10-24 (34)		22.3					
50		SP						(34)							
 55	SS	ML		54.0 ▼ Dense	gray SILT, little sand.		(Moist)	13-19-28 (47)		18					
				57 <u>.0</u> Very st	iff gray CLAYEY SILT, little sa		 (Moist)								
60	SS	ML					; ;	7-8-9 (17)		21.1					
- - 65	ss	CL		53.5 Stiff gra	ay SILTY CLAY, little sand, fe	•	——— (Moist)	4-4-5 (9)		28.6					
					Bottom of hole at 65.	D feet.									



### BORING NUMBER B-7 PAGE 1 OF 2

1						Sewer District										<u> </u>
					09570x10						v 14th	Street	s, Clev	eland,	Ohio	
1						COMPLETED 12/3/09		_			·1/-	م مادم	- 4 <b>1</b>			
i						Testing Laboratories, Inc.				D IO AL	Dey (r	ionn e	na)			
						Auger DRILLER J. Deranek	GROUND WATE			704						
NOTE						DAILLER J. Belatier	WATER O						-			
HOLE						AUGER SIZE 4.25 I.D.			HRS:				··			
	T		T	(n	T	AOOER CALL TIED IID.			Ī	Ī.,				AT	TERBE	
DEPTH (#)	F	<u> </u>	C.S.	IC LOG		MATERIAL DESCRIPT	TION		BLOW COUNTS (N VALUE)	ÆRY %	TURE %	OMP.	TW T'S	0.	LIMITS	
DE C	100	SAMPLE 17PE	U.S.	GRAPHIC		WATERIAL DECORNI	ioit		30 <b>₹</b>	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIMIT	PLASTICITY INDEX	PLASTIC LIMIT
0	<u> </u>	_	┡			10" TOPSOIL.	•			Γ_		S	_		<u>a</u>	<u> </u>
-	ss		$\vdash$	<u>11.</u>	0.8	FILL: Brown SAND, little silt, trace grav	vel. brick.		2-2-3-4 (5)							
<u> </u>	<u> </u>			▓			•	(Moist)	- (0)							
5	ss			▓	3.5	FILL Brown SAND & GRAVEL, trace s	silt, brick.	(Moist)	3-3-5 (8)							
				▓												
-	SS			▓					4-3-3 (6)							
10	ŞS			▓					3-3-4 (7)		7					
-				▓												
-				▓												'
15	SS			❈					10-16-20 (36)		5					
				▓												
	SS		- 617	燚	19.0 19.5	At the state of th		(9.4-1-4)	9-13-17		14.5					
20	33		ML		20.5	Medium dense brown SILTY SAND.  Medium dense brown SILT, little sand.  Dense brown fine to medium SAND, tra	ace slit.	(Moist) (Moist)	(30)		14.5					
								(Moist)								
	SS		SP						12-15-16 (31)							
<u>25</u> 						4100			(31)							
					<u>27.0 ¥</u>	Loose to very dense brown FINE SAND silt layers.	), little silt few thin	 (Wet)								
30	SS								9-9-12 (21)		22.1				٠.	
-			SM				~									
						SILTY SA	N t7									
 35	SS								18-19- 50/4"							



