
**FINAL REPORT
GEOTECHNICAL EXPLORATION REPORT
SUM-77-24.12 GHENT ROAD
SUMMIT COUNTY, OHIO
PID: 111404**

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NEAS PROJECT 20-0071

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SUM-77-24.12

Summit County, Ohio

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1. INTRODUCTION

1.1. General

National Engineering & Architectural Services, Inc. (NEAS) presents our Geotechnical Exploration Report for the interstate improvement project (SUM-77-24.12, PID 111404) for Interstate Route 77 (IR-77) and associated ramps within the City of Akron, Summit County, Ohio. The overall project objective is to reduce the congestion along the IR-77 corridor, as well as improve both safety and the infrastructure condition within the project limits. The improvements proposed to accomplish this objective include: 1) the widening of the IR-77 northbound (NB) and southbound (SB) freeway segments within the project limits; 2) the construction/reconstruction of 10 associated ramps (Ramp A, Ramp B, Ramp C, Ramp D, Ramp L, Ramp M, Ramp N, Ramp P, Ramp R, and Ramp S); 3) the construction of a noise wall along the southeastern side of Ramp L; 4) the construction of fifteen new high mast light poles; and, 5) the reconstruction/refurbishment of three existing culverts. This report presents a summary of the project encountered surficial and subsurface conditions and our recommendations for subgrade stabilization, embankment construction, pavement design parameters and noise wall foundation design. The roadway analysis performed as part of this report has been performed in accordance with ODOT's July 2020 revision of *Geotechnical Bulletin 1* (GB1) (ODOT [1], 2020) and *Pavement Design Manual* (PDM) (ODOT, 2020). The noise wall foundation analysis performed as part of this report has been performed in accordance with ODOT's January 2021 revision of the *ODOT's 2020 LRFD Bridge Design Manual* (BDM) (ODOT, 2021).

The exploration was conducted in general accordance with NEAS's proposal to GPD Group (GPD), dated June 2, 2020 and with the provisions of the July 2020 (ODOT, 2020) revisions of ODOT's *Specifications for Geotechnical Explorations* (SGE).

The scope of work performed by NEAS as part of the referenced project included: a review of published geotechnical information; performing 118 total test borings; laboratory testing of soil samples in accordance with the SGE; performing geotechnical engineering analysis to assess subgrade and roadway embankment stabilization requirements, recommended pavement design parameters as well as noise wall drilled shaft foundations; and development of this summary report.

2. GEOLOGY AND OBSERVATIONS OF THE PROJECT

2.1. Geology and Physiography

The majority of the project site is located within the Killbuck-Glaciated Pittsburgh Plateau physiographic region, part of the Glaciated Allegheny (Southern New York) Plateaus, with portions located near lake basin/deposits outside of the Huron-Erie Lake Plains. A small segment (less than 1000 ft) of the southern portion of project site is located within the Akron-Canton Interlobate Plateau which is also a part of the Glaciated Allegheny Plateaus. The Killbuck-Glaciated Pittsburgh Plateau region is characterized by ridges and flat uplands of moderate relief generally above 1,200 ft, covered with thin drift and dissected by steep valleys. Valley segments alternate between broad drift-filled and narrow rock-walled reaches. Elevations of the region ranges from 600 to 1,505 ft above mean sea level (amsl), with moderate relief (200 ft). The geology within this region is described as thin to thick Wisconsinan-age clay to loam till over Mississippian- and Pennsylvanian-age shales, sandstones, conglomerates and coals. The lake basin/deposits are characterized as extremely flat plains often comprised of sandy beach ridges and dunes formed along the shore of ancient lakes. The Akron-Canton Interlobate Plateau is characterized as a moderate relief,

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hummocky area between two converging glacial lobes dominated by kames, kame terraces, eskers, kettles, kettle lakes, and bogs/fens. Soils in this region are characteristically sandy Wisconsinan-age clay to loam till over Mississippian- and Pennsylvanian-age shales, sandstones, conglomerates and coals (ODGS, 1998).

The geology in the southern portion of the project site, south of about Shade Road (Rd), is mapped as an average of 100 ft of ice-contact deposits atop up to 320 ft of complexly interbedded deposits of clay, silt, sand, gravel and till all over Devonian-age Ohio Shale bedrock. Areas of Holocene-age organic deposits are also mapped throughout the region. The ice-contact deposits are generally described as highly variable deposits of poorly sorted, Wisconsinan-age gravel and sand with inclusions of silt, clay and till lenses deposited directly from stagnant ice as kame or esker landforms. The northern portion of the project site, north of about Shade Rd, is mapped as an average of 20 ft of till over Mississippian-age sandstone and shale. The till in this region is generally described as consisting of an unsorted mix of Wisconsinan-age clay, silt, gravel and boulders with possible silt, sand and gravel lenses. The till was deposited directly from the ice of several separate advances and may be older than Wisconsinan in buried valleys and thicker areas.

Based on the Bedrock Geologic Units Map of Ohio (USGS & ODGS, 2005), bedrock within the majority of the project area consists of Mississippian Maxville Limestone as well as the undivided Rushville, Logan and Cuyhoga formations. The bedrock of these formations are described as interbedded siltstone, shale and sandstone with minor constituents of conglomerate and limestone. The major constituents are described as being various shades of gray and yellow to brown in color weathering to similar colors. The sandstone in this formation is described as silty to granular with local strings of quartz pebbles while the shale is described as clayey to silty and locally fossiliferous. In another area for the site, from approximately 1000 ft northeast of North Cleveland Massillon Rd to about 350 ft southwest of Yellow Creek Rd along IR-77, bedrock is mapped as a combination of Devonian-age undivided Berea Sandstone, Bedford Shale bedrock, and Devonian-age Ohio Shale bedrock. The Berea Sandstone is described as brown in color weathering to light brown to reddish brown, with siltstone interbeds in the lower portion. The Bedford Shale is described as gray to brown and locally reddish brown in color while the Ohio Shale is described as brownish black to greenish gray in color weathering to brown that is carbonaceous to clayey. According to the ODNR bedrock topography map of Ohio, bedrock elevations at the project site can be expected to range from 1150 ft to 600 ft amsl. Therefore, bedrock is anticipated to range from a depth of 12 ft to a depth of 400 ft below ground surface (bgs).

The majority of soils directly underlying project site have been mapped (Web Soil Survey) by the Natural Resources Conservation Service as being Udorthents. Udorthents are soils that have been disturbed by cutting or filling and are not rated for local roads. Though udorthents was mapped as the dominant unit underlying the project site, various other soil series were mapped within or adjacent to the project boundaries. Of these units, the most dominant included the Rittman silt loam, Chili loam and gravelly loam, Wadsworth silt loam, Mahoning silt loam and Ellsworth silt loam. The Rittman, Wadsworth, Mahoning and Ellsworth series (mapped within or adjacent to about 35 percent of the project area) are all characteristically similar and are described as very deep, moderately well to somewhat poorly drained soils formed in Wisconsinan-age low lime till on till plains. Some pedons (overburden units) of these series are noted as having a thin mantel of loess or other silty material. The till in the Mahoning and Ellsworth series are characterized as deriving from primarily shale and siltstone with minor amounts of limestone and crystalline rocks. Soils within these series are predominantly fine-grained cohesive soil that classify as A-4, A-6 and A-7 type soils according to the AASHTO method of soil classification. The Chili series (mapped within or adjacent to about 6 percent of the project area) is described as very deep, well drained soils formed in Wisconsinan-age outwash deposits on outwash plains, terraces, kames and beach ridges, mainly of non-calcareous sandstone and shale with a large amount of quartz gravel. Soils within this series are

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commonly mantled with silt and consist of both coarse- and fine-grained non-cohesive soil that classify as A-1, A-2 and A-4 type soils (AASHTO method of soil classification). Other less dominant (i.e., less than 1 percent) series mapped within or adjacent to the project boundaries include the Canfield, Carlisle, Conotton-Oshtemo, Fitchville, Lodbell, Loudonville, Olmsted, Sebring, and Wheeling series (USDA, 2015).

2.2. Hydrology/Hydrogeology

Groundwater elevations throughout the project site are anticipated to vary throughout the length of the project with exception being the portion of the project located in close proximity to Yellow Creek. Based on the potentiometric surface map of Ohio, groundwater throughout the project site generally decreases in elevation approaching Yellow Creek, where the groundwater elevation is expected to be near the elevation of Yellow Creek. Groundwater elevation decreases from approximate elevations of 1,150 ft amsl and 1,000 ft amsl near the project's northern and southern boundaries, respectively, to a minimum groundwater elevation near Yellow Creek of approximately 850 ft amsl. It should be noted that perched groundwater systems may also exist due to the presence of fine-grained soils making it difficult for groundwater to permeate to the natural phreatic surface.

Portions of the project within about 50 ft of Yellow Creek are located within a 0.2% and 1% Annual Chance Flood Hazard area. Based on available mapping by the Federal Emergency Management Agency's (FEMA) National Flood Hazard mapping program (FEMA, 2016), Yellow Creek is noted as a regulatory floodway with a 1% Annual Chance Flood elevation ranging from about 885 to 890 ft amsl within the flood hazard area.

2.3. Mining and Oil/Gas Production

No abandoned mines are noted on ODNR's Abandoned Underground Mine Locator within the immediate vicinity of the project's boundaries (ODNR [1], 2016).

Five (5) oil and gas wells were noted on ODNR's Ohio Oil & Gas Locator within the immediate vicinity of the project's boundaries (within 300 ft of existing roadways/ramps). The first oil and gas well (API Well No. 34153226610000) is located near the western boundary of the project, approximately 880 ft south of Yellow Creek Rd and approximately 200 ft west of IR-77. The second and third wells (API Well Nos. 34153227880000 and 34153228690000) are located near the eastern boundary of the project, with the wellheads about 210 ft north of and 100 ft north of Yellow Creek Rd, respectively and about 235 ft east of and 275 ft east of IR-77, respectively. These first three identified wells were drilled to depths ranging from 3,631 to 4,215 ft bgs with the most recent production being recorded in 2015. The fourth well (API Well No. 34153227360000) is located near the western boundary of the project, approximately 200 ft north of Martadale Dr and approximately 100 ft west of IR-77. The fifth well (API Well No. 34153220510000) is located near the western boundary of the project, approximately 1000 ft south of Shade Rd and approximately 260 ft west of IR-77. These last two identified wells were drilled to depths ranging from 3,709 to 3,717 ft bgs and are noted as currently producing (ODNR [2], 2016). More information on the identified wells can be found on the ODNR Oil Well reports included within Appendix A.

2.4. Historical Records and Previous Phases of Project Exploration

A historic record search was performed through ODOT's Geotechnical Data Management System (GeoMS) and the following report/plans were available for review and evaluation for this report:

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- Soil Profile Sheets for the ODOT project SUM-21-4.31, prepared by the State of Ohio Department of Highways State Testing Laboratory, dated November 16, 1955;
- Soil Profile Sheets, Structure Foundation Investigations and Geotechnical Exploration Findings for the ODOT project SUM-21-11.42, prepared by the State of Ohio Department of Highways State Testing Laboratory, dated March 22, 1961 and May 22, 1961;
- Soil Profile Sheets and Geotechnical Exploration Findings for the ODOT project SUM-18-1.31, prepared by the State of Ohio Department of Highways, submitted on July 16, 1963 and August 15, 1963;
- Soil Profile Sheets and Geotechnical Exploration Findings for the ODOT project SUM-77-19.85, prepared by the State of Ohio Department of Highways State Testing Laboratory, submitted on July 1, 1969 and July 3, 1969;
- Final Slope Stability Report, Stabilization Recommendations and Structure Foundation Exploration Sheets for Bridge SUM-77-40.538L&R over Yellow Creek as part of the ODOT Project SUM-77-24.19 prepared by BBC&M Engineering, Inc., dated May 28, 1999 and October 9, 2000;
- Structure Foundation Exploration Sheets for Bridge SUM-77-41.954L&R over Bath Road as part of ODOT project SUM-77-41.954 prepared by Prime Engineering and Architecture, Inc., dated August 14, 2000;

Historical soil borings associated with the above plans were reviewed, however, the available information was not utilized for our evaluation of the site. The information was not utilized because the subject project is primarily a pavement replacement project and boring information of the previous projects subgrade and pavement buildups have a high probability of change between various projects and maintenance over the years. Therefore, this historical information are not referenced or presented within this report.

2.5. Field Reconnaissance

A field reconnaissance visit for the overall project area was conducted between August 18, 2020 and August 21, 2020. The reconnaissance was performed along IR-77, the associated Ghent Rd ramps (Ramp L, Ramp M, Ramp N, Ramp P, Ramp R, and Ramp S) and the associated Roadside Rest Area ramps (Ramp A, Ramp B, Ramp C, and Ramp D). Site conditions, including the existing pavement conditions, were noted and photographed during the visit. Photographs of notable pavement distress and a summary of our observations by roadway segment are provided below.

2.5.1. Land Use and Cover

The land use of most of the project area consists of a combination of wooded and residential properties. Other land uses of the area surrounding the project include: 1) industrial facilities; 2) commercial properties; and 3) institutional facilities. Additionally, east of IR-77 from about 1,000 ft north of the IR-77/Ghent Rd intersection to the end of the project, high voltage electrical lines with associated electrical towers and tree cleared grass lands are present.

2.5.2. IR-77 from Beginning of Project to Ghent Road

In general, the pavement condition along this section of IR-77 was observed to be fair with various signs of weathering and surface wear. Moderate severity longitudinal and transverse cracking was frequent along this section, as well as occasional moderate severity patching and potholing (Photograph 1). The roadway drains to open drainage swales on either side of the roadway as well as to an apparent lowland in the median between IR-77 northbound (NB) and southbound (SB) just south Ghent Rd. The indicated lowland area is heavily vegetated with signs of long-term standing water observed (i.e., cattails and other vegetation)

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(Photograph 2). This area appeared to drain to a culvert that runs under the NB lanes of IR-77 to another low-lying area to the east of IR-77 (Photograph 3). The inlet of the culvert was not visible due to the large amount of vegetation. In general, this area appeared to be stable with no apparent signs of instability observed during our visit.

Photograph 1: Pavement transition at beginning of project



Photograph 2: Drainage area in median



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Photograph 3: Culvert directing drainage from median to east of IR-77 NB



2.5.3. IR-77 From Ghent Road to Ira Road

In general, the pavement condition along this section of IR-77 was observed to be fair to good with few signs of weathering and surface wear. Occasional moderate severity longitudinal and transverse cracking was observed along this section as well as moderate severity patching and crack sealing deficiencies. The wearing courses of the bridges in this section appear to be in good condition with very few signs of surface wear. This section of IR-77 from just north of Ghent Rd to Ira Rd includes various transitions between cut sections and fill section before leveling out with the surrounding area just south of Ira Rd. The cut and fill slopes along this segment range from about 2 Horizontal:1 Vertical (2H:1V) to about 3H:1V. Both cut and fill slopes along this segment appeared to be stable with no apparent signs of instability noted during our visit. IR-77 along this segment appears to drain to open drainage swales on the outside shoulders of the highway as well as to drainage basins in the median, where present. Drainage swales were observed to be vegetated with the exception of a small section of a concrete lined drainage swale on the east side of IR-77 NB, about halfway between Shade Rd and Ira Rd (Photograph 4). The pavement section along IR-77 from just north of Ghent Rd to Ira Rd was observed to be well drained with no signs of standing water in the roadway.

Photograph 4: Paved drainage swale between Shade Road and Ira Road



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2.5.4. IR-77 from Ira Road to End of Project

In general, the pavement condition along this section of IR-77 was observed to be fair to good with minor signs of weathering and surface wear. Occasional light severity longitudinal and transverse cracking was observed along this section as well as occasional moderate severity patching and raveling. With the exception of the portion of IR-77 just north of the Ira Rd overpass, IR-77 SB is relatively level with the surrounding area while, IR-77 NB is supported on a relatively small embankment with side slopes of about 3H:1V. Immediately north of Ira Rd, the interstate is supported on embankment leading up to the Ira Rd overpass, with embankment slopes of about 2H:1V. Embankment slopes along this segment were observed to be stable with no apparent signs of instability noted during our visit. Similar to the other segments of IR-77 within the project area, this segment of interstate directed drainage to open vegetated swales on the outside shoulders of the highway as well as to drainage basins in the median.

2.5.5. Ramp L, Ramp M, Ramp N, Ramp P, Ramp R, and Ramp S

In general, the pavement condition along the Ghent Rd and IR-77 interchange ramps was observed to be fair to good with various signs of weathering and surface wear. Frequent low to moderate severity longitudinal and transverse cracking and moderate to high severity map cracking, edge cracking and crack sealing deficiencies, and occasional moderate severity patching was observed along these ramp sections (Photograph 5). The referenced ramps all sit atop embankments with side slopes ranging from 2H:1V to flatter than 4H:1V. The exception to this is Ramp L (IR-77 NB exit ramp to Ghent Rd), which is also the ramp which the proposed Noise Wall is planned to approximately parallel, that follows the natural rise in terrain up to Ghent Rd. Embankment and natural slopes along these segment were observed to be stable with no apparent signs of instability noted during our site visit. The referenced ramp segments appeared to drain to open vegetated drainage swales on either side of the ramp as well as to large vegetated areas in between the ramps and/or interstate. Some signs of standing water were observed in these areas (i.e., cat tails) though no sign of standing water on the ramps were observed.

Photograph 5: Pavement condition of IR-77 NB ramp from Ghent Road (Ramp M)



2.5.6. Ramp A, Ramp B, Ramp C and Ramp D

In general, the pavement condition along the IR-77 NB entrance and exit ramps to the Roadside Rest Stop (Ramps A and B) was observed to be fair with various signs of weathering and surface wear. Frequent moderate severity longitudinal and transverse cracking was observed along this section, as well as

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occasional moderate severity map cracking and potholing (Photograph 6). The pavement condition along the IR-77 SB entrance and exit ramps (Ramps C and D) was observed to be poor with more severe signs of weathering and surface wear. Frequent moderate severity longitudinal and transverse cracking was observed along this section as well as occasional high severity rutting, patching, bleeding and map cracking (Photograph 7). The referenced rest stop ramps are supported by embankment at the approximate level of the interstate and slope downward to the rest stop elevation which is more consistent with that of the surrounding area. The indicated embankments were observed to have side slopes of about 2H:1V and appeared stable with no apparent signs of instability noted during our visit. The ramps appeared to drain to open vegetated drainage swales on both sides of the ramp as well as to catch basins in the grassy areas between the rest stop and IR-77. Though signs of standing water (i.e., cattails) were observed in areas adjacent to the ramps, no sign of ponding within the ramp pavement was observed.

Photograph 6: Pavement condition along IR-77 NB entrance ramp from Roadside Rest Stop (Ramp B)



Photograph 7: Pavement condition along IR-77 SB entrance ramp from Roadside Rest Stop (Ramp D)



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3. GEOTECHNICAL EXPLORATION

3.1. Exploration Program

The subsurface exploration was conducted by NEAS and GPD between August 8, 2020 and February 2, 2022 and included 118 borings drilled to depths between 6 and 52.0 ft bgs. The boring locations were selected by NEAS in general accordance with the guidelines contained in the SGE with the intent to evaluate subsurface soil and groundwater conditions. Borings were typically located either within existing pavement areas that are planned to undergo full-depth replacement, within areas where widening and/or realignment is planned, at proposed high mast lighting locations, and at culvert locations where jack and bore drilling may be performed. Target boring locations were located in the field by NEAS or GPD prior to drilling and the boring locations were drilled in areas that were not restricted by underground utilities or dictated by terrain (i.e. steep embankment slopes). Each as-drilled project boring location and corresponding ground surface elevation was surveyed in the field following drilling. Each individual project boring log (included within Appendix C) includes the recorded boring latitude and longitude location (based on the surveyed Ohio State Plane North, NAD83, location) and the corresponding ground surface elevation. The boring locations are depicted within the boring location plan provided in Appendix B. It should be noted that a number of borings were drilled for a project structure (i.e., noise wall) but can serve as both structure and roadway borings and therefore, are included within this report.

Borings were drilled using either a CME 55X track-mounted or a CME 45B truck-mounted drilling rig utilizing 3.25-inch (inner diameter) hollow stem augers. Soil samples for subgrade borings were typically recovered continuously to a depth of 7.5 ft bgs, while samples for structure borings were typically recovered at 2.5-ft intervals, each using an 18-inch split spoon sampler (AASHTO T-206 "Standard Method for Penetration Test and Split Barrel Sampling of Soils."). Samples from joint subgrade (Type A) and structure borings (Type E4) were typically recovered continuously to a depth of 7.5 ft bgs then at 2.5-ft intervals thereafter. The soil samples obtained from the exploration program were visually observed in the field by the NEAS/GPD field representative and preserved for review by a Geologist for possible laboratory testing. Standard penetration tests (SPT) were conducted using CME auto hammers that have been calibrated on December 5, 2019 or January 26, 2022, to be between 67.6% and 81.9% efficient as indicated on the boring logs (Appendix C).

Field boring logs were prepared by drilling personnel and included pavement description (where present), lithological description, SPT results recorded as blows per 6-inch increment of penetration and estimated unconfined shear strength values on specimens exhibiting cohesion (using a hand penetrometer). Groundwater level observations were recorded both during and after the completion of drilling. These groundwater level observations are included on the individual boring logs (provided in Appendix C). After completing the borings, the boreholes were backfilled with either auger cuttings, bentonite chips, or a combination of these materials and patched accordingly with cold patch asphalt and/or cement when drilled through the roadway.

3.2. Pavement Coring Exploration Program

The coring exploration program for this project was conducted by NEAS between November 17, 2020 and December 16, 2020 and included a total of sixteen (16) pavement cores. Pavement cores were obtained at four (4) project boring locations (B-014-0-20, B-029-0-20, B-042-0-20 and B-057-0-20) performed through the existing pavement. In addition to the cores obtained at the indicated boring locations, four (4) additional cores were taken within the bridge approach shoulders of each of the following bridges: IR-77 over Yellow Creek Rd/Yellow Creek, IR-77 over West Bath Rd, and IR-77 over Ira Rd. As described in

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Section 3.1. of this report, the indicated target boring/coring locations were located in the field by NEAS prior to drilling utilizing handheld GPS equipment in areas that were not restricted by maintenance of traffic efforts or utilities. Measurements, location information, photographs and other details of each core sample can be found in the Pavement Core Logs included within Appendix D. The approximate location for each core is depicted on the Boring Location Plan provided in Appendix B.

Cores were drilled using a portable, truck-mounted, electric powered coring drill with a 4-inch (outer diameter) diamond tipped drill bit and utilizing water as the circulating fluid. Asphalt and concrete thicknesses were measured in the field after the cores were extracted and down-hole measurements were made. Each core sample was then photographed, logged, and stored for transportation to NEAS's laboratory. Following field documentation and photographs, the core hole was backfilled to existing grade with either asphalt patch or concrete (as appropriate). Once in the laboratory the cores were: 1) re-measured for thickness verification and photographed; 2) checked for composition; and, 3) reviewed for individual layer identification and subsequent measurements.

3.3. Laboratory Testing Program

The laboratory testing program consisted of classification testing, moisture content determinations, organic content loss on ignition, sulfate content testing and one-dimensional consolidation testing. Data from the laboratory testing program were incorporated onto the boring logs (Appendix C). Soil samples are retained at the laboratory for 60 days following report submittal, after which time they will be discarded.

3.3.1. Classification Testing

Representative soil samples were selected for index property (Atterberg Limits) and gradation testing for classification purposes on approximately 40% of the samples. At each subgrade boring location, the upper two samples obtained below the proposed top of subgrade elevation were generally tested while additional samples were selected for testing with the intent of properly classifying the subsurface soil and groundwater conditions within the planned project limits. Soils not selected for testing were compared to laboratory tested samples/strata and classified visually. Moisture content testing was conducted on all samples. The laboratory testing was performed in general accordance with applicable AASHTO specifications and ODOT Supplements.

Final classification of soil strata in accordance with AASHTO M-145 "Classification of Soils and Soil-Aggregate Mixtures for Highway Construction Purposes," as modified by ODOT "Classification of Soils" was made once laboratory test results became available. The results of the soil classification are presented on the boring logs in Appendix C.

3.3.2. Standard Penetration Test Results

Standard Penetration Tests (SPT) and split-barrel (commonly known as split-spoon) sampling of soils were performed at varying intervals (i.e., continuous, 2.5-ft, or 5-ft intervals) in the project borings performed. To account for the high efficiency (automatic) hammers used during SPT sampling, field SPT N-values were converted based on the calibrated efficiency (energy ratio) of the specific drill rig's hammer. Field N-values were converted to an equivalent rod energy of 60% (N_{60}) for use in analysis or for correlation purposes. The resulting N_{60} values are shown on the boring logs provided in Appendix C.

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3.3.3. *Organic Content Loss on Ignition*

Organic Content Loss on Ignition testing (LOI) was performed on two samples (SS-1 and SS-4) from boring B-095-0-20 and one undisturbed sample (ST-1) from boring B-093-0-20, each of which were performed for embankment/roadway design purposes. The selected samples were tested in accordance with AASHTO T267 “Standard Method of Test for Determination of Organic Content in Soils by Loss on Ignition”. The samples were found to have an organic content ranging from 3.4% to 8.2%. Per the SGE, an organic content greater than 10% is considered highly organic. A summary of the LOI laboratory testing results are provided in Table 1 below while the lab testing report of the LOI tests is presented within Appendix C.

Table 1: Summary of Organic Content Loss on Ignition Testing

Boring ID	Sample	Depth (ft)	Moisture Content (%)	Organic Content (%)
B-095-0-20	SS-1	2.5 - 4.0	20	4.1
B-095-0-20	SS-4	10.0 - 11.5	28	8.2
B-093-0-20	ST-1	13.5 - 13.8	19	3.4

3.3.4. *Consolidation Testing*

Two (2) consolidation tests were performed in accordance with ASTM D 2435-04 “Standard Test Methods for One-Dimensional Consolidation Properties of Soils Using Incremental Loading” on relatively undisturbed cohesive soil samples collected from borings B-093-0-20 and B-097-0-20; the results of the tests are presented in Table 2 below, while the laboratory testing report is included within Appendix C.

Table 2: Summary of Consolidation Testing

Boring Number	Depth (ft)	Elevation (ft)	Compression Index (Cc)	Recompression Index (Cr)	Preconsolidation Pressure (psf)	Initial Void Ratio
B-093-0-20	13.5 - 13.6	997.8 - 997.7	0.102	0.006	3,500	0.564
B-097-0-20	10.6 - 10.7	983.0 - 982.9	0.063	0.011	5,500	0.474

3.3.5. *Sulfate Testing*

Sulfate testing was generally performed on one sample for each subgrade/roadway boring performed for pavement/subgrade design purposes. The selected samples were tested in accordance with ODOT Supplement 1122, “Determining Sulfate Content in Soils” dated July 17, 2015. In general, the upper most sample (within 3 ft of the proposed subgrade elevation) from each boring was tested when feasible. Testing results are summarized in Table 3 below, provided in Appendix E and presented on the boring logs within Appendix C.

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Table 3: Sulfate Test Summary by Boring

Boring ID	Sample	Depth (ft)	Dilution Ratio	Average Sulfate Content (ppm)	Boring ID	Sample	Depth (ft)	Dilution Ratio	Average Sulfate Content (ppm)
B-001-0-20	SS-1A	1.5 - 2.7	20	53	B-048-0-20	SS-1	1.5 - 3.0	20	113
B-002-0-20	SS-1	1.5 - 3.0	20	53	B-049-0-20	SS-1	0.0 - 1.5	20	487
B-003-0-20	SS-1	0.0 - 1.5	20	0	B-050-0-20	SS-1	1.5 - 3.0	20	73
B-004-0-20	SS-1	1.5 - 3.0	20	67	B-051-0-20	SS-1	1.5 - 3.0	20	67
B-005-0-20	SS-1	0.0 - 1.5	20	13	B-052-0-20	SS-1	1.5 - 3.0	20	67
B-006-0-20	SS-1	0.0 - 1.5	20	20	B-053-0-20	SS-1	0.0 - 1.5	20	67
B-007-0-20	SS-1	1.5 - 3.0	20	147	B-054-0-20	SS-1	0.0 - 1.5	20	20
B-008-0-20	SS-1	1.5 - 3.0	20	53	B-055-0-20	SS-1	0.0 - 1.5	20	120
B-009-0-20	SS-1	1.5 - 3.0	20	253	B-056-0-20	SS-1	0.0 - 1.5	20	347
B-010-0-20	SS-1	0.0 - 1.5	20	173	B-057-0-20	SS-1	1.5 - 3.0	20	80
B-011-0-20	SS-1	1.5 - 3.0	20	133	B-058-0-20	SS-1	1.5 - 3.0	20	107
B-012-0-20	SS-1	1.5 - 3.0	20	47	B-059-0-20	SS-1	1.5 - 3.0	20	107
B-013-0-20	SS-1	0.0 - 1.5	20	113	B-061-0-20	SS-2	1.5 - 3.0	20	0
B-014-0-20	SS-1	1.5 - 3.0	20	73	B-062-0-20	SS-1	1.5 - 3.0	20	20
B-015-0-20	SS-1	0.0 - 1.5	20	13	B-063-0-20	SS-1	0.0 - 1.5	20	140
B-016-0-20	SS-1	1.5 - 3.0	20	20	B-064-0-20	SS-1	1.5 - 3.0	20	40
B-017-0-20	SS-1	0.0 - 1.5	20	40	B-065-0-20	SS-1	1.5 - 3.0	20	20
B-018-0-20	SS-1	1.5 - 3.0	20	40	B-066-0-20	SS-1	1.5 - 3.0	20	60
B-019-0-20	SS-1A	1.5 - 2.0	20	87	B-067-0-20	SS-1	1.5 - 3.0	20	40
B-020-0-20	SS-1	1.5 - 3.0	20	140	B-068-0-20	SS-1	1.5 - 3.0	20	827
B-021-0-20	SS-1	1.5 - 3.0	20	20	B-069-0-20	SS-1	1.5 - 3.0	20	33
B-022-0-20	SS-1	0.0 - 1.5	20	120	B-070-0-20	SS-1	1.5 - 3.0	20	20
B-023-0-20	SS-1	1.5 - 3.0	20	113	B-071-0-20	SS-1	1.5 - 3.0	20	33
B-024-0-20	SS-1A	0.0 - 1.0	40	1973	B-072-0-20	SS-1	1.5 - 3.0	20	280
B-025-0-20	SS-2	3.0 - 4.5	20	107	B-074-0-20	SS-1	1.5 - 3.0	20	127
B-026-0-20	SS-1	0.0 - 1.0	20	113	B-075-0-20	SS-1	1.5 - 3.0	20	313
B-027-0-20	SS-1	0.0 - 1.0	20	13	B-076-0-20	SS-1	1.5 - 3.0	20	100
B-028-0-20	SS-1	1.5 - 3.0	20	73	B-078-0-20	SS-1	1.5 - 3.0	20	93
B-029-0-20	SS-1	1.5 - 3.0	20	80	B-079-0-20	SS-1	1.5 - 3.0	20	313
B-030-0-20	SS-1	0.0 - 1.5	100	5467	B-080-0-20	SS-1	1.5 - 3.0	20	20
B-032-0-20	SS-1	0.0 - 1.5	20	87	B-081-0-20	SS-1	1.5 - 3.0	20	20
B-033-0-20	SS-1	1.5 - 3.0	20	1360	B-082-0-20	SS-1	1.5 - 3.0	20	127
B-034-0-20	SS-1	1.5 - 3.0	20	307	B-084-0-20	SS-1	1.5 - 3.0	20	7
B-035-0-20	SS-1	0.0 - 1.5	20	193	B-085-0-20	SS-1	1.5 - 3.0	20	60
B-036-0-20	SS-1	0.0 - 1.5	20	40	B-086-0-20	SS-2	1.5 - 3.0	20	33
B-037-0-20	SS-1	1.5 - 3.0	20	380	B-087-0-20	SS-1	1.5 - 3.0	40	1200
B-038-0-20	SS-1	0.0 - 1.5	20	160	B-088-0-20	SS-1	1.5 - 3.0	20	93
B-039-0-20	SS-1	0.0 - 1.5	20	233	B-089-0-20	SS-2	1.5 - 3.0	20	107
B-040-0-20	SS-1	1.5 - 3.0	20	40	B-090-0-20	SS-2	1.5 - 3.0	20	167
B-041-0-20	SS-1	0.0 - 1.5	20	80	B-091-0-20	SS-1	1.5 - 3.0	20	167
B-042-0-20	SS-1	1.5 - 3.0	20	147	B-092-0-20	SS-1	2.5 - 4.0	20	313
B-043-0-20	SS-1	1.5 - 3.0	20	80	B-093-0-20	SS-1	2.5 - 4.0	20	93
B-044-0-20	SS-1	0.0 - 1.5	20	67	B-094-0-20	SS-1	2.5 - 4.0	20	80
B-045-0-20	SS-1	0.0 - 1.5	20	173	B-095-0-20	SS-1	2.5 - 4.0	40	1760
B-046-0-20	SS-1	1.5 - 3.0	20	113	B-096-0-20	SS-2	2.5 - 4.0	20	187
B-047-0-20	SS-2	0.0 - 1.5	20	113	B-097-0-20	SS-1	2.5 - 4.0	20	13

4. FINDINGS

The subsurface conditions encountered during NEAS's explorations are described in the following subsections and/or on each boring log presented in Appendix C. The boring logs represent NEAS's interpretation of the subsurface conditions encountered at each boring location based on our site observations, field logs, visual review of the soil samples by NEAS's geologist, and laboratory test results. The lines designating the interfaces between various soil strata on the boring logs represent the approximate

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interface location; the actual transition between strata may be gradual and indistinct. The subsurface soil and groundwater characterizations included herein, including summary test data, are based on the subsurface findings from the geotechnical explorations performed by NEAS as part of the referenced project. At the time of this report, pavement grade information has been assumed to be consistent with preliminary proposed roadway grades found within digital design models developed by GPD and accessed on January 12, 2021. It should be noted that for the purposes of this report and our analysis the term 'subgrade' has been assumed to represent soils and/or soil conditions from 1.5 ft below proposed final pavement grades to a depth of 7.5 ft below the proposed pavement grades.

4.1. Core Results

Thickness measurements were obtained for each of the indicated pavement cores performed for the project. A summary of these measurements along with the material encountered and the associated boring location at which the pavement core was obtained (where applicable) is summarized in Table 4. Laboratory photographs and measurements of each of the cores are presented within the Pavement Core Logs included within Appendix D. Locations of the pavement cores or the boring locations where pavement cores were performed are depicted on the Boring Location Plan included within Appendix B.

Table 4: Pavement Core Summary

Core ID	Alignment	Asphalt Thickness (in)	Concrete Thickness (in)	Total Thickness (in)
B-014-0-20 / PC-1	IR-77 SB	6.25	-	6.25
PC-2	IR-77 (SB Shoulder)	12.50	0.25	12.75
PC-3	IR-77 (SB Shoulder)	3.50	6.75	10.25
PC-4	IR-77 (NB Shoulder)	14.75	-	14.75
PC-5	IR-77 (NB Shoulder)	12.75	-	12.75
B-029-0-20 / PC-6	IR-77 (NB Shoulder)	5.75	-	5.75
PC-7	IR-77 (SB Shoulder)	11.75	0.75	12.50
PC-8	IR-77 (SB Shoulder)	15.25	-	15.25
PC-9	IR-77 (NB Shoulder)	14.75	-	14.75
PC-10	IR-77 (NB Shoulder)	14.00	-	14.00
B-042-0-20 / PC-11	IR-77 (SB Shoulder)	6.50	-	6.50
PC-12	IR-77 (SB Shoulder)	12.25	-	12.25
PC-13	IR-77 (SB Shoulder)	6.25	-	6.25
PC-14	IR-77 (NB Shoulder)	10.25	-	10.25
PC-15	IR-77 (NB Shoulder)	14.25	-	14.25
B-057-0-20 / PC-16	IR-77 (NB Shoulder)	12.25	-	12.25

4.2. Existing Pavement

The pavement section thicknesses in terms of asphalt, concrete and granular base were measured at representative project subgrade borings during the subsurface exploration for the project and are recorded on the test boring logs provided in Appendix C. A summary of these measurements is provided in Table 5 below.

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Table 5: Measured Pavement Thickness at Boring Locations

Boring ID	Proposed Alignment	Drilled Depth (ft)	Asphalt Thickness (in)	Concrete Thickness (in)	Base Thickness (in)	Total Thickness (in)	Boring ID	Proposed Alignment	Drilled Depth (ft)	Asphalt Thickness (in)	Concrete Thickness (in)	Base Thickness (in)	Total Thickness (in)
B-001-0-20	IR-77 NB	7.5	10.0	0.0	8.0	18.0	B-064-0-20	IR-77 SB	7.5	10.0	0.0	5.0	15.0
B-004-0-20	IR-77 SB	7.5	12.0	0.0	6.0	18.0	B-065-0-20	Ramp S	7.5	10.0	0.0	4.0	14.0
B-007-0-20	IR-77 NB	26.5	10.0	0.0	6.0	16.0	B-066-0-20	Ramp S	7.5	8.0	0.0	7.0	15.0
B-008-0-20	IR-77 SB	7.5	10.0	0.0	6.0	16.0	B-067-0-20	Ramp S	7.5	8.0	0.0	6.0	14.0
B-009-0-20	IR-77 NB	7.5	12.0	0.0	4.0	16.0	B-068-0-20	Ramp P	7.5	8.0	0.0	5.0	13.0
B-012-0-20	IR-77 SB	7.5	12.0	0.0	6.0	18.0	B-069-0-20	Ramp P	7.5	8.0	0.0	4.0	12.0
B-014-0-20	IR-77 SB	7.5	6.0	0.0	6.0	12.0	B-070-0-20	Ramp P	7.5	10.0	0.0	6.0	16.0
B-018-0-20	IR-77 SB	7.5	12.0	0.0	6.0	18.0	B-071-0-20	Ramp P	7.5	10.0	0.0	7.0	17.0
B-020-0-20	IR-77 SB	7.5	12.0	0.0	4.0	16.0	B-072-0-20	Ramp R	7.5	9.0	0.0	6.0	15.0
B-021-0-20	IR-77 NB	7.5	11.0	0.0	6.0	17.0	B-073-0-20	Ramp L	26.5	6.0	0.0	7.0	13.0
B-023-0-20	IR-77 NB	7.5	15.0	0.0	0.0	15.0	B-074-0-20	Ramp L	26.5	6.0	0.0	7.0	13.0
B-025-0-20	IR-77	7.5	10.0	0.0	0.0	10.0	B-075-0-20	Ramp L	26.5	6.0	0.0	10.0	16.0
B-028-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-076-0-20	Ramp L	26.5	0.0	0.0	10.0	10.0
B-029-0-20	IR-77	7.5	6.0	0.0	7.0	13.0	B-077-0-20	Ramp L	26.5	0.0	0.0	8.0	8.0
B-033-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-078-0-20	Ramp L	26.5	0.0	0.0	10.0	10.0
B-034-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-079-0-20	Ghent Rd	7.5	6.0	0.0	7.0	13.0
B-037-0-20	IR-77	7.5	9.0	9.0	0.0	18.0	B-080-0-20	Ramp M	7.5	6.0	0.0	7.0	13.0
B-042-0-20	IR-77	6.5	12.0	0.0	6.0	18.0	B-081-0-20	Ramp N	7.5	6.0	0.0	7.0	13.0
B-043-0-20	IR-77	7.5	9.0	0.0	4.0	13.0	B-082-0-20	Ramp N	7.5	6.0	0.0	7.0	13.0
B-048-0-20	IR-77	7.5	12.0	0.0	4.0	16.0	B-083-0-20	IR-77 NB	7.5	6.0	0.0	7.0	13.0
B-050-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-084-0-20	IR-77	7.5	6.0	0.0	0.0	6.0
B-051-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-085-0-20	Ramp D	7.5	11.0	0.0	0.0	11.0
B-052-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-086-0-20	Ramp C	7.5	9.0	0.0	0.0	9.0
B-057-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-088-0-20	Ramp C	7.5	5.0	0.0	8.0	13.0
B-059-0-20	IR-77	7.5	7.0	0.0	6.0	13.0	B-089-0-20	Ramp A	7.5	8.5	0.0	6.0	14.5
B-060-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-090-0-20	Ramp B	7.5	5.0	10.5	0.0	15.5
B-062-0-20	IR-77	7.5	12.0	0.0	6.0	18.0	B-091-0-20	IR-77	7.5	0.0	0.0	11.0	11.0

4.3. Subgrade Conditions

The subgrade conditions within the project limits are relatively consistent and are generally comprised of either fill soils (i.e., embankment fill) or natural soils consisting of gravel, sand and silt, or low to moderately plastic sandy silt and silt/clay combinations. The subgrade soils encountered within the project limits are generally classified as either bedrock, A-1-a, A-1-b, A-2-4, A-2-6, A-3, A-3a, A-4a, A-4b, A-6a, A-6b, A-7-5 or A-7-6 type soils. With respect to sulfate within the subgrade soil, based on the project laboratory testing program, each subgrade soil sample tested was determined to have a sulfate content of less than 5,000 parts per million (ppm) (i.e., lower than the level which ODOT considers high and may prevent the use of chemical stabilization) with the exception of one boring (B-030-0-20) in which a sample was determined to have a sulfate content of 5,500 ppm.

The following subsections present a brief summary of the subsurface conditions by ramp/roadway segment with problem areas highlighted where present.

4.3.1. IR-77 NB & SB

The project portions of IR-77 NB and SB are planned to be widened into the median as well as undergo full depth pavement replacement. The borings performed along this portion of roadway included borings B-001-0-20 through B-063-0-20.

Along IR-77, seventy percent (70%) of the soil samples were identified as fine-grained soils and were comprised of: 1) cohesive Sandy Silt (A-4a, 29% of samples); 2) Silt (A-4b, 3% of samples); 3) Silt and

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Clay (A-6a, 25% of samples); 4) Silty Clay (A-6b, 9% of samples); and, 5) Clay (A-7-6, 3% of samples). With respect to the consistency of the fine-grained soils, the descriptions varied from medium stiff to hard correlating to converted SPT-N values (N_{60}) between 5 and 66 blows per foot (bpf). Natural moisture contents ranged from 8 to 28 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along the project portions of IR-77, the liquid and plastic limits ranged from 25 to 43 percent and from 15 to 35 percent, respectively.

Twenty-nine percent (29%) of the samples taken along the proposed roadway were classified as coarse-grained, non-cohesive soils and were comprised of: 1) Gravel (A-1-a, 1% of samples); 2) Gravel with Sand (A-1-b, 6% of samples); 3) Gravel and Stone Fragments with Sand and Silt (A-2-4, 8% of samples); 4) Gravel and Stone Fragments with Sand, Silt and Clay (A-2-6, 2% of samples); and, 5) non-cohesive Sandy Silt (A-4a, 3% of samples). With respect to the relative density of the coarse-grained soils, the descriptions varied from very loose to very dense correlating to N_{60} values between 3 and 82 bpf. Natural moisture contents ranged from 6 to 26 percent.

The remaining one percent (1%) of samples (3 samples) obtained along the project portions of IR-77 were identified as rock that was visually classified as shale. Rock was encountered in boring B-042-0-20.

4.3.2. Ramps A and B

Ramps A and B are the entrance and exit ramps for the IR-77 NB rest area which is planned for full depth pavement replacement. The borings performed along Ramps A and B included borings B-089-0-20 through B-091-0-20.

Eighty-two percent (82%) of the soil samples taken along the proposed ramps were identified as fine-grained soils and were comprised of: 1) cohesive Sandy Silt (A-4a, 18% of samples); and, 2) Silt and Clay (A-6a, 64% of samples). With respect to the consistency of the fine-grained soils, the descriptions varied from stiff to hard correlating to N_{60} values between 10 and 33 bpf. Natural moisture contents ranged from 11 to 31 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along the project portion of Ramps A and B, the liquid and plastic limits ranged from 21 to 33 percent and from 16 to 20 percent, respectively.

Eighteen percent (18%) of the samples taken along the proposed ramps were classified as coarse-grained, non-cohesive soils and were comprised of Gravel and Stone Fragments with Sand and Silt (A-2-4, 2 samples). With respect to the relative density of the coarse-grained soils, the soils can be described as medium dense correlating to N_{60} values of 12 and 14 bpf. Natural moisture contents of the two non-cohesive samples were determined to be 12 and 17 percent.

4.3.3. Ramps C and D

Ramps C and D are the entrance and exit ramps for the IR-77 SB rest area which is planned for full depth pavement replacement. The borings performed along Ramps C and D included borings B-084-0-20 through B-088-0-20.

Seventy-five percent (75%) of the soil samples taken along the proposed ramps were identified as fine-grained soils and were comprised of: 1) cohesive Sandy Silt (A-4a, 10% of samples); 2) Silt and Clay (A-6a, 45% of samples); 3) Elastic Clay (A-7-5, 10% of samples); and, 4) Clay (A-7-6, 10 % of samples). With respect to the consistency of the fine-grained soils, the descriptions varied from medium stiff to very stiff correlating to N_{60} values between 5 and 23 bpf. Natural moisture contents ranged from 11 to 33 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils

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obtained along the project portion of Ramps C and D, the liquid and plastic limits ranged from 20 to 69 percent and from 13 to 34 percent, respectively.

Twenty-five percent (25%) of the samples taken along the proposed ramps were classified as coarse-grained, non-cohesive soils and were comprised of: 1) Gravel with Sand (A-1-b, 1 sample); 2) Gravel with Sand and Silt (A-2-4, 2 samples); and, 3) Coarse and Fine Sand (A-3a, 2 samples). With respect to the relative density of the coarse-grained soils, descriptions ranged from loose to medium dense correlating to N_{60} values between 8 and 16 bpf. Natural moisture contents of the non-cohesive samples ranged from 7 to 18 percent.

4.3.4. Ramp L

Ramp L is the IR-77 NB exit ramp to Ghent Rd which are planned for full depth pavement replacement. The borings performed along Ramp L included borings B-073-0-20 through B-078-0-20.

Sixty-three percent (63%) of the soil samples taken along the proposed ramp were identified as fine-grained soils and classified as: 1) cohesive Sandy Silt (A-4a, 32% of samples); 2) Silt and Clay (A-6a, 21% of samples); and, 3) Silty Clay (A-6b, 11% of samples). With respect to the consistency of the fine-grained soils, the descriptions varied from medium stiff to very stiff correlating to N_{60} values between 8 and 26 bpf. Natural moisture contents ranged from 10 to 30 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along the project portions of Ramp L, the liquid and plastic limits ranged from 20 to 40 percent and from 15 to 24 percent, respectively.

Thirty-seven percent (37%) of the samples taken along the proposed ramp were classified as coarse-grained, non-cohesive soils and were comprised of: 1) Gravel and Stone Fragments with Sand and Silt (A-2-4, 2 samples); 2) Gravel with Sand, Silt and Clay (A-2-6, 1 sample); 3) Coarse and Fine Sand (A-3a, 2 samples); and, 4) Sandy Silt (A-4a, 3 samples). With respect to the relative density of the coarse-grained soils, descriptions ranged from loose to medium dense correlating to N_{60} values between 10 and 18 bpf. Natural moisture contents of the non-cohesive samples ranged from 8 to 14 percent.

4.3.5. Ramps M and N

Ramps M and N are the IR-77 NB entrance ramps from Ghent Rd which is planned for full depth pavement replacement. The borings performed along Ramps M and N included borings B-079-0-20 through B-083-0-20.

Sixty-eight percent (68%) of the samples taken along the proposed ramps were classified as coarse-grained, non-cohesive soils and were comprised of: 1) Gravel with Sand (A-1-b, 26% of samples); 2) Gravel with Sand and Silt (A-2-4, 16% of samples); 3) Coarse and Fine Sand (A-3a, 2 samples); and, 4) non-cohesive Sandy Silt (A-4a, 16 % of samples). With respect to the relative density of the coarse-grained soils, the soils can be described as medium dense correlating to N_{60} values between 14 and 25 bpf. Natural moisture contents ranged from 3 to 14 percent.

Thirty-two percent (32%) of the soil samples were identified as fine-grained soils and were comprised of: 1) cohesive Sandy Silt (A-4a, 1 sample); and, 2) Silt and Clay (A-6a, 26% of samples). With respect to the consistency of the fine-grained soils, the descriptions varied from stiff to very stiff correlating to N_{60} values between 10 and 19 bpf. Natural moisture contents ranged from 12 to 23 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along Ramps M and N, the liquid and plastic limits ranged from 23 to 35 percent and from 16 to 20 percent, respectively.

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4.3.6. Ramps P and R

Ramps P and R are the IR-77 SB exits ramps to Ghent Rd which are planned for full depth pavement replacement. The borings performed along Ramps P and R included borings B-068-0-20 through B-072-0-20.

Sixty-five percent (65%) of the samples taken along the proposed ramps were classified as coarse-grained, non-cohesive soils and were comprised of: 1) Gravel with Sand (A-1-b, 2 samples); 2) Gravel with Sand and Silt (A-2-4, 25% of samples); 3) Gravel and Stone Fragments with Sand, Silt and Clay (A-2-6, 2 samples); and, 4) Coarse and Fine Sand (A-3a, 20% of samples). With respect to the relative density of the coarse-grained soils, descriptions ranged from loose to very dense correlating to N_{60} values between 7 and 61 bpf. Natural moisture contents ranged from 7 to 18 percent.

Thirty-five percent (35%) of the soil samples were identified as fine-grained soils and were comprised of: 1) cohesive Sandy Silt (A-4a, 25 % of samples); and, 2) Silt and Clay (A-6a, 2 samples). With respect to the consistency of the fine-grained soils, the descriptions varied from medium stiff to very stiff correlating to N_{60} values between 7 and 26 bpf. Natural moisture contents ranged from 10 to 18 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along Ramps P and R, the liquid and plastic limits ranged from 21 to 30 percent and from 14 to 19 percent, respectively.

4.3.7. Ramp S

Ramp S is the IR-77 SB entrance ramp from Ghent Rd which is planned for full depth pavement replacement. The borings performed along Ramp S included borings B-064-0-20 through B-067-0-20.

Sixty-three percent (63%) of the samples taken along the proposed ramp were classified as fine-grained soils and were comprised of: 1) cohesive Sandy Silt (A-4a, 35% of samples); 2) Silt and Clay (A-6a, 19% of samples); and, 3) Silty Clay (A-6b, 1 sample). With respect to the consistency of the fine-grained soils, the descriptions varied from stiff to very stiff correlating to N_{60} values between 11 and 23 bpf. Natural moisture contents ranged from 12 to 19 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along Ramp S, the liquid and plastic limits ranged from 22 to 29 percent and from 14 to 19 percent, respectively.

Thirty-seven percent (37%) of the soil samples were identified as fine-grained soils and were comprised of: 1) cohesive Sandy Silt (A-4a, 38% of samples); 2) Silt and Clay (A-6a, 19% of samples); and, 3) Silty Clay (A-6b, 1 sample). With respect to the consistency of the fine-grained soils, the descriptions varied from stiff to very stiff correlating to N_{60} values between 11 and 23 bpf. Natural moisture contents ranged from 11 to 19 percent. Based on Atterberg Limit tests performed on representative samples of the fine-grained subgrade soils obtained along Ramp S, the liquid and plastic limits ranged from 22 to 29 percent and from 14 to 19 percent, respectively.

4.3.8. Groundwater

Groundwater was observed within proposed subgrade depths during drilling in one (1) of the borings (B-003-0-20) performed at the site as part of the roadway exploration. Based on measurements at this boring location groundwater was encountered at a depth of 4.5 ft bgs (elevation 1002.5 ft amsl). It should be noted that groundwater is affected by many hydrologic characteristics in the area and may vary from those measured at the time of the exploration. The specific groundwater readings are included on the individual test boring logs located within Appendix C.

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5. ANALYSES AND RECOMMENDATIONS

We understand that reconstruction and widening of the IR-77 mainline freeway segment as well as reconstruction of various adjacent ramps are planned as part of the interchange improvement project (SUM-77-24.12, PID 111404). In addition to the roadway reconstruction and/or widening, the construction of a noise barrier along the southeastern side of the IR-77 NB exit ramp to Ghent Rd (Ramp L) is also planned. For this purpose, a geotechnical exploration and subsequent analysis was completed for the referenced project. The analysis completed for the proposed roadway improvements included a subgrade (GB1) analysis as well as a noise wall drilled shaft foundation analysis. The subgrade analysis was performed in accordance with ODOT's GB1 criteria utilizing the ODOT provided *GB1: Subgrade Analysis Spreadsheet* (GB1_SubgradeAnalysis.xls, Version 14.5 dated January 18, 2019). The noise wall foundation analysis was performed in accordance with *ODOT's 2020 LRFD Bridge Design Manual* (BDM) (ODOT, 2020), specifically utilizing the methodology presented in Section 802.1.2. Input information for our analyses was based on the soil characteristics gathered during NEAS's geotechnical exploration (i.e., SPT results, laboratory test results, etc.).

Based on our evaluation of the subsurface conditions and our geotechnical engineering analyses of the proposed reconstruction and widening project, it is our opinion that subgrade conditions are generally satisfactory, and pavement can be supported by the underlying subsurface material utilizing 12-inches of chemical stabilization (global stabilization) per ODOT's GB1, though certain segments of mainline IR-77, at which unsuitable soils were encountered, may require additional stabilization beyond the recommended 12-inches. Further detail regarding our subgrade analysis and the recommended remediation are provided in Section 5.1 and Section 5.2 of this report, respectively.

Noise wall drilled shaft foundation analysis and recommendations are provided in Section 5.5 of this report.

5.1. Subgrade Analysis

A GB1 analysis was performed to identify the method, location, and dimensions (including depth) of required subgrade stabilization for the project. In addition to identifying stabilization recommendations, pavement design parameters are also determined to aid in pavement section design. The subsections below present the results of our GB1 analysis including pavement design parameters and unsuitable subgrade conditions identified within the project limits. GB1 analysis spreadsheets are provided in Appendix F.

Again, it should be noted that for the purposes of this report and our analysis, the term 'proposed subgrade' has been assumed to represent soils and/or soil conditions from 1.5 ft below proposed final pavement grades to a depth of 7.5 ft below the proposed pavement grades.

5.1.1. Pavement Design Recommendations

It is our understanding that pavement analysis and design is to be performed to determine the proposed pavement sections for the segments within the project limits to undergo full depth replacement. A GB1 analysis was performed using the subgrade soil data obtained during our field exploration program to evaluate the soil characteristics and develop pavement parameters for use in pavement design. The subgrade parameters recommended for use in pavement design are presented in Table 6 below. Provided in the table are ranges of maximum, minimum and average N_{60L} values for the indicated segments as well as the design CBR value recommended for use in pavement design.

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Table 6: Pavement Design Values

Segment	Maximum N _{60L}	Minimum N _{60L}	Average N _{60L}	Average PI Values	Design CBR
IR-77 NB & SB	30	3	13	11	7
IR-77 NB & SB - Existing Subgrade	30	5	15	10	8
IR-77 NB & SB - Widened Areas	30	3	11	12	7
Ramp A & B	22	10	14	12	7
Ramp C & D	11	5	9	15	7
Ramp L	18	8	13	10	7
Ramp M & N	18	10	15	11	9
Ramp R	22	7	13	8	10
Ramp S	15	5	12	9	8
Entire Project	30	3	13	11	8

5.1.2. *Unsuitable Subgrade*

Per ODOT's GB1, the presence of select subgrade conditions (i.e., unsuitable) are prohibited within the subgrade zone for new pavement construction. These unsuitable subgrade conditions generally include the presence of rock and specific soil types. With respect to the proposed pavement construction and realignment project these subgrade conditions are further discussed in the following subsections.

5.1.2.1. *Rock*

Rock was encountered within the subgrade in one (1) boring performed (B-042-0-20) within the project roadway limits. The bedrock was encountered at a depth of 3.0 ft bgs (elevation 1101.1 ft amsl) in boring B-042-0-20. Per ODOT's GB1, if rock is encountered within 24 inches of the bottom of the proposed asphalt or concrete pavement it is to be removed in accordance with 204.05 of the ODOT CMS and replaced with Item 204 Embankment. Therefore, based on the one boring where rock was encountered, no rock remediation is required at the site. It should be noted however, that rock remediation may be required if rock is encountered within 24 inches of the bottom of the proposed asphalt or concrete pavement during construction.

