TE-54-A

GENERAL INFORMATION

11 TEGEL 07 101

The project consists of a section of the Youngstown Expressway System, designated PAP-II-1.70, approximately 7.00 miles in length, located approximately 2.5 miles west of Youngstown, beginning approximately 2400 feet south of USP 224, approximately 0.5 miles east of Canfield, extending in a generally northerly direction and terminating approximately 1.3 miles north of SP 10, 0.75 mile east of SP 10. Also included in this report are the profiles of the associated ramps of the major interchanges at USP 224 and SP 10.

The proposed grades indicate the following:

Hainline – cuts, ranging between C and OR feet in depth, and fill embackments, ranging between C and Ω feet in height.

POP CO! Interchance

Panp A - cuts, ranging between C and G feet in depth, and fill embankments, ranging between Ω and Ω feet in height.

Panp F - cuts, ranging between O and II feet in depth, and fill embankments, ranging between O and 7 feet in height.

Pamp C - cuts, ranging between C and C feet in depth, and fill embankments, ranging between C and II feet in height.

Pamp D - cuts, ranging between C and 12 feet in depth, and fill embankments, ranging between C and D feet in depth.

Pamp Γ - cuts, ranging between Γ and $\overline{}$ feet in depth, and fill embankments, ranging between Γ and Γ feet in height.

SP 18 Interchange

Pamp A - cuts, ranging Letweer O and IO feet in depth, and fill embankments, ranging between O and I foot in height.

Pamp B - cuts, ranging between 0 and 20 feet in depth.

Pamp Γ - cuts, ranging between Ω and β feet in depth, and fill embankments, ranging between Γ and 16 feet in height.

Pamp N - fill embankment, ranging between 0 and 23 feet in height.

GEOLOGY ALL OPSELVATIONS OF THE FROJECT

The project is located on the glaciated gently rolling Allegheny Plateau, presently being dissected by several streams and creeks. Pedrock, composed of shale, sandstone, indurated clay and associated coal and underclay, of Pennsylvanian age, is overlain by moderately thick glacial-derived soils. Several localized areas of poor surface drainage were observed along the project.

EXELCEATION

Exploratory roadway borings were made by means of truck-mounted mechanical earth auger, hand auger (in areas of difficult access) and rotary type drilling between Cotober 31 and November 15, 1061. Also included in this report are the logs of drive sample-core borings made in conjunction with the structure foundation investigations.

IN VESTIGATION AL LISCICISCIES

Mainlin

Haterials occurring immediately below proposed grade consist predominantly of sandy silts and silt clays, in the A-La and A fa classifications, generally having moisture contents in the lower portion of the plastic range, as well as shale bedrock, occurring at grade and both ditchlines, between approximately stations 746+00 and 754+00.

Frest susceptible silts were found to occur within three feet of grade at the following stations:

•	1:55+00	536+00	597+00	680+
	1460+00	555+00	610400	684+
	11-35-45	560+00	636400	6014
	1479400	565+00	615100	700#
	7:331+00	575+00	650400	7134
	1:90+00	580400	650+50	7184
	1/01/+30	564+00	671+00	71,54
	811400	500400	677450	7864

Embankment foundation materials are largely comprised of sandy silts and silt clays, in the A-Ua and A-Ga classifications generally having moisture contents in the lower portion of the plastic range. In three areas, between approximately stations 797+00 to 799+00, at station 806+75 and at station 813+15, soft, wet, low strength organic soils and sediments occur at surface, ranging between 0 and 5 feet thick.

USR 224 Interchange (Ramps A, P, C D, and E)

Materials occurring immediately below grade and in the embankment foundation area consist of sandy silt, silt and silt clays, in the A-H and A-6a classifications, having moisture contents in the lower portion of the plastic range. Frost susceptible silts were encountered within three feet of grade at Ramp A; stations 13+45 and 17+80; Ramp B; stations 5+25, 8+77, 13+90 and 18+90; Ramp C; stations 10+13 15+07 and 20+07; Ramp D; stations 2+26, 5+05, and 18+55; and Ramp E; stations 7+85 and 11+40.

SP 10 Interchange (Pamps A, P, C, and D)

Embankment foundation materials and materials occurring immediately below proposed grade consist of sandy silts, silt clays and clays, in the A-Ha,A-Ga, and A-7-6 classifications, having moisture contents in the lower portion of the plastic range. Frost susceptible silts were found to occur within three feet of proposed grade at Pamp A; stations [14-60] and [3405] and Pamp P; station 16-15.