BORING NUMBER B-7
PAGE 1 OF 2

<b></b>																
						Sewer District				-						
i											<u>v 14tn</u>	Street	s, Ciev	eland,	Unio	
ŀ						completed 12/3/09 esting Laboratories, Inc.					abov (n	orth o	nd)			
					Hollow Stem					ID IO AL	buey (I	iorun ei	iiu)			
						DRILLER J. Deranek				7 O ft						
	SIZE					AUGER SIZE 4.25 I.D.			HRS:			•				
			Γ	,			•		<del></del>	T				AT	TERBE	RG
I	SAMPI E TYPE	=	S	OCI JIHQVQU	3				_\Σ <u>Ψ</u>	% }	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	-	LIMITS I≻	
DEPTH (ft)	<u>i</u>	}	U.S.C.S.	١	<u> </u>	MATERIAL DESCRIPT	TION		ALC N		SE SE	8 <u>5</u>	E G	₽⊨	먇	阜上
	AMA	į	٦	2	3				BLOW COUNTS (N VALUE)	RECOVERY (RQD)	88	S.E.	<u>`</u>	LIQUID	PLASTICITY INDEX	PLASTIC LIMIT
0	υ.	) 		ſ	1					<u>~</u>	-0	ST	□	_	]	۵
	ss		<u> </u>	×>	0.8	10" TOPSOIL.			2-2-3-4							
				×	▓	FILL: Brown SAND, little silt, trace gra	vel, brick.	(Moist)	(5)							
				$\bigotimes$	× .											
	ss			×	3.5	FILL: Brown SAND & GRAVEL, trace	silt, brick.	 (A dain4)	3-3-5	1						
5	33			$\bigotimes$	്			(Moist)	(8)							
				$\otimes$	$\aleph$											
	ss			$\otimes$	×				4-3-3							
				燹	8				(6)							
	SS			$\bowtie$	X .				3-3-4	1	7					
10				燹	X				(7)							
	-			$\bigotimes$	8						·					
				燹	8										.	
• -				$\bigotimes$	8										.	
	SS			$\otimes$	8				10-16-20		5				ļ	
15	-			$\otimes$	8				(36)							
				燹	Ž											
				$\bowtie$	ૅ											
				燚	8100											
20	ss			$\widetilde{A}$	19.0	Medium dense brown SILTY SAND.		(Moist)	9-13-17 (30)		14.5					
20	-	ļ	ML.	Щ	20.5	Medium dense brown SILT, little sand.		(Moist)	(00)							
٠ ٦						Dense brown fine to medium SAND, tra	ace silt.	(Moist)								
`														Ì		
. 1			SP		.]				10 17 10			1		l		
25	SS				.]				12-15-16 (31)					ľ		
											İ					- 1
	ĺ	į			27.0 <b>V</b>					İ		ľ				
					: <del>-</del>	Loose to very dense brown FINE SANI silt layers.	), little silt few thin	(Wet)								
. }	_				.]	on layors.			9-9-12		- 1					
30	SS		İ						(21)		22.1					
4			ѕм													
					-											
_																
_	ss								18-19-							
35	1	- 1	ŀ	-1.1	-1			i	50/4"		- 1	- 1	ı			



#### **BORING NUMBER B-7**

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CLIENT Northeast Ohio Regional Sewer District PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project PROJECT NUMBER A09570x10 PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

PROJ	ECT	NUM	BER	₹ <u>_</u>	\09570x1	0						PR(	DJECT	LOCA	TION .	W 11th, A	bbey, \	<u>V 14th</u>	Street	s, Clev	eland,	Ohio	
25 DEPTH (ft)	TOY II IOMAG	מאולים ביים	U.S.C.S.	GRAPHIC LOG				M	ATERI.	IAL DE	ESCRIF	PTION				BLOW COUNTS (N VALUE)	RECOVERY %	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	LIMIT	PLASTICITY INDEX	<u>ş</u>
40	SS		SM			Lo silt	ose to ve layers.	ery den (continu	ued)	own Fli			silt few		(Wet)	3-4-5 (9)	_						
45	SS	1	SM		47 <u>.0</u> 49.8	Me	dium dei	nse gra	FINE	E SAN			S:AN	Ø 	 (Wet)	5-6-9 (15) 7-10-13 (23)		25.3					
55		"ST	ML			Der	nse gray	SILT,	little sa	and, cl	ay.			(PP	(Wet) ⊃≃4.5+)	()	13	18.1			24	3	20 20
60	SS				60.0			Во	ttom of	f hole	at 60.0	feet.				16-24-25 (49)		21.2					
	-																			The state of the s			
																						,	



#### **BORING NUMBER B-7**

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CLIENT Northeast Ohio Regional Sewer District PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project PROJECT NUMBER A09570x10 PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

					0001001									
35 (#)	SAMDI E TVDE		U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION		BLOW COUNTS (N VALUE)	RECOVERY % (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	PLASTICITY WE HE INDEX	
40	SS		SM			Loose to very dense brown FINE SAND, little silt few thin silt layers. (continued)	(Wet)	3-4-5 (9)						
45	SS		SM		47 <u>.0</u>	Medium dense gray FINE SAND, little silt.  Dense gray SILT, little sand, clay.	(Wet)	5-6-9 (15) 7-10-13 (23)		25.3				
  - 55		ST	ML				(Wet) =4.5+)		13	18.1				
60	SS				60.0	Bottom of hole at 60.0 feet.		16-24-25 (49)		21.2				