5.1.2.2. *Unsuitable Soils*

Unsuitable soil types per the GB1, which include A-4b, A-2-5, A-5, A-7-5, A-8a, A-8b, and soils with liquid limits greater than 65, were encountered within the subgrade of the referenced project roadway segments. Soil Type A-4b (Silt) was encountered within four (4) borings performed along the project portion of IR-77. A summary of the prohibited soils encountered and the associated GB1 recommended remediation depths are shown in Tables 7 below.

Table 7: Prohibited Soils Location Summary

Boring ID	Prohibited Soil Type	Depth Below Subgrade (ft)	Remediation Depth (inches)	
			Excavate and Replace (Item 204 w/ Geotextile)	Chemical Stabilization (Item 206)
Ramp/Roadway Segment: IR-77				
B-013-0-20	A-4b	1.0 - 5.5	36	14
B-025-0-20	A-4b	0.0 - 3.0	36	14
B-026-0-20	A-4b	0.5 - 2.5	30	14
B-027-0-20	A-4b	1.5 - 3.0	36	14

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5.1.3. Unstable Soils

The GB1 recommends subgrade stabilization for soils considered unstable in which the N_{60} value of a particular soil sample (SS) at a referenced boring location is less than 12 bpf and in some cases less than 15 bpf (i.e., where moisture content is greater than optimum plus 3 percent). Based on the specific N_{60} value at the subject boring, *Figure B - Subgrade Stabilization* within the GB1 recommends a depth of subgrade stabilization for ODOT standard stabilization methods. It should be noted that although a soil sample's N_{60} value may meet the criteria to be considered an unstable soil, the depth in which the unstable soil is encountered in relation to the proposed subgrade is considered when each individual subgrade boring is analyzed. For example, if the GB1 recommends an excavate and replace of 12 inches within a weak soil underlying 18 inches of stable material, it would be unreasonable to recommend the removal of both the stable and unstable material for a total of 30 inches of excavate and replace.

Based on N_{60} values encountered within the project borings, our GB1 analysis suggests the need for 12 to 14 inches of chemical treatment or 12 to 15 inches excavate and replace at select locations. A summary of the boring locations where unstable soils were encountered and determined to have a potential impact on subgrade performance are shown in Table 8 below, per the roadway segment for which they were encountered. Also included is the associated GB1 recommended remediation depth at that location.

Table 8: Unstable Soil Locations Summary

Boring ID	Average HP (tsf)	N_{60}	Moisture Above Optimum (%)	Depth Below Subgrade (ft)	Remediation Depth (inches)		
					Excavate and Replace (Item 204 w/ Geotextile)	Excavate and Replace (Item 204 w/ Geogrid - SS 861)	Chemical Stabilization (Item 206)
Roadway Segment: IR-77							
B-011-0-20	1.75	-	4	0.0 - 1.5	12	-	12
B-022-0-20	-	10	-	0.0 - 1.0	12	-	14
B-025-0-20	-	14	7	0.0 - 3.0	12	-	12
B-026-0-20	-	11	-	0.0 - 0.5	12	-	12
B-028-0-20	-	11	3	0.0 - 1.5	12	-	12
B-032-0-20	-	5	-	0.0 - 0.8	12	-	12
B-035-0-20	-	10	-	0.0 - 0.4	12	-	12
B-036-0-20	-	10	3	0.0 - 0.9	12	-	12
B-037-0-20	-	14	4	0.0 - 1.5	12	-	12
B-038-0-20	-	10	-	0.0 - 0.8	12	-	12
B-039-0-20	-	11	-	0.0 - 0.8	12	-	12
B-044-0-20	-	7	-	0.0 - 3.9	15	-	14
B-046-0-20	-	11	3	0.0 - 1.5	12	-	12
B-053-0-20	-	7	-	0.0 - 1.5	15	-	14
B-054-0-20	-	8	-	0.0 - 0.7	12	-	12
B-055-0-20	1.5	10	3	0.0 - 0.1	12	-	12
B-058-0-20	-	11	-	0.0 - 1.5	12	-	12
B-061-0-20	2	8	-	0.0 - 4.0	12	-	14
B-063-0-20	-	11	3	0.0 - 1.2	12	-	12
Roadway Segment: Ramp L							
B-073-0-20	-	14	3	0.0 - 2.5	12	-	12
Roadway Segment: Ramps P & R							
B-071-0-20	-	8	7	0.0 - 1.5	12	-	14
Roadway Segment: Ramp S							
B-067-0-20	-	14	4	0.0 - 1.5	12	-	12

It should be noted that *Figure B - Subgrade Stabilization* does not apply to soil types A-1-a, A-1-b, A-3, or A-3a, nor to soils with N_{60L} values of 15 or more. Per GB1 guidance, *these soils should be reworked to stabilize the subgrade*.

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5.1.3.1. High Moisture Content Soils

High moisture content soils are defined by the GB1 as soils that exceed the estimated optimum moisture content (per *Figure A - Optimum Moisture Content* within the GB1) for a given classification by 3 percent or more. Per the GB1, soils determined to be above the identified moisture content levels are a likely indication of the presence of an unstable subgrade and may require some form of subgrade stabilization. Similar to our analysis of unstable soils, although a soil sample's moisture content may meet the criteria to be considered high, the depth in which the high moisture soil is encountered in relation to the proposed subgrade is considered when each individual subgrade boring is analyzed for stabilization recommendations. Summaries of the boring locations where high moisture content conditions were encountered in the top 3 ft of subgrade within the limits of each proposed roadway segment are shown in Table 9 below.

Table 9: High Moisture Content Soils Location Summary

Boring ID	Moisture Content (%)	Optimum Moisture Content (%)	Depth Below Subgrade (ft)	Boring ID	Moisture Content (%)	Optimum Moisture Content (%)	Depth Below Subgrade (ft)	
Roadway Segment: IR-77								
B-001-0-20	18	15	1.2 - 3.0	B-090-0-20	13	10	1.5 - 3.0	
B-006-0-20	17	10	1.1 - 2.6	B-091-0-20	17	10	1.5 - 3.0	
B-008-0-20	16	10	1.5 - 3.0	Roadway Segment: Ramp C				
B-009-0-20	16	12	1.5 - 3.0	B-084-0-20	17	14	0.0 - 1.5	
B-017-0-20	12	8	0.0 - 1.0	Roadway Segment: Ramp D				
B-021-0-20	17	12	1.5 - 3.0	B-086-0-20	13	10	1.5 - 3.0	
B-023-0-20	20	14	0.0 - 1.5	Roadway Segment: Ramp L				
B-026-0-20	26	14	0.5 - 2.5	B-075-0-20	25	12	0.0 - 1.5	
B-027-0-20	25	11	1.5 - 3.0	B-078-0-20	19	15	0.5 - 2.0	
B-031-0-20	14 & 21	10 & 12	0.0 - 3.0	Roadway Segment: Ramp M				
B-034-0-20	13	10	1.5 - 3.0	B-079-0-20	19	14	1.5 - 3.0	
B-043-0-20	16	10	1.5 - 3.0	Roadway Segment: Ramp P				
B-047-0-20	13	10	0.8 - 2.3	B-070-0-20	18	14	1.5 - 3.0	
B-053-0-20	19	16	1.5 - 3.0	Roadway Segment: Ramp S				
B-059-0-20	14	10	1.5 - 3.0	B-064-0-20	15 & 14	11	0.0 - 3.0	
				B-066-0-20	15 & 19	10 & 14	0.0 - 3.0	

5.2. Stabilization Recommendations

5.2.1. Subgrade Stabilization

Based on the results of our analysis, subgrade soils designated by ODOT's GB1 as both "unsuitable" and "unstable" were present at various locations throughout the project. Subgrade soils designated as "unsuitable" consisted of soils classifying as A-4b (Silt) and were encountered within subgrade depths that require remediation in four (4) borings (B-013-0-20 and B-025-0-20 through B-027-0-20) performed along IR-77. Subgrade soils designated as "unstable" were encountered at the various locations identified in Section 5.1.3 of this report. Although these materials were encountered throughout the site, guidance from ODOT's GB1 states that *"For all Interstates and other divided highways with four or more lanes more than 1-mile in project length, the subgrade of the entire project shall be chemically stabilized (global stabilization), except where it is determined that soil is present where a majority of sulfate content values are found to be greater than 3,000 parts per million (ppm), or individual soil samples with sulfate contents greater than 5,000 ppm are present"* and therefore global chemical stabilization is recommended for the proposed interstate interchange improvement project except where otherwise indicated in this report.

The global chemical stabilization of the referenced mainline and ramp subgrade soils included within this project, should be performed to a minimum depth of 12 inches utilizing cement as the stabilizing chemical.

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The stabilization efforts should extend a minimum of 18-inches beyond the edge of the paved roadway, shoulder or median. The mix design should be conducted in accordance with ODOT's CMS Supplement 1120 (Mixture Design for Chemically Stabilized Soils). For design purposes it may be assumed that the cement addition will be 5% using the following formula.

$$\text{Cement: } C = 0.75 \times T \times 115 \times 0.05$$

Where:

C = amount of chemical in pounds / square yard and

T = thickness of the treatment zone in inches

A dry density of 115-pounds per cubic foot (pcf) is assumed.

For areas where “unsuitable” A-4b (Silt) soils were encountered, it is recommended that either Excavate and Replace with geotextile (Item 204) be performed to a depth of 36 inches below the proposed top of subgrade, or chemical stabilization be performed to a depth of 14 inches. Our recommended limits for the indicated project subgrade stabilization are provided in Table 10 below.

Table 10: Stabilization Recommendations

Start Station	End Station	Excavate and Replace w/ Item 204 ⁽¹⁾ (inches)	Chemical Stabilization (inches)	Unsuitable Subgrade Conditions	Borings Considered
Entire Project					
Begin Work	End Work	12	14	N/A	-
IR-77 Northbound Lanes					
626+50 (CL IR-77)	631+00 (CL IR-77)	30	14	A-4b (Silt)	B-013-0-20
IR-77 Northbound and Southbound Lanes					
662+00 (CL IR-77)	674+50 (CL IR-77)	36	14	A-4b (Silt)	B-025-0-20, B-026-0-20, B-027-0-20

Notes:

1. Excavate and Replace depths for areas where Chemical Stabilization is not feasible.

It should be noted that per ODOT's GB1, *typical chemical stabilization equipment cannot stabilize areas less than 8 ft in width*. If it is anticipated that the project will require multiple maintenance of traffic phases, it is recommended that the roadway work is coordinated with the maintenance of traffic schemes in such a way that an 8-ft minimum width for chemical stabilization exists. If areas of less than 8 ft in width are anticipated, subgrade soils may be excavated out, mixed with stabilization chemical, and compacted in place, though this method is not practical for large areas

5.3. Embankment Stability Analysis

At the time of this report, project required embankment fills, sliver fills, or fills required for roadway widening purposes have not been identified. Following the development of project proposed cross-sections and the determination of required fills, NEAS will review the provided information for embankment stability. This review will also include fills potentially placed near the identified project lowland/wetland located within the vicinity of borings B-092-0-20 through B-097-0-20.

5.3.1. Embankment Construction Recommendations

In areas where additional embankment material is proposed along existing slopes (i.e., side-hill sliver fills) that are steeper than 8H:1V but flatter than 4H:1V, it is recommended that the proposed embankment be benched into the existing slopes in accordance with Item 203.05 “Embankment Construction Methods” of

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the ODOT CMS. For areas where additional embankment material is proposed along existing slopes that are steeper than 4H:1V, it is recommended that the proposed embankment be designed and constructed in accordance with ODOT's GB2. For sidehill fills planned on existing slopes steeper than 4H:1V, ODOT's GB2 recommends that *the embankment slopes be constructed utilizing special benching in order to blend the new embankment with the existing slope to prevent the development of a weak shear plane at the interface between the proposed fill and existing slope material* (ODOT [2], 2017). As proposed cross-sections are not available at this time, at this stage of the project a special benching scheme similar to that shown in Figures 1, 2 or 3, as appropriate, of the ODOT GB2 should be used in areas where special benching is recommended. The height and width dimensions of the special benching scheme shown in these figures should be arranged to minimize the required cut and fill quantities, though the height of a single bench shall not exceed 20 ft without a stability analysis and design per OSHA requirements. Additionally, it may be appropriate to adjust the bench slope shown from a 1H:1V to a 1.75H:1V slope if the existing slope is made up of primarily granular materials. The benched material should be replaced with compacted engineered fill per Item 203 of the ODOT CMS, while proper lift thicknesses and material density should be maintained in the proposed fill per Item 203.06 of the ODOT CMS. In situations where it is not practical to extend the final bench through the existing roadway due to maintenance of traffic concerns, a benching scheme similar to that shown in Figure 1a of the ODOT GB2 can be used in order to avoid impacting the existing roadway, guardrail or shoulder. This scheme results in the placement of a temporary over-steepened fill that can later be "shaved-off" to bring the slope to the final proposed grade.

5.4. Noise Wall Foundation Design

This section provides information required to complete the design of 30-inch diameter drilled shaft noise wall supports. The geotechnical information has been developed in accordance with the ODOT BDM, Section 802.1.2. ODOT design methodology requires that the N_{60} values of the granular soils be corrected using a factor to account for the depth of each test, and the results analyzed to determine a mean (average N_{60}/N_{160}) or minimum (N_{60L}/N_{160L}) depending on the trend of the data and the specific soil type (i.e., granular or cohesive). Using the broad distinction between cohesive and granular soils, the mean or minimum is then used (designated as the design N_{160} herein) together with the proposed wall geometry to determine the depth of shaft required at that boring location based on the design tables provided in the ODOT BDM. As several sampling intervals may have not aligned with those shown in the ODOT BDM, linear interpolation was used to acquire N_{160} correction factors for unlisted depths. This analysis is presented within Appendices G and H.

The ODOT shaft design method should be a two-step process if the design is to be optimized. This process is described below using boring B-073-0-20 as an example and a noise wall with post spacing of 12 ft and a height of 15 ft. Level ground and no cut or fill is assumed for the example as well.

The design N_{160} value for B-073-0-20 is 8, based on the lowest value as the values are dissimilar and do not increase with depth. Furthermore, the plasticity index is less than 7 where the N_{160} value of 8 occurs (see boring log in Appendix C); therefore, the material is considered granular. Consulting the ODOT BDM Figure 802.1.2-1 for the conditions of a barrier height of 15 ft, a post spacing of 12 ft, a design N_{160} of 8, and a level ground condition, the shaft length is 11 ft.

Reviewing Appendix H for a situation where the foundation depth is 11 ft shows that the soils along a shaft of this length would be predominantly cohesive and would have a design N_{160} value of 8. Tables indicating design N_{160} value for various design shafts depth (i.e., 6 ft, 8 ft, 10 ft, etc.) per boring are provided in Appendix H. Referring to Figure 802.1.2-2 due to the soil at 11 ft being cohesive in nature, considering of a barrier height of 15 ft, a post spacing of 12 ft, and a design N_{160} value of 8, and a level ground condition,

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the shaft length should be increased to 13.5 ft. Subsequent iterations are performed until the design N_{60} value or predominant soil type is not altered further after a change in the shaft length is determined. The ultimate result of these iterations for the example case using Boring B-073-0-20 is a design N_{60} value of 8 with predominantly cohesive soils along the shaft, yielding a shaft length of 13.5 ft.

At the time of this report the proposed noise wall grades (i.e., top of shaft elevations) were not available for review. Furthermore, if significant amounts of cuts or fills of the soils along the noise wall alignments are anticipated, the foundation design should be reviewed, and our analysis be updated to reflect the actual soil profiles along the proposed wall alignment.

The conditions reflected at each boring in Appendices G and H were observed at those locations only and may not be indicative of conditions at intermediate points between borings. However, for purposes of design it is recommended that the supports be sized based on conditions at the nearest boring. In other terms, each boring may be considered representative of sub-surface conditions up to half the distance to the next nearest boring away for design purposes.

5.4.1. Drilled Shaft Depths

Utilizing the design methodology presented in Section 5.4 of this report and in accordance with Section 800 "Noise Barriers" of the ODOT BDM, the drilled shaft design depths for the project noise walls are to be determined by the GPD Group. These drilled shaft depth calculations will be provided to ODOT as part of a separate submission.

5.4.2. Drilled Shaft Construction Considerations

Due to the observed cave-in depth of the noise wall borings performed at the site, it is anticipated that the holes bored for shaft construction will generally remain stable without the need for casing at the majority of the shaft locations so long as shaft lengths are not towards the upper bound of allowable length per the noted cave-in depths below. It should be noted that boring B-074-0-20 was indicated to have cave-in at a depth of 4 ft. Furthermore, with the exception of borings B-075-0-20 and B-078-0-20, groundwater was encountered in each of the noise wall borings performed at depths between 14.0 and 19.2 ft bgs. Each of these factors could be an indication that cave-in may occur, especially when extending the shaft below groundwater depths. If shaft termination elevations are determined to be below the groundwater level encountered within the adjacent borings, consideration to the presence of groundwater should be made in the construction of the shaft.

5.5. Light Pole Foundations Recommendations

It is our understanding that a total of fifteen (15) new high mast light poles are proposed as part of the project. To aide in the evaluation of light pole foundation design, the boring logs located adjacent to proposed light pole locations were reviewed, and a generalized material profile was developed. Utilizing the generalized soil profile, engineering properties (i.e., shear strength and unit weight) including properties for lateral load analysis (i.e., LPILE analysis) for each soil strata were estimated based on their field (i.e., SPT N_{60} values, hand penetrometer values, etc.) and laboratory (i.e., Atterberg Limits, grain size, etc.) test results using correlations provided in published engineering manuals, research reports and guidance documents. The developed soil profile and estimated engineering soil properties for evaluation of proposed signal pole foundations (with sited correlation/reference material) are summarized within Table 11 below.

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Table 11: Shear Strength and LPILE Parameters at Light Pole Locations

Shear Strength and LPILE Parameters							
Boring Number	p-y model	Elevation (ft-amsl)	Effective Unit Weight ⁽¹⁾ (pcf)	Friction Angle ⁽²⁾ (degrees)	Undrained Shear Strength ⁽³⁾ (psf)	Lateral Soil Modulus Parameter, k (pci)	Soil Strain Parameter, E ₅₀ (%)
B-001-1-20	Sand (Reese)	1012.6 - 1005.6	135	40	-	650	-
	Stiff Clay w/o Water	1005.6 - 988.1	125	27	2,650	890	0.0054
	Sand (Reese)	988.1 - 986.1	120	27	-	13	-
B-002-1-20	Sand (Reese)	1010.4 - 1003.4	125	36	-	220	-
	Sand (Reese)	1003.4 - 998.4	122	35	-	180	-
	Sand (Reese)	998.4 - 995.9	120	28	-	22	-
	Sand (Reese)	995.9 - 988.4	125	34	-	140	-
	Stiff Clay with Water	988.4 - 983.9	67	26	2,300	770	0.0058
B-004-1-20	Sand (Reese)	1011.3 - 1001.8	120	31	-	60	-
	Stiff Clay w/o Water	1001.8 - 999.3	118	23	1,000	220	0.0095
	Stiff Clay w/o Water	999.3 - 997.8	118	22	1,000	220	0.0095
	Sand (Reese)	997.8 - 993.8	120	31	-	60	-
	Stiff Clay w/o Water	993.8 - 989.3	122	25	2,000	660	0.0062
	Sand (Reese)	989.3 - 984.8	128	37	-	150	-
B-006-1-20	Sand (Reese)	997.0 - 990.5	118	27	-	15	-
	Soft Clay	990.5 - 985.0	112	19	500	55	0.0155
	Stiff Clay with Water	985.0 - 977.5	118	25	2,375	790	0.0057
	Sand (Reese)	977.5 - 975.0	66	35	-	100	-
	Sand (Reese)	975.0 - 970.5	68	39	-	205	-
B-008-1-20	Stiff Clay w/o Water	1006.1 - 996.6	122	25	1,950	650	0.0063
	Sand (Reese)	996.6 - 994.1	128	38	-	350	-
	Sand (Reese)	994.1 - 991.6	118	27	-	15	-
	Soft Clay	991.6 - 989.1	115	21	625	85	0.0132
	Sand (Reese)	989.1 - 984.1	128	38	-	350	-
	Sand (Reese)	984.1 - 979.6	125	32	-	85	-
B-009-1-20	Sand (Reese)	997.5 - 988.0	122	35	-	180	-
	Stiff Clay w/o Water	988.0 - 985.5	125	27	2,500	830	0.0056
	Stiff Clay w/o Water	985.5 - 981.5	122	25	1,800	600	0.0066
	Sand (Reese)	981.5 - 971.0	67	30	-	35	-
B-011-1-20	Stiff Clay w/o Water	1003.4 - 998.9	122	24	1,875	625	0.0065
	Sand (Reese)	998.9 - 993.9	122	33	-	105	-
	Stiff Clay w/o Water	993.9 - 991.4	120	23	1,250	350	0.0082
	Sand (Reese)	991.4 - 986.4	128	38	-	350	-
	Sand (Reese)	986.4 - 976.9	60	31	-	45	-
B-013-1-20	Stiff Clay w/o Water	997.5 - 993.0	122	25	1,750	580	0.0067
	Sand (Reese)	993.0 - 990.5	132	42	-	800	-
	Stiff Clay w/o Water	990.5 - 980.5	120	23	1,350	400	0.0079
	Sand (Reese)	980.5 - 978.0	122	30	-	45	-
	Stiff Clay with Water	978.0 - 971.0	118	23	960	200	0.0098
B-014-1-20	Stiff Clay w/o Water	996.3 - 981.3	120	23	1,475	480	0.0074
	Sand (Reese)	981.3 - 974.3	125	36	-	225	-
	Sand (Reese)	974.3 - 969.8	125	34	-	140	-
B-016-1-20	Sand (Reese)	979.3 - 969.8	120	33	-	105	-
	Stiff Clay w/o Water	969.8 - 967.3	122	26	2,250	750	0.0059
	Sand (Reese)	967.3 - 957.3	122	32	-	80	-
	Stiff Clay with Water	957.3 - 952.8	120	24	1,685	560	0.0069

Notes:

1. Values interpreted from Geotechnical Bulletin 7 Table 1.
2. Values calculated from Terzaghi and Peck (1967) if $N_{1\text{ a0}} < 52$, else Stroud and Butler (1975) was used.
3. Values interpreted from Geotechnical Bulletin 7 Table 2.

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Table 11 Continued: Shear Strength and LPILE Parameters at Light Pole Locations

Shear Strength and LPILE Parameters							
Boring Number	p-y model	Elevation (ft-amsl)	Effective Unit Weight ⁽¹⁾ (pcf)	Friction Angle ⁽²⁾ (degrees)	Undrained Shear Strength ⁽³⁾ (psf)	Lateral Soil Modulus Parameter, k (pci)	Soil Strain Parameter, E ₅₀ (%)
B-019-1-20	Stiff Clay w/o Water	966.6 - 962.1	122	25	2,000	665	0.0062
	Sand (Reese)	962.1 - 940.1	120	33	-	110	-
B-022-1-20	Stiff Clay w/o Water	954.4 - 939.9	120	24	1,650	550	0.0069
	Stiff Clay w/o Water	939.9 - 934.9	120	24	1,500	500	0.0073
	Stiff Clay w/o Water	934.9 - 932.4	120	22	1,250	350	0.0082
	Sand (Reese)	932.4 - 927.9	122	32	-	85	-
B-023-1-20	Sand (Reese)	946.2 - 941.7	128	38	-	350	-
	Stiff Clay w/o Water	941.7 - 924.2	122	24	1,750	580	0.0067
	Sand (Reese)	924.2 - 919.7	125	32	-	85	-
B-070-1-20	Sand (Reese)	1007.0 - 1000.0	120	31	-	60	-
	Sand (Reese)	1000.0 - 997.0	122	33	-	110	-
	Sand (Reese)	997.0 - 980.5	125	36	-	225	-
B-071-1-20	Sand (Reese)	1000.1 - 993.1	122	32	-	80	-
	Sand (Reese)	993.1 - 988.1	122	33	-	105	-
	Sand (Reese)	988.1 - 973.6	122	34	-	140	-

Notes:

1. Values interpreted from Geotechnical Bulletin 7 Table 1.
2. Values calculated from Terzaghi and Peck (1967) if $N_{160} < 52$, else Stroud and Butler (1975) was used.
3. Values interpreted from Geotechnical Bulletin 7 Table 2.

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6. QUALIFICATIONS

This investigation was performed in accordance with accepted geotechnical engineering practice for the purpose of characterizing the subsurface conditions along the referenced portions of roadways. This report has been prepared for GPD, ODOT and their design consultants to be used solely in evaluating the roadway embankment and subgrade soils within the project limits and presenting geotechnical engineering recommendations specific to this project. The assessment of general site environmental conditions or the presence of pollutants in the soil, rock and groundwater of the site was beyond the scope of this geotechnical exploration. Our recommendations are based on the results of our field explorations, laboratory tests results from representative soil samples, and geotechnical engineering analyses. The results of the field explorations and laboratory tests, which form the basis of our recommendations, are presented in the appendices as noted. This report does not reflect any variations that may occur between the borings or elsewhere on the site, or variations whose nature and extent may not become evident until a later stage of construction. In the event that any changes occur in the nature, design or location of the proposed interstate improvement work, the conclusions and recommendations contained in this report should not be considered valid until they are reviewed, and have been modified or verified in writing by a geotechnical engineer.

It has been a pleasure to be of service to GPD Group in performing this geotechnical exploration for the SUM-77- 24.12 Ghent Rd interstate improvement project. Please call if there are any questions, or if we can be of further service.

Respectfully Submitted,

Brendan P. Andrews, P.E.
Project Geotechnical Engineer

Kevin C. Arens, P.E.
Geotechnical Engineer

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APPENDIX A

ODNR OIL AND GAS WELL REPORTS

WELL SUMMARY

ODNR DIVISION OF OIL & GAS RESOURCES MANAGEMENT

API Well Number	34153220510000						Permit Issued	1/6/2004						
Well Name	LASALLE UNIT		Acres	28.7722	Well No.	1	Date Commenced	6/25/1985						
Owner	DIVERSIFIED PRODUCTION LLC				Well No.	3352001	Date Completed	7/2/1985						
Logging Co.	Eastern		Core No.	Sample No.										
County	SUMMIT	Township	BATH	Quadrangle	WEST RICHFIELD		Zone	N						
Section	Lot	46	Tract	Twp. Qtr.	Surface X	2240250 Y 549980	Bottom X	Y NAD27						
					Surface Lon	-81.627306 Lat 41.172983	Bottom Lon	Lat NAD27						
Measured	895' NL & 153' EL OF LOT 46			Surface X	2208786 Y 550010	Bottom X	Y NAD83 SPS							
				Prop TD	3709	Class	POOL	Tool SERV						
GL	1030	DF	KB	1035 LTD	3709	DTD	PB Depth	Date PB						
TD Form.	QUEENSTON FORMATION			Prod. Form.	CLINTON GROUP		Status	Producing						
IP Natural	1 MCF & 1 BO	IP AT	10 MCF & 10 BO & 1 BW		Initial Rock Pressure		Date Abandoned							
Perforations	PI: 3517-3586, # Shots: 32 PI: 3496-3588, Csg: PROD, Cmmnt:													
Stimulations	SI: 0-0, Fmtn Cd: 357170, Type: H2O, Vol: 1500 Bbl, #Prop: 50000, Cmmnt: SI: 0-0, Type: N2, Vol: 190 Mscf, Cmmnt:													
Casing Record	SURF 8.625 0-465, Comment: PROD 4.5 0-3665, Comment:													
Log Types														

Formations

Formation	Top	Bottom	Source	Prod.	Non-Standard	Remarks
BIG LIME	1916	3376	Driller	No		
ORISKANY SANDSTONE	2130	2180	Driller	No		
PACKER SHELL	3450	3475	Driller	No		
CLINTON SAND	3496	3588	Driller	Yes		
MEDINA SAND	3588	3670	Driller	No		
QUEENSTON FORMATION	3670		Driller	No		

Annual Production

Year	Quarter	Source	Oil	Gas	Water	Remarks
1986	N\A	RBDMS	983	19502	180	
1987	N\A	RBDMS	448	15589	70	
1988	N\A	RBDMS	270	9249	45	
1989	N\A	RBDMS	277	7312	40	
1990	N\A	RBDMS	138	3183	30	
1991	N\A	RBDMS	215	5582	40	
1992	N\A	RBDMS	68	3241	35	
1993	N\A	RBDMS	151	4733	39	
1994	N\A	RBDMS	89	4122	117	
1995	N\A	RBDMS	182	4246	125	
1996	N\A	RBDMS	0	3857	25	
1997	N\A	RBDMS	162	4070	92	
1998	N\A	RBDMS	78	4963	54	
1999	N\A	RBDMS	117	2682	26	
2000	N\A	RBDMS	0	1536	21	
2001	N\A	RBDMS	104	361	6	
2002	N\A	RBDMS	9	0	0	
2002	N\A	RBDMS	9	0	0	
2002	N\A	RBDMS	0	0	0	
2003	N\A	RBDMS	0	0	0	

2004	N\A	RBDMS	0	0	0
2005	N\A	RBDMS	0	0	0
2006	N\A	RBDMS	0	0	0
2007	N\A	RBDMS	0	304	3
2008	N\A	RBDMS	0	770	0
2009	N\A	RBDMS	0	409	0
2010	N\A	RBDMS	0	289	0
2011	N\A	RBDMS	0	678	0
2012	N\A	RBDMS	0	692	0
2013	N\A	RBDMS	0	709	60
2014	N\A	RBDMS	120	629	0
2015	N\A	RBDMS	0	337	0
2016	N\A	RBDMS	0	246	0
2017	N\A	RBDMS	0	1	0
2018	N\A	RBDMS	0	0	0
2019	N\A	RBDMS	0	81	0

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WELL SUMMARY

ODNR DIVISION OF OIL & GAS RESOURCES MANAGEMENT

API Well Number	34153226610000										Permit Issued	5/16/1990																
Well Name	BILLMAN										Date Commenced	8/28/1990																
Owner	ST CROIX LTD										Date Completed	9/3/1990																
Logging Co.	Eastern										Sample No.																	
County	SUMMIT	Township	BATH			Quadrangle	WEST RICHFIELD				Zone	N																
Section	Lot	75	Tract			Twp. Qtr.	Surface X	2239950	Y	543230	Bottom X	Y	NAD27															
							Surface Lon	-81.628641	Lat	41.154465	Bottom Lon	Lat	NAD27															
Measured	385'NL & 225'EL OF LOT 75										Surface X	2208486	Y	543260	Bottom X	Y	NAD83 SPS											
							Prop TD				Class	POOL	Tool	RTF														
GL	930	DF	KB	935	LTD	3624	DTD	3631	PB Depth		Date PB																	
TD Form.	QUEENSTON FORMATION					Prod. Form.	CLINTON GROUP				Status	Producing																
IP Natural		IP AT	20 MCF & 3 BO				Initial Rock Pressure				Date Abandoned																	
Perforations	PI: 3439-3469, # Shots: 35PI: 3405-3470, Csg: PROD, Cmmnt:																											
Stimulations	SI: 0-0, Fmtn Cd: 357170, Type: H2O, Vol: 105175 Gal, #Prop: 56000, Cmmnt:																											
Casing Record	SURF 8.625 0-433, Comment: PROD 4.5 0-3602, Comment:																											
Log Types																												

Formations

Formation	Top	Bottom	Source	Prod.	Non-Standard	Remarks
BIG LIME	1830	3300	Driller	No		
PACKER SHELL	3371	3401	Driller	No		
CLINTON SAND	3405	3470	Driller	Yes		
QUEENSTON FORMATION	3592		Driller	No		

Annual Production

Year	Quarter	Source	Oil	Gas	Water	Remarks
1990	N\A	RBDMS	993	2280	2136	
1991	N\A	RBDMS	1708	3923	1227	
1992	N\A	RBDMS	957	2516	297	
1993	N\A	RBDMS	400	3160	284	
1994	N\A	RBDMS	260	1399	218	
1995	N\A	RBDMS	116	723	157	
1996	N\A	RBDMS	304	3179	282	
1997	N\A	RBDMS	410	3035	254	
1998	N\A	RBDMS	231	664	306	
1999	N\A	RBDMS	110	501	422	
2000	N\A	RBDMS	160	515	346	
2001	N\A	RBDMS	149	708	330	
2002	N\A	RBDMS	86	756	327	
2003	N\A	RBDMS	112	468	462	
2004	N\A	RBDMS	90	468	253	
2005	N\A	RBDMS	109	492	158	
2006	N\A	RBDMS	68	455	188	
2007	N\A	RBDMS	114	424	276	
2008	N\A	RBDMS	99	407	130	
2009	N\A	RBDMS	56	344	85	
2010	N\A	RBDMS	0	323	0	
2011	N\A	RBDMS	21	336	45	

2012	N\A	RBDMS	17	353	162
2013	N\A	RBDMS	16	342	92
2014	N\A	RBDMS	10	247	101
2015	N\A	RBDMS	22	238	87
2016	N\A	RBDMS	0	0	0
2017	N\A	RBDMS	0	0	0
2018	N\A	RBDMS	0	0	0

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WELL SUMMARY

ODNR DIVISION OF OIL & GAS RESOURCES MANAGEMENT

API Well Number	34153227360000						Permit Issued	11/15/1991					
Well Name	DITOMMASO		Acres	23	Well No.	1	Date Commenced	2/10/1992					
Owner	TRANSCONTINENTAL OIL & GAS INC				Well No.		Date Completed	2/15/1992					
Logging Co.	Renegade Services, Eastern		Core No.		Sample No.								
County	SUMMIT	Township	BATH		Quadrangle	WEST RICHFIELD	Zone	N					
Section	Lot 54 Tract		Twp. Qtr.		Surface X	2240425 Y 546800	Bottom X	Y	NAD27				
Measured	700'SL & 301'WL OF LOT 54				Surface Lon	-81.626786 Lat 41.164250	Bottom Lon	Lat	NAD27				
					Surface X	2208961 Y 546830	Bottom X	Y	NAD83 SPS				
					Prop TD		Class	POOL	Tool				
GL	985	DF	KB	990 LTD	4716	DTD	3717	PB Depth	Date PB				
TD Form.	QUEENSTON FORMATION			Prod. Form.	CLINTON GROUP		Status	Producing					
IP Natural	IP AT 50 MCF & 2 BO & 1 BW				Initial Rock Pressure		1100	Date Abandoned					
Perforations	PI: 3530-3574, # Shots: 25PI: 3506-3612, Csg: PROD, Cmmnt:												
Stimulations	SI: 0-0, Fmtn Cd: 357170, Type: ACID, Vol: 500 Gal, #Prop: 70000, MISIP: 1100, BHP: 1000, Cmmnt: SI: 0-0, Type: N2, Vol: 250 Mscf, MISIP: 1000, BHP: 1000SI: 0-0, Type: H2O, Vol: 2400 Bbl, MISIP: 1000, BHP: 1000, Cmmnt:												
Casing Record	SURF 8.625 0-403, Comment: PROD 4.5 0-3684, Comment:												
Log Types	Perforating Depth Control, Perforating												

Formations

Formation	Top	Bottom	Source	Prod.	Non-Standard	Remarks
BIG LIME	1912	3388	Driller	No		
PACKER SHELL	3458	3489	Driller	No		
CLINTON SAND	3506	3612	Driller	Yes		
QUEENSTON FORMATION	3678		Driller	No		

Annual Production

Year	Quarter	Source	Oil	Gas	Water	Remarks
1992	N\A	RBDMS	0	0	100	
1993	N\A	RBDMS	0	0	0	
1994	N\A	RBDMS	0	0	0	
1995	N\A	RBDMS	0	0	0	
1996	N\A	RBDMS	7380	26989	957	
1997	N\A	RBDMS	4839	36704	113	
1998	N\A	RBDMS	3439	29533	74	
1999	N\A	RBDMS	2287	23317	61	
2000	N\A	RBDMS	2464	14952	45	
2001	N\A	RBDMS	1809	14377	0	
2002	N\A	RBDMS	1465	13431	0	
2003	N\A	RBDMS	1396	11229	20	
2004	N\A	RBDMS	1246	10058	0	
2005	N\A	RBDMS	976	8338	0	
2006	N\A	RBDMS	938	6143	0	
2007	N\A	RBDMS	806	5424	40	
2008	N\A	RBDMS	1466	9707	105	
2009	N\A	RBDMS	1126	11656	51	
2010	N\A	RBDMS	1084	9389	61	
2011	N\A	RBDMS	833	8687	0	
2012	N\A	RBDMS	522	8765	0	
2013	N\A	RBDMS	361	7306	37	
2014	N\A	RBDMS	546	5917	52	

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<https://gis.ohiodnr.gov/MapViewer/WellSummaryCard.asp?api=34153227360000>

2015	N\A	RBDMS	381	5491	0
2016	N\A	RBDMS	361	5000	0
2017	N\A	RBDMS	348	4208	0
2018	N\A	RBDMS	428	3756	80
2019	N\A	RBDMS	325	3675	141

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WELL SUMMARY

ODNR DIVISION OF OIL & GAS RESOURCES MANAGEMENT

API Well Number	34153227880000						Permit Issued	3/31/1995								
Well Name	FARR		Acres	20		Well No.	1		Date Commenced	9/21/1995						
Owner	ST CROIX LTD					Well No.			Date Completed	9/28/1995						
Logging Co.	Eastern		Core No.			Sample No.										
County	SUMMIT	Township	BATH	Quadrangle	WEST RICHLFIELD				Zone	N						
Section	Lot 67 Tract		Twp. Qtr.	Surface X 2240700 Y 544400 Bottom X 2240950 Y 544944 NAD27 Surface Lon -81.625875 Lat 41.157656 Bottom Lon -81.624947 Lat 41.159142 NAD27												
Measured	1664 NL & 562 WL OF LOT 67				Surface X	2209236	Y	544430	Bottom X	2209486	Y	544974 NAD83 SPS				
	Target: 1120' NL & 810' WL OF LOT 67				Prop TD	0			Class	POOL	Tool	RTAF				
GL	900	DF	KB	LTD	3670	DTD	3695	PB Depth				Date PB				
TD Form.	CABOT HEAD SHALE			Prod. Form.	CLINTON GROUP			Status	Producing							
IP Natural	IP AT 10 MCF & 5 BO			Initial Rock Pressure				Date Abandoned								
Perforations	PI: 3535-3585, # Shots: 40 PI: 3517-3595, Csg: PROD, Cmmnt:															
Stimulations	SI: 0-0, Fmtn Cd: 357170, Type: H2O, Vol: 121000 Gal, #Prop: 62500, Cmmnt:															
Casing Record	SURF 8.625 0-342, Comment: PROD 4.5 0-3687, Comment:															
Log Types																

Formations

Formation	Top	Bottom	Source	Prod.	Non-Standard	Remarks
BIG LIME	1804	3390	Driller	No		
PACKER SHELL	3466	3500	Driller	No		
CLINTON SAND	3517	3595	Driller	Yes		
CABOT HEAD SHALE	3595		Driller	No		

Annual Production

Year	Quarter	Source	Oil	Gas	Water	Remarks
1997	N\A	RBDMS	627	4998	541	
1998	N\A	RBDMS	681	5716	140	
1999	N\A	RBDMS	706	5162	139	
2000	N\A	RBDMS	698	4887	379	
2001	N\A	RBDMS	664	3542	41	
2002	N\A	RBDMS	390	2299	47	
2003	N\A	RBDMS	405	1718	29	
2004	N\A	RBDMS	380	1817	62	
2005	N\A	RBDMS	293	1829	78	
2006	N\A	RBDMS	330	1763	110	
2007	N\A	RBDMS	346	1787	120	
2008	N\A	RBDMS	344	1574	160	
2009	N\A	RBDMS	334	1295	90	
2010	N\A	RBDMS	216	1516	196	
2011	N\A	RBDMS	276	1395	101	
2012	N\A	RBDMS	209	1498	95	
2013	N\A	RBDMS	202	1451	64	
2014	N\A	RBDMS	117	979	38	
2015	N\A	RBDMS	88	522	54	
2016	N\A	RBDMS	0	0	0	
2017	N\A	RBDMS	0	0	0	
2018	N\A	RBDMS	0	0	0	

8/17/2020

<https://gis.ohiodnr.gov/MapViewer/WellSummaryCard.asp?api=34153227880000>

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WELL SUMMARY

ODNR DIVISION OF OIL & GAS RESOURCES MANAGEMENT

API Well Number	34153228690000						Permit Issued	10/7/1997							
Well Name	FARR		Acres	21.26	Well No.	2	Date Commenced	12/19/1997							
Owner	ST CROIX LTD		Well No.		Date Completed		12/30/1997								
Logging Co.	Superior Well Services		Core No.	Sample No.											
County	SUMMIT	Township	BATH	Quadrangle	WEST RICHFIELD			Zone	N						
Section	Lot 67 Tract		Twp. Qtr.	Surface X 2241000 Y 544330 Bottom X 2240720 Y 545780 NAD27 Surface Lon -81.624788 Lat 41.157455 Bottom Lon -81.625752 Lat 41.161443 NAD27											
Measured	1825' NL & 668' WL OF LOT 67			Surface X 2209536 Y 544360 Bottom X 2209256 Y 545810 NAD83 SPS											
	Target: 302' NL & 413' WL OF LOT 67			Prop TD	0	Class	POOL	Tool	RTAF						
GL	940	DF	KB	LTD	4184	DTD	4215	PB Depth	Date PB						
TD Form.	QUEENSTON FORMATION			Prod. Form.	CLINTON GROUP			Status	Producing						
IP Natural	IP AT 10 MCF & 5 BO			Initial Rock Pressure			Date Abandoned								
Perforations	PI: 3940-4018, S/Ft: 53, # Shots: 53														
Stimulations	SI: 3940-4018, Fmtn Cd: 357170, Stim In: CS, Type: H2O, Vol: 51503 Gal, #Prop: 68100, MBP: 1428, MTP: 1760, MISIP: 1473, 5SIP: 1297														
Casing Record	SURF 8.625 0-377-0, Comment: , Sks: 150 PROD 4.5 0-4203, Comment: , Sks: 140														
Log Types	Cased hole neutron, Casing collar locator/Gamma ray, Gamma Ray, Neutron														

Formations

Formation	Top	Bottom	Source	Prod.	Non-Standard	Remarks
GLACIAL DEPOSITS	0	120	Driller	No		
BIG LIME	1821	3766	Log	No		
PACKER SHELL	3867	3896	Log	No		
CLINTON SAND	3914	3995	Log	Yes		
QUEENSTON FORMATION	4117		Log	No		

Annual Production

Year	Quarter	Source	Oil	Gas	Water	Remarks
1999	N\A	RBDMS	113	0	400	
2000	N\A	RBDMS	1716	3359	199	
2001	N\A	RBDMS	937	2750	186	
2002	N\A	RBDMS	449	1760	93	
2003	N\A	RBDMS	407	1738	29	
2004	N\A	RBDMS	428	1817	62	
2005	N\A	RBDMS	335	1540	131	
2006	N\A	RBDMS	300	1308	110	
2007	N\A	RBDMS	277	1312	76	
2008	N\A	RBDMS	290	1303	113	
2009	N\A	RBDMS	166	1213	48	
2010	N\A	RBDMS	165	1085	131	
2011	N\A	RBDMS	141	1139	67	
2012	N\A	RBDMS	200	1148	81	
2013	N\A	RBDMS	194	1112	55	
2014	N\A	RBDMS	112	860	32	
2015	N\A	RBDMS	83	687	38	
2016	N\A	RBDMS	0	0	0	
2017	N\A	RBDMS	0	0	0	
2018	N\A	RBDMS	0	0	0	

APPENDIX B

BORING LOCATION PLAN

DRAWN
KCA
CHECKED
BPA

SUM-77-24.12

1
8BORING LOCATION PLAN
SUM-77-24.12 GHENT ROAD



BORING LOCATION PLAN
SUM-77-24.12 GHENT ROAD

SUM-77-24.12

2
8

DRAWN
KCA
CHECKED
BPA
HORIZONTAL
SCALE IN FEET



LEGEND

BORING LOCATION



N

4
8

TARGET BORING PLAN

SUM-77-24.12

DRAWN	0
ZM	100
CHECKED	50
CH	200

HORIZONTAL SCALE IN FEET

B-032-0-20

P.C.-7

B-033-0-20

P.C.-8

P.C.-9

P.C.-10

B-034-0-20

W BATH RD

B-035-0-20

B-036-0-20

SUM-77 NORTHBOUND

SUM-77 SOUTHBOUND

B-037-0-20

B-038-0-20



LEGEND

BORING LOCATION



DRAWN
ZM
CHECKED
CH
HORIZONTAL
SCALE IN FEET
200
100
50

TARGET BORING PLAN
SUM-77

SUM-77-24.12

B-047-0-20

B-048-0-20

B-049-0-20

B-050-0-20
SUM-77 NORTHBOUND

B-051-0-20

SUM-77 SOUTHBOUND

P.C.-12
P.C.-13
P.C.-14
P.C.-15

B-052-0-20
B-053-0-20

IRA RD



DRAWN
ZM
CHECKED
CH100
50
0
HORIZONTAL
SCALE IN FEET

TARGET BORING PLAN

SUM-77, RAMP A, B, C & D

SUM-77-24.12

7
8

LEGEND
BOARING LOCATIONDRAWN
ZM
CHECKED
CH100
50
0
HORIZONTAL
SCALE IN FEETTARGET BORING PLAN
SUM-77

SUM-77-24.12



APPENDIX C

BORING LOGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 300+01, 18' LT.	EXPLORATION ID B-001-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77 NB																
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1012.4 (MSL)	PAGE															
START: 8/25/20 END: 8/25/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.145999, -81.638665	1 OF 1															
MATERIAL DESCRIPTION AND NOTES	ELEV. 1012.4	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI				
10.0" ASPHALT AND 8.0" BASE (DRILLERS DESCRIPTION)	1010.9			1															
MEDIUM DENSE, BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, DAMP (FILL)	1009.7			2	6	SS-1A	-	35	20	23	16	6	NP	NP	NP	8	A-1-b (0)	<100	
VERY STIFF TO HARD, BROWNISH GRAY AND BROWN, SILT AND CLAY, TRACE SAND, TRACE GRAVEL, CONTAINS TRACE IRON STAINING, DAMP	1004.9	EOB		3	5	SS-1B	4.50	-	-	-	-	-	-	-	-	17	A-6a (V)	-	
				4	6	SS-2	3.75	1	1	3	54	41	33	20	13	18	A-6a (9)	-	
				5	7	SS-3	4.50	-	-	-	-	-	-	-	-	15	A-6a (V)	-	
				6	10											15	A-6a (V)	-	
				7	12	SS-4	4.50	-	-	-	-	-	-	-	-				

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 403+91, 3' LT.	EXPLORATION ID: B-002-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77 SB																
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1012.2 (MSL) EOB: 7.5 ft.	PAGE: 1 OF 1															
START: 11/24/20 END: 11/24/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.146716, -81.637602																
MATERIAL DESCRIPTION AND NOTES	ELEV. 1012.2	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI				
LOOSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CLAY, DAMP																			
				1															
				2															
				3	3	10	33	SS-1	-	-	-	-	-	-	-	10	A-3a (V)	<100	
				4	4														
				8	12	33	44	SS-2	4.50	6	9	15	47	23	30	19	11	A-6a (7)	-
				4	12														
				5	8	22	39	SS-3	4.50	-	-	-	-	-	-	-	13	A-6a (V)	-
				6	8														
				7	3	10	44	SS-4	2.25	5	8	8	43	36	34	21	13	A-6a (9)	-
				8	4														
		EOB																	
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																			
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVEL ED. SOIL CUTTINGS																			

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES			DRILL RIG: CME 55X			STATION / OFFSET: 408+18, 9' LT.			EXPLORATION ID B-004-0-20							
TYPE: SUBGRADE		SAMPLING FIRM / LOGGER: NEAS / J. HODGES			HAMMER: CME AUTOMATIC			ALIGNMENT: IR-77 SB										
PID: 111404 SFN: _____		DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 12/5/19			ELEVATION: 1016.3 (MSL) EOB: 7.5 ft.			PAGE 1 OF 1							
START: 11/24/20 END: 11/24/20		SAMPLING METHOD: SPT			ENERGY RATIO (%): 81.9			LAT / LONG: 41.147517, -81.636476										
MATERIAL DESCRIPTION AND NOTES			ELEV. 1016.3	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)		ATTERBERG	WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL		
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)						1												
MEDIUM DENSE, BROWN, GRAVEL AND STONE FRAGMENTS WITH SAND, SILT, AND CLAY, DAMP				1014.8		2	4	SS-1	-	-	-	-	-	-	10	A-2-6 (V)	<100	
HARD, BROWN, SANDY SILT, LITTLE GRAVEL, LITTLE CLAY, DAMP				1013.3		3	5											
STIFF TO VERY STIFF, BROWN, SILT AND CLAY, SOME SAND, LITTLE GRAVEL, DAMP				1010.3		4	10	SS-2	4.25	17	21	24	25	13	24	15	9	11 A-4a (1) -
						5	6	SS-3	4.50	-	-	-	-	-	-	-	-	15 A-4a (V) -
						6	8											
						7	2	SS-4	2.00	14	18	16	31	21	29	17	12	16 A-6a (4) -
							3											
				EOB														
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																		
ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS																		

PROJECT:	SUM-77-24.12	DRILLING FIRM / OPERATOR:	NEAS / J. HODGES	DRILL RIG:	CME 55X	STATION / OFFSET:	610+13, 34' LT.	EXPLORATION ID																
TYPE:	LIGHT TOWER	SAMPLING FIRM / LOGGER:	NEAS / J. HODGES	HAMMER:	CME AUTOMATIC	ALIGNMENT:	IR-77	B-004-1-20																
PID:	111404	SFN:		CALIBRATION DATE:	12/5/19	ELEVATION:	1011.3 (MSL)	PAGE																
START:	9/28/21	END:	9/28/21	SAMPLING METHOD:	SPT	ENERGY RATIO (%):	81.9	1 OF 1																
MATERIAL DESCRIPTION AND NOTES			ELEV. 1011.3	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL				
LOOSE, BROWN, COARSE AND FINE SAND, LITTLE TO SOME GRAVEL, LITTLE SILT, TRACE CLAY, DAMP TO MOIST (FILL)						1				GR	CS	FS	SI	CL	LL	PL	PI			<L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L> >R>L <L><L>				
					4	3 2	7	100	SS-1	-	21	32	20	17	10	NP	NP	NP	10	A-3a (0)				
					3	2 2	5	33	SS-2	-	-	-	-	-	-	-	-	-	12	A-3a (V)				
					2	3	7	39	SS-3	-	-	-	-	-	-	-	-	-	11	A-3a (V)				
					3	3 3	8	89	SS-4	3.00	1	5	33	40	21	23	18	5	19	A-4a (5)				
					4	3 3	8	100	SS-5A	1.75	1	0	8	41	50	33	21	12	30	A-6a (9)				
									SS-5B	-	-	-	-	-	-	-	-	-	24	A-3a (V)				
					2	2 4	8	44	SS-6	-	-	-	-	-	-	-	-	-	12	A-3a (V)				
					3	3 4	10	50	SS-7	-	15	9	16	40	20	27	20	7	18	A-4a (5)				
					4	4 12	22	39	SS-8	-	-	-	-	-	-	-	-	-	17	A-4a (V)				
					5	5 10	20	44	SS-9	-	-	-	-	-	-	-	-	-	9	A-1-b (V)				
					9	9 14	31	100	SS-10	-	-	-	-	-	-	-	-	-	8	A-1-b (V)				
EOB																								
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																								
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVELLED, SOIL CUTTINGS																								

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES		DRILL RIG: CME 55X				STATION / OFFSET: 614+20, 90' LT.				EXPLORATION ID B-006-1-20							
TYPE: LIGHT TOWER		SAMPLING FIRM / LOGGER: NEAS / J. HODGES		HAMMER: CME AUTOMATIC				ALIGNMENT: IR-77											
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA		CALIBRATION DATE: 12/5/19				ELEVATION: 997.0 (MSL) EOB: 26.5 ft.				PAGE 1 OF 1							
START: 9/28/21 END: 9/28/21		SAMPLING METHOD: SPT		ENERGY RATIO (%): 81.9				LAT / LONG: 41.148463, -81.634659											
MATERIAL DESCRIPTION AND NOTES				ELEV. 997.0	DEPTHs		SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)		ATTERBERG	WC	ODOT CLASS (GI)	BACK FILL		
VERY LOOSE, BLACK, ORGANIC SILT , SOME SAND, LITTLE CLAY, LITTLE GRAVEL, TRACE ROOTS, HIGH MOISTURE RESULTS DUE TO ORGANICS, DAMP					1											< /> < />			
@2.5' - 6.5'; 16.4% LOI (HIGHLY ORGANIC)					2											< /> < />			
					3	1 1 1	3	33	SS-1	-	11 18 12 41 18	NP NP NP 83	A-8a (V)			< /> < />			
					4											< /> < />			
					5											< /> < />			
					6	0 1 1	3	44	SS-2	-	- - - - -	- - - - -	100	A-8a (V)		< /> < />			
SOFT, GRAY, CLAY , "AND" SILT, TRACE SAND, TRACE GRAVEL, MOIST					7											< /> < />			
					8	0 1 2	4	100	SS-3	0.25	4 4 5 59 28	47 26 21 41	A-7-6 (14)			< /> < />			
					9											< /> < />			
STIFF TO HARD, GRAY, SILT AND CLAY , TRACE SAND, TRACE GRAVEL, DAMP TO MOIST					10	0 0 3	4	89	SS-4	0.25	- - - -	- - - -	29	A-7-6 (V)		< /> < />			
					11											< /> < />			
					12											< /> < />			
					13	3 3 6	12	100	SS-5	3.50	6 4 6 48 36	29 18 11 18	A-6a (8)			< /> < />			
					14											< /> < />			
					15	4 4 4	11	100	SS-6	4.50	- - - -	- - - -	19	A-6a (V)		< /> < />			
					16											< /> < />			
					17											< /> < />			
					18	6 11 14	34	72	SS-7	1.75	- - -	- - -	- - -	22	A-6a (V)		< /> < />		
					19											< /> < />			
MEDIUM DENSE, BROWN, COARSE AND FINE SAND , LITTLE GRAVEL, TRACE SILT, TRACE CLAY, WET					20	12 10 9	26	56	SS-8	-	- - -	- - -	- - -	23	A-3a (V)		< /> < />		
					21											< /> < />			
					22											< /> < />			
DENSE, BROWN AND GRAY, GRAVEL WITH SAND , TRACE SILT, TRACE CLAY, MOIST TO WET					23	12 12 13	34	100	SS-9	-	- - -	- - -	- - -	12	A-1-b (V)		< /> < />		
					24											< /> < />			
					25	14 15 14	40	67	SS-10	-	- - -	- - -	- - -	14	A-1-b (V)		< /> < />		
					26											< /> < />			
EOB																			
NOTES: GROUNDWATER ENCOUNTERED AT 19.0' DURING DRILLING. HOLE DID NOT CAVE.																			
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																			

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 319+10, 1' LT.	EXPLORATION ID: B-009-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77 NB																
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 999.0 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1															
START: 8/8/20 END: 8/8/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.148983, -81.632968																
MATERIAL DESCRIPTION AND NOTES	ELEV. 999.0	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI				
12.0" ASPHALT AND 4.0" BASE (DRILLERS DESCRIPTION)	997.7																		
MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE CLAY, DAMP	996.0	1																	
SOFT TO VERY STIFF, GRAY, SANDY SILT, LITTLE CLAY, TRACE TO LITTLE GRAVEL, DAMP TO MOIST	991.5	2	8	15	44	SS-1	-	-	-	-	-	-	-	-	11	A-2-4 (V)	250		
		3	6	5															
		4	2	7	100	SS-2	0.50	10	21	22	32	15	26	17	9	16	A-4a (2)	-	
		5	4	6	14	44	SS-3	3.75	11	18	24	32	15	26	17	9	13	A-4a (2)	-
		6	4	3	10	56	SS-4	2.50	-	-	-	-	-	-	-	-	18	A-4a (V)	-
		7	3	4															
		EOB																	
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																			
ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVEL ED SOIL CUTTINGS																			

