

	PIER MAIN SPA	OFFSETS N-NORTHI			
PIER NO.	STATION	OFFSET 'A'	ROTATION	OFFSET 'B'	
****26NB	233+62.50	35.50	0	0.142 / 0.189	
27 NB	235+/2.50	35.48	0	0./89	ſ
27 A-NB	236+62.50	35.48	0	0./89	ſ
27 B-NB	238+12.50	35.48	0	0./89	
27 C - NB	239+62.50	35.48	0	0./89	ſ
28 (PYLON)	241+25.00	0.00	0	0.189	
29NB	247+37.50	35.48	0	0./89	
***30NB	248+87.50	35.50	0	0.189 / 0.142	-
** CTATION	NEESETS 9. D	OTATION TA	KEN EDOM		line

ABUTMENT	DRILLED	COMPRESS.	
OR PIER	SHAFT	LOAD	
NUMBER	DIAMETER	(TONS)	
26SB	8′-0″	359	
27 SB	8′-0″	3037	
27 A-SB	8′-0″	2597	
27 B-SB	8′-0″	2603	
27C-SB	8'-0"	2607	
28SB & NB	8'-0"	57 37	
29SB	8′-0″	3249	
30SB	8'-0"	3643	
26NB	8'-0"	3589	
27 NB	8'-0"	3/83	
27 A-NB	8′-0″	2597	
27 B-NB	8'-0"	2603	
27 C - NB	8'-0"	2607	
SEE SOU	THBOUND F	OR PIER 2	8
29NB	8′-0″	3249	
30NB	8'-0"	3625	

NOTES:

- SHALL BE REMOVED TO AT LEAST 3'-O" BELOW MUDLINE.
- 6. FOR TEMP. PIERS TOP OF SHAFT ELEVATION: 577.0 (IGDL85).
- AND DRILLED SHAFT COLLARS.

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DRILLED SHAFT SCHEDULE - SOUTHBOUND MAINSPAN

					INSTALLAT	ION CRITER						
•	UPLIFT LOAD (TONS)	TOP OF SHAFT ELEV.*	ESTIMATED TIP ELEVATION (ft)	TIP	ROCK	MINIMUM ROCK SOCKET LENGTH (ft)	ESTIMATED DRILLED SHAFT LENGTH (ft)	MINIMUM DRILLED SHAFT LENGTH (ft)	FACTORED DESIGN LOAD (tons)	DOWNDRAG (tons)	MAXIMUM SCOUR DEPTH (ft)	DRILLED SHAFT TYPE
	0	569.25	493	493	N/A	N/A	76′-3″	76′-3″	6032	0	N/A	Ι
	0	563.25	502	502	N/A	N/A	61′-3″	61'-3"	6032	0	N/A	Ι
	0	577	483	483	15	15	94′-0″	94'-0"	6032	0	8.2	VI
	0	577	482	482	/5	15	95′-0″	95′-0″	6032	0	8.9	VI
	0	577	483	483	15	15	94'-0″	94'-0"	6032	0	10.7	V I
	152	521.352	482	482	15	15	39' -4'/4"	39' -41/4"	6 88	0	32.0	VI
	0	573.25	496.5	496.5	N/A	N/A	76′-9″	76′-9″	6032	0	N/A	Ι
	0	577.75	491	491	N/A	N/A	86′-9″	86′-9″	6032	0	N/A	Ι

DRILLED SHAFT SCHEDULE - NORTHBOUND MAINSPAN

0	568.75	493	493	N/A	N/A	75'-9"	75′-9″	6032	0	N/A	Ι
0	565.25	502	502	N/A	N/A	63' - 3"	63' -3"	6032	0	N/A	Ι
0	577	483	483	/5	/5	94'-0"	94'-0"	6032	0	8.2	V I
0	577	482	482	15	/5	95′-0″	95′-0″	6032	0	8.9	V I
0	577	483	483	15	15	94'-0"	94′-0″	6032	0	10.7	V I
3											
0	573.25	496.5	496.5	N/A	N/A	76′-9″	76′-9″	6032	0	N/A	Ι
0	574.25	491	491	N/A	N/A	83'-3"	83'-3"	6032	0	N/A	Ι

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I. SEE FOUNDATION LAYOUT SHEETS FOR LOCATION AND NUMBER OF DRILLED SHAFTS.

2. FOR DRILLED SHAFT DETAILS SEE SHEETS B-823 & B-824.

3. FOR DRILLED SHAFT COLLAR DETAILS SEE SHEETS B-825 & B-826.

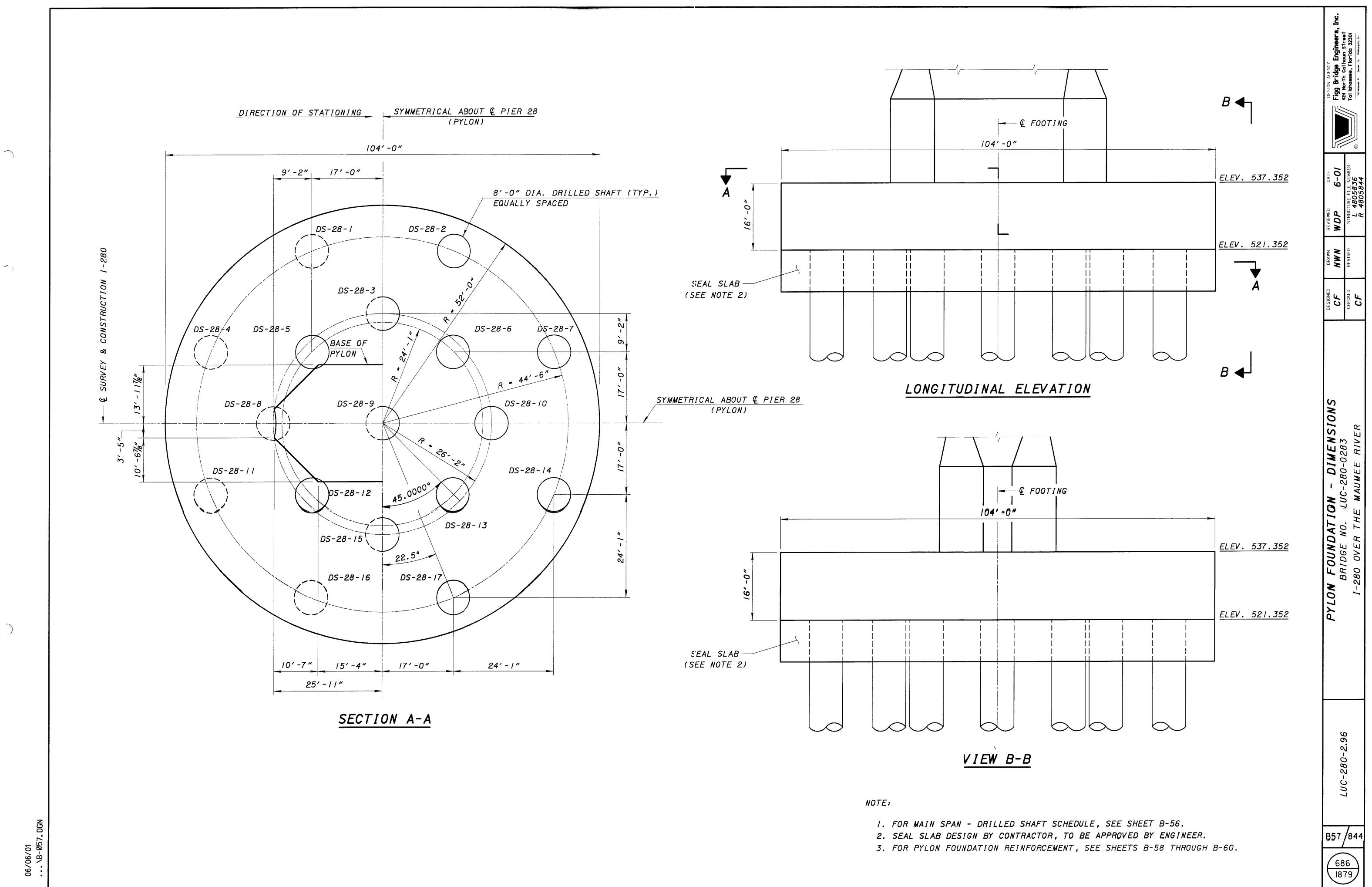
4. FOR PYLON FOUNDATION DETAILS SEE SHEETS B-57 THRU B-60.