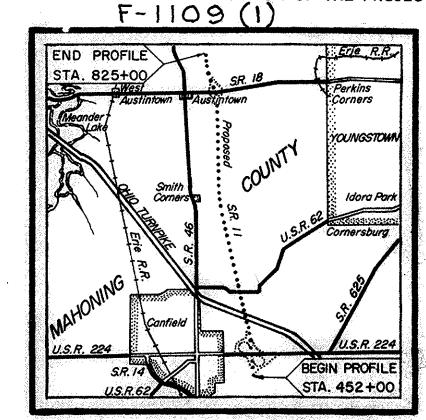
EG	END FOR PROJ										PLES 7						
	DESCRIPTION	H. R. B. CLASS	OHIO CLASS	% AGG.	% C. SAND	% F. SAND	% SILT	% CLAY	LIQUID LIMIT	PLASTICITY INDEX	WATER CONTENT	SAMPL TESTE					
e e	Gravel	A-1-a(0)	A-1-a	ů,	. 19	5	440-	0 -	ļiÞ	קין	15	t					
a a	Gravel and/or stone fragments with sand	A-1-b(0)	A-1-b	116	15	∴	10	9	Hib.	НР	ខា) î					
	Coarse and fine sand	any spin spin spin spin	А-За	50	19	35	†):	12	ЫÞ	ĦP	15	3					
1	Gravel and/or stone fragments with sand and silt	A-2-1:(0)	A-2-1)!e	10	15	1-7	12	ಜ	3	13	15					
	Sandy silt	A-14(5)	A-11a	15	8	18	371	25	23	5	13	252					
7	Silt	A-1;(8)	A-11b	3	3	દ	• 57	29	26) ;	ıc	27					
	Silt and clay	A-6(9)	A-Ga	10	5	10	35	1;0	30	12	17	151					
	Silty clay	A-6(II)	A-Fid	5	<u>}</u> :	દ	32	51	3 0	17	17	11					
7	Flastic clay without organic material unless otherwise noted	A-7-5 (20)	A-7-5	0	3	15	29	53	£ 0	<i>1</i> 13	\ ! 5	2					
i R	Clay	A-7-6(15)	A-7-6	: ;	1:	7	32	53	1:7	23	-55 25	15					
7	Sediments			VISU	AL CLASSIFICA	ATTOH:											
	Under clay			VISUAL CLASSIFICATION VISUAL CLASSIFICATION													
	Coal				VISUAL CLASSIFICATION												
	Weathered shale			VISUAL CLASSIFICATION													
	Weathered sandstone			VISUAL CLASSIFICATION													
	Indurated clay			VISUAL CLASSIFICATION													
	Shale .			VISUAL CLASSIFICATIO													
	Sandstone		÷	VISUAL CLASSIFICATION													
XI	Various other materials			Alan	AL CLASSIFICA	4T1C}:	•										
61 ²⁶ L	Sod and/or Topsoil_X'_Approximate d	epth.			·												
CXI	Perm material.	•	•					•									
) -	Auger boring - plan view.					•											
)	Drive sample and/or core boring - p	lan view.	·		•												
	Auger poring plotted to vertical so	ale only.															
	Drive sample and/or core poring plo vertical scale only.	tted to															
)	Number of blows for "Standard Penet X=number of blows for the first fi in Y=number of blows for the second fi	nches.															
	Water content nearly equal to or gr	eater than liqu	uid limit.														
) •1	Indicates a non-plastic material wi	th high water (content.														
_w	Free water.																
	Static water level.																
	Indicates broken rock interval.																

SOIL PROFILE MAHONING COUNTY MAH-II-8.70



OHIO STATE HIGHWAY TESTING LABORATORY COLUMBUS, OHIO

NOTE: INFORMATION SHOWN BY THIS SUBGRADE PRO-FILE WAS OBTAINED SOLELY FOR USE IN ESTABLISHING DESIGN CONTROLS FOR THE PROJECT. THE STATE OF OHIO DOES NOT GUARANTEE THE ACCURACY OF THIS DATA AND IT IS NOT TO BE CONSTRUED AS A PART OF THE PLANS GOVERNING CONSTRUCTION OF THE PROJECT.