## BORING NUMBER B-8 PAGE 1 OF 2

CLIE	NT _	North	east	Oh	io Regional	Sewer District	PRO	JECT NAM	E Wa	lworth Run la	ntercep	tor Re	alignm	ent (V	/RIR)	Project	<u>t </u>
PRO.	JECT	NUN	IBEF	₹ _/	A09570x10		PRO	JECT LOCA	NOITA	W 11th, At	bey, V	V 14th	Street	s, Clev	eland,	Ohio	
DATE	STA	RTE	D _	12/1	/09	COMPLETED _12/2/09	GRO	UND ELEV	ATION								
DRIL	LING	CON	ITRA	CT	OR Solar	Testing Laboratories, Inc.	BOR	ING LOCAT	по <b>м</b> _/	V. 14th & Fa	irfield						
DRIL	LING	MET	HOD	<u> </u>	lollow Stem	Auger	GRO	UND WATE	R LEV	ELS:							
LOG	BED E	BY _	R. S	pella	су	DRILLER J. Deranek	<u>\</u>	WATER O	N ENC	OUNTER _2	6,0 ft						
NOTE	:s _						<u>Y</u>	WATER O	N COM	IPLETION _	44.0 ft						
HOLE	SIZI	<u> </u>		1	<del></del>	AUGER SIZE 4.25 I.D.		WATER A	FTER	HRS:				<u> </u>			
		ቪ		99	. ]						%	  %	UN. COMP. STRENGTH (tsf)	F.		TERBE LIMITS	
Ħ.C	F		C.S.	길	-[	AJATTOJA, DE				SES	图	18.5 18.5 18.5 18.5 18.5 18.5 18.5 18.5	SE F	<u>}</u>		≽	O
DEPTH (ft)	Ş	SAMPLE IYPE	U.S.C.S.	GRAPHIC		MATERIAL DE	ESCRIPTION			BLOW COUNTS (N VALUE)	ŠE	욶류	28	58	LIQUID	EA	TIM
	5	Š		GR.	İ					05	RECOVERY (RQD)	MOISTURE CONTENT (%)	58	DRY UNIT WT. (pdf)	월크	PLASTICITY INDEX	PLASTIC LIMIT
0			$\vdash$		0.9	2½" ASPHALT, 7¾" CONCRE	ETE.									<u></u>	
				X	X	FILL: Brown SAND & GRAVE	L, trace silt, few	thin layers	(Moist	<del> </del>	·						
	5\$			燹	3 3.0	of black sandy silt with little cla	ay.		(MDIST	5-6-7-8 (13)							
		1	Г	o.	3.0	Loose to medium dense brown	n SAND & GRA	VEL, trace	(Moist	3-5-4-4							
 5	SS			0	₫	silt.			(IVIOISI,	(9)							
	22	ĺ		ø						4-2-2-3							
	SS			٥. (						(4)							
_	SS	/	SP.		9					2-2-1-2						.	Į
_ ]	33	(	GP-	8						(3)						.	
10	SS	Ì		0						2-2-4-6		5.7					
				) )	( <u> </u> :					(6)		5.1					
	SS			Ø						4-5-6-8							
				o.	13.2					(11)							
. 4	ss		ML.	Щ	14.0	Medium dense brown SILT, litt			(Moist)	,				ĺ			
15						Medium dense brown fine to m silt.	<del></del>		(Moist)	(13)							
	SS		SP				GRAINE	§O		8-10-11-14 (21)	.	ł					
			ML	Ш	17.0	Medium dense brown SILT, litt	tle sand frace cla	av								1	
• 🚽	55		IVIL	Ш	18.0	Medium dense brown fine to m		•	(Moist)	4-6-7-10 (13)				.			.
` <u>"</u>	$\dashv$		SP			· .	•		(Moist)	10-13-15-	i					•	- 1
20	SS				21.0	20': 2-inch SILT layer.				20 (28)		8.3					.
1				П	21.0	Medium dense brown SILTY F	NE SAND few	ell orc	(Moist)	10-11-10-					;		
1	SS					interlayers.	Y SAND		(MOISI)	10 (21)	- 1			. ]		l	1
1			SM			3101	1 SHAD			4-6-7-9	1					İ	
25	SS									(13)							
	SS				ュ				/\Aza+\	5-6-7-9							
]	33			11:	26.5 <del>▽</del>	Medium dense brown SILT, littl	le sand		(Wet)	(13)		ļ	Ì				ŀ
. ]	SS		ML	$\  \ $		modelin delice erem elett, ma	o cara.		(Moist)	7-12-11-14	- 1		İ			ĺ	
				Щ	29.0		<del></del>			(23)			ļ				l
30	ss		SM			Medium dense brown FINE SA	-	A. 10	(Wet)	9-11-13-14		1	ŀ				İ
1		Y	M	łł.	310		SILTY S			(24)							
4	ss					interlayers, stratified.	few same	thin silt	(Wet)	7-8-10-11							
4			зм			•		•		(18)							
-	ss									4-8-9-11						ł	
35	<u>.</u> . İ			1.1:		·				(17)	1	- 1		- 1	- 1	1	1