STANDARD ODOT LOG W/ SULFATES (8.5 X 11) PROJECT: SUM-77-24.12 TYPE: SUBGRADE PID: 111404 SFN: _____ START: 8/8/20 END: 8/8/20	DRILLING FIRM / OPERATOR: NEAS / J. HODGES		DRILL RIG: CME 55X		STATION / OFFSET: 323+93, 2' LT.		EXPLORATION ID B-011-0-20															
	SAMPLING FIRM / LOGGER: NEAS / J. HODGES		HAMMER: CME AUTOMATIC		ALIGNMENT: IR-77 NB																	
	DRILLING METHOD: 3.25" HSA		CALIBRATION DATE: 12/5/19		ELEVATION: 995.0 (MSL)		EOB: 7.5 ft.															
	SAMPLING METHOD: SPT		ENERGY RATIO (%): 81.9		LAT / LONG: 41.149754, -81.631542		PAGE 1 OF 1															
	MATERIAL DESCRIPTION AND NOTES	ELEV. 995.0	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL		
GR									CS	FS	SI	CL	LL	PL	PI							
STIFF TO VERY STIFF, BROWN AND GRAY, SANDY SILT , LITTLE TO SOME CLAY, TRACE TO SOME GRAVEL, DAMP TO MOIST @3.0' - 7.5'; CONTAINS IRON STAINING				1														< > < > > > < > < > > > < > < > > > < > < > > >				
				2	5	4	16	67	SS-1	1.75	5	14	20	38	23	25	16	9	15	A-4a (5)	133	< > < > > > < > < > > > < > < > > > < > < > > >
				3	3	4	12	44	SS-2	2.00	24	17	20	27	12	25	16	9	14	A-4a (1)	-	< > < > > > < > < > > > < > < > > > < > < > > >
				4	4	5																< > < > > > < > < > > > < > < > > > < > < > > >
				5	3	2	7	89	SS-3	2.50	-	-	-	-	-	-	-	-	17	A-4a (V)	-	< > < > > > < > < > > > < > < > > > < > < > > >
				6	6	7	14	44	SS-4	2.50	-	-	-	-	-	-	-	-	16	A-4a (V)	-	< > < > > > < > < > > > < > < > > > < > < > > >
				7	3																	< > < > > > < > < > > > < > < > > > < > < > > >
				987.5	EOB																	
				NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.									ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS									

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES			DRILL RIG: CME 55X			STATION / OFFSET: 625+08, 123' LT.			EXPLORATION ID B-011-1-20								
TYPE: LIGHT TOWER		SAMPLING FIRM / LOGGER: NEAS / J. HODGES			HAMMER: CME AUTOMATIC			ALIGNMENT: IR-77											
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 12/5/19			ELEVATION: 1003.4 (MSL) EOB: 26.5 ft.			PAGE								
START: 9/29/21 END: 9/29/21		SAMPLING METHOD: SPT			ENERGY RATIO (%): 81.9			LAT / LONG: 41.150174, -81.631726			1 OF 1								
MATERIAL DESCRIPTION AND NOTES	ELEV. 1003.4	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)			ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL			
								GR	CS	FS	SI	CL	LL				PL	PI	
HARD, BROWN, SILT AND CLAY, LITTLE SAND, TRACE GRAVEL, DAMP				1															
				2															
			5	6	15	83	SS-1	4.50	5	8	12	46	29	33	19	14	16	A-6a (10)	
			3	5															
			4																
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, TRACE TO LITTLE GRAVEL, TRACE TO LITTLE SILT, TRACE CLAY, DAMP			5	4	14	100	SS-2	-	-	-	-	-	-	-	-	-	-	13	A-3a (V)
			6	5															
			7																
			8	1	11	22	SS-3	-	-	-	-	-	-	-	-	-	-	15	A-3a (V)
			9	3															
STIFF, BROWN, SILT AND CLAY, LITTLE SAND, TRACE GRAVEL, CONTAINS NO INTACT SOIL FOR HP READINGS, MOIST			10	2	10	33	SS-4	-	2	7	12	44	35	33	20	13	22	A-6a (9)	
			11	3															
			12																
MEDIUM DENSE, BROWN, GRAVEL WITH SAND, TRACE TO LITTLE SILT, TRACE CLAY, MOIST TO DAMP			13	2	26	44	SS-5	-	-	-	-	-	-	-	-	-	-	14	A-1-b (V)
			14	8															
			15	11															
LOOSE, BROWN, COARSE AND FINE SAND, LITTLE SILT, TRACE CLAY, TRACE GRAVEL, WET			16	3	27	39	SS-6	-	-	-	-	-	-	-	-	-	-	6	A-1-b (V)
			17																
			18	4	8	100	SS-7	-	4	17	62	13	4	NP	NP	NP	26	A-3a (0)	
			19	3															
			20																
			21	2	7	89	SS-8	-	-	-	-	-	-	-	-	-	-	26	A-3a (V)
			22																
			23	3	10	100	SS-9	-	-	-	-	-	-	-	-	-	-	26	A-3a (V)
			24	3															
			25	2	10	100	SS-10	-	-	-	-	-	-	-	-	-	-	26	A-3a (V)
			26	4															
EOB																			
NOTES: GROUNDWATER ENCOUNTERED AT 17.5' DURING DRILLING. HOLE DID NOT CAVE.																			
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																			

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 328+78, 16' LT.	EXPLORATION ID: B-013-0-20																
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77 NB																	
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 988.5 (MSL) EOB: 7.5 ft.	PAGE: 1 OF 1																
START: 8/31/20 END: 8/31/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.150647, -81.630244																	
MATERIAL DESCRIPTION AND NOTES	ELEV. 988.5	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI					
MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE CLAY, DAMP	987.0			4 5 6	15	78	SS-1	-	21	24	23	22	10	NP	NP	NP	11	A-2-4 (0)	110	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
HARD, BROWN, SILT, "AND" CLAY, LITTLE SAND, TRACE GRAVEL, DAMP TO MOIST	981.0	EOB		1 2 3 4 5 6 7	31 9 14 8 14 6 3 6 8	100	SS-2	4.50	2	4	8	50	36	29	19	10	18	A-4b (8)	-	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
							SS-3	4.50	-	-	-	-	-	-	-	-	18	A-4b (V)	-	<LV >> <LV >> <LV >> <LV >>
							SS-4	4.50	-	-	-	-	-	-	-	-	14	A-4b (V)	-	<LV >> <LV >> <LV >> <LV >>
							SS-5	4.50	-	-	-	-	-	-	-	-	23	A-4b (V)	-	<LV >> <LV >> <LV >> <LV >>
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																				
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVELLED, SOIL CUTTINGS																				

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES		DRILL RIG: CME 55X				STATION / OFFSET: 29+15, 74' LT.				EXPLORATION ID B-013-1-20						
TYPE: LIGHT TOWER		SAMPLING FIRM / LOGGER: NEAS / J. HODGES		HAMMER: CME AUTOMATIC				ALIGNMENT: RAMP N										
PID: 111404	SFN:	DRILLING METHOD: 3.25" HSA		CALIBRATION DATE: 12/5/19				ELEVATION: 997.5 (MSL) EOB: 26.5 ft.				PAGE 1 OF 1						
START: 10/4/21	END: 10/4/21	SAMPLING METHOD: SPT		ENERGY RATIO (%): 81.9				LAT / LONG: 41.150450, -81.629714										
MATERIAL DESCRIPTION AND NOTES	ELEV. 997.5	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)			ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL		
								GR	CS	FS	SI	CL	LL				PL	PI
HARD, BROWN, SANDY SILT, SOME CLAY, TRACE GRAVEL AND STONE FRAGMENTS, CONTAINS IRON STAINING, DAMP (FILL)																		
		1																
		2																
		3	4	5	14	100	SS-1	4.25	4	15	19	37	25	26	18	8	12	A-4a (5)
		4																
		5																
		6																
		7																
		8	5	4	11	22	SS-2	-	-	-	-	-	-	-	-	-	11	A-2-4 (V)
		9																
		10																
		11	3	3	10	28	SS-3	4.25	-	-	-	-	-	-	-	-	27	A-6a (V)
		12																
		13	4	5	12	100	SS-4	4.50	1	3	5	43	48	36	22	14	19	A-6a (10)
		14																
		15																
		16	4	3	10	100	SS-5	4.25	-	-	-	-	-	-	-	-	23	A-6a (V)
		17																
		18	3	4	11	33	SS-6	-	8	1	8	65	18	NP	NP	NP	20	A-4b (8)
		19																
		20																
		21	2	3	8	39	SS-7	3.00	0	0	2	64	34	24	16	8	19	A-4b (8)
		22																
		23	3	3	7	89	SS-8	2.25	-	-	-	-	-	-	-	-	19	A-4b (V)
		24																
		25																
		26	3	2	8	67	SS-9	2.00	-	-	-	-	-	-	-	-	19	A-4b (V)
		EOB																
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																		
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																		

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 428+74, 41' LT.	EXPLORATION ID B-014-0-20																
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77 SB																	
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 988.8 (MSL)	EOB: 7.5 ft.	PAGE 1 OF 1																
START: 12/7/20 END: 12/7/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.151315, -81.630975																	
MATERIAL DESCRIPTION AND NOTES	ELEV. 988.8	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI					
6.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)	987.8			1																
MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE CLAY, CONTAINS TRACE IRON STAINING, DAMP	985.8			2	10 12 7	26	67	SS-1	-	33	21	16	20	10	NP	NP	NP	10	A-2-4 (0)	<100
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, TRACE SILT, TRACE GRAVEL, TRACE CLAY, CONTAINS TRACE IRON STAINING, DAMP	984.3			3	4 9 11	27	100	SS-2	-	-	-	-	-	-	-	-	-	12	A-3a (V)	-
VERY STIFF, BROWN, SANDY SILT, SOME GRAVEL, LITTLE CLAY, CONTAINS TRACE IRON STAINING, DAMP	982.8			4	4 5 5	14	67	SS-3	2.25	21	22	20	24	13	20	13	7	11	A-4a (0)	-
MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE CLAY, CONTAINS TRACE IRON STAINING, MOIST	981.3	EOB		5	3 6	19	89	SS-4	-	-	-	-	-	-	-	-	-	16	A-2-4 (V)	-

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 332+00, 16' LT.	EXPLORATION ID: B-015-0-20																																																																																																		
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77 NB																																																																																																			
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 982.8 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1																																																																																																		
START: 8/31/20 END: 8/31/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.151300, -81.629462																																																																																																			
MATERIAL DESCRIPTION AND NOTES	ELEV. 982.8	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL																																																																																			
								GR	CS	FS	SI	CL	LL	PL	PI																																																																																							
LOOSE TO DENSE, BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, CONTAINS IRON STAINING, DAMP																																																																																																						<img alt="Soil profile diagram showing a vertical column of soil layers from top to bottom.

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES		DRILL RIG: CME 55X				STATION / OFFSET: 635+12, 29' LT.				EXPLORATION ID B-016-1-20							
TYPE: LIGHT TOWER		SAMPLING FIRM / LOGGER: NEAS / J. HODGES		HAMMER: CME AUTOMATIC				ALIGNMENT: IR-77											
PID: 111404	SFN:	DRILLING METHOD: 3.25" HSA		CALIBRATION DATE: 12/5/19				ELEVATION: 979.3 (MSL) EOB: 26.5 ft.				PAGE 1 OF 1							
START: 9/29/21	END: 9/29/21	SAMPLING METHOD: SPT		ENERGY RATIO (%): 81.9				LAT / LONG: 41.151961, -81.629039											
MATERIAL DESCRIPTION AND NOTES	ELEV. 979.3	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)				ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL		
								GR	CS	FS	SI	CL	LL	PL				PI	
LOOSE TO MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE CLAY, DAMP				1															
				2															
			3	3	7	100	SS-1	-	23	30	24	17	6	24	17	7	10	A-2-4 (0)	
			4																
			5																
			6	3	2	5	100	SS-2	-	-	-	-	-	-	-	-	-	13	A-2-4 (V)
			7																
			8	3	4	14	28	SS-3	-	-	-	-	-	-	-	-	-	10	A-2-4 (V)
			9																
			10	4	5	18	44	SS-4	4.50	22	10	16	36	16	27	18	9	13	A-4a (3)
			11	8															
			12																
			13	4	5	12	33	SS-5	-	-	-	-	-	-	-	-	-	8	A-3a (V)
			14	4															
			15	3	4	11	44	SS-6	-	-	-	-	-	-	-	-	-	5	A-3a (V)
			16	4	4														
			17																
			18	4	4	11	28	SS-7	-	-	-	-	-	-	-	-	-	6	A-3a (V)
			19																
			20	3															
			21	4	5	12	39	SS-8	-	-	-	-	-	-	-	-	-	5	A-3a (V)
			22																
			23	4	5	15	50	SS-9	4.50	5	3	15	59	18	27	21	6	18	A-4b (8)
			24																
			25	6	4	12	67	SS-10	4.25	-	-	-	-	-	-	-	-	16	A-4b (V)
			26	5															
EOB																			
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																			
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																			

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 436+21, 0' RT.	EXPLORATION ID B-018-0-20																	
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77 SB																		
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 971.7 (MSL)	PAGE																	
START: 11/23/20 END: 11/23/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.152589, -81.628873	1 OF 1																	
MATERIAL DESCRIPTION AND NOTES	ELEV. 971.7	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL		
								GR	CS	FS	SI	CL	LL	PL	PI						
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)		970.2		1																	
MEDIUM DENSE, BROWN, SANDY SILT, LITTLE GRAVEL, LITTLE CLAY, DAMP		967.2		2	12 6	16	100	SS-1	-	-	-	-	-	-	-	-	11	A-4a (V)	<100		
MEDIUM DENSE, BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, DAMP		964.5		3	4	10 11	29	44	SS-2	-	15	22	27	25	11	NP	NP	NP	8	A-4a (0)	-
HARD, BROWN, SANDY SILT, SOME GRAVEL, LITTLE CLAY, DAMP		964.2	EOB	4	5	8 9	23	56	SS-3	-	-	-	-	-	-	-	-	7	A-1-b (V)	-	
				6	4	4	11	56	SS-4A	-	-	-	-	-	-	-	-	7	A-1-b (V)	-	
				7	4	4	4.50		SS-4B	-	-	-	-	-	-	-	-	10	A-4a (V)	-	

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES		DRILL RIG: CME 55X				STATION / OFFSET: 640+38, 24' LT.				EXPLORATION ID B-019-1-20						
TYPE: LIGHT TOWER		SAMPLING FIRM / LOGGER: NEAS / J. HODGES		HAMMER: CME AUTOMATIC				ALIGNMENT: IR-77										
PID: 111404 SFN: 3.25" HSA		CALIBRATION DATE: 12/5/19		ENERGY RATIO (%): 81.9				ELEVATION: 966.6 (MSL) EOB: 26.5 ft.				PAGE 1 OF 1						
START: 9/29/21 END: 9/29/21		SAMPLING METHOD: SPT						LAT / LONG: 41.153169, -81.628018										
MATERIAL DESCRIPTION AND NOTES	ELEV. 966.6	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)			ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL		
								GR	CS	FS	SI	CL	LL				PL	PI
HARD, BROWN, SANDY SILT, SOME CLAY, TRACE GRAVEL, DAMP																		
				1														
				2														
			3	6	16	100	SS-1	4.50	8	4	11	47	30	28	18	10	15	A-4a (8)
			4															
			5															
			6	2	5	100	SS-2	-	-	-	-	-	-	-	-	-	6	A-1-b (V)
			7															
			8	2	7	39	SS-3	-	7	43	41	7	2	NP	NP	NP	7	A-1-b (0)
			9															
			10															
			11	2	4	44	SS-4	-	-	-	-	-	-	-	-	-	7	A-1-b (V)
			12															
			13	2	3	10	SS-5	-	-	-	-	-	-	-	-	-	10	A-1-b (V)
			14															
			15															
			16	2	5	14	SS-6	-	35	35	15	12	3	NP	NP	NP	11	A-1-b (0)
			17															
			18	3	2	5	SS-7	-	-	-	-	-	-	-	-	-	10	A-1-b (V)
			19															
			20															
			21	2	1	4	SS-8	-	-	-	-	-	-	-	-	-	8	A-1-b (V)
			22															
			23	3	4	14	SS-9	-	-	-	-	-	-	-	-	-	7	A-1-b (V)
			24															
			25	6	5	14	SS-10	-	-	-	-	-	-	-	-	-	10	A-1-b (V)
			26															
EOB																		
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																		
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																		

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES		DRILL RIG: CME 55X				STATION / OFFSET: 645+87, 3' LT.				EXPLORATION ID B-022-1-20							
TYPE: LIGHT TOWER		SAMPLING FIRM / LOGGER: NEAS / J. HODGES		HAMMER: CME AUTOMATIC				ALIGNMENT: IR-77											
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA		CALIBRATION DATE: 12/5/19				ELEVATION: 954.4 (MSL) EOB: 26.5 ft.				PAGE 1 OF 1							
START: 9/30/21 END: 9/30/21		SAMPLING METHOD: SPT		ENERGY RATIO (%): 81.9				LAT / LONG: 41.154514, -81.627136											
MATERIAL DESCRIPTION AND NOTES	ELEV. 954.4	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)				ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL		
								GR	CS	FS	SI	CL	LL	PL				PI	
VERY STIFF TO HARD, BROWN BECOMING GRAY, SANDY SILT , LITTLE TO SOME CLAY, TRACE TO LITTLE GRAVEL, DAMP TO MOIST																			
			1																
			2																
			3	10 8	25	100	SS-1	4.50	7	13	24	39	17	22	15	7	11	A-4a (4)	
			4																
			5																
			6	2 3	7	100	SS-2	4.50	-	-	-	-	-	-	-	-	-	14	A-4a (V)
			7																
			8	3 4 6	14	100	SS-3	4.50	-	-	-	-	-	-	-	-	-	16	A-4a (V)
			9																
			10																
			11	2 4 5	12	56	SS-4	3.50	-	-	-	-	-	-	-	-	-	13	A-4a (V)
			12																
			13	3 2 4	8	100	SS-5	2.75	-	-	-	-	-	-	-	-	-	19	A-4a (V)
			14																
			15																
			16	2 4 6	14	100	SS-6	4.50	5	8	8	53	26	29	19	10	19	A-4b (8)	
			17																
			18	3 3 4	10	22	SS-7	4.25	-	-	-	-	-	-	-	-	-	14	A-4b (V)
			19																
			20																
			21	2 3 4	10	100	SS-8	4.50	1	1	1	25	72	48	24	24	24	A-7-6 (15)	
			22																
			23	3 4 6	14	100	SS-9	-	-	-	-	-	-	-	-	-	-	9	A-3a (V)
			24																
			25																
			26	2 4 6	14	89	SS-10	-	-	-	-	-	-	-	-	-	-	13	A-3a (V)
EOB																			
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																			
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																			

PID: 111404 SEN: PROJECT: SUM-77-24 12 STATION / OFFSET: 644+65 79' RT START: 1/31/22 END: 1/31/22 PG 2 QE 2 B-022-2-20

NOTES: GROUNDWATER ENCOUNTERED AT 34.0' DURING DRILLING. HOLE CAVE-IN AT 31.0'.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVELED SOIL CUTTINGS

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: GPD / JT			DRILL RIG: CME 55			STATION / OFFSET: 645+30, 80' LT.			EXPLORATION ID B-022-3-20										
TYPE: CULVERT		SAMPLING FIRM / LOGGER: NEAS / D. CAMPANA			HAMMER: CME AUTOMATIC			ALIGNMENT: IR-77													
PID: 111404 SFN: _____		DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 1/26/22			ELEVATION: 951.2 (MSL) EOB: 48.0 ft.			PAGE 1 OF 2										
START: 2/2/22 END: 2/2/22		SAMPLING METHOD: SPT			ENERGY RATIO (%): 67.6			LAT / LONG: 41.154443, -81.627471													
MATERIAL DESCRIPTION AND NOTES			ELEV. 951.2	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)			ATTERBERG								
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)								GR	CS	FS	SI	CL	LL	PL	PI	WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL		
MEDIUM DENSE, BROWN, GRAVEL AND STONE FRAGMENTS WITH SAND AND SILT, TRACE CLAY, DAMP				949.7				SS-1	-	-	-	-	-	-	-	7	A-2-4 (V)	-			
LOOSE, BROWN, SILT, SOME SAND, SOME CLAY, TRACE GRAVEL, DAMP				948.2				SS-2	-	2	8	16	51	23	NP	NP	NP	14	A-4b (8)	-	
UNCONTROLLED FILL, 1.25" TILE				944.4				SS-3	-	-	-	-	-	-	-	-	-	UCF (V)	-		
HARD, BROWN, SILT AND CLAY, SOME SAND, TRACE GRAVEL, DAMP				939.4				SS-4	4.50	7	14	20	31	28	28	17	11	11	A-6a (5)	-	
VERY STIFF TO HARD, BROWN, SANDY SILT, LITTLE CLAY, LITTLE GRAVEL, SS-6 CONTAINS ROOTS AND IRON STAINING, DAMP TO MOIST				934.4				SS-5	4.25	-	-	-	-	-	-	-	9	A-4a (V)	-		
MEDIUM DENSE, BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, DAMP				928.2				SS-6	3.00	-	-	-	-	-	-	-	21	A-4a (V)	-		
VERY STIFF TO HARD, BROWN MOTTLED WITH GRAY, SILT AND CLAY, LITTLE SAND, TRACE GRAVEL, DAMP TO MOIST				925.7				SS-7	-	-	-	-	-	-	-	-	9	A-1-b (V)	-		
								SS-8	4.50	0	5	7	59	29	27	16	11	17	A-6a (8)	-	
								SS-9	3.50	-	-	-	-	-	-	-	19	A-6a (V)	-		

NOTES: GROUNDWATER ENCOUNTERED AT 33.0' DURING DRILLING. HOLE CAVE-IN AT 30.0'.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVELED SOIL CUTTINGS

PID:	111404	SFN:		PROJECT:	SUM-77-24.12		STATION / OFFSET:	645+30, 80' LT.			START:	2/2/22		END:	2/2/22		PG 2 OF 2	B-022-3-20					
MATERIAL DESCRIPTION AND NOTES				ELEV.	DEPTH(S)		SPT/RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
				921.2								GR	CS	FS	SI	CL	LL	PL	PI				
VERY STIFF TO HARD, BROWN MOTTLED WITH GRAY, SILT AND CLAY , LITTLE SAND, TRACE GRAVEL, DAMP TO MOIST (continued)				918.2	W 918.2							-	-	-	-	-	-	-	-	18	A-6a (V)	-	
MEDIUM DENSE, BROWN, COARSE AND FINE SAND , SOME SILT, TRACE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, WET				913.2								-	0	3	66	26	5	NP	NP	NP	21	A-3a (0)	-
MEDIUM DENSE, GRAY, SILT , LITTLE SAND, TRACE TO LITTLE CLAY, TRACE GRAVEL, WET TO MOIST				903.2	BECOMES DAMP							-	-	-	-	-	-	-	-	17	A-3a (V)	-	
												-	0	0	14	76	10	NP	NP	NP	21	A-4b (8)	-
												-	-	-	-	-	-	-	-	24	A-4b (V)	-	
												-	-	-	-	-	-	-	-	15	A-4b (V)	-	
												-	-	-	-	-	-	-	-	9	A-4b (V)	-	
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PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES		DRILL RIG: CME 55X				STATION / OFFSET: 651+47, 6' RT.				EXPLORATION ID B-023-1-20						
TYPE: LIGHT TOWER		SAMPLING FIRM / LOGGER: NEAS / J. HODGES		HAMMER: CME AUTOMATIC				ALIGNMENT: IR-77										
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA		CALIBRATION DATE: 12/5/19				ELEVATION: 946.2 (MSL) EOB: 26.5 ft.				PAGE 1 OF 1						
START: 9/30/21 END: 9/30/21		SAMPLING METHOD: SPT		ENERGY RATIO (%): 81.9				LAT / LONG: 41.155985, -81.626548										
MATERIAL DESCRIPTION AND NOTES	ELEV. 946.2	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)				ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL				PI
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, LITTLE SILT, TRACE CLAY, MOIST																		
				1														
				2														
			3	4 7 11	25	100	SS-1	-	21	24	31	15	9	NP	NP	NP	12	A-3a (0)
			4															
			5															
			6	5 8	18	100	SS-2	4.50	-	-	-	-	-	-	-	-	18	A-6a (V)
			7															
			8	3 5 6	15	100	SS-3	4.50	-	-	-	-	-	-	-	-	13	A-6a (V)
			9															
			10															
			11	3 4 7	15	67	SS-4	4.25	-	-	-	-	-	-	-	-	13	A-6a (V)
			12															
			13	4 4 5	12	72	SS-5	3.50	5	9	9	44	33	30	18	12	18	A-6a (9)
			14															
			15															
			16	3 4 8	16	100	SS-6	4.50	9	13	12	40	26	30	18	12	15	A-6a (7)
			17															
			18	2 4 5	12	100	SS-7	3.50	-	-	-	-	-	-	-	-	23	A-6a (V)
			19															
			20															
			21	3 3 4	10	83	SS-8	4.25	-	-	-	-	-	-	-	-	22	A-6a (V)
			22															
			23	2 5 8	18	100	SS-9	-	-	-	-	-	-	-	-	-	7	A-3a (V)
			24															
			25	2 3 6	12	33	SS-10	-	-	-	-	-	-	-	-	-	9	A-3a (V)
		EOB	26															
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																		
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																		

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: GPD / JT			DRILL RIG: CME 55			STATION / OFFSET: 659+91, 71' LT.			EXPLORATION ID B-023-3-20		
TYPE: CULVERT		SAMPLING FIRM / LOGGER: NEAS / D. CAMPANA			HAMMER: CME AUTOMATIC			ALIGNMENT: IR-77					
PID: 111404	SFN: _____	DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 1/26/22			ELEVATION: 961.8 (MSL) EOB: 40.0 ft.			PAGE 1 OF 2		
START: 2/1/22	END: 2/2/22	SAMPLING METHOD: SPT			ENERGY RATIO (%): 67.6			LAT / LONG: 41.158290, -81.626518					
MATERIAL DESCRIPTION AND NOTES			ELEV. 961.8	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)			ATTERBERG
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)									GR	CS	FS	SI	CL
HARD, BROWN, SANDY SILT , LITTLE GRAVEL AND STONE FRAGMENTS, TRACE CLAY, CONTAINS IRON STAINING, DAMP				960.3		1	40		-	-	-	-	-
					33	50	78	SS-1	4.50	3	10	13	40
					11					34	28	18	10
HARD, BROWN AND GRAY, SANDY SILT , SOME CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				958.8		4	7	SS-2	4.50	14	A-4a (8)	-	
					8	16	75						
					6								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				941.3		9	6	SS-3	4.50	15	A-4a (V)	-	
					4	10	86						
					5								
VERY DENSE, TAN AND GRAY, STONE FRAGMENTS , LITTLE SAND, TRACE SILT, TRACE CLAY, DAMP				936.3		11	12	SS-4	4.50	15	A-4a (V)	-	
					6	12	78						
VERY DENSE, ORANGISH BROWN, SILT , LITTLE CLAY, TRACE SAND, TRACE GRAVEL, CONTAINS IRON STAINING, WET				933.8		17	17	SS-5	4.50	14	A-4a (V)	-	
					8	17	89						
					5								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				921.3		18	18	SS-6	4.50	15	A-4a (V)	-	
					7	17	78						
					8								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				911.3		19	18	SS-7	4.50	13	A-4a (V)	-	
					9	18	67						
					5								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				901.3		21	6	SS-8	4.50	15	A-4b (6)	-	
					10	24	100						
					11								
VERY DENSE, TAN AND GRAY, STONE FRAGMENTS , LITTLE SAND, TRACE SILT, TRACE CLAY, DAMP				891.3		22	8	SS-9	4.50	9	A-4b (V)	-	
					19	19	78						
					8								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				881.3		23		SS-10	-	2	A-1-a (V)	-	
					19	56	0						
					25								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				871.3		24	10	SS-11	-	0	1	1	82
					8	19	78			1	1	16	NP
					9					NP	NP	NP	NP
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				861.3		25	36	SS-12	-	23	A-4b (8)	-	
					38	54	39						
					10								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				851.3		26		SS-13	-				
					19								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				841.3		27	25	SS-14	-				
					25								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				831.3		28		SS-15	-				
					36								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				821.3		29		SS-16	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				811.3		30		SS-17	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				801.3		31		SS-18	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				791.3		32		SS-19	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				781.3		33		SS-20	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				771.3		34		SS-21	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				761.3		35		SS-22	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				751.3		36		SS-23	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				741.3		37		SS-24	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				731.3		38		SS-25	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				721.3		39		SS-26	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				711.3		40		SS-27	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				701.3		41		SS-28	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				691.3		42		SS-29	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				681.3		43		SS-30	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				671.3		44		SS-31	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				661.3		45		SS-32	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				651.3		46		SS-33	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				641.3		47		SS-34	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				631.3		48		SS-35	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				621.3		49		SS-36	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				611.3		50		SS-37	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				601.3		51		SS-38	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				591.3		52		SS-39	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				581.3		53		SS-40	-				
					38								
HARD, BROWN WITH GRAY MOTTLES, SILT , SOME SAND, LITTLE CLAY, TRACE GRA													

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE CAVE-IN AT 28.0'.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVELED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 664+36, 39' RT.	EXPLORATION ID: B-025-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 973.1 (MSL) EOB: 7.5 ft.	PAGE: 1 OF 1															
START: 8/8/20 END: 8/8/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.159507, -81.626093																
MATERIAL DESCRIPTION AND NOTES	ELEV. 973.1	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI				
10.0" ASPHALT (DRILLERS DESCRIPTION)	972.3																		
VERY STIFF TO HARD, BROWN MOTTLED WITH GRAY AND ORANGISH BROWN, SILT, SOME CLAY, LITTLE SAND, TRACE GRAVEL, CONTAINS IRON STAINING, MOIST		1																	
		2	4	14	33	SS-1	4.50	2	3	11	52	32	28	18	10	20	A-4b (8)	-	
		3	4	6				-	-	-	-	-	-	-	-	19	A-4b (V)	110	
		4	4	5	12	67	SS-2	2.75											
		5	9	12	29	44	SS-3	3.50	16	28	19	24	13	24	16	8	13	A-4a (0)	-
		6	6	3	12	67	SS-4	3.25	-	-	-	-	-	-	-	-	22	A-4a (V)	-
		7																	
		EOB																	
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																			
ABANDONMENT METHODS MATERIALS QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVEL ED SOIL CUTTINGS																			

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: GPD / JT			DRILL RIG: CME 55			STATION / OFFSET: 664+86, 71' LT.			EXPLORATION ID B-025-2-20														
TYPE: CULVERT		SAMPLING FIRM / LOGGER: NEAS / D. CAMPANA			HAMMER: CME AUTOMATIC			ALIGNMENT: IR-77																	
PID: 111404	SFN: _____	DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 1/26/22			ELEVATION: 974.0 (MSL) EOB: 44.0 ft.			PAGE 1 OF 2														
START: 2/1/22	END: 2/1/22	SAMPLING METHOD: SPT			ENERGY RATIO (%): 67.6			LAT / LONG: 41.159648, -81.626488																	
MATERIAL DESCRIPTION AND NOTES			ELEV. 974.0	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)		ATTERBERG	WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL									
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)										GR	CS	FS	SI	CL	LL	PL	PI								
DENSE, BROWN, FINE SAND , SOME COARSE SAND, LITTLE GRAVEL, TRACE SILT, TRACE CLAY, DAMP (FILL)				972.5		1	32																		
VERY STIFF TO HARD, BROWN AND GRAY, SILT AND CLAY , LITTLE TO SOME SAND, TRACE GRAVEL, CONTAINS TRACE BRICK FRAGMENTS, DAMP (FILL)				971.0		2	26 11	42	97	SS-1	-	16	32	43	7	2	NP	NP	NP	5	A-3 (0)	-			
SS-4 CONTAINS NO RECOVERY						3																			
						4	4	5	11	61	SS-2	4.50	-	-	-	-	-	-	-	13	A-6a (V)	-			
						5	5																		
						6	6	7	10	19	81	SS-3	4.50	4	7	11	46	32	29	16	13	14	A-6a (9)	-	
						7																			
						8																			
						9																			
						10																			
						11																			
						12	6	7	8	17	0	SS-4	-	-	-	-	-	-	-	-	-	-	-	-	
						13																			
						14	4	5	11	72	SS-5	3.50	-	-	-	-	-	-	-	-	12	A-6a (V)	-		
						15	5	5																	
						16																			
						17																			
						18																			
						19	5	8	9	19	78	SS-7	4.50	-	-	-	-	-	-	-	13	A-6a (V)	-		
						20																			
						21																			
						22	3	19	14	37	72	SS-8	-	39	12	10	16	23	NP	NP	NP	11	A-4a (1)	-	
						23																			
						24	7	14	14	32	56	SS-9	4.50	21	14	20	28	17	24	13	11	10	A-6a (2)	-	
						25																			
						26																			
						27	2	3	4	8	61	SS-10	4.50	3	10	14	24	49	40	21	19	19	A-6b (11)	-	
						28																			
						29	3	2	4	7	69	SS-11	4.50	-	-	-	-	-	-	-	-	16	A-6b (V)	-	

PID:	SFN:	PROJECT:	SUM-77-24.12		STATION / OFFSET:				664+86, 71' LT.		START:	2/1/22		END:	2/1/22		PG 2 OF 2	B-025-2-20						
MATERIAL DESCRIPTION AND NOTES				ELEV. 944.0	DEPTH(S)		SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
												GR	CS	FS	SI	CL	LL	PL	PI					
HARD, GRAY, SILTY CLAY , LITTLE TO SOME SAND, TRACE GRAVEL, DAMP TO MOIST (continued)					31																13	A-6b (V)	-	<L> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>>
VERY STIFF TO HARD, GRAY, SILT AND CLAY , TRACE SAND, TRACE GRAVEL, MOIST				938.5	32	5 9 9	20	92	SS-12	4.50	-	-	-	-	-	-	-	-	-	24	A-6b (V)	-	<L> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>>	
				930.0	33																			
					34	5 6 9	17	83	SS-13	4.25	-	-	-	-	-	-	-	-	-	23	A-6a (9)	-	<L> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>>	
					35																			
					36																			
					37	4 5 7	14	81	SS-14	4.50	1	0	2	70	27	29	17	12	23	A-6a (V)	-	<L> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>>		
					38																			
					39	3 4 6	11	89	SS-15	4.50	-	-	-	-	-	-	-	-	22	A-6a (V)	-	<L> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>>		
					40																			
					41	3 7 6	15	100	SS-16	4.25	-	-	-	-	-	-	-	-	22	A-6a (V)	-	<L> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>>		
					42	8 8 11	21	83	SS-17	4.00	-	-	-	-	-	-	-	-	24	A-6a (V)	-	<L> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>> <>> >>>		
					43																			
					44																			
EOB																								
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE CAVE-IN AT 31.0'.																								
ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS																								

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 672+27, 30' RT.	EXPLORATION ID: B-027-0-20																
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																	
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 990.9 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1																
START: 9/1/20 END: 9/1/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.161679, -81.626075																	
MATERIAL DESCRIPTION AND NOTES	ELEV. 990.9	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI					
MEDIUM DENSE, BROWN, SANDY SILT, LITTLE CLAY, TRACE GRAVEL, CONTAINS TRACE ROOTS, DAMP	989.4			3 5 5	14	78	SS-1	-	6	13	40	28	13	NP	NP	NP	10	A-4a (1)	<100	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
MEDIUM DENSE, BROWN, SILT, LITTLE CLAY, TRACE SAND, TRACE GRAVEL, WET	987.9			2 5 5 7	16	100	SS-2	-	1	0	2	85	12	NP	NP	NP	25	A-4b (8)	-	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, TRACE SILT, TRACE GRAVEL, TRACE CLAY, MOIST	986.4			3 5 5 5	14	100	SS-3	-	-	-	-	-	-	-	-	-	15	A-3a (V)	-	<LV >> <LV >> <LV >> <LV >>
LOOSE, BROWN, SANDY SILT, TRACE CLAY, TRACE GRAVEL, WET	984.9			4 5 2 3 3	10	100	SS-4	-	-	-	-	-	-	-	-	-	22	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, TRACE SILT, TRACE GRAVEL, TRACE CLAY, DAMP	983.4	EOB		6 7 2 3 3 5	11	100	SS-5	-	-	-	-	-	-	-	-	-	6	A-3a (V)	-	<LV >> <LV >> <LV >> <LV >>
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																				
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																				

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 684+31, 29' LT.	EXPLORATION ID: B-030-0-20																																	
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																																		
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1002.6 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1																																	
START: 9/1/20 END: 9/1/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.164983, -81.626217																																		
MATERIAL DESCRIPTION AND NOTES	ELEV. 1002.6	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL																		
								GR	CS	FS	SI	CL	LL	PL	PI																						
HARD, GRAYISH BROWN, SANDY SILT, SOME CLAY, LITTLE GRAVEL, CONTAINS IRON STAINING, DAMP	1001.1	EOB	2	1	5	15	78	SS-1	4.50	14	13	15	36	22	28	18	10	12	A-4a (5)	5500	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>																
HARD, GRAY, SILT AND CLAY, LITTLE GRAVEL, LITTLE SAND, DAMP					1001.1	2	7	26	67	SS-2	4.50	18	7	9	38	28	28	17	11	12	A-6a (7)	-	<LV >> <LV >> <LV >> <LV >> <LV >>														
							995.1	3	4	19	100	SS-3	4.50	-	-	-	-	-	-	-	-	13	A-6a (V)	-	<LV >> <LV >> <LV >> <LV >>												
									995.1	4	6	12	100	SS-4	4.25	-	-	-	-	-	-	-	-	14	A-6a (V)	-	<LV >> <LV >> <LV >> <LV >>										
											995.1	5	3	12	100	SS-5	4.25	-	-	-	-	-	-	-	-	15	A-6a (V)	-	<LV >> <LV >> <LV >>								
													995.1	6	3	12	100	SS-5	4.25	-	-	-	-	-	-	-	-	15	A-6a (V)	-	<LV >> <LV >> <LV >>						
															995.1	7	4	12	100	SS-5	4.25	-	-	-	-	-	-	-	-	15	A-6a (V)	-	<LV >> <LV >>				
																	995.1	8	5	12	100	SS-5	4.25	-	-	-	-	-	-	-	-	15	A-6a (V)	-	<LV >> <LV >>		
																			995.1	9	6	12	100	SS-5	4.25	-	-	-	-	-	-	-	-	15	A-6a (V)	-	<LV >> <LV >>
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																																					
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVELLED, SOIL CUTTINGS																																					

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 708+46, 32' LT.	EXPLORATION ID: B-036-0-20																
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																	
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1031.1 (MSL) EOB: 7.5 ft.	PAGE: 1 OF 1																
START: 11/19/20 END: 11/19/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.171556, -81.626090																	
MATERIAL DESCRIPTION AND NOTES	ELEV. 1031.1	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI					
HARD, BROWN, SANDY SILT, LITTLE GRAVEL, LITTLE CLAY, DAMP	1029.6			2 1 3 4	10	67	SS-1	4.50	17	21	19	28	15	26	17	9	15	A-4a (2)	<100	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
HARD, BROWN MOTTLED WITH GRAY, SILTY CLAY, SOME SAND, TRACE GRAVEL, CONTAINS ROOTS, DAMP	1026.6			2 5 6 10 3 5 7 10 4 9 6 7	22	67	SS-2	4.50	7	10	16	40	27	34	18	16	15	A-6b (9)	-	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
HARD, BROWN, SILT AND CLAY, SOME SAND, LITTLE GRAVEL, DAMP	1023.6	EOB		5 6 7 4 5 8	18	89	SS-4	4.50	15	13	15	37	20	34	19	15	12	A-6a (6)	-	<LV >> <LV >> <LV >> <LV >>
					18	100	SS-5	4.50	-	-	-	-	-	-	-	-	16	A-6a (V)	-	<LV >> <LV >> <LV >>

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 720+49, 34' RT.	EXPLORATION ID: B-039-0-20																	
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																		
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1067.4 (MSL) EOB: 7.5 ft.	PAGE: 1 OF 1																	
START: 9/3/20 END: 9/3/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.174855, -81.625783																		
MATERIAL DESCRIPTION AND NOTES	ELEV. 1067.4	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL		
								GR	CS	FS	SI	CL	LL	PL	PI						
HARD, BROWN, SILT AND CLAY, SOME SAND, TRACE GRAVEL, DAMP	1062.9	EOB	2	3	11	89	SS-1	4.50	10	11	15	39	25	30	17	13	13	A-6a (7)	230	< LV >>T < LV >>T < LV >>T < LV >>T < LV >>T < LV >>T < LV >>T < LV >>T < LV >>T	
			1	5																	
			2	12																	
			3	13																	
			4	15																	
			5	5																	
			6	6																	
HARD, ORANGISH BROWN, SANDY SILT, LITTLE CLAY, LITTLE GRAVEL, CONTAINS IRON STAINING, DAMP	1059.9	EOB	7	7	18	100	SS-3	4.50	-	-	-	-	-	-	-	-	-	12	A-6a (V)	-	< LV >>T < LV >>T < LV >>T < LV >>T < LV >>T < LV >>T < LV >>T < LV >>T < LV >>T
			7	7																	
			8	7																	
			9	7																	
			10	7																	
			11	7																	
			12	7																	
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																					
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																					

PROJECT: SUM-77-24.12 TYPE: SUBGRADE PID: 111404 SFN: START: 11/17/20 END: 11/17/20	DRILLING FIRM / OPERATOR: NEAS / J. HODGES SAMPLING FIRM / LOGGER: NEAS / J. HODGES DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	DRILL RIG: CME 55X HAMMER: CME AUTOMATIC CALIBRATION DATE: 12/5/19 ENERGY RATIO (%): 81.9	STATION / OFFSET: 724+53, 41' LT. ALIGNMENT: IR-77 ELEVATION: 1080.3 (MSL) EOB: 7.5 ft. LAT / LONG: 41.175966, -81.626032	EXPLORATION ID B-040-0-20 PAGE 1 OF 1
	MATERIAL DESCRIPTION AND NOTES VERY STIFF, BROWN, SANDY SILT, LITTLE GRAVEL, LITTLE CLAY, DAMP	ELEV. 1080.3	DEPTHs	SPT/ RQD
				N ₆₀
				REC (%)
				SAMPLE ID
				HP (tsf)
				GRADATION (%)
				GR CS FS SI CL
				ATTERBERG
				LL PL PI
				WC
				ODOT CLASS (GI)
				SO4 ppm
				BACK FILL
	1077.3			
				1
				8
				16 7
				31 100
				SS-1 3.00
				16 15 29 28 12 18 13 5
				11 A-4a (1) 40
	1072.8			
				3
				8
				10 15
				34 100
				SS-2 -
				19 13 27 28 13 NP NP NP
				10 A-4a (1) -
				5
				12 15 15
				41 100
				SS-3 - - - - - - - -
				9 A-4a (V) -
				6
				9
				12 12
				33 100
				SS-4 - - - - - - - -
				9 A-4a (V) -
				7
				EOB
STANDARD ODOT LOG W/ SULFATES (8.5 X 11) - OH DOT GDT - 11/17/21 13:32 - X:ACTIVE PROJECTS\ACTIVE SOIL PROJECTS\SUM-77-24.12 GHENT TINT FILE				
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.				
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS				

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 732+51, 71' LT.	EXPLORATION ID B-042-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ENERGY RATIO (%): 81.9	ELEVATION: 1104.1 (MSL) EOB: 6.5 ft.	PAGE 1 OF 1															
START: 11/17/20 END: 11/17/20	SAMPLING METHOD: SPT		LAT / LONG: 41.178158, -81.626097																
MATERIAL DESCRIPTION AND NOTES	ELEV. 1104.1	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
				GR	CS	FS	SI	CL	LL	PL	PI								
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)	1102.6			1															
MEDIUM DENSE, BROWN, STONE FRAGMENTS WITH SAND AND SILT, TRACE CLAY, STONE FRAGMENTS ARE SHALE, DAMP	1101.1	TR		2	5	SS-1	-	32	21	13	25	9	22	16	6	8	A-2-4 (0)	150	
SHALE, BROWNISH GRAY, MODERATELY WEATHERED, WEAK TO MODERATELY STRONG, FISSILE, SILTY.	1097.6	EOB		3	9	SS-2	-	-	-	-	-	-	-	-	-	8	Rock (V)	-	
				4	36 50/4"	SS-3	-	-	-	-	-	-	-	-	-	6	Rock (V)	-	
				5	9 50/5"	SS-4	-	-	-	-	-	-	-	-	-	-	Rock (V)	-	
				6	50														

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES			DRILL RIG: CME 55X			STATION / OFFSET: 736+56, 40' RT.			EXPLORATION ID B-043-0-20																							
TYPE: SUBGRADE		SAMPLING FIRM / LOGGER: NEAS / J. HODGES			HAMMER: CME AUTOMATIC			ALIGNMENT: IR-77																										
PID: 111404	SFN: _____	DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 12/5/19			ELEVATION: 1116.6 (MSL) EOB: 7.5 ft.			PAGE 1 OF 1																							
START: 12/9/20	END: 12/9/20	SAMPLING METHOD: SPT			ENERGY RATIO (%): 81.9			LAT / LONG: 41.179263, -81.625669																										
MATERIAL DESCRIPTION AND NOTES		ELEV. 1116.6	DEPTH(S)		SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)		ATTERBERG		WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL																	
9.0" ASPHALT AND 4.0" BASE (DRILLERS DESCRIPTION)		1115.5			1																													
MEDIUM DENSE, BROWN AND BLACK, GRAVEL WITH SAND , LITTLE SILT, TRACE CLAY, DAMP		1113.6			2	6	16	SS-1	-	25	28	23	19	5	NP	NP	NP	8	A-1-b (0)	<100														
MEDIUM DENSE, BROWN, GRAVEL AND STONE FRAGMENTS WITH SAND AND SILT , LITTLE CLAY, MOIST TO DAMP		1110.6			3	4	5	SS-2	-	-	-	-	-	-	-	-	-	16	A-2-4 (V)	-														
MEDIUM DENSE, BROWN, COARSE AND FINE SAND , SOME SILT, LITTLE CLAY, LITTLE GRAVEL, MOIST		1109.1			4	5	15	SS-3	-	-	-	-	-	-	-	-	-	10	A-2-4 (V)	-														
		EOB																																
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																																		
ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS																																		

PROJECT: SUM-77-24.12 TYPE: SUBGRADE PID: 111404 SFN: _____ START: 9/3/20 END: 9/3/20	DRILLING FIRM / OPERATOR: NEAS / J. HODGES SAMPLING FIRM / LOGGER: NEAS / J. HODGES DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	DRILL RIG: CME 55X HAMMER: CME AUTOMATIC CALIBRATION DATE: 12/5/19 ENERGY RATIO (%): 81.9	STATION / OFFSET: 740+56, 34' LT. ALIGNMENT: IR-77 ELEVATION: 1127.6 (MSL) EOB: 7.5 ft. LAT / LONG: 41.180365, -81.625916	EXPLORATION ID B-044-0-20 PAGE 1 OF 1
	MATERIAL DESCRIPTION AND NOTES HARD, BROWN, SANDY SILT , LITTLE TO SOME CLAY, LITTLE TO SOME GRAVEL, CONTAINS ROOTS AND IRON STAINING, DAMP	ELEV. 1127.6	DEPTHs	SPT/ RQD
				N ₆₀ REC (%) SAMPLE ID HP (tsf)
				GR CS FS SI CL 1 2 3 7 44 SS-1 4.50 21 9 11 38 21 29 21 8 2 4 4 11 94 SS-2 4.25 12 11 15 42 20 25 18 7 3 1 1 3 22 SS-3 - - - - - - - - - - - - 4 1 1 3 22 SS-3 - - - - - - - - - - - - 5 7 9 22 56 SS-4 - - - - - - - - - - - - 6 3 4 10 67 SS-5 - - - - - - - - - - - -
				LL PL PI WC ODOT CLASS (GI) SO4 ppm BACK FILL
 SOFT, DARK BROWN, SANDY SILT , LITTLE CLAY, TRACE GRAVEL, MODERATELY ORGANIC, CONTAINS MANY ROOTS, RESEMBLES TOPSOIL, CONTAINS NO INTACT SOIL FOR HP READINGS, MOIST				
 MEDIUM DENSE, GRAY AND BROWN, GRAVEL AND STONE FRAGMENTS WITH SAND, SILT, AND CLAY , DAMP @6.0' - 7.5'; CONTAINS A RELIC ROCK STRUCTURE				
EOB				
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.				
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS				

PROJECT:	SUM-77-24.12	DRILLING FIRM / OPERATOR:	NEAS / J. HODGES	DRILL RIG:	CME 55X	STATION / OFFSET:	744+53, 32' RT.	EXPLORATION ID:													
TYPE:	SUBGRADE	SAMPLING FIRM / LOGGER:	NEAS / J. HODGES	HAMMER:	CME AUTOMATIC	ALIGNMENT:	IR-77	B-045-0-20													
PID:	111404	SFN:		DRILLING METHOD:	3.25" HSA	CALIBRATION DATE:	12/5/19	ELEVATION:	1139.4 (MSL)	EOB:	7.5 ft.	PAGE									
START:	9/3/20	END:	9/3/20	SAMPLING METHOD:	SPT	ENERGY RATIO (%):	81.9	LAT / LONG:	41.181451, -81.625652	1 OF 1											
MATERIAL DESCRIPTION AND NOTES		ELEV.	DEPTH(S)	SPT/RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)		ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL				
		1139.4			GR	CS	FS	SI	CL	LL	PL	PI									
VERY STIFF TO HARD, ORANGISH BROWN AND BROWN, SANDY SILT , LITTLE TO SOME GRAVEL AND STONE FRAGMENTS, LITTLE CLAY, CONTAINS IRON STAINING, DAMP					10 6 5	15	78	SS-1	4.50	24	9	15	33	19	25	18	7	13	A-4a (3)	170	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
			1133.4		1 2 3 4 5 6 7	15 5 6 3 5 6 8	100	SS-2	4.25	12	11	28	33	16	21	15	6	12	A-4a (3)	-	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
HARD, GRAY, SILT AND CLAY , SOME SAND, LITTLE STONE FRAGMENTS, DAMP			1131.9	EOB				SS-3	2.50	-	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
								SS-4	4.50	-	-	-	-	-	-	-	-	12	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>
								SS-5	4.50	-	-	-	-	-	-	-	-	12	A-6a (V)	-	<LV >> <LV >> <LV >>

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 756+55, 41' LT.	EXPLORATION ID B-048-0-20																		
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																			
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1170.9 (MSL)	PAGE																		
START: 11/16/20 END: 11/16/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.184752, -81.625850	1 OF 1																		
MATERIAL DESCRIPTION AND NOTES	ELEV. 1170.9	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL			
								GR	CS	FS	SI	CL	LL	PL	PI							
12.0" ASPHALT AND 4.0" BASE (DRILLERS DESCRIPTION)	1169.6			1																		
MEDIUM DENSE, BROWN AND DARK GRAY, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, CONTAINS ASPHALT FRAGMENTS, DAMP (FILL)	1167.9			2	5	6	19	11	SS-1	-	-	-	-	-	-	-	8	A-1-b (V)	110	<,>,<, >,>,< <,>,<, >,>,< <,>,<, >,>,< <,>,<, >,>,<		
HARD, BROWN AND GRAY, SILTY CLAY, LITTLE SAND, LITTLE GRAVEL, DAMP TO MOIST	1163.4	EOB		3	6	6	18	56	SS-2	4.50	12	7	13	39	29	34	17	17	15	A-6b (9)	-	
				4	6	7	19	67	SS-3	4.50	-	-	-	-	-	-	-	-	16	A-6b (V)	-	
				5	5	7	7		SS-4	4.50	-	-	-	-	-	-	-	-	21	A-6b (V)	-	
				6	5	6	20	100														
				7	9																	

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT:	SUM-77-24.12	DRILLING FIRM / OPERATOR:	NEAS / J. HODGES	DRILL RIG:	CME 55X	STATION / OFFSET:	760+56, 31' RT.	EXPLORATION ID:														
TYPE:	SUBGRADE	SAMPLING FIRM / LOGGER:	NEAS / J. HODGES	HAMMER:	CME AUTOMATIC	ALIGNMENT:	IR-77	B-049-0-20														
PID:	111404	SFN:		CALIBRATION DATE:	12/5/19	ELEVATION:	1174.8 (MSL)	EOB:														
START:	9/3/20	END:	9/3/20	SAMPLING METHOD:	SPT	ENERGY RATIO (%):	81.9	LAT / LONG:														
MATERIAL DESCRIPTION AND NOTES			ELEV.	DEPTH(S)	SPT/RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
			1174.8							GR	CS	FS	SI	CL	LL	PL	PI					
VERY STIFF, BROWN, SILTY CLAY, SOME GRAVEL, LITTLE SAND, CONTAINS ROOT HAIRS, DAMP			1173.3		1	3 4 6	14	44	SS-1	3.75	23	7	12	34	24	39	20	19	17	A-6b (8)	490	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
VERY STIFF TO HARD, BROWN MOTTLED WITH ORANGISH BROWN AND GRAY, CLAY, "AND" SILT, LITTLE SAND, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP TO MOIST			1167.3	EOB	2	6 8 10	25	67	SS-2	4.50	5	5	13	44	33	41	20	21	19	A-7-6 (13)	-	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
					3	2 5 7	16	100	SS-3	4.25	-	-	-	-	-	-	-	-	17	A-7-6 (V)	-	<LV >> <LV >> <LV >>
					4	2 5 7	12	100	SS-4	3.75	-	-	-	-	-	-	-	-	19	A-7-6 (V)	-	<LV >> <LV >>
					5	2 3 6	12	100	SS-5	2.50	-	-	-	-	-	-	-	-	21	A-7-6 (V)	-	<LV >> <LV >>
					6	2 4 5	12	100														<LV >> <LV >>
					7	2 4 5	12	100														<LV >> <LV >>

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 768+59, 32' RT.	EXPLORATION ID B-051-0-20																
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																	
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1181.9 (MSL)	PAGE																
START: 9/3/20 END: 9/3/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.188054, -81.625516	1 OF 1																
MATERIAL DESCRIPTION AND NOTES	ELEV. 1181.9	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI					
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)		1180.4		1																
HARD, BROWN, SANDY SILT, SOME GRAVEL, LITTLE CLAY, DAMP		1177.4		2	6 9 14	31	44	SS-1	4.50	-	-	-	-	-	-	-	12	A-4a (V)	<100	
HARD, BROWN, SILT AND CLAY, SOME SAND, SOME GRAVEL, CONTAINS IRON STAINING, DAMP		1174.4	EOB	3	4 16 7	31	44	SS-2	4.50	28	12	15	30	15	26	18	8	10	A-4a (2)	-
				4	4 6 8	19	100	SS-3	4.50	21	10	14	34	21	31	17	14	12	A-6a (6)	-
				5	5 6 10	22	100	SS-4	4.25	-	-	-	-	-	-	-	16	A-6a (V)	-	

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

STANDARD ODOT LOG W/ SULFATES (8.5 X 11) PROJECT: SUM-77-24.12 TYPE: SUBGRADE PID: 111404 SFN: _____ START: 11/16/20 END: 11/16/20	DRILLING FIRM / OPERATOR: NEAS / J. HODGES		DRILL RIG: CME 55X		STATION / OFFSET: 773+45, 23' LT.		EXPLORATION ID B-052-0-20									
	SAMPLING FIRM / LOGGER: NEAS / J. HODGES		HAMMER: CME AUTOMATIC		ALIGNMENT: IR-77											
	DRILLING METHOD: 3.25" HSA		CALIBRATION DATE: 12/5/19		ELEVATION: 1183.0 (MSL) EOB: 7.5 ft.		PAGE									
	SAMPLING METHOD: SPT		ENERGY RATIO (%): 81.9		LAT / LONG: 41.189390, -81.625691		1 OF 1									
	MATERIAL DESCRIPTION AND NOTES		ELEV. 1183.0	DEPTHs	SPT/ RQD	N ₆₀ REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)	ATTERBERG		WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)			1181.5		1											
MEDIUM DENSE, BROWN AND GRAY, GRAVEL WITH SAND AND SILT, TRACE CLAY, DAMP			1180.0		2	7 5	16 56	SS-1	- 31	22 14	23 10	10 25	17 8	10 A-2-4 (0)	67	
MEDIUM DENSE, BROWN, GRAVEL, SOME SAND, TRACE SILT, TRACE CLAY, DAMP			1178.5		3	7 6	18 44	SS-2	- 54	21 11	10 4	NP NP	NP NP	6 A-1-a (0)	-	
MEDIUM DENSE TO DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE CLAY, DAMP			1175.5		4	2 15 18	45 33	SS-3	- -	- -	- -	- -	- -	10 A-2-4 (V)	-	
				EOB	5	2 10	22 6	SS-4	- -	- -	- -	- -	- -	11 A-2-4 (V)	-	
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																
ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS																