LOCATION MAP

Recon-J.T.B. , F.L.R.-10/14/61

Auger - L.M.D. , A.J.P. , C.M.C. , F.S. - 10/31/61 to 11/9/61

Core - C.S.C., J.H.S., C.P.- 10/26/61 to 11/15/61

Drafting--- R.A.W., R.C.B.- 12/7/61

SUMMARY OF SOIL TEST DATA

		SUMMARY OF SCIL TEST DATA NOTE: NP shown in Liquid Limit and Plasticity Index columns indicates that the material is non-plastic. *Denotes sample taken at or near grade.	COLUMBUS, OHIO
CTATION & GEFORT	CEPTH % % % % % % SHTL	DEPTH # # # # # SHTL DEPTH # # # # SHTL DEPTH # # DEPTH # # # SHTL # DEPTH #	% % % % SHTL
STATION & OFFSET	L.L. P. I. FROM-TO AGG. C.S. F.S. SILT CLAY W.C. CLASS. 0.7-14.0 9 6 17 39 29 23 7 11 A-11a *	FROM-TO AGG. C.S. F.S. SILT CLAY W.C. CLASS. FROM-TO AGG. C.S. F.S. SILT CLAY W.C. CLASS. FROM-TO AGG	. C.S. F.S. SILT CLAY L.L. P. T. W.C. CLASS
460+00 551Lt	0.7-4.0 9 6 17 39 29 23 7 11 A-4a * 4.0-10.0 23 6 22 33 16 23 4 8 A 4a * 4		1 3 6 31 51 35 13 19 A-6a 1 10 11 19 41 28 11 15 A-6a
1000 1000 1000 1000	0.7-4.0 10 11 15 35 29 26 6 10 A-4a * 4.0-8.0 0 1 3 63 33 29 8 12 A-4b 8.0-12.0 18 10 6 35 31 30 11 13 A-6a	580+00 55147 0.0-4.0 8 8 12 39 33 26 11 13 A-6a x 4.0-9.0 11 8 17 37 27 22 5 15 A-4a x 671+00 Cl 0.6-5.5 17 8 18 32 25 25 25 13 A-4a x	1 9 15 34 28 25 7 16 A-Ha 2 8 16 29 25 21 6 13 A-Ha 4 11 18 32 15 NP NP 12 A-Ha
465+00 551Pt	0.7-3.0 0 6 13 144 37 27 11 13 A-6a * 3.0-5.0 27 10 27 24 12 NP NP 17 A-4a * 5.0-7.0 16 9 20 28 27 24 6 15 A-4a 7.0-8.0 16 10 28 18 28 22 4 15 A-4a	11.0-15.0 56 7 9 16 12 21 5 15 A-2-4 674+50 CL 0.6-5.0 4 1 15 37 43 28 11 9 A-6a- 773+00 65'Lt 0.3-3.0 12 5.0-10.5 0 1 20 42 37 26 6 10 A-4a 773+00 65'Lt 0.3-3.0 12	2 9 26 51 19 24 34 A-7-6 5 14 37 34 26 11 14 A-6a
\!70.00 E511+		50\frac{1}{2}+00 CL 0.0-5.0 11 7 13 31 38 30 11 20 A-6a ** 5.0-10.0 19 13 13 26 29 2\frac{1}{2} 9 1\frac{1}{2} A-6a ** 10.0-15.0 26 9 5 33 27 30 11 12 A-6a 5.0-11 0 29 8 19 30 1\frac{1}{2} NP NP 13 A-\frac{1}{2}a ** 500+00 CL 0.0-5.0 12 7 19 30 2\frac{1}{2} 6 LL A-\frac{1}{2}a ** 500+00 CL 0.0-5.0 12 7 19 30 2\frac{1}{2} 6 LL A-\frac{1}{2}a ** 500+00 CL 0.0-5.0 12 7 19 30 2\frac{1}{2} 6 LL A-\frac{1}{2}a ** 500+00 CL 0.0-5.0 12 7 19 30 2\frac{1}{2} 6 LL A-\frac{1}{2}a ** 500+50 551+1 0 29 8 19 30 1\frac{1}{2} NP NP NP 13 A-\frac{1}{2}a ** 500+00 CL 0.0-5.0 12 7 19 30 2\frac{1}{2} 6 LL A-\frac{1}{2}a ** 500+50 551+1 0 6-5.0 13 0 15 0 10 A-\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2} A-\frac{1}{2}a ** 500+50 551+1 0 6-5.0 13 0 15 0 10 A-\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2} A-\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2} A-\frac{1}{2}a ** 500+50 551+1 0 6-5.0 13 0 15 0 10 A-\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+50 551+1 0 6-5.0 13 0 10 A-\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 2\frac{1}{2}a ** 500+60 CL 0.0-5.0 12 7 19 30 12 12 12 12 12 12 12 12 12 12 12 12 12	0 1 140 33 NP NP 15 A-4a 0 0 1 144 55 36 15 23 A-6a 7 11 21 26 35 18 2 13 A-4a
1470+00 55'Lt	0.7-5.0 0 2 4 44 50 36 14 15 A-6a 5.0-9.0 9 6 12 38 35 26 11 14 A-6a * 9.0-12.0 7 6 39 22 26 21 5 21 A-4a	508+00 CL 0.0-5.0 12 7 18 29 34 24 6 11 A-4a * 680+50 55'Lt 0.6-5.0 13 8 15 37 27 25 8 10 A-4a *	3 14 13 141 19 20 6 11 A-14a
475+50 CL	0.7-3.0 11 5 12 36 36 30 11 14 A-6a 3.0-8.0 7 5 15 41 32 27 7 14 A-4a *	14.0-16.0 Black Coal W/Shale Fragments Visual	6 13 37 30 26 11 12 A-6a 1 9 12 27 21 21 6 13 A-4a 5 6 13 45 31 21 5 17 A-4a
	8.0-13.0 16 6 18 36 24 18 2 16 A-4a * 13.0-16.0 16 5 25 28 26 20 3 14 A-4a	590+20 65'Rt 2.0-5.0 3I 2 29 I6 22 22 6 I7 A-4a) 6 13 31 20 20 4 14 A-Ha) 9 20 36 25 NP NP 14 A-4a
1179+00 551Rt	0.6-4.0 28 17 20 22 13 20 3 10 A-2-14 4.0-7.0 0 7 17 45 31 26 11 18 A-6a 7.0-12.0 7 8 16 40 29 21 6 13 A-4a *	590+50 65°Lt 1.0-4.0 7 7 38 21 27 23 7 21 A-4a	3 1 6 36 54 47 25 30 A-7-6