a di .,,

Solar Testing Laboratories, Inc. 1125 Valley Belt Road Brooklyn Heights, Ohio 44131 Telephone: 216-741-7007 Fax: 216-741-7011

### BORING NUMBER B-8 PAGE 1 OF 2

			<u> </u>	o i togionai c	Sewer District	PROJECT NAME	= <u>vval</u>	vorth Run in	itercep	tor Re	alignm	ent (V	/RIR) I	roject	
PROJE	CT NUM	BER	<u> </u>	\09570x10		PROJECT LOCA	ATION ,	W 11th, Ab	bey, V	/ 14th	Streets	s, Clev	eland,	Ohio	
DATE	STARTE	<u>1</u>	2/1/	/09	COMPLETED _12/2/09	GROUND ELEV	ATION _								
					esting Laboratories, Inc.										
DRILLI	NG METH	dOb	Н	ollow Stem	Auger	GROUND WATE	R LEVE	LS:							
LOGGI	ED BY <u>F</u>	R. Sp	ella	су	DRILLER J. Deranek	abla water 0	N ENC	DUNTER 2	6.0 ft						
NOTES	3					WATER O	N COM	PLETION _4	14.0 ft						
HOLE	SIZE				AUGER SIZE 4.25 I.D.	WATER A	FTER _	HRS:							
	Щ		၂ ဗ						%	⊋	st)	⊢	ΑТ	TERBE	
DEPTH (ft)	SAMPLE TYPE	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPT	ΓΙΟΝ		BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	9.1	γ	
0	SAMI	ם	GRA					mos	REC	Ø N N N N	STRE	DRY	LIQUID	PLAST IND	PLASTIC LIMIT
				0.9	2½" ASPHALT, 7¾" CONCRETE.										
	ss		$\overset{\otimes}{\otimes}$	3.0	FILL: Brown SAND & GRAVEL, trace of black sandy silt with little clay.	silt, few thin layers	(Moist)	5-6-7-8 (13)				:			
	ss		0		Loose to medium dense brown SAND silt.	& GRAVEL, trace	(Moist)	3-5-4-4 (9)							
	SS		0 (					4-2-2-3 (4)							
- +	ss	SP- GP	)	d				2-2-1-2 (3)							
10	ss		o (					2-2-4-6 (6)		5.7					
	ss		) Ø					4-5-6-8							
- +	ss	ML	° Ш	13.2 14.0	Medium dense brown SILT, little sand,		(Moist)	(11) 3-5-8-13							
15	ss	SP			Medium dense brown fine to medium S silt.	SAND, trace gravel,	(Moist)	(13) 8-10-11-14							
. ]	33			17.0				(21)							
.	ss	ML.	Щ	18.0	Medium dense brown SILT, little sand,  Medium dense brown fine to medium S			4-6-7-10 (13)				i			
20	ss	SP		21.0	20': 2-inch SILT layer.		(Moist)	10-13-15- 20 (28)		8.3					
• +	ss		I	21.0	Medium dense brown SILTY FINE SAI interlayers.	ND, few silt	(Moist)	10-11-10- 10 (21)							
	ss	SM						4-6-7-9 (13)							
25	ss			26.5 <del>V</del>			(Wet)	5-6-7-9 (13)							
. +	ss	ML			Medium dense brown SILT, little sand.		(Moist)	7-12-11-14 (23)							
30	ss	SM		29.0	Medium dense brown FINE SAND, little	e silt.	(Wet)	9-11-13-14							
-	 ss			31.0	Medium dense brown SILTY FINE SAI interlayers, stratified.	ND, few thin silt	(Wet)	7-8-10-11							
. +		SM						(18) 4-8-9-11 (17)							