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 784+58, 35' RT.	EXPLORATION ID: B-055-0-20																	
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																		
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1173.2 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1																	
START: 11/16/20 END: 11/16/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.192449, -81.625466																		
MATERIAL DESCRIPTION AND NOTES	ELEV. 1173.2	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL		
								GR	CS	FS	SI	CL	LL	PL	PI						
STIFF TO HARD, BROWN, SILTY CLAY, LITTLE TO SOME SAND, TRACE TO LITTLE GRAVEL, CONTAINS TRACE ROOTS AND IRON STAINING, DAMP		EOB	3	3	10	44	SS-1	1.50	14	12	19	31	24	39	22	17	20	A-6b (7)	120	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>	
			1	4																	
			2	3	15	67	SS-2	4.50	2	3	8	40	47	37	20	17	18	A-6b (11)	-	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>	
			3	5																	
			4	6	22	33	SS-3	3.25	-	-	-	-	-	-	-	-	-	18	A-6b (V)	-	<LV >> <LV >> <LV >> <LV >>
			5	5																	
			6	6	15	100	SS-4	1.75	-	-	-	-	-	-	-	-	-	14	A-6b (V)	-	<LV >> <LV >> <LV >>
			7	4	15	100	SS-5	4.50	-	-	-	-	-	-	-	-	-	12	A-6b (V)	-	<LV >> <LV >> <LV >>

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 789+10, 34' LT.	EXPLORATION ID: B-056-0-20																		
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																			
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1168.1 (MSL) EOB: 7.5 ft.	PAGE: 1 OF 1																		
START: 11/16/20 END: 11/16/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.193689, -81.625722																			
MATERIAL DESCRIPTION AND NOTES	ELEV. 1168.1	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL			
								GR	CS	FS	SI	CL	LL	PL	PI							
VERY STIFF, BROWN, SILT AND CLAY, SOME SAND, TRACE GRAVEL, CONTAINS TRACE IRON STAINING, DAMP		1166.6	2 3 4 5 6 7 8	1	14	100	SS-1	2.50	10	9	17	39	25	30	17	13	14	A-6a (7)	350	< L V > > < L V > > < L V > > < L V > >		
VERY STIFF TO HARD, BROWN MOTTLED WITH ORANGISH BROWN AND GRAY, SILTY CLAY, SOME SAND, TRACE TO LITTLE GRAVEL, CONTAINS TRACE IRON STAINING, DAMP				2	19	39	SS-2	3.75	11	9	20	37	23	37	20	17	17	17	A-6b (8)	-	< L V > > < L V > > < L V > >	
				3	23	100	SS-3	2.75	-	-	-	-	-	-	-	-	-	16	A-6b (V)	-	< L V > > < L V > >	
				4	14	100	SS-4	3.00	-	-	-	-	-	-	-	-	-	14	A-6b (V)	-	< L V > > < L V > >	
				5	12	100	SS-5	4.50	-	-	-	-	-	-	-	-	-	16	A-6b (V)	-	< L V > > < L V > >	
				6																		< L V > > < L V > >
				7																		< L V > > < L V > >
			EOB																			
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																						
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVEL ED, SOIL CUTTINGS																						

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 793+08, 72' RT.	EXPLORATION ID B-057-0-20																
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																	
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1164.9 (MSL)	PAGE																
START: 12/9/20 END: 12/9/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.194780, -81.625340	1 OF 1																
MATERIAL DESCRIPTION AND NOTES	ELEV. 1164.9	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI					
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)	1163.4			1																
MEDIUM DENSE, BROWN, SANDY SILT, LITTLE GRAVEL, LITTLE CLAY, DAMP	1161.9			2	4	14	100	SS-1	-	18	18	14	36	14	NP	NP	NP	10	A-4a (3)	<100
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, LITTLE SILT, LITTLE GRAVEL, LITTLE CLAY, DAMP TO MOIST	1158.9			3	5	15	89	SS-2	-	17	27	26	19	11	NP	NP	NP	11	A-3a (0)	-
VERY STIFF, BROWN, SILT AND CLAY, SOME SAND, TRACE GRAVEL, MOIST	1157.4	EOB		4	5	12	100	SS-3	-	-	-	-	-	-	-	-	-	18	A-3a (V)	-
				5	4	11	100	SS-4	2.50	-	-	-	-	-	-	-	-	17	A-6a (V)	-
				6	5															
				7	4															

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 797+10, 38' LT.	EXPLORATION ID: B-058-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1161.2 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1															
START: 11/16/20 END: 11/16/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.195883, -81.625746																
MATERIAL DESCRIPTION AND NOTES	ELEV. 1161.2	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI				
HARD, BROWN, SANDY SILT, LITTLE CLAY, TRACE GRAVEL, DAMP	1158.2	1																	
		2	7	4	11	56	SS-1	4.50	10	19	24	29	18	22	14	8	12	A-4a (2)	110
		3	2	4	8	67	SS-2	2.25	7	6	14	38	35	33	16	17	20	A-6b (10)	-
		4	3	3	5	44	SS-3	2.00	-	-	-	-	-	-	-	-	15	A-6b (V)	-
		5	2	2	7	44	SS-4	3.00	-	-	-	-	-	-	-	-	20	A-6b (V)	-
		6	2	2	3	44													
		7	2	3	7	44													
				EOB															
STIFF TO VERY STIFF, BROWNISH GRAY, SILTY CLAY, LITTLE SAND, TRACE GRAVEL, MOIST TO DAMP																			

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 805+10, 40' LT.	EXPLORATION ID B-060-0-20																		
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																			
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ENERGY RATIO (%): 81.9	ELEVATION: 1160.8 (MSL)	EOB: 7.5 ft.																		
START: 11/16/20 END: 11/16/20	SAMPLING METHOD: SPT	LAT / LONG: 41.198078, -81.625761	PAGE 1 OF 1																			
MATERIAL DESCRIPTION AND NOTES	ELEV. 1160.8	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL			
								GR	CS	FS	SI	CL	LL	PL	PI							
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)	1159.3			1																		
VERY STIFF, BROWN, SANDY SILT, LITTLE GRAVEL, LITTLE CLAY, DAMP	1157.8			2	9	6	14	39	SS-1	3.50	15	16	30	26	13	18	13	5	11	A-4a (1)	-	
STIFF, BROWN AND GRAY, SILT AND CLAY, "AND" SAND, LITTLE GRAVEL, DAMP	1156.3			3	2	11	4	31	SS-2	1.50	11	9	29	31	20	27	15	12	15	A-6a (4)	-	
HARD, BROWN, SANDY SILT, LITTLE CLAY, LITTLE GRAVEL, DAMP	1153.3	EOB		4	11	12																
				5	6	7	8	20	SS-3	4.50	-	-	-	-	-	-	-	-	10	A-4a (V)	-	
				6	6	7	9	22	SS-4	4.50	-	-	-	-	-	-	-	-	13	A-4a (V)	-	
				7	9																	

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 809+75, 34' RT.	EXPLORATION ID: B-061-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1162.0 (MSL) EOB: 7.5 ft.	PAGE: 1 OF 1															
START: 10/15/20 END: 10/15/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.199354, -81.625497																
MATERIAL DESCRIPTION AND NOTES	ELEV. 1162.0	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI				
STIFF TO VERY STIFF, BROWN MOTTLED WITH ORANGISH BROWN, SILT AND CLAY , SOME SAND, TRACE GRAVEL, CONTAINS TRACE IRON STAINING, DAMP TO MOIST	1157.5	EOB	2	3	8	SS-1	2.00	10	8	17	38	27	28	17	11	15	A-6a (6)	<100	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
			1	3															
			2	3	11	SS-2	2.00	7	7	14	42	30	32	18	14	20	A-6a (9)	-	<LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >> <LV >>
			3	3															
			4	4	11	SS-3	2.50	-	-	-	-	-	-	-	-	19	A-6a (V)	-	<LV >> <LV >> <LV >> <LV >> <LV >>
			5	6	19	SS-4	4.50	-	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>
			6	4	20	SS-5	4.50	-	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>
HARD, BROWN, SANDY SILT , LITTLE CLAY, TRACE GRAVEL, CONTAINS TRACE IRON STAINING, DAMP	1154.5	EOB	7	6	100	SS-6	5.00	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>	
			8	9															
			9	10	100	SS-7	5.00	-	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>
			10	11	100	SS-8	5.00	-	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>
			11	12	100	SS-9	5.00	-	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>
			12	13	100	SS-10	5.00	-	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>
			13	14	100	SS-11	5.00	-	-	-	-	-	-	-	-	13	A-4a (V)	-	<LV >> <LV >> <LV >> <LV >>

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 813+15, 40' LT.	EXPLORATION ID B-062-0-20																
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																	
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ENERGY RATIO (%): 81.9	ELEVATION: 1164.5 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1																
START: 11/16/20 END: 11/16/20	SAMPLING METHOD: SPT		LAT / LONG: 41.200288, -81.625770																	
MATERIAL DESCRIPTION AND NOTES	ELEV. 1164.5	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI					
12.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)	1163.0			1																
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, TRACE SILT, TRACE CLAY, DAMP	1161.7			2	11 15 6	29	44	SS-1	-	-	-	-	-	-	-	-	9	A-3a (V)	<100	
HARD, BROWN, SILT AND CLAY, LITTLE SAND, TRACE GRAVEL, DAMP	1157.0	EOB		3	6 9 11	27	67	SS-2	4.50	1	5	9	44	41	30	19	11	15	A-6a (8)	-
				4	6 10 14	33	78	SS-3	4.50	8	6	11	40	35	32	18	14	15	A-6a (10)	-
				5	5 10 16	35	67	SS-4	4.50	-	-	-	-	-	-	-	14	A-6a (V)	-	

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 816+93, 27' RT.	EXPLORATION ID: B-063-0-20																			
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																				
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1165.0 (MSL) EOB: 7.5 ft.	PAGE: 1 OF 1																			
START: 11/16/20 END: 11/16/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.201325, -81.625530																				
MATERIAL DESCRIPTION AND NOTES	ELEV. 1165.0	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL				
								GR	CS	FS	SI	CL	LL	PL	PI								
VERY STIFF, BROWN, SILT AND CLAY, SOME SAND, LITTLE GRAVEL, CONTAINS TRACE IRON STAINING, DAMP	1163.5	EOB		1	11	100	SS-1	2.25	14	13	20	29	24	30	17	13	17	A-6a (5)	140	< LV >> < LV >> < LV >> < LV >> < LV >> < LV >> < LV >> < LV >>			
STIFF TO VERY STIFF, BROWN MOTTLED WITH ORANGISH BROWN AND GRAY, CLAY, "AND" SILT, LITTLE SAND, TRACE GRAVEL, CONTAINS IRON STAINING, MOIST							2	8	100	SS-2	2.25	1	4	10	38	47	43	21	22	23	A-7-6 (13)	-	< LV >> < LV >> < LV >> < LV >> < LV >> < LV >> < LV >> < LV >>
							3	5															< LV >> < LV >> < LV >>
							4	15	89	SS-3	1.50	-	-	-	-	-	-	-	-	24	A-7-6 (V)	-	< LV >> < LV >> < LV >>
							5	18	100	SS-4	1.75	-	-	-	-	-	-	-	-	28	A-7-6 (V)	-	< LV >> < LV >> < LV >>
							6	18	100	SS-5	3.75	-	-	-	-	-	-	-	-	23	A-7-6 (V)	-	< LV >> < LV >> < LV >>
							7																< LV >> < LV >> < LV >>
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																							
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVEL ED, SOIL CUTTINGS																							

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 221+81, 15' RT.	EXPLORATION ID B-069-0-20																	
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: RAMP P																		
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ENERGY RATIO (%): 81.9	ELEVATION: 1007.8 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1																	
START: 11/7/20 END: 11/7/20	SAMPLING METHOD: SPT	LAT / LONG: 41.150290, -81.633101																			
MATERIAL DESCRIPTION AND NOTES 8.0" ASPHALT AND 4.0" BASE (DRILLERS DESCRIPTION) MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE TO LITTLE CLAY, CONTAINS IRON STAINING, DAMP	ELEV. 1007.8	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL		
				GR	CS	FS	SI	CL	LL	PL	PI										
	1006.8			1																	
				2	5	6	16	44	SS-1	-	-	-	-	-	-	-	-	11	A-2-4 (V)	<100	
				3	9	6	25	78	SS-2	-	24	25	22	22	7	21	16	5	11	A-2-4 (O)	-
				4	9	9															
				5	3	5	12	100	SS-3	-	-	-	-	-	-	-	-	10	A-2-4 (V)	-	
				6	4	4	12	100	SS-4	-	-	-	-	-	-	-	-	14	A-2-4 (V)	-	
				7	4	5															
	1000.3	EOB																			

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 218+57, 15' RT.	EXPLORATION ID B-070-0-20																		
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: RAMP P																			
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ENERGY RATIO (%): 81.9	ELEVATION: 1009.4 (MSL)	EOB: 7.5 ft.	PAGE 1 OF 1																	
START: 12/7/20 END: 12/7/20	SAMPLING METHOD: SPT		LAT / LONG: 41.150671, -81.634118																			
MATERIAL DESCRIPTION AND NOTES	ELEV. 1009.4	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL			
10.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)		1008.1		1				GR	CS	FS	SI	CL	LL	PL	PI							
HARD, BROWN AND GRAY, SANDY SILT, LITTLE GRAVEL, LITTLE CLAY, DAMP		1006.4		2	6	8	22	89	SS-1	4.50	20	18	17	31	14	25	17	8	13	A-4a (2)	<100	
VERY STIFF, BROWN AND GRAY, SILT AND CLAY, SOME SAND, TRACE GRAVEL, DAMP		1003.4		3	6	4	14	100	SS-2	2.50	0	7	21	50	22	30	19	11	18	A-6a (8)	-	
LOOSE, BROWN, GRAVEL WITH SAND AND SILT, LITTLE CLAY, MOIST	DH	1001.9	EOB	4	3	3	10	100	SS-3	2.50	-	-	-	-	-	-	-	-	17	A-6a (V)	-	
				5	3	4																
				6	3	3																
				7	3	2																

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

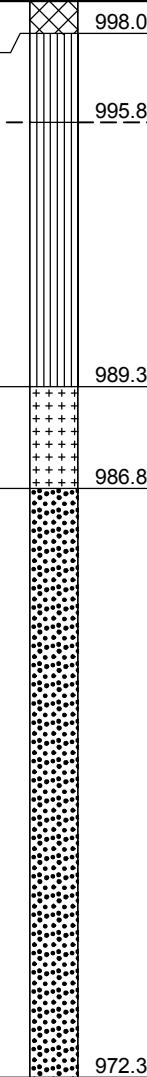
PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / JL			DRILL RIG: CME 55T			STATION / OFFSET: 12+26, 52' LT.			EXPLORATION ID B-071-1-20							
TYPE: LIGHT TOWER		SAMPLING FIRM / LOGGER: NEAS / JL			HAMMER: CME AUTOMATIC			ALIGNMENT: RAMP R										
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 12/5/19			ELEVATION: 1000.1 (MSL) EOB: 26.5 ft.			PAGE							
START: 9/22/21 END: 9/22/21		SAMPLING METHOD: SPT			ENERGY RATIO (%): 68.4			LAT / LONG: 41.151369, -81.632552			1 OF 1							
MATERIAL DESCRIPTION AND NOTES	ELEV. 1000.1	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)				ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
								GR	CS	FS	SI	CL	LL	PL				
6.0" TOPSOIL (DRILLERS DESCRIPTION) LOOSE, BROWN, GRAVEL WITH SAND, SILT, AND CLAY, DAMP	999.6																	
		1																
		2																
		3	4	5	10	100	SS-1	-	27	22	17	22	12	31	20	11	11 A-2-6 (0) -	
		4																
		5	2	4	8	33	SS-2	-	-	-	-	-	-	-	-	-	14 A-2-6 (V) -	
		6	3	4														
		7																
		8	2	3	7	22	SS-3	-	-	-	-	-	-	-	-	-	12 A-2-4 (V) -	
		9																
		10	2	4	13	56	SS-4	-	46	23	8	16	7	27	18	9	12 A-2-4 (0) -	
		11	7															
		12																
		13	3	3	6	44	SS-5	-	-	-	-	-	-	-	-	-	9 A-1-b (V) -	
		14	2															
		15																
		16	2	2	3	50	SS-6	-	16	49	26	8	1	NP	NP	NP	9 A-1-b (0) -	
		17																
		18	2	3	8	89	SS-7	-	-	-	-	-	-	-	-	-	8 A-1-b (V) -	
		19		4														
		20																
		21	7	6	14	67	SS-8	-	-	-	-	-	-	-	-	-	7 A-1-b (V) -	
		22																
		23	6	7	17	56	SS-9	-	-	-	-	-	-	-	-	-	7 A-1-b (V) -	
		24																
		25	8	7	17	78	SS-10	-	-	-	-	-	-	-	-	-	8 A-1-b (V) -	
		26		8														
		EOB																
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.																		
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																		

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 17+63, 9' LT.	EXPLORATION ID B-072-0-20																	
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: RAMP R																		
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1006.1 (MSL)	EOB: 7.5 ft.	PAGE 1 OF 1																	
START: 12/7/20 END: 12/7/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.9	LAT / LONG: 41.151475, -81.632363																		
MATERIAL DESCRIPTION AND NOTES	ELEV. 1006.1	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL		
								GR	CS	FS	SI	CL	LL	PL	PI						
9.0" ASPHALT AND 6.0" BASE (DRILLERS DESCRIPTION)		1004.8		1																	
MEDIUM DENSE TO VERY DENSE, BROWN AND BLACK, GRAVEL AND STONE FRAGMENTS WITH SAND, LITTLE SILT, TRACE CLAY, CONTAINS ASPHALT FRAGMENTS, MOIST TO WET (FILL)		1001.6		2	10 23 22	61	100	SS-1	-	46	21	14	15	4	NP	NP	NP	11	A-1-b (0)	280	
HARD, BROWN, SANDY SILT, LITTLE CLAY, LITTLE GRAVEL, DAMP		998.6	EOB	3	7																
				4	5 6	15	44	SS-2	-	-	-	-	-	-	-	-	-	18	A-1-b (V)	-	
				5	5 7 12	26	100	SS-3	4.50	14	19	21	29	17	23	14	9	12	A-4a (2)	-	
				6	4	5	19	SS-4	4.50	-	-	-	-	-	-	-	-	10	A-4a (V)	-	
				7	9																

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH			DRILL RIG: CME 45B			STATION / OFFSET: 118+92, 0' LT.			EXPLORATION ID B-074-0-20												
TYPE: NOISE WALL		SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH			HAMMER: CME AUTOMATIC			ALIGNMENT: RAMP L															
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 12/5/19			ELEVATION: 998.0 (MSL) EOB: 26.5 ft.			PAGE 1 OF 1												
START: 10/13/20 END: 10/13/20		SAMPLING METHOD: SPT			ENERGY RATIO (%): 81.7			LAT / LONG: 41.148826, -81.632906															
MATERIAL DESCRIPTION AND NOTES			ELEV. 998.0	DEPTH(S)	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)		ATTERBERG	ODOT CLASS (GI)	SO4 ppm	BACK FILL								
6.0" ASPHALT AND 7.0" BASE (DRILLERS DESCRIPTION)			996.9			1				GR	CS	FS	SI	CL	LL	PL	PI	WC					
LOOSE, BROWN, COARSE AND FINE SAND, LITTLE GRAVEL, LITTLE SILT, TRACE CLAY, DAMP			995.0			2	6	SS-1	-	-	-	-	-	-	-	-	-	8	A-3a (V)	127			
VERY STIFF, BROWN AND ORANGISH BROWN, SANDY SILT, LITTLE GRAVEL, LITTLE CLAY, CONTAINS TRACE IRON STAINING, DAMP			993.5			3	4	3	10	39	SS-2	3.00	20	18	22	25	15	22	15	7	12	A-4a (1)	-
VERY STIFF, BROWN MOTTLED WITH ORANGISH BROWN AND BLACK, SILTY CLAY, SOME SAND, TRACE GRAVEL, CONTAINS IRON STAINING, SLIGHTLY ORGANIC, MOIST			992.0			4	5		12	50	SS-3	2.75	8	13	17	41	21	40	24	16	30	A-6b (8)	-
MEDIUM STIFF TO STIFF, BROWN AND ORANGISH BROWN, SANDY SILT, TRACE TO SOME GRAVEL, TRACE TO LITTLE CLAY, DAMP TO MOIST						5	2	4	8	67	SS-4	1.00	-	-	-	-	-	-	-	23	A-4a (V)	-	
@10.0' - 14.0'; SS-6 AND SS-7 BECOME HARD						6	3		10	78	SS-5	0.75	-	-	-	-	-	-	-	18	A-4a (V)	-	
						7	4	3			SS-6	4.50	25	12	13	36	14	25	18	7	16	A-4a (3)	-
						8	3	4	14	61	SS-7	4.50	-	-	-	-	-	-	-	19	A-4a (V)	-	
						9	6				SS-8	-	-	-	-	-	-	-	-	19	A-4a (V)	-	
						10	3	4	11	78	SS-9	-	6	16	39	29	10	NP	NP	NP	19	A-4a (1)	-
						11	4	4			SS-10	-	-	-	-	-	-	-	-	27	A-4b (V)	-	
						12					SS-11	-	-	-	-	-	-	-	-	23	A-4b (V)	-	
						13	4	3	10	56	SS-12	-	0	0	21	75	4	NP	NP	NP	26	A-4b (8)	-
						14	4	4															
						15	3	3	8	50													
						16	3	3															
						17																	
						18	2	3	10	56													
						19	3	4															
						20																	
						21	5	5	18	83													
						22																	
						23	4	4	10	89													
						24																	
						25	5	3	11	100													
						26	5	5															
						EOB																	
NOTES: GROUNDWATER ENCOUNTERED AT 14.0' DURING DRILLING. HOLE CAVED-IN AT 4.0'.																							
ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; Poured 0.5 BAG HOLE PLUG; SHOVED SOIL CUTTINGS																							

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH			DRILL RIG: CME 45B			STATION / OFFSET: 122+95, 25' RT.			EXPLORATION ID B-076-0-20										
TYPE: NOISE WALL		SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH			HAMMER: CME AUTOMATIC			ALIGNMENT: RAMP L													
PID: 111404 SFN: _____		DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 12/5/19			ELEVATION: 998.8 (MSL) EOB: 26.5 ft.			PAGE 1 OF 1										
START: 10/14/20 END: 10/14/20		SAMPLING METHOD: SPT			ENERGY RATIO (%): 81.7			LAT / LONG: 41.149214, -81.631546													
MATERIAL DESCRIPTION AND NOTES		ELEV. 998.8	DEPTHs		SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)			ATTERBERG								
		998.0			1					GR	CS	FS	LL								
10.0" BASE/ASPHALT MILLINGS (DRILLERS DESCRIPTION) HARD, BROWN, SANDY SILT , LITTLE GRAVEL, TRACE CLAY, CONTAINS IRON STAINING, DAMP		995.8			2	6	5	SS-1	4.50	19	18	25	28	10	20	16	4	10	A-4a (1)	100	
MEDIUM DENSE, BROWN, SANDY SILT , TRACE CLAY, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP TO WET		989.3			3	5	4	SS-2	-	7	4	41	41	7	NP	NP	NP	13	A-4a (3)	-	
STIFF, BROWN, SILT , SOME CLAY, TRACE SAND, TRACE GRAVEL, CONTAINS IRON STAINING, WET		986.8			4	3	5	SS-3	-	-	-	-	-	-	-	-	-	13	A-4a (V)	-	
LOOSE TO MEDIUM DENSE, BROWN BECOMING GRAY, COARSE AND FINE SAND , LITTLE TO SOME SILT, TRACE CLAY, TRACE GRAVEL, CONTAINS INTERBEDDED SILT LAYERS, CONTAINS IRON STAINING, MOIST TO WET		984.3			5	4	4	SS-4	-	-	-	-	-	-	-	-	-	9	A-4a (V)	-	
					6	6	7	SS-5	-	-	-	-	-	-	-	-	-	25	A-4a (V)	-	
					7	5	7	SS-6	1.75	0	0	1	68	31	31	26	5	32	A-4b (8)	-	
					8	4	6	SS-7	-	-	-	-	-	-	-	-	-	19	A-3a (V)	-	
					9	7	7	SS-8	-	-	-	-	-	-	-	-	-	30	A-3a (V)	-	
					10	5	7	SS-9	-	-	-	-	-	-	-	-	-	18	A-3a (V)	-	
					11	4	6	SS-10	-	-	-	-	-	-	-	-	-	23	A-3a (V)	-	
					12	3	3	SS-11	-	-	-	-	-	-	-	-	-	25	A-3a (V)	-	
					13	4	6	SS-12	-	-	-	-	-	-	-	-	-	22	A-3a (V)	-	
					14	7	7														
					15	4	3														
					16	4	3														
					17																
					18																
					19																
					20																
					21																
					22																
					23																
					24																
					25																
					26																
NOTES: GROUNDWATER ENCOUNTERED AT 14.5' DURING DRILLING, 16.0' AFTER COMPLETION. HOLE DID NOT CAVE.																					
ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; POURED 0.5 BAG HOLE PLUG; SHOVED SOIL CUTTINGS																					

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH				DRILL RIG: CME 45B				STATION / OFFSET: 126+90, 5' RT.				EXPLORATION ID: B-078-0-20									
TYPE: NOISE WALL		SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH				HAMMER: CME AUTOMATIC				ALIGNMENT: RAMP L													
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA				CALIBRATION DATE: 12/5/19				ELEVATION: 1007.6 (MSL) EOB: 26.5 ft.				PAGE 1 OF 1									
START: 10/14/20 END: 10/15/20		SAMPLING METHOD: SPT				ENERGY RATIO (%): 81.7				LAT / LONG: 41.149662, -81.630231													
MATERIAL DESCRIPTION AND NOTES				ELEV. 1007.6	DEPTHs		SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)			ATTERBERG		WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL			
10.0" BASE/ASPHALT MILLINGS (DRILLERS DESCRIPTION)				1006.8	1001.6	1						GR	CS	FS	SI	CL	LL	PL	PI				
HARD, BROWN, SILT AND CLAY , TRACE TO LITTLE SAND, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP						2	4	6	18	78	SS-1	4.50	10	3	5	45	37	35	20	15	19	A-6a (10)	<100
						3	5	7															
						4	5	8	18	100	SS-2	4.50	9	7	8	45	31	32	20	12	17	A-6a (9)	-
						5	6	8	25	78	SS-3	4.50	-	-	-	-	-	-	-	-	19	A-6a (V)	-
						6	7	10															
						7	7	12	26	83	SS-4	4.50	-	-	-	-	-	-	-	-	20	A-6b (V)	-
						8	6																
						9	7	11	25	67	SS-5	4.50	0	3	5	49	43	35	19	16	20	A-6b (10)	-
						10	5																
						11	8	10	25	56	SS-6	3.50	-	-	-	-	-	-	-	-	20	A-6b (V)	-
						12																	
VERY STIFF TO HARD, BROWN, SILTY CLAY , TRACE SAND, TRACE GRAVEL, MOIST						13	7	9	27	89	SS-7	4.00	0	2	4	48	46	36	22	14	21	A-6a (10)	-
						14																	
VERY STIFF TO HARD, BROWN, SILT AND CLAY , TRACE SAND, TRACE GRAVEL, DAMP TO MOIST						15	4				SS-8A	4.25	-	-	-	-	-	-	-	-	23	A-6a (V)	-
						16	4	6	14	67	SS-8B	-	-	-	-	-	-	-	-	-	9	A-3a (V)	-
MEDIUM DENSE, BROWN, COARSE AND FINE SAND , LITTLE TO SOME SILT, TRACE TO LITTLE GRAVEL, TRACE CLAY, CONTAINS IRON STAINING, DAMP						17																	
						18	5	7	19	61	SS-9	-	-	-	-	-	-	-	-	-	7	A-3a (V)	-
						19																	
						20	4				SS-10	-	-	-	-	-	-	-	-	-	7	A-3a (V)	-
						21	4	7	15	61	SS-10	-	-	-	-	-	-	-	-	-	7	A-3a (V)	-
						22																	
						23	5				SS-11	-	-	-	-	-	-	-	-	-	5	A-3a (V)	-
						24	6	9	20	78	SS-11	-	-	-	-	-	-	-	-	-	14	A-3a (V)	-
						25	4				SS-12	-	-	-	-	-	-	-	-	-			
						26	6	7	18	83													
EOB																							

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH	DRILL RIG: CME 45B	STATION / OFFSET: 127+44, 73' RT.	EXPLORATION ID B-080-0-20																
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH	HAMMER: CME AUTOMATIC	ALIGNMENT: RAMP M																	
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1002.8 (MSL)	PAGE																
START: 10/15/20 END: 10/15/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.7	LAT / LONG: 41.149991, -81.629003	1 OF 1																
MATERIAL DESCRIPTION AND NOTES	ELEV. 1002.8	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI					
6.0" ASPHALT AND 7.0" BASE (DRILLERS DESCRIPTION)	1001.7			1																
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, SOME GRAVEL, TRACE SILT, TRACE CLAY, DAMP (FILL)	999.8			2	5	14	44	SS-1	-	-	-	-	-	-	-	3	A-3a (V)	<100		
MEDIUM DENSE, BROWN, GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, CONTAINS BRICK FRAGMENTS, DAMP (FILL)	998.3			3	5	9	20	SS-2	-	40	19	19	16	6	NP	NP	NP	6	A-1-b (0)	-
MEDIUM DENSE, BROWN, SANDY SILT, TRACE CLAY, TRACE GRAVEL, DAMP	995.3	EOB		4	6	6	19	SS-3	-	8	24	30	28	10	NP	NP	NP	11	A-4a (1)	-
				5	6	8	18	SS-4	-	-	-	-	-	-	-	-	-	11	A-4a (V)	-
				6	8	5														
				7																

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH	DRILL RIG: CME 45B	STATION / OFFSET: 27+99, 26' LT.	EXPLORATION ID B-081-0-20																		
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH	HAMMER: CME AUTOMATIC	ALIGNMENT: RAMP N																			
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1010.5 (MSL)	PAGE																		
START: 10/15/20 END: 10/15/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.7	LAT / LONG: 41.150109, -81.629687	1 OF 1																		
MATERIAL DESCRIPTION AND NOTES	ELEV. 1010.5	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL			
								GR	CS	FS	SI	CL	LL	PL	PI							
6.0" ASPHALT AND 7.0" BASE (DRILLERS DESCRIPTION)	1009.4			1																		
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, LITTLE SILT, LITTLE CLAY, LITTLE GRAVEL, CONTAINS ROOTS, DAMP	1007.5			2	4	6	16	44	SS-1	-	-	-	-	-	-	-	10	A-3a (V)	<100			
MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE CLAY, DAMP	1006.0			3	4	5	7	16	56	SS-2	-	24	23	20	23	10	NP	NP	NP	8	A-2-4 (0)	-
HARD, BROWN, SILT AND CLAY, LITTLE SAND, TRACE GRAVEL, DAMP TO MOIST	1003.0	EOB		4	6	7	18	67	SS-3	4.50	2	4	7	49	38	35	20	15	19	A-6a (10)	-	
				5	4	6	7	19	67	SS-4	4.50	-	-	-	-	-	-	-	21	A-6a (V)	-	

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

STANDARD ODOT LOG W/ SULFATES (8.5 X 11) PROJECT: SUM-77-24.12 TYPE: SUBGRADE PID: 111404 SFN: _____ START: 10/15/20 END: 10/15/20	DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	DRILL RIG: CME 45B HAMMER: CME AUTOMATIC CALIBRATION DATE: 12/5/19 ENERGY RATIO (%): 81.7	STATION / OFFSET: 336+08, 58' RT. ALIGNMENT: IR-77 NB ELEVATION: 975.5 (MSL) EOB: 7.5 ft. LAT / LONG: 41.152081, -81.628359	EXPLORATION ID B-083-0-20 PAGE 1 OF 1	
	MATERIAL DESCRIPTION AND NOTES 6.0" ASPHALT AND 7.0" BASE (DRILLERS DESCRIPTION) MEDIUM DENSE, BROWN AND ORANGISH BROWN, SANDY SILT, LITTLE GRAVEL, TRACE CLAY, CONTAINS IRON STAINING, DAMP @1.5'; SS-1 NO RECOVERY	ELEV. 975.5	DEPTHs	SPT/ RQD	
		974.4		N ₆₀ REC (%)	
			1		
			2	5 9 10	
			3		
MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, LITTLE CLAY, DAMP		971.0		HP (tsf)	
			4	5 5 8	
			5	5 8 7	
			6	6 7	
			7	11	
		968.0	EOB		
NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.					
ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS					

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 786+82, 97' LT.	EXPLORATION ID B-084-0-20																			
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																				
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ENERGY RATIO (%): 81.9	ELEVATION: 1170.5 (MSL) EOB: 7.5 ft.	PAGE 1 OF 1																			
START: 12/10/20 END: 12/10/20	SAMPLING METHOD: SPT		LAT / LONG: 41.193063, -81.625949																				
MATERIAL DESCRIPTION AND NOTES 6.0" ASPHALT (DRILLERS DESCRIPTION) VERY STIFF, BROWN MOTTLED WITH GRAY AND ORANGISH BROWN, SILT AND CLAY, LITTLE TO SOME SAND, LITTLE TO SOME GRAVEL, CONTAINS IRON STAINING, DAMP TO MOIST	ELEV. 1170.5	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL				
				GR	CS	FS	SI	CL	LL	PL	PI												
	1170.0			1																			
				2	9	7	19	100	SS-1	3.00	12	8	11	36	33	32	18	14	17	A-6a (8)	<100		
				3	3	2	10	44	SS-2	3.75	-	-	-	-	-	-	-	-	16	A-6a (V)	-		
				4	5	5			SS-3	3.50	21	8	13	39	19	30	19	11	17	A-6a (5)	-		
				5	6	8	20	39	SS-4	3.00	-	-	-	-	-	-	-	-	20	A-6a (V)	-		
				6	5	7	16	56															
				7																			
	1163.0	EOB																					

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / J. HODGES	DRILL RIG: CME 55X	STATION / OFFSET: 23+06, 14' RT.	EXPLORATION ID B-085-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / J. HODGES	HAMMER: CME AUTOMATIC	ALIGNMENT: RAMP D																
PID: 111404 SFN: 3.25" HSA	CALIBRATION DATE: 12/5/19	ENERGY RATIO (%): 81.9	ELEVATION: 1160.1 (MSL)	EOB: 7.5 ft.	PAGE 1 OF 1														
START: 12/10/20 END: 12/10/20	SAMPLING METHOD: SPT		LAT / LONG: 41.194777, -81.626030																
MATERIAL DESCRIPTION AND NOTES	ELEV. 1160.1	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
				GR	CS	FS	SI	CL	LL	PL	PI								
11.0" ASPHALT (DRILLERS DESCRIPTION)	1159.2			1															
VERY STIFF TO HARD, BROWN MOTTLED WITH ORANGISH BROWN, SILT AND CLAY , SOME SAND, TRACE GRAVEL, CONTAINS IRON STAINING, DAMP				2	6	SS-1	3.00	-	-	-	-	-	-	-	-	12	A-6a (V)	<100	
				3	7														
MEDIUM STIFF TO VERY STIFF, DARK BROWNISH GRAY AND BLACK, ELASTIC CLAY , "AND" SILT, TRACE SAND, TRACE GRAVEL, MODERATELY ORGANIC, DAMP	1155.6			4	4	SS-2	4.50	10	10	18	36	26	28	16	12	14	A-6a (6)	-	
				5	3														
				6	5	SS-3	0.75	1	2	7	42	48	69	34	35	17	A-7-5 (20)	-	
				7	4														
	1152.6	EOB		3	10	SS-4	2.50	-	-	-	-	-	-	-	-	23	A-7-5 (V)	-	

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH	DRILL RIG: CME 45B	STATION / OFFSET: 107+16, 1' LT.	EXPLORATION ID B-088-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH	HAMMER: CME AUTOMATIC	ALIGNMENT: RAMP C																
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1161.3 (MSL)	PAGE															
START: 10/21/20 END: 10/21/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.7	LAT / LONG: 41.198644, -81.625927	1 OF 1															
MATERIAL DESCRIPTION AND NOTES	ELEV. 1161.3	DEPTH(S)	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
				GR	CS			FS	SI	CL	LL	PL	PI						
5.0" ASPHALT AND 8.0" BASE (DRILLERS DESCRIPTION)	1160.2			1															
MEDIUM DENSE, BROWN, COARSE AND FINE SAND, LITTLE TO SOME SILT, LITTLE GRAVEL, TRACE CLAY, DAMP	1156.8			2	4	SS-1	-	20	24	26	21	9	NP	NP	NP	9	A-3a (0)	<100	
LOOSE, BROWN, GRAVEL WITH SAND AND SILT, LITTLE CLAY, CONTAINS NO INTACT SOIL FOR HP READINGS, DAMP TO MOIST	1153.8	EOB		3	5	SS-2	-	17	27	36	14	6	NP	NP	NP	7	A-3a (0)	-	
				4	5	SS-3	-	9	27	29	24	11	20	13	7	13	A-2-4 (0)	-	
				5	4	SS-4	-	-	-	-	-	-	-	-	-	18	A-2-4 (V)	-	
				6	5														
				7	3														

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH	DRILL RIG: CME 45B	STATION / OFFSET: 7+13, 9' LT.	EXPLORATION ID B-090-0-20																			
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH	HAMMER: CME AUTOMATIC	ALIGNMENT: RAMP B																				
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1159.2 (MSL)	PAGE																			
START: 10/20/20 END: 10/20/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.7	LAT / LONG: 41.195890, -81.625231	1 OF 1																			
MATERIAL DESCRIPTION AND NOTES	ELEV. 1159.2	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL				
								GR	CS	FS	SI	CL	LL	PL	PI								
5.0" ASPHALT AND 10.5" CONCRETE (DRILLERS DESCRIPTION)	1157.9			1																			
HARD, BROWN AND GRAY, SANDY SILT, SOME GRAVEL, LITTLE CLAY, DAMP	1154.7			2	4	6	18	50	SS-1	4.50	23	11	22	30	14	21	16	5	11	A-4a (2)	-		
MEDIUM STIFF TO VERY STIFF, BROWNISH GRAY, SILT AND CLAY, SOME SAND, TRACE GRAVEL, MOIST TO WET	1151.7	EOB		3	3	3	10	56	SS-2	4.50	-	-	-	-	-	-	-	-	13	A-4a (V)	170		
				4	4	4	14	83	SS-3	2.25	7	9	17	35	32	32	18	14	19	A-6a (8)	-		
				5	4	4	6												31	A-6a (V)	-		
				6	4	5	16	89	SS-4	1.00	-	-	-	-	-	-	-	-					
				7	7																		

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

PROJECT: SUM-77-24.12	DRILLING FIRM / OPERATOR: NEAS / ASHBAUGH	DRILL RIG: CME 45B	STATION / OFFSET: 804+00, 92' RT.	EXPLORATION ID B-091-0-20															
TYPE: SUBGRADE	SAMPLING FIRM / LOGGER: NEAS / ASHBAUGH	HAMMER: CME AUTOMATIC	ALIGNMENT: IR-77																
PID: 111404 SFN:	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 12/5/19	ELEVATION: 1159.8 (MSL)	PAGE															
START: 10/21/20 END: 10/21/20	SAMPLING METHOD: SPT	ENERGY RATIO (%): 81.7	LAT / LONG: 41.197778, -81.625279	1 OF 1															
MATERIAL DESCRIPTION AND NOTES	ELEV. 1159.8	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
				GR	CS			FS	SI	CL	LL	PL	PI						
11.0" BASE/ASPHALT MILLINGS (DRILLERS DESCRIPTION)	1158.9			1															
MEDIUM DENSE, BROWN AND BLACK, GRAVEL WITH SAND AND SILT, TRACE CLAY, CONTAINS ASPHALT FRAGMENTS, DAMP TO MOIST (FILL)	1155.3			2	4	SS-1	-	27	24	22	18	9	NP	NP	NP	12	A-2-4 (0)	170	
STIFF TO VERY STIFF, BROWN AND GRAY, SILT AND CLAY, SOME SAND, TRACE GRAVEL, DAMP TO MOIST	1152.3	EOB		3	6	SS-2	-	-	-	-	-	-	-	-	-	17	A-2-4 (V)	-	
				4	4	SS-3	3.25	20	13	13	31	23	32	18	14	15	A-6a (5)	-	
				5	3	SS-4	2.00	-	-	-	-	-	-	-	-	23	A-6a (V)	-	
				6	6														
				7	3														

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING. HOLE DID NOT CAVE.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PLACED 0.5 BAG ASPHALT PATCH; SHOVED SOIL CUTTINGS

Consolidation Test

Project Name: SUM-77-24.12

Prepared by: LR

Source: B-093-0-20 ST-1 (13.5' - 13.6')

Checked by: ZM

Description: Stiff, gray and brown, SANDY SILT, little clay, little gravel, damp.

Date: 1/16/2021

Test Specification: ASTM D 2435

Initial Void Ratio: 0.564

Initial Bulk Unit Weight (lb/ft^3): 128

In-situ Vertical Effective Stress: 1600

Dry Unit Weight (lb/ft^3): 108

Compression and Swelling Index

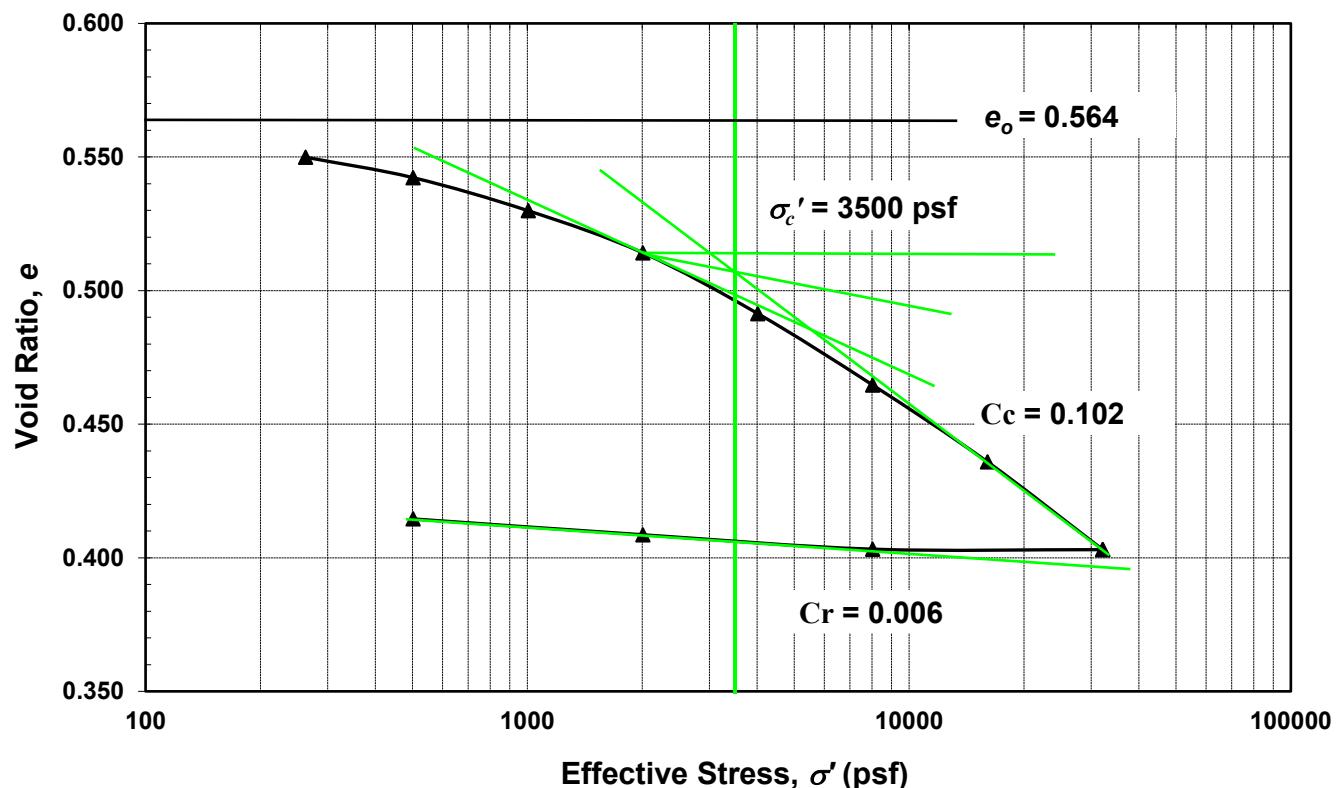
Compression Index (C_c): 0.102

Preconsolidation Pressure (σ'_c): 3500

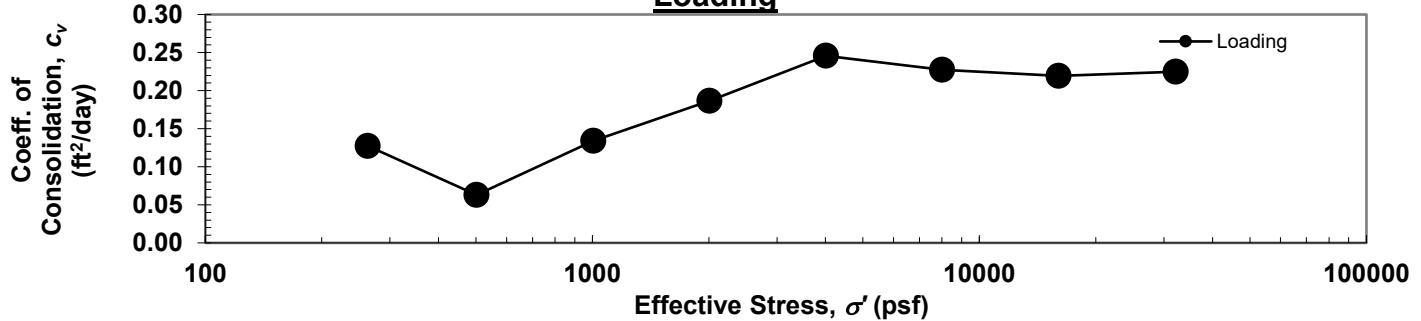
Recompression Index (C_r): 0.006

Over-Consolidation Ratio (OCR): 2.2

Consolidation Curve



Loading



Organic Content in Soils by Loss on Ignition (AASHTO T267)

Date of Test: 11/18/2021 Technician: LR

Project Name: SUM-77-24.12 Ghent

Boring Number:	B-095-0-20	B-095-0-20	B-093-0-20	B-006-1-20	
Sample Number:	SS-1	SS-4	ST-1	SS-1	
Depth:	2.5-4.0	10.0-11.5	13.5-13.8	2.5-4.0	
Initial -#10 sample weight:	104.91	103.26	102.52	101.01	

Moisture Content:

MC%:	20%	28%	19%	83% (org)	
------	-----	-----	-----	-----------	--

Organic Content 455+10°C (10 to 40g):

(Peat may be less than 10g but should be of sufficient amount to fill crucible >3/4 full)

Crucible ID:	A	C	B	C	
Crucible Wt:	62.3	60.85	33.94	37.77	
Crucible and Soil before:	98.98	98.12	57.76	53.6	
Crucible and Soil After:	97.48	95.06	56.95	51.01	
% Organic Content:	4.1%	8.2%	3.4%	16.4%	

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES			DRILL RIG: CME 55X				STATION / OFFSET: 316+24, 25' LT.			EXPLORATION ID B-096-0-20										
TYPE: COMPRESSIBLE SOILS		SAMPLING FIRM / LOGGER: NEAS / J. HODGES			HAMMER: CME AUTOMATIC				ALIGNMENT: IR-77 NB													
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 12/5/19				ELEVATION: 998.9 (MSL) EOB: 26.5 ft.			PAGE 1 OF 1										
START: 8/26/20 END: 8/26/20		SAMPLING METHOD: SPT			ENERGY RATIO (%): 81.9				LAT / LONG: 41.148583, -81.633866													
MATERIAL DESCRIPTION AND NOTES				ELEV. 998.9	DEPTHs		SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)		ATTERBERG		WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL			
VERY STIFF, BROWN, SANDY SILT, LITTLE TO SOME GRAVEL, LITTLE CLAY, CONTAINS TRACE ROOTS AND IRON STAINING, DAMP				998.9	1							GR	CS	FS	SI	CL	LL	PL	PI			
				998.9	2																	
				998.9	3	6	4	11	11	SS-1	4.00	-	-	-	-	-	-	-	12	A-4a (V)	-	
				998.9	4																	
				998.9	5																	
				998.9	6	3	3	8	100	SS-2	3.50	17	21	22	27	13	26	17	9	14	A-4a (1)	190
				998.9	7																	
				998.9	8	4	3	10	78	SS-3	-	-	-	-	-	-	-	-	-	13	A-2-6 (V)	-
				998.9	9																	
				998.9	10																	
				998.9	11	1	1	3	67	SS-4	0.25	23	21	17	26	13	29	18	11	18	A-6a (1)	-
				998.9	12																	
				998.9	13	4	6	16	89	SS-5	-	-	-	-	-	-	-	-	-	13	A-1-b (V)	-
				998.9	14																	
				998.9	15	5	6	20	17	SS-6	-	-	-	-	-	-	-	-	-	19	A-1-b (V)	-
				998.9	16																	
				998.9	17																	
				998.9	18	6	10	22	44	SS-7	-	28	19	30	17	6	NP	NP	NP	13	A-2-4 (0)	-
				998.9	19																	
				998.9	20																	
				998.9	21	4	5	15	67	SS-8	-	-	-	-	-	-	-	-	-	18	A-2-4 (V)	-
				998.9	22																	
				998.9	23	6	4	11	100	SS-9	-	-	-	-	-	-	-	-	-	16	A-3a (V)	-
				998.9	24																	
				998.9	25	4	4	11	100	SS-10	-	-	-	-	-	-	-	-	-	24	A-3a (V)	-
				998.9	26																	
EOB																						

PROJECT: SUM-77-24.12		DRILLING FIRM / OPERATOR: NEAS / J. HODGES			DRILL RIG: CME 55X			STATION / OFFSET: 317+90, 59' LT.			EXPLORATION ID B-097-0-20								
TYPE: COMPRESSIBLE SOILS		SAMPLING FIRM / LOGGER: NEAS / J. HODGES			HAMMER: CME AUTOMATIC			ALIGNMENT: IR-77 NB											
PID: 111404 SFN:		DRILLING METHOD: 3.25" HSA			CALIBRATION DATE: 12/5/19			ELEVATION: 993.6 (MSL) EOB: 26.5 ft.			PAGE								
START: 8/26/20 END: 8/26/20		SAMPLING METHOD: SPT / ST			ENERGY RATIO (%): 81.9			LAT / LONG: 41.148924, -81.633447			1 OF 1								
MATERIAL DESCRIPTION AND NOTES	ELEV. 993.6	DEPTHs	SPT/ RQD	N ₆₀	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	SO4 ppm	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI				
MEDIUM DENSE, BROWN, GRAVEL WITH SAND AND SILT, TRACE CLAY, CONTAINS IRON STAINING, DAMP				1															
				2															
				3	6	SS-1	-	46	18	13	15	8	30	22	8	10	A-2-4 (0)	13	
				4	8														
				5	9														
				6	4	SS-2	-	5	4	4	69	18	NP	NP	NP	24	A-4b (8)	-	
				7	12														
				8	6														
				9	15	SS-3	-	-	-	-	-	-	-	-	-	15	A-4b (V)	-	
				10	7														
				11	56	ST-1	-	1	3	11	64	21	NP	NP	NP	18	A-4b (8)	-	
				12	4														
				13	3	SS-4	-	-	-	-	-	-	-	-	-	25	A-4b (V)	-	
				14	2														
				15	2	SS-5	-	10	10	7	63	10	NP	NP	NP	23	A-4b (8)	-	
				16	2														
				17															
				18	1	SS-6	-	-	-	-	-	-	-	-	-	33	A-4b (V)	-	
				19	1														
				20	2														
				21	2	SS-7	-	-	-	-	-	-	-	-	-	29	A-4b (V)	-	
				22	2														
				23	1	SS-8	-	-	-	-	-	-	-	-	-	28	A-4b (V)	-	
				24	2														
				25	2	SS-9	-	-	-	-	-	-	-	-	-	25	A-4b (V)	-	
				26	3														
				967.1	6	12	100												
EOB																			
NOTES: GROUNDWATER ENCOUNTERED AT 12.0' DURING DRILLING. HOLE DID NOT CAVE.																			
ABANDONMENT METHODS, MATERIALS, QUANTITIES: SHOVED SOIL CUTTINGS																			

Consolidation Test

Project Name: SUM-77-24.12

Prepared by: LR

Source: B-097-0-20 ST-1 (10.6' - 10.7')

Checked by: ZM

Description: Medium dense, gray, SILT, some clay, little sand, trace gravel, wet.