	7.0-12.0 7 6 16 40 29 21 6 13 A-14a * 12.0-16.0 2 2 5 42 49 27 11 22 A-6a * 16.0-20.0 21 3 5 59 31 11P 11P 19 A-14b	6.0-8.0 5 10 15 113 27 20 0 12 A-11a	7 17 36 36 24 11 15 A-6a 7 6 13 35 29 21 4 13 A-4a 0 0 1 56 43 25 6 20 A-4a
484+00 551Lt	0.0-5.0 9 6 18 40 27 22 6 13 A-4a 5.0-7.0 15 15 36 17 17 NP NP 12 A-3a * 7.0-10.0 6 8 21 37 28 24 8 15 A-4a *	$4.0^{-9.0}$ 6 9 25 29 31 27 11 13 A-6a	2 17 22 37 12 NP NP 16 A-1a 2 7 19 11 21 19 11 13 A-1a
	10.0-15.0 5 8 15 37 35 22 6 14 A-4a 15.0-17.0 16 7 18 31 28 21 7 14 A-4a	5.0-9.0 10 11 21 36 22 NP NP 12 A-Na 11.0-9.0 8	1 3 6 28 59 37 15 18 A-6a 3 8 13 41 30 26 11 12 A-6a 5 7 13 37 33 27 11 13 A-6a
1490+00 551Rt	0.7-5.0 21 6 8 43 22 26 7 12 A-4a * 5.0-9.0 17 11 22 30 20 19 2 14 A-4a 9.0-14.0 9 9 19 35 28 22 5 16 A-4a	21:0=25:0 1	5 8 18 37 22 19 14 12 A-14a 7 5 16 55 17 NP NP 19 A-14b 7 9 19 32 23 19 3 13 A-14a
л18л1+30 СГ	0.7-5.0 16 5 19 34 26 25 6 14 A-4a * 5.0-10.0 15 10 20 32 23 22 5 10 A-4a	4.0-9.0 12 8 14 35 31 26 6 15 A-4a x 765+00 55 kt 0.7-4.0 41 3 11 26 19 32 12 16 A-6a 770+00 C	5 17 39 34 29 11 21 A-6a 7 13 31 27 24 7 10 A-4a
500+00 CL		6.0-12.0 22 6.0-12.0 22 6.0-12.0 22 6.0-12.0 22 7.0-9.0 21 9 19 32 19 19 3 11 A-4a	6 13 31 28 23 6 14 A-14a 6 14 38 25 21 6 13 A-14a 7 9 15 144 25 19 3 13 A-14a
50150	10.0-14.0 8 12 24 33 23 18 4 10 A-4a 1	2.5-4.0 28 10 16 26 20 25 7 13 A-4a *) 8 15 35 22 23 7 18 A-4a
504+50 CL	0.7-5.0 12 8 17 35 28 24 8 15 A-4a 5.0-10.0 6 7 17 39 31 24 11 16 A-6a 10.0-15.0 14 11 22 32 21 18 3 13 A-4a 15.0-20.0 12 7 23 35 23 19 6 12 A-4a	- 4	0 6 29 33 32 28 9 23 A-4a 7 10 14 42 27 28 11 13 A-6a 1 2 9 67 18 NP NP 17 A-4a 1 2 9 67 18 NP NP 17 A-4a
511+00 CL	0.7-5.0 6 3 10 57 24 31 9 19 A-46 *	615+00 CL 1.2-5.0 39 7 22 23 9 NP NP 11 A-2-14	9 20 23 140 33 17 16 A-6b 3 8 14 142 33 22 5 16 A-14a 3 10 19 37 26 22 5 114 A-14a 4 8 8 25 15 21 14 18 A-14a
	0.7-5.0 6 3 10 57 24 31 9 19 A-46 * 5.0-10.0 7 10 24 34 25 22 5 14 A-46 * 10.0-15.0 6 10 24 36 24 19 3 11 A-4a * 15.0-20.0 13 9 21 34 23 21 6 12 A-4a	14.0-17.0 12 9 36 13 30 NP NP 8 A-14 7.0-10.0 6 11 38 30 15 NP NP 19 A-14a 786+00 CL 0.3-3.0 15	
517+10 CL	0.7-5.0 36 10 18 20 16 23 14 8 A-14a 5.0-8.0 19 10 15 13 13 NP NP 9 A-2-14	620+00 55'Rt 0.0-2.0 9 9 19 39 24 24 6 12 A-4a 3.0-7.0 2 2.0-7.0 31 12 15 27 15 29 5 19 A-4a 727+60 50'Rt 0.6-5.0 17 4 11 38 30 25 11 11 A-6a * 7.0-10.0 22 7.0-12.0 10 10 30 27 23 NP NP 10 A-4a 5.0-9.0 15 5 10 11 26 25 11 13 A-6a	12 15 27 27 29 9 16 A-Ha * 3 3 4 19 51 35 11 19 A-6a * 2 31 26 8 13 NP NP 18 A-1-6 5 10 17 34 34 24 6 15 A-4a
519+80 CL	0.7-6.0 17 15 17 32 19 24 5 8 A-lia	700.00 SELLA A 2.0 S	16 9 35 30 30 11 11 A-6a 3 3 5 37 17 35 14 20 A-6a * 5 7 38 35 14 NP NP 21 A-14 46 5 6 14 33 32 24 7 12 A-148
524+70 65'lt 524+70 Cl	0.7-2.0 6L 8 13 13 5 NP NP 30 A-1-6	8.0-12.0 14 9 9 39 29 24 4 11 A-4a 738+00 55'Rt 0.6-2.0 6 6 7 46 35 35 11 19 A-6a 4 11.5-13.0 18	
524+70 651Pt	1.5-2.5 Brown Broken Stone Fragments Visual	630+00 55'Rt 0.0-5.0 10 8 18 48 16 25 7 10 A-4a	5 8 11 31 25 23 6 6 A-4a 3 5 32 50 38 17 17 A-6b A-1 3 6 9 36 23 23 4 12 A-4a 3 17 20 30 15 NP NP 15 A-4a 13 18 31 19 20 5 14 A-4a
BOHOO CF	0.0-5.0 29 11 16 28 16 22 5 14 A-4a 5.0-10.0 25 5 12 31 27 26 7 12 A-4a 10.0-17.0 7 7 17 11 28 NP NP 16 A-4a 17.0-20.0 Brown Sandy Silt W/Stone Fragments 14 Visual	10.0-10.0 6 7 25 42 20 NP NP 16 A-4a * 5.0-7.0 45 4 8 38 46 35 14 17 A-6a 12.0-17.0 18 10.0-12.0 0 2 3 57 38 37 11 30 A-6a 7.0-9.0 52 14 8 17 9 26 5 19 A-2-4	
536+00 CL		3.0-7.0 4 12 38 39 30 11 19 A-6a: 3.0-7.0 4 7 14 49 26 29 11 15 A-6a: 4.0-7.5 6	3 4 31 62 37 14 20 A-64 4 1 12 39 23 17 NP NP 20 A-4a
