FINAL REPORT MARCH 2025

## POR-43-3.87-3.94

Safety Study SR-43 at Trares Road & Randolph Road Suffield Township | Portage County Crash Data (2016-2020)





Lanham Engineering LLC Prepared for: ODOT Highway Safety Program 1980 West Broad Street Columbus, OH 43223 (614) 466-7045

Prepared by: Lanham Engineering, LLC and Carpenter Marty Transportation







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## **1.0 Executive Summary**

The study area is along the corridor of SR-43 (Cleveland Canton Road) in Suffield Township, within Portage County. It includes the unsignalized intersections of SR-43 at Randolph Road and SR-43 at Trares Road, which is located approximately 350 feet to the south of Randolph Road. The intersections of SR-43 at Randolph Road and Trares Road appeared on ODOT's Highway Safety Improvement Program's (HSIP) Priority Locations list, ranking #54 and #53, respectively, on the 2020 rural intersection list.

SR-43 is classified as a rural principal arterial. At its intersection with Randolph Road, the east leg of Randolph is a local road while the west leg is a major collector. At Trares Road intersection, the east and west legs of Trares Road are classified as local roads.

In the five-year period between 2016 and 2020, a total of 21 crashes occurred at the intersection of SR-43 & Randolph Road, with one involving serious injuries, four involving minor injuries, and four involving possible injuries. These crashes consisted of 16 angle crashes, three rear end crashes, and two left turn crashes. Failure to yield was the highest contributing factor, accounting for 76% of the crashes. These trends indicate that drivers are accepting a smaller gap in traffic to complete their turns.

In the five-year period between 2016 and 2020, a total of 16 crashes occurred at the intersection of SR-43 & Trares Road, with two involving serious injuries, seven involving minor injuries, and one involving possible injuries. These crashes consisted of six angle crashes, four rear end crashes, four left turn crashes, one fixed object crash, and one overturning crash. Failure to yield was the highest contributing factor, accounting for 43% of the crashes.

According to HSM methods, the study segment and intersections combined are performing slightly worse than their peers overall. While the Randolph Road intersection is the only element that shows a potential for safety improvement for all crash severities, it does show a higher likelihood of injury crashes at the Trares Road intersection compared to similar intersections. Based on the findings of the study, it is recommended to implement the following countermeasures listed below:

#### Short Term

• Add an advance warning sign (W7-6) on the south leg of the Randolph Road intersection and on the north leg of the Trares Road intersection.

#### Long Term

• Alterative 2: Install a mountable median on SR-43 at the Randolph Road intersection in order to restrict movements at the intersection. This also includes constructing a single lane roundabout at SR-43 & Trares Road.





## 2.0 Purpose and Need

The intersections of SR-43 at Randolph Road and at Trares Road appeared on ODOT's Highway Safety Improvement Program's (HSIP) Priority Locations list, ranking #54 and #53, respectively, on the 2020 rural intersection list.

The purpose of this study is to analyze the existing safety performance of the ranked intersections above and to identify potential countermeasures to reduce crashes and to improve overall safety.

## 3.0 Existing Conditions

#### SR-43 and Randolph Road

The intersection of SR-43 and Randolph Road is unsignalized with traffic operating free flow along SR-43 (northbound/southbound) and stop-controlled along Randolph Road (eastbound/westbound). It is a two-lane road with a speed limit of 45 mph.

Approximately 570 feet north of the intersection with Randolph Road, there is an Advisory Speed sign of 35 mph cautioning for the limited sight distance along SR-43 approaching adjacent intersections. The existing travel lanes are approximately 11 feet wide with five-foot paved shoulders on both sides. There are no pedestrian facilities such as sidewalks, curb ramps, or crosswalks present at the intersection. The cross street, Randolph Road, is one lane in each direction and it does not have paved shoulders. There are dual Stop Signs and Advance Stop Ahead signs located on both legs of Randolph Road at the intersection. The east leg of Randolph is at an approximate 47-degree skew angle while the west leg is at a 26-degree skew angle. The speed limit on Randolph Road is 45 mph. The lanes on Randolph Road are approximately 10 feet wide. There are luminaires present at the intersection.

The north leg of SR-43 has an approximate downgrade of 5.8% to the intersection while the south leg has an approximate downgrade of 5.2% to the intersection. This is notable as downhill grades greater than 3% increase breaking distances. The east and west legs of Randolph Road have an approximate upgrade of 1.0% and 1.3% respectively. The west leg segment is nearly 650 feet in length and terminates at Trares Road, creating a stopcontrolled T-intersection. A sight distance study was completed by ODOT in 2021 and the results show a restricted stopping sight distance (SSD) in the northbound direction. The SSD is approximately 360 feet where the design SSD adjusted for the grade is 470 feet, according to the design standards from the *Location & Design Manual, Volume 1*. The southbound direction of SR-43 does not have sight distance issues based on that study.





Both the eastbound and westbound traffic have restricted intersection sight distance when looking south due to the roadway profile of SR-43. Additionally, sight lines for eastbound traffic are restricted by vegetation when looking north.

SR-43 is classified as a rural principal arterial at its intersection with Randolph Road. The east leg of Randolph is a local road while the west leg is a major collector. Pavement and pavement markings on SR-43 and Randolph Road are in good condition. Based on ODOT's Transportation Information Management Systems (TIMS), the Pavement Condition Rating (PCR) is 94 on SR-43, which is in very good condition. There is no PCR data for the east leg of Randolph Road, while the PCR for the west leg is 81, indicating that it is in good condition.

#### SR-43 and Trares Road

The intersection of SR-43 and Trares Road is unsignalized with traffic operating free flow along SR-43 (northbound/southbound) and stop controlled along Trares Road (eastbound/westbound). The speed limit on both sides of the minor street is 45 mph. Approximately 660 feet south of the intersection with Trares Road, there is an Advisory Speed sign of 35 mph due to the limited sight distance along SR-43 approaching adjacent intersections. The existing travel lanes are approximately 11 feet wide with paved fivefoot shoulders on both sides. Trares Road has one roughly 10 foot lane in each direction and paved shoulders are not present. The north leg of SR-43 has an approximate upgrade of 5.2% to the intersection while the south leg has an approximate upgrade of 2.0% to the intersection. The east leg of Trares Road has an approximate downgrade of 2.0% and the west leg has an approximate upgrade of 3.5%. The 2021 ODOT Sight Distance study shows the southbound direction of SR-43 has a restricted stopping sight distance of 250 feet, well below the design standard of 425 feet. The eastbound and westbound directions have restricted intersection sight distance due to the roadway profile of SR-43 when looking to the north.

SR-43 is classified as a rural principal arterial at its intersection with Trares Road. The east leg of Trares Road is classified as a local road. The west leg of Trares Road is classified as a local road until the T-intersection with Randolph Road, at which point it transitions to a classification of a major collector. On both the eastbound and westbound approaches of the intersection, there are dual stop signs. Pavement and pavement markings on SR-43 and Randolph Road/Trares Road are in good condition. The PCR for SR-43 is 94, which is in very good condition. The PCR for the west leg is 81 up until the T-intersection with Randolph Road, indicating that it is in good condition. There is no PCR data for Randolph Road/Trares Road east of the T-intersection.