#### **BORING NUMBER B-8**

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CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10 PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

L	<b></b> .			<b>,</b>					<b>4.</b>				
		<u>7</u> ਜ		ဗ္ဂ			%		. (g	F.		TERBE	
DEPTH (#)		SAMPLE IYPE	U.S.C.S.	GRAPHIC LOG	MATERIAL PROPERTION	BLOW COUNTS (N VALUE)	RECOVERY (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT (pcf)			
声	3	<u> </u>	U.S.	APH	MATERIAL DESCRIPTION	1400 ×	8£	SIS	ENG C	Y Cod	LINGT	SE	PLASTIC LIMIT
35	3	₹ S		8		٦	Ä.	≱ც	STR	R	2-	PLASTICITY INDEX	7
	ss		SM	1	36.0 (Wel	5-8-13-15					,		
	33				Medium dense brown fine to medium SAND, trace silt, few silt layers. (Wel	(21)							
	ss		SP		Heaving Śand,	5-7-9-8 (16)		18.8					
40	ss				41.0	4-9-6-7 (15)							
	ss				Madium dance brown EINE CAND little cit	9-12-11-16							
	SS				SILTY SAND	4-5-6-4							
45		(	SM		2(2)   3(10)	(11) 4-5-6-4							
	SS				and the second s	(11) 6-7-10-11							
• ·	SS				49.5	(17)							
50	SS				Dense gray SILT, little sand.	9-15-18-21 (33)		20.5			NP	NP	NP
 	SS		ML.		pressures (Wet	14-19-25- 28							
		070		41	53.0 Stiff gray CLAYEY SILT little sand. (Wet	(44)			/		2		-
55		ST	/ eL-							`(	24	4	20
- 			ML		silty clay								
	SS				590000000000000000000000000000000000000	5-6-8-10 (14)		19.3					
60	ss		γV		Stratified. (Wet	4-5-7-7 (12)							
-			CIA			(12)							
- -		ST	CL- ML								25	5	20
 65	SS				65.0 Stiff gray SILTY CLAY, little sand, laminated.	5-7-7-8 (14)							
	SS				Stiff gray SILTY CLAY, little sand, laminated. (Wet)	3-4-4-5 (8)		24.1					
	SS		CL		LEAN CLAY PRESSURES	5-6-6-8 (12)							
 70					PRESSURES	··-/							
- · ·		ST	_		71.0						30	10	20
	ss				<b>1</b>	9-10-14-16 (24)		21.1					
<b>-</b> -	ss		ML		CHECKE THE	10-14-16- 17		20.2					
75				Ш	75.0 CL-ML	(30)						Ì	

Bottom of hole at 75.0 feet.



Fax: 216-741-7011

#### **BORING NUMBER B-8**

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CLIENT Northeast Ohio Regional Sewer District