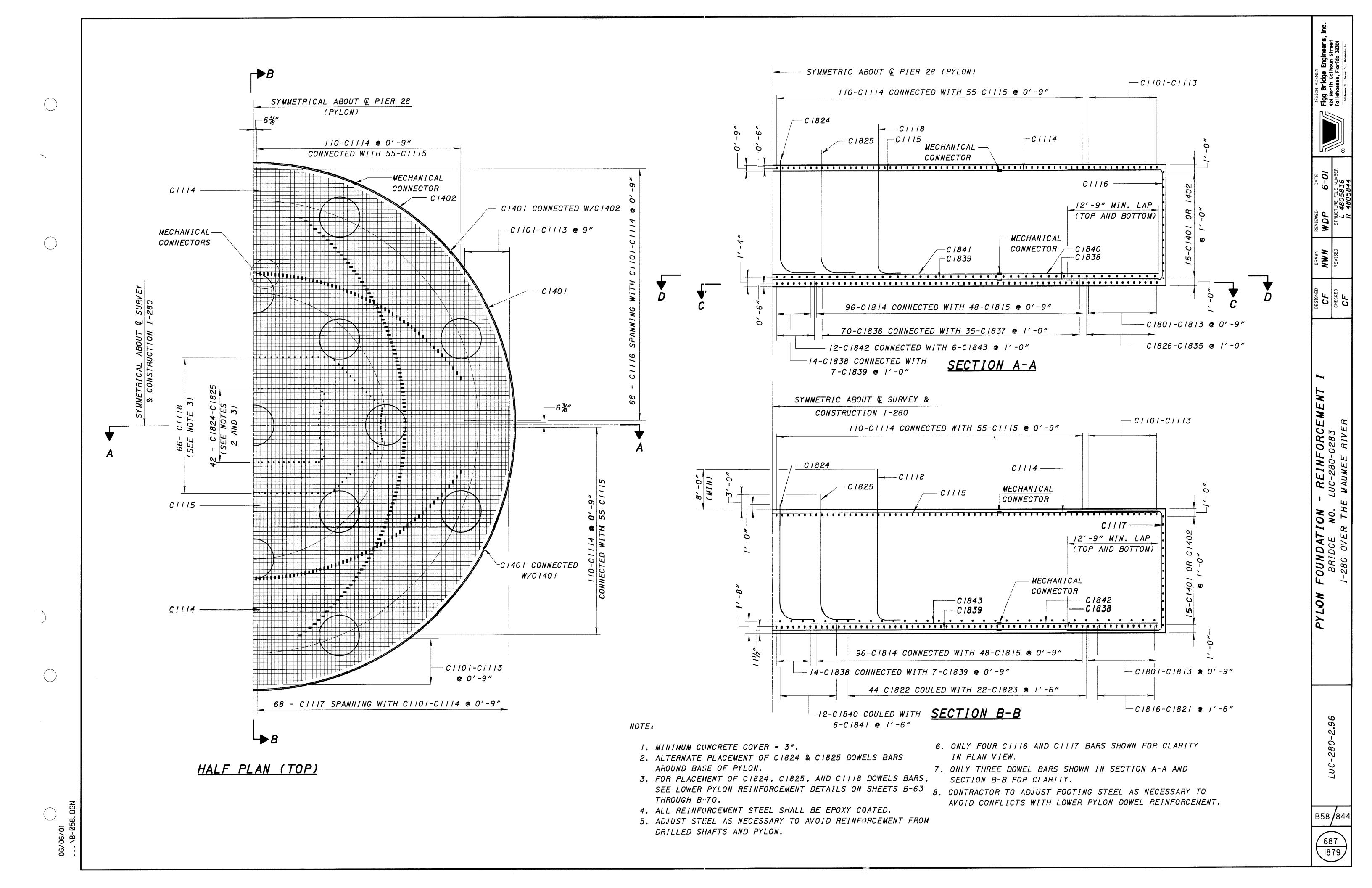
5. FOUNDATIONS FOR THE TEMPORARY PIERS 27A, 27B & 27C, NB AND SB,

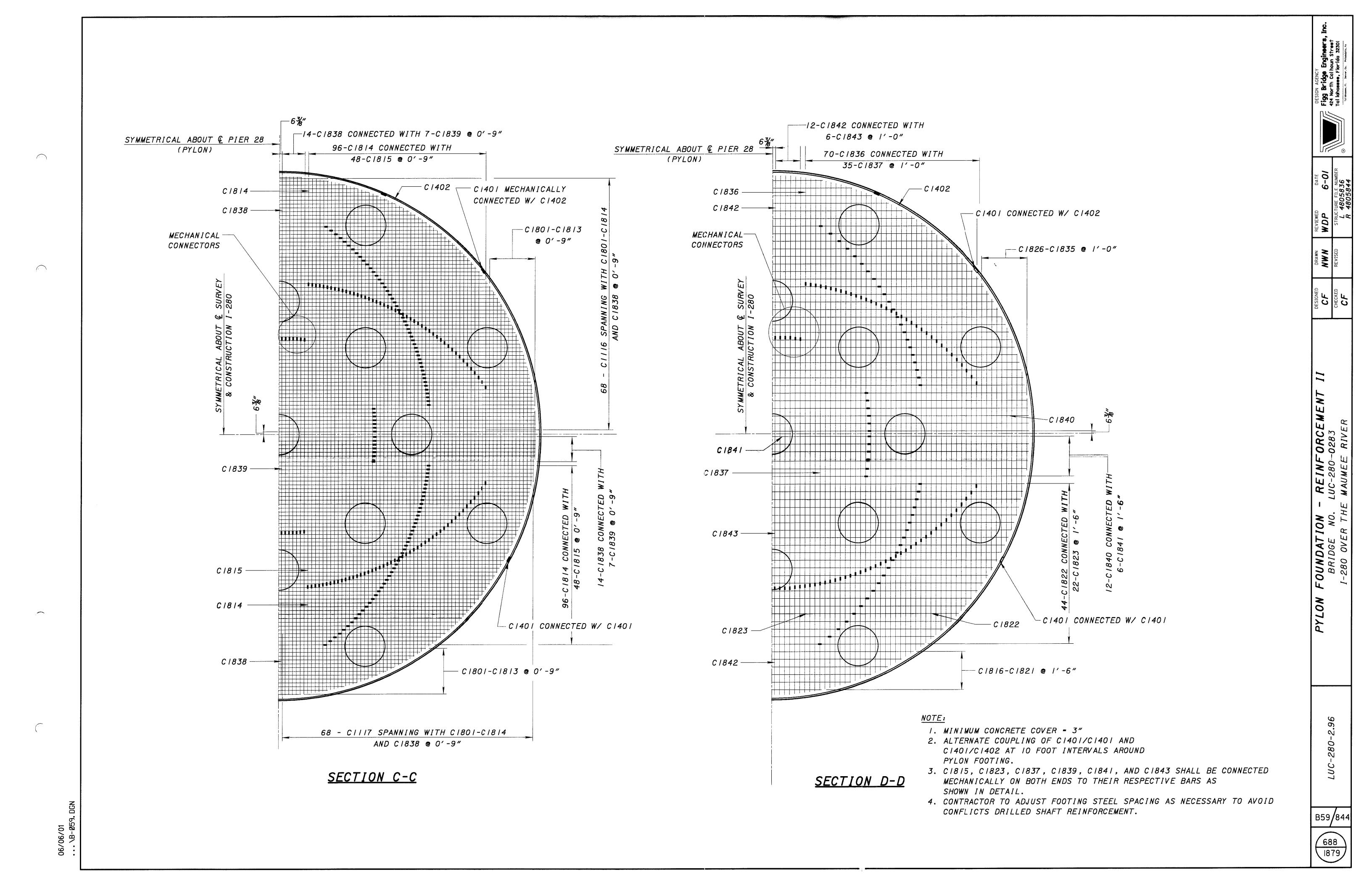
7. BID QUANTITIES DO NOT INCLUDE DIRECT PAYMENT FOR DRILLED SHAFT

* - TOP OF SHAFT ELEVATION IS EQUAL TO BOTTOM OF FOOTING ELEVATION FOR ALL DRILLED SHAFTS.

BESIGN AGENCY Figg Bridge Engineers, Inc. 424 North Calhoun Street Tal lahoasse, Florida 32301 Tal koue. A. Milaapia. Po
REVIEWED DATE WDP 7-01 STRUCTURE FILE NUMBER L 4805836 R 4805844
DESIGNEDDRAWNCFMLBCHECKEDREVISED
MAIN SPAN UNIT - DRILLED SHAFT SCHEDULE BRIDGE NO. LUC-280-0283 I-280 OVER THE MAUMEE RIVER
LUC-280-2.96
B56/844