The study area is rural in nature due to being surrounded by largely undeveloped land with few homes interspersed. There is existing lighting at both intersections, with one luminaire on utility poles (not high/low mast poles) at each intersection. Suffield Township is an unincorporated community located just southeast of the city of Akron. The existing conditions diagram for the corridor can be found in **Appendix A**, while the sight distance and spot speed data can be found in **Appendix B**.

Figure 1 shows the study area with AADT's calculated from the count data.



#### **Figure 1: Study Area**

A field review was conducted on September 23, 2022. Below is a summary of observations:

• The intersection of SR-43 at Randolph Road has limited sight distance for the minor road approaches. In the summer, large amounts of vegetation can be found on the northeast and northwest corners, which may make it difficult for drivers to determine suitable gaps in traffic to cross or turn from Randolph Road. Large trees and bushes are visible in both corners, while a large sign (not expected to be an encroachment) on the northeast corner is observed in **Photo 1**.





#### Photo 1: Randolph Road Eastbound Approach Looking North (Photo taken 9/23/2022)



- In the summertime, foliage creates additional interference of the sight distance for the minor road approach of SR-43 at Randolph.
- **Photo 2** was taken at the driver's eye level at 17.8 feet offset from the nearest edge line and shows the sight distance at the eastbound approach looking north.





• Looking south from the minor road approaches shows that the intersection sight distance is restricted due to the profile of the roadway, as seen in **Photo 3**.





#### Photo 3: Randolph Road Eastbound Approach Looking North (Photo taken 9/23/2022)



• The SR-43 southbound approach to the intersection with Randolph Road includes an approximately 5.8% downgrade sag curve (**Photo 4**), which may contribute to the observed southbound vehicles' excessive speeds. While the posted speed limit is 45 mph with additional advisory speeds of 35 mph, spot speed data indicated vehicles typically exceeded the posted speed limit on both the northbound and southbound approaches. The speeding vehicles in addition to the high volume of traffic traveling along SR-43 may be contributing to the large number of angle crashes at this intersection.





#### Photo 4: SR-43 at Randolph Road Looking North (Photo taken 9/23/2022)



• The north leg of SR-43 at the intersection with Trares Road includes an approximately 5.2% upgrade crest curve toward the intersection, while the south leg includes a 2.0% upgrade. As observed in **Photo 5**, this grade differential causes a visibility issue, with southbound vehicles disappearing briefly to drivers on the northbound approach.

#### Photo 5: SR-43 at Trares Road Northbound Approach (Photo taken 9/23/2022)







## 4.0 Traffic Volume Development

Turning movement counts were collected at the study intersection on May 4, 2022, from 7 AM – 7 PM. Using the count data, the peak hours were determined to be 7:00-8:00 AM and 4:15-5:15 PM for the corridor. At the intersection of SR-43 at Randolph Road, the daily heavy vehicle traffic accounts for about 5% of the traffic on northbound SR-43, 4% on southbound SR-43, and 2% on eastbound and westbound Randolph. At the intersection of SR-43 at Trares Road, the daily heavy vehicle traffic accounts for about 5% of the traffic accounts for about 5% of the traffic on northbound SR-43, 4% on southbound SR-43, 4% on southbound SR-43, 2% on eastbound Randolph Road, and 4% on westbound Randolph Road.

2022 ODOT Peak Hour to Design Hour factors were applied to the count data. A design hour factor of 1.19 was applied to the AM and PM peak hours to determine the peak design hours for SR-43 (northbound and southbound). For the eastbound and westbound approaches, a design hour factor of 1.10 was applied to both Randolph Road and Trares Road. Annual growth rates of 0.25% were applied to SR-43, while a growth rate of 2% was applied to both Randolph Road and Trares Road. These values were obtained from ODOT's Transportation Data Management System (TFMS). Count data is provided in **Appendix C**.

The count, opening, and design year volumes are shown for the corridor in Figure 2 and Figure 3. Traffic volume calculations are provided in **Appendix C**.



#### Figure 2: SR-43 at Randolph Road Volumes (AM/PM)

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#### Figure 3: SR-43 at Trares Road Volumes (AM/PM)



### 5.0 Crash Data

Crash data, the Crash Analysis Module (CAM) tool, and crash diagrams between 2016 and 2020 were obtained from ODOT. A total of 37 crashes occurred within the study area with three involving serious injuries, eleven involving minor injuries, and five involving possible injuries. This results in an injury rate of 51.3%.

A total of 21 crashes occurred at the intersection of SR-43 & Randolph Road, with one involving serious injuries, four involving minor injuries, and four involving possible injuries. These crashes consisted of 15 angle crashes, three rear end crashes, and two left turn crashes. Failure to yield was the highest contributing factor, accounting for 76% of the crashes. These trends indicate that drivers are accepting a smaller gap in traffic to complete their turns to cross over SR-43.

A total of 16 crashes occurred at the intersection of SR-43 & Trares Road, with two involving serious injuries, seven involving minor injuries, and one involving possible injuries. These crashes consisted of six angle crashes, four rear end crashes, four left turn crashes, one fixed object crash, and one overturning crash. Failure to yield was the highest contributing factor, accounting for 43% of the crashes.







#### Graph 1: Percentage of Crashes by Type Versus Statewide Averages - Randolph Road

Graph 1 shows that at the SR-43 & Randolph Road intersection, all crash types occur more frequently than is typical. **Table 1** shows notable crash statistics for this intersection and **Appendix D** contains the full crash data from the CAM tool. The crash diagram for this intersection is shown in **Figure 4**.

Crashes at the Randolph intersection were slightly higher on weekdays, especially on Tuesday (19%) and Wednesday (19%), but the peak occurred on Friday (24%). The crashes were spread evenly throughout the day with a slight peak from 2:00-3:00 PM. There was a large proportion of crashes in September, with 24% occurring during that month. Failure to yield was the highest contributing factor (76%) of crashes. Failure to yield consisted of fourteen angle crashes and two left turn crashes. Both of the left turn crashes are between a northbound left turning vehicle and a southbound vehicle, indicating drivers were accepting a smaller gap in traffic. Following too closely/assured clear distance ahead (ACDA) was the next most common contributing factor (14%), with all three being rear end crashes. Pavement friction is likely not a significant contributing factor since 81% of the crashes occurred on dry pavement.





## Table 1: Randolph Road Crash Statistics

Hour of Day	Number	%
7	1	5
8	2	10
9	1	5
10	2	10
12	2	10
13	2	10
14	4	19
15	1	5
16	1	5
18	1	5
19	2	10
20	1	5
22	1	5

Crash Month	Number	%
January	2	10
March	4	19
June	2	10
July	3	14
August	1	5
September	5	24
October	3	14
November	1	5

Day of Week	Number	%
Sunday	3	14
Monday	1	5
Tuesday	4	19
Wednesday	4	19
Thursday	1	5
Friday	5	24
Saturday	3	14

Light Condition	Number	%
Daylight	18	85
Dark - Lighted Roadway	1	5
Dark - Roadway Not Lighted	1	5
Dawn/Dusk	1	5

Road Condition	Number	%
Dry	17	81
Wet	4	19

Contributing Factor	Number	%
Failure to Yield	16	76
Following Too Closely/ACDA	3	14
Improper Lane Change	1	5
Ran Stop Sign	1	5

Estimated Speed (mph)	Number	%
<15	12	57
15-19	2	10
20-24	3	14
30-34	2	10
40-44	2	10