Date: 1/16/2021

Test Specification: ASTM D 2435

Initial Void Ratio: 0.474

Initial Bulk Unit Weight (lb/ft³): 137

In-situ Vertical Effective Stress: 1300

Dry Unit Weight (lb/ft³): 114

Compression and Swelling Index

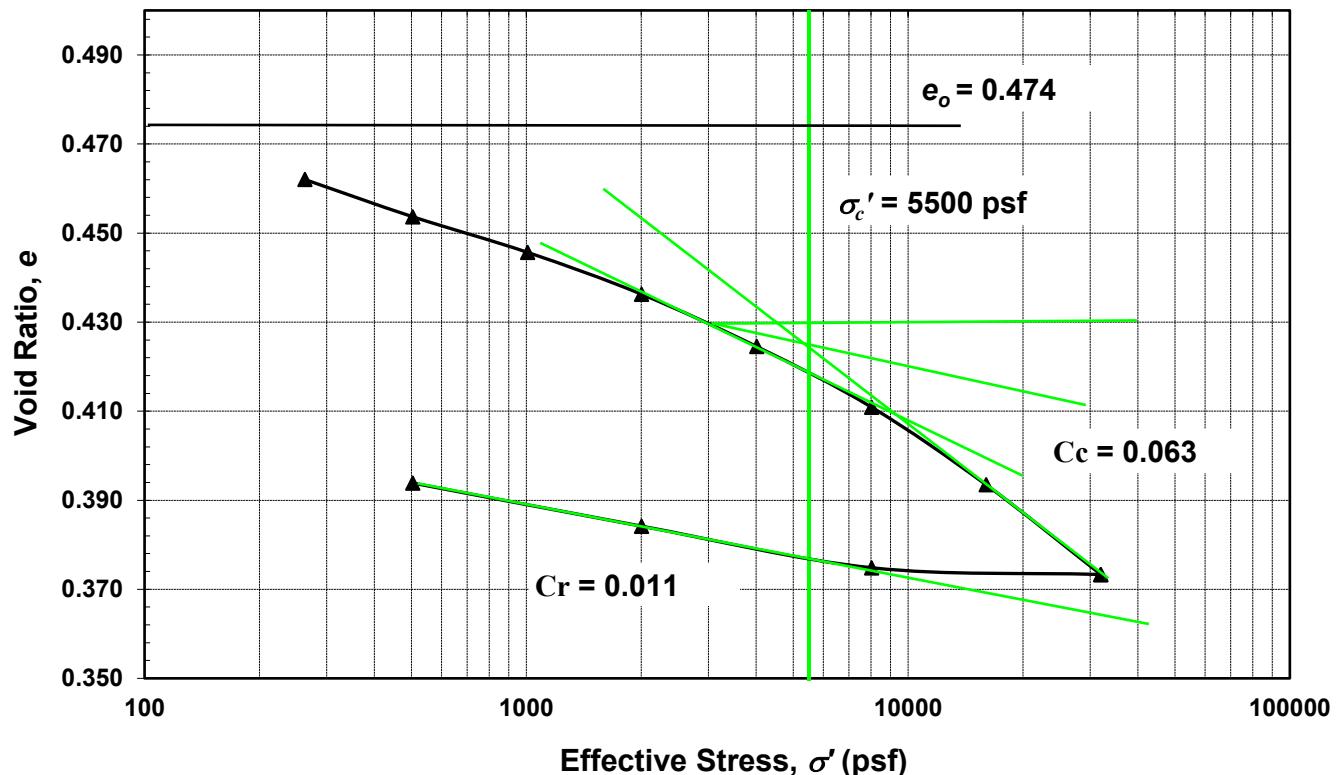
Compression Index (C_c): 0.063

Preconsolidation Pressure (σ_c'): 5500

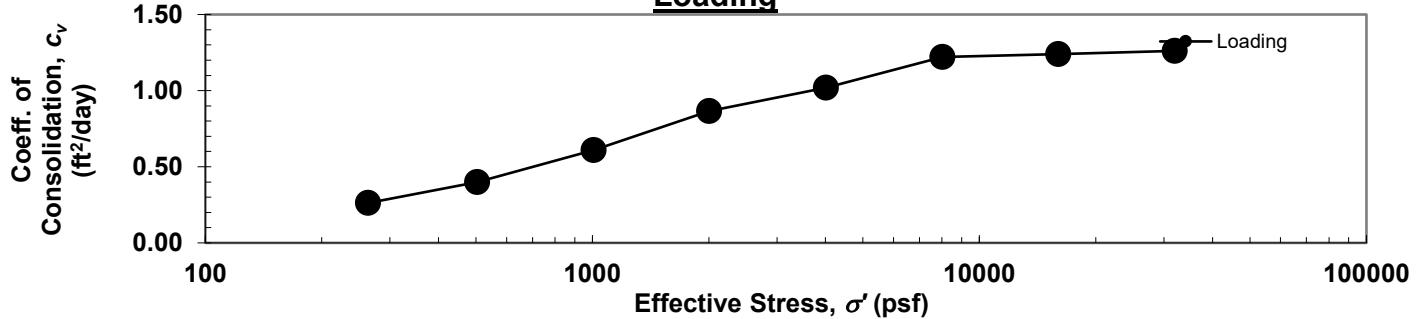
Recompression Index (C_r): 0.011

Over-Consolidation Ratio (OCR): 4.2

Consolidation Curve



Loading



APPENDIX D

PAVEMENT CORE LOGS

Core Log: B-014-0-20 / PC-1

Core Location: SUM-77-24.12 Ghent
 IR-77 SB Right Shoulder
 41.151314, -81.630974

Project: SUM-77-24.12 Ghent, PID 111404 **Date:** 12/7/2020

Location: City of Akron, Summit Co., OH **Core Type / Alignment:** Pavement / IR-77

Client: GPD Group **Coring Crew:** NEAS - CA/JH

Core Barrel Size (O.D.): 4.00" **Hole Patched w/:** Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±1.50" Surface Course</p> <p>- ±3.75" Intermediate Course</p> <p>- ±1.00" Intermediate Course</p> <p style="text-align: center;">Total Core Recovery = 6.25"</p>

Abbreviations and Notes

Core Log: PC-2

Core Location:	SUM-77-24.12 Ghent
	IR-77 SB Left Shoulder
	41.156166, -81.626637
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
	Date: 11/19/2020
	Core Type / Alignment: Pavement / IR-77
	Coring Crew: NEAS - CA/JH
	Hole Patched w/: Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
 Total Core Recovery = 12.75"	<p style="text-align: center;">FACE OF THE CORE IS AT ZERO</p> <p style="text-align: center;">- ±1.75" Surface Course</p> <p style="text-align: center;">- ±4.00" Intermediate Course</p> <p style="text-align: center;">- ±6.75" Base Course</p>

Abbreviations and Notes

Core Log: PC-3

Core Location:	SUM-77-24.12 Ghent
	IR-77 SB Right Shoulder
	41.157761, -81.626537
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
Date:	12/10/2020
Core Type / Alignment:	Pavement / IR-77
Coring Crew:	NEAS - CA/JH
Hole Patched w/:	Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±1.50" Surface Course</p> <p>- ±2.00" Intermediate Course</p> <p>- ±6.75" Concrete</p> <p>Total Core Recovery = 10.25"</p>

Abbreviations and Notes

Core Log: PC-4

Core Location:	SUM-77-24.12 Ghent
	IR-77 NB Right Shoulder
	41.156164, -81.626258
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
Date:	12/11/2020
Core Type / Alignment:	Pavement / IR-77
Coring Crew:	NEAS - CA/JH
Hole Patched w/:	Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±1.75" Surface Course</p> <p>- ±2.25" Intermediate Course</p> <p>- ±10.75" Base Course</p> <p style="text-align: center;">Total Core Recovery = 14.75"</p>

Abbreviations and Notes

Core Log: PC-5

Core Location: SUM-77-24.12 Ghent
 IR-77 NB Left Shoulder
 41.157724, -81.626171

Project: SUM-77-24.12 Ghent, PID 111404 **Date:** 12/8/2020

Location: City of Akron, Summit Co., OH **Core Type / Alignment:** Pavement / IR-77

Client: GPD Group **Coring Crew:** NEAS - CA/JH

Core Barrel Size (O.D.): 4.00" **Hole Patched w/:** Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
 <small>LOWES</small> <small>Do you have it all covered?</small> <small>• Primer</small> <small>JO</small>	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±1.75" Surface Course</p> <p>- ±6.00" Intermediate Course</p> <p>- ±5.00" Base Course</p> <p style="text-align: center;">Total Core Recovery = 12.75"</p>

Abbreviations and Notes

Core Log: B-029-0-20 / PC-6

Core Location: SUM-77-24.12 Ghent
 IR-77 NB Right Shoulder
 41.163887, -81.625758

Project: SUM-77-24.12 Ghent, PID 111404 **Date:** 12/16/2020

Location: City of Akron, Summit Co., OH **Core Type / Alignment:** Pavement / IR-77

Client: GPD Group **Coring Crew:** NEAS - CA/JH

Core Barrel Size (O.D.): 4.00" **Hole Patched w/:** Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p style="text-align: center;">FACE OF THE CORE IS AT ZERO</p> <p style="text-align: center;">- ±1.25" Surface Course</p> <p style="text-align: center;">- ±2.25" Intermediate Course</p> <p style="text-align: center;">- ±2.25" Intermediate Course</p>
Total Core Recovery = 5.75"	

Abbreviations and Notes

Core Log: PC-7

Core Location:	SUM-77-24.12 Ghent
	IR-77 SB Left Shoulder
	41.168769, -81.626142
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
	Date: 11/19/2020
	Core Type / Alignment: Pavement / IR-77
	Coring Crew: NEAS - CA/JH
	Hole Patched w/: Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p style="text-align: center;">FACE OF THE CORE IS AT ZERO</p> <p style="text-align: center;">- ±1.50" Surface Course</p> <p style="text-align: center;">- ±2.75" Intermediate Course</p> <p style="text-align: center;">- ±7.50" Base Course</p> <p style="text-align: center;">- ±0.75" Concrete</p> <p style="text-align: center;">Total Core Recovery = 12.50"</p>

Abbreviations and Notes

Core Log: PC-8

Core Location:	SUM-77-24.12 Ghent
	IR-77 SB Right Shoulder
	41.169307, -81.626288
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
Date:	12/10/2020
Core Type / Alignment:	Pavement / IR-77
Coring Crew:	NEAS - CA/JH
Hole Patched w/:	Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±3.50" Surface Course</p> <p>- ±6.75" Intermediate Course</p> <p>- ±5.00" Base Course</p> <p style="text-align: center;">Total Core Recovery = 15.25"</p>

Abbreviations and Notes

Core Log: PC-9

Core Location:	SUM-77-24.12 Ghent
	IR-77 NB Left Shoulder
	41.168778, -81.625919
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
Date:	12/8/2020
Core Type / Alignment:	Pavement / IR-77
Coring Crew:	NEAS - CA/JH
Hole Patched w/:	Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±1.75" Surface Course</p> <p>- ±2.50" Intermediate Course</p> <p>- ±6.00" Base Course</p> <p>- ±4.50" Base Course</p> <p>Total Core Recovery = 14.75"</p>

Abbreviations and Notes

Core Log: PC-10

Core Location: SUM-77-24.12 Ghent
 IR-77 NB Right Shoulder
 41.169319, -81.625758

Project: SUM-77-24.12 Ghent, PID 111404 **Date:** 12/11/2020

Location: City of Akron, Summit Co., OH **Core Type / Alignment:** Pavement / IR-77

Client: GPD Group **Coring Crew:** NEAS - CA/JH

Core Barrel Size (O.D.): 4.00" **Hole Patched w/:** Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±2.50" Surface Course</p> <p>- ±2.75" Intermediate Course</p> <p>- ±8.75" Base Course</p> <p style="text-align: center;">Total Core Recovery = 14.00"</p>

Abbreviations and Notes

Core Log: B-042-0-20 / PC-11

Core Location: SUM-77-24.12 Ghent
IR-77 SB Right Shoulder
41.178158, -81.626097

Project: SUM-77-24.12 Ghent, PID 111404 **Date:** 11/17/2020

Location: City of Akron, Summit Co., OH **Core Type / Alignment:** Pavement / IR-77

Client: GPD Group **Coring Crew:** NEAS - CA/JH

Core Barrel Size (O.D.): 4.00" **Hole Patched w/:** Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±1.00" Surface Course</p> <p>- ±2.25" Intermediate Course</p> <p>- ±3.25" Base Course</p> <p style="text-align: center;">Total Core Recovery = 6.50"</p>

Abbreviations and Notes

Core Log: PC-12

Core Location:	SUM-77-24.12 Ghent
	IR-77 SB Left Shoulder
	41.188742, -81.625723
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
	Date: 11/16/2020
	Core Type / Alignment: Pavement / IR-77
	Coring Crew: NEAS - CA/JH
	Hole Patched w/: Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p style="text-align: center;">FACE OF THE CORE IS AT ZERO</p> <p style="text-align: center;">- ±2.25" Surface Course</p> <p style="text-align: center;">- ±1.75" Base Course</p> <p style="text-align: center;">- ±7.25" Intermediate Course</p> <p style="text-align: center;">- ±1.00" Intermediate Course</p> <p style="text-align: center;">Total Core Recovery = 12.25"</p>

Abbreviations and Notes

Core Log: PC-13

Core Location:	SUM-77-24.12 Ghent
	IR-77 SB Right Shoulder
	41.189286, -81.625880
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
Date:	12/10/2020
Core Type / Alignment:	Pavement / IR-77
Coring Crew:	NEAS - CA/JH
Hole Patched w/:	Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±2.00" Surface Course</p> <p>- ±4.25" Base Course</p> <p style="text-align: center;">Total Core Recovery = 6.25"</p>

Abbreviations and Notes

Core Log: PC-14

Core Location:	SUM-77-24.12 Ghent
	IR-77 NB Right Shoulder
	41.188742, -81.625356
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
	Date: 12/11/2020
	Core Type / Alignment: Pavement / IR-77
	Coring Crew: NEAS - CA/JH
	Hole Patched w/: Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±2.00" Surface Course</p> <p>- ±2.75" Base Course</p> <p>- ±5.50" Base Course</p> <p>Total Core Recovery = 10.25"</p>

Abbreviations and Notes

Core Log: PC-15

Core Location:	SUM-77-24.12 Ghent
	IR-77 NB Left Shoulder
	41.189305, -81.625488
Project:	SUM-77-24.12 Ghent, PID 111404
Location:	City of Akron, Summit Co., OH
Client:	GPD Group
Core Barrel Size (O.D.):	4.00"
	Date: 12/8/2020
	Core Type / Alignment: Pavement / IR-77
	Coring Crew: NEAS - CA/JH
	Hole Patched w/: Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p style="text-align: center;">FACE OF THE CORE IS AT ZERO</p> <p style="text-align: center;">- ±1.50" Surface Course</p> <p style="text-align: center;">- ±1.50" Surface Course</p> <p style="text-align: center;">- ±3.75" Intermediate Course</p> <p style="text-align: center;">- ±3.5" Intermediate Course</p> <p style="text-align: center;">- ±4.00" Intermediate Course</p> <p style="text-align: center;">Total Core Recovery = 14.25"</p>

Abbreviations and Notes

Core Log: B-057-0-20 / PC-16

Core Location: SUM-77-24.12 Ghent
 IR-77 NB Right Shoulder
 41.194780, -81.625340

Project: SUM-77-24.12 Ghent, PID 111404 **Date:** 12/8/2020

Location: City of Akron, Summit Co., OH **Core Type / Alignment:** Pavement / IR-77

Client: GPD Group **Coring Crew:** NEAS - CA/JH

Core Barrel Size (O.D.): 4.00" **Hole Patched w/:** Asphalt Patch

Photograph and Core Length	Description and Noted Features of Core Sample
	<p>FACE OF THE CORE IS AT ZERO</p> <p>- ±1.75" Surface Course</p> <p>- ±4.50" Intermediate Course</p> <p>- ±6.00" Base Course</p> <p style="text-align: center;">Total Core Recovery = 12.25"</p>

Abbreviations and Notes

APPENDIX E

SULFATE TEST DATA REPORT



OHIO DEPARTMENT OF TRANSPORTATION
DETERMINING SULFATE CONTENT IN SOILS
SUPPLEMENT 1122

Project C-R-S: SUM-77-24.12 Ghent
PID No: 111404
Report Date: 1/5/2021
Consultant: NEAS Inc.
Technician: L. Rosenbeck

Boring ID & Sample #	Station	Offset	Latitude & Longitude or State Plane Coordinates	Elevation	Soaking Time (hr)	Replicate Sample Readings						Sulfate Content (ppm)	
						1		2		3			
						Dilution	Reading	Dilution	Reading	Dilution	Reading		
B-001-0-20 SS-1A					20.67	20	2	20	3	20	3	53	
B-002-0-20 SS-1					16.42	20	2	20	3	20	3	53	
B-003-0-20 SS-1					18.6	20	0	20	0	20	0	0	
B-004-0-20 SS-1					16.43	20	4	20	2	20	4	67	
B-005-0-20 SS-1					18.58	20	1	20	0	20	1	13	
B-006-0-20 SS-1					18.58	20	1	20	1	20	1	20	
B-007-0-20 SS-1					17.42	20	6	20	9	20	7	147	
B-008-0-20 SS-1					19.62	20	2	20	3	20	3	53	
B-009-0-20 SS-1					18.85	20	13	20	13	20	12	253	
B-010-0-20 SS-1					20.17	20	10	20	7	20	9	173	
B-011-0-20 SS-1					17.47	20	7	20	7	20	6	133	
B-012-0-20 SS-1					16.12	20	2	20	3	20	2	47	
B-013-0-20 SS-1					17.33	20	7	20	3	20	7	113	
B-014-0-20 SS-1					16.42	20	4	20	3	20	4	73	
B-015-0-20 SS-1					17.33	20	1	20	0	20	1	13	
B-016-0-20 SS-1					16.11	20	1	20	1	20	1	20	
B-017-0-20 SS-1					17.75	20	3	20	1	20	2	40	
B-018-0-20 SS-1					18.85	20	2	20	2	20	2	40	

B-019-0-20 SS-1A					17.48	20	4	20	4	20	5	87
B-020-0-20 SS-1					18.83	20	7	20	7	20	7	140
B-021-0-20 SS-1					17.45	20	1	20	1	20	1	20
B-022-0-20 SS-1					17.33	20	10	20	4	20	4	120
B-023-0-20 SS-1					17.33	20	4	20	6	20	7	113
B-024-0-20 SS-1A					17.8	40	50	40	51	40	47	1973
B-025-0-20 SS-2					17.45	20	5	20	6	20	5	107
B-026-0-20 SS-1					16.42	20	5	20	6	20	6	113
B-027-0-20 SS-1					17.82	20	0	20	1	20	1	13
B-028-0-20 SS-1					19.82	20	4	20	4	20	3	73
B-029-0-20 SS-1					16.11	20	4	20	4	20	4	80
B-030-0-20 SS-1					16.44	100	52	100	65	100	47	5467
B-032-0-20 SS-1					17.33	20	3	20	5	20	5	87
B-033-0-20 SS-1					16.44	20	65	20	70	20	69	1360
B-034-0-20 SS-1					19.62	20	13	20	17	20	16	307
B-035-0-20 SS-1					17.33	20	8	20	7	20	14	193
B-036-0-20 SS-1					19.17	20	2	20	2	20	2	40
B-037-0-20 SS-1					17.33	20	17	20	18	20	22	380
B-038-0-20 SS-1					16.42	20	7	20	9	20	8	160
B-039-0-20 SS-1					17.33	20	8	20	16	20	11	233
B-040-0-20 SS-1					19.75	20	2	20	2	20	2	40
B-041-0-20 SS-1					17.33	20	5	20	2	20	5	80
B-042-0-20 SS-1					19.82	20	8	20	6	20	8	147
B-043-0-20 SS-1					17.78	20	4	20	4	20	4	80
B-044-0-20 SS-1					17.73	20	2	20	7	20	1	67
B-045-0-20 SS-1					19.83	20	10	20	10	20	6	173
B-046-0-20 SS-1					19.78	20	5	20	6	20	6	113
B-047-0-20 SS-2					16.13	20	6	20	5	20	6	113
B-048-0-20 SS-1					17.5	20	8	20	4	20	5	113
B-049-0-20 SS-1					19.32	20	20	20	20	20	33	487
B-050-0-20 SS-1					17.78	20	4	20	4	20	3	73
B-051-0-20 SS-1					16.13	20	3	20	4	20	3	67
B-052-0-20 SS-1					17.8	20	2	20	4	20	4	67

B-053-0-20 SS-1					17.77	20	2	20	4	20	4	67
B-054-0-20 SS-1					19.38	20	1	20	1	20	1	20
B-055-0-20 SS-1					19.3	20	6	20	6	20	6	120
B-056-0-20 SS-1					19.22	20	14	20	10	20	28	347
B-057-0-20 SS-1					17.78	20	4	20	4	20	4	80
B-058-0-20 SS-1					19.88	20	4	20	6	20	6	107
B-059-0-20 SS-1					20.17	20	6	20	5	20	5	107
B-061-0-20 SS-1					19.18	20	0	20	0	20	0	0
B-062-0-20 SS-1					16.14	20	1	20	1	20	1	20
B-063-0-20 SS-1					17.47	20	7	20	7	20	7	140
B-064-0-20 SS-1					17.44	20	2	20	2	20	2	40
B-065-0-20 SS-1					17.4	20	1	20	1	20	1	20
B-066-0-20 SS-1					17.47	20	3	20	3	20	3	60
B-067-0-20 SS-1					17.45	20	2	20	2	20	2	40
B-068-0-20 SS-1					18.02	20	43	20	41	20	40	827
B-069-0-20 SS-1					18.85	20	1	20	2	20	2	33
B-070-0-20 SS-1					17.44	20	1	20	1	20	1	20
B-071-0-20 SS-1					18.8	20	1	20	2	20	2	33
B-072-0-20 SS-1					18.8	20	14	20	14	20	14	280
B-074-0-20 SS-1					17.42	20	5	20	7	20	7	127
B-075-0-20 SS-1					17.43	20	18	20	14	20	15	313
B-076-0-20 SS-1					17.48	20	5	20	5	20	5	100
B-078-0-20 SS-1					17.45	20	4	20	5	20	5	93
B-079-0-20 SS-1					19.13	20	15	20	16	20	16	313
B-080-0-20 SS-1					16.14	20	1	20	1	20	1	20
B-081-0-20 SS-1					19.83	20	1	20	1	20	1	20
B-082-0-20 SS-1					17.82	20	7	20	5	20	7	127
B-084-0-20 SS-1					16.42	20	0	20	1	20	0	7
B-085-0-20 SS-1					18.84	20	3	20	3	20	3	60
B-086-0-20 SS-2					18.85	20	2	20	1	20	2	33
B-087-0-20 SS-1					18.05	40	30	40	30	40	30	1200
B-088-0-20 SS-1					20.17	20	4	20	5	20	5	93
B-089-0-20 SS-2					20.17	20	4	20	6	20	6	107

B-090-0-20 SS-2					20.17	20	9	20	7	20	9	167
B-091-0-20 SS-1					20.17	20	7	20	9	20	9	167
B-092-0-20 SS-1					21.17	20	16	20	15	20	16	313
B-093-0-20 SS-1					21.17	20	5	20	4	20	5	93
B-094-0-20 SS-1					21.17	20	4	20	4	20	4	80
B-095-0-20 SS-1					21.17	40	43	40	42	40	47	1760
B-096-0-20 SS-2					21.17	20	10	20	8	20	10	187
B-097-0-20 SS-1					18.58	20	0	20	1	20	1	13

APPENDIX F

**GEOTECHNICAL BULLETIN 1 (GB1) ANALYSIS
SPREADSHEETS**

ENTIRE PROJECT

OHIO DEPARTMENT OF TRANSPORTATION
OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES
Geotechnical Bulletin GB1

SUM-77-24.12

111404

Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75

NEAS Inc.

Prepared By: KCA
Date prepared: Monday, January 11, 2021

Brendan P. Andrews
2800 Corporate Exchange Drive
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NO. OF BORINGS: **95**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-001-0-20	IR-77 NB	300+01	18	LT	CME 55X	82	1012.4	1010.9	1.5 C
2	B-002-0-20	IR-77 SB	403+91	3	LT	CME 55X	82	1012.2	1010.7	1.5 C
3	B-003-0-20	IR-77 NB	307+04	16	LT	CME 55X	82	1007.0	1007.6	0.6 F
4	B-004-0-20	IR-77 SB	408+18	9	LT	CME 55X	82	1016.3	1014.8	1.5 C
5	B-005-0-20	IR-77 NB	310+99	15	LT	CME 55X	82	1006.1	1004.6	1.5 C
6	B-006-0-20	IR-77 SB	411+96	6	RT	CME 55X	82	1015.9	1015.5	0.4 C
7	B-007-0-20	IR-77 NB	315+00	41	RT	CME 45B	82	1002.0	1000.5	1.5 C
8	B-008-0-20	IR-77 SB	415+88	9	LT	CME 55X	82	1015.5	1014.0	1.5 C
9	B-009-0-20	IR-77 NB	319+10	1	LT	CME 55X	82	999.0	997.5	1.5 C
10	B-010-0-20	IR-77 SB	419+97	15	RT	CME 55X	82	1008.2	1008.3	0.1 F
11	B-011-0-20	IR-77 NB	323+93	2	LT	CME 55X	82	995.0	993.5	1.5 C
12	B-012-0-20	IR-77 SB	424+12	9	RT	CME 55X	82	1000.6	999.1	1.5 C
13	B-013-0-20	IR-77 NB	328+78	16	LT	CME 55X	82	988.5	988.0	0.5 C
14	B-014-0-20	IR-77 SB	428+74	41	LT	CME 55X	82	988.8	987.3	1.5 C
15	B-015-0-20	IR-77 NB	332+00	16	LT	CME 55X	82	982.8	982.1	0.7 C
16	B-016-0-20	IR-77 SB	432+37	1	RT	CME 55X	82	981.2	979.7	1.5 C
17	B-017-0-20	IR-77 NB	336+02	13	LT	CME 55X	82	972.9	972.4	0.5 C
18	B-018-0-20	IR-77 SB	436+21	0	RT	CME 55X	82	971.7	970.2	1.5 C
19	B-019-0-20	IR-77 NB	340+31	1	LT	CME 55X	82	963.9	962.4	1.5 C
20	B-020-0-20	IR-77 SB	440+21	1	RT	CME 55X	82	961.8	960.3	1.5 C
21	B-021-0-20	IR-77 NB	343+97	3	LT	CME 55X	82	955.0	953.5	1.5 C
22	B-022-0-20	IR-77 SB	443+14	12	RT	CME 55X	82	954.4	953.9	0.5 C
23	B-023-0-20	IR-77 NB	348+72	6	LT	CME 55X	82	949.5	948.0	1.5 C
24	B-024-0-20	IR-77	660+27	14	LT	CME 55X	82	962.0	961.6	0.4 C
25	B-025-0-20	IR-77	664+36	39	RT	CME 55X	82	973.1	971.6	1.5 C
26	B-026-0-20	IR-77	668+28	33	LT	CME 55X	82	982.2	981.2	1.0 C
27	B-027-0-20	IR-77	672+27	30	RT	CME 55X	82	990.9	990.9	0.0 F
28	B-028-0-20	IR-77	676+34	39	LT	CME 55X	82	999.0	997.5	1.5 C
29	B-029-0-20	IR-77	680+33	71	RT	CME 45B	82	1001.8	1000.3	1.5 C
30	B-030-0-20	IR-77	684+31	29	LT	CME 55X	82	1002.6	1002.4	0.2 C
31	B-031-0-20	IR-77	688+28	41	RT	CME 55X	82	1006.3	1004.8	1.5 C
32	B-032-0-20	IR-77	692+52	26	LT	CME 55X	82	1007.1	1006.4	0.7 C
33	B-033-0-20	IR-77	696+54	35	RT	CME 55X	82	1009.6	1008.1	1.5 C
34	B-034-0-20	IR-77	701+52	23	LT	CME 55X	82	1014.7	1013.2	1.5 C
35	B-035-0-20	IR-77	705+15	25	RT	CME 55X	82	1021.6	1020.5	1.1 C
36	B-036-0-20	IR-77	708+46	32	LT	CME 55X	82	1031.1	1030.5	0.6 C
37	B-037-0-20	IR-77	712+59	47	RT	CME 55X	82	1044.8	1043.3	1.5 C
38	B-038-0-20	IR-77	716+54	34	LT	CME 55X	82	1055.8	1055.0	0.8 C
39	B-039-0-20	IR-77	720+49	34	RT	CME 55X	82	1067.4	1066.7	0.7 C
40	B-040-0-20	IR-77	724+53	41	LT	CME 55X	82	1080.3	1078.8	1.5 C
41	B-041-0-20	IR-77	728+54	33	RT	CME 55X	82	1091.5	1090.9	0.6 C
42	B-042-0-20	IR-77	732+51	71	LT	CME 55X	82	1104.1	1102.6	1.5 C
43	B-043-0-20	IR-77	736+56	40	RT	CME 55X	82	1116.6	1115.1	1.5 C
44	B-044-0-20	IR-77	740+56	34	LT	CME 55X	82	1127.6	1127.0	0.6 C
45	B-045-0-20	IR-77	744+53	32	RT	CME 55X	82	1139.4	1139.1	0.3 C



#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
46	B-046-0-20	IR-77	748+52	41	LT	CME 55X	82	1152.3	1150.8	1.5 C
47	B-047-0-20	IR-77	752+52	32	RT	CME 55X	82	1162.3	1161.6	0.7 C
48	B-048-0-20	IR-77	756+55	41	LT	CME 55X	82	1170.9	1169.4	1.5 C
49	B-049-0-20	IR-77	760+56	31	RT	CME 55X	82	1174.8	1174.1	0.7 C
50	B-050-0-20	IR-77	764+57	33	LT	CME 55X	82	1178.7	1177.2	1.5 C
51	B-051-0-20	IR-77	768+59	32	RT	CME 55X	82	1181.9	1180.4	1.5 C
52	B-052-0-20	IR-77	773+45	23	LT	CME 55X	82	1183.0	1181.5	1.5 C
53	B-053-0-20	IR-77	777+09	19	RT	CME 55X	82	1179.2	1179.2	0.0 F
54	B-054-0-20	IR-77	781+04	27	LT	CME 55X	82	1176.1	1175.3	0.8 C
55	B-055-0-20	IR-77	784+58	35	RT	CME 55X	82	1173.2	1171.8	1.4 C
56	B-056-0-20	IR-77	789+10	34	LT	CME 55X	82	1168.1	1167.5	0.6 C
57	B-057-0-20	IR-77	793+08	72	RT	CME 55X	82	1164.9	1163.4	1.5 C
58	B-058-0-20	IR-77	797+10	38	LT	CME 55X	82	1161.2	1159.7	1.5 C
59	B-059-0-20	IR-77	799+87	99	RT	CME 45B	82	1158.4	1156.9	1.5 C
60	B-060-0-20	IR-77	805+10	40	LT	CME 55X	82	1160.8	1159.3	1.5 C
61	B-061-0-20	IR-77	809+75	34	RT	CME 55X	82	1162.0	1161.5	0.5 C
62	B-062-0-20	IR-77	813+15	40	LT	CME 55X	82	1164.5	1163.0	1.5 C
63	B-063-0-20	IR-77	816+93	27	RT	CME 55X	82	1165.0	1164.7	0.3 C
64	B-064-0-20	IR-77 SB	409+38	50	LT	CME 55X	82	1015.5	1014.0	1.5 C
65	B-065-0-20	Ramp S	14+70	17	LT	CME 55X	82	1016.2	1014.7	1.5 C
66	B-066-0-20	Ramp S	18+82	9	LT	CME 55X	82	1013.4	1011.9	1.5 C
67	B-067-0-20	Ramp S	22+92	4	LT	CME 55X	82	1009.5	1008.0	1.5 C
68	B-068-0-20	Ramp P	225+67	7	LT	CME 55X	82	997.0	995.5	1.5 C
69	B-069-0-20	Ramp P	221+81	15	RT	CME 55X	82	1007.8	1006.3	1.5 C
70	B-070-0-20	Ramp P	218+57	15	RT	CME 55X	82	1009.4	1007.9	1.5 C
71	B-071-0-20	Ramp P	214+18	17	RT	CME 55X	82	1003.7	1002.2	1.5 C
72	B-072-0-20	Ramp R	17+63	9	LT	CME 55X	82	1006.1	1004.6	1.5 C
73	B-073-0-20	Ramp L	116+93	1	RT	CME 45B	82	1000.2	998.7	1.5 C
74	B-074-0-20	Ramp L	118+92	0	LT	CME 45B	82	998.0	996.5	1.5 C
75	B-075-0-20	Ramp L	120+95	15	RT	CME 45B	82	996.4	994.9	1.5 C
76	B-076-0-20	Ramp L	122+95	25	RT	CME 45B	82	998.8	997.8	1.0 C
77	B-077-0-20	Ramp L	124+91	12	RT	CME 45B	82	1003.3	1002.3	1.0 C
78	B-078-0-20	Ramp L	126+90	5	RT	CME 45B	82	1007.6	1006.6	1.0 C
79	B-079-0-20	Ghent Road	85+42	13	RT	CME 45B	82	999.3	997.8	1.5 C
80	B-080-0-20	Ramp M	127+44	73	RT	CME 45B	82	1002.8	1001.3	1.5 C
81	B-081-0-20	Ramp N	27+99	26	LT	CME 45B	82	1010.5	1009.0	1.5 C
82	B-082-0-20	Ramp N	31+00	35	RT	CME 45B	82	992.2	990.7	1.5 C
83	B-083-0-20	IR-77 NB	336+08	58	RT	CME 45B	82	975.5	974.0	1.5 C
84	B-084-0-20	IR-77	786+82	97	LT	CME 55X	82	1170.5	1169.0	1.5 C
85	B-085-0-20	Ramp D	23+06	14	RT	CME 55X	82	1160.1	1158.6	1.5 C
86	B-086-0-20	Ramp C	99+01	13	RT	CME 55X	82	1154.7	1153.2	1.5 C
87	B-087-0-20	Ramp C	103+04	16	RT	CME 55X	82	1158.4	1156.9	1.5 C
88	B-088-0-20	Ramp C	107+16	1	LT	CME 45B	82	1161.3	1159.8	1.5 C
89	B-089-0-20	Ramp A	88+52	17	LT	CME 45B	82	1162.0	1160.5	1.5 C
90	B-090-0-20	Ramp B	7+13	9	LT	CME 45B	82	1159.2	1157.7	1.5 C

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
91	B-091-0-20	IR-77	803+00	92	RT	CME 45B	82	1159.8	1158.3	1.5 C
92	B-092-0-20	IR-77 SB	413+49	12	RT	CME 55X	82	1014.1	1015.1	1.0 F
93	B-093-0-20	IR-77 SB	416+09	22	RT	CME 55X	82	1011.3	1013.2	1.9 F
94	B-095-0-20	IR-77 NB	313+26	16	LT	CME 55X	82	1002.2	1002.3	0.1 F
95	B-096-0-20	IR-77 NB	316+24	25	LT	CME 55X	82	998.9	1000.0	1.1 F



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
			From	To	From	To																					
1	B 001-0 20	SS-1A	1.5	2.7	0.0	1.2	19	19	3.75	NP	NP	NP	16	6	22	8	6	A-1-b	0	100							
		SS-2	2.7	4.5	1.2	3.0	22			33	20	13	54	41	95	18	15	A-6a	9			Mc					
		SS-3	4.5	6.0	3.0	4.5	23			4.5							15	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	25			4.5							15	14	A-6a	10							
2	B 002-0 20	SS-1	1.5	3.0	0.0	1.5	10	10	4.5								10	8	A-3a	0	100						
		SS-2	3.0	4.5	1.5	3.0	33			30	19	11	47	23	70	15	14	A-6a	7								
		SS-3	4.5	6.0	3.0	4.5	22			4.5							13	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	10			2.25	34	21	13	43	36	79	18	16	A-6a	9							
3	B 003-0 20	SS-1	0.0	1.5	0.6	2.1	12	7	1.5	NP	NP	NP	21	6	27	8	8	A-3a	0	100							
		SS-2	1.5	3.0	2.1	3.6	11										10	8	A-3a	0							
		SS-3	3.0	4.5	3.6	5.1	7										9	8	A-3a	0							
		SS-4	4.5	6.0	5.1	6.6	7			25	18	7	50	25	75	23	13	A-4b									
4	B 004-0 20	SS-1	1.5	3.0	0.0	1.5	15	10	4.25								10	10	A-2-6	4	100						
		SS-2	3.0	4.5	1.5	3.0	26			24	15	9	25	13	38	11	10	A-4a	1								
		SS-3	4.5	6.0	3.0	4.5	23			4.5							15	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	10			2	29	17	12	31	21	52	16	12	A-4a	4							
5	B 005-0 20	SS-2	1.5	3.0	0.0	1.5	16	8	1.5	NP	NP	NP	13	3	16	8	6	A-1-b	0	100							
		SS-3	3.0	4.5	1.5	3.0	16										8	6	A-1-b	0							
		SS-4	4.5	6.0	3.0	4.5	8										25	10	A-4a	8							
6	B 006-0 20	SS-1	0.0	1.5	-0.4	1.1	25	7	4.25	28	20	8	31	16	47	11	15	A-4a	2	100						12"	
		SS-2	1.5	3.0	1.1	2.6	8										17	10	A-4a	8		N ₆₀ & Mc				12"	
		SS-3	3.0	4.5	2.6	4.1	7			29	17	12	40	27	67	16	14	A-6a	7							12"	
		SS-4	4.5	6.0	4.1	5.6	14			4.25							16	14	A-6a	10						12"	
7	B 007-0 20	SS-1	1.5	3.0	0.0	1.5	18	16	4.25	28	17	11	39	17	56	11	14	A-6a	5	150							
		SS-2	3.0	4.5	1.5	3.0	16			27	17	10	33	19	52	12	12	A-4a	3								
		SS-3	4.5	6.0	3.0	4.5	20										16	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	22										14	10	A-4a	8							
8	B 008-0 20	SS-1	1.5	3.0	0.0	1.5	16	8	1.5	NP	NP	NP	20	8	28	12	8	A-3a	0	100							
		SS-2	3.0	4.5	1.5	3.0	8			2.5							16	10	A-4a	8		N ₆₀ & Mc					
		SS-3	4.5	6.0	3.0	4.5	15			3	24	16	8	32	20	52	15	11	A-4a	3							
		SS-4	6.0	7.5	4.5	6.0	18			1.5							15	10	A-4a	8							
9	B 009-0 20	SS-1	1.5	3.0	0.0	1.5	15	7	0.5								11	10	A-2-4	0	250						
		SS-2	3.0	4.5	1.5	3.0	7			26	17	9	32	15	47	16	12	A-4a	2				HP & Mc				
		SS-3	4.5	6.0	3.0	4.5	14			26	17	9	32	15	47	13	12	A-4a	2								
		SS-4	6.0	7.5	4.5	6.0	10			2.5							18	10	A-4a	8							



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
			From	To	From	To																					
10	B 010-0 20	SS-1	0.0	1.5	0.1	1.6	23	14	4.5	28	17	11	37	21	58	11	14	A-6a	5	170							
		SS-2	1.5	3.0	1.6	3.1	38		4.5	28	15	13	25	17	42	13	14	A-6a	2								
		SS-3	3.0	4.5	3.1	4.6	22		4.5									15	14	A-6a	10						
		SS-4	4.5	6.0	4.6	6.1	14		4.5									14	14	A-6a	10						
11	B 011-0 20	SS-1	1.5	3.0	0.0	1.5	16	7	1.75	25	16	9	38	26	64	15	11	A-4a	6	130			HP & Mc	12"			
		SS-2	3.0	4.5	1.5	3.0	12		2	25	16	9	27	12	39	14	11	A-4a	1				N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	7		2.5									17	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	14		2.5									16	10	A-4a	8						
12	B 012-0 20	SS-1	1.5	3.0	0.0	1.5	14	11		NP	NP	NP	17	6	23	12	6	A-1-b	0	100							
		SS-2	3.0	4.5	1.5	3.0	11											11	6	A-1-b	0						
		SS-3	4.5	6.0	3.0	4.5	11											13	6	A-1-b	0						
		SS-4	6.0	7.5	4.5	6.0	11			24	16	8	21	13	34	13	10	A-2-4	0								
13	B 013-0 20	SS-1	0.0	1.5	-0.5	1.0	15	15		NP	NP	NP	22	10	32	11	10	A-2-4	0	110							
		SS-2	1.5	3.0	1.0	2.5	31		4.5	29	19	10	50	36	86	18	14	A-4b	8		A-4b	Mc	30"				
		SS-3	3.0	4.5	2.5	4.0	30		4.5									18	10	A-4b	8						
		SS-4	4.5	6.0	4.0	5.5	18		4.5									14	10	A-4b	8						
14	B 014-0 20	SS-1	1.5	3.0	0.0	1.5	26	14		NP	NP	NP	20	10	30	10	10	A-2-4	0	100							
		SS-2	3.0	4.5	1.5	3.0	27											12	8	A-3a	0						
		SS-3	4.5	6.0	3.0	4.5	14		2.25	20	13	7	24	13	37	11	10	A-4a	0								
		SS-4	6.0	7.5	4.5	6.0	19											16	10	A-2-4	0						
15	B 015-0 20	SS-1	0.0	1.5	-0.7	0.8	20	16										8	6	A-1-b	0	100					
		SS-2	1.5	3.0	0.8	2.3	34			NP	NP	NP	13	3	16	6	6	A-1-b	0								
		SS-3	3.0	4.5	2.3	3.8	20											10	6	A-1-b	0						
		SS-4	4.5	6.0	3.8	5.3	16											7	6	A-1-b	0						
16	B 016-0 20	SS-1	1.5	3.0	0.0	1.5	16	16		NP	NP	NP	20	10	30	10	10	A-2-4	0	100							
		SS-2	3.0	4.5	1.5	3.0	29			NP	NP	NP						10	10	A-2-4	0						
		SS-3	4.5	6.0	3.0	4.5	26											9	8	A-3a	0						
		SS-4	6.0	7.5	4.5	6.0	25											12	8	A-3a	0						
17	B 017-0 20	SS-1	0.0	1.5	-0.5	1.0	11	4		NP	NP	NP	14	12	26	12	8	A-3a	0	100							
		SS-2	1.5	3.0	1.0	2.5	14			35	19	16	13	12	25	15	10	A-2-6	1				N ₆₀ & Mc	12"			
		SS-3	3.0	4.5	2.5	4.0	10											15	10	A-2-6	4						
		SS-4	4.5	6.0	4.0	5.5	4											16	10	A-2-6	4						
18	B 018-0 20	SS-1	1.5	3.0	0.0	1.5	16	11										11	10	A-4a	8	100					
		SS-2	3.0	4.5	1.5	3.0	29			NP	NP	NP	25	11	36	8	11	A-4a	0								
		SS-3	4.5	6.0	3.0	4.5	23											7	6	A-1-b	0						
		SS-4A	6.0	7.2	4.5	5.7	11											7	6	A-1-b	0						



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
19	B 019-0	SS-1A	1.5	2.0	0.0	0.5	20	20	4							12	10	A-4a	8	100							
		SS-1B	2.0	3.0	0.5	1.5	20			NP	NP	NP	14	3	17	9	8	A-3a	0								
		SS-2A	3.0	4.0	1.5	2.5	27			NP	NP	NP	13	4	17	8	6	A-1-b	0								
		SS-2B	4.0	4.5	2.5	3.0	27		1							14	10	A-4a	8					HP & Mc			
20	B 020-0	SS-1	1.5	3.0	0.0	1.5	29	10								10	10	A-2-4	0	140							
		SS-2	3.0	4.5	1.5	3.0	26			NP	NP	NP	24	7	31	6	10	A-2-4	0								
		SS-3	4.5	6.0	3.0	4.5	19									6	8	A-3a	0								
		SS-4	6.0	7.5	4.5	6.0	10									6	8	A-3a	0								
21	B 021-0	SS-1	1.5	3.0	0.0	1.5	19	14								10	8	A-3a	0	100							
		SS-2	3.0	4.5	1.5	3.0	18		3.25	21	17	4	39	12	51	17	12	A-4a	3						Mc		
		SS-3	4.5	6.0	3.0	4.5	25									13	8	A-3a	0								
		SS-4	6.0	7.5	4.5	6.0	14		3.25	24	17	7	42	20	62	23	12	A-4a	5								
22	B 022-0	SS-1	0.0	1.5	-0.5	1.0	10	10	3	27	17	10	30	17	47	12	12	A-4a	2	120					N ₆₀	12"	
		SS-2	1.5	3.0	1.0	2.5	25		4.5							11	10	A-4a	8								
		SS-3	3.0	4.5	2.5	4.0	19		4.5							12	10	A-4a	8								
		SS-4	4.5	6.0	4.0	5.5	12		4.5	31	17	14	37	30	67	14	12	A-4a	8								
23	B 023-0	SS-1	1.5	3.0	0.0	1.5	20	15	4.5							20	14	A-6a	10	110					Mc		
		SS-2	3.0	4.5	1.5	3.0	15		4.5	31	20	11	37	19	56	14	15	A-6a	5								
		SS-3	4.5	6.0	3.0	4.5	25		4.5							14	14	A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	16		4.5	39	20	19	48	39	87	19	16	A-6b	12								
24	B 024-0	SS-1A	0.0	1.0	-0.4	0.6	82	18	4.5							10	6	A-1-b	0	2000							
		SS-2	1.0	3.0	0.6	2.6	35		4.5	30	18	12	41	31	72	15	14	A-6a	8								
		SS-3	3.0	4.5	2.6	4.1	18		4.5	35	19	16	41	36	77	17	16	A-6b	10								
		SS-4	4.5	6.0	4.1	5.6	19		4.5							18	16	A-6b	16								
25	B 025-0	SS-1	1.5	3.0	0.0	1.5	14	12	4.5	28	18	10	52	32	84	20	13	A-4b	8						A-4b & Mc	12"	
		SS-2	3.0	4.5	1.5	3.0	12		2.75							19	10	A-4b	8	110							
		SS-3	4.5	6.0	3.0	4.5	29		3.5	24	16	8	24	13	37	13	11	A-4a	0								
		SS-4	6.0	7.5	4.5	6.0	12		3.25							22	10	A-4a	8								
26	B 026-0	SS-1	0.0	1.5	-1.0	0.5	11	11	4.5	23	16	7	33	21	54	11	11	A-4a	4	110						N ₆₀	12"
		SS-2	1.5	3.5	0.5	2.5	38		3.5	25	19	6	75	23	98	26	14	A-4b	8						Mc		
		SS-3B	3.5	4.5	2.5	3.5	20									10	8	A-3	0								
		SS-4	4.5	6.0	3.5	5.0	20									10	8	A-3	0								
27	B 027-0	SS-1	0.0	1.5	0.0	1.5	14	10		NP	NP	NP	28	13	41	10	11	A-4a	1	100							
		SS-2	1.5	3.0	1.5	3.0	16			NP	NP	NP	85	12	97	25	11	A-4b	8						A-4b		
		SS-3	3.0	4.5	3.0	4.5	14									15	8	A-3a	0								
		SS-4	4.5	6.0	4.5	6.0	10									22	10	A-4a	8								



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
			From	To	From	To																					
28	B 028-0 20	SS-1	1.5	3.0	0.0	1.5	11	11	4.5	22	15	7	33	22	55	13	10	A-4a	4	100			N ₆₀ & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	16		4.5	26	17	9	42	30	72	14	12	A-4a	7								
		SS-3	4.5	6.0	3.0	4.5	18		3									A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	23		2.25									A-6a	10								
29	B 029-0 20	SS-1	1.5	3.0	0.0	1.5	20	20										8	10	A-2-4	0	100					
		SS-2	3.0	4.5	1.5	3.0	26			NP	NP	NP	22	7	29	6	10	A-2-4	0								
		SS-3	4.5	6.0	3.0	4.5	25		4.5	19	13	6	23	9	32	12	10	A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	26											A-3a	0								
30	B 030-0 20	SS-1	0.0	1.5	-0.2	1.3	15	12	4.5	28	18	10	36	22	58	12	13	A-4a	5	5500							
		SS-2	1.5	3.0	1.3	2.8	26		4.5	28	17	11	38	28	66	12	14	A-6a	7								
		SS-3	3.0	4.5	2.8	4.3	19		4.5									A-6a	10								
		SS-4	4.5	6.0	4.3	5.8	12		4.25									A-6a	10								
31	B 031-0 20	SS-1	1.5	3.0	0.0	1.5	18	12	4.25	26	16	10	13	11	24	14	10	A-2-4	0				Mc				
		SS-2	3.0	4.5	1.5	3.0	19		2	26	17	9	46	33	79	21	12	A-4a	8				Mc				
		SS-3	4.5	6.0	3.0	4.5	12		4.5									A-4a	8								
		SS-4	6.0	7.5	4.5	6.0	15		3									A-4a	8								
32	B 032-0 20	SS-1	0.7	1.5	0.0	0.8	5	5	2.25	32	20	12	36	20	56	17	15	A-6a	5	100			N ₆₀		21"		
		SS-2	1.5	3.0	0.8	2.3	25		4.5	33	18	15	43	32	75	15	14	A-6a	10								
		SS-3	3.0	4.5	2.3	3.8	22		4.5									A-4a	8								
		SS-4	4.5	6.0	3.8	5.3	11		4									A-4a	8								
33	B 033-0 20	SS-1	1.5	3.0	0.0	1.5	25	16	4.5	32	18	14	38	30	68	13	14	A-6a	8	1400							
		SS-2	3.0	4.5	1.5	3.0	16		4.5	28	17	11	37	24	61	12	14	A-6a	6								
		SS-3	4.5	6.0	3.0	4.5	16		4.5									A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	18		4.5									A-6a	10								
34	B 034-0 20	SS-1	1.5	3.0	0.0	1.5	15	12	4.5	25	15	10	28	15	43	12	10	A-4a	2	310							
		SS-2	3.0	4.5	1.5	3.0	12		4.25	25	15	10	29	18	47	13	10	A-4a	2				N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	14		4.5									A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	15		4.5									A-6a	10								
35	B 035-0 20	SS-1	0.0	1.5	-1.1	0.4	10	10	4.5	32	18	14	38	23	61	16	14	A-6a	7	190			N ₆₀		12"		
		SS-2	1.5	3.0	0.4	1.9	25		4.5	31	19	12	30	20	50	12	14	A-6a	4								
		SS-3	3.0	4.5	1.9	3.4	27		1.5									A-6a	10				HP & Mc				
		SS-4	4.5	6.0	3.4	4.9	14		3									A-6a	10								
36	B 036-0 20	SS-1	0.0	1.5	-0.6	0.9	10	10	4.5	26	17	9	28	15	43	15	12	A-4a	2	100			N ₆₀ & Mc		12"		
		SS-2	1.5	3.0	0.9	2.4	22		4.5	34	18	16	40	27	67	15	16	A-6b	9								
		SS-3	3.0	4.5	2.4	3.9	23		4.5									A-6b	16								
		SS-4	4.5	6.0	3.9	5.4	18		4.5	34	19	15	37	20	57	12	14	A-6a	6								



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
37	B 037-0 20	SS-1	1.5	3.0	0.0	1.5	14	14	4.5									18	14	A-6a	10	380		N ₆₀ & Mc		12"	
		SS-2	3.0	4.5	1.5	3.0	16			39	22	17	36	31	67	17	17	A-6b	9								
		SS-3	4.5	6.0	3.0	4.5	23			29	19	10	27	14	41	11	14	A-4a	1								
		SS-4	6.0	7.5	4.5	6.0	22											13	10	A-4a	8						
38	B 038-0 20	SS-1	0.0	1.5	-0.8	0.8	10	10	4.5	31	19	12	36	20	56	13	14	A-6a	5	160		N ₆₀		12"			
		SS-2	1.5	3.0	0.8	2.3	27											15	14	A-6a	10						
		SS-3	3.0	4.5	2.3	3.8	15											14	14	A-6a	10						
		SS-4	4.5	6.0	3.8	5.3	26			30	19	11	43	32	75	13	14	A-6a	8								
39	B 039-0 20	SS-1	0.0	1.5	-0.7	0.8	11	11	4.5	30	17	13	39	25	64	13	14	A-6a	7	230		N ₆₀		12"			
		SS-2	1.5	3.0	0.8	2.3	38											11	14	A-6a	10						
		SS-3	3.0	4.5	2.3	3.8	18											12	14	A-6a	10						
		SS-4	4.5	6.0	3.8	5.3	18			22	15	7	31	14	45	12	10	A-4a	2								
40	B 040-0 20	SS-1	1.5	3.0	0.0	1.5	31	30	3	18	13	5	28	12	40	11	10	A-4a	1	100							
		SS-2	3.0	4.5	1.5	3.0	34			NP	NP	NP	28	13	41	10	11	A-4a	1								
		SS-3	4.5	6.0	3.0	4.5	41											9	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	33											9	10	A-4a	8						
41	B 041-0 20	SS-1	0.0	1.5	-0.6	0.9	30	30	4.25									7	10	A-2-4	0	100					
		SS-2	1.5	2.0	0.9	1.4	50											7	6	A-1-a	0						
		SS-3	3.0	4.5	2.4	3.9	52			41	25	16	33	12	45	13	22	A-7-6	4								
		SS-4	4.5	6.0	3.9	5.4	66											8	18	A-7-6	16						
42	B 042-0 20	SS-1	1.5	3.0	0.0	1.5	29	29	22	16	6	25	9	34	8	10	A-2-4	0	150								
		SS-2	3.0	4.3	1.5	2.8	50											8	0	Rock	0		Rock	Mc			
		SS-3	4.5	5.4	3.0	3.9	50											6	0	Rock	0						
		SS-4	6.0	6.5	4.5	5.0	50											0	Rock	0							
43	B 043-0 20	SS-1	1.5	3.0	0.0	1.5	16	16	NP	NP	NP	19	5	24	8	6	A-1-b	0	100								
		SS-2	3.0	4.5	1.5	3.0	27											16	10	A-2-4	0			Mc			
		SS-3	4.5	6.0	3.0	4.5	25											10	10	A-2-4	0						
		SS-4	6.0	7.5	4.5	6.0	18											11	8	A-3a	0						
44	B 044-0 20	SS-1	0.0	1.5	-0.6	0.9	7	3	4.5	29	21	8	38	21	59	14	16	A-4a	5	100		N ₆₀		15"			
		SS-2	1.5	3.0	0.9	2.4	11			25	18	7	42	20	62	15	13	A-4a	5			N ₆₀		12"			
		SS-3	3.0	4.5	2.4	3.9	3											23	10	A-4a	8						
		SS-4	4.5	6.0	3.9	5.4	22											12	10	A-2-6	4						
45	B 045-0 20	SS-1	0.0	1.5	-0.3	1.2	15	11	4.5	25	18	7	33	19	52	13	13	A-4a	3	170							
		SS-2	1.5	3.0	1.2	2.7	15			21	15	6	33	16	49	12	10	A-4a	3								
		SS-3	3.0	4.5	2.7	4.2	11											13	10	A-4a	8						
		SS-4	4.5	6.0	4.2	5.7	19											12	10	A-4a	8						



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
			From	To	From	To																					
46	B 046-0 20	SS-1	1.5	3.0	0.0	1.5	11	11	2.25	23	14	9	32	16	48	13	10	A-4a	3	110			N ₆₀ & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	20		4.5	27	17	10	43	24	67	14	12	A-4a	6								
		SS-3	4.5	6.0	3.0	4.5	18		4.5									A-4a	8								
		SS-4	6.0	7.5	4.5	6.0	26		4.5									A-4a	8								
47	B 047-0 20	SS-1	0.0	1.5	-0.7	0.8	16	16	4.5	25	16	9	34	22	56	11	11	A-4a	4								
		SS-2	1.5	3.0	0.8	2.3	45		4.5									A-4a	8	110			Mc				
		SS-3	3.0	4.5	2.3	3.8	20		4.5	34	19	15	37	42	79	18	14	A-6a	10								
		SS-4	4.5	6.0	3.8	5.3	16		3									A-6a	10								
48	B 048-0 20	SS-1	1.5	3.0	0.0	1.5	19	18										8	6	A-1-b	0	110					
		SS-2	3.0	4.5	1.5	3.0	18		4.5	34	17	17	39	29	68	15	16	A-6b	9								
		SS-3	4.5	6.0	3.0	4.5	19		4.5									A-6b	16								
		SS-4	6.0	7.5	4.5	6.0	20		4.5									A-6b	16								
49	B 049-0 20	SS-1	0.0	1.5	-0.7	0.8	14	12	3.75	39	20	19	34	24	58	17	16	A-6b	8	490							
		SS-2	1.5	3.0	0.8	2.3	25		4.5	41	20	21	44	33	77	19	18	A-7-6	13								
		SS-3	3.0	4.5	2.3	3.8	16		4.25									A-7-6	16								
		SS-4	4.5	6.0	3.8	5.3	12		3.75									A-7-6	16								
50	B 050-0 20	SS-1	1.5	3.0	0.0	1.5	31	29	4.5	27	18	9	25	14	39	11	13	A-4a	1	100							
		SS-2	3.0	4.5	1.5	3.0	29		4.5	36	20	16	33	20	53	11	16	A-6b	6								
		SS-3	4.5	6.0	3.0	4.5	31		4.5									A-6b	16								
		SS-4	6.0	7.5	4.5	6.0	63		4.5									A-6b	16								
51	B 051-0 20	SS-1	1.5	3.0	0.0	1.5	31	19	4.5									12	10	A-4a	8	100					
		SS-2	3.0	4.5	1.5	3.0	31		4.5	26	18	8	30	15	45	10	13	A-4a	2								
		SS-3	4.5	6.0	3.0	4.5	19		4.5	31	17	14	34	21	55	12	14	A-6a	6								
		SS-4	6.0	7.5	4.5	6.0	22		4.25									A-6a	10								
52	B 052-0 20	SS-1	1.5	3.0	0.0	1.5	16	16	3	25	17	8	23	10	33	10	10	A-2-4	0	100							
		SS-2	3.0	4.5	1.5	3.0	18			NP	NP	NP	10	4	14	6	6	A-1-a	0								
		SS-3	4.5	6.0	3.0	4.5	45											A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	22											A-2-4	0								
53	B 053-0 20	SS-1	0.0	1.5	0.0	1.5	7	7	4	36	22	14	31	18	49	17	17	A-6a	4	100			N ₆₀		15"		
		SS-2	1.5	3.0	1.5	3.0	15		4.5	34	21	13	47	28	75	19	16	A-6a	9				Mc				
		SS-3	3.0	4.5	3.0	4.5	20		4.5									A-6a	10								
		SS-4	4.5	6.0	4.5	6.0	23		4.5									A-6a	10								
54	B 054-0 20	SS-1	0.0	1.5	-0.8	0.7	8	8	2.5	35	20	15	28	17	45	15	15	A-6a	4	100			N ₆₀		12"		
		SS-2	1.5	3.0	0.7	2.2	23		4.5	28	18	10	44	29	73	15	13	A-4a	8								
		SS-3	3.0	4.5	2.2	3.7	15		2.75									A-4a	8								
		SS-4	4.5	6.0	3.7	5.2	15		2.25									A-4a	8								



