



CLIENT ODOT  
 PROJECT CUY 271  
 SUBJECT Wall SW1  
 Soil Nail Wall  
 Facing Design

PROJECT NO. 1122-1001-90

BY: A. Porter Date: 8/15/2014  
 CHK BY: M. Crossley Date: 8/15/2014

$T_{max-s}$ (from geotech)=	10	k	Perm. Face Rebar Size =	#4
Vertical Nail Head Spacing =	3.5	ft	Perm. Face Rebar Spacing =	12 in.
Horizontal Nail Head Spacing =	3.5	ft	Perm. Facing Concrete $f'_c$ =	4,000 psi
Spacing Ratio =	1.00		Perm. Steel Yield Strength, $f_y$ =	60 ksi
# of Waler Bars (Horizontal) =	0		Perm. Facing Thickness =	8 in.
Waler Bar Size (Horizontal) =	#4		$N_H$ =	4
# of Waler Bars (Vertical) =	0		Stud Diameter =	0.5 in.
Waler Bar Size (Vertical) =	#4		Stud Length =	4.125 in.
Temp. Face WWF =	4x4-W2.9 x W2.9		Head Stud Head Thickness =	0.31
Temp. Facing Thickness =	4	in.	Stud Type =	A307
Temp. Facing Concrete $f'_c$ =	4,000	psi	Headed Stud Spacing =	5 in.
Temp. Yield Strength, $f_y$ =	60	ksi	Bearing Plate Length =	9 in.
			Bearing Plate Thickness =	0.75 in.
Temp. Rein. Ratio @ Midspan =	OK		Temp. Face Tensile Resistance =	OK
Temp. Rein. Ratio @ Nailhead =	OK		Perm. Face Tensile Resistance =	OK
Perm. Rein. Ratio =	OK		Temp. Punching Shear Resistance =	OK
Facing Head Stud Resistance =	OK		Perm. Punching Shear Resistance =	OK

Spreadsheet developed following FHWA-IF-03-017, Geotechnical Engineering Circular No.7, Soil Nail Walls 2003  
 Spreadsheet is only valid for equal waler bar spacing

Maximum design tensile force at the face:

$$T_0 = T_{max-s} [0.6 + 0.057 (S_{max} - 3)] = 10 [ 0.6 + 0.057 ( 3.5 - 3 ) ] = 6.3 \text{ k}$$

**Temporary Facing Reinforcement**

a) Reinforcement in vertical and horizontal direction in midspan (Table A.2)

$$a_{vm} = a_{hm} = 0.087 \text{ in}^2/\text{ft for } 4x4-W2.9 \times W2.9$$

b) Reinforcement in vertical and horizontal directions around soil nail head

$$a_{vm} = a_{nn} = a_{vm} + A_{vw}/S_H = 0.087 + ( 0.2 \times 0 ) / 3.5 = 0.09 \text{ in}^2/\text{ft}$$

c)  $C_F = 2.0$  (Table 5.1)

d)  $\rho_n = a_{vn}/0.5h = ( 0.09 / 12 ) / ( 0.5 \times 4 ) \times 100 = 0.36 \%$

e)  $\rho_m = a_{vm}/0.5h = ( 0.087 / 12 ) / ( 0.5 \times 4 ) \times 100 = 0.36 \%$

f)  $\rho_{min} = 0.24 \times (f'_c / f_y)^{0.5} = 0.24 \times 4,000^{0.5} / 60 = 0.25 \%$

g)  $\rho_{max} = 0.05 \times (f'_c / f_y) (90 / (90 + f_y)) = 0.05 \times ( 4,000 / 60 ) \times ( 90 / ( 90 + 60 ) ) = 2 \%$

h)  $\rho_{min} < \rho_m < \rho_{max} ?$   
 $0.25 < 0.36 < 2$  OK

i)  $\rho_{min} < \rho_n < \rho_{max} ?$   
 $0.25 < 0.36 < 2$  OK

j)  $\rho_{total} = \rho_n + \rho_m = 0.36 + 0.36 = 0.73 \%$



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**Permanent Facing Reinforcement**

a) Reinforcement area per unit length

$$a_{vn} = a_{vm} = 0.2 \text{ in}^2/\text{ft}$$

b) Total Reinforcement in Vertical Direction (no waler bars in perm. facing)

$$a_{vn} = a_{vm} = 0.2 \text{ in}^2/\text{ft}$$

c)  $C_F = 1.0$  (Table 5.1)

d)  $\rho_{min} = 0.24 \times (f'_c)^{0.5} / f_y = 0.24 \times 4,000^{0.5} / 60 = 0.25 \%$

e)  $\rho_{max} = 0.05 \times (f'_c / f_y) \times (90 / (90 + f_y)) = 0.05 \times (4,000 / 60) \times (90 / (90 + 60)) = 2 \%$

f)  $\rho_n = \rho_m = a_{vn} / 0.5h = (0.20 / 12) / (0.5 \times 8) \times 100 = 0.42 \%$

$$\begin{matrix} \rho_{min} < \rho_n < \rho_{max} & ? \\ 0.25 < 0.42 < 2 & \text{OK} \end{matrix}$$

g)  $\rho_{total} = 0.83 \%$

**Facing Tensile Flexural Resistance ( $R_{FF}$ ) - Temp. and Perm. Facing**

a) Facing flexural resistance ( $R_{FF}$ )

Temporary: From Table 6.4a,  $R_{FF} = 26 \text{ k}$   
 Permanent: From Table 6.4a,  $R_{FF} = 59 \text{ k}$

b) Verify:  $FS_{FF} T_0 < R_{FF}$

Temporary:	1.35	x	6.3	=	8.5	k <	26	k	OK
Permanent:	1.5	x	6.3	=	9.4	k <	59	k	OK

(Table 5.3)

**Facing Punching Shear Resistance ( $R_{FP}$ ) - Temp. and Perm. Facing**

a) Facing Punching resistance ( $R_{FP}$ )

Temporary: From Table 6.4b,  $R_{FP} = 40 \text{ k}$   
 Permanent: From Table 6.4c,  $R_{FP} = 39 \text{ k}$   $h_c = 5.00$

b) Verify:  $FS_{FP} T_0 < R_{FP}$

Temporary:	1.35	x	6.3	=	8.5	k <	40	k	OK
Permanent:	1.5	x	6.3	=	9.4	k <	39	k	OK

(Table 5.3)

**Facing Head Stud Resistance ( $R_{HT}$ ) - Permanent Facing**

$$A_{SH} = 0.20 \text{ in}^2$$

a) Maximum tensile resistance (headed-stud tensile failure) ( $R_{HT}$ )

$$R_{HT} = N_H A_{SH} f_y = 4 \times 0.20 \times 60 = 47.1 \text{ k}$$

b) Verify:  $FS_{HT} T_0 = 1.8 \times 6.3 = 11.3 \text{ k} < 47.1 \text{ k}$  OK  
 (Table 5.3)