	0.0-5.0 7 8 17 43 25 24 3 14 A-4a 5.0-10.0 15 7 16 38 24 25 7 13 A-4a 10.0-14.0 8 5 17 38 32 25 5 13 A-4a * 14.0-19.0 11 1 20 43 25 23 7 12 A+4a *	3.0-7.0 14 7 114 149 26 29 11 15 A-6a * 745+00 55'Lt 0.6-5.0 7 14 6 34 149 31 11 16 A-6a 7.0-10.0 15 8 18 38 21 19 2 15 A-4a * 5.0-7.0 21 6 8 37 28 27 11 11 A-6a 797+00 CL 0.6-3.0 8 10.0-11.5 10 8 22 39 21 NP NP 16 A-4a 7.0-12.0 21 8 16 30 25 21 6 12 A-4a 3.0-4.0 12 11.5-15.0 5 10 12 140 33 24 6 16 A-4a 12.0-14.5 15 8 18 35 24 24 6 13 A-4a 3.0-4.0 12 14.5-20.0 10 5 7 58 20 NP NP 16 A-4a 799+00 80'Rt 0.6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2.0 (6-2	27 27 26 12 68 41 38 A-7 ¹ 6 7 14 38 -29 26 7 20 A-4a
541+00 CL		041+73 OL 0.6-2.0 0 1 9 51 39 34 14 24 A-6a	own Broken Stone Fragments Visual
	0.0-5.0 6 6 19 38 31 28 7 12 A-4a * 5.0-9.0 17 7 14 37 25 25 6 13 A-4a * 9.0-14.0 7 6 16 33 38 29 11 16 A-6a 14.0-18.0 12 10 20 36 22 22 5 10 A-4a	2.0-8.0 20 4 10 28 38 30 11 16 A-6a X 749+00 55'Rt 0.6-5.0 4 5 8 39 44 29 11 13 A-6a 8.0-13.0 8 6 15 140 31 23 7 13 A-4a 5.0-7.0 6 8 16 40 30 23 6 11 A-4a 803+00 45'Lt 0.6-5.0 25 13.0-14.0 22 5 16 41 16 19 3 16 A-4a 7.0-12.0 Brown Sandy Silt W/Shale Fragments 8 Visual 5.0-10.0 21 14.0-16.0 8 7 17 33 35 21 5 14 A-4a 12.0-14.0 Brown Broken Shale 9 Visual 10.0-15.0 11	3 6 10 27 34 29 11 14 A-6a * 1 10 21 11 34 NP NP 14 A-4a * 7 10 41 31 23 6 13 A-4a 3 8 14 /33 36 30 12 16 A-6a
543+50 CL	0.0-4.0 0 3 17 48 32 29 5 27 A-4a	645+55 55'Rt 0.6-5.0 17 5 14 36 28 26 7 9 A-4a * 753+27 36'Rt 0.4-5.0 6 7 11 32 44 30 11 17 A-6a 15.0-18.0 9 5.0-8.0 3 6 16 48 27 20 3 15 A-4a * 5.0-10.0 14 3 5 28 50 34 13 17 A-6a 806+73 CL 0.0-3.0 BI 8.0-12.0 7 7 12 33 41 24 11 15 A-6a 10.0-13.0 6 4 6 30 54 35 14 17 A-6a 30-31 0 30	8 14 (33 36 30 12 16 A-6a Visual
550+00 CL	0.0-5.0 8 5 12 37 38 29 11 15 A-6a * 5.0-10.0 L1 8 17 34 30 25 6 14 A-4a 10.0-12.0 11 7 14 34 34 28 11 14 A-6a 1	8.0-12.0 / / 12 33 41 24 11 15 A-6a 10.0-13.0 6 4 6 30 54 35 14 17 A-6a 3.0-4.0 28 13.0-14.0 Brownish-Gray Silty Clay W/Shale Fragments 12 Visual 306+75 601 t 0.0-2.0 Gr	ay to Black Sediments 154 Visual
555+00 CL	0.0-5.0 10 5 12 34 39 33 11 15 A-6a * 5.0-10.0 28 7 13 28 24 23 5 13 A-4a * 10.0-14.0 20 8 11 39 22 25 5 12 A-4a 14.0-18.0 20 8 14 35 23 23 5 12 A-4a	5.0-7.0 29 6 10 30 25 27 7 14 A-4a 6.0-11.0 5 5 8 32 50 37 16 15 A-6b	ay to Black Sediments 100 Visual
	d a me	12.0-15.0 18 6 13 3H 29 25 11 13 A-6a 3.5-7.0 15	10 9 33 148 34 14 20 A-6a 5 5 15 44 21 22 3 15 A-4a 5 10 16 36 32 22 5 12 A-4a 6 11 33 25 23 4 14 A-4a
560+00 · CL	0.0-5.0 23 14 8 26 39 34 12 22 A-6a 5.0-10.0 9 8 15 140 28 23 5 16 A-14a * 10.0-14.0 10 9 16 39 26 27 8 11 A-14a * 114.0-18.0 7 10 19 36 28 22 6 12 A-14a	10.0-12.0 10 9 10 33 28 21 4 13 A-4a 6.0-11.0 5 7 15 37 36 25 11 13 A-6a	6 11 33 25 23 4 14 A-4a 2 12 36 34 27 11 25 A-6a
565+00 55†Rt	0.0-4.0 7 11 '8 31 50 37 16 to Men	658+00 55'Lt 0.6-3.0 14 4 15 42 25 22 4 11 A-4a 766+80 CL 0.4-2.0 0 22 14 34 30 28 7 24 A-4a 3.0-6.0 27 5 9 35 24 28 11 13 A-6a 2.0-4.0 7 2 7 33 51 35 13 18 A-6a 813+15 CL 0.0-5.0 RI 6.0-10.5 28 3 3 41 25 27 4 7 A-4a 4.0 4.0-8.0 22 5 10 32 31 26 11 15 A-6a 5.0-9.0 18	ack Sediments 157 Visual 6 14 27 35 26 11 21 A-6a
•	11.0-7.0 3 14 7 33 53 140 17 17 A-6b * 7.0-10.0 8 8 10 144 30 24 5 14 A-14a * 10.0-13.0 7 8 17 140 28 26 8 14 A-14a 13.0-16.0 9 9 14 37 31 21 14 11 A-14a	8.0-10.0 6 8 15 37 34 23 4 16 A-4a 663+00 55'Rt 0.6-3.0 0 0 1 41 58 53 29 25 A-7-6 10.0-14.0 11 7 13 34 35 23 6 12 A-4a 813+15 65'Rt 0.0-4.5 81	ack Sediments 105 Visual
570+00 551Lt		3.0-6.0 3 . 3 10 53 31 29 11 25 A-6a 14.0-17.0 0 1 1 52 46 30 9 23 A-4b 60-8.0 7 7 20 38 28 24 7 13 A-4a 17.0-22.0 13 10 16 35 26 21 6 12 A-4a 818+00 551Lt 0.3-2.0 0 18.0-14.0 27 5 16 32 20 21 5 14 A-4a 7.0-11.0 17.0-22.0 13 10 16 35 26 21 6 12 A-4a 818+00 551Lt 0.3-2.0 0 18.0-14.0 27 5 16 32 20 21 5 14 A-4a 7.0-11.0	1 6 32 61 43 18 24 A-7-6 5 4 6 27 48 34 13 16 A-6a * 7 3 6 34 50 31 11 17 A-6a *
	0.0-5.0 14 7 12 32 35 29 11 12 A-6a 5.0-10.0 17 10 15 35 23 17 5 11 A-9a		