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable	
55	B 055-0 20	SS-1	0.0	1.5	-1.4	0.1	10	10	1.5	39	22	17	31	24	55	20	17	A-6b	7	120		HP & Mc		12"	
		SS-2	1.5	3.0	0.1	1.6	15		4.5	37	20	17	40	47	87	18	16	A-6b	11						
		SS-3	3.0	4.5	1.6	3.1	22		3.25							18	16	A-6b	16						
		SS-4	4.5	6.0	3.1	4.6	15		1.75							14	16	A-6b	16						
56	B 056-0 20	SS-1	0.0	1.5	-0.6	0.9	14	14	2.5	30	17	13	39	25	64	14	14	A-6a	7	350					
		SS-2	1.5	3.0	0.9	2.4	19		3.75	37	20	17	37	23	60	17	16	A-6b	8						
		SS-3	3.0	4.5	2.4	3.9	23		2.75							16	16	A-6b	16						
		SS-4	4.5	6.0	3.9	5.4	14		3							14	16	A-6b	16						
57	B 057-0 20	SS-1	1.5	3.0	0.0	1.5	14	11		NP	NP	NP	36	14	50	10	11	A-4a	3	100					
		SS-2	3.0	4.5	1.5	3.0	15			NP	NP	NP	19	11	30	11	8	A-3a	0						
		SS-3	4.5	6.0	3.0	4.5	12									18	8	A-3a	0						
		SS-4	6.0	7.5	4.5	6.0	11		2.5							17	14	A-6a	10						
58	B 058-0 20	SS-1	1.5	3.0	0.0	1.5	11	5	4.5	29	18	11	22	14	36	12	13	A-4a	0	110		N ₆₀		12"	
		SS-2	3.0	4.5	1.5	3.0	8		2.25	38	35	3	33	16	49	20	30	A-6b	3			N ₆₀			
		SS-3	4.5	6.0	3.0	4.5	5		2							15	16	A-6b	16						
		SS-4	6.0	7.5	4.5	6.0	7		3							20	16	A-6b	16						
59	B 059-0 20	SS-1	1.5	3.0	0.0	1.5	12	10	4.5	26	15	11	31	21	52	13	14	A-6a	4	110					
		SS-2	3.0	4.5	1.5	3.0	15		4.25	24	14	10	32	21	53	14	10	A-4a	4			Mc			
		SS-3	4.5	6.0	3.0	4.5	10		2.25							18	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	15		2							20	10	A-4a	8						
60	B 060-0 20	SS-1	1.5	3.0	0.0	1.5	14	14	3.5	18	13	5	26	13	39	11	10	A-4a	1						
		SS-2	3.0	4.5	1.5	3.0	31		1.5	27	15	12	31	20	51	15	14	A-6a	4			HP			
		SS-3	4.5	6.0	3.0	4.5	20		4.5							10	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	22		4.5							13	10	A-4a	8						
61	B 061-0 20	SS-1	0.0	1.5	-0.5	1.0	8	8	2	38	27	11	28	17	45	15	22	A-6a	2	100		N ₆₀		12"	
		SS-2	1.5	3.0	1.0	2.5	11		2	42	30	12	32	18	50	20	25	A-6a	4			N ₆₀		12"	
		SS-3	3.0	4.5	2.5	4.0	11		2.5							19	14	A-6a	10						
		SS-4	4.5	6.0	4.0	5.5	19		4.5							13	10	A-4a	8						
62	B 062-0 20	SS-1	1.5	3.0	0.0	1.5	29	27								9	8	A-3a	0	100					
		SS-2	3.0	4.5	1.5	3.0	27		4.5	30	19	11	44	41	85	15	14	A-6a	8						
		SS-3	4.5	6.0	3.0	4.5	33		4.5	32	18	14	40	35	75	15	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	35		4.5							14	14	A-6a	10						
63	B 063-0 20	SS-1	0.0	1.5	-0.3	1.2	11	8	2.25	30	17	13	29	24	53	17	14	A-6a	5	140		N ₆₀ & Mc		12"	
		SS-2	1.5	3.0	1.2	2.7	8		2.25	43	21	22	38	47	85	23	18	A-7-6	13			N ₆₀ & Mc			
		SS-3	3.0	4.5	2.7	4.2	15		1.5							24	18	A-7-6	16						
		SS-4	4.5	6.0	4.2	5.7	18		1.75							28	18	A-7-6	16						



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
64	B 064-0 20	SS-1	1.5	3.0	0.0	1.5	15	15	4.5	26	16	10	37	22	59	15	11	A-4a	5	100		Mc				
		SS-2	3.0	4.5	1.5	3.0	23		4.5	24	16	8	34	19	53	14	11	A-4a	4			Mc				
		SS-3	4.5	6.0	3.0	4.5	23									17	10	A-2-4	0							
		SS-4	6.0	7.5	4.5	6.0	40									13	10	A-2-4	0							
65	B 065-0 20	SS-1	1.5	3.0	0.0	1.5	14	14	4.5	27	19	8	44	22	66	16	14	A-4a	6	100						
		SS-2	3.0	4.5	1.5	3.0	15		4.5	22	16	6	33	13	46	12	11	A-4a	2							
		SS-3	4.5	6.0	3.0	4.5	16		4.5							16	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	34									11	6	A-1-a	0							
66	B 066-0 20	SS-1	1.5	3.0	0.0	1.5	20	12	4.25	25	15	10	31	14	45	15	10	A-4a	2	100		Mc				
		SS-2	3.0	4.5	1.5	3.0	12		2.5	29	18	11	41	19	60	19	14	A-6a	5			N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	16		4.25							16	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	12									15	8	A-3a	0							
67	B 067-0 20	SS-1	1.5	3.0	0.0	1.5	14	5	3.25	24	14	10	20	10	30	14	10	A-2-4	0	100		N ₆₀ & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	5		3.5	24	16	8	21	12	33	13	10	A-2-4	0			N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	11		2.25							16	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	16		1.75							19	16	A-6b	16							
68	B 068-0 20	SS-1	1.5	3.0	0.0	1.5	34	22								9	8	A-3a	0	830						
		SS-2	3.0	4.5	1.5	3.0	27			NP	NP	NP	22	4	26	7	8	A-3a	0							
		SS-3	4.5	6.0	3.0	4.5	23									7	8	A-3a	0							
		SS-4	6.0	7.5	4.5	6.0	22									8	8	A-3a	0							
69	B 069-0 20	SS-1	1.5	3.0	0.0	1.5	16	12								11	10	A-2-4	0	100						
		SS-2	3.0	4.5	1.5	3.0	25			21	16	5	22	7	29	11	10	A-2-4	0							
		SS-3	4.5	6.0	3.0	4.5	12									10	10	A-2-4	0							
		SS-4	6.0	7.5	4.5	6.0	12									14	10	A-2-4	0							
70	B 070-0 20	SS-1	1.5	3.0	0.0	1.5	22	7	4.5	25	17	8	31	14	45	13	12	A-4a	2	100						
		SS-2	3.0	4.5	1.5	3.0	14		2.5	30	19	11	50	22	72	18	14	A-6a	8			N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	10		2.5							17	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	7									17	10	A-2-4	0							
71	B 071-0 20	SS-1	1.5	3.0	0.0	1.5	8	7	2.5							17	10	A-4a	8	100		N ₆₀ & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	7		0.25	26	18	8	34	16	50	18	13	A-4a	3			HP & Mc				
		SS-3	4.5	6.0	3.0	4.5	10									14	10	A-2-6	4							
		SS-4	6.0	7.5	4.5	6.0	7									15	10	A-2-6	4							
72	B 072-0 20	SS-1	1.5	3.0	0.0	1.5	61	15		NP	NP	NP	15	4	19	11	6	A-1-b	0	280						
		SS-2	3.0	4.5	1.5	3.0	15									18	6	A-1-b	0							
		SS-3	4.5	6.0	3.0	4.5	26		4.5	23	14	9	29	17	46	12	10	A-4a	2							
		SS-4	6.0	7.5	4.5	6.0	19		4.5							10	10	A-4a	8							



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable	
73	B 073-0 20	SS-1	2.5	4.0	1.0	2.5	14	11	4.5	26	16	10	28	20	48	14	11	A-4a	3	N ₆₀ & Mc			12"		
		SS-2	5.0	6.5	3.5	5.0	11		2.5							22	10	A-4a	8						
74	B 074-0 20	SS-1	1.5	3.0	0.0	1.5	10	8	3	22	15	7	25	15	40	12	10	A-3a	0	130					
		SS-2	3.0	4.5	1.5	3.0	12		2.75	40	24	16	41	21	62	30	19	A-4a	1						
		SS-3	4.5	6.0	3.0	4.5	8		1							23	10	A-6b	8						
		SS-4	6.0	7.5	4.5	6.0	10											A-4a	8						
75	B 075-0 20	SS-1	1.5	3.0	0.0	1.5	16	15		26	17	9	32	14	46	25	12	A-4a	2	310	Mc				
		SS-2	5.0	6.5	3.5	5.0	15		2.75							17	10	A-2-6	4						
76	B 076-0 20	SS-1	1.5	3.0	0.5	2.0	15	11	4.5	20	16	4	28	10	38	10	11	A-4a	1	100					
		SS-2	3.0	4.5	2.0	3.5	12			NP	NP	NP	41	7	48	13	11	A-4a	3						
		SS-3	4.5	6.0	3.5	5.0	11									13	10	A-4a	8						
		SS-4	6.0	7.5	5.0	6.5	11									9	10	A-4a	8						
77	B 077-0 20	SS-1	2.5	4.0	1.5	3.0	15	15		25	18	7	20	9	29	11	10	A-2-4	0						
		SS-2A	5.0	5.8	4.0	4.8	18									14	10	A-2-4	0						
		SS-2B	5.8	6.5	4.8	5.5	18		3							20	14	A-6a	10						
78	B 078-0 20	SS-1	1.5	3.0	0.5	2.0	18	18	4.5	35	20	15	45	37	82	19	15	A-6a	10	100	Mc				
		SS-2	3.0	4.5	2.0	3.5	18		4.5	32	20	12	45	31	76	17	15	A-6a	9						
		SS-3	4.5	6.0	3.5	5.0	25		4.5							19	14	A-6a	10						
		SS-4	6.0	7.5	5.0	6.5	26		4.5							20	16	A-6b	16						
79	B 079-0 20	SS-1	1.5	3.0	0.0	1.5	14	10	4.5	25	16	9	38	22	60	12	11	A-4a	5	310					
		SS-2	3.0	4.5	1.5	3.0	12		4	29	18	11	43	31	74	19	14	A-6a	8		N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	10		3							23	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	15		2.5							21	14	A-6a	10						
80	B 080-0 20	SS-1	1.5	3.0	0.0	1.5	14	14								3	8	A-3a	0	100					
		SS-2	3.0	4.5	1.5	3.0	20			NP	NP	NP	16	6	22	6	6	A-1-b	0						
		SS-3	4.5	6.0	3.0	4.5	19			NP	NP	NP	28	10	38	11	11	A-4a	1						
		SS-4	6.0	7.5	4.5	6.0	18									11	10	A-4a	8						
81	B 081-0 20	SS-1	1.5	3.0	0.0	1.5	16	16								10	8	A-3a	0	100					
		SS-2	3.0	4.5	1.5	3.0	16			NP	NP	NP	23	10	33	8	10	A-2-4	0						
		SS-3	4.5	6.0	3.0	4.5	18		4.5	35	20	15	49	38	87	19	15	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	19		4.5							21	14	A-6a	10						



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
82	B 082-0 20	SS-1	1.5	3.0	0.0	1.5	19	15	NP NP NP NP	NP	NP	NP	10	3	13	5	6	A-1-b	0	130						
		SS-2	3.0	4.5	1.5	3.0	15			NP	NP	NP	7	2	9	6	6	A-1-b	0							
		SS-3	4.5	6.0	3.0	4.5	20												A-1-b	0						
		SS-4	6.0	7.5	4.5	6.0	19												A-1-b	0						
83	B 083-0 20	SS-1	1.5	3.0	0.0	1.5	26	18	NP NP 4.5 4.25																	
		SS-2	3.0	4.5	1.5	3.0	18			NP	NP	NP	28	8	36	11	11	A-4a	0							
		SS-3	4.5	6.0	3.0	4.5	20			23	16	7	24	11	35	10	10	A-2-4	0							
		SS-4	6.0	7.5	4.5	6.0	25												A-2-4	0						
84	B 084-0 20	SS-1	1.5	3.0	0.0	1.5	19	10	3 3.75 3.5 3	3	32	18	14	36	33	69	17	14	A-6a	8	100			Mc		
		SS-2	3.0	4.5	1.5	3.0	10			28															N ₆₀	
		SS-3	4.5	6.0	3.0	4.5	20			30	19	11	39	19	58	17	14	A-6a	5							
		SS-4	6.0	7.5	4.5	6.0	16												A-6a	10						
85	B 085-0 20	SS-1	1.5	3.0	0.0	1.5	18	10	3 4.5 0.75 2.5	3									12	14	A-6a	10	100			
		SS-2	3.0	4.5	1.5	3.0	10			28	16	12	36	26	62	14	14	A-6a	6						N ₆₀	
		SS-3	4.5	6.0	3.0	4.5	11			69	34	35	42	48	90	17		A-7-5	20							
		SS-4	6.0	7.5	4.5	6.0	10												23		A-7-5	16				
86	B 086-0 20	SS-1	1.5	3.0	0.0	1.5	23	5	3.75 1.5 1 0.75	3.75	23	14	9	24	12	36	11	10	A-4a	0						
		SS-2	3.0	4.5	1.5	3.0	8												13	10	A-4a	8	100		HP & Mc	
		SS-3	4.5	6.0	3.0	4.5	5			46	23	23	35	23	58	30	20	A-7-6	10							
		SS-4	6.0	7.5	4.5	6.0	7												33	18	A-7-6	16				
87	B 087-0 20	SS-1	1.5	3.0	0.0	1.5	11	11	NP 4.5 4.25 4.5	NP	NP	NP	13	3	16	18	6	A-1-b	0	1200						
		SS-2	3.0	4.5	1.5	3.0	20			27	16	11	30	27	57	12	14	A-6a	5							
		SS-3	4.5	6.0	3.0	4.5	20												16	14	A-6a	10				
		SS-4	6.0	7.5	4.5	6.0	20												13	14	A-6a	10				
88	B 088-0 20	SS-1	1.5	3.0	0.0	1.5	15	8	NP NP 20 NP	NP	NP	NP	21	9	30	9	8	A-3a	0	100						
		SS-2	3.0	4.5	1.5	3.0	16			NP	NP	NP	14	6	20	7	8	A-3a	0							
		SS-3	4.5	6.0	3.0	4.5	8			13	7	24	11	35	13	10	A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	10												18	10	A-2-4	0				
89	B 089-0 20	SS-1	1.5	3.0	0.0	1.5	22	22	4.5 4.5 4.5 4.5																	
		SS-2	3.0	4.5	1.5	3.0	26			32	17	15	29	27	56	11	14	A-6a	6	110						
		SS-3	4.5	6.0	3.0	4.5	29			33	20	13	36	34	70	14	15	A-6a	8							
		SS-4	6.0	7.5	4.5	6.0	33												12	14	A-6a	10				
90	B 090-0 20	SS-1	1.5	3.0	0.0	1.5	18	10	4.5 4.5 2.25 1	21	16	5	30	14	44	11	11	A-4a	2							
		SS-2	3.0	4.5	1.5	3.0	10												13	10	A-4a	8	170		N ₆₀ & Mc	
		SS-3	4.5	6.0	3.0	4.5	14			32	18	14	35	32	67	19	14	A-6a	8							
		SS-4	6.0	7.5	4.5	6.0	16												31	14	A-6a	10				



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
91	B 091-0 20	SS-1	1.5	3.0	0.0	1.5	12	10	4.5	NP	NP	NP	18	9	27	12	10	A-2-4	0	170						
		SS-2	3.0	4.5	1.5	3.0	14											17	10	A-2-4	0			N ₆₀ & M _c		
		SS-3	4.5	6.0	3.0	4.5	12			3.25	32	18	14	31	23	54	15	14	A-6a	5						
		SS-4	6.0	7.5	4.5	6.0	10			2								23	14	A-6a	10					
92	B 092-0 20	SS-1	2.5	4.0	3.5	5.0	8	8	4.5	30	20	10	37	25	62	15	15	A-4a	5	310						
93	B 093-0 20	SS-1	2.5	4.0	4.4	5.9	33	30	4.5	32	18	14	32	20	52	14	14	A-6a	5	100						
94	B 095-0 20	SS-1	2.5	4.0	2.6	4.1	10	10	3.5	35	23	12	34	18	52	20	18	A-6a	4	1800						
		SS-2	5.0	6.5	5.1	6.6	14			4.5								18	14	A-6a						
95	B 096-0 20	SS-1	2.5	4.0	3.6	5.1	11	11	4								12	10	A-4a	8	190					

PID: 111404

County-Route-Section: SUM-77-24.12
No. of Borings: 95

Geotechnical Consultant: NEAS Inc.
Prepared By: KCA
Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options	
Global Geotextile Average(N60L):	12"
Average(HP):	0"
Global Geogrid Average(N60L):	0"
Average(HP):	0"

Design CBR	8
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% Samples within 6 feet of subgrade			
N ₆₀ ≤ 5	2%	HP ≤ 0.5	1%
N ₆₀ < 12	22%	0.5 < HP ≤ 1	2%
12 ≤ N ₆₀ < 15	13%	1 < HP ≤ 2	6%
N ₆₀ ≥ 20	36%	HP > 2	59%
M+	13%		
Rock	0%		
Unsuitable	4%		

Excavate and Replace at Surface	
Average	0"
Maximum	0"
Minimum	0"

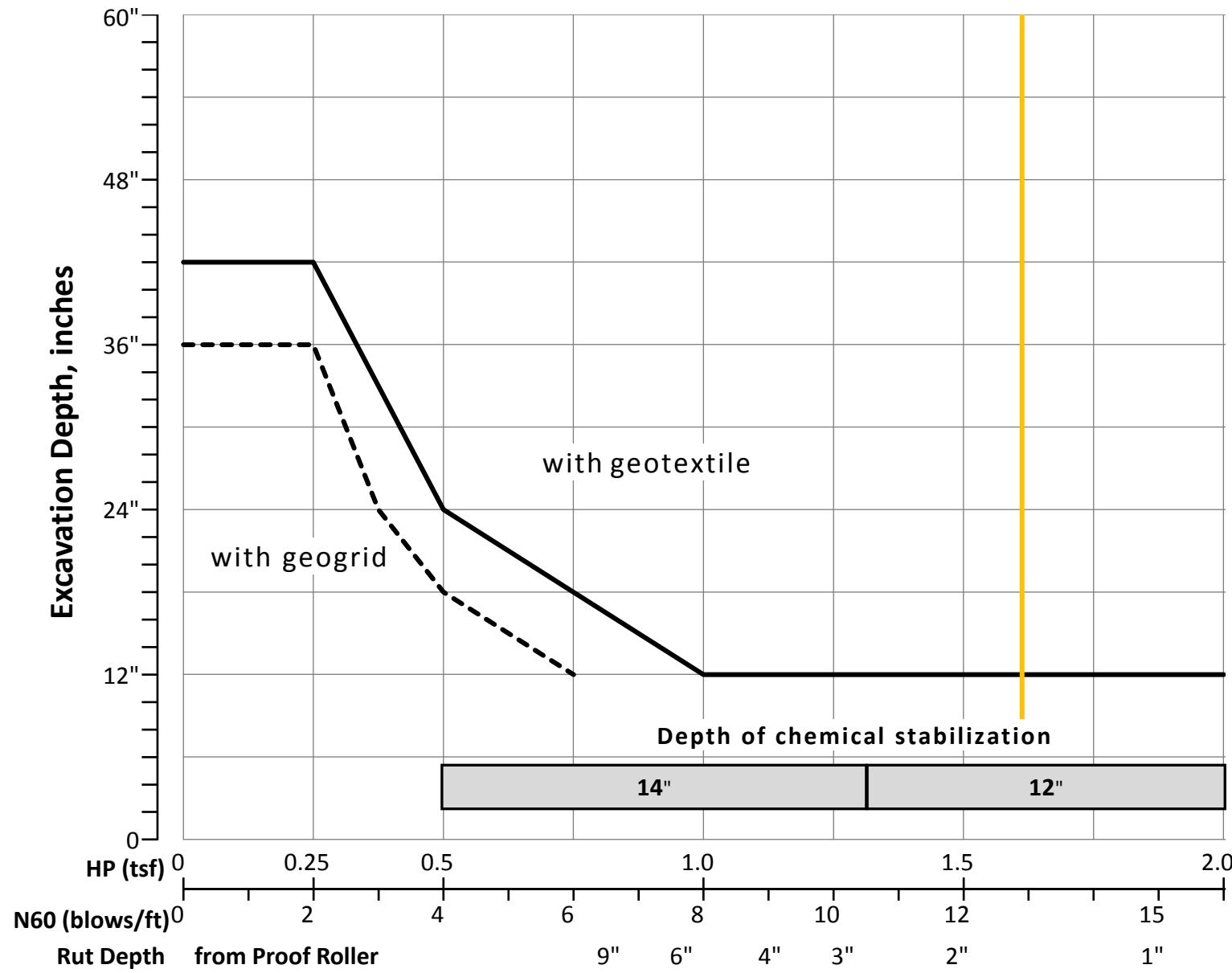
% Proposed Subgrade Surface	
Unstable & Unsuitable	35%
Unstable	32%
Unsuitable	3%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{opt}	GI
Average	19	13	3.66	29	18	11	32	19	51	14	12	5
Maximum	82	30	4.50	69	35	35	85	48	98	33	30	20
Minimum	3	3	0.25	18	13	3	7	2	9	3	0	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	3	3	24	38	0	8	0	2	30	111	8	0	96	26	2	10	0	0	361
Percent	1%	1%	7%	11%	0%	2%	0%	1%	8%	31%	2%	0%	27%	7%	1%	3%	0%	0%	100%
% Rock Granular Cohesive	1%	60%										39%						100%	
Surface Class Count	1	2	18	22	0	3	0	1	17	66	6	0	49	13	0	5	0	0	203
Surface Class Percent	0%	1%	9%	11%	0%	1%	0%	0%	8%	33%	3%	0%	24%	6%	0%	2%	0%	0%	100%



GB1 Figure B – Subgrade Stabilization

OVERRIDE TABLE

Calculated Average	New Values	Check to Override
3.66		<input type="checkbox"/> HP
12.95		<input type="checkbox"/> N60L

Average HP
Average N_{60L}

EXISTING SUBGRADE BORINGS

OHIO DEPARTMENT OF TRANSPORTATION
OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES
Geotechnical Bulletin GB1

SUM-77-24.12

111404

IR-77 Existing Subgrade

Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75

NEAS Inc.

Prepared By: KCA

Date prepared: Monday, January 11, 2021

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2800 Corporate Exchange Drive
Suite 240
Columbus, OH 43231
(920) 427-0671
brendan.andrews@neasinc.com

NO. OF BORINGS: **35**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-001-0-20	IR-77 NB	300+01	18	LT	CME 55X	82	1012.4	1010.9	1.5 C
2	B-002-0-20	IR-77 SB	403+91	3	LT	CME 55X	82	1012.2	1010.7	1.5 C
3	B-004-0-20	IR-77 SB	408+18	9	LT	CME 55X	82	1016.3	1014.8	1.5 C
4	B-007-0-20	IR-77 NB	315+00	41	RT	CME 45B	82	1002.0	1000.5	1.5 C
5	B-008-0-20	IR-77 SB	415+88	9	LT	CME 55X	82	1015.5	1014.0	1.5 C
6	B-009-0-20	IR-77 NB	319+10	1	LT	CME 55X	82	999.0	997.5	1.5 C
7	B-011-0-20	IR-77 NB	323+93	2	LT	CME 55X	82	995.0	993.5	1.5 C
8	B-012-0-20	IR-77 SB	424+12	9	RT	CME 55X	82	1000.6	999.1	1.5 C
9	B-014-0-20	IR-77 SB	428+74	41	LT	CME 55X	82	988.8	987.3	1.5 C
10	B-016-0-20	IR-77 SB	432+37	1	RT	CME 55X	82	981.2	979.7	1.5 C
11	B-018-0-20	IR-77 SB	436+21	0	RT	CME 55X	82	971.7	970.2	1.5 C
12	B-019-0-20	IR-77 NB	340+31	1	LT	CME 55X	82	963.9	962.4	1.5 C
13	B-020-0-20	IR-77 SB	440+21	1	RT	CME 55X	82	961.8	960.3	1.5 C
14	B-021-0-20	IR-77 NB	343+97	3	LT	CME 55X	82	955.0	953.5	1.5 C
15	B-023-0-20	IR-77 NB	348+72	6	LT	CME 55X	82	949.5	948.0	1.5 C
16	B-025-0-20	IR-77	664+36	39	RT	CME 55X	82	973.1	971.6	1.5 C
17	B-028-0-20	IR-77	676+34	39	LT	CME 55X	82	999.0	997.5	1.5 C
18	B-029-0-20	IR-77	680+33	71	RT	CME 45B	82	1001.8	1000.3	1.5 C
19	B-031-0-20	IR-77	688+28	41	RT	CME 55X	82	1006.3	1004.8	1.5 C
20	B-033-0-20	IR-77	696+54	35	RT	CME 55X	82	1009.6	1008.1	1.5 C
21	B-034-0-20	IR-77	701+52	23	LT	CME 55X	82	1014.7	1013.2	1.5 C
22	B-037-0-20	IR-77	712+59	47	RT	CME 55X	82	1044.8	1043.3	1.5 C
23	B-040-0-20	IR-77	724+53	41	LT	CME 55X	82	1080.3	1078.8	1.5 C
24	B-042-0-20	IR-77	732+51	71	LT	CME 55X	82	1104.1	1102.6	1.5 C
25	B-043-0-20	IR-77	736+56	40	RT	CME 55X	82	1116.6	1115.1	1.5 C
26	B-046-0-20	IR-77	748+52	41	LT	CME 55X	82	1152.3	1150.8	1.5 C
27	B-048-0-20	IR-77	756+55	41	LT	CME 55X	82	1170.9	1169.4	1.5 C
28	B-050-0-20	IR-77	764+57	33	LT	CME 55X	82	1178.7	1177.2	1.5 C
29	B-051-0-20	IR-77	768+59	32	RT	CME 55X	82	1181.9	1180.4	1.5 C
30	B-052-0-20	IR-77	773+45	23	LT	CME 55X	82	1183.0	1181.5	1.5 C
31	B-057-0-20	IR-77	793+08	72	RT	CME 55X	82	1164.9	1163.4	1.5 C
32	B-058-0-20	IR-77	797+10	38	LT	CME 55X	82	1161.2	1159.7	1.5 C
33	B-059-0-20	IR-77	799+87	99	RT	CME 45B	82	1158.4	1156.9	1.5 C
34	B-060-0-20	IR-77	805+10	40	LT	CME 55X	82	1160.8	1159.3	1.5 C
35	B-062-0-20	IR-77	813+15	40	LT	CME 55X	82	1164.5	1163.0	1.5 C



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
			From	To	From	To																					
1	B 001-0 20	SS-1A	1.5	2.7	0.0	1.2	19	19	3.75	NP	NP	NP	16	6	22	8	6	A-1-b	0	100							
		SS-2	2.7	4.5	1.2	3.0	22			33	20	13	54	41	95	18	15	A-6a	9			Mc					
		SS-3	4.5	6.0	3.0	4.5	23			4.5							15	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	25			4.5							15	14	A-6a	10							
2	B 002-0 20	SS-1	1.5	3.0	0.0	1.5	10	10	4.5								10	8	A-3a	0	100						
		SS-2	3.0	4.5	1.5	3.0	33			30	19	11	47	23	70	15	14	A-6a	7								
		SS-3	4.5	6.0	3.0	4.5	22			4.5							13	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	10			2.25	34	21	13	43	36	79	18	16	A-6a	9							
3	B 004-0 20	SS-1	1.5	3.0	0.0	1.5	15	10	4.25								10	10	A-2-6	4	100						
		SS-2	3.0	4.5	1.5	3.0	26			24	15	9	25	13	38	11	10	A-4a	1								
		SS-3	4.5	6.0	3.0	4.5	23			4.5							15	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	10			2	29	17	12	31	21	52	16	12	A-4a	4							
4	B 007-0 20	SS-1	1.5	3.0	0.0	1.5	18	16	4.25	28	17	11	39	17	56	11	14	A-6a	5	150							
		SS-2	3.0	4.5	1.5	3.0	16			27	17	10	33	19	52	12	12	A-4a	3								
		SS-3	4.5	6.0	3.0	4.5	20									16	10	A-4a	8								
		SS-4	6.0	7.5	4.5	6.0	22									14	10	A-4a	8								
5	B 008-0 20	SS-1	1.5	3.0	0.0	1.5	16	8	1.5	NP	NP	NP	20	8	28	12	8	A-3a	0	100							
		SS-2	3.0	4.5	1.5	3.0	8			2.5							16	10	A-4a	8			N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	15			3	24	16	8	32	20	52	15	11	A-4a	3							
		SS-4	6.0	7.5	4.5	6.0	18			1.5							15	10	A-4a	8							
6	B 009-0 20	SS-1	1.5	3.0	0.0	1.5	15	7	0.5								11	10	A-2-4	0	250						
		SS-2	3.0	4.5	1.5	3.0	7			26	17	9	32	15	47	16	12	A-4a	2			HP & Mc					
		SS-3	4.5	6.0	3.0	4.5	14			26	17	9	32	15	47	13	12	A-4a	2								
		SS-4	6.0	7.5	4.5	6.0	10			2.5							18	10	A-4a	8							
7	B 011-0 20	SS-1	1.5	3.0	0.0	1.5	16	7	1.75	25	16	9	38	26	64	15	11	A-4a	6	130			HP & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	12			25	16	9	27	12	39	14	11	A-4a	1			N ₆₀ & Mc					
		SS-3	4.5	6.0	3.0	4.5	7			2.5							17	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	14			2.5							16	10	A-4a	8							
8	B 012-0 20	SS-1	1.5	3.0	0.0	1.5	14	11	NP	NP	NP	17	6	23	12	6	A-1-b	0	100								
		SS-2	3.0	4.5	1.5	3.0	11										11	6	A-1-b	0							
		SS-3	4.5	6.0	3.0	4.5	11										13	6	A-1-b	0							
		SS-4	6.0	7.5	4.5	6.0	11			24	16	8	21	13	34	13	10	A-2-4	0								
9	B 014-0 20	SS-1	1.5	3.0	0.0	1.5	26	14	2.25	NP	NP	NP	20	10	30	10	10	A-2-4	0	100							
		SS-2	3.0	4.5	1.5	3.0	27										12	8	A-3a	0							
		SS-3	4.5	6.0	3.0	4.5	14			20	13	7	24	13	37	11	10	A-4a	0								
		SS-4	6.0	7.5	4.5	6.0	19										16	10	A-2-4	0							



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
10	B 016-0 20	SS-1	1.5	3.0	0.0	1.5	16	16	NP NP NP NP	NP	NP	NP	20	10	30	10	10	A-2-4	0	100							
		SS-2	3.0	4.5	1.5	3.0	29										10	10	A-2-4	0							
		SS-3	4.5	6.0	3.0	4.5	26										9	8	A-3a	0							
		SS-4	6.0	7.5	4.5	6.0	25										12	8	A-3a	0							
11	B 018-0 20	SS-1	1.5	3.0	0.0	1.5	16	11	NP NP NP NP								11	10	A-4a	8	100						
		SS-2	3.0	4.5	1.5	3.0	29						25	11	36	8	11	A-4a	0								
		SS-3	4.5	6.0	3.0	4.5	23										7	6	A-1-b	0							
		SS-4A	6.0	7.2	4.5	5.7	11										7	6	A-1-b	0							
12	B 019-0 20	SS-1A	1.5	2.0	0.0	0.5	20	20	4 NP NP NP 1								12	10	A-4a	8	100						
		SS-1B	2.0	3.0	0.5	1.5	20						14	3	17	9	8	A-3a	0								
		SS-2A	3.0	4.0	1.5	2.5	27						13	4	17	8	6	A-1-b	0								
		SS-2B	4.0	4.5	2.5	3.0	27										14	10	A-4a	8		HP & Mc					
13	B 020-0 20	SS-1	1.5	3.0	0.0	1.5	29	10	NP NP NP NP								10	10	A-2-4	0	140						
		SS-2	3.0	4.5	1.5	3.0	26						24	7	31	6	10	A-2-4	0								
		SS-3	4.5	6.0	3.0	4.5	19										6	8	A-3a	0							
		SS-4	6.0	7.5	4.5	6.0	10										6	8	A-3a	0							
14	B 021-0 20	SS-1	1.5	3.0	0.0	1.5	19	14	3.25 NP NP NP 3.25								10	8	A-3a	0	100						
		SS-2	3.0	4.5	1.5	3.0	18						39	12	51	17	12	A-4a	3				Mc				
		SS-3	4.5	6.0	3.0	4.5	25										13	8	A-3a	0							
		SS-4	6.0	7.5	4.5	6.0	14						42	20	62	23	12	A-4a	5								
15	B 023-0 20	SS-1	1.5	3.0	0.0	1.5	20	15	4.5 4.5 4.5 4.5								20	14	A-6a	10	110		Mc				
		SS-2	3.0	4.5	1.5	3.0	15						37	19	56	14	15	A-6a	5								
		SS-3	4.5	6.0	3.0	4.5	25										14	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	16						48	39	87	19	16	A-6b	12								
16	B 025-0 20	SS-1	1.5	3.0	0.0	1.5	14	12	4.5 2.75 3.5 3.25				52	32	84	20	13	A-4b	8		A-4b	N ₆₀ & Mc		12"			
		SS-2	3.0	4.5	1.5	3.0	12										19	10	A-4b	8	110	A-4b	N ₆₀ & Mc	36"			
		SS-3	4.5	6.0	3.0	4.5	29						24	13	37	13	11	A-4a	0								
		SS-4	6.0	7.5	4.5	6.0	12										22	10	A-4a	8							
17	B 028-0 20	SS-1	1.5	3.0	0.0	1.5	11	11	4.5 4.5 3 2.25				7	33	22	55	13	10	A-4a	4	100		N ₆₀ & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	16						42	30	72	14	12	A-4a	7								
		SS-3	4.5	6.0	3.0	4.5	18										14	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	23						9	32	12	10	A-6a	10									
18	B 029-0 20	SS-1	1.5	3.0	0.0	1.5	20	20	NP 4.5 4.5 4.5								8	10	A-2-4	0	100						
		SS-2	3.0	4.5	1.5	3.0	26						22	7	29	6	10	A-2-4	0								
		SS-3	4.5	6.0	3.0	4.5	25						23	9	32	12	10	A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	26										6	8	A-3a	0							



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
19	B 031-0	SS-1	1.5	3.0	0.0	1.5	18	12	4.25	26	16	10	13	11	24	14	10	A-2-4	0			Mc					
		SS-2	3.0	4.5	1.5	3.0	19		2	26	17	9	46	33	79	21	12	A-4a	8			Mc					
		SS-3	4.5	6.0	3.0	4.5	12		4.5									24	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	15		3									26	10	A-4a	8						
20	B 033-0	SS-1	1.5	3.0	0.0	1.5	25	16	4.5	32	18	14	38	30	68	13	14	A-6a	8	1400							
		SS-2	3.0	4.5	1.5	3.0	16		4.5	28	17	11	37	24	61	12	14	A-6a	6								
		SS-3	4.5	6.0	3.0	4.5	16		4.5									12	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	18		4.5									13	14	A-6a	10						
21	B 034-0	SS-1	1.5	3.0	0.0	1.5	15	12	4.5	25	15	10	28	15	43	12	10	A-4a	2	310							
		SS-2	3.0	4.5	1.5	3.0	12		4.25	25	15	10	29	18	47	13	10	A-4a	2			N ₆₀ & Mc					
		SS-3	4.5	6.0	3.0	4.5	14		4.5									13	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	15		4.5									17	14	A-6a	10						
22	B 037-0	SS-1	1.5	3.0	0.0	1.5	14	14										18	14	A-6a	10	380		N ₆₀ & Mc		12"	
		SS-2	3.0	4.5	1.5	3.0	16		4.5	39	22	17	36	31	67	17	17	A-6b	9								
		SS-3	4.5	6.0	3.0	4.5	23		3.5	29	19	10	27	14	41	11	14	A-4a	1								
		SS-4	6.0	7.5	4.5	6.0	22		4.5									13	10	A-4a	8						
23	B 040-0	SS-1	1.5	3.0	0.0	1.5	31	30	3	18	13	5	28	12	40	11	10	A-4a	1	100							
		SS-2	3.0	4.5	1.5	3.0	34			NP	NP	NP	28	13	41	10	11	A-4a	1								
		SS-3	4.5	6.0	3.0	4.5	41											9	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	33											9	10	A-4a	8						
24	B 042-0	SS-1	1.5	3.0	0.0	1.5	29	29		22	16	6	25	9	34	8	10	A-2-4	0	150							
		SS-2	3.0	4.3	1.5	2.8	50											8	0	Rock	0		Rock	Mc			
		SS-3	4.5	5.4	3.0	3.9	50											6	0	Rock	0						
		SS-4	6.0	6.5	4.5	5.0	50											0	Rock	0							
25	B 043-0	SS-1	1.5	3.0	0.0	1.5	16	16		NP	NP	NP	19	5	24	8	6	A-1-b	0	100							
		SS-2	3.0	4.5	1.5	3.0	27											16	10	A-2-4	0			Mc			
		SS-3	4.5	6.0	3.0	4.5	25											10	10	A-2-4	0						
		SS-4	6.0	7.5	4.5	6.0	18											11	8	A-3a	0						
26	B 046-0	SS-1	1.5	3.0	0.0	1.5	11	11	2.25	23	14	9	32	16	48	13	10	A-4a	3	110		N ₆₀ & Mc		12"			
		SS-2	3.0	4.5	1.5	3.0	20		4.5	27	17	10	43	24	67	14	12	A-4a	6								
		SS-3	4.5	6.0	3.0	4.5	18		4.5									13	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	26		4.5									15	10	A-4a	8						
27	B 048-0	SS-1	1.5	3.0	0.0	1.5	19	18										8	6	A-1-b	0	110					
		SS-2	3.0	4.5	1.5	3.0	18		4.5	34	17	17	39	29	68	15	16	A-6b	9								
		SS-3	4.5	6.0	3.0	4.5	19		4.5									16	16	A-6b	16						
		SS-4	6.0	7.5	4.5	6.0	20		4.5									21	16	A-6b	16						



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
28	B 050-0 20	SS-1	1.5	3.0	0.0	1.5	31	29	4.5	27	18	9	25	14	39	11	13	A-4a	1	100							
		SS-2	3.0	4.5	1.5	3.0	29		4.5	36	20	16	33	20	53	11	16	A-6b	6								
		SS-3	4.5	6.0	3.0	4.5	31		4.5							9	16	A-6b	16								
		SS-4	6.0	7.5	4.5	6.0	63		4.5							10	16	A-6b	16								
29	B 051-0 20	SS-1	1.5	3.0	0.0	1.5	31	19	4.5							12	10	A-4a	8	100							
		SS-2	3.0	4.5	1.5	3.0	31		4.5	26	18	8	30	15	45	10	13	A-4a	2								
		SS-3	4.5	6.0	3.0	4.5	19		4.5	31	17	14	34	21	55	12	14	A-6a	6								
		SS-4	6.0	7.5	4.5	6.0	22		4.25							16	14	A-6a	10								
30	B 052-0 20	SS-1	1.5	3.0	0.0	1.5	16	16	3	25	17	8	23	10	33	10	10	A-2-4	0	100							
		SS-2	3.0	4.5	1.5	3.0	18			NP	NP	NP	10	4	14	6	6	A-1-a	0								
		SS-3	4.5	6.0	3.0	4.5	45									10	10	A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	22									11	10	A-2-4	0								
31	B 057-0 20	SS-1	1.5	3.0	0.0	1.5	14	11		NP	NP	NP	36	14	50	10	11	A-4a	3	100							
		SS-2	3.0	4.5	1.5	3.0	15			NP	NP	NP	19	11	30	11	8	A-3a	0								
		SS-3	4.5	6.0	3.0	4.5	12									18	8	A-3a	0								
		SS-4	6.0	7.5	4.5	6.0	11		2.5							17	14	A-6a	10								
32	B 058-0 20	SS-1	1.5	3.0	0.0	1.5	11	5	4.5	29	18	11	22	14	36	12	13	A-4a	0	110			N ₆₀		12"		
		SS-2	3.0	4.5	1.5	3.0	8		2.25	38	35	3	33	16	49	20	30	A-6b	3				N ₆₀				
		SS-3	4.5	6.0	3.0	4.5	5		2							15	16	A-6b	16								
		SS-4	6.0	7.5	4.5	6.0	7		3							20	16	A-6b	16								
33	B 059-0 20	SS-1	1.5	3.0	0.0	1.5	12	10	4.5	26	15	11	31	21	52	13	14	A-6a	4	110							
		SS-2	3.0	4.5	1.5	3.0	15		4.25	24	14	10	32	21	53	14	10	A-4a	4				Mc				
		SS-3	4.5	6.0	3.0	4.5	10		2.25							18	10	A-4a	8								
		SS-4	6.0	7.5	4.5	6.0	15		2							20	10	A-4a	8								
34	B 060-0 20	SS-1	1.5	3.0	0.0	1.5	14	14	3.5	18	13	5	26	13	39	11	10	A-4a	1								
		SS-2	3.0	4.5	1.5	3.0	31		1.5	27	15	12	31	20	51	15	14	A-6a	4				HP				
		SS-3	4.5	6.0	3.0	4.5	20		4.5								10	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	22		4.5							13	10	A-4a	8								
35	B 062-0 20	SS-1	1.5	3.0	0.0	1.5	29	27								9	8	A-3a	0	100							
		SS-2	3.0	4.5	1.5	3.0	27		4.5	30	19	11	44	41	85	15	14	A-6a	8								
		SS-3	4.5	6.0	3.0	4.5	33		4.5	32	18	14	40	35	75	15	14	A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	35		4.5							14	14	A-6a	10								

PID: 111404

County-Route-Section: SUM-77-24.12
No. of Borings: 35

Geotechnical Consultant: NEAS Inc.
Prepared By: KCA
Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options	
Global Geotextile Average(N60L):	12"
Average(HP):	0"
Global Geogrid Average(N60L):	0"
Average(HP):	0"

Design CBR	8
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% Samples within 6 feet of subgrade			
N ₆₀ ≤ 5	1%	HP ≤ 0.5	1%
N ₆₀ < 12	14%	0.5 < HP ≤ 1	1%
12 ≤ N ₆₀ < 15	12%	1 < HP ≤ 2	6%
N ₆₀ ≥ 20	45%	HP > 2	56%
M+	14%		
Rock	1%		
Unsuitable	4%		

Excavate and Replace at Surface	
Average	0"
Maximum	0"
Minimum	0"

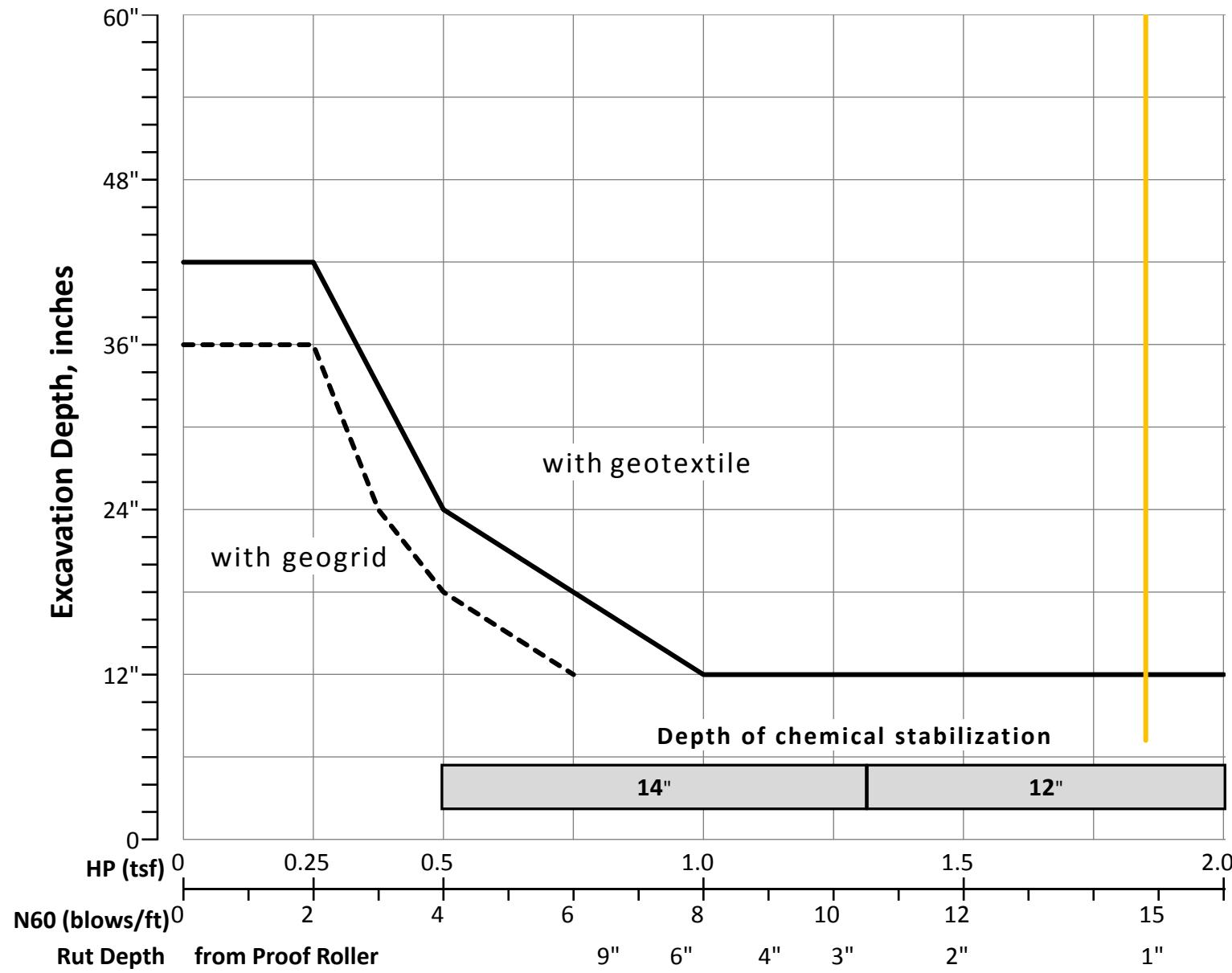
% Proposed Subgrade Surface	
Unstable & Unsuitable	35%
Unstable	31%
Unsuitable	4%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{opt}	GI
Average	20	15	3.67	27	17	10	30	18	48	13	11	5
Maximum	63	30	4.50	39	35	19	54	41	95	26	30	16
Minimum	5	5	0.50	18	13	3	10	3	14	6	0	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	3	1	9	18	0	1	0	0	15	53	2	0	27	11	0	0	0	0	140
Percent	2%	1%	6%	13%	0%	1%	0%	0%	11%	38%	1%	0%	19%	8%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	2%	69%										29%						100%	
Surface Class Count	1	1	6	12	0	1	0	0	7	27	2	0	11	4	0	0	0	0	72
Surface Class Percent	1%	1%	8%	17%	0%	1%	0%	0%	10%	38%	3%	0%	15%	6%	0%	0%	0%	0%	100%



GB1 Figure B – Subgrade Stabilization

OVERRIDE TABLE

Calculated Average	New Values	Check to Override
3.67		<input type="checkbox"/> HP
14.86		<input type="checkbox"/> N _{60L}

Average HP

Average N_{60L}

WIDENED AREA BORINGS

OHIO DEPARTMENT OF TRANSPORTATION**OFFICE OF GEOTECHNICAL ENGINEERING****PLAN SUBGRADES**
Geotechnical Bulletin GB1**SUM-77-24.12****111404****IR-77 Widened Area****Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75****NEAS Inc.**

Prepared By: KCA

Date prepared: Monday, January 11, 2021

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NO. OF BORINGS:**32**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-003-0-20	IR-77 NB	307+04	16	LT	CME 55X	82	1007.0	1007.6	0.6 F
2	B-005-0-20	IR-77 NB	310+99	15	LT	CME 55X	82	1006.1	1004.6	1.5 C
3	B-006-0-20	IR-77 SB	411+96	6	RT	CME 55X	82	1015.9	1015.5	0.4 C
4	B-010-0-20	IR-77 SB	419+97	15	RT	CME 55X	82	1008.2	1008.3	0.1 F
5	B-013-0-20	IR-77 NB	328+78	16	LT	CME 55X	82	988.5	988.0	0.5 C
6	B-015-0-20	IR-77 NB	332+00	16	LT	CME 55X	82	982.8	982.1	0.7 C
7	B-017-0-20	IR-77 NB	336+02	13	LT	CME 55X	82	972.9	972.4	0.5 C
8	B-022-0-20	IR-77 SB	443+14	12	RT	CME 55X	82	954.4	953.9	0.5 C
9	B-024-0-20	IR-77	660+27	14	LT	CME 55X	82	962.0	961.6	0.4 C
10	B-026-0-20	IR-77	668+28	33	LT	CME 55X	82	982.2	981.2	1.0 C
11	B-027-0-20	IR-77	672+27	30	RT	CME 55X	82	990.9	990.9	0.0 F
12	B-030-0-20	IR-77	684+31	29	LT	CME 55X	82	1002.6	1002.4	0.2 C
13	B-032-0-20	IR-77	692+52	26	LT	CME 55X	82	1007.1	1006.4	0.7 C
14	B-035-0-20	IR-77	705+15	25	RT	CME 55X	82	1021.6	1020.5	1.1 C
15	B-036-0-20	IR-77	708+46	32	LT	CME 55X	82	1031.1	1030.5	0.6 C
16	B-038-0-20	IR-77	716+54	34	LT	CME 55X	82	1055.8	1055.0	0.8 C
17	B-039-0-20	IR-77	720+49	34	RT	CME 55X	82	1067.4	1066.7	0.7 C
18	B-041-0-20	IR-77	728+54	33	RT	CME 55X	82	1091.5	1090.9	0.6 C
19	B-044-0-20	IR-77	740+56	34	LT	CME 55X	82	1127.6	1127.0	0.6 C
20	B-045-0-20	IR-77	744+53	32	RT	CME 55X	82	1139.4	1139.1	0.3 C
21	B-047-0-20	IR-77	752+52	32	RT	CME 55X	82	1162.3	1161.6	0.7 C
22	B-049-0-20	IR-77	760+56	31	RT	CME 55X	82	1174.8	1174.1	0.7 C
23	B-053-0-20	IR-77	777+09	19	RT	CME 55X	82	1179.2	1179.2	0.0 F
24	B-054-0-20	IR-77	781+04	27	LT	CME 55X	82	1176.1	1175.3	0.8 C
25	B-055-0-20	IR-77	784+58	35	RT	CME 55X	82	1173.2	1171.8	1.4 C
26	B-056-0-20	IR-77	789+10	34	LT	CME 55X	82	1168.1	1167.5	0.6 C
27	B-061-0-20	IR-77	809+75	34	RT	CME 55X	82	1162.0	1161.5	0.5 C
28	B-063-0-20	IR-77	816+93	27	RT	CME 55X	82	1165.0	1164.7	0.3 C
29	B-092-0-20	IR-77 SB	413+49	12	RT	CME 55X	82	1014.1	1015.1	1.0 F
30	B-093-0-20	IR-77 SB	416+09	22	RT	CME 55X	82	1011.3	1013.2	1.9 F
31	B-095-0-20	IR-77 NB	313+26	16	LT	CME 55X	82	1002.2	1002.3	0.1 F
32	B-096-0-20	IR-77 NB	316+24	25	LT	CME 55X	82	998.9	1000.0	1.1 F



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
1	B 003-0 20	SS-1	0.0	1.5	0.6	2.1	12	7	1.5	NP	NP	NP	21	6	27	8	8	A-3a	0	100							
		SS-2	1.5	3.0	2.1	3.6	11												10	8	A-3a	0					
		SS-3	3.0	4.5	3.6	5.1	7												9	8	A-3a	0					
		SS-4	4.5	6.0	5.1	6.6	7						50	25	75	23	13	A-4b									
2	B 005-0 20	SS-2	1.5	3.0	0.0	1.5	16	8	1.5	NP	NP	NP	13	3	16	8	6	A-1-b	0	100							
		SS-3	3.0	4.5	1.5	3.0	16												8	6	A-1-b	0					
		SS-4	4.5	6.0	3.0	4.5	8												25	10	A-4a	8					
3	B 006-0 20	SS-1	0.0	1.5	-0.4	1.1	25	7	4.25	4.5	28	20	8	31	16	47	11	15	A-4a	2	100						
		SS-2	1.5	3.0	1.1	2.6	8												17	10	A-4a	8					
		SS-3	3.0	4.5	2.6	4.1	7						40	27	67	16	14	A-6a	7								
		SS-4	4.5	6.0	4.1	5.6	14												16	14	A-6a	10					
4	B 010-0 20	SS-1	0.0	1.5	0.1	1.6	23	14	4.5	4.5	28	17	11	37	21	58	11	14	A-6a	5	170						
		SS-2	1.5	3.0	1.6	3.1	38						25	17	42	13	14	A-6a	2								
		SS-3	3.0	4.5	3.1	4.6	22												15	14	A-6a	10					
		SS-4	4.5	6.0	4.6	6.1	14												14	14	A-6a	10					
5	B 013-0 20	SS-1	0.0	1.5	-0.5	1.0	15	15	4.5	NP	NP	NP	22	10	32	11	10	A-2-4	0	110							
		SS-2	1.5	3.0	1.0	2.5	31						50	36	86	18	14	A-4b	8								
		SS-3	3.0	4.5	2.5	4.0	30												18	10	A-4b	8					
		SS-4	4.5	6.0	4.0	5.5	18												14	10	A-4b	8					
6	B 015-0 20	SS-1	0.0	1.5	-0.7	0.8	20	16	4.5										8	6	A-1-b	0	100				
		SS-2	1.5	3.0	0.8	2.3	34						13	3	16	6	6	A-1-b	0								
		SS-3	3.0	4.5	2.3	3.8	20												10	6	A-1-b	0					
		SS-4	4.5	6.0	3.8	5.3	16												7	6	A-1-b	0					
7	B 017-0 20	SS-1	0.0	1.5	-0.5	1.0	11	4	4.5	NP	NP	NP	14	12	26	12	8	A-3a	0	100							
		SS-2	1.5	3.0	1.0	2.5	14						35	19	25	15	10	A-2-6	1								
		SS-3	3.0	4.5	2.5	4.0	10												15	10	A-2-6	4					
		SS-4	4.5	6.0	4.0	5.5	4												16	10	A-2-6	4					
8	B 022-0 20	SS-1	0.0	1.5	-0.5	1.0	10	10	4.5	3	27	17	10	30	17	47	12	12	A-4a	2	120						
		SS-2	1.5	3.0	1.0	2.5	25												11	10	A-4a	8					
		SS-3	3.0	4.5	2.5	4.0	19												12	10	A-4a	8					
		SS-4	4.5	6.0	4.0	5.5	12						37	30	67	14	12	A-4a	8								
9	B 024-0 20	SS-1A	0.0	1.0	-0.4	0.6	82	18	4.5										10	6	A-1-b	0	2000				
		SS-2	1.0	3.0	0.6	2.6	35						41	31	72	15	14	A-6a	8								
		SS-3	3.0	4.5	2.6	4.1	18						41	36	77	17	16	A-6b	10								
		SS-4	4.5	6.0	4.1	5.6	19												18	16	A-6b	16					