#### Figure 4: Crash Diagram: SR-43 at Randolph Road









Graph 2: Percentage of Crashes by Type Versus Statewide Averages – Trares Road

**Graph 2** shows that all crash types at the SR-43 & Trares Road intersection, except fixed object crashes, occur more frequently than is typical. **Table 2** shows notable crash statistics at this intersection and **Appendix D** contains the full crash data from the CAM tool. The crash diagram for this intersection is shown in **Figure 5**. Crashes at this intersection were slightly higher on weekdays, especially on Monday (19%) and Tuesday (19%), but the peak occurred on Saturday (38%). The crashes were spread evenly throughout the day with a slight peak from 6:00-7:00 PM. There was a large proportion of crashes in September, with 25% occurring during that month. Failure to yield was the highest contributing factor (56%) of crashes. Failure to yield consisted of five angle crashes and four left turn crashes. Three of the left turn crashes are from movements from the free-flowing northbound or southbound SR-43, indicating drivers were accepting a smaller gap in traffic. Following too closely/assured clear distance ahead (ACDA) was the next most common contributing factor (19%), with all three being rear end crashes. Pavement friction is likely not a significant contributing factor since 88% of the crashes occurred on dry pavement.





#### **Table 2: Trares Road Crash Statistics**

Hour of Day	Number	%
8	1	6
9	1	6
10	1	6
11	1	6
12	2	13
13	2	13
14	1	6
17	2	13
18	3	19
19	1	6
20	1	6

Crash Month	Number	%
March	1	6
May	2	13
June	1	6
July	2	13
August	2	13
September	4	25
October	2	13
November	2	13

Day of Week	Number	%
Monday	3	19
Tuesday	3	19
Wednesday	2	13
Thursday	2	13
Saturday	6	38

Light Condition	Number	%
Daylight	14	88
Dark - Lighted Roadway	1	6
Dark - Roadway Not Lighted	1	6

Road Condition	Number	%
Dry	14	88
Snow	1	6
Wet	1	6

Contributing Factor	Number	%
Failure to Yield	9	56
Following Too Closely/ACDA	3	19
Improper Lane Change	1	6
Ran Stop Sign	1	6
Other Improper Action	1	6
Improper Start From a Parked Position	1	6

Estimated Speed (mph)	Number	%
<15	11	69
15-19	1	6
35-39	1	6
40-44	1	6
45-49	2	13





#### Figure 5: Crash Diagram: SR-43 at Trares Road



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## 6.0 Existing Transportation Analysis

#### Capacity Analysis

Capacity analysis for the existing conditions was performed in *HCS Version* 2024 for the unsignalized intersections. **Table 3** shows the level of service (LOS) and volume-to-capacity (v/c) ratio thresholds for both unsignalized intersections and roundabouts as published in the *Highway Capacity Manual*.

#### Table 3: HCM LOS Criteria

Loval of Samica	<b>Unsignalized Intersection</b>	Roundabout		
Level of Service	Delay (Seconds)	Delay (Seconds)		
А	≤ 10	≤ 10		
В	> 10 - 15	> 10 - 15		
С	> 15 - 25	> 15 - 25		
D	> 25 - 35	> 25 - 35		
E	> 35 - 50	> 35 - 50		
F	> 50 or V/C ratio > 1.00	> 50 or V/C ratio > 1.00		

Per OATS Section 5.9, an LOS of D for the overall intersection and E for each approach and movement is considered acceptable.

**Table 4** shows the results of the existing 2022 capacity analysis for the study intersections for the AM and PM peak hours.

			AM		PM Peak				
Moven	nent	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	eue LOS Delay (sec) V/C		95 <sup>th</sup> % Queue (feet)	
SR-43 at Randolph	EBLTR	С	23.8	0.12	10	D	28.7	0.24	23
	WBLTR	С	24.7	0.18	16	D	28.1	0.13	13
	NBLTR	А	0.10	0.00	0	А	0.10	0.00	0
Roau	SBLTR	А	0.20	0.00	0	А	0.10	0.00	0
	EBLTR	F	68.4	0.62	80	F	84.4	0.89	180
SR-43 at	WBLTR	Е	37.3	0.36	38	D	25.9	0.15	13
Trares Road	NBLTR	A	2.8	0.12	8	A	1.7	0.06	4
	SBLTR	А	0.4	0.01	0	А	0.40	0.02	0

#### Table 4: 2022 Existing Conditions Results

The unsignalized intersection, SR-43 at Randolph Road, functions in an acceptable manner on the minor street with a LOS D, and functions well on the major street with a





LOS A in both the AM and PM peaks. The v/c ratio is low for SR-43 at Randolph Road in the AM and PM peaks.

The unsignalized intersection, SR-43 at Trares Road, functions in an unacceptable manner on the minor street with an eastbound LOS F in both the AM and PM peaks. In the AM peak, the westbound approach operates poorly at a LOS E while in the PM peak, the westbound approach operates well at a LOS D. The v/c ratio remains low on the major street but has high ratios for the eastbound approach. Full capacity analysis printouts are in **Appendix E**.

**Tables 5 and 6** show the 2027 and 2047 No Build capacity analysis results for the AM and PM design hours.

			AM		PM Peak				
Moven	nent	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)
CD 42 at	EBLTR	С	23.3	0.16	16	D	31.1	0.28	28
SK-43 at	WBLTR	D	25.8	0.22	21	D	28.0	0.17	16
Road	NBLTR	А	0.30	0.01	0	А	0.30	0.01	0
Roau	SBLTR	А	0.40	0.01	0	А	0.30	0.01	0
	EBLTR	F	108.8	0.82	123	F	150.0	1.11	257
SR-43 at	WBLTR	F	56.6	0.53	63	F	51.3	0.35	36
Trares Road	NBLTR	A	3.0	0.13	8	A	1.8	0.07	4
	SBLTR	А	0.40	0.01	0	А	0.50	0.02	2

#### Table 5: 2027 Opening Year No Build Results

For the 2027 model, the intersection of SR-43 at Randolph Road performs in a similar manner to the existing conditions for the major road. The eastbound and westbound approaches perform with acceptable delays, but they have worsened in the five-year forecast, increasing in delay time from a LOS C to LOS D. The northbound and southbound approaches continue to perform well with a LOS A.

The intersection of SR-43 at Trares Road worsened significantly for the minor road with the 2027 model. Both the eastbound and westbound approaches had failing LOS results. The eastbound approach had a v/c ratio approaching 1.0 in the AM peak and it was greater than 1.0 in the PM peak, indicating that it is overcapacity.





			AM	Peak		PM Peak				
Moven	nent	LOS	Delay (sec)	V/C	C 95 <sup>th0</sup> / <sub>0</sub> Queue LOS Delay (sec) V/C		V/C	95 <sup>th</sup> % Queue (feet)		
CD 42 at	EBLTR	D	33.0	0.28	29	E	<b>47.0</b>	0.47	55	
SK-45 at	WBLTR	D	31.0	0.31	34	E	35.9	0.26	26	
Randolph	NBLTR	А	0.30	0.01	0	А	0.30	0.01	0	
Roau	SBLTR	А	0.40	0.01	0	А	0.30	0.01	0	
	EBLTR	F	351.2	1.49	260	F	391.6	1.71	517	
SR-43 at	WBLTR	F	70.2	0.67	95	F	94.4	0.60	69	
Trares Road	NBLTR	A	3.0	0.13	8	A	1.9	0.07	4	
	SBLTR	А	0.40	0.01	0	А	0.50	0.02	2	

#### Table 6: 2047 Design Year No Build Results

For the 2047 model, the intersection of SR-43 at Randolph Road has acceptable delays for the minor street in the AM peak with a LOS D. The PM peak has increased delay times leading to an underperforming LOS of E for the eastbound and westbound approaches. SR-43 continues to perform well in both directions during both peaks.