MARK	NO.	LENGTH	WEIGHT	TYPE	A	В	С	D	E	F	G
C / 10 /	4	8'-9 ³ /"	187	1	8'-9%						
CI102	4	19'-6"	4/4	1	19'-5 ¹³ /16"						
C//03	4	26' -01/2"	553	1	26'-03/"						
CI104	4	31'-2"	662	1	31'-1 ^{!5} /16"						
C//05	4	35'-6"	754	1	35'-515/6"					ar 9 (1944) (1944) (1944) (1944)	-
C 106	4	39' - 3 ³ /"	835	1	39' - 35/8"						
C 07	4	42' -83/"	908	1	42' -8%6"						:
C 08	4	45' - 10"	974	1	45′ -9 ¹⁵ /16″						
C//09	4	48' -81/2"	/,035	1	48' -85/16"						
CIIIO	4	51'-41/2"	1,091	1	51'-41/4"						
2////	4	53' - 10 ¹ /4"	1,144	1	53' - 101/8"						
21112	4	56' -2 '/4 "	1,194	1	56' -2 '/4 "						
2///3	4	58' - 4 ³ /4"	1,241	1	58' -4 ¾ "						
2///4	440	21'-0"	49,092	1	21'-0"						
2///5	220	47'-3"	55,2/6	1	47'-2 % "						
21116	27 2	39'-5 ³ /"	<i>57</i> ,036	3	12'-9"	14' -81/8"					
C 7	272	40' - 21/4"	58,052	3	12'-9"	15' -4%6"					
21118	/ 30	25' - 11/4"	17,338	2	3'-0"	22' - 51/2"					
C 40	75	60'-0"	34,425	42	60'-0"	51'-85/16"					
:1402	/5	24' -91/2"	2,844	42	24' -97/16"						
C 80	4	8'-9 % "	479	1	8'-9%"						
C1802	4	19'-6"	1,060	1	19' - 5 ¹³ / ₁₆ "						
C 1803	4	26′ -0½″	1,416		26'-0%"						
C 1804	4	31'-2"	1,695		31'-15/16"						-
C/805	4	35'-6"	1,931	1	35' -5 ^{!5} /16"			·	-		
C1806	4	39' - 3%"	2,/38	/	39' - 35/8"				-		
C 807	4	42' -8%	2,324	/	42' -8%6"			1			-
C 808	4	45' - 10"	2,493		45'-9 ¹⁵ /16"						
:1809	4	48' -8 ¹ /2"	2,649		48' -85/16"	-					
C1810	4	51'-41/2"	2,794		$51' - 4^{1}/_{4}''$						
C 8	4	53' - 10 //4"	2,929		53' - 101/8"						
C1812	4	56' - 21/4"	3,057		56' -21/4"						
C1813	4	58' -4%	3,177		58' -4%					-	
C/8/4	384	21'-0"	109,670	1	21'-0"						
C/8/5	192	45'-5"	//8,566		45' -47/8"		· · · ·				
C / 8 / 6	2	19'-91/2"	538		19'-9/4"						
C1817	2	31'-41/4"	853		$31' - 4\frac{1}{8}''$						
C 8 8	2	39' - 51/2"	1,073		39' - 5%6"						
C 18 19	2	45' - 111/2"	1,250		45'-11%						
01820	2	51'-5%	1,400		51'-5%6"						
C1821	2	56' - 3'/2"	/,53/	1	56' - 37/ ₁₆ "						
1822	88	21'-0"	25,/33		21'-0"						
C / 823	44	43' -81/2"	26,150		43' -8¾"	15'-51/16"	ار الای این از این از این از این				
C 1824	41	$19' - 3'/_4''$	10,742	2	4'-6"					· · · · ·	
C / 825	41	$21' - 3'/_4''$	11,857	2	4'-6"	17'-51/16"				-	
C / 826	2	13'-10"	376	1	$ 3'-9' _{16}''$		<u> </u>	·		· · ·	
C 1827	2	$24' - 3'/_4''$	660 857	1	24' - 3'/8''			······································		<u>.</u>	
C / 828	2	$31' - 4\frac{3}{4}''$	853	1	$31' - 4\frac{1}{2''}$						
C 1829	2	36' - 1 13/4"	1,005	1	36' - 1 19/16"						
C1830	2	41'-9"	1,135		41'-87/8"						
C1831	2	45' - 11/4''	1,249	1	45' - 3 /6" 49' - 8 [!] /2"						
C 1832	2	49' -8 <u>1/2</u> " 53' - 13/4"	1,352	1	49° -8% 53′ - 1%6″						
C 1833	2	$53' - 1'_{4''}$ $56' - 3'/_{2''}$	1,445	/ 	55' - 17/16" 56' - 37/16"						
C 1834	2	59' - 21/2"	1,531	1	59' - 27/16"			, <u></u> ,,,_,,_,,_,,,,,,,,,,,,,,			
C 1835		21'-0"	1,610 39 984	1	21'-0"						
C 1836	140		39,984 43,270		45' -5 ⁷ /16"						
C 1837	70	45' -5½" 32' -0"	43,270	1	45' -5'/16" 32' -0"						
C 1838	<u>56</u>	32' -0" 37' -9 <u>3/</u> "	24,371	1	32' -0" 37' -9%"						
C 1839	28	32'-9%" 32'-0"	/4,396 /0,445	1	32'-0"					}	
C 1840	24 	32" -0" 37' -6 ¹ /4"	<i>10,445</i> <i>6,122</i>	1	32 -0" 37' -6 ¹ /8"						
C 1841	24	32'-0"	10,445	1	32'-0"						
C 1842 C 1843	12	37'-9 ¹ /4"	6,163	1	37'-9 ¹ /8"			L	<u> </u>		

DGN 06/06/01 ... \B-Ø6Ø. |

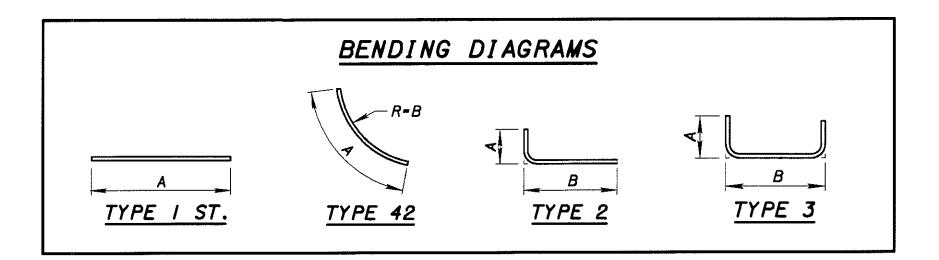
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<u>788,312</u> LBS.

TOTAL

◆ BAR DIMENSIONS AND QUANTITY ARE AVERAGE FOR GROUP OF BARS IDENTIFIED BY THE BAR MARK.



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ESTIMATED QUANT	ITIES / PY	LON	FOUNDATION
ITEM		UNIT	QUANTITY
CLASS 4000M CONCRETE	CU.	YARD	S 5,034
REINFORCING STEEL		LBS.	788,312

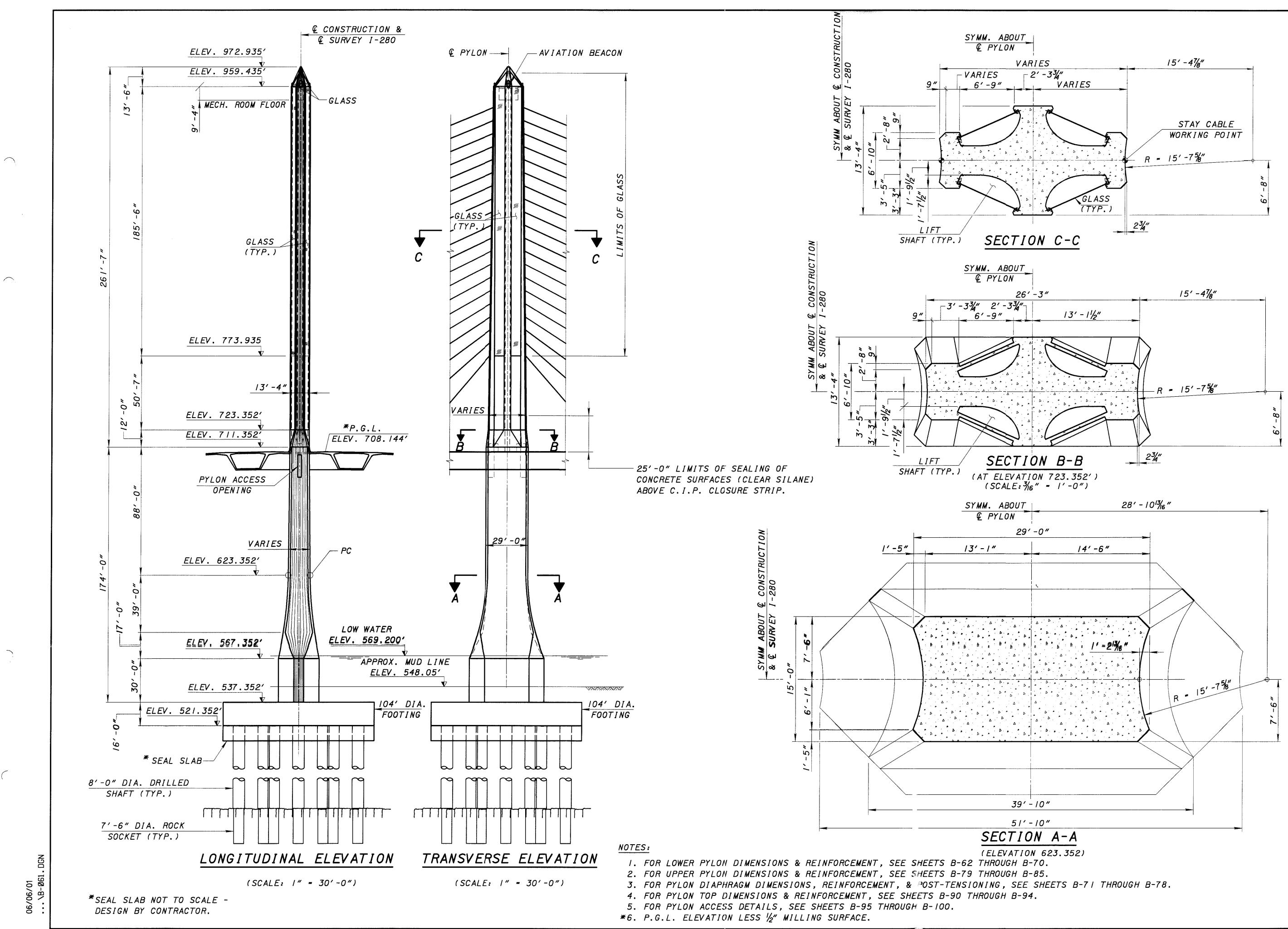
<u>NOTE:</u>

- I. WEIGHT GIVEN IN LBS.

- COATED.
- INFORMATION ONLY.
- BY THE ENGINEER.

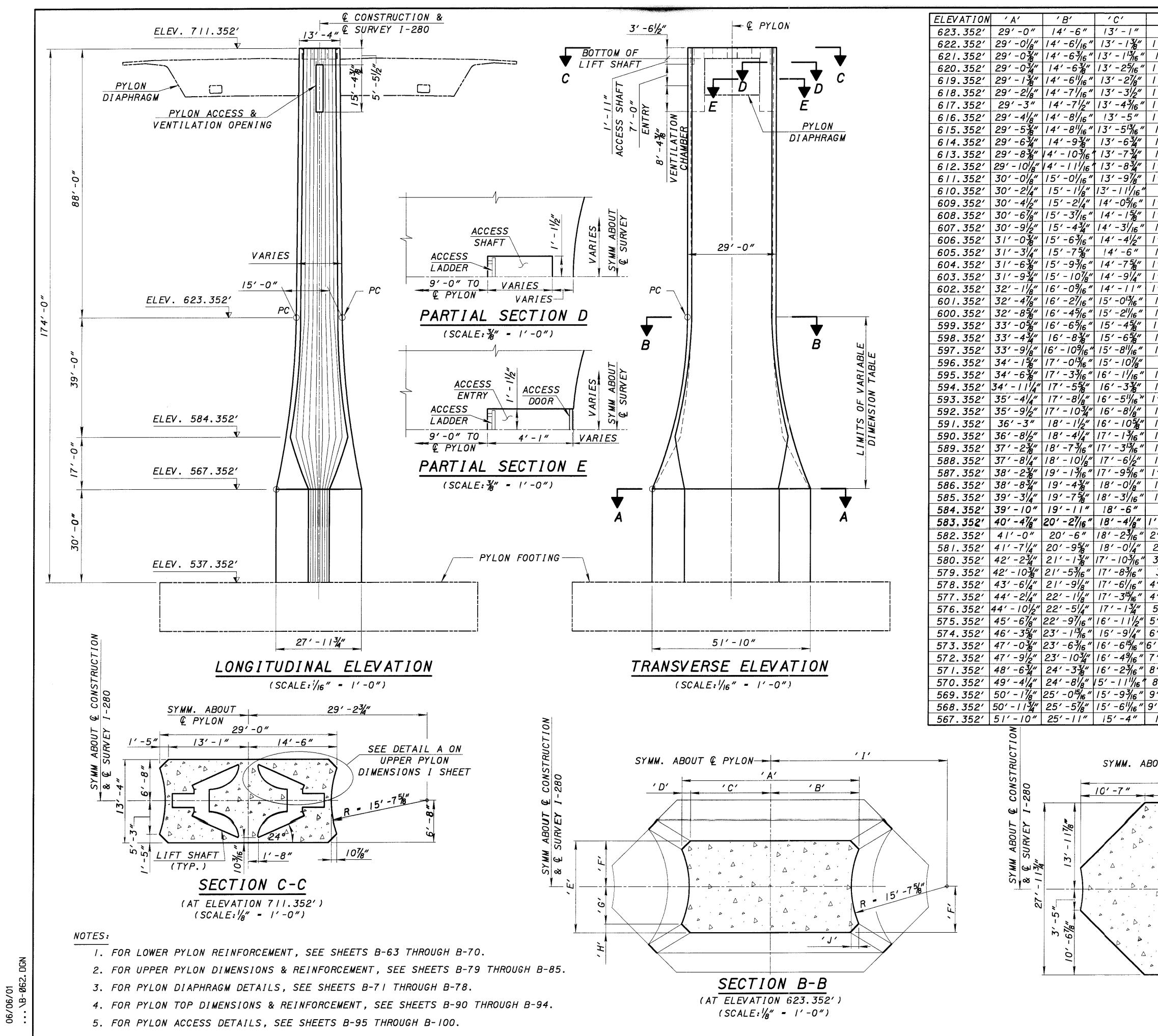
2. COLUMNS H,K,O, & R NOT NEEDED. 3. ALL DIMENSIONS OUT TO TOP OF BAR. 4. ALL REINFORCING STEEL SHALL BE EPOXY 5. REINFORCEMENT WEIGHTS AND LENGTHS FOR 6. MECHANICAL CONNECTIONS SHALL BE CADWELD 125% OF YIELD STRENGTH SPLICES OR EQUIVALENT TO BE APPROVED 7. THE CONCRETE USED IN THE PYLON FOOTING SHALL BE CONSIDERED TO BE MASS CONCRETE, AND SHALL BE PAID UNDER PAY ITEM SPECIAL, EXT. 8427//00, CONCRETE, MISC.: CLASS 4000M CONCRETE, PYLON FOUNDATION (MASS CONC.).





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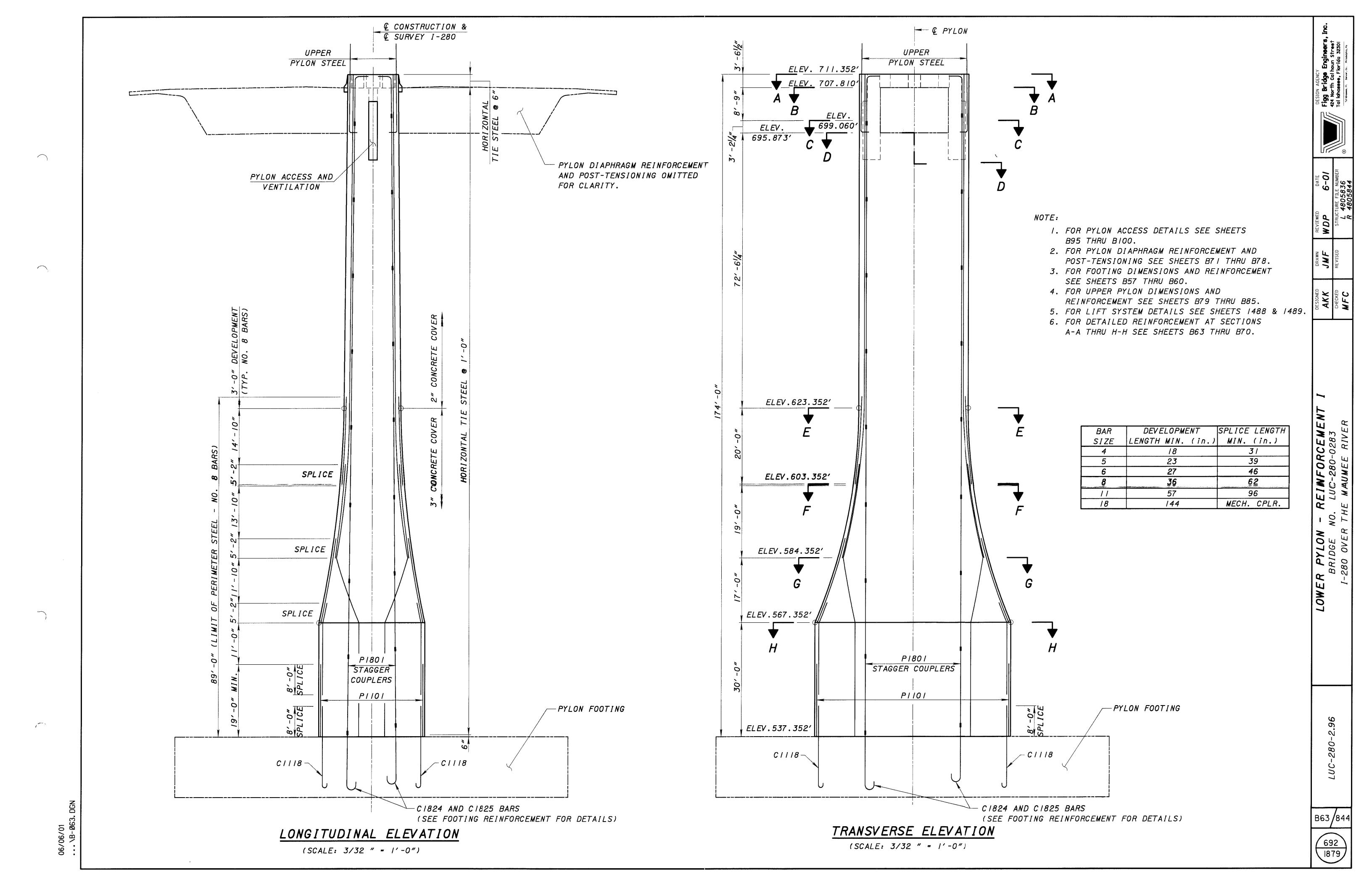


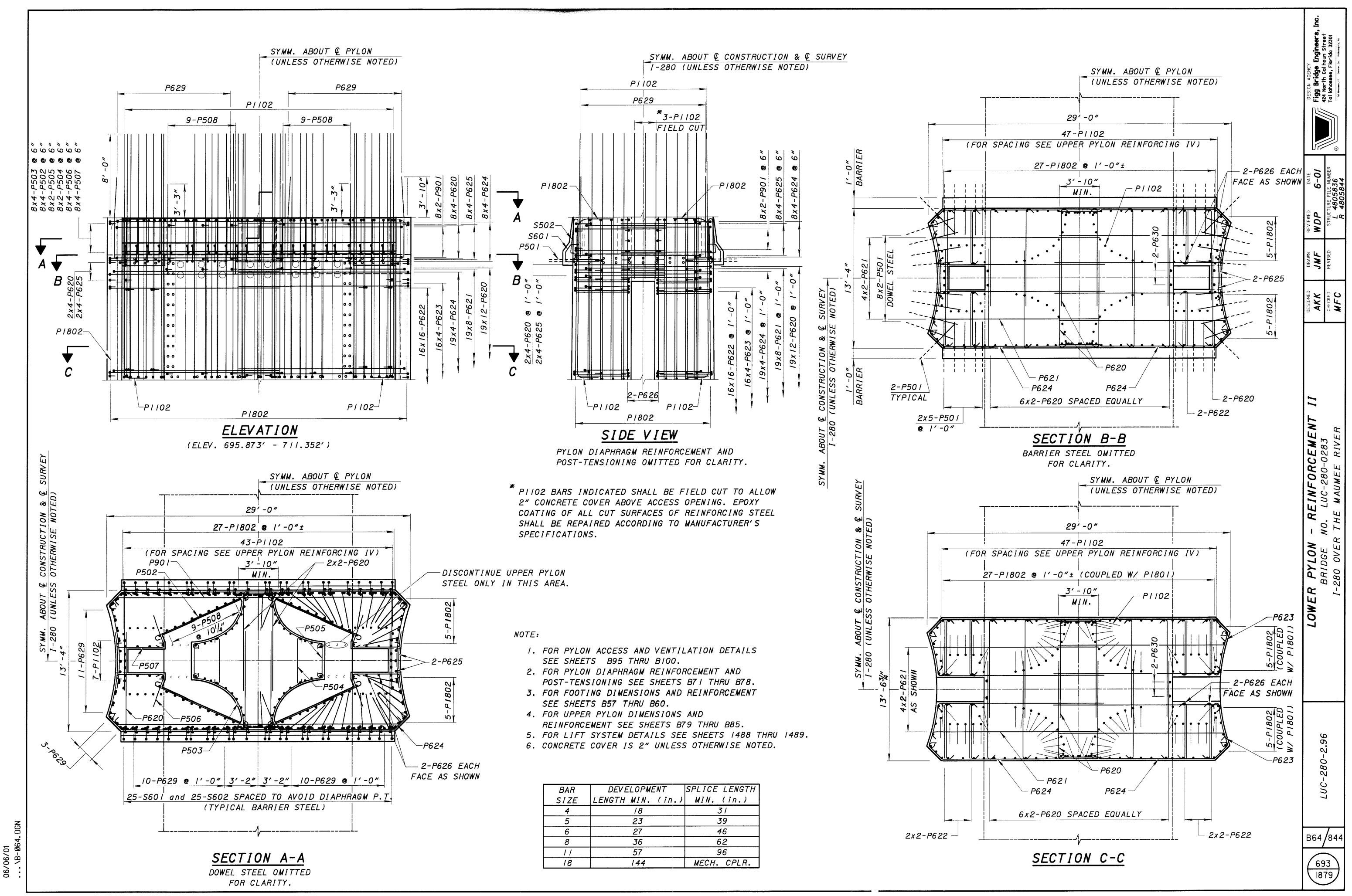


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' D'	' E'	' <i>F</i> '	' G'	' H'	<i>'I'</i>	<i>'</i>] <i>'</i>]	
<u> </u>	15'-0"	7'-6"	6'-1"				N AGENCY Bridge Engineers, Inc. rth calhoun Street cesses, Florida 32301
'-4 /16″	15'-01/2"	7'-61/4"	6'-1"	1'-53/16"	28' - 10 7/8"	1'-2'3/16"	Ber 4 reet 2301
1'-43/1"	15' - 1"	7' - 6'/2''	$6' - 1'_{8''}$	1'-5 % "	28' - 10 ¹⁵ /16"	' -2 ¹³ //6"	DESIGN AGENCY Figg Bridge Engineers 424 North Calhoun Street Tal lahassee, Florida 32301 Tal Hammer, H. Dower, Co. Millonophic, Pa
'-4 / ₁₆ "	$15' - 1\frac{5}{18}''$	$7' - 6^{13}/_{16}''$	6' - 1'/4''	'-5%6" '-5%4"	28′ - / ₈ ″ 28′ - ⁵ / ₁₆ ″	' -2 ⁷ /8" ' -2 ¹⁵ /16"	ENCY Gal hou e. Flori
'-3 ³ /16" '-39/16"	5'-2 /4" 5'-3 /8"	7'-7 /8" 7'-7 ⁹ /16"	6' - 17/16" 6' - 15/6"		28' - 1 1716" 28' - 1 15/1		AGEN th C
1'-35/16"	15'-4"	7'-8"	6' - 1 ¹⁵ /16"	1'-61/16"	28' - 1 ¹⁵ /16"	1'-33/16"	DESIGN AGENCY Figg Bridge 424 North Call Tal Idhassee, Fi Tal Massee, Fi
1'-31/16"	15' -47/8"		6' - 21/4"	1'-6 <u>¾6</u> ″	29'-0 % "	'-35/16"	
1'-2 % "	15'-6"	7'-9"	6'-2 % "	1'-65/16"	29' -0 ¹³ / ₆ "	1'-31/2"	
1'-25/8"	15'-71/8"	7'-9%6"	$6' - 3'/_{16}''$	<u>1'-67/16"</u>	29' - 15/16"	' - 3 / ₁₆ "	
'-21/2" '-25/16"	$15' - 8'/_4''$	7'-10 ¹ /8" 7'-10 ¹³ /16"	6' -3 <u>%</u> 6" 6' -4 <u>%</u> "	1'-6%/6"	29′ - ¹⁵ /16″ 29′ - 2 ⁹ /16″	'-37/8" '-41/8"	
1'-2 <u>716</u> 1'-2 3 /16"	15'-11"	7'-11/2"	$6' - 4\frac{3}{4}''$	$1' - 6\frac{3}{4}''$	29' - 3!/4''	$\frac{1}{1^{\prime}-4\frac{3}{8}^{\prime\prime}}$	
1'-2"	16'-0%"		6'-5 ¾ "	1'-6 ¹³ /16"		1'-4"/16"	α
' - ¹⁵ /16″	16' -2"	8'-1"	6′-6′/ ₁₆ ″	1'-67/8"	29' -47/8"	1'-5"	VIEWED DATE DP 6-01 STRUCTURE FILE NUMBER L 4805836 R 4805844
' - ¹³ / ₁₆ "	16'-35/"	8' - ¹³ / ₁₆ "	$6' - 6^{13}/_{16}''$	1'-6 ¹⁵ /16"	$29' - 5\frac{3}{4}''$	$1' - 5\frac{3}{8}''$	6 C
' - 3/" ' - /16 "	16' -5 <mark>'/4</mark> " 16' -7'/8"	8' - 25/8" 8' - 3%16"	6' -7 5/" 6' -8 1/2"	' -7 " ' -7 !/ ₁₆ "	29'-6 <u>%</u> " 29'-7 <u>%</u> "	$\frac{1'-5\frac{3}{4}''}{1'-6\frac{1}{8}''}$	805 805 805
	16'-9"	8' - 4!/2''	6'-9 % "	' -7 / ₁₆ "	29' -8 ¹ //6"	1'-6 <u>%</u>	
1' - 1%6"	16'-107/8"	8' - 57/16"	6' - 10 % "	$1' - 7'/_{R''}$	29' -9 ¹³ /16"	' -7 / ₁₆ "	REVIEWED WDP STRUC R
' - %6"	17'-1"	8'-61/2"	$6' - 1 \frac{3}{8}''$	'-7 /8"	29′ - 10 ¹⁵ /16″	' -7 <i>%</i> /6″	
<u> ' - %6"</u>	$17' - 3\frac{1}{8}''$	8' -7 ⁹ /16"	7'-07/16"	$1' - 7\frac{1}{8}''$	$30' - 0'/_8''$	1'-8 ¹ /16"	SED T
' - 5/" ' - 5/"	17'-5 <u>/4</u> 17'-75/"	8' -8 <u>%</u> 8' -9 ¹³ /16"	7' - 19/16" 7' - 23/:"	1' -7 ¹ /16"	30' - ¾" 30' -2 /16"	' -85/" ' -9 [!] /4"	drawn JSF Revised
' - 5/" ' - ¹¹ /16"	17' -7 % " 17' - 10"	8'-9'% 8'-11"	7'-2 <u>/4</u> 7'-3 ¹⁵ /6"	' -7 / ₁₆ " ' -7 "	30' -2'/ ₁₆ " 30' -4 [!] / ₁₆ "		
' - <u>3/</u> "	18'-01/2"		$7'-5'/_4''$	1′ -7″	30' -57/16"	' - 0%6"	
1'-17/8"	18'-3"	9' - 11/2"	7′-6%6″	1'-6 ¹⁵ /16"	30′-67⁄%″	' - 5/16"	AKK AKK CHECKED
1'-2"	18'-5%"	9' - 2 ¹³ /16"	7'-8"	1'-67/8"	30' -8%"	2'-01/16"	E en P Es
$\frac{1'-2!}{8''}$	18' -8%"	9'-4%6" 9'-55/"	7'-97/16" 7'-10 ¹⁵ /2"	$1' - 6\frac{3}{4}''$	30′ -97⁄8″ 30′ -117⁄16″	2' - 0'%/6"	
'-2 <mark>'/4</mark> " '-2 ⁷ /16"	18' - 11/4" 19' - 21/8"	9'-5% 9'-7 [!] /16"	8'-0 ¹ //"	1'-6%/16"	31' - 11/16" 31' - 11/16"	<u>~ 1/16</u> 21-211/16"	
1'-25/8"	$19' - 5'/_{R''}$	9' -8%16"	8'-21/16"	' -67/16"	31'-2"/16"	2' - 3"/16"	
1'-27/8"	19'-81/8"	9′ - 10 <mark>′/16</mark> ″	8'-3 <u>4</u> "	1' -65/16"	31'-4%"	2' -4 ¹¹ /16"	
$1' - 3'/_8''$	19' - 11/4''	$9' - 1 \frac{5}{8}''$	8'-51/2"	'-6 <u>%</u> 6"		$2' - 5^{13}/16''$	
'-3 <u>3</u> /" '-35/"	20' - 2'/2"	10' - 1 '/4'' 10' -2 ¹⁵ /16''	$8' - \frac{1}{4}''$	1'-6"	3 ' -7 ³ /6 " 3 ' -9%/6 "		
- 3 18 ' - 3 ¹⁵ /16 "	20'-9 '/4 "	10'-45%"	8'-11"	1'-5%"	31'-113/"	2'-91/2"	
$ ' - 4^{1}/_{4}''$	21'-03/4"	10' -63/8"	9′-0 ¹⁵ /16″	1' -57/16"	32' - 11/8"	2' - 107/8"	S
1'-45/8"	21'-4%"	10' -83/16"	9'-2 ¹⁵ /16"	1'-5 ¹ /4"	32' -2 ¹⁵ /16"	3' -05/16"	> ~
1'-5"	21'-8"			1'-5"	$32' - 4\frac{3}{4}''$	$\frac{3' - 17''}{9''}$	S10 83 IVE
2' - 3 ¹³ / ₁₆ "	21' = 114''	10' - 1 % " 1 ' - ¹³ / ₁₆ "	9' - 17/16"		$32' - 10\frac{34''}{4}$ $33' - 4\frac{34''}{4}$	2' - 1 7/16" 2' - 8 ¹³ /16"	
2'-9 <u>%</u> "	22 - 578	$11 - \frac{17}{16}$ $11' - \frac{34''}{4}$	8'-6 3 /"		<u>33' - 10'3/6"</u>		
<u>3' - 3'/8"</u>	22' - 115/1"	11'-5 ¹³ /16"	8'-25/"	$\frac{2}{3'-3'/_{B''}}$	34' - 4 ¹⁵ /16"		I N M L
3'-9"	23' - 35/8"	′ -7 <i>'3/₁₆"</i>	7′ - 10 ¹³ //6″	3'-9"	34′ - I I'/ ₁₆ ″	$2' - 1\frac{3}{4}''$	
4' - 3 ¹ /16"	23' -7 1/8"	11'-9 ¹⁵ /16"	$7' - 6\frac{7}{8}''$	$4' - 3'/_{16}''$	35' -5 ¹ /4"	$\frac{1'-11'/2''}{1'-11'/2''}$	N.
4' -9'/16" 5' -3 [!] /2"	24' -0'/8" 24' -4!/2"	12'-01/16" 12'-21/4"	1'-2'/8" 6'-10 ³ /4"	$\frac{4'-9'}{16''}$ 5'-3'/2"	35' - 7/ ₁₆ " 36' -55/8"	1'-9/16"	H ⊡ . S
5'-9 ¹⁵ /16"	24' -9"	$12' - 4'/_{2''}$	6′-6%/6″	5' -9 ¹⁵ /16"	36' - 1 1 ⁷ / ₈ "	$\frac{1}{1'-5'/a''}$	PYLON ER TH
5′ - 4 <i>%</i> 6″	25' - 11/2"	12'-63/4"	6′ -2 ¾ 6″	6'-4% ₆ "	37'-6!/8"	1' - 35/16"	
′ - I ⁵ /16 ″	25' -61/8"	12' -9 <u>'/16</u> "	5' -9 ¹³ //6"	6' - 1 15/16"	38'-0%"	' - 7/ ₁₆ "	
<u>' -6³/16"</u>	$25' - 10\frac{7}{8}''$	$\frac{12' - 11'_{16''}}{13'_{13'}}$	$5' - 5'/_4''$	7'-6 ³ /16"	38'-65/"	1 1/16 "	
3' - ³ /16" 8' - 8 ³ /1"	26' - 35/8" 26' - 85/8"	13' - 19/16" 13' - 45/16"	5'-0%" 4'-7%"	8' - ³ /16" 8' -8 ³ /8"	39' -0 ¹⁵ /16" 39' -7 ³ /16"	10 ¹ /16″ 8 ¹ /2″	LOWE BRI 1-280
0'-3 /16"	20 0 /8 27' - 15/"	13' -6 ¹³ / ₁₆ "	$\frac{4'-3!}{16''}$	9' - 3 ^{!!} /16"	40' - 11/2"	71/16"	 10
' - <u>3/</u> 16"	27'-65/8"	13'-95/16"		9′ - ¾6″	40' -7 3/4"	5 ³ /4	
10' -7 "	27'-113/4"	13'-11%"	3' -5"	10'-67/8"	41'-21/16"	4 ⁹ /16 "	
			A 1 /	-21/16″			
OUT @ P			71	<u>-//b</u>			
	51'-1		5/_1//				
<u>/5'-</u>			5' - 11"				
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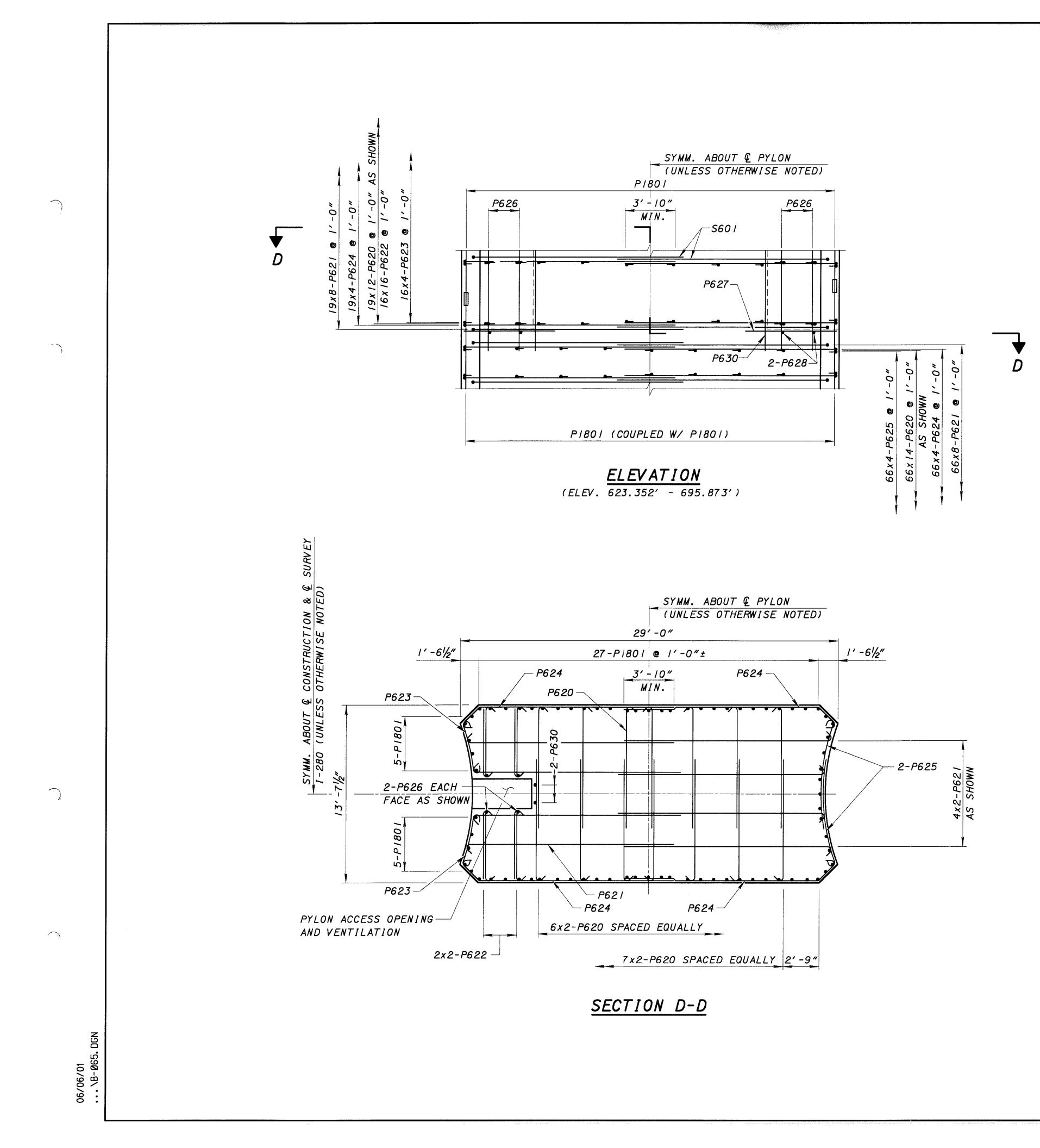


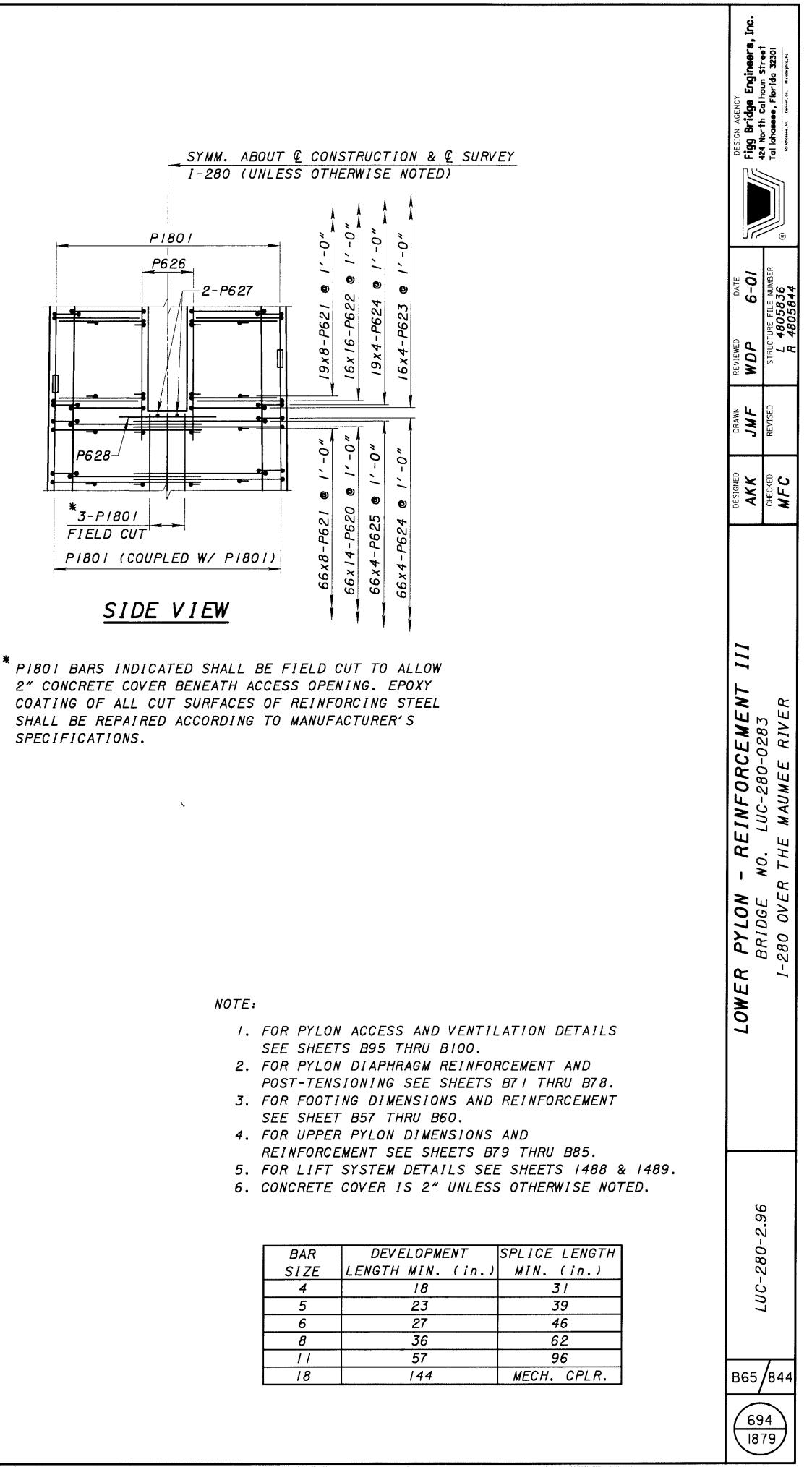
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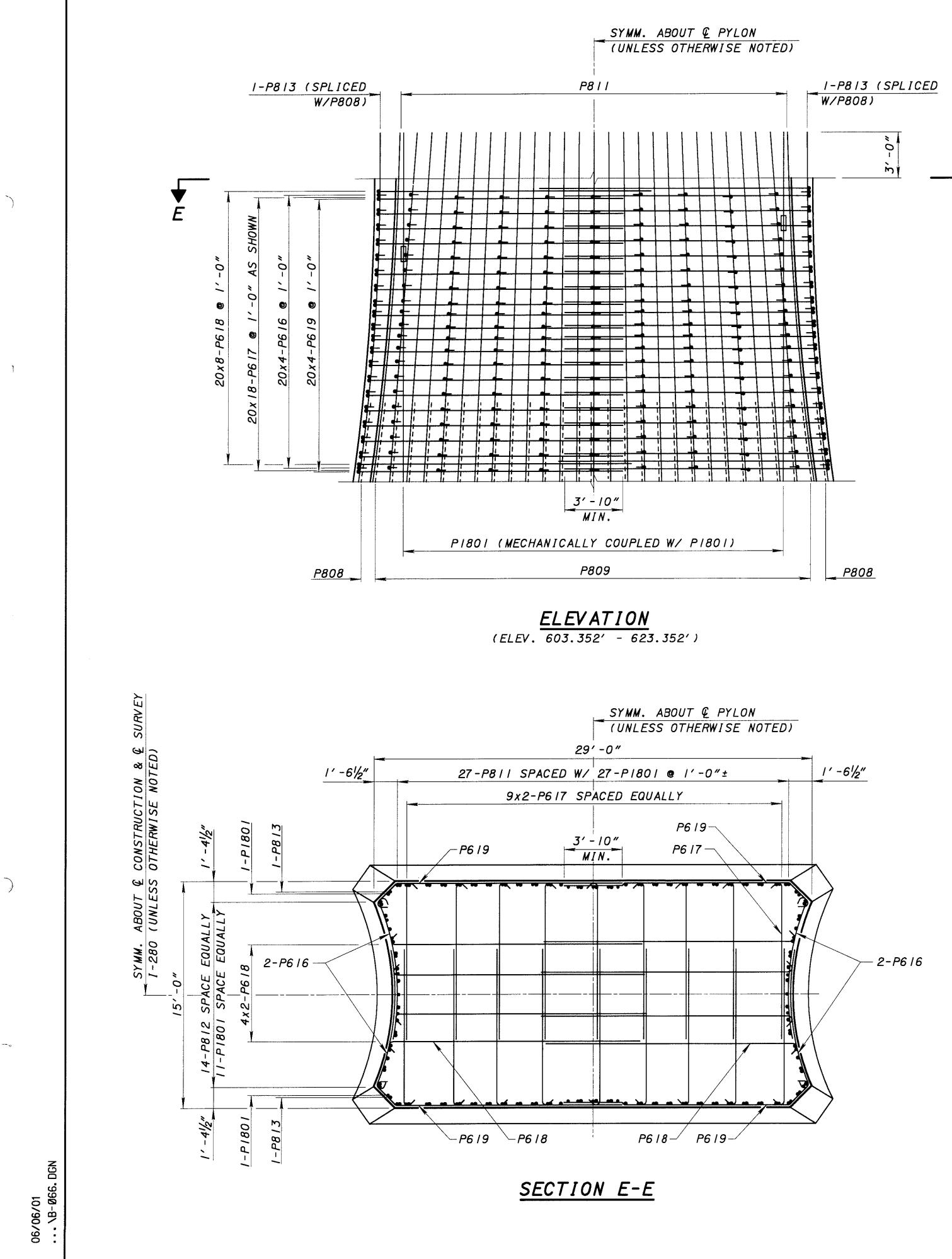
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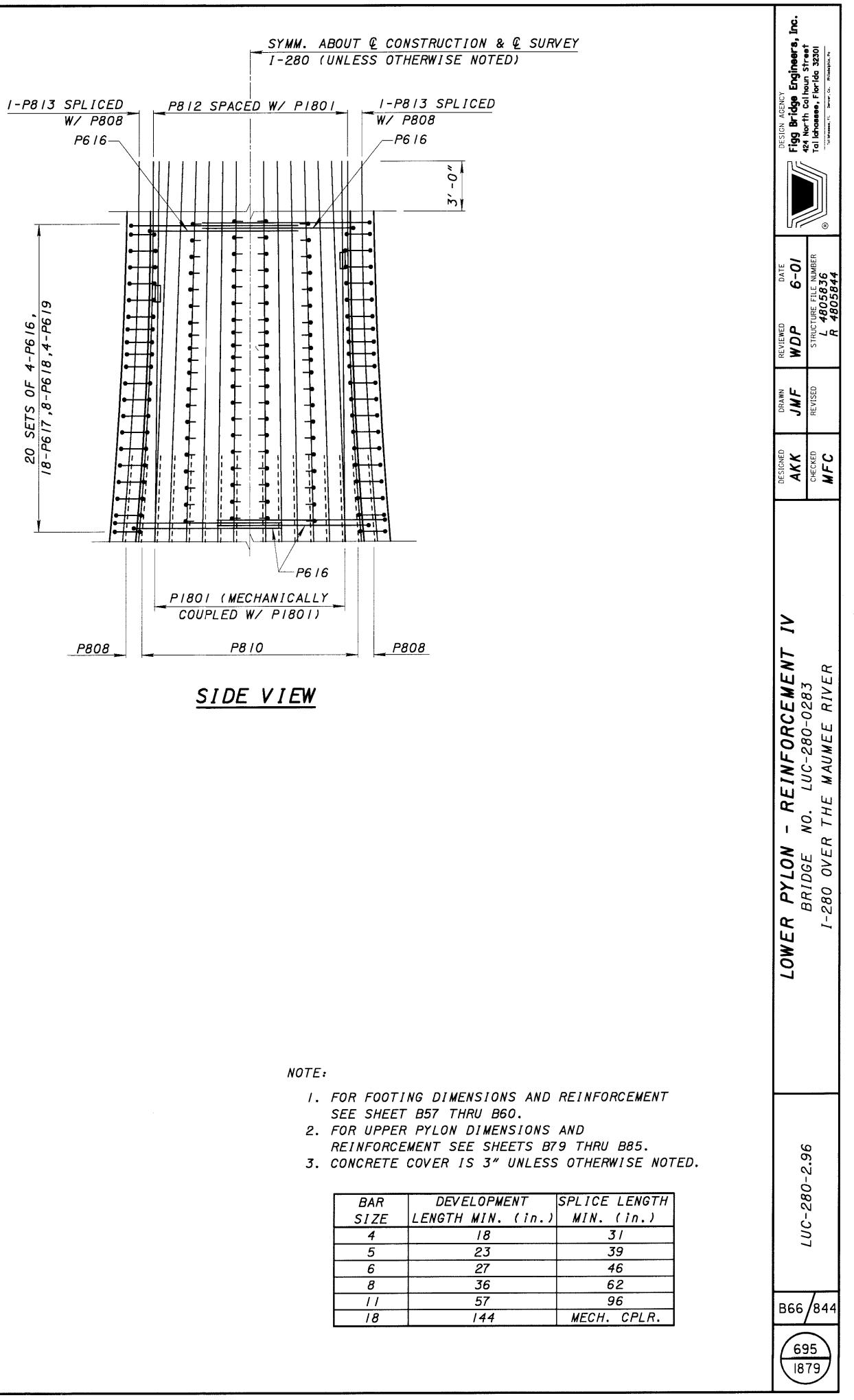
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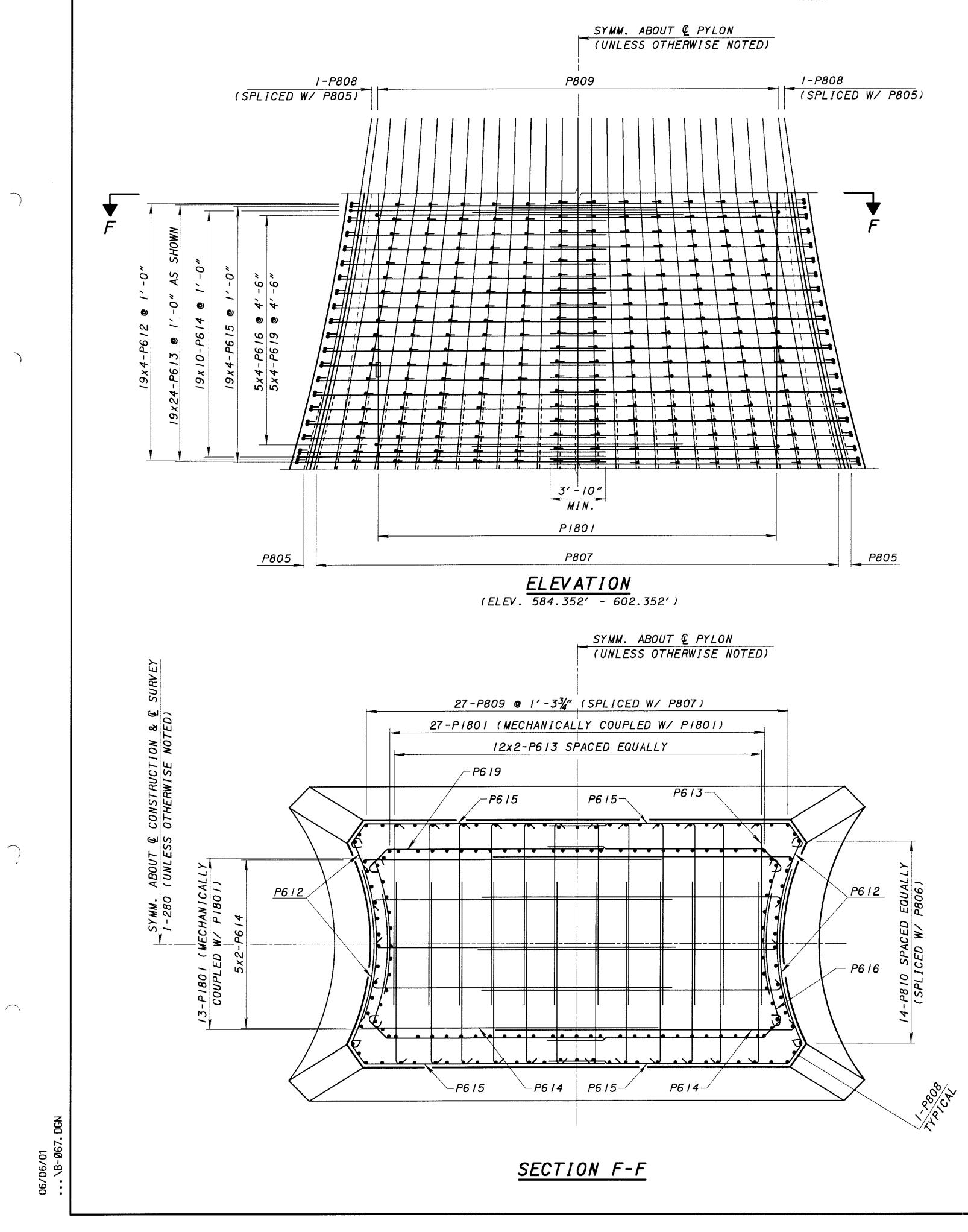


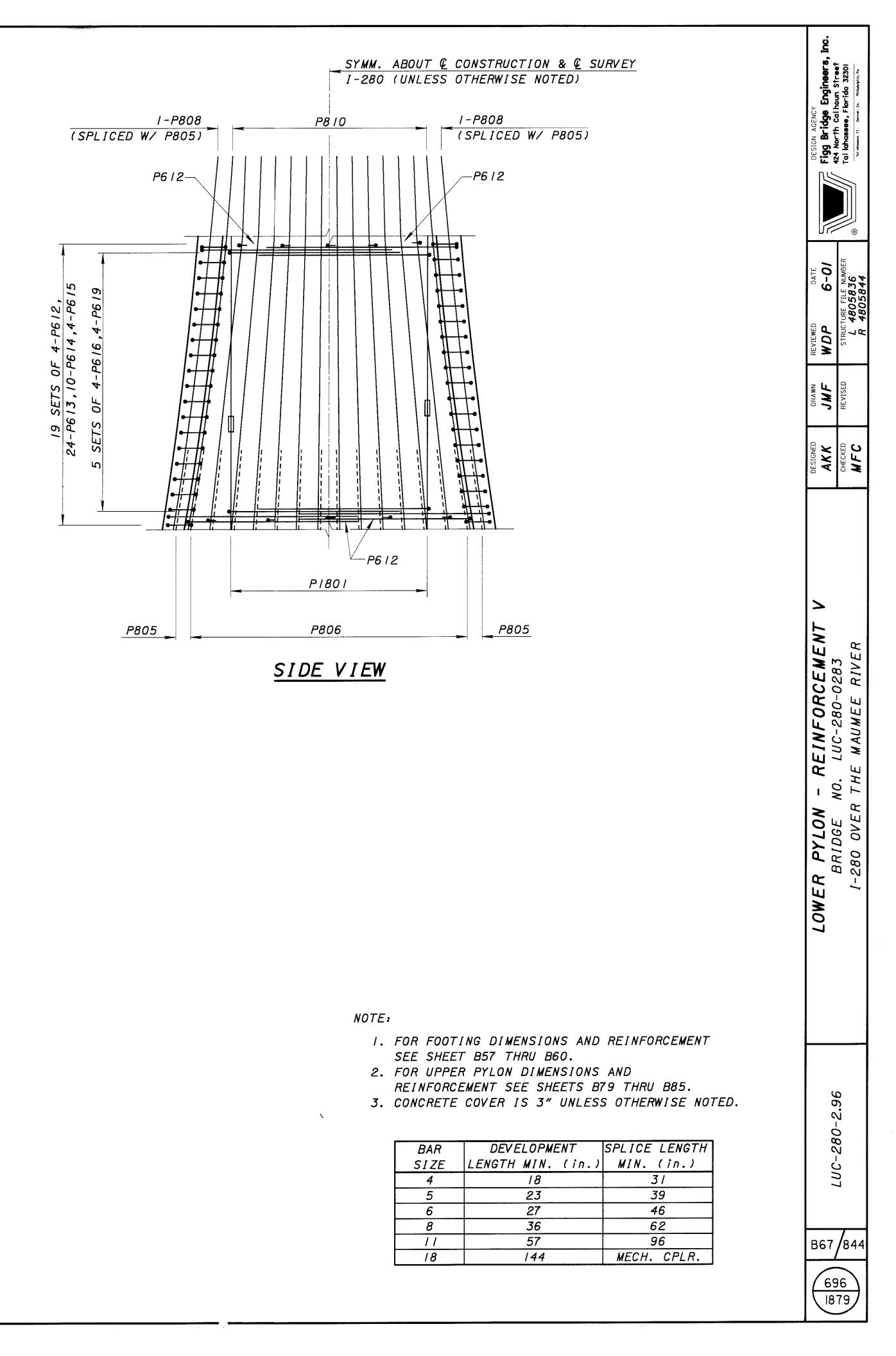


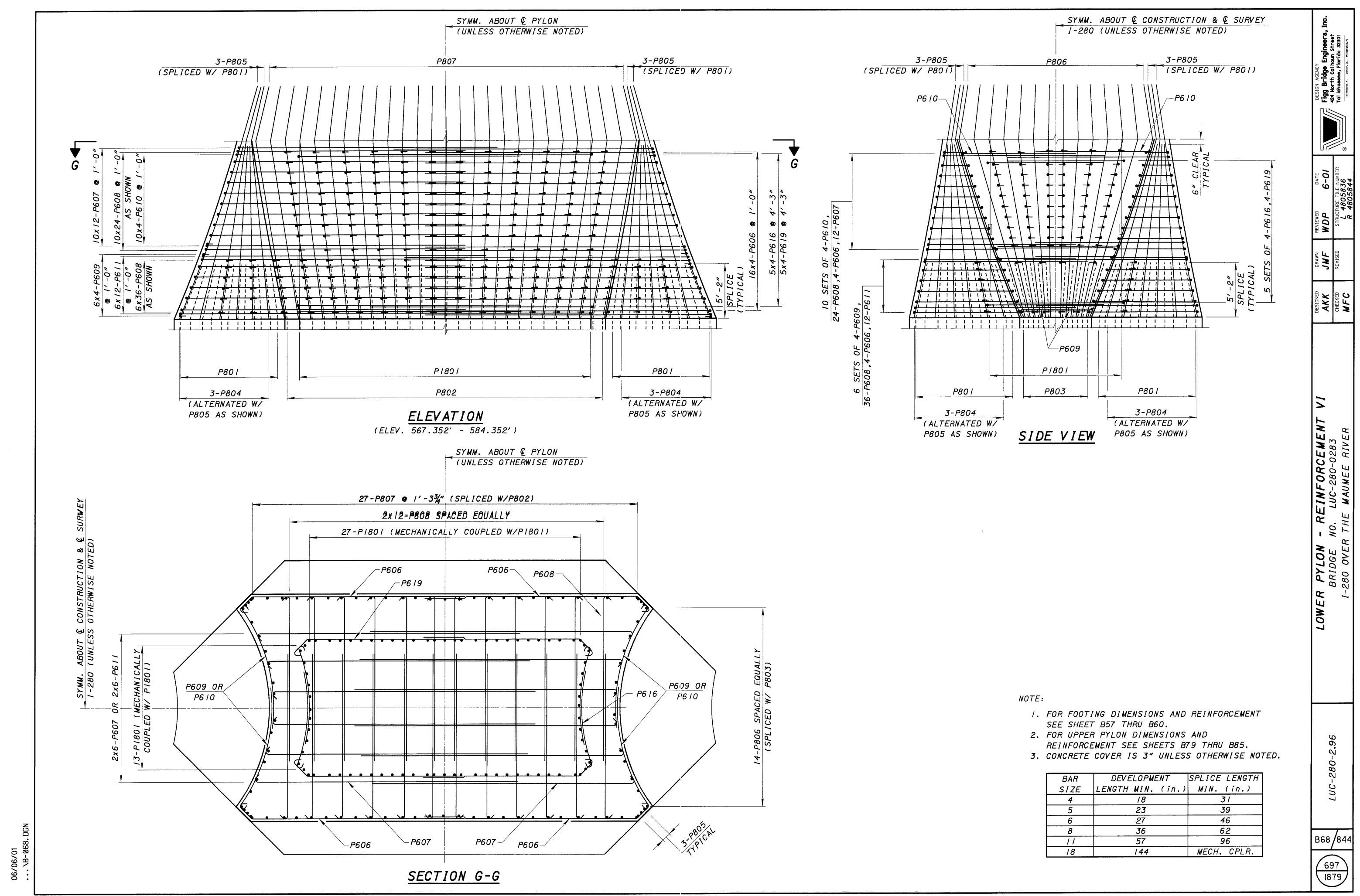
SPECIFICATIONS.











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