COLUMBUS. OHIO

J L.L. P. T.

A-11a A-11a A-11a A-11a A-2-11

10 A-2-14
11 A-14a
12 A-14a
9 A-14a
13 A-14a
10 A-14a
10 A-14a

34 A-4a 18 A-4a 20 A-4b 15 Visual

A-11a A-11a A-3a A-11a A-11a A-11a A-11a

A-110 A-11a A-14a

21 A-6b
18 A-6a
24 A-7-6
20 A-4a
14 A-4a
14 A-4a

NP NP NP NP

38 19 NP

33 23 26

33 <u>+ 33</u> 등 전 15 전 2

293332373749

AGG. C.S. F.S. SILT CLAY

DRIVE SAMPLE SOIL TEST DATA

0 6 14 47 3 5 8 22 42 2 0 2 20 52 2 Gray Sandstone Fragments

3 13 12

I STATION & OFFSET

505+61

777+15 65!Rt

5.0-6.0 10.0-11.0 12.5-13.5 15.0-16.0 17.5-18.5

5.0-6.0 7.5-8.5 10.0-11.0 12.5-13.5 15.0-16.0 17.5-18.5 20.0-21.0

2.5-3.5 5.0-6.0 7.5-8.5 10.0-11.0 12.5-13.5 15.0-16.0 17.5-18.5 20.0-21.0 25.0-26.0

2.5-3.5 5.0-6.0 7.5-8.5

10.0-11.0

2.5-3.5 5.6-6.0 7.5-8.5 10.0-11.0 12.5-13.5 15.0-16.0

2.5-3.5 5.0-6.0 7.5-8.5 10.0-11.0 12.5-13.5 15.0-16.0 17.5-18.5 20.0-21.0 25.0-26.0

NOTE: NP shown in Liquid Limit and Placticity SOIL TEST DATA (Cont'd)