At the SR-43 and Trares Road intersection, both the eastbound and westbound approaches had failing LOS results for both the AM and PM peaks. Also the v/c ratio is over 1.0 for the eastbound approach, indicating that Trares Road is overcapacity. The northbound and southbound approaches had LOS of A with minimal delay.

#### **Signal Warrant Analysis**

Signal warrant analyses were performed at the study intersections using the standards outlined in the OMUTCD Chapter 4 to investigate if a traffic signal is warranted. Warrant 1 (eight-hour volume threshold), Warrant 2 (four-hour volume threshold), and Warrant 7 (crash experience) were evaluated using the existing volumes and crash data. All other warrants outlined in the OMUTCD are not applicable to the study area. Right turn reductions were applied to the count volumes for both intersections.

Per section 402-3.2 in the Traffic Engineering Manual (TEM), for new ODOT signals, Warrants 1 and 2 shall be based on the 100 percent values in the OMUTCD and right-turn reduction factors, unless there are five or more correctable crashes in one year (that can be corrected with the addition of a signal) and the speed exceeds 40 miles per hour on the major street. If both of the exceptions are applicable, then Warrants 1 and 2 may be based on the 70 percent values combined with engineering judgment and right-turn reduction factors.





#### SR-43 and Randolph Road

Between 2016 and 2020, there were 16 crashes that would be corrected by the installation of a signal at this intersection. However, there is never an instance where five of these crashes occurred within a 12-month period. Therefore, Warrant 1 and Warrant 2 cannot be met with 70% volume thresholds for this intersection.

Warrant 1 is based on 8 hours of traffic meeting the prescribed volume thresholds outlined in the OMUTCD. This warrant can be met if either Condition A or Condition B are satisfied (using 100% of the volumes due to ODOT's requirement for new signals) or if 80% of Condition A <u>and</u> Condition B are satisfied. Condition A requires that SR-43 has a minimum volume of 500 vehicles per hour and Randolph Road has a minimum volume of 150 vehicles for at least 8 hours. Condition B requires that SR-43 has a minimum volume of 750 vehicles per hour and Randolph Road has a minimum volume of 75 vehicles for at least 8 hours. At the 80% volume threshold, S-43 needs a minimum volume of 400 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum volume of 600 vehicles per hour and Randolph Road needs a minimum of 60 vehicles for Condition B. None of the volumes met or exceeded the requirements for either condition, therefore Warrant 1 was not met.

Warrant 2 is based on 4 hours of traffic meeting the volume thresholds shown on Figure 4C-1 of the OMUTCD. Utilizing the 100% volume requirements per ODOT's requirements for new signals, the minimum volume on the major street for both approaches is 400 vehicles per hour. For the four highest volume hours on SR-43, Randolph Road would need a minimum of approximately 310 vehicles for each of those four hours. None of those four hours met the criteria set in Figure 4C-1 of the OMUTCD, therefore the signal warrant is not met.

Warrant 7 (Crash Experience) signal warrant conditions are intended for application where the type and frequency of crashes are the principal reasons to consider installing a traffic control signal. As stated earlier, there was no 12-month period between 2016-2020 where five correctable crashes occurred. Therefore, this warrant was not met.

#### SR-43 and Trares Road

Between 2016 and 2020, there were six crashes that would be corrected by the installation of a signal at this intersection. However, there is never an instance where five of these crashes occurred within a 12-month period. Therefore, Warrant 1 and Warrant 2 cannot be met with 70% volume thresholds for this intersection.





For the intersection of SR-43 at Trares Road, Condition A (100%), Condition B (100%), and Combination A and B (80%) were not met for Warrant 1.

Warrant 2 had two unique hours that met the volume requirements on Figure 4C-1. Warrant 2 requires four unique hours to meet the threshold and as there were only two hours that reached the threshold, a traffic signal remains unwarranted.

As stated earlier, between 2016-2020 there was no 12-month period where 5 or more correctable crashes occurred at this intersection. Therefore, installing a new traffic signal at this location is not warranted based on Warrant 7.

Neither intersection of SR-43 at Randolph Road nor Trares Road met the criteria required for the installation of a traffic signal. The detailed signal warrant analyses are in **Appendix F**.

#### All-Way Stop Control Analysis

All-way stop control was analyzed for both intersections. According to the OMUTCD Section 2B.07, an all-way stop control criteria may be satisfied if it meets any of the listed four requirements. Criterion A is applying an all-way stop control for an intersection where a traffic control signal is warranted, as an interim measure. Criterion B requires five or more reported crashes in a twelve-month period that are susceptible to correction by an all-way stop control installation. Criterion C focuses on minimum volume requirements over eight 1-hour periods and Criterion D allows for a combination of the other criteria being satisfied to 80% of minimum volume requirements.

For the SR-43 & Randolph Road intersection only Criteria B was satisfied due to six crashes occurring between 9/30/2018-9/11/2019 that could possibly be corrected with the installation of all-way stop-control. Therefore, all-way stop-control could be considered for this intersection, but was ultimately dismissed for reasons discussed later in this report.

For the SR-43 & Trares Road intersection only Criteria B was satisfied due to five crashes occurring between 9/20/2016-9/12/2017 that could possibly be corrected with the installation of all-way stop-control. Therefore, all-way stop-control should be considered for this intersection.

The detailed all-way stop control analyses are in Appendix F.

#### Turn Lane Warrant

Turn lane warrant analyses were completed for left and right turn lanes at both intersections. The left turn lane warrant for two-lane high-speed roads is found in the *Location & Design Manual, Volume 1*, Figure 401-5b. This warrant is a function of the





advancing (approach) traffic and the opposing traffic. The right turn lane warrant for two-lane high-speed roads is found in the *Location & Design Manual, Volume 1,* Figure 401-6b. The balanced 2047 design traffic volumes were used in the analyses.

For SR-43 & Randolph Road, a 225' northbound left turn lane, a 225' southbound left turn lane, and a 225' southbound right turn lane are warranted. All turn lane lengths are inclusive of a 50' diverging taper.

For SR-43 & Trares Road, a 245' northbound left turn lane, a 225' southbound left turn lane, and a 225' southbound right turn lane are warranted. All turn lane lengths are inclusive of a 50' diverging taper.

It should be noted that only approximately 300' of space is available between the Randolph Road and Trares Road intersections, so installation of a 225' northbound left turn lane at Randolph Road and a 225' southbound left turn lane at Trares Road is not feasible.

Overall, while turn lanes are warranted at the study intersections, the installation of turn lanes alone will not mitigate the primary crash pattern (angle crashes). Therefore, it is not recommended that installing turn lanes be recommended as a safety improvement, unless the turn lanes are paired with an additional improvement that will mitigate the primary crash pattern.

The detailed turn lane warrant analyses are in Appendix F.