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
			From	To	From	To																				
10	B 026-0 20	SS-1	0.0	1.5	-1.0	0.5	11	11	4.5	23	16	7	33	21	54	11	11	A-4a	4	110		N ₆₀		12"		
		SS-2	1.5	3.5	0.5	2.5	38		3.5	25	19	6	75	23	98	26	14	A-4b	8		A-4b	Mc	30"			
		SS-3B	3.5	4.5	2.5	3.5	20									10	8	A-3	0							
		SS-4	4.5	6.0	3.5	5.0	20									10	8	A-3	0							
11	B 027-0 20	SS-1	0.0	1.5	0.0	1.5	14	10		NP	NP	NP	28	13	41	10	11	A-4a	1	100						
		SS-2	1.5	3.0	1.5	3.0	16			NP	NP	NP	85	12	97	25	11	A-4b	8		A-4b	Mc				
		SS-3	3.0	4.5	3.0	4.5	14									15	8	A-3a	0							
		SS-4	4.5	6.0	4.5	6.0	10									22	10	A-4a	8							
12	B 030-0 20	SS-1	0.0	1.5	-0.2	1.3	15	12	4.5	28	18	10	36	22	58	12	13	A-4a	5	5500						
		SS-2	1.5	3.0	1.3	2.8	26		4.5	28	17	11	38	28	66	12	14	A-6a	7							
		SS-3	3.0	4.5	2.8	4.3	19		4.5							13	14	A-6a	10							
		SS-4	4.5	6.0	4.3	5.8	12		4.25							14	14	A-6a	10							
13	B 032-0 20	SS-1	0.7	1.5	0.0	0.8	5	5	2.25	32	20	12	36	20	56	17	15	A-6a	5	100		N ₆₀		21"		
		SS-2	1.5	3.0	0.8	2.3	25		4.5	33	18	15	43	32	75	15	14	A-6a	10							
		SS-3	3.0	4.5	2.3	3.8	22		4.5							15	10	A-4a	8							
		SS-4	4.5	6.0	3.8	5.3	11		4							20	10	A-4a	8							
14	B 035-0 20	SS-1	0.0	1.5	-1.1	0.4	10	10	4.5	32	18	14	38	23	61	16	14	A-6a	7	190		N ₆₀		12"		
		SS-2	1.5	3.0	0.4	1.9	25		4.5	31	19	12	30	20	50	12	14	A-6a	4							
		SS-3	3.0	4.5	1.9	3.4	27		1.5							24	14	A-6a	10		HP & Mc					
		SS-4	4.5	6.0	3.4	4.9	14		3							16	14	A-6a	10							
15	B 036-0 20	SS-1	0.0	1.5	-0.6	0.9	10	10	4.5	26	17	9	28	15	43	15	12	A-4a	2	100		N ₆₀ & Mc		12"		
		SS-2	1.5	3.0	0.9	2.4	22		4.5	34	18	16	40	27	67	15	16	A-6b	9							
		SS-3	3.0	4.5	2.4	3.9	23		4.5							18	16	A-6b	16							
		SS-4	4.5	6.0	3.9	5.4	18		4.5	34	19	15	37	20	57	12	14	A-6a	6							
16	B 038-0 20	SS-1	0.0	1.5	-0.8	0.8	10	10	4.5	31	19	12	36	20	56	13	14	A-6a	5	160		N ₆₀		12"		
		SS-2	1.5	3.0	0.8	2.3	27		4.5							15	14	A-6a	10							
		SS-3	3.0	4.5	2.3	3.8	15		4.5							14	14	A-6a	10							
		SS-4	4.5	6.0	3.8	5.3	26		4.5	30	19	11	43	32	75	13	14	A-6a	8							
17	B 039-0 20	SS-1	0.0	1.5	-0.7	0.8	11	11	4.5	30	17	13	39	25	64	13	14	A-6a	7	230		N ₆₀		12"		
		SS-2	1.5	3.0	0.8	2.3	38		4.5							11	14	A-6a	10							
		SS-3	3.0	4.5	2.3	3.8	18		4.5							12	14	A-6a	10							
		SS-4	4.5	6.0	3.8	5.3	18		4.5	22	15	7	31	14	45	12	10	A-4a	2							
18	B 041-0 20	SS-1	0.0	1.5	-0.6	0.9	30	30								7	10	A-2-4	0	100						
		SS-2	1.5	2.0	0.9	1.4	50									7	6	A-1-a	0							
		SS-3	3.0	4.5	2.4	3.9	52		4.25	41	25	16	33	12	45	13	22	A-7-6	4							
		SS-4	4.5	6.0	3.9	5.4	66		4.5							8	18	A-7-6	16							



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable	
			From	To	From	To																			
19	B 044-0	SS-1	0.0	1.5	-0.6	0.9	7	3	4.5	29	21	8	38	21	59	14	16	A-4a	5	100		N ₆₀		15"	
		SS-2	1.5	3.0	0.9	2.4	11		4.25	25	18	7	42	20	62	15	13	A-4a	5			N ₆₀		12"	
		SS-3	3.0	4.5	2.4	3.9	3									23	10	A-4a	8						
		SS-4	4.5	6.0	3.9	5.4	22									12	10	A-2-6	4						
20	B 045-0	SS-1	0.0	1.5	-0.3	1.2	15	11	4.5	25	18	7	33	19	52	13	13	A-4a	3	170					
		SS-2	1.5	3.0	1.2	2.7	15		4.25	21	15	6	33	16	49	12	10	A-4a	3						
		SS-3	3.0	4.5	2.7	4.2	11		2.5							13	10	A-4a	8						
		SS-4	4.5	6.0	4.2	5.7	19		4.5							12	10	A-4a	8						
21	B 047-0	SS-1	0.0	1.5	-0.7	0.8	16	16	4.5	25	16	9	34	22	56	11	11	A-4a	4						
		SS-2	1.5	3.0	0.8	2.3	45		4.5							13	10	A-4a	8	110			Mc		
		SS-3	3.0	4.5	2.3	3.8	20		4.5	34	19	15	37	42	79	18	14	A-6a	10						
		SS-4	4.5	6.0	3.8	5.3	16		3							17	14	A-6a	10						
22	B 049-0	SS-1	0.0	1.5	-0.7	0.8	14	12	3.75	39	20	19	34	24	58	17	16	A-6b	8	490					
		SS-2	1.5	3.0	0.8	2.3	25		4.5	41	20	21	44	33	77	19	18	A-7-6	13						
		SS-3	3.0	4.5	2.3	3.8	16		4.25							17	18	A-7-6	16						
		SS-4	4.5	6.0	3.8	5.3	12		3.75							19	18	A-7-6	16						
23	B 053-0	SS-1	0.0	1.5	0.0	1.5	7	7	4	36	22	14	31	18	49	17	17	A-6a	4	100		N ₆₀		15"	
		SS-2	1.5	3.0	1.5	3.0	15		4.5	34	21	13	47	28	75	19	16	A-6a	9			Mc			
		SS-3	3.0	4.5	3.0	4.5	20		4.5							23	14	A-6a	10						
		SS-4	4.5	6.0	4.5	6.0	23		4.5							16	14	A-6a	10						
24	B 054-0	SS-1	0.0	1.5	-0.8	0.7	8	8	2.5	35	20	15	28	17	45	15	15	A-6a	4	100		N ₆₀		12"	
		SS-2	1.5	3.0	0.7	2.2	23		4.5	28	18	10	44	29	73	15	13	A-4a	8						
		SS-3	3.0	4.5	2.2	3.7	15		2.75							16	10	A-4a	8						
		SS-4	4.5	6.0	3.7	5.2	15		2.25							16	10	A-4a	8						
25	B 055-0	SS-1	0.0	1.5	-1.4	0.1	10	10	1.5	39	22	17	31	24	55	20	17	A-6b	7	120		HP & Mc		12"	
		SS-2	1.5	3.0	0.1	1.6	15		4.5	37	20	17	40	47	87	18	16	A-6b	11						
		SS-3	3.0	4.5	1.6	3.1	22		3.25							18	16	A-6b	16						
		SS-4	4.5	6.0	3.1	4.6	15		1.75							14	16	A-6b	16						
26	B 056-0	SS-1	0.0	1.5	-0.6	0.9	14	14	2.5	30	17	13	39	25	64	14	14	A-6a	7	350					
		SS-2	1.5	3.0	0.9	2.4	19		3.75	37	20	17	37	23	60	17	16	A-6b	8						
		SS-3	3.0	4.5	2.4	3.9	23		2.75							16	16	A-6b	16						
		SS-4	4.5	6.0	3.9	5.4	14		3							14	16	A-6b	16						
27	B 061-0	SS-1	0.0	1.5	-0.5	1.0	8	8	2	38	27	11	28	17	45	15	22	A-6a	2	100		N ₆₀		12"	
		SS-2	1.5	3.0	1.0	2.5	11		2	42	30	12	32	18	50	20	25	A-6a	4			N ₆₀		12"	
		SS-3	3.0	4.5	2.5	4.0	11		2.5							19	14	A-6a	10						
		SS-4	4.5	6.0	4.0	5.5	19		4.5							13	10	A-4a	8						



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)			
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable				
28	B 063-0 20	SS-1	0.0	1.5	-0.3	1.2	11	8	2.25	30	17	13	29	24	53	17	14	A-6a	5	140			N ₆₀ & Mc		12"			
		SS-2	1.5	3.0	1.2	2.7	8		2.25	43	21	22	38	47	85	23	18	A-7-6	13				N ₆₀ & Mc					
		SS-3	3.0	4.5	2.7	4.2	15		1.5							24	18	A-7-6	16									
		SS-4	4.5	6.0	4.2	5.7	18		1.75							28	18	A-7-6	16									
29	B 092-0 20	SS-1	2.5	4.0	3.5	5.0	8	8	4.5	30	20	10	37	25	62	15	15	A-4a	5	310								
30	B 093-0 20	SS-1	2.5	4.0	4.4	5.9	33	30	4.5	32	18	14	32	20	52	14	14	A-6a	5	100								
31	B 095-0 20	SS-1	2.5	4.0	2.6	4.1	10	10	3.5	35	23	12	34	18	52	20	18	A-6a	4	1800								
		SS-2	5.0	6.5	5.1	6.6	14		4.5								18	14	A-6a									
32	B 096-0 20	SS-1	2.5	4.0	3.6	5.1	11	11	4								12	10	A-4a	8	190							

PID: 111404

County-Route-Section: SUM-77-24.12
No. of Borings: 32

Geotechnical Consultant: NEAS Inc.
Prepared By: KCA
Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	No
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options		
Global Geotextile Average(N60L):	12"	0"
Global Geogrid Average(N60L):	0"	0"

Design CBR	7
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% Samples within 6 feet of subgrade			
N₆₀ ≤ 5	3%	HP ≤ 0.5	0%
N₆₀ < 12	28%	0.5 < HP ≤ 1	0%
12 ≤ N₆₀ < 15	12%	1 < HP ≤ 2	8%
N₆₀ ≥ 20	34%	HP > 2	71%
M+	10%		
Rock	0%		
Unsuitable	5%		

Excavate and Replace at Surface		
Average		0"
Maximum		12"
Minimum		0"

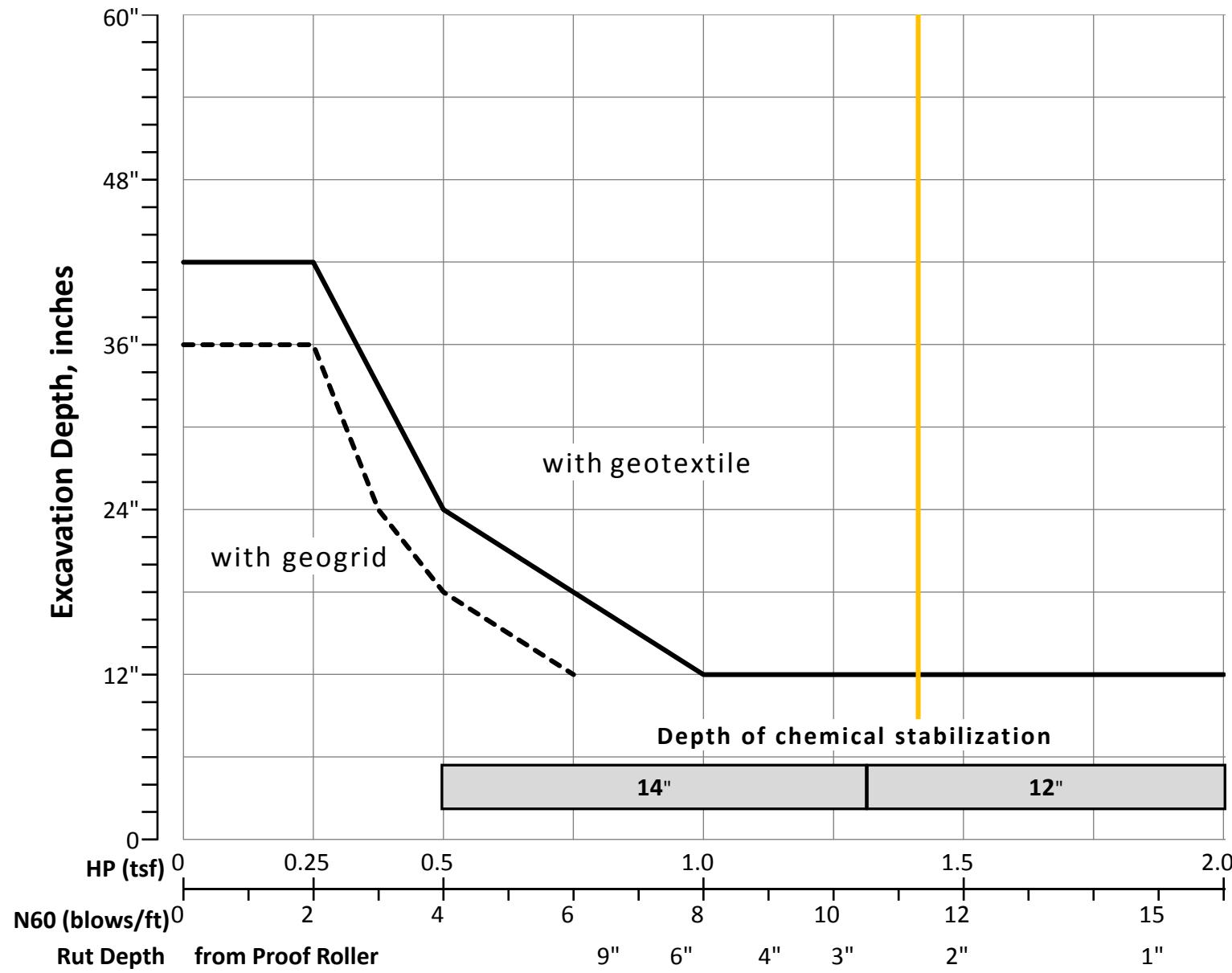
% Proposed Subgrade Surface		
Unstable & Unsuitable	34%	
Unstable	30%	
Unsuitable	4%	

	N₆₀	N_{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M_c	M_{opt}	GI
Average	19	11	3.83	31	19	12	36	22	58	15	13	7
Maximum	82	30	4.50	43	30	22	85	47	98	28	25	16
Minimum	3	3	1.50	21	15	6	13	3	16	6	6	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	1	7	2	0	4	0	2	5	30	6	0	39	12	0	8	0	0	116
Percent	0%	1%	6%	2%	0%	3%	0%	2%	4%	26%	5%	0%	34%	10%	0%	7%	0%	0%	100%
% Rock Granular Cohesive	0%	44%										56%						100%	
Surface Class Count	0	1	6	2	0	2	0	1	3	20	4	0	27	9	0	5	0	0	80
Surface Class Percent	0%	1%	8%	3%	0%	3%	0%	1%	4%	25%	5%	0%	34%	11%	0%	6%	0%	0%	100%



GB1 Figure B – Subgrade Stabilization

OVERRIDE TABLE

Calculated Average	New Values	Check to Override
3.83		<input type="checkbox"/> HP
11.38		<input type="checkbox"/> N60L

Average HP
Average N_{60L}

IR-77

OHIO DEPARTMENT OF TRANSPORTATION
OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES
Geotechnical Bulletin GB1

SUM-77-24.12

111404

IR-77

Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75

NEAS Inc.

Prepared By: KCA

Date prepared: Monday, January 11, 2021

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NO. OF BORINGS: **63**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-001-0-20	IR-77 NB	300+01	18	LT	CME 55X	82	1012.4	1010.9	1.5 C
2	B-002-0-20	IR-77 SB	403+91	3	LT	CME 55X	82	1012.2	1010.7	1.5 C
3	B-003-0-20	IR-77 NB	307+04	16	LT	CME 55X	82	1007.0	1007.6	0.6 F
4	B-004-0-20	IR-77 SB	408+18	9	LT	CME 55X	82	1016.3	1014.8	1.5 C
5	B-005-0-20	IR-77 NB	310+99	15	LT	CME 55X	82	1006.1	1004.6	1.5 C
6	B-006-0-20	IR-77 SB	411+96	6	RT	CME 55X	82	1015.9	1015.5	0.4 C
7	B-007-0-20	IR-77 NB	315+00	41	RT	CME 45B	82	1002.0	1000.5	1.5 C
8	B-008-0-20	IR-77 SB	415+88	9	LT	CME 55X	82	1015.5	1014.0	1.5 C
9	B-009-0-20	IR-77 NB	319+10	1	LT	CME 55X	82	999.0	997.5	1.5 C
10	B-010-0-20	IR-77 SB	419+97	15	RT	CME 55X	82	1008.2	1008.3	0.1 F
11	B-011-0-20	IR-77 NB	323+93	2	LT	CME 55X	82	995.0	993.5	1.5 C
12	B-012-0-20	IR-77 SB	424+12	9	RT	CME 55X	82	1000.6	999.1	1.5 C
13	B-013-0-20	IR-77 NB	328+78	16	LT	CME 55X	82	988.5	988.0	0.5 C
14	B-014-0-20	IR-77 SB	428+74	41	LT	CME 55X	82	988.8	987.3	1.5 C
15	B-015-0-20	IR-77 NB	332+00	16	LT	CME 55X	82	982.8	982.1	0.7 C
16	B-016-0-20	IR-77 SB	432+37	1	RT	CME 55X	82	981.2	979.7	1.5 C
17	B-017-0-20	IR-77 NB	336+02	13	LT	CME 55X	82	972.9	972.4	0.5 C
18	B-018-0-20	IR-77 SB	436+21	0	RT	CME 55X	82	971.7	970.2	1.5 C
19	B-019-0-20	IR-77 NB	340+31	1	LT	CME 55X	82	963.9	962.4	1.5 C
20	B-020-0-20	IR-77 SB	440+21	1	RT	CME 55X	82	961.8	960.3	1.5 C
21	B-021-0-20	IR-77 NB	343+97	3	LT	CME 55X	82	955.0	953.5	1.5 C
22	B-022-0-20	IR-77 SB	443+14	12	RT	CME 55X	82	954.4	953.9	0.5 C
23	B-023-0-20	IR-77 NB	348+72	6	LT	CME 55X	82	949.5	948.0	1.5 C
24	B-024-0-20	IR-77	660+27	14	LT	CME 55X	82	962.0	961.6	0.4 C
25	B-025-0-20	IR-77	664+36	39	RT	CME 55X	82	973.1	971.6	1.5 C
26	B-026-0-20	IR-77	668+28	33	LT	CME 55X	82	982.2	981.2	1.0 C
27	B-027-0-20	IR-77	672+27	30	RT	CME 55X	82	990.9	990.9	0.0 F
28	B-028-0-20	IR-77	676+34	39	LT	CME 55X	82	999.0	997.5	1.5 C
29	B-029-0-20	IR-77	680+33	71	RT	CME 45B	82	1001.8	1000.3	1.5 C
30	B-030-0-20	IR-77	684+31	29	LT	CME 55X	82	1002.6	1002.4	0.2 C
31	B-031-0-20	IR-77	688+28	41	RT	CME 55X	82	1006.3	1004.8	1.5 C
32	B-032-0-20	IR-77	692+52	26	LT	CME 55X	82	1007.1	1006.4	0.7 C
33	B-033-0-20	IR-77	696+54	35	RT	CME 55X	82	1009.6	1008.1	1.5 C
34	B-034-0-20	IR-77	701+52	23	LT	CME 55X	82	1014.7	1013.2	1.5 C
35	B-035-0-20	IR-77	705+15	25	RT	CME 55X	82	1021.6	1020.5	1.1 C
36	B-036-0-20	IR-77	708+46	32	LT	CME 55X	82	1031.1	1030.5	0.6 C
37	B-037-0-20	IR-77	712+59	47	RT	CME 55X	82	1044.8	1043.3	1.5 C
38	B-038-0-20	IR-77	716+54	34	LT	CME 55X	82	1055.8	1055.0	0.8 C
39	B-039-0-20	IR-77	720+49	34	RT	CME 55X	82	1067.4	1066.7	0.7 C
40	B-040-0-20	IR-77	724+53	41	LT	CME 55X	82	1080.3	1078.8	1.5 C
41	B-041-0-20	IR-77	728+54	33	RT	CME 55X	82	1091.5	1090.9	0.6 C
42	B-042-0-20	IR-77	732+51	71	LT	CME 55X	82	1104.1	1102.6	1.5 C
43	B-043-0-20	IR-77	736+56	40	RT	CME 55X	82	1116.6	1115.1	1.5 C
44	B-044-0-20	IR-77	740+56	34	LT	CME 55X	82	1127.6	1127.0	0.6 C
45	B-045-0-20	IR-77	744+53	32	RT	CME 55X	82	1139.4	1139.1	0.3 C

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
46	B-046-0-20	IR-77	748+52	41	LT	CME 55X	82	1152.3	1150.8	1.5 C
47	B-047-0-20	IR-77	752+52	32	RT	CME 55X	82	1162.3	1161.6	0.7 C
48	B-048-0-20	IR-77	756+55	41	LT	CME 55X	82	1170.9	1169.4	1.5 C
49	B-049-0-20	IR-77	760+56	31	RT	CME 55X	82	1174.8	1174.1	0.7 C
50	B-050-0-20	IR-77	764+57	33	LT	CME 55X	82	1178.7	1177.2	1.5 C
51	B-051-0-20	IR-77	768+59	32	RT	CME 55X	82	1181.9	1180.4	1.5 C
52	B-052-0-20	IR-77	773+45	23	LT	CME 55X	82	1183.0	1181.5	1.5 C
53	B-053-0-20	IR-77	777+09	19	RT	CME 55X	82	1179.2	1179.2	0.0 F
54	B-054-0-20	IR-77	781+04	27	LT	CME 55X	82	1176.1	1175.3	0.8 C
55	B-055-0-20	IR-77	784+58	35	RT	CME 55X	82	1173.2	1171.8	1.4 C
56	B-056-0-20	IR-77	789+10	34	LT	CME 55X	82	1168.1	1167.5	0.6 C
57	B-057-0-20	IR-77	793+08	72	RT	CME 55X	82	1164.9	1163.4	1.5 C
58	B-058-0-20	IR-77	797+10	38	LT	CME 55X	82	1161.2	1159.7	1.5 C
59	B-059-0-20	IR-77	799+87	99	RT	CME 45B	82	1158.4	1156.9	1.5 C
60	B-060-0-20	IR-77	805+10	40	LT	CME 55X	82	1160.8	1159.3	1.5 C
61	B-061-0-20	IR-77	809+75	34	RT	CME 55X	82	1162.0	1161.5	0.5 C
62	B-062-0-20	IR-77	813+15	40	LT	CME 55X	82	1164.5	1163.0	1.5 C
63	B-063-0-20	IR-77	816+93	27	RT	CME 55X	82	1165.0	1164.7	0.3 C



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
			From	To	From	To																					
1	B 001-0 20	SS-1A	1.5	2.7	0.0	1.2	19	19	3.75	NP	NP	NP	16	6	22	8	6	A-1-b	0	100							
		SS-2	2.7	4.5	1.2	3.0	22			33	20	13	54	41	95	18	15	A-6a	9			Mc					
		SS-3	4.5	6.0	3.0	4.5	23			4.5							15	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	25			4.5							15	14	A-6a	10							
2	B 002-0 20	SS-1	1.5	3.0	0.0	1.5	10	10	4.5								10	8	A-3a	0	100						
		SS-2	3.0	4.5	1.5	3.0	33			30	19	11	47	23	70	15	14	A-6a	7								
		SS-3	4.5	6.0	3.0	4.5	22			4.5							13	14	A-6a	10							
		SS-4	6.0	7.5	4.5	6.0	10			2.25	34	21	13	43	36	79	18	16	A-6a	9							
3	B 003-0 20	SS-1	0.0	1.5	0.6	2.1	12	7	1.5	NP	NP	NP	21	6	27	8	8	A-3a	0	100							
		SS-2	1.5	3.0	2.1	3.6	11										10	8	A-3a	0							
		SS-3	3.0	4.5	3.6	5.1	7										9	8	A-3a	0							
		SS-4	4.5	6.0	5.1	6.6	7			25	18	7	50	25	75	23	13	A-4b									
4	B 004-0 20	SS-1	1.5	3.0	0.0	1.5	15	10	4.25								10	10	A-2-6	4	100						
		SS-2	3.0	4.5	1.5	3.0	26			24	15	9	25	13	38	11	10	A-4a	1								
		SS-3	4.5	6.0	3.0	4.5	23			4.5							15	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	10			2	29	17	12	31	21	52	16	12	A-4a	4							
5	B 005-0 20	SS-2	1.5	3.0	0.0	1.5	16	8	1.5	NP	NP	NP	13	3	16	8	6	A-1-b	0	100							
		SS-3	3.0	4.5	1.5	3.0	16										8	6	A-1-b	0							
		SS-4	4.5	6.0	3.0	4.5	8										25	10	A-4a	8							
6	B 006-0 20	SS-1	0.0	1.5	-0.4	1.1	25	7	4.25	28	20	8	31	16	47	11	15	A-4a	2	100						12"	
		SS-2	1.5	3.0	1.1	2.6	8										17	10	A-4a	8		N ₆₀ & Mc				12"	
		SS-3	3.0	4.5	2.6	4.1	7			29	17	12	40	27	67	16	14	A-6a	7							12"	
		SS-4	4.5	6.0	4.1	5.6	14			4.25							16	14	A-6a	10						12"	
7	B 007-0 20	SS-1	1.5	3.0	0.0	1.5	18	16	4.25	28	17	11	39	17	56	11	14	A-6a	5	150							
		SS-2	3.0	4.5	1.5	3.0	16			27	17	10	33	19	52	12	12	A-4a	3								
		SS-3	4.5	6.0	3.0	4.5	20										16	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	22										14	10	A-4a	8							
8	B 008-0 20	SS-1	1.5	3.0	0.0	1.5	16	8	2.5	NP	NP	NP	20	8	28	12	8	A-3a	0	100							
		SS-2	3.0	4.5	1.5	3.0	8										16	10	A-4a	8		N ₆₀ & Mc					
		SS-3	4.5	6.0	3.0	4.5	15			24	16	8	32	20	52	15	11	A-4a	3								
		SS-4	6.0	7.5	4.5	6.0	18			1.5							15	10	A-4a	8							
9	B 009-0 20	SS-1	1.5	3.0	0.0	1.5	15	7	0.5								11	10	A-2-4	0	250						
		SS-2	3.0	4.5	1.5	3.0	7			26	17	9	32	15	47	16	12	A-4a	2				HP & Mc				
		SS-3	4.5	6.0	3.0	4.5	14			26	17	9	32	15	47	13	12	A-4a	2								
		SS-4	6.0	7.5	4.5	6.0	10			2.5							18	10	A-4a	8							



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
10	B 010-0 20	SS-1	0.0	1.5	0.1	1.6	23	14	4.5	28	17	11	37	21	58	11	14	A-6a	5	170						
		SS-2	1.5	3.0	1.6	3.1	38		4.5	28	15	13	25	17	42	13	14	A-6a	2							
		SS-3	3.0	4.5	3.1	4.6	22		4.5							15	14	A-6a	10							
		SS-4	4.5	6.0	4.6	6.1	14		4.5							14	14	A-6a	10							
11	B 011-0 20	SS-1	1.5	3.0	0.0	1.5	16	7	1.75	25	16	9	38	26	64	15	11	A-4a	6	130		HP & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	12		2	25	16	9	27	12	39	14	11	A-4a	1			N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	7		2.5							17	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	14		2.5							16	10	A-4a	8							
12	B 012-0 20	SS-1	1.5	3.0	0.0	1.5	14	11		NP	NP	NP	17	6	23	12	6	A-1-b	0	100						
		SS-2	3.0	4.5	1.5	3.0	11									11	6	A-1-b	0							
		SS-3	4.5	6.0	3.0	4.5	11									13	6	A-1-b	0							
		SS-4	6.0	7.5	4.5	6.0	11			24	16	8	21	13	34	13	10	A-2-4	0							
13	B 013-0 20	SS-1	0.0	1.5	-0.5	1.0	15	15		NP	NP	NP	22	10	32	11	10	A-2-4	0	110						
		SS-2	1.5	3.0	1.0	2.5	31		4.5	29	19	10	50	36	86	18	14	A-4b	8		A-4b	Mc	30"			
		SS-3	3.0	4.5	2.5	4.0	30		4.5							18	10	A-4b	8							
		SS-4	4.5	6.0	4.0	5.5	18		4.5							14	10	A-4b	8							
14	B 014-0 20	SS-1	1.5	3.0	0.0	1.5	26	14		NP	NP	NP	20	10	30	10	10	A-2-4	0	100						
		SS-2	3.0	4.5	1.5	3.0	27									12	8	A-3a	0							
		SS-3	4.5	6.0	3.0	4.5	14		2.25	20	13	7	24	13	37	11	10	A-4a	0							
		SS-4	6.0	7.5	4.5	6.0	19									16	10	A-2-4	0							
15	B 015-0 20	SS-1	0.0	1.5	-0.7	0.8	20	16								8	6	A-1-b	0	100						
		SS-2	1.5	3.0	0.8	2.3	34			NP	NP	NP	13	3	16	6	6	A-1-b	0							
		SS-3	3.0	4.5	2.3	3.8	20									10	6	A-1-b	0							
		SS-4	4.5	6.0	3.8	5.3	16									7	6	A-1-b	0							
16	B 016-0 20	SS-1	1.5	3.0	0.0	1.5	16	16		NP	NP	NP	20	10	30	10	10	A-2-4	0	100						
		SS-2	3.0	4.5	1.5	3.0	29			NP	NP	NP				10	10	A-2-4	0							
		SS-3	4.5	6.0	3.0	4.5	26									9	8	A-3a	0							
		SS-4	6.0	7.5	4.5	6.0	25									12	8	A-3a	0							
17	B 017-0 20	SS-1	0.0	1.5	-0.5	1.0	11	4		NP	NP	NP	14	12	26	12	8	A-3a	0	100						
		SS-2	1.5	3.0	1.0	2.5	14			35	19	16	13	12	25	15	10	A-2-6	1			N ₆₀ & Mc		12"		
		SS-3	3.0	4.5	2.5	4.0	10									15	10	A-2-6	4							
		SS-4	4.5	6.0	4.0	5.5	4									16	10	A-2-6	4							
18	B 018-0 20	SS-1	1.5	3.0	0.0	1.5	16	11								11	10	A-4a	8	100						
		SS-2	3.0	4.5	1.5	3.0	29			NP	NP	NP	25	11	36	8	11	A-4a	0							
		SS-3	4.5	6.0	3.0	4.5	23									7	6	A-1-b	0							
		SS-4A	6.0	7.2	4.5	5.7	11									7	6	A-1-b	0							



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
19	B 019-0	SS-1A	1.5	2.0	0.0	0.5	20	20	4							12	10	A-4a	8	100							
		SS-1B	2.0	3.0	0.5	1.5	20			NP	NP	NP	14	3	17	9	8	A-3a	0								
		SS-2A	3.0	4.0	1.5	2.5	27			NP	NP	NP	13	4	17	8	6	A-1-b	0								
		SS-2B	4.0	4.5	2.5	3.0	27		1							14	10	A-4a	8					HP & Mc			
20	B 020-0	SS-1	1.5	3.0	0.0	1.5	29	10								10	10	A-2-4	0	140							
		SS-2	3.0	4.5	1.5	3.0	26			NP	NP	NP	24	7	31	6	10	A-2-4	0								
		SS-3	4.5	6.0	3.0	4.5	19									6	8	A-3a	0								
		SS-4	6.0	7.5	4.5	6.0	10									6	8	A-3a	0								
21	B 021-0	SS-1	1.5	3.0	0.0	1.5	19	14								10	8	A-3a	0	100							
		SS-2	3.0	4.5	1.5	3.0	18		3.25	21	17	4	39	12	51	17	12	A-4a	3						Mc		
		SS-3	4.5	6.0	3.0	4.5	25									13	8	A-3a	0								
		SS-4	6.0	7.5	4.5	6.0	14		3.25	24	17	7	42	20	62	23	12	A-4a	5								
22	B 022-0	SS-1	0.0	1.5	-0.5	1.0	10	10	3	27	17	10	30	17	47	12	12	A-4a	2	120					N ₆₀	12"	
		SS-2	1.5	3.0	1.0	2.5	25		4.5							11	10	A-4a	8								
		SS-3	3.0	4.5	2.5	4.0	19		4.5							12	10	A-4a	8								
		SS-4	4.5	6.0	4.0	5.5	12		4.5	31	17	14	37	30	67	14	12	A-4a	8								
23	B 023-0	SS-1	1.5	3.0	0.0	1.5	20	15	4.5							20	14	A-6a	10	110					Mc		
		SS-2	3.0	4.5	1.5	3.0	15		4.5	31	20	11	37	19	56	14	15	A-6a	5								
		SS-3	4.5	6.0	3.0	4.5	25		4.5							14	14	A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	16		4.5	39	20	19	48	39	87	19	16	A-6b	12								
24	B 024-0	SS-1A	0.0	1.0	-0.4	0.6	82	18	4.5							10	6	A-1-b	0	2000							
		SS-2	1.0	3.0	0.6	2.6	35		4.5	30	18	12	41	31	72	15	14	A-6a	8								
		SS-3	3.0	4.5	2.6	4.1	18		4.5	35	19	16	41	36	77	17	16	A-6b	10								
		SS-4	4.5	6.0	4.1	5.6	19		4.5							18	16	A-6b	16								
25	B 025-0	SS-1	1.5	3.0	0.0	1.5	14	12	4.5	28	18	10	52	32	84	20	13	A-4b	8						A-4b	12"	
		SS-2	3.0	4.5	1.5	3.0	12		2.75							19	10	A-4b	8	110							
		SS-3	4.5	6.0	3.0	4.5	29		3.5	24	16	8	24	13	37	13	11	A-4a	0								
		SS-4	6.0	7.5	4.5	6.0	12		3.25							22	10	A-4a	8								
26	B 026-0	SS-1	0.0	1.5	-1.0	0.5	11	11	4.5	23	16	7	33	21	54	11	11	A-4a	4	110						N ₆₀	12"
		SS-2	1.5	3.5	0.5	2.5	38		3.5	25	19	6	75	23	98	26	14	A-4b	8								
		SS-3B	3.5	4.5	2.5	3.5	20									10	8	A-3	0								
		SS-4	4.5	6.0	3.5	5.0	20									10	8	A-3	0								
27	B 027-0	SS-1	0.0	1.5	0.0	1.5	14	10		NP	NP	NP	28	13	41	10	11	A-4a	1	100							
		SS-2	1.5	3.0	1.5	3.0	16			NP	NP	NP	85	12	97	25	11	A-4b	8								
		SS-3	3.0	4.5	3.0	4.5	14									15	8	A-3a	0								
		SS-4	4.5	6.0	4.5	6.0	10									22	10	A-4a	8								



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
28	B 028-0 20	SS-1	1.5	3.0	0.0	1.5	11	11	4.5	22	15	7	33	22	55	13	10	A-4a	4	100			N ₆₀ & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	16		4.5	26	17	9	42	30	72	14	12	A-4a	7								
		SS-3	4.5	6.0	3.0	4.5	18		3							14	14	A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	23		2.25							15	14	A-6a	10								
29	B 029-0 20	SS-1	1.5	3.0	0.0	1.5	20	20								8	10	A-2-4	0	100							
		SS-2	3.0	4.5	1.5	3.0	26			NP	NP	NP	22	7	29	6	10	A-2-4	0								
		SS-3	4.5	6.0	3.0	4.5	25		4.5	19	13	6	23	9	32	12	10	A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	26									6	8	A-3a	0								
30	B 030-0 20	SS-1	0.0	1.5	-0.2	1.3	15	12	4.5	28	18	10	36	22	58	12	13	A-4a	5	5500							
		SS-2	1.5	3.0	1.3	2.8	26		4.5	28	17	11	38	28	66	12	14	A-6a	7								
		SS-3	3.0	4.5	2.8	4.3	19		4.5							13	14	A-6a	10								
		SS-4	4.5	6.0	4.3	5.8	12		4.25							14	14	A-6a	10								
31	B 031-0 20	SS-1	1.5	3.0	0.0	1.5	18	12	4.25	26	16	10	13	11	24	14	10	A-2-4	0				Mc				
		SS-2	3.0	4.5	1.5	3.0	19		2	26	17	9	46	33	79	21	12	A-4a	8				Mc				
		SS-3	4.5	6.0	3.0	4.5	12		4.5							24	10	A-4a	8								
		SS-4	6.0	7.5	4.5	6.0	15		3							26	10	A-4a	8								
32	B 032-0 20	SS-1	0.7	1.5	0.0	0.8	5	5	2.25	32	20	12	36	20	56	17	15	A-6a	5	100			N ₆₀		21"		
		SS-2	1.5	3.0	0.8	2.3	25		4.5	33	18	15	43	32	75	15	14	A-6a	10								
		SS-3	3.0	4.5	2.3	3.8	22		4.5							15	10	A-4a	8								
		SS-4	4.5	6.0	3.8	5.3	11		4							20	10	A-4a	8								
33	B 033-0 20	SS-1	1.5	3.0	0.0	1.5	25	16	4.5	32	18	14	38	30	68	13	14	A-6a	8	1400							
		SS-2	3.0	4.5	1.5	3.0	16		4.5	28	17	11	37	24	61	12	14	A-6a	6								
		SS-3	4.5	6.0	3.0	4.5	16		4.5							12	14	A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	18		4.5							13	14	A-6a	10								
34	B 034-0 20	SS-1	1.5	3.0	0.0	1.5	15	12	4.5	25	15	10	28	15	43	12	10	A-4a	2	310							
		SS-2	3.0	4.5	1.5	3.0	12		4.25	25	15	10	29	18	47	13	10	A-4a	2				N ₆₀ & Mc				
		SS-3	4.5	6.0	3.0	4.5	14		4.5							13	14	A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	15		4.5							17	14	A-6a	10								
35	B 035-0 20	SS-1	0.0	1.5	-1.1	0.4	10	10	4.5	32	18	14	38	23	61	16	14	A-6a	7	190			N ₆₀		12"		
		SS-2	1.5	3.0	0.4	1.9	25		4.5	31	19	12	30	20	50	12	14	A-6a	4								
		SS-3	3.0	4.5	1.9	3.4	27		1.5							24	14	A-6a	10				HP & Mc				
		SS-4	4.5	6.0	3.4	4.9	14		3							16	14	A-6a	10								
36	B 036-0 20	SS-1	0.0	1.5	-0.6	0.9	10	10	4.5	26	17	9	28	15	43	15	12	A-4a	2	100			N ₆₀ & Mc		12"		
		SS-2	1.5	3.0	0.9	2.4	22		4.5	34	18	16	40	27	67	15	16	A-6b	9								
		SS-3	3.0	4.5	2.4	3.9	23		4.5							18	16	A-6b	16								
		SS-4	4.5	6.0	3.9	5.4	18		4.5	34	19	15	37	20	57	12	14	A-6a	6								



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
37	B 037-0 20	SS-1	1.5	3.0	0.0	1.5	14	14	4.5							18	14	A-6a	10	380			N ₆₀ & Mc		12"		
		SS-2	3.0	4.5	1.5	3.0	16			39	22	17	36	31	67	17	17	A-6b	9								
		SS-3	4.5	6.0	3.0	4.5	23			29	19	10	27	14	41	11	14	A-4a	1								
		SS-4	6.0	7.5	4.5	6.0	22									13	10	A-4a	8								
38	B 038-0 20	SS-1	0.0	1.5	-0.8	0.8	10	10	4.5	31	19	12	36	20	56	13	14	A-6a	5	160			N ₆₀		12"		
		SS-2	1.5	3.0	0.8	2.3	27									15	14	A-6a	10								
		SS-3	3.0	4.5	2.3	3.8	15									14	14	A-6a	10								
		SS-4	4.5	6.0	3.8	5.3	26			30	19	11	43	32	75	13	14	A-6a	8								
39	B 039-0 20	SS-1	0.0	1.5	-0.7	0.8	11	11	4.5	30	17	13	39	25	64	13	14	A-6a	7	230			N ₆₀		12"		
		SS-2	1.5	3.0	0.8	2.3	38									11	14	A-6a	10								
		SS-3	3.0	4.5	2.3	3.8	18									12	14	A-6a	10								
		SS-4	4.5	6.0	3.8	5.3	18			22	15	7	31	14	45	12	10	A-4a	2								
40	B 040-0 20	SS-1	1.5	3.0	0.0	1.5	31	30	3	18	13	5	28	12	40	11	10	A-4a	1	100							
		SS-2	3.0	4.5	1.5	3.0	34			NP	NP	NP	28	13	41	10	11	A-4a	1								
		SS-3	4.5	6.0	3.0	4.5	41									9	10	A-4a	8								
		SS-4	6.0	7.5	4.5	6.0	33									9	10	A-4a	8								
41	B 041-0 20	SS-1	0.0	1.5	-0.6	0.9	30	30	4.25							7	10	A-2-4	0	100							
		SS-2	1.5	2.0	0.9	1.4	50									7	6	A-1-a	0								
		SS-3	3.0	4.5	2.4	3.9	52			41	25	16	33	12	45	13	22	A-7-6	4								
		SS-4	4.5	6.0	3.9	5.4	66									8	18	A-7-6	16								
42	B 042-0 20	SS-1	1.5	3.0	0.0	1.5	29	29	22	16	6	25	9	34	8	10	A-2-4	0	150								
		SS-2	3.0	4.3	1.5	2.8	50									8	0	Rock	0				Rock	Mc			
		SS-3	4.5	5.4	3.0	3.9	50									6	0	Rock	0								
		SS-4	6.0	6.5	4.5	5.0	50									0	0	Rock	0								
43	B 043-0 20	SS-1	1.5	3.0	0.0	1.5	16	16	NP	NP	NP	19	5	24	8	6	A-1-b	0	100								
		SS-2	3.0	4.5	1.5	3.0	27									16	10	A-2-4	0					Mc			
		SS-3	4.5	6.0	3.0	4.5	25									10	10	A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	18									11	8	A-3a	0								
44	B 044-0 20	SS-1	0.0	1.5	-0.6	0.9	7	3	4.5	29	21	8	38	21	59	14	16	A-4a	5	100			N ₆₀		15"		
		SS-2	1.5	3.0	0.9	2.4	11			25	18	7	42	20	62	15	13	A-4a	5				N ₆₀		12"		
		SS-3	3.0	4.5	2.4	3.9	3									23	10	A-4a	8								
		SS-4	4.5	6.0	3.9	5.4	22									12	10	A-2-6	4								
45	B 045-0 20	SS-1	0.0	1.5	-0.3	1.2	15	11	4.5	25	18	7	33	19	52	13	13	A-4a	3	170							
		SS-2	1.5	3.0	1.2	2.7	15			21	15	6	33	16	49	12	10	A-4a	3								
		SS-3	3.0	4.5	2.7	4.2	11									13	10	A-4a	8								
		SS-4	4.5	6.0	4.2	5.7	19									12	10	A-4a	8								



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
46	B 046-0 20	SS-1	1.5	3.0	0.0	1.5	11	11	2.25	23	14	9	32	16	48	13	10	A-4a	3	110			N ₆₀ & Mc		12"	
		SS-2	3.0	4.5	1.5	3.0	20		4.5	27	17	10	43	24	67	14	12	A-4a	6							
		SS-3	4.5	6.0	3.0	4.5	18		4.5							13	10	A-4a	8							
		SS-4	6.0	7.5	4.5	6.0	26		4.5							15	10	A-4a	8							
47	B 047-0 20	SS-1	0.0	1.5	-0.7	0.8	16	16	4.5	25	16	9	34	22	56	11	11	A-4a	4							
		SS-2	1.5	3.0	0.8	2.3	45		4.5							13	10	A-4a	8	110			Mc			
		SS-3	3.0	4.5	2.3	3.8	20		4.5	34	19	15	37	42	79	18	14	A-6a	10							
		SS-4	4.5	6.0	3.8	5.3	16		3							17	14	A-6a	10							
48	B 048-0 20	SS-1	1.5	3.0	0.0	1.5	19	18								8	6	A-1-b	0	110						
		SS-2	3.0	4.5	1.5	3.0	18		4.5	34	17	17	39	29	68	15	16	A-6b	9							
		SS-3	4.5	6.0	3.0	4.5	19		4.5							16	16	A-6b	16							
		SS-4	6.0	7.5	4.5	6.0	20		4.5							21	16	A-6b	16							
49	B 049-0 20	SS-1	0.0	1.5	-0.7	0.8	14	12	3.75	39	20	19	34	24	58	17	16	A-6b	8	490						
		SS-2	1.5	3.0	0.8	2.3	25		4.5	41	20	21	44	33	77	19	18	A-7-6	13							
		SS-3	3.0	4.5	2.3	3.8	16		4.25							17	18	A-7-6	16							
		SS-4	4.5	6.0	3.8	5.3	12		3.75							19	18	A-7-6	16							
50	B 050-0 20	SS-1	1.5	3.0	0.0	1.5	31	29	4.5	27	18	9	25	14	39	11	13	A-4a	1	100						
		SS-2	3.0	4.5	1.5	3.0	29		4.5	36	20	16	33	20	53	11	16	A-6b	6							
		SS-3	4.5	6.0	3.0	4.5	31		4.5							9	16	A-6b	16							
		SS-4	6.0	7.5	4.5	6.0	63		4.5							10	16	A-6b	16							
51	B 051-0 20	SS-1	1.5	3.0	0.0	1.5	31	19	4.5							12	10	A-4a	8	100						
		SS-2	3.0	4.5	1.5	3.0	31		4.5	26	18	8	30	15	45	10	13	A-4a	2							
		SS-3	4.5	6.0	3.0	4.5	19		4.5	31	17	14	34	21	55	12	14	A-6a	6							
		SS-4	6.0	7.5	4.5	6.0	22		4.25							16	14	A-6a	10							
52	B 052-0 20	SS-1	1.5	3.0	0.0	1.5	16	16	3	25	17	8	23	10	33	10	10	A-2-4	0	100						
		SS-2	3.0	4.5	1.5	3.0	18			NP	NP	NP	10	4	14	6	6	A-1-a	0							
		SS-3	4.5	6.0	3.0	4.5	45									10	10	A-2-4	0							
		SS-4	6.0	7.5	4.5	6.0	22									11	10	A-2-4	0							
53	B 053-0 20	SS-1	0.0	1.5	0.0	1.5	7	7	4	36	22	14	31	18	49	17	17	A-6a	4	100			N ₆₀		15"	
		SS-2	1.5	3.0	1.5	3.0	15		4.5	34	21	13	47	28	75	19	16	A-6a	9				Mc			
		SS-3	3.0	4.5	3.0	4.5	20		4.5							23	14	A-6a	10							
		SS-4	4.5	6.0	4.5	6.0	23		4.5							16	14	A-6a	10							
54	B 054-0 20	SS-1	0.0	1.5	-0.8	0.7	8	8	2.5	35	20	15	28	17	45	15	15	A-6a	4	100			N ₆₀		12"	
		SS-2	1.5	3.0	0.7	2.2	23		4.5	28	18	10	44	29	73	15	13	A-4a	8							
		SS-3	3.0	4.5	2.2	3.7	15		2.75							16	10	A-4a	8							
		SS-4	4.5	6.0	3.7	5.2	15		2.25							16	10	A-4a	8							



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable	
55	B 055-0 20	SS-1	0.0	1.5	-1.4	0.1	10	10	1.5	39	22	17	31	24	55	20	17	A-6b	7	120		HP & Mc		12"	
		SS-2	1.5	3.0	0.1	1.6	15		4.5	37	20	17	40	47	87	18	16	A-6b	11						
		SS-3	3.0	4.5	1.6	3.1	22		3.25							18	16	A-6b	16						
		SS-4	4.5	6.0	3.1	4.6	15		1.75							14	16	A-6b	16						
56	B 056-0 20	SS-1	0.0	1.5	-0.6	0.9	14	14	2.5	30	17	13	39	25	64	14	14	A-6a	7	350					
		SS-2	1.5	3.0	0.9	2.4	19		3.75	37	20	17	37	23	60	17	16	A-6b	8						
		SS-3	3.0	4.5	2.4	3.9	23		2.75							16	16	A-6b	16						
		SS-4	4.5	6.0	3.9	5.4	14		3							14	16	A-6b	16						
57	B 057-0 20	SS-1	1.5	3.0	0.0	1.5	14	11		NP	NP	NP	36	14	50	10	11	A-4a	3	100					
		SS-2	3.0	4.5	1.5	3.0	15			NP	NP	NP	19	11	30	11	8	A-3a	0						
		SS-3	4.5	6.0	3.0	4.5	12									18	8	A-3a	0						
		SS-4	6.0	7.5	4.5	6.0	11		2.5							17	14	A-6a	10						
58	B 058-0 20	SS-1	1.5	3.0	0.0	1.5	11	5	4.5	29	18	11	22	14	36	12	13	A-4a	0	110		N ₆₀		12"	
		SS-2	3.0	4.5	1.5	3.0	8		2.25	38	35	3	33	16	49	20	30	A-6b	3			N ₆₀			
		SS-3	4.5	6.0	3.0	4.5	5		2							15	16	A-6b	16						
		SS-4	6.0	7.5	4.5	6.0	7		3							20	16	A-6b	16						
59	B 059-0 20	SS-1	1.5	3.0	0.0	1.5	12	10	4.5	26	15	11	31	21	52	13	14	A-6a	4	110					
		SS-2	3.0	4.5	1.5	3.0	15		4.25	24	14	10	32	21	53	14	10	A-4a	4			Mc			
		SS-3	4.5	6.0	3.0	4.5	10		2.25							18	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	15		2							20	10	A-4a	8						
60	B 060-0 20	SS-1	1.5	3.0	0.0	1.5	14	14	3.5	18	13	5	26	13	39	11	10	A-4a	1						
		SS-2	3.0	4.5	1.5	3.0	31		1.5	27	15	12	31	20	51	15	14	A-6a	4			HP			
		SS-3	4.5	6.0	3.0	4.5	20		4.5							10	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	22		4.5							13	10	A-4a	8						
61	B 061-0 20	SS-1	0.0	1.5	-0.5	1.0	8	8	2	38	27	11	28	17	45	15	22	A-6a	2	100		N ₆₀		12"	
		SS-2	1.5	3.0	1.0	2.5	11		2	42	30	12	32	18	50	20	25	A-6a	4			N ₆₀		12"	
		SS-3	3.0	4.5	2.5	4.0	11		2.5							19	14	A-6a	10						
		SS-4	4.5	6.0	4.0	5.5	19		4.5							13	10	A-4a	8						
62	B 062-0 20	SS-1	1.5	3.0	0.0	1.5	29	27								9	8	A-3a	0	100					
		SS-2	3.0	4.5	1.5	3.0	27		4.5	30	19	11	44	41	85	15	14	A-6a	8						
		SS-3	4.5	6.0	3.0	4.5	33		4.5	32	18	14	40	35	75	15	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	35		4.5							14	14	A-6a	10						
63	B 063-0 20	SS-1	0.0	1.5	-0.3	1.2	11	8	2.25	30	17	13	29	24	53	17	14	A-6a	5	140		N ₆₀ & Mc		12"	
		SS-2	1.5	3.0	1.2	2.7	8		2.25	43	21	22	38	47	85	23	18	A-7-6	13			N ₆₀ & Mc			
		SS-3	3.0	4.5	2.7	4.2	15		1.5							24	18	A-7-6	16						
		SS-4	4.5	6.0	4.2	5.7	18		1.75							28	18	A-7-6	16						

PID: 111404

County-Route-Section: SUM-77-24.12
No. of Borings: 63

Geotechnical Consultant: NEAS Inc.
Prepared By: KCA
Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options	
Global Geotextile Average(N60L):	12"
Average(HP):	0"
Global Geogrid Average(N60L):	0"
Average(HP):	0"

Design CBR	7
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% Samples within 6 feet of subgrade			
N₆₀ ≤ 5	2%	HP ≤ 0.5	0%
N₆₀ < 12	20%	0.5 < HP ≤ 1	0%
12 ≤ N₆₀ < 15	12%	1 < HP ≤ 2	7%
N₆₀ ≥ 20	40%	HP > 2	62%
M+	12%		
Rock	1%		
Unsuitable	4%		

Excavate and Replace at Surface	
Average	0"
Maximum	0"
Minimum	0"

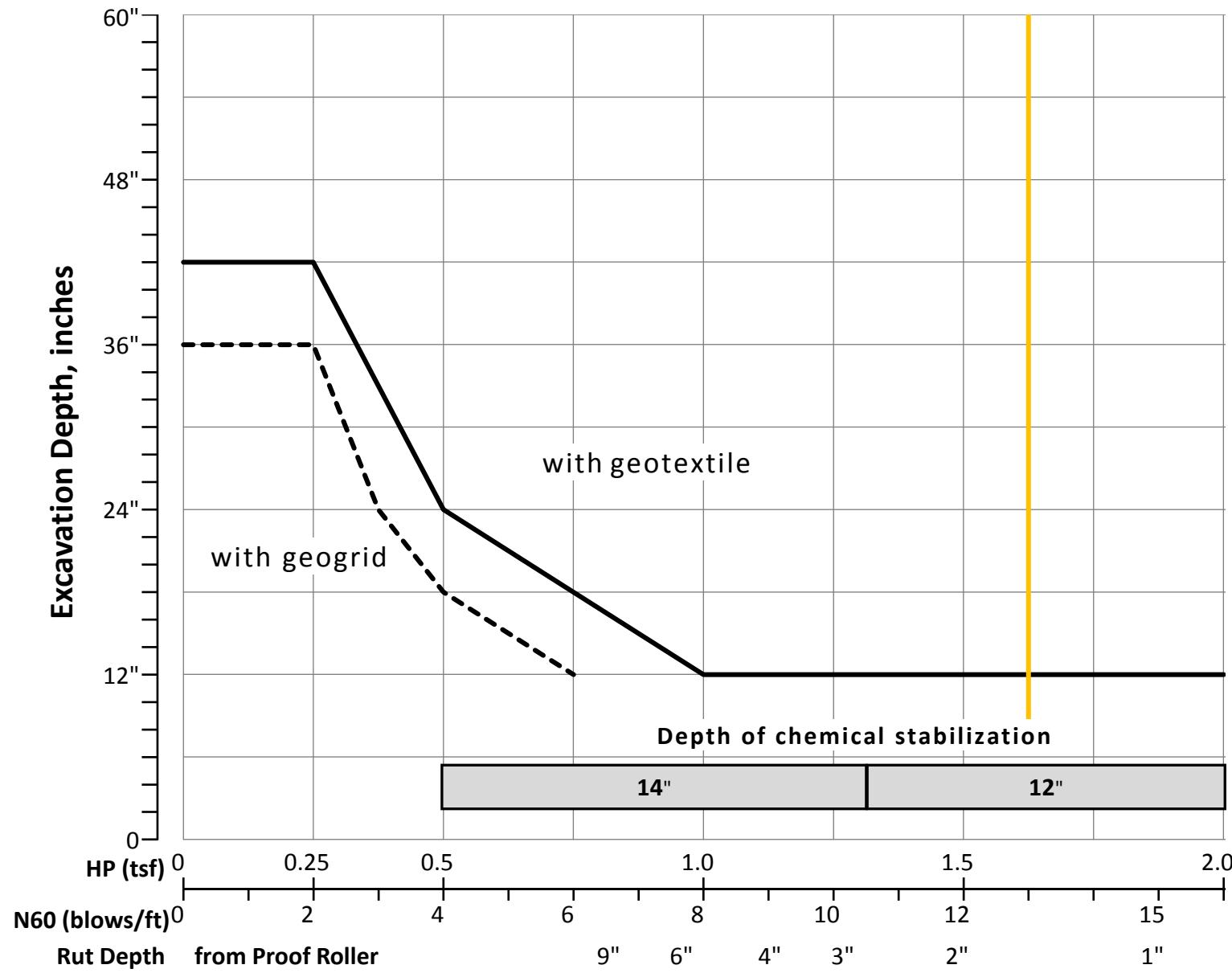
% Proposed Subgrade Surface	
Unstable & Unsuitable	34%
Unstable	30%
Unsuitable	4%

	N₆₀	N_{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M_c	M_{opt}	GI
Average	20	13	3.74	29	18	11	33	20	52	14	12	6
Maximum	82	30	4.50	43	35	22	85	47	98	28	30	16
Minimum	3	3	0.50	18	13	3	10	3	14	6	0	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	3	2	16	20	0	5	0	2	20	81	8	0	63	23	0	8	0	0	251
Percent	1%	1%	6%	8%	0%	2%	0%	1%	8%	32%	3%	0%	25%	9%	0%	3%	0%	0%	100%
% Rock Granular Cohesive	1%	58%										41%						100%	
Surface Class Count	1	2	12	14	0	3	0	1	10	47	6	0	37	13	0	5	0	0	151
Surface Class Percent	1%	1%	8%	9%	0%	2%	0%	1%	7%	31%	4%	0%	25%	9%	0%	3%	0%	0%	100%



GB1 Figure B – Subgrade Stabilization

OVERRIDE TABLE

Calculated Average	New Values	Check to Override
3.74		<input type="checkbox"/> HP
13.10		<input type="checkbox"/> N60L

Average HP

Average N_{60L}

RAMP A & B

OHIO DEPARTMENT OF TRANSPORTATION
OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES
Geotechnical Bulletin GB1

SUM-77-24.12

111404

Ramp A & B (Northbound Rest Area)

Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75

NEAS Inc.