PROJECT NAME Walworth Run Interceptor Realignment (WRIR) Project

PROJECT NUMBER A09570x10

PROJECT LOCATION W 11th, Abbey, W 14th Streets, Cleveland, Ohio

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ŀ	İ	<u> </u>	١.	9				%	ш8	(fg . ,	₹	AI	TERBE <u>LIMITS</u>	
DEPTH (ft)		SAMPLE TYPE	U.S.C.S.	GRAPHIC LOG		MATERIAL DESCRIPTION	BLOW COUNTS (N VALUE)	RECOVERY % (RQD)	MOISTURE CONTENT (%)	UN. COMP. STRENGTH (tsf)	DRY UNIT WT. (pcf)	으누	PLASTICITY INDEX	일
🛎		AMP	٦	₹			<u> </u>	S S	MOIS	Z N N	}  }	LIQUID	AST	PLASTIC LIMIT
35	<u> </u>	თ <del></del>	_	L			ļ	2	-0	ST	△		7	Ы
ļ	ss		SM			Medium dense brown fine to medium SAND, trace silt,	5-8-13-15 (21)							
<u> </u>	+	1				few slit layers. (Wet) Heaving Sand.	<b> </b>							
[ ]	SS		SP			reaving cand.	5-7-9-8 (16)		18.8					
40	ss						4-9-6-7 (15)							
<u> </u>	00	1	-		1	11.0  Medium dense brown FINE SAND, little silt. (Wet)	9-12-11-16							
[ ]	SS	-				(,	(23)							
45	ss					Ţ	4-5-6-4 (11)							
	ss		SM				4-5-6-4							
-							(11) 6-7-10-11							
-	SS						(17)							
50	ss				. [4	9.5  Dense gray SILT, little sand. (Wet)	9-15-18-21 (33)		20.5			ļ		ŀ
			ML			,	14-19-25-							
	SS				5	3.0	28 (44)							ļ
		ST				Stiff gray CLAYEY SILT, little sand. (Wet)								
55					İ								ŀ	
			ML	Ш										
	ss				Ì		5-6-8-10		19.3			Ì		
				 	5	9.0 Stiff gray SILTY CLAY, little sand, interlayers of SILT,	(14)				ŀ			
60	SS					stratified. (Wet)	4-5-7-7 (12)							
		ST	CL- ML		1									
			ML								:			
	ss					- 0	5-7-7-8 (14)							
65					10:	5.0 Stiff gray SILTY CLAY, little sand, laminated. (Wet)	3-4-4-5							
	SS					(116.)	(8)		24.1					İ
	ss		CL				5-6-6-8 (12)						İ	
- 70		OT							Ì					
		ST			7	1.0								
	SS					Very stiff gray CLAYEY SILT, little sand. (Wet)	9-10-14-16 (24)		21.1					
			ML			}	10-14-16-				ľ			
 75	SS				75	5.0	17 (30)		20.2					
					•••	Pottom of halo at 75 0 fact	\- ·/							

Bottom of hole at 75.0 feet.

Red 3/23/2010

						)
	Classic Schedule Layout					
	Walworth Run Interceptor	Critical Activity		23MAR10 10:20	23MA	Run Date
Ite Revision Checked Approved	NEORSD Sheet 2 of 2	Early Bar WRIR Progress Bar		06NOV09 17AUG11		Start Date Finish Date
Complete Project			0	17AUG11		8030
Prepare O & M Manual			20	17AUG11	21JUL11	8020
Project As-Builts			20	17AUG11	21JUL11	8010
Project Closeout			20*	17AUG11	21JUL11	8000
						Closeout
Complete Construction◆			0	20JUL11		7040
	Resident Project Representation		195	20JUL11	120CT10	7030
	Contract Administration		215	20JUL11	14SEP10	7020
Contractor Issued Notice to Proceed	<b>◆</b> Contractor		0		14SEP10	7010
	Contract Administration		215*	20JUL11	14SEP10	7000
		300				Construction
Contractor Signs Contract	◆ Contractor		0	13SEP10		6110
EORSD Contract Preparation	NEORSD C		20	13SEP10	16AUG10	6100
Approval	<b>◆</b> NEORSD Board Approval		0	13AUG10		6090
NEORSD Recommendation to Board	NEORSD Recomm		ហ	13AUG10	09AUG10	6080
dation to NEORSD	<b>◆</b> Award Recommendation to NEORSD		0	06AUG10		6070
	Evaluate Bids		ഗ	06AUG10	02AUG10	6060
Bids	Contractors Submit Bids		0	30JUL10		6050
Bids	Contractors Prepare Bids		20	30JUL10	02JUL10	6040
	◆Pre-Bid Meeting		0	01JUL10		6030
riod	Second Advertisement Period		51	01JUL10	25JUN10	6020
	First Advertisement Period		51	24JUN10	18JUN10	6010
	Submit Final Documents for Bid		0	02JUN10		5060
	Address Final Comments		Oī	02JUN10	27MAY10	5050
	Final Design Review Meeting		0	26MAY10		5040
	NEORSD Review Final Design		Οī	26MAY10	19MAY10	5030
ward	Bid and Award		81*	13SEP10	19MAY10	5025
						Bidding
	<b>♦</b> Submit Final Design to NEORSD		0	18MAY10		5020
OCT NOV DEC JAN FEB MAR APR MAY JUN JUL AUG SEP	OCT NOV DEC JAN FEB MAR APR MAY JUN JUL AUG SEP OCT N	NOV DEC JAN FEB N	Dur OCT	Finish	Start	ID