#### **Speed Limit Review**

Section 4511.21 of the Ohio Revised Code sets the statutory speed limit for rural highways at 55 mph, however, speed limits may be altered based on an engineering study. One of the primary factors in the determination of a speed zone is the 85<sup>th</sup> percentile speed that vehicles are currently travelling; it is generally considered to be a safe speed, minimizing crashes, and promoting uniform traffic flow along a corridor. Although a full speed study was not performed, the most recent speed check completed by ODOT in 2021 was reviewed. Based on the data provided, the 50<sup>th</sup> percentile speed ranges between 46 and 48 mph and the pace is between 44-53 mph. The 85<sup>th</sup> percentile speed is between 51 to 52 mph. This indicates the existing 45 mph speed limit on SR-43 is appropriate since the speeds are near the existing speed limit. As a result, a speed reduction is not warranted. The spot speed data is included in **Appendix B**.





## 7.0 Probable Causes

The major crash patterns within the study area are described below:

- **Angle:** Angle crashes are the most prominent type of crash that occurred in the SR-43 corridor, with a total of 21 crashes during the four-year study period. At the intersection of SR-43 at Randolph Road, there were 15 angle crashes. Eleven of the crashes involved southbound and westbound vehicles, three were northbound and eastbound vehicles, and the remaining one was northbound and westbound vehicles. At the intersection of SR-43 at Trares Road, there were six angle crashes. Three of the crashes involved northbound and westbound vehicles, two involved northbound and eastbound vehicles, and the last crash involved a southbound and westbound vehicle. Eighteen of the angle crashes for the corridor had failure to yield as the primary contributing factor and two had running the stop sign as the primary contributing factor. Failure to yield crashes are typically due to drivers having difficulty judging gaps along the mainline. Other possible reasons could include driver inattention, poor judgment, speeding along the major street, and sight distance issues. In past speed samples collected within the study area, it was found that the 85<sup>th</sup> percentile speed was 51 mph for SR-43 between Randolph Road and Trares Road. The posted speed limit for SR-43 is 45 mph with 35 mph advisory signs located before each of the intersections. Additionally, there are considerable issues with sight distance at both intersections. SR-43 at Randolph Road has a vertical curve on the north leg which may have contributed to the high number of angle crashes involving southbound and eastbound/westbound vehicles.
- **Rear End:** Rear end crashes are the second most prominent type of crash that occurred in the SR-43 corridor, with a total of seven crashes during the four-year study period. At the intersection of SR-43 and Randolph Road, there were three northbound rear end crashes. At the intersection of SR-43 and Trares Road, there were three northbound and one eastbound rear end crashes. All seven crashes were approaching the intersections; all had following too closely as the primary contributing factor. It is suspected that the rear end crashes are the result of the lack of turn lanes at the intersections, especially on the free-flow northbound/southbound approaches.
- Left Turn: Left turn crashes are the third most common crash type that occurred along the SR-43 corridor, with a total of six crashes during the five-year study period (2016-2020). At the intersection of SR-43 at Randolph, there were two northbound left turn movement crashes. At the intersection of SR-43 and Trares Road, there were two left turn movement crashes in the northbound direction, one





in the southbound direction, and one in the eastbound direction. All had failure to yield as the primary contributing factor. Crashes at both intersections are most likely due to sight distance issues. For the intersection of SR-43 at Randolph Road, the crossing itself is located in a valley between two hills which limits the sight distance for southbound vehicles especially. Northbound vehicles also have a vertical crest that blocks southbound vehicles north of the intersection, though to a lesser degree than what southbound vehicles contend with at the intersection. At SR-43 and Trares Road, there is an existing vertical dip on SR-43, just north of the intersection. This causes southbound vehicles to be briefly invisible to drivers on the northbound approach of SR-43.

## 8.0 Potential Countermeasures

Angle, rear end, and left turn crashes are the most prominent crash types throughout the corridor, so countermeasures should focus on mitigating these crash types. The following section suggests potential improvements that may reduce the potential for the most common crash types.

#### Short Term

- Add an advance warning sign (W7-6) with advisory speed plaque.
  - At the Randolph Road intersection, the SSD on the northbound approach falls short of the required, grade adjusted distance of 465 feet. The measured SSD is 360 feet, therefore the advisory speed should be 45 MPH, based on ODOT's stopping sight distance table.



- At the Trares Road intersection, the SSD on the southbound approach falls short of the required distance of 425 feet, with a measured SSD of 250 feet. Therefore the advisory speed should be 35 MPH, based on ODOT's stopping sight distance table.
- These signs should be installed in the right-of-way at a distance of 250 feet from the corresponding intersection.
- Convert both intersections from a two-way stop control to an all-way stop control (AWSC).

#### Long Term

• Alternative 1: Construct single-lane roundabouts for both SR-43 at Randolph Road and Trares Road.





- Note: constructing a peanut roundabout was considered, but had no apparent benefit compared to two single-lane roundabouts.
- Alterative 2: Install a median at the Randloph Road intersection to restrict eastbound/westbound left and through movements, as well as northbound/southbound left turn movements. This also includes constructing a northbound right turn lane at Randloph Road and a single-lane roundabout at SR-43 & Trares Road.
  - Note: adding cul-de-sacs on the east and west legs of the Randloph Road intersection was considered, but installing a median is expected to provide similar safety benefits while reducing costs and right-of-way impacts.

#### All-Way Stop-Control

Capacity analysis for the all-way stop-control countermeasure is shown in **Tables 7 and 8**. Full capacity results for the all-way stop-control countermeasure are in **Appendix G**.

Movement			AM	Peak		PM Peak			
		LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)
	EBLTR	А	9.9	0.07	5	В	10.4	0.10	8
SR-43 at Randolph	WBLTR	В	10.1	0.09	8	В	10.2	0.06	5
	NBLTR	D	32.6	0.89	294	С	19.8	0.72	156
Road	SBLTR	В	14.4	0.57	93	E	43.9	0.95	361
	Overall	С	24.5			D	32.3		
	EBLTR	В	11.1	0.18	15	В	14.1	0.39	48
CD 42 at	WBLTR	В	10.8	0.14	13	В	11.4	0.09	8
SK-43 at	NBLTR	F	82.5	1.09	550	D	33.1	0.85	238
Trafes Road	SBLTR	С	16.0	0.59	101	F	86.9	1.09	513
	Overall	F	53.6			F	55.2		

#### Table 7: 2027 Opening Year AWSC Intersections Results

The 2027 HCS model shows a general decline in the operation of both intersections.

For SR-43 at Randolph Road, the eastbound and westbound directions have improved LOS in comparison to the 2027 No Build. The v/c ratios and queue lengths remain low. In contrast, the northbound and southbound directions worsen from a LOS A to a LOS C through F. In addition, the delay times are much longer due to the conversion of the free-flow approach to a stop-control approach. The v/c ratio approaches 1.0 and there are now queue lengths as compared to none in the No Build condition. The intersection





performs in an acceptable manner with a LOS C in the AM peak and LOS D in the PM peak.

For SR-43 at Trares Road, the eastbound and westbound directions have improved from failing LOS F in the No Build to a LOS B for both the AM and PM peaks. The v/c ratios and queue lengths remain low. The northbound and southbound directions worsen from a LOS A to a LOS range from C through F. The v/c ratio is greater than 1.0 in the northbound AM peak and the southbound PM peak, indicating the intersection is overcapacity. The overall intersection fails to perform with long delay times and significant queuing northbound and southbound. Note, the southbound queues are expected to extend past the next upstream intersection.