Prepared By: KCA

Date prepared: Monday, January 11, 2021

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NO. OF BORINGS: **3**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-089-0-20	Ramp A	88+52	17	LT	CME 45B	82	1162.0	1160.5	1.5 C
2	B-090-0-20	Ramp B	7+13	9	LT	CME 45B	82	1159.2	1157.7	1.5 C
3	B-091-0-20	IR-77	803+00	92	RT	CME 45B	82	1159.8	1158.3	1.5 C



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
1	B 089-0 20	SS-1	1.5	3.0	0.0	1.5	22	22	4.5	32	17	15	29	27	56	11	14	A-6a	6	110						
		SS-2	3.0	4.5	1.5	3.0	26		4.5	33	20	13	36	34	70	14	15	A-6a	8							
		SS-3	4.5	6.0	3.0	4.5	29		4.5																	
		SS-4	6.0	7.5	4.5	6.0	33		4.5																	
2	B 090-0 20	SS-1	1.5	3.0	0.0	1.5	18	10	4.5	21	16	5	30	14	44	11	11	A-4a	2							
		SS-2	3.0	4.5	1.5	3.0	10		4.5											13	10	A-4a	8	170	N ₆₀ & Mc	
		SS-3	4.5	6.0	3.0	4.5	14		2.25	32	18	14	35	32	67	19	14	A-6a	8							
		SS-4	6.0	7.5	4.5	6.0	16		1											31	14	A-6a	10			
3	B 091-0 20	SS-1	1.5	3.0	0.0	1.5	12	10		NP	NP	NP	18	9	27	12	10	A-2-4	0	170						
		SS-2	3.0	4.5	1.5	3.0	14													17	10	A-2-4	0		N ₆₀ & Mc	
		SS-3	4.5	6.0	3.0	4.5	12		3.25	32	18	14	31	23	54	15	14	A-6a	5							
		SS-4	6.0	7.5	4.5	6.0	10		2											23	14	A-6a	10			

PID: 111404

County-Route-Section: SUM-77-24.12
No. of Borings: 3

Geotechnical Consultant: NEAS Inc.
Prepared By: KCA
Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options	
Global Geotextile Average(N60L):	12"
Average(HP):	0"
Global Geogrid Average(N60L):	0"
Average(HP):	0"

Design CBR	7
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% Samples within 6 feet of subgrade			
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%
N ₆₀ < 12	17%	0.5 < HP ≤ 1	8%
12 ≤ N ₆₀ < 15	33%	1 < HP ≤ 2	8%
N ₆₀ ≥ 20	33%	HP > 2	58%
M+	17%		
Rock	0%		
Unsuitable	0%		

Excavate and Replace at Surface	
Average	0"
Maximum	0"
Minimum	0"

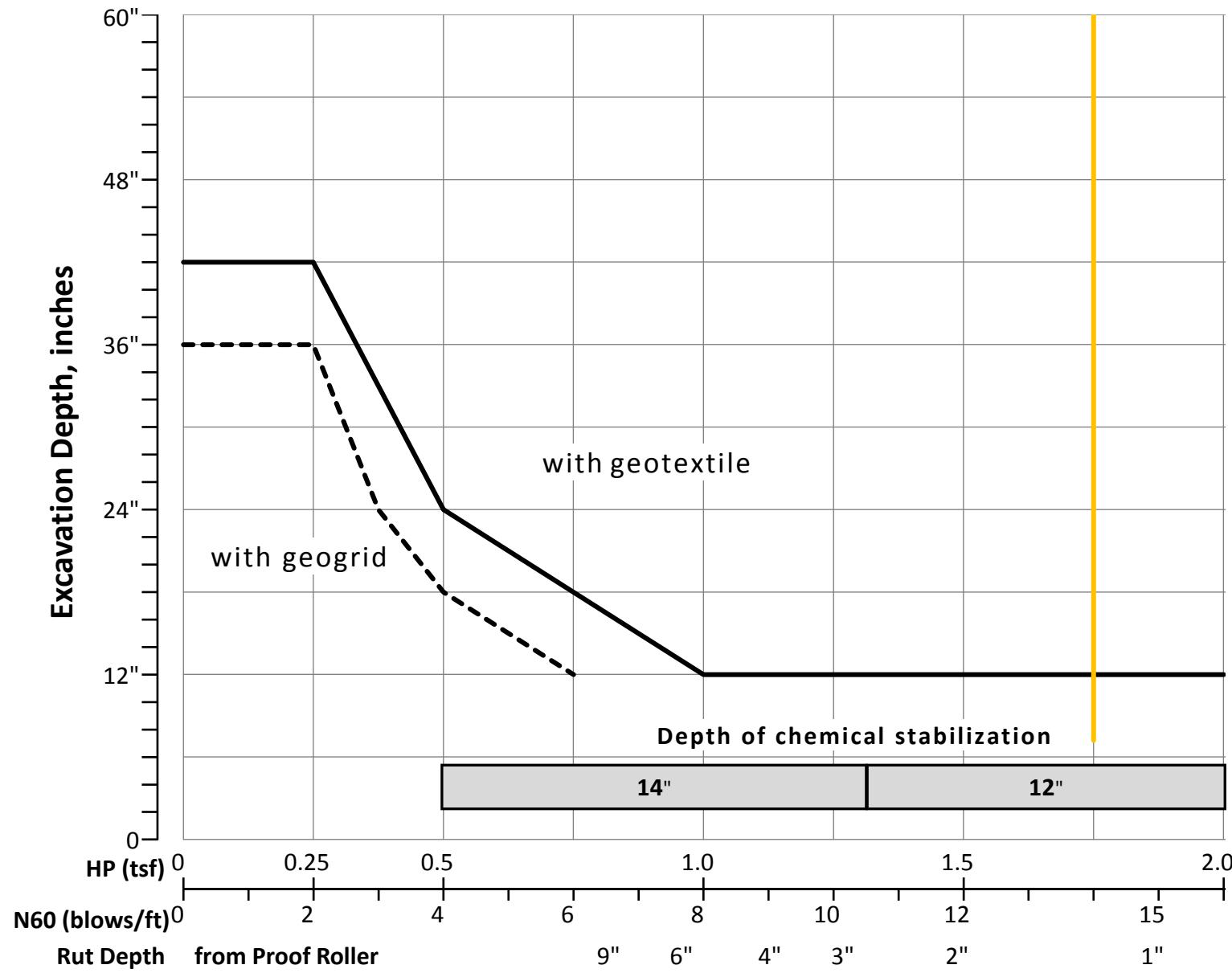
% Proposed Subgrade Surface	
Unstable & Unsuitable	40%
Unstable	40%
Unsuitable	0%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{opt}	GI
Average	18	14	3.44	30	18	12	30	23	53	16	13	6
Maximum	33	22	4.50	33	20	15	36	34	70	31	15	10
Minimum	10	10	1.00	21	16	5	18	9	27	11	10	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	0	2	0	0	0	0	0	2	0	0	7	0	0	0	0	11	
Percent	0%	0%	0%	18%	0%	0%	0%	0%	0%	18%	0%	0%	64%	0%	0%	0%	0%	100%	
% Rock Granular Cohesive	0%	36%										64%					100%		
Surface Class Count	0	0	0	2	0	0	0	0	0	2	0	0	1	0	0	0	0	5	
Surface Class Percent	0%	0%	0%	40%	0%	0%	0%	0%	0%	40%	0%	0%	20%	0%	0%	0%	0%	100%	



GB1 Figure B – Subgrade Stabilization

OVERRIDE TABLE

Calculated Average	New Values	Check to Override
3.44		<input type="checkbox"/> HP
14.00		<input type="checkbox"/> N60L

Average HP

Average N_{60L}

RAMP C & D

OHIO DEPARTMENT OF TRANSPORTATION**OFFICE OF GEOTECHNICAL ENGINEERING****PLAN SUBGRADES
Geotechnical Bulletin GB1****SUM-77-24.12****111404****Ramp C & D (Southbound Rest Area)****Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75****NEAS Inc.**

Prepared By: KCA

Date prepared: Monday, January 11, 2021

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NO. OF BORINGS:**5**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-084-0-20	IR-77	786+82	97	LT	CME 55X	82	1170.5	1169.0	1.5 C
2	B-085-0-20	Ramp D	23+06	14	RT	CME 55X	82	1160.1	1158.6	1.5 C
3	B-086-0-20	Ramp C	99+01	13	RT	CME 55X	82	1154.7	1153.2	1.5 C
4	B-087-0-20	Ramp C	103+04	16	RT	CME 55X	82	1158.4	1156.9	1.5 C
5	B-088-0-20	Ramp C	107+16	1	LT	CME 45B	82	1161.3	1159.8	1.5 C



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
			From	To	From	To																					
1	B 084-0 20	SS-1	1.5	3.0	0.0	1.5	19	10	3	32	18	14	36	33	69	17	14	A-6a	8	100		Mc					
		SS-2	3.0	4.5	1.5	3.0	10		3.75									16	14	A-6a	10		N ₆₀				
		SS-3	4.5	6.0	3.0	4.5	20		3.5	30	19	11	39	19	58	17	14	A-6a	5								
		SS-4	6.0	7.5	4.5	6.0	16		3							20	14	A-6a	10								
2	B 085-0 20	SS-1	1.5	3.0	0.0	1.5	18	10	3									12	14	A-6a	10	100					
		SS-2	3.0	4.5	1.5	3.0	10		4.5	28	16	12	36	26	62	14	14	A-6a	6			N ₆₀					
		SS-3	4.5	6.0	3.0	4.5	11		0.75	69	34	35	42	48	90	17		A-7-5	20								
		SS-4	6.0	7.5	4.5	6.0	10		2.5							23		A-7-5	16								
3	B 086-0 20	SS-1	1.5	3.0	0.0	1.5	23	5	3.75	23	14	9	24	12	36	11	10	A-4a	0								
		SS-2	3.0	4.5	1.5	3.0	8		1.5									13	10	A-4a	8	100	HP & Mc				
		SS-3	4.5	6.0	3.0	4.5	5		1	46	23	23	35	23	58	30	20	A-7-6	10								
		SS-4	6.0	7.5	4.5	6.0	7		0.75							33	18	A-7-6	16								
4	B 087-0 20	SS-1	1.5	3.0	0.0	1.5	11	11		NP	NP	NP	13	3	16	18	6	A-1-b	0	1200							
		SS-2	3.0	4.5	1.5	3.0	20		4.5	27	16	11	30	27	57	12	14	A-6a	5								
		SS-3	4.5	6.0	3.0	4.5	20		4.25									16	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	20		4.5							13	14	A-6a	10								
5	B 088-0 20	SS-1	1.5	3.0	0.0	1.5	15	8		NP	NP	NP	21	9	30	9	8	A-3a	0	100							
		SS-2	3.0	4.5	1.5	3.0	16			NP	NP	NP	14	6	20	7	8	A-3a	0								
		SS-3	4.5	6.0	3.0	4.5	8			20	13	7	24	11	35	13	10	A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	10									18	10	A-2-4	0								

PID: 111404

County-Route-Section: SUM-77-24.12
No. of Borings: 5

Geotechnical Consultant: NEAS Inc.
Prepared By: KCA
Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	No
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	14"

Excavate and Replace Stabilization Options		
Global Geotextile Average(N60L):	12"	0"
Global Geogrid Average(N60L):	0"	0"

Design CBR	7
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% Samples within 6 feet of subgrade			
N ₆₀ ≤ 5	5%	HP ≤ 0.5	0%
N ₆₀ < 12	50%	0.5 < HP ≤ 1	15%
12 ≤ N ₆₀ < 15	0%	1 < HP ≤ 2	5%
N ₆₀ ≥ 20	25%	HP > 2	55%
M+	10%		
Rock	0%		
Unsuitable	10%		

Excavate and Replace at Surface		
Average		0"
Maximum		0"
Minimum		0"

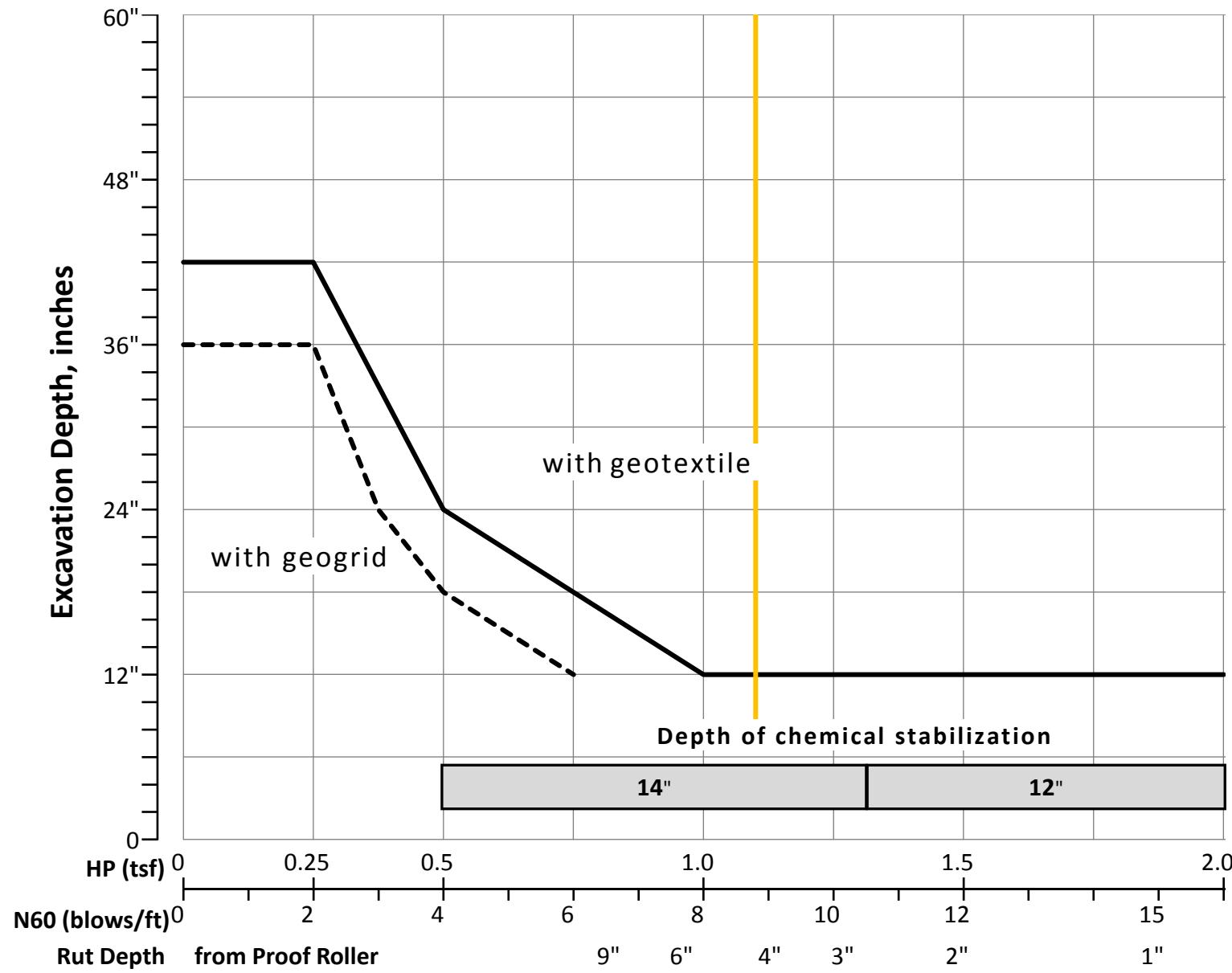
% Proposed Subgrade Surface		
Unstable & Unsuitable		40%
Unstable		40%
Unsuitable		0%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{opt}	GI
Average	14	9	2.95	34	19	15	29	20	48	16	13	7
Maximum	23	11	4.50	69	34	35	42	48	90	33	20	20
Minimum	5	5	0.75	20	13	7	13	3	16	7	6	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	1	2	0	0	0	0	2	2	0	0	9	0	2	2	0	0	20
Percent	0%	0%	5%	10%	0%	0%	0%	0%	10%	10%	0%	0%	45%	0%	10%	10%	0%	0%	100%
% Rock Granular Cohesive	0%																		100%
Surface Class Count	0	0	1	0	0	0	0	0	2	2	0	0	5	0	0	0	0	0	10
Surface Class Percent	0%	0%	10%	0%	0%	0%	0%	0%	20%	20%	0%	0%	50%	0%	0%	0%	0%	0%	100%



GB1 Figure B – Subgrade Stabilization



Calculated Average	New Values	Check to Override
2.95		<input type="checkbox"/> HP
8.80		<input type="checkbox"/> N60L

RAMP L

OHIO DEPARTMENT OF TRANSPORTATION
OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES
Geotechnical Bulletin GB1

SUM-77-24.12

111404

Ramp L

Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75

NEAS Inc.

Prepared By: KCA

Date prepared: Monday, January 11, 2021

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NO. OF BORINGS: **6**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-073-0-20	Ramp L	116+93	1	RT	CME 45B	82	1000.2	998.7	1.5 C
2	B-074-0-20	Ramp L	118+92	0	LT	CME 45B	82	998.0	996.5	1.5 C
3	B-075-0-20	Ramp L	120+95	15	RT	CME 45B	82	996.4	994.9	1.5 C
4	B-076-0-20	Ramp L	122+95	25	RT	CME 45B	82	998.8	997.8	1.0 C
5	B-077-0-20	Ramp L	124+91	12	RT	CME 45B	82	1003.3	1002.3	1.0 C
6	B-078-0-20	Ramp L	126+90	5	RT	CME 45B	82	1007.6	1006.6	1.0 C



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{OPT}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
1	B 073-0 20	SS-1	2.5	4.0	1.0	2.5	14	11	4.5	26	16	10	28	20	48	14	11	A-4a	3				N ₆₀ & M _c		12"	
		SS-2	5.0	6.5	3.5	5.0	11		2.5																	
2	B 074-0 20	SS-1	1.5	3.0	0.0	1.5	10	8										8	8	A-3a	0	130				
		SS-2	3.0	4.5	1.5	3.0	12		3	22	15	7	25	15	40	12	10	A-4a	1							
		SS-3	4.5	6.0	3.0	4.5	8		2.75	40	24	16	41	21	62	30	19	A-6b	8							
		SS-4	6.0	7.5	4.5	6.0	10		1									23	10	A-4a	8					
3	B 075-0 20	SS-1	1.5	3.0	0.0	1.5	16	15		26	17	9	32	14	46	25	12	A-4a	2	310			Mc			
		SS-2	5.0	6.5	3.5	5.0	15		2.75									17	10	A-2-6	4					
4	B 076-0 20	SS-1	1.5	3.0	0.5	2.0	15	11	4.5	20	16	4	28	10	38	10	11	A-4a	1	100						
		SS-2	3.0	4.5	2.0	3.5	12		NP	NP	NP		41	7	48	13	11	A-4a	3							
		SS-3	4.5	6.0	3.5	5.0	11											13	10	A-4a	8					
		SS-4	6.0	7.5	5.0	6.5	11											9	10	A-4a	8					
5	B 077-0 20	SS-1	2.5	4.0	1.5	3.0	15	15		25	18	7	20	9	29	11	10	A-2-4	0							
		SS-2A	5.0	5.8	4.0	4.8	18											14	10	A-2-4	0					
		SS-2B	5.8	6.5	4.8	5.5	18		3									20	14	A-6a	10					
6	B 078-0 20	SS-1	1.5	3.0	0.5	2.0	18	18	4.5	35	20	15	45	37	82	19	15	A-6a	10	100			Mc			
		SS-2	3.0	4.5	2.0	3.5	18		4.5	32	20	12	45	31	76	17	15	A-6a	9							
		SS-3	4.5	6.0	3.5	5.0	25		4.5									19	14	A-6a	10					
		SS-4	6.0	7.5	5.0	6.5	26		4.5									20	16	A-6b	16					

PID: 111404

County-Route-Section: SUM-77-24.12

No. of Borings: 6

Geotechnical Consultant: NEAS Inc.

Prepared By: KCA

Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options	
Global Geotextile Average(N60L):	12"
Average(HP):	0"
Global Geogrid Average(N60L):	0"
Average(HP):	0"

Design CBR	7
-------------------	---

% Samples within 6 feet of subgrade			
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%
N ₆₀ <12	32%	0.5 < HP ≤ 1	5%
12 ≤ N ₆₀ < 15	16%	1 < HP ≤ 2	0%
N ₆₀ ≥ 20	11%	HP > 2	58%
M+	16%		
Rock	0%		
Unsuitable	0%		

Excavate and Replace at Surface	
Average	0"
Maximum	0"
Minimum	0"

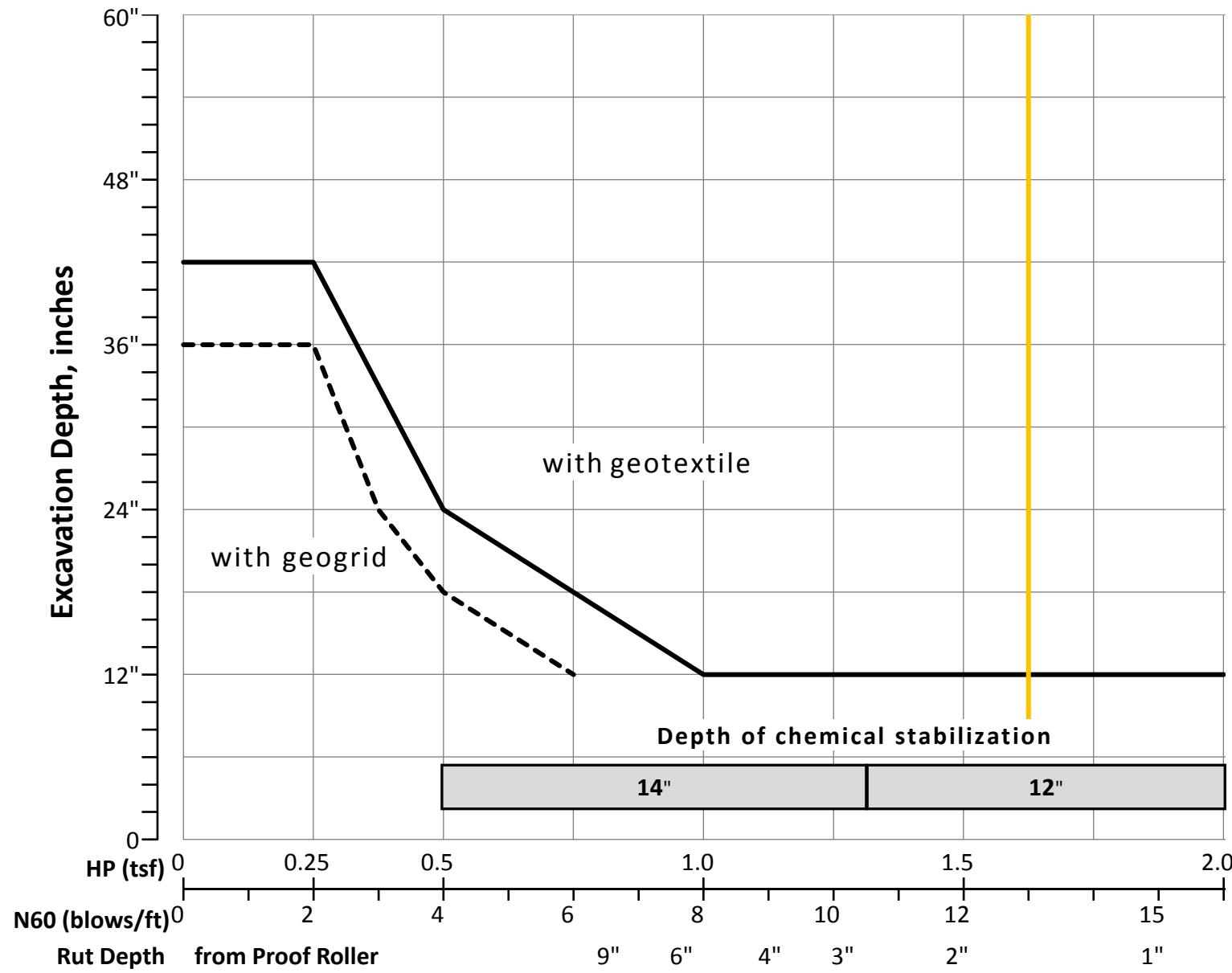
% Proposed Subgrade Surface	
Unstable & Unsuitable	33%
Unstable	33%
Unsuitable	0%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{opt}	GI
Average	15	13	3.50	28	18	10	34	18	52	17	12	6
Maximum	26	18	4.50	40	24	16	45	37	82	30	19	16
Minimum	8	8	1.00	20	15	4	20	7	29	8	8	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	0	2	0	1	0	0	1	9	0	0	4	2	0	0	0	0	19
Percent	0%	0%	0%	11%	0%	5%	0%	0%	5%	47%	0%	0%	21%	11%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%	68%										32%					100%		
Surface Class Count	0	0	0	1	0	0	0	0	1	5	0	0	2	0	0	0	0	0	9
Surface Class Percent	0%	0%	0%	11%	0%	0%	0%	0%	11%	56%	0%	0%	22%	0%	0%	0%	0%	0%	100%



GB1 Figure B – Subgrade Stabilization



Average HP
Average N_{60L}

RAMP M & N

OHIO DEPARTMENT OF TRANSPORTATION
OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES
Geotechnical Bulletin GB1

SUM-77-24.12

111404

Ramp M & N

Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75

NEAS Inc.

Prepared By: KCA

Date prepared: Monday, January 11, 2021

Brendan P. Andrews
2800 Corporate Exchange Drive
Suite 240
Columbus, OH 43231
(920) 427-0671
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NO. OF BORINGS: **5**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-079-0-20	Ghent Road	85+42	13	RT	CME 45B	82	999.3	997.8	1.5 C
2	B-080-0-20	Ramp M	127+44	73	RT	CME 45B	82	1002.8	1001.3	1.5 C
3	B-081-0-20	Ramp N	27+99	26	LT	CME 45B	82	1010.5	1009.0	1.5 C
4	B-082-0-20	Ramp N	31+00	35	RT	CME 45B	82	992.2	990.7	1.5 C
5	B-083-0-20	IR-77 NB	336+08	58	RT	CME 45B	82	975.5	974.0	1.5 C



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)		
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable			
1	B 079-0 20	SS-1	1.5	3.0	0.0	1.5	14	10	4.5	25	16	9	38	22	60	12	11	A-4a	5	310							
		SS-2	3.0	4.5	1.5	3.0	12		4	29	18	11	43	31	74	19	14	A-6a	8			N ₆₀ & M _c					
		SS-3	4.5	6.0	3.0	4.5	10		3									23	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	15		2.5									21	14	A-6a	10						
2	B 080-0 20	SS-1	1.5	3.0	0.0	1.5	14	14										3	8	A-3a	0	100					
		SS-2	3.0	4.5	1.5	3.0	20			NP	NP	NP	16	6	22	6	6	A-1-b	0								
		SS-3	4.5	6.0	3.0	4.5	19			NP	NP	NP	28	10	38	11	11	A-4a	1								
		SS-4	6.0	7.5	4.5	6.0	18											11	10	A-4a	8						
3	B 081-0 20	SS-1	1.5	3.0	0.0	1.5	16	16										10	8	A-3a	0	100					
		SS-2	3.0	4.5	1.5	3.0	16			NP	NP	NP	23	10	33	8	10	A-2-4	0								
		SS-3	4.5	6.0	3.0	4.5	18		4.5	35	20	15	49	38	87	19	15	A-6a	10								
		SS-4	6.0	7.5	4.5	6.0	19		4.5									21	14	A-6a	10						
4	B 082-0 20	SS-1	1.5	3.0	0.0	1.5	19	15		NP	NP	NP	10	3	13	5	6	A-1-b	0	130							
		SS-2	3.0	4.5	1.5	3.0	15			NP	NP	NP	7	2	9	6	6	A-1-b	0								
		SS-3	4.5	6.0	3.0	4.5	20											6	6	A-1-b	0						
		SS-4	6.0	7.5	4.5	6.0	19											8	6	A-1-b	0						
5	B 083-0 20	SS-1	1.5	3.0	0.0	1.5	26	18																			
		SS-2	3.0	4.5	1.5	3.0	18			NP	NP	NP	28	8	36	11	11	A-4a	0								
		SS-3	4.5	6.0	3.0	4.5	20		4.5	23	16	7	24	11	35	10	10	A-2-4	0								
		SS-4	6.0	7.5	4.5	6.0	25		4.25									14	10	A-2-4	0						

PID: 111404

County-Route-Section: SUM-77-24.12
No. of Borings: 5

Geotechnical Consultant: NEAS Inc.
Prepared By: KCA
Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options	
Global Geotextile Average(N60L):	12"
Average(HP):	0"

Global Geogrid Average(N60L):	0"
Average(HP):	0"

Design CBR	9
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% Samples within 6 feet of subgrade			
N ₆₀ ≤ 5	0%	HP ≤ 0.5	0%
N ₆₀ < 12	5%	0.5 < HP ≤ 1	0%
12 ≤ N ₆₀ < 15	15%	1 < HP ≤ 2	0%
N ₆₀ ≥ 20	25%	HP > 2	40%
M+	5%		
Rock	0%		
Unsuitable	0%		

Excavate and Replace at Surface	
Average	0"
Maximum	0"
Minimum	0"

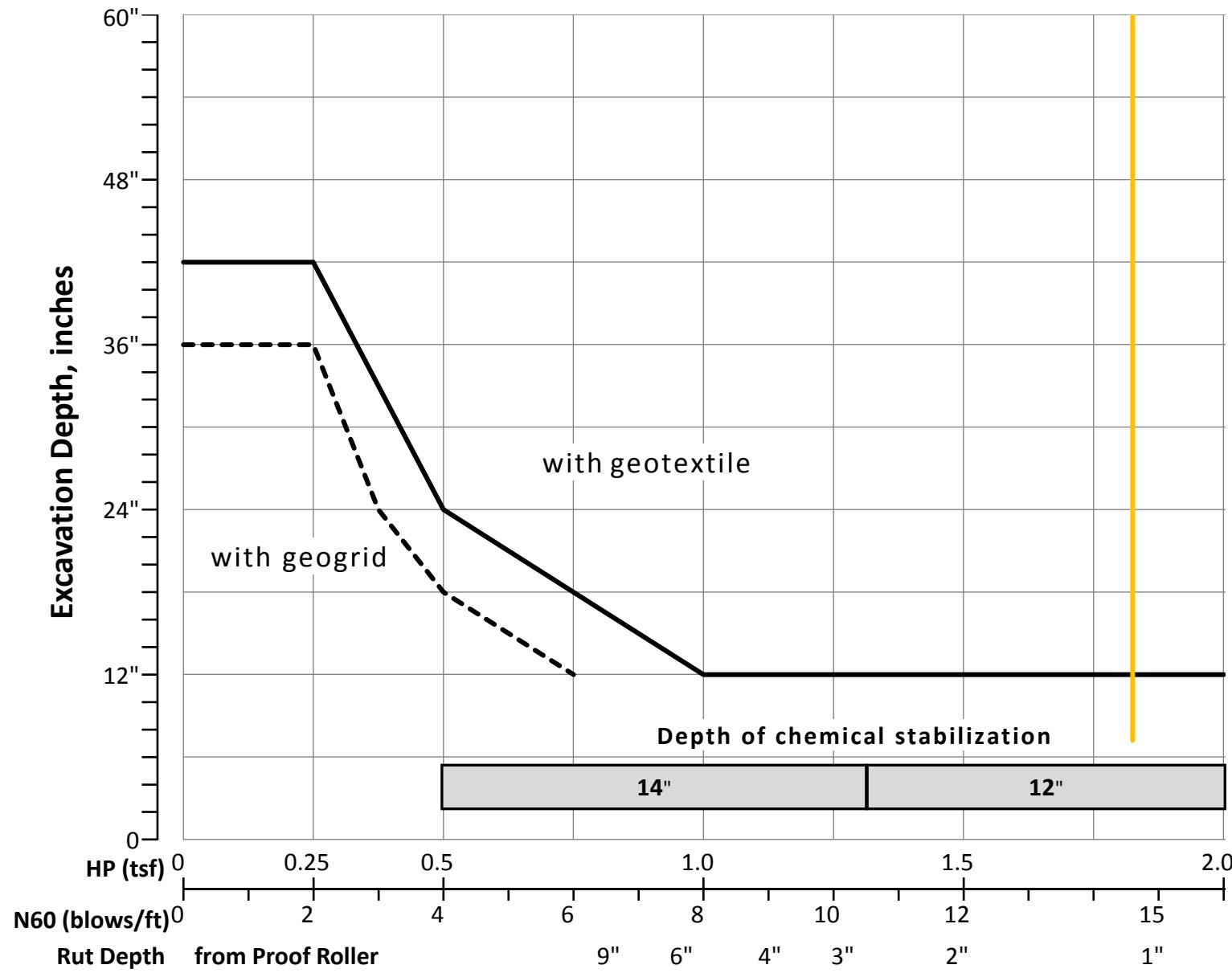
% Proposed Subgrade Surface	
Unstable & Unsuitable	11%
Unstable	11%
Unsuitable	0%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{opt}	GI
Average	18	15	3.97	28	18	11	27	14	41	12	10	3
Maximum	26	18	4.50	35	20	15	49	38	87	23	15	10
Minimum	10	10	2.50	23	16	7	7	2	9	3	6	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	5	3	0	0	0	0	2	4	0	0	5	0	0	0	0	19	
Percent	0%	0%	26%	16%	0%	0%	0%	0%	11%	21%	0%	0%	26%	0%	0%	0%	0%	100%	
% Rock Granular Cohesive	0%																	100%	
Surface Class Count	0	0	3	1	0	0	0	0	2	2	0	0	1	0	0	0	0	9	
Surface Class Percent	0%	0%	33%	11%	0%	0%	0%	0%	22%	22%	0%	0%	11%	0%	0%	0%	0%	100%	



GB1 Figure B – Subgrade Stabilization

OVERRIDE TABLE

Calculated Average	New Values	Check to Override
3.97		<input type="checkbox"/> HP
14.60		<input type="checkbox"/> N60L

Average HP
Average N_{60L}

RAMP P & R

OHIO DEPARTMENT OF TRANSPORTATION
OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES
Geotechnical Bulletin GB1

SUM-77-24.12

111404

Ramp P & R

Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75

NEAS Inc.

Prepared By: KCA

Date prepared: Monday, January 11, 2021

Brendan P. Andrews
2800 Corporate Exchange Drive
Suite 240
Columbus, OH 43231
(920) 427-0671
brendan.andrews@neasinc.com

NO. OF BORINGS: **5**

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-068-0-20	Ramp P	225+67	7	LT	CME 55X	82	997.0	995.5	1.5 C
2	B-069-0-20	Ramp P	221+81	15	RT	CME 55X	82	1007.8	1006.3	1.5 C
3	B-070-0-20	Ramp P	218+57	15	RT	CME 55X	82	1009.4	1007.9	1.5 C
4	B-071-0-20	Ramp P	214+18	17	RT	CME 55X	82	1003.7	1002.2	1.5 C
5	B-072-0-20	Ramp R	17+63	9	LT	CME 55X	82	1006.1	1004.6	1.5 C



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)	
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable		
			From	To	From	To																				
1	B 068-0 20	SS-1	1.5	3.0	0.0	1.5	34	22	22							9	8	A-3a	0	830						
		SS-2	3.0	4.5	1.5	3.0	27			NP	NP	NP	22	4	26	7	8	A-3a	0							
		SS-3	4.5	6.0	3.0	4.5	23									7	8	A-3a	0							
		SS-4	6.0	7.5	4.5	6.0	22									8	8	A-3a	0							
2	B 069-0 20	SS-1	1.5	3.0	0.0	1.5	16	12	12							11	10	A-2-4	0	100						
		SS-2	3.0	4.5	1.5	3.0	25			21	16	5	22	7	29	11	10	A-2-4	0							
		SS-3	4.5	6.0	3.0	4.5	12									10	10	A-2-4	0							
		SS-4	6.0	7.5	4.5	6.0	12									14	10	A-2-4	0							
3	B 070-0 20	SS-1	1.5	3.0	0.0	1.5	22	7	7	4.5	25	17	8	31	14	45	13	12	A-4a	2	100					
		SS-2	3.0	4.5	1.5	3.0	14			2.5	30	19	11	50	22	72	18	14	A-6a	8					N ₆₀ & Mc	
		SS-3	4.5	6.0	3.0	4.5	10			2.5							17	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	7									17	10	A-2-4	0							
4	B 071-0 20	SS-1	1.5	3.0	0.0	1.5	8	7	7	2.5						17	10	A-4a	8	100					N ₆₀ & Mc	12"
		SS-2	3.0	4.5	1.5	3.0	7			0.25	26	18	8	34	16	50	18	13	A-4a	3					HP & Mc	
		SS-3	4.5	6.0	3.0	4.5	10									14	10	A-2-6	4							
		SS-4	6.0	7.5	4.5	6.0	7									15	10	A-2-6	4							
5	B 072-0 20	SS-1	1.5	3.0	0.0	1.5	61	15	15		NP	NP	NP	15	4	19	11	6	A-1-b	0	280					
		SS-2	3.0	4.5	1.5	3.0	15									18	6	A-1-b	0							
		SS-3	4.5	6.0	3.0	4.5	26			4.5	23	14	9	29	17	46	12	10	A-4a	2						
		SS-4	6.0	7.5	4.5	6.0	19			4.5						10	10	A-4a	8							

PID: 111404

County-Route-Section: SUM-77-24.12

No. of Borings: 5

Geotechnical Consultant: NEAS Inc.

Prepared By: KCA

Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	Option
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options	
Global Geotextile Average(N60L):	12" 0"
Global Geogrid Average(N60L):	0" 0"

Design CBR	10
-------------------	-----------

% Samples within 6 feet of subgrade			
N ₆₀ ≤ 5	0%	HP ≤ 0.5	5%
N ₆₀ < 12	30%	0.5 < HP ≤ 1	0%
12 ≤ N ₆₀ < 15	15%	1 < HP ≤ 2	0%
N ₆₀ ≥ 20	40%	HP > 2	30%
M+	15%		
Rock	0%		
Unsuitable	0%		

Excavate and Replace at Surface	
Average	0"
Maximum	0"
Minimum	0"

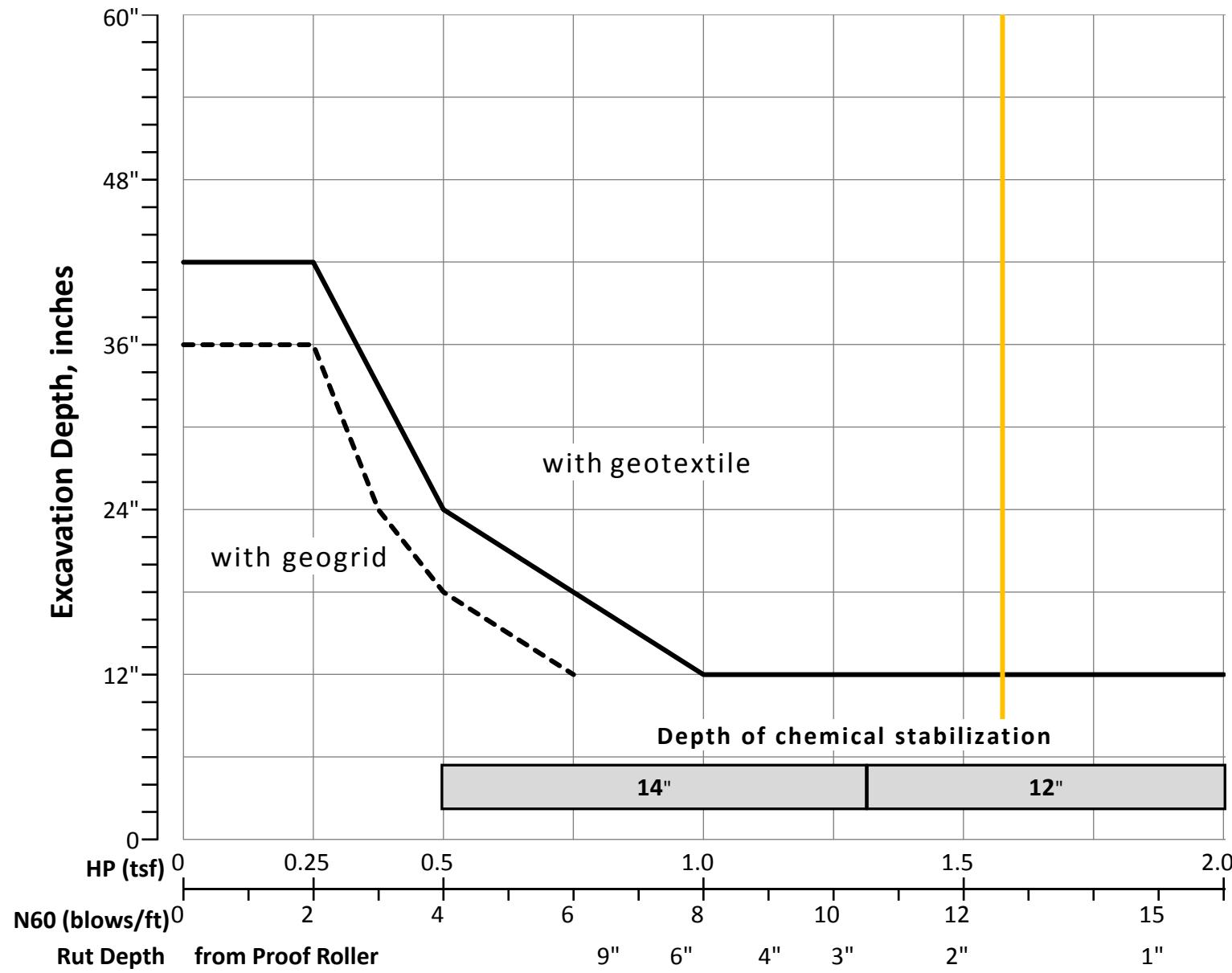
% Proposed Subgrade Surface	
Unstable & Unsuitable	30%
Unstable	30%
Unsuitable	0%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{opt}	GI
Average	19	13	3.04	25	17	8	29	12	41	13	10	2
Maximum	61	22	4.50	30	19	11	50	22	72	18	14	10
Minimum	7	7	0.25	21	14	5	15	4	19	7	6	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	0	2	5	0	2	0	0	4	5	0	0	2	0	0	0	0	20	
Percent	0%	0%	10%	25%	0%	10%	0%	0%	20%	25%	0%	0%	10%	0%	0%	0%	0%	100%	
% Rock Granular Cohesive	0%	90%										10%						100%	
Surface Class Count	0	0	2	2	0	0	0	0	2	3	0	0	1	0	0	0	0	10	
Surface Class Percent	0%	0%	20%	20%	0%	0%	0%	0%	20%	30%	0%	0%	10%	0%	0%	0%	0%	100%	



GB1 Figure B – Subgrade Stabilization

OVERRIDE TABLE

Calculated Average	New Values	Check to Override
3.04		<input type="checkbox"/> HP
12.60		<input type="checkbox"/> N _{60L}

Average HP
Average N_{60L}

RAMP S

OHIO DEPARTMENT OF TRANSPORTATION
OFFICE OF GEOTECHNICAL ENGINEERING

PLAN SUBGRADES
Geotechnical Bulletin GB1

SUM-77-24.12

111404

Ramp S

Widening of IR-77 NB & SB and associated ramps from SLM 24.02 to SLM 28.75

NEAS Inc.

Prepared By: KCA

Date prepared: Monday, January 11, 2021

Brendan P. Andrews
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NO. OF BORINGS:

4

#	Boring ID	Alignment	Station	Offset	Dir	Drill Rig	ER	Boring EL.	Proposed Subgrade EL	Cut Fill
1	B-064-0-20	IR-77 SB	409+38	50	LT	CME 55X	82	1015.5	1014.0	1.5 C
2	B-065-0-20	Ramp S	14+70	17	LT	CME 55X	82	1016.2	1014.7	1.5 C
3	B-066-0-20	Ramp S	18+82	9	LT	CME 55X	82	1013.4	1011.9	1.5 C
4	B-067-0-20	Ramp S	22+92	4	LT	CME 55X	82	1009.5	1008.0	1.5 C



#	Boring	Sample	Sample Depth		Subgrade Depth		Standard Penetration		HP (tsf)	Physical Characteristics						Moisture		Ohio DOT		Sulfate Content (ppm)	Problem		Excavate and Replace (Item 204)		Recommendation (Enter depth in inches)
			From	To	From	To	N ₆₀	N _{60L}		LL	PL	PI	% Silt	% Clay	P200	M _c	M _{opt}	Class	GI		Unsuitable	Unstable	Unsuitable	Unstable	
1	B 064-0 20	SS-1	1.5	3.0	0.0	1.5	15	15	4.5	26	16	10	37	22	59	15	11	A-4a	5	100		Mc			
		SS-2	3.0	4.5	1.5	3.0	23		4.5	24	16	8	34	19	53	14	11	A-4a	4		Mc				
		SS-3	4.5	6.0	3.0	4.5	23									17	10	A-2-4	0						
		SS-4	6.0	7.5	4.5	6.0	40									13	10	A-2-4	0						
2	B 065-0 20	SS-1	1.5	3.0	0.0	1.5	14	14	4.5	27	19	8	44	22	66	16	14	A-4a	6	100					
		SS-2	3.0	4.5	1.5	3.0	15		4.5	22	16	6	33	13	46	12	11	A-4a	2						
		SS-3	4.5	6.0	3.0	4.5	16		4.5							16	10	A-4a	8						
		SS-4	6.0	7.5	4.5	6.0	34									11	6	A-1-a	0						
3	B 066-0 20	SS-1	1.5	3.0	0.0	1.5	20	12	4.25	25	15	10	31	14	45	15	10	A-4a	2	100		Mc			
		SS-2	3.0	4.5	1.5	3.0	12		2.5	29	18	11	41	19	60	19	14	A-6a	5			N ₆₀ & Mc			
		SS-3	4.5	6.0	3.0	4.5	16		4.25							16	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	12									15	8	A-3a	0						
4	B 067-0 20	SS-1	1.5	3.0	0.0	1.5	14	5	3.25	24	14	10	20	10	30	14	10	A-2-4	0	100		N ₆₀ & Mc		12"	
		SS-2	3.0	4.5	1.5	3.0	5		3.5	24	16	8	21	12	33	13	10	A-2-4	0			N ₆₀ & Mc			
		SS-3	4.5	6.0	3.0	4.5	11		2.25							16	14	A-6a	10						
		SS-4	6.0	7.5	4.5	6.0	16		1.75							19	16	A-6b	16						

PID: 111404

County-Route-Section: SUM-77-24.12

No. of Borings: 4

Geotechnical Consultant: NEAS Inc.

Prepared By: KCA

Date prepared: 1/11/2021

Chemical Stabilization Options		
320	Rubblize & Roll	No
206	Cement Stabilization	Option
	Lime Stabilization	No
206	Depth	12"

Excavate and Replace Stabilization Options		
Global Geotextile Average(N60L):	12"	0"
Global Geogrid Average(N60L):	0"	0"

Design CBR	8
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% Samples within 6 feet of subgrade			
N ₆₀ ≤ 5	6%	HP ≤ 0.5	0%
N ₆₀ < 12	13%	0.5 < HP ≤ 1	0%
12 ≤ N ₆₀ < 15	25%	1 < HP ≤ 2	6%
N ₆₀ ≥ 20	31%	HP > 2	69%
M+	38%		
Rock	0%		
Unsuitable	0%		

Excavate and Replace at Surface		
Average		0"
Maximum		0"
Minimum		0"

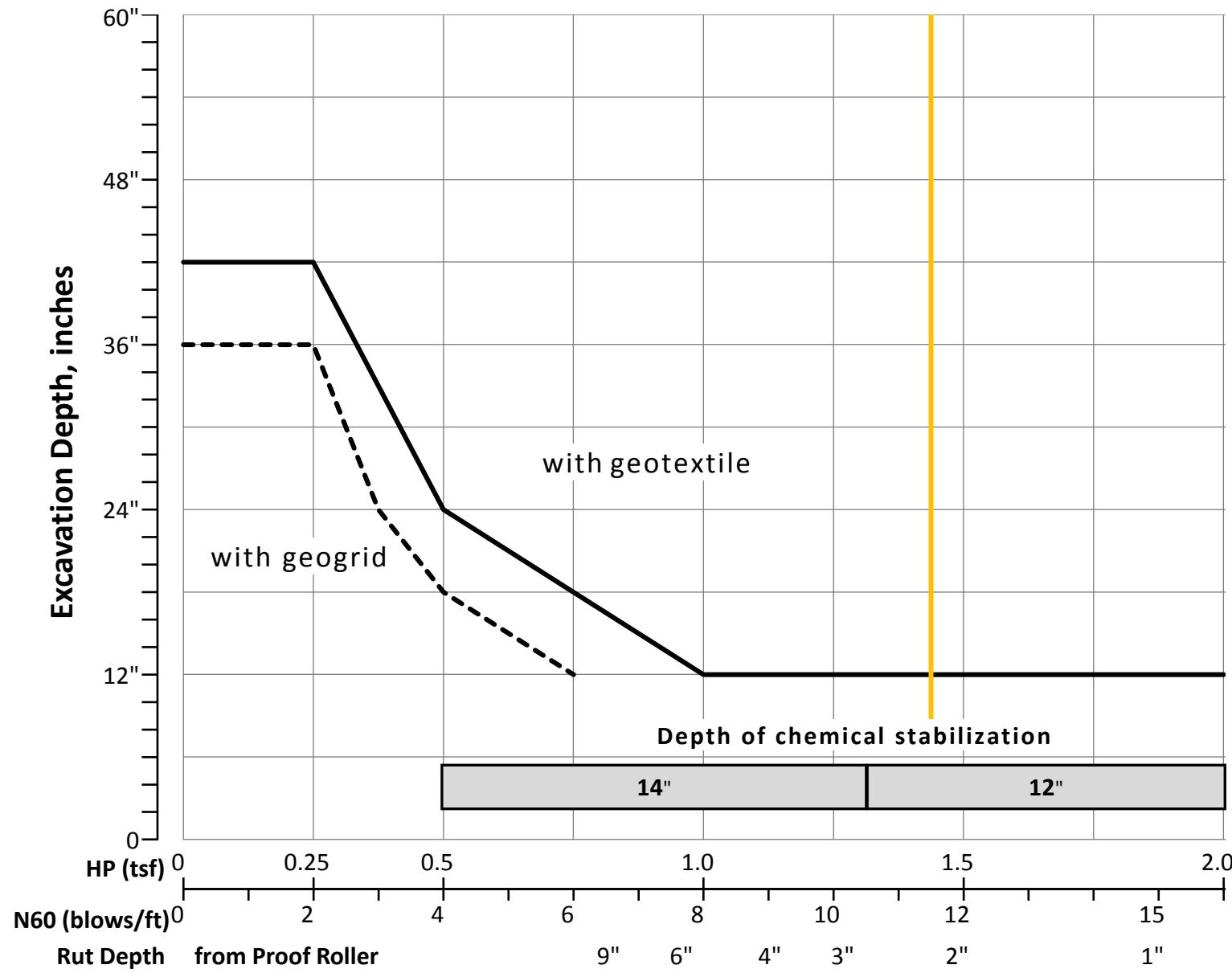
% Proposed Subgrade Surface	
Unstable & Unsuitable	75%
Unstable	75%
Unsuitable	0%

	N ₆₀	N _{60L}	HP	LL	PL	PI	Silt	Clay	P 200	M _c	M _{opt}	GI
Average	18	12	3.69	25	16	9	33	16	49	15	11	4
Maximum	40	15	4.50	29	19	11	44	22	66	19	16	16
Minimum	5	5	1.75	22	14	6	20	10	30	11	6	0

Classification Counts by Sample																			
ODOT Class	Rock	A-1-a	A-1-b	A-2-4	A-2-5	A-2-6	A-2-7	A-3	A-3a	A-4a	A-4b	A-5	A-6a	A-6b	A-7-5	A-7-6	A-8a	A-8b	Totals
Count	0	1	0	4	0	0	0	0	1	6	0	0	3	1	0	0	0	0	16
Percent	0%	6%	0%	25%	0%	0%	0%	0%	6%	38%	0%	0%	19%	6%	0%	0%	0%	0%	100%
% Rock Granular Cohesive	0%																		100%
Surface Class Count	0	0	0	2	0	0	0	0	0	5	0	0	1	0	0	0	0	0	8
Surface Class Percent	0%	0%	0%	25%	0%	0%	0%	0%	0%	63%	0%	0%	13%	0%	0%	0%	0%	0%	100%



GB1 Figure B – Subgrade Stabilization



Average HP
Average N_{60L}

APPENDIX G

N1₆₀ VALUES AND SOIL TYPE

Noise Wall
SUM-77-24.12 Ghent
PID: 111404

Depth of SPT (ft)	Correction Factor	B-007-0-20		B-073-0-20		B-074-0-20		B-075-0-20		B-076-0-20		B-077-0-20	
		N ₆₀	N _{1,60}	Cohesive or Granular		N ₆₀	N _{1,60}	Cohesive or Granular	N ₆₀	N _{1,60}	Cohesive or Granular	N ₆₀	N _{1,60}
3	1.56	18	-	Cohesive				10	16	Granular	16	-	Cohesive
4	1.48				14	-	Cohesive						
4.5	1.44	16	-	Cohesive				12	-	Cohesive			12
6	1.32	20	-	Cohesive				8	-	Cohesive			11
6.5	1.28				11	-	Cohesive				15	19	Granular
7.5	1.2	22	-	Cohesive				10	-	Cohesive			11
9	1.14				12	-	Cohesive	14	-	Cohesive	8	9	Granular
11.5	1.1	15	-	Cohesive	8	-	Cohesive	11	-	Cohesive	10	11	Granular
14	1.04	15	-	Cohesive	10	-	Cohesive	10	10	Granular	19	20	Granular
16.5	0.976	8	-	Cohesive	14	14	Granular	8	8	Granular	26	25	Granular
19	0.93	7	6	Granular	14	13	Granular	10	9	Granular	16	15	Granular
21.5	0.892	27	24	Granular	10	9	Granular	18	16	Granular	19	17	Granular
24	0.856	26	22	Granular	14	12	Granular	10	9	Granular	23	20	Granular
26.5	0.816	29	24	Granular	14	11	Granular	11	9	Granular	27	22	Granular
											11	9	Granular
											25	20	Granular

Depth of SPT (ft)	Correction Factor	B-078-0-20		Cohesive or Granular	
		N ₆₀	N _{1,60}		
3	1.56	18	-	Cohesive	
4	1.48				
4.5	1.44	18	-	Cohesive	
6	1.32	25	-	Cohesive	
6.5	1.28				
7.5	1.2	26	-	Cohesive	
9	1.14	25	-	Cohesive	
11.5	1.1	25	-	Cohesive	
14	1.04	27	-	Cohesive	
16.5	0.976	14	14	Granular	
19	0.93	19	18	Granular	
21.5	0.892	15	13	Granular	
24	0.856	20	17	Granular	
26.5	0.816	18	15	Granular	

APPENDIX H

DESIGN $N1_{60}$ VALUES BASED ON DRILLED SHAFT LENGTH

Noise Wall
SUM-77-24.12 Ghent
PID: 111404

Depth of Shaft (ft)	B-007-0-20		B-073-0-20		B-074-0-20		B-075-0-20		B-076-0-20		B-077-0-20		B-078-0-20	
	Design N1 ₆₀	Cohesive or Granular												
6	16	Cohesive	11	Cohesive	8	Cohesive	16	Granular	15	Granular	18	Granular	20 Avg.	Cohesive
8	16	Cohesive	11	Cohesive	8	Cohesive	9	Granular	13	Granular	18	Granular	22 Avg.	Cohesive
10	16	Cohesive	11	Cohesive	8	Cohesive	9	Granular	13	Granular	18	Granular	22 Avg.	Cohesive
12	15	Cohesive	8	Cohesive	8	Granular	9	Granular	13	Granular	18	Cohesive	23 Avg.	Cohesive
14	15	Cohesive	8	Cohesive	8	Granular	9	Granular	13	Granular	18	Granular	23 Avg.	Cohesive
16	8	Cohesive	8	Granular	8	Granular	9	Granular	10	Granular	18	Granular	14	Cohesive
18	6	Granular	8	Granular	8	Granular	9	Granular	10	Granular	13	Granular	14	Granular
20	6	Granular	8	Granular	8	Granular	9	Granular	7	Granular	13	Granular	13	Granular
22	6	Granular	8	Granular	8	Granular	9	Granular	7	Granular	13	Granular	13	Granular
24	6	Granular	8	Granular	8	Granular	9	Granular	7	Granular	13	Granular	13	Granular