																NOTE:	NP sh	own in	Liquid	Limit a	SUMMARY UF S and Plasticity In *Denotes sample	ult IESI UAIA idex columns in	(Contrd) dicates tha	it the materia	al is i	non∸plas	tic.				•	
STATIC	I & OFFSET		%	%	ø	o	<u>«</u> ا	l. f.l	ø,	SHTL.	. CTATIO	k & OFFSET	(EPTh	ø	%	%	%	%		%	SHTL.	taken at or ne	ar grade.	(ÆPTE	æ	æ.	ø	x				••
822+0	0 551Pt	FR01570 0.3-1.5	AGG. 3	C.S. F	î.S. 6	SILT (1 32 :	.AY	l3 1 5	W.C	. CLASS. A-Ga *	, SIRTIU	IN (P. CIFFOLI	FROI'-TO	AGG.	C. S.			(1.AY		P.15 W-C	. CLASS.	1 STATIO	& OFFSET	FROM: TO	AGG.	C.S.	F.S. S	e ILT (L	AY L.L.	P.1.	SHT W.C. CLASS	
		1.5-6.0 6.0-12.0	7 14	5	15 S	39 :	7 0 9 2	25 11	17	A-6a	5+85	33'Lt	0.0-5.0	411	<u> 13</u>	amp "D"		·						·	••	-	"B" (Cont		•••	· '	nivi Gunoc	·•
÷ 825+0	U CL	0.2-2.5	0	2	3	17 7		7 25	. 28		V-00	00 21	0.0-5.0 5.0-10.0 10.0-12.5	9 57	5 7	17 7	33 53 15	16	32 NP 25	11 10 11P 11	6 A-6a 7 A-11b * 0A-2-11	8+47	131Lt	4.0-8.0 0.3-4.0	¥ 6	3 7	6 8	26 30	61 41 49 33	19 13	16 A-7-6	j
	•	2.5-5.0 5.0-8.0 8.0-11.0	2 38	3 16	3 7 19	55 3	20 34 - 2 30 - 3	8 12 2 5	18 16 14	A-6a A-1:b A-2-1:	9+25	261Lt	0.3-14.0	8	7	13	110		30	11 11		12+35	7'Lt	8.0-12.5	22	6	11.0	_1 .	24 20	,	13 A-11a	`
			*		_	4 INTERC		·• •	•-1	6 1 <u>6</u> 1 − 24			4.0-8.0 8.0-12.0 12.0-16.0	18 8 26	15 8	23 20 17	24 37	20 27	51 55	3 16 5 15	3 A-4a * 5 A-4a	12100		0.3-4.0 4.0-8.0 8.0-10.5	8	4 3 5	6	27	53 38 56 34 31 32	. (4	121 A-6a 16 A-6a	*
				:	Ra	amp "A"	1 4 3 E				13+53	16'Lt	0.0-5.0	20 8	8	17	29 37		21 26	5 H	A-Na A-Na	سرد کم		10.5-15.0	Ŏ	2	14	28	56 38	16	15 A-6a 21 A-6b	· • •
2+00	7'Lt	0.0-5.0 5.0-9.0	8 6	7 5	15 10	36 3 50 2)4 2 9 2	8 II 8 8	13 11	A-6a A-14b		·	5.0-7.0 7.0-12.0	0	0	5	72 85	22 14	NP NP	NP 21	A-110 ★	16+45	16'Lt	0.0-2.0 2.0-6.0 6.0-7.0	110 12	2 6	12 1	15 %	24 33 25 27		27 A-6a 10 A-14a	*
6+03	PL.	0.0-5.0	1,71	2	15	10 2	9 2	6 11	10	A-fa *		•	12.0-16.0 16.0-18.0 18.0-20.0	0 0	0 2 0	2 10 17	56 65 40	142 23 20	25 MP MP	5 23 NP 22 NP 13	A-14b *** 2 - A-14b		•	7.0-8.5 8.5-11.0	114 57	ა 6 5	୍ଷ 2	29 1	17. S7. 13. 58 18. 37.		.20 A-6a 13 A-6a 17 A-2-4	
10+03	PL	5.0-10.0 0.7-5.0	3 8	·6		45 3 38 3	3 2 6 2		13	A-6a A-6a * °	18+55	2 3'Lt	0.0-5.0	10	7.	16		32				50+00	71Lt	0.3-1.5	0	.8	18 3		7	22	23 A-7-6	,
13+45	8'Lt	5.0-8.0	35	6 :	20	18 2	1 2	3 7	17	A-1ta	23+53	22'Lt	5.0-11.0 0.0-5.0	14 oʻ	9				NP	NP . D	A-1'a *			1.5-5.0 5.0-8.0 8.0-12.0	5)† 33 1,†	12 10 8	10 10 18	9 7 9	99 45 25 28 90 28 21 18	5	13 A-4a 11 A-14a 9 A-14a	
	€\+` L , L	0.0-5.0 5.0-8.0	25 7	8 8 2	13 21	27. 2 35 2	7 2! 9 2:	5 5 5 5	16	A-1 a * ' A-1 a	y o		5.0-10.0	9	7	13 16	¥0 36	35 3/1	29 28	11 14 11 18	A-6a A-6a **		•		-	Ramp			jo		8 A-4a	
17+80	231Lt	0.0-5.0 5.0-10.0	3 15	5 10	9 6	50 3 35 2	3 21 4 21	9 5 8	18 13	A-lib * A-lia *	1+03	35!Pt	Ó O.R.O	~	Ra	ımp "F"	-				4	2+07	5'Lt	0.4-5.0 5.0-10.0	5 19	2	2 2	8 6	3 42	18	18 A-7-6	*