Movement			AM		PM Peak				
		LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)
	EBLTR	В	10.6	0.09	8	В	11.0	0.14	13
SR-43 at	WBLTR	В	10.7	0.12	11	В	10.6	0.08	8
Randolph	NBLTR	F	51.0	0.98	406	D	25.7	0.80	207
Road	SBLTR	С	16.2	0.61	108	F	66.7	1.04	470
	Overall	E	35.7			E	46.0		
	EBLTR	В	12.1	0.25	25	С	19.0	0.57	88
CD 42 at	WBLTR	В	11.6	0.19	18	В	12.6	0.14	13
SK-43 at	NBLTR	F	116.3	1.18	671	F	50.9	0.94	315
Trafes Road	SBLTR	С	18.5	0.64	120	F	157.6	1.27	729
	Overall	F	71.0			F	91.4		

#### Table 8: 2047 Design Year AWSC Intersections Results

The 2047 HCS model behaves in a similar way to the 2027 HCS model.

For SR-43 at Randolph Road, the eastbound and westbound directions improve from a range of LOS D through F to a LOS B. The delay times are greatly reduced, while the v/c ratios and queue lengths remain low. The northbound and southbound directs were formerly at a LOS A due to the free-flow traffic, but have now worsened to a range of LOS C through F. The v/c ratios greatly increase, with the northbound AM peak and southbound PM peak exceeding 1.0, leading to overcapacity conditions. The overall LOS deteriorated to an E in the AM peak and PM peak.

For SR-43 at Trares Road, the eastbound and westbound movements have improved upon the No Build condition, with scores of LOS B and C. The v/c ratios are significantly lower and the queue lengths are shorter. The reverse is true for the northbound and





southbound movements. All movements fail in the AM and PM peaks with the exception of the southbound AM peak having a LOS C. The v/c ratios and queue lengths are much higher than the No Build condition. The overall LOS for both AM and PM peaks is unacceptable at an F.

Converting the SR-43 intersections with Randolph Road and Trares Road from two-way stop-control to all-way stop-control is not expected to significantly increase vehicular and EMS travel times, as all movements that currently exist at the intersections will be retained.

Stopping sight distance analyses were conducted for both intersections due to concerns about installing a stop-controlled condition for SR-43 traffic in the presence of vertical curvature. Since SR-43 has a posted speed limit of 45 MPH, a stopping sight distance of 360' was utilized for this analysis. For the Trares Road intersection, it was determined that both southbound and northbound traffic would be able to see the stop sign. However, it is expected that the vertical curvature south of the Trares Road intersection would hide, or shadow, a vehicle stopped at the stop-sign, which may lead to rear-end crashes. Additionally, it is expected that southbound vehicles at the Randolph Road intersection would be unable to see vehicles stopped at the stop sign due to the vertical curvature north of Randolph Road.

It is advised that an all-way stop control be disregarded as a countermeasure to improve the operation and safety of these intersections due to the excessively long queues and the overcapacity conditions it creates on SR-43. Additionally, installing an all-way stop control at both intersections will most likely lead to an increase in rear end crashes as SR-43 had previously been free-flowing and has a hill between the two intersections with limited sight distance. The stopping sight distance exhibits can be seen in **Appendix G**.

#### Alternative 1

The capacity analysis for the long-term countermeasure, Alternative 1 is shown in **Tables 9 and 10**.





Movement			AM	Peak		PM Peak				
		LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	
	EBLTR	А	4.6	0.04	3	Α	6.2	0.08	5	
SR-43 at Randolph Road	WBLTR	А	6.6	0.08	5	Α	5.0	0.04	3	
	NBLTR	А	8.6	0.05	83	Α	6.7	0.40	51	
	SBLTR	А	5.8	0.32	36	А	8.7	0.54	86	
	Overall	А	7.4			А	7.7			
SR-43 at Trares Road	EBLTR	Α	4.8	0.11	10	Α	9.1	0.31	33	
	WBLTR	А	7.6	0.12	10	Α	5.4	0.06	5	
	NBLTR	В	10.8	0.62	117	Α	7.8	0.45	61	
	SBLTR	А	7.2	0.37	44	Α	9.4	0.56	91	
	Overall	A	9.1			A	8.7			

#### Table 9: 2027 Design Year Alternative 1 Results

The 2027 HCS model for single-lane roundabouts at both intersections shows positive results. All movements have a LOS B or better, with minimal delay times and v/c ratios well below 1.0. The 95<sup>th</sup> percentile queue lengths are shorter for the eastbound and westbound movements compared to the No Build and the overall LOS is an A for both intersections in both peaks.

#### Table 10: 2047 Design Year Alternative 1 Results

Movement			AM	Peak		PM Peak				
		LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	
SR-43 at Randolph Road	EBLTR	А	4.8	0.06	5	Α	6.8	0.11	10	
	WBLTR	А	7.3	0.10	8	А	5.4	0.06	5	
	NBLTR	А	9.6	0.57	99	А	7.4	0.44	89	
	SBLTR	А	6.1	0.34	39	А	9.3	0.57	97	
	Overall	А	8.1			А	8.3			
SR-43 at Trares Road	EBLTR	Α	5.3	0.15	13	В	11.9	0.44	58	
	WBLTR	В	8.5	0.17	15	Α	5.9	0.09	8	
	NBLTR	В	11.6	0.65	130	Α	8.5	0.48	67	
	SBLTR	A	7.5	0.39	47	В	10.1	0.59	104	
	Overall	В	9.6			В	9.8			

The 2047 HCS model for single-lane roundabouts at both intersections shows positive results. All movements have a LOS B or better, with minimal delay times and v/c ratios





well below 1.0. The 95<sup>th</sup> percentile queue lengths are shorter for the eastbound and westbound movements compared to the No Build and the overall LOS is an A for the Randolph Road intersection and LOS B for the Trares Road intersection in both peaks.

The conversion from a two-way stop-controlled intersection to a roundabout appears to have positive effects on the operation of the intersection; however, consideration must be taken regarding the elevation difference in the area. There is a hill on the north leg of SR-43 at Randolph Road, which may cause increased speeds on the southbound approach going into the proposed roundabout. The crest of the hill is approximately 550' beyond the tie-in point for the north leg of the roundabout. The 95<sup>th</sup> percentile queue on the southbound approach is 97' in the Design Year PM peak. The cost estimate for this proposed project assumed grades will be improved as much as possible within the limits of the proposed roundabout and legs. If this countermeasure is to be considered, additional signage, enhanced pavement markings, lighting, and other additional traffic calming features should be evaluated during design.

This alternative is expected to have minimal impact on the surrounding properties at Trares Road/Randolph Road with the exception of some driveway relocations. Considering the Randolph intersection, it is likely the construction of a roundabout will require a partial or full take of the residential property at the northwest corner.

Converting the SR-43 intersections with Randolph Road and Trares Road from two-way stop-control to roundabouts is not expected to significantly increase local traffic or EMS travel times, as all movements that currently exist at the intersections will be retained.

#### Alternative 2

A signal warrant was performed at SR-43 & Trares Road assuming that traffic from the Randolph Road intersection would be rerouted to the Trares Road intersection due to restricted movements caused by the median. The results of the signal warrant analysis show that neither Warrant 1 nor Warrant 2 were met with the rerouted volumes.

Per the Intersection Control Evaluation (ICE) methodology, CAP-X was utilized to determine the best control type for the Trares Road intersection with the rerouted volumes. Since the signal warrants are not met for the Trares Road intersection, it was not included in the CAP-X analysis.

The CAP-X analysis evaluated two-way stop-control, all-way stop-control, and a singlelane roundabout. Since all-way stop-control was previously analyzed and showed failing levels of service before the additional rerouted traffic was added to the Trares Road intersection, it was concluded that all-way stop-control would not be an acceptable traffic control type for this alternative. It was determined that a single-lane roundabout was the





best control type option for the Trares Road intersection, as it is the only intersection type that provides a v/c ratio of less than 1.0.

The capacity analysis for the long-term countermeasure, Alternative 2 is shown in **Tables 11 and 12**.

Movement		AM Peak				PM Peak				
		LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	
SR-43 at Randolph Road	EBR	В	10.7	0.02	3	В	13.2	0.02	3	
	WBR	В	13.1	0.03	3	В	11.3	0.02	3	
SR-43 at Trares Road	EBLTR	А	5.2	0.13	13	В	10.3	0.37	43	
	WBLTR	А	8.6	0.19	18	Α	6.0	0.09	8	
	NBLTR	В	11.7	0.64	130	Α	8.5	0.47	67	
	SBLTR	A	7.8	0.39	49	В	10.0	0.58	99	
	Overall	A	9.7			A	9.4			

#### Table 11: 2027 Design Year Alternative 2 Results

The 2027 HCS model for a two-way stop-control with restricted movements at Randolph and a single-lane roundabout at Trares shows positive results. All movements have a LOS B or better, with minimal delay times and v/c ratios well below 1.0. The 95<sup>th</sup> percentile queue lengths are shorter for the eastbound and westbound movements at Trares Road compared to the No Build.

#### Table 12: 2047 Design Year Alternative 2 Results

Movement		AM Peak				PM Peak				
		LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	LOS	Delay (sec)	V/C	95 <sup>th</sup> % Queue (feet)	
SR-43 at Randolph Road	EBR	В	10.8	0.02	3	В	13.6	0.02	3	
	WBR	В	13.8	0.03	3	В	11.8	0.02	3	
SR-43 at Trares Road	EBLTR	А	5.8	0.19	18	В	14.5	0.54	83	
	WBLTR	В	10.2	0.27	28	Α	6.9	0.14	13	
	NBLTR	В	13.0	0.68	146	Α	9.6	0.51	77	
	SBLTR	A	8.3	0.41	52	В	11.1	0.62	114	
	Overall	В	10.6			В	11.1			





The 2047 HCS model for a two-way stop-control with restricted movements at Randolph and a single-lane roundabout at Trares shows positive results. All movements have a LOS B or better, with minimal delay times and v/c ratios well below 1.0. The 95<sup>th</sup> percentile queue lengths are shorter for the eastbound and westbound movements at Trares compared to the No Build and the overall LOS is B for the Trares Road intersection in both peaks.

Right turn lane warrant analyses were completed at the SR-43 & Randolph Road intersection to see if the warrants changed with the rerouted volumes. The analysis shows that a 245' northbound right turn lane and a 225' southbound right turn lane are warranted with rerouted volumes. In consideration that vehicle speeds are lower immediately downstream of a roundabout, a low-speed (less than or equal to 40 MPH) northbound right turn lane warrant was also conducted. The results show that a 150' northbound right turn lane is warranted. All turn lane lengths are inclusive of a 50' diverging taper. Due to the proximity of the Trares Road intersection, the expected lower speeds immediately downstream of a roundabout, the rerouted volumes result in a higher volume of vehicles making a northbound right movement at Randolph Road it is recommended that a 150' northbound right turn lane be installed at the Randolph Road intersection, since. It is not recommended that the 225' southbound right turn lane be installed, as that movement is not expected to experience any changes in volumes. The detailed turn lane warrant analyses are in **Appendix F**.

Eastbound right turning vehicles at Randolph Road can have acceptable sight lines as long as vegetation on the northwest corner of the Randolph Road intersection is properly maintained.

Unless grading is performed on SR-43 to flatten the roadway profile of SR-43 between the two study intersections, the westbound right turning vehicles at Randolph Road will still have restricted sight lines. However, it is expected that vehicles exiting the proposed roundabout at Trares Road would be at a lower speed than the posted speed limit of 45 MPH, thereby potentially decreasing the required intersection sight distance for westbound right turning vehicles at Randolph Road. It is recommended that this be further investigated during detailed design.

Alternative 2 is expected to have minimal impact on the surrounding properties at Trares Road with the exception of some drive relocations. The construction of a mountable median at the Randolph intersection will minimally impact adjacent residential properties.

Restricting access to SR-43 via a mountable median at the Randolph Road intersection is





expected to increase vehicular and EMS travel times. However, by utilizing Google Maps, the increase in travel time is expected to be minimal with the reroute.

An example of this difference can be seen in the photos below. **Photo 6** shows the current travel time (approximately 5:30 PM on a Wednesday in October) from the Summa Akron City Hospital, located west of the study area in Akron, to a business located on the east leg of Randolph Road. **Photo 7** shows the new route that would be taken to reach the same location. It is not expected to add any additional time to the EMS travel time if the eastbound through movement were restricted at the Randolph Road intersection. A similar result was found at 8:00 AM on a Thursday.

#### Photo 6: Current Travel Time



#### Photo 7: Proposed Travel Time



Another example of this difference can be seen in the photos below. **Photo 8** shows the current travel time (approximately 5:30 PM on a Wednesday in October) from the Suffield Township Fire Station, located south of the study area, to a residential house located on the west leg of Randolph Road. **Photo 9** shows the new route that would be taken to reach the same location. It is expected to add approximately one minute to the travel time if the





northbound left movement were restricted at the Randolph Road intersection. A similar result of a one-minute addition to the travel time was found at 8:00 AM on a Thursday.

#### Photo 8: Current Travel Time



#### Photo 9: Proposed Travel Time



The movement that will be impacted the most from this change is the current westbound left-turning vehicles, which are expected to be mostly local drivers. **Photo 10** shows the current travel time (approximately 5:30 PM on a Wednesday in October) from a residential road on the east leg of the Randolph intersection to Suffield Elementary School, located south of the study area. **Photo 11** shows the new route that would be taken to reach the same location. It is expected to add approximately four minutes to the travel time if the westbound left movement were restricted at the Randolph Road intersection. A similar result of a five-minute addition to the travel time was found at 8:00 AM on a Thursday.





#### Photo 10: Current Travel Time



#### Photo 11: Proposed Travel Time



## 9.0 Safety Benefits

The Highway Safety Manual (HSM) is used to determine how a corridor is performing compared to similar corridors and to assess the safety benefit of countermeasures. ODOT's Economic Crash Analysis Tool (ECAT) was used to evaluate both the existing corridor and the proposed long-term countermeasures.

Crash modification factors (CMF) are used in ECAT to calculate the reduction in crashes for each countermeasure. For example, a CMF of 0.85 reduces crashes by 15%. Not all countermeasures have been studied adequately enough to provide a CMF value. The CMF values used for each scenario are listed below. To avoid overestimating the value of the combined countermeasures, ODOT recommends that no more than four CMF values should be used per scenario.




### Short Term

- Install "Hill Blocks View" (W7-6) sign: No CMF was applied for this countermeasure. However, this countermeasure is expected to reduce rear end crashes as drivers may potentially reduce their speeds and/or enhance their situational awareness which could improve their reaction time.
  - According to the OMUTCD Table 2C-4, the advance placement of warning signs should be located approximately 250 feet from the intersection. The 85<sup>th</sup> percentile speed on SR-43 is 51 mph and the Condition B deceleration is 0 mph.
  - Two signs should be installed: one on each mainline approach of SR-43 at Randolph Road. The northbound advisory speed should be 35 MPH and the southbound advisory speed should be 45 MPH, according to ODOT's stopping sight distance standards.
  - These countermeasures were not analyzed in ECAT due to the lack of applicable CMFs.

### Long Term: Alternative 1

• Convert both intersections from a minor-road stop control to single-lane roundabouts: No direct CMF was applied. Instead, the intersections were analyzed directly in the ECAT by changing the site type to a roundabout.

### Long Term: Alternative 2

- Restrict movements at the intersection at SR-43 and Randolph Road to rightin/right-out (RIRO): A CMF of 0.20 for fatal and serious injury crashes and 0.32 for all other crashes was applied. These CMFs were found on the CMF Clearinghouse and are provided in **Appendix H**.
- Construct a northbound right turn lane at SR-43 and Randolph Road: No direct CMF was applied. Instead, the intersections were analyzed directly in the ECAT by changing the proposed conditions to include a right turn lane.
- Construct a single lane roundabout at SR-43 and Trares Road: In a similar manner to Alternative 1, no direct CMF was applied.

**Table** 13 shows how the existing corridor ( $N_{expected\_existing}$ ) compares to similar corridors ( $N_{predicted\_existing}$ ) and the proposed conditions ( $N_{predicted\_proposed}$ ). From the table, the study area is functioning worse than its peers for injury type crashes. For the proposed scenarios, only the CMFs listed for each scenario above are used, i.e. the long-term



predicted crashes do not include CMFs for the short-term countermeasures. Full HSM results are included in **Appendix H**.

	KA	В	C	0	Total
${f N}_{predicted}$ - Existing Conditions	0.4736	1.1505	0.7602	4.0919	6.4762
$\mathbf{N}_{ extbf{expected}}$ - Existing Conditions	0.5335	1.2954	0.8573	3.8484	6.5346
$\mathbf{N}_{ ext{potential}}$ for improvement – Existing Conditions	0.0599	0.1449	0.0971	-0.2435	0.0584
Nexpected - Proposed Conditions, Alt. 1 Roundabout	0.0255	0.1416	0.1510	2.8440	3.1621
Nexpected - Proposed Conditions, Alt. 2 RIRO Randolph/Roundabout Trares	0.0352	0.1524	0.1300	1.8350	2.1526

### **Table 13: HSM Results Summary**

Based on the ECAT calculations, the long-term Alternative 1 countermeasures are expected to reduce the number of crashes per year by about 3.37 crashes compared to the existing conditions. The long-term Alternative 2 countermeasures are expected to reduce the number of crashes per year by about 4.38 crashes per year. Note, the CMFs applied for the roundabout installations are not necessarily comparable to the CMF applied for the RIRO installation. It is expected that installing a RIRO at the Randolph Road intersection will mitigate more crashes than a roundabout installation at this intersection.





### **10.0** Conclusions and Recommendations

A benefit cost analysis was prepared using the ECAT tool to compare the estimated cost of the long-term countermeasures to their respective safety benefit. Benefit cost ratios greater than 1.00 indicate a positive return on the investment. The results of the benefit cost analysis are shown in **Table 14**. Full calculations and detailed cost estimates are in **Appendix I**.

### **Table 14: Benefit Cost Analysis**

	Long Term Alt. 1	Long Term Alt. 2
Expected Annual Crash Adjustment	-3.314	-4.324
Net Present Value of Project	\$5,933,217.10	\$3,696,477.20
Net Present Value of Safety Benefit	\$4,558,661.83	\$4,494,271.66
Benefit Cost Ratio	0.77	1.22

The benefit-cost (b/c) ratio for Alternative 2 is favorable since it is above the threshold value of 1.00. Alternative 1 has an unfavorable b/c ratio of 0.77.

Alternative 2 is recommended because it is expected to mitigate crash issues at both intersections at a lower cost than Alternative 1. The median on SR-43 would eliminate angle and left turn crashes, with minimal increases in travel time. Additionally, Alternative 1 is expected to require more right-of-way, thus having a greater impact on the surrounding private properties. The roundabout on Trares Road is expected to improve capacity, which would reduce rear-end crashes. The roundabout is also expected to have a significant impact on the angle and left turn crashes occurring at this intersection.

See **Figure 6** and **Figure 7** for the long-term concept plans. See **Appendix I** for roundabout dimensions, critical design parameters, and truck turns through the roundabout. Note, the design is conceptual and will be further refined during detailed design when survey data is available.



### **Figure 6: Long Term Alternative 1**







### Figure 7: Long Term Alternative 2





## Appendix A Existing Conditions Diagram









repared by AFL
ssued by DEG



EXISTING CONDITIONS AS OF JUNE 2022

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### POR SR 43 AT TRARES AND RANDOL

A4 of 5

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	PREPARED BY
PH RD	ISSUED BY



### Appendix B Sight Distance and Spot Speed Studies



### **Sight Distance Study**



\*Label road names and draw north arrow. Draw in neighboring drives with distances if necessary. Describe what is blocking the sight distance such as vegetation, pavement on hill crest, etc.

Notes/Recommendations:	Desig
EB traffic stopped at 17', 17', 24', 9', and 14'.	DEDIO
All traffic squared up to intersection.	SPEE
ISD (555') Looking north restricted by vegetation/ Looking south restricted by roadway profile	(mph)
	20
WB traffic stopped at 17 and 10.	25
All traffic squared up to intersection.	30
	35
ISD (555') Looking north not restricted / Looking south restricted by roadway profile	40
SB SSD (425') adjusted for grade = $475'$ (Not Restricted)	45
	50
NB SSD (425') adjusted for grade = 470' (Restricted)	55
	60

	Design standards from L & D Manual (Vol 1,														
	Sect Rev July 2013)														
-	DESIGN SPEED (mph)	SSD (fig 201-1E)	ISD for passenger car turning left (Fig	ISD for passenger car turning right or crossing											
			201-5E)	(Fig 201-5E)											
-	20	115'	225'	195'											
_	25	155'	280'	240'											
	30	200'	335'	290'											
-	35	250'	390'	335'											
_	40	305'	445'	385'											
	45	360'	500'	430'											
-	50	425'	555'	480'											
_	55	495'	610'	530'											
	60	570'	665'	575'											

### **Sight Distance Study**



\*Label road names and draw north arrow. Draw in neighboring drives with distances if necessary. Describe what is blocking the sight distance such as vegetation, pavement on hill crest, etc.

### Notes/Recommendations:

EB traffic stopped at 17', 14', 14', 17' and 25'.
All stopping traffic squared up to the stop intersection.
ISD (555') Looking north restricted by roadway profile / Looking south not restricted
WB traffic stopped at 20' and 14'.
ISD (555') Looking north restricted by roadway profile / Looking south not restricted
SSD (425') not adjusted for grade - NB not restricted / SB restricted

Design s	tandards fro	m L & D Ma	anual (Vol 1,											
Sect Rev July 2013)														
DESIGN SPEED (mph