					Pa	imp "P"				• ,		Opr NC	0.8-6.0 6.0-8.0 8.0-10.0	15 33	18 11	16 31 14	51 23 24		22 NP - 1 20	2 21 19 16	A-11b A-11a A-11a	8+93	151Lt	0.2-4.0	0	i i			9 24 2 59	6 32	13 A-4a 29 A-7-6	1
2+02	<u>RL</u>	0.4-4.0 4.0-7.0	3 12	5 1	8 9	35 5. 34 76	0 20 7 20	3 11	18 17	A-6a A-11a	14.07	**** A	10.0-14.0	6	10	20	38		21	3 16	A-Ha A-Ha	1,11+0,11	1011+	14.0-10.0 0.3-3.0	20	2	2 3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2 58 0 37	iπ	18 A-6a	
		7.0-10.0 10.0-12.0 12.0-14.0	15 35 12	9 2	30 16	33 23 21 1	3 10 1 MF	9 NP	12	A-lia A-lia	4+97	71Lt	0.0-2.0 2.0-5.0 5.0-8.0	0 5	2 2		52 148 23	38 2	%P 1	P 12 11 17	A-110 A-6a ***			3,0-8.0 8.0-13.0	0 18	5 5 5	10 2 7 2 13 3	6 6	2 42 2 41	17 18	28 A-7-6 18 A-7-6	
5+25	13°Lt	0.0-3.0	11	9 I		32 36 32 36	9 MF 3 33		13 16	A-1ia A-6a *>			5.0-8.0 8.0-11.0 11.0-14.0	22 12	17 7	38	13 35	10	IP 1 IP 1 25	IP 18 14 14 14 14	A-4a A-3a A-6a	•		13.0-18.0 18.0-22.5 22.5-29.0	2	5 3	12 4	0 4 5 5	23		15 A-6a 15 A-6a 25 A-6a	
		3.0-7.0 7.0-10.0	13 11		6 3	29 20 24 20) 21	14	13 16	A-14a * A-14a	7+85	8ºLt	0.0-5.0 5.0-8.0	46	Ħ .	15	19	16 2	27	7 13	V-5-11	17+05	IO'Lt	0.0-5.0	- 41 - 6	3	11 2 2 3		6 19 	3	8 A-11a	•
8+77	7!Lt	0.0-4.0 4.0-8.0	16 31	9	1ļ ;	38 20 22 16	3 23 5 21	3 14	10	A-34a * * A-14a * *	•		8.0-8.0 8.0-12.0 12.0-16.0	0 0	3 2 7	12 7 10 :	12 66	25	IP I	20 25 P 20	A-110 **	•	.,	5.0-11.0 11.0-13.0	1Ĭ 28	5 17	9 3	1 1	4 30 4 37 9 26	12 15 10	16 A-6a 19 A-6a 18 A-14a	:
•		8.0-12.0 12.0-15.0	9 7	9 3		22 16 20 33 20 33	1 20) 2	12	A-1:a A-1:a	1-1-40	151Lt	1.0-8.0 0.0-11.0	5	6	124	1 1 14	31 2	25 I 27	1 20 6 12	A-6a A-11a			13.0-18.0 18.0-22.0 22.0-28.0	13 9	7 4	15 3 8 7 11 3	3 30	5 23	5]	15 A-11a 16 A-6a	
13+90	12"Lt	0.0-4.0 4.0-7.5	24 13	12 2 12 2	2 3	22 20 32 23) 26 3 26	7	15	A-Ha *			4.0-8.0 8.0-11.0 11.0-13.0	5 12	7 13	33 3	31	N N		7 13 P 13	A-1 a * A-1 a *	•.		22.0 20.0	F. 1	Ramp *		' a	3 21	. 	II A-la	
18+98	15'Lt	0.0-14.0	8	2 1	2 1	40 39	3 29		17	A-Ha A-fia			13.0-17.0	30	6		35 28	23 N 21 2	17 19 12	P 11 5 13	A-Ha A-Ha	9+740	53'Lt	0.3-3.0 3.0-7.0	7	3		2 14	37	114	30 A-6a	,# .
		4.0-8.0 8.0-11.0 11.0-15.0	23 6	6 2	5 0 8	28 23 39 29 50 28	3 28) 14	13 13	A-11a A-11a *	29+60#	5'Lt	0.0-5.0 5.0-10.0	13 13	98	23 (17 3 25 2	2	1 ~ 16 6 14	A-Na			7.0-11.0 11.0-13.5	8	6 9	9 14 15 27	33	20 26 27 28		15 A-6a 13 A-6a 15 A-6a	
23+70	PL	0.11-11.0	5	4 1		ou 26 40 38			12 13	A-146 * A-6a *		,	10.0-15.0 15.0-18.0	6 12	8 8		141 29	22 27	8 9	3 13 5 10	A-Ha A-Ha			13.5-16.0 16.0-19.5	0	Ş	10 62 2 115	26 52	NP 30	NP	19 A-46 24 A-6a	
		4.0-6.0 6.0-7.5	¹ 15 2	6 H	0 2	26 15 45 37	22 29	5 11	5 7	A-lla * A-6a					·	NTERCHA	ANGE_					,		19.5-24.0 24.0-28.0	. 19	8	18 31 16 14	30 24	19 19	5 3	13 A-4a 12 A-4a	
	•			· .	Ramp	o_"C"			, \$		2+25	12'Et	0.3-3.0	,	<u>Ram</u> •	<u>р "А"</u> У	(iá	160	· · ·		4	13+17.	filt :	0.3-3.0 3.0-10.0	38 2	13	10 16 6 27	23 63	29 36	8 12	12 A-4a × 17 A-6a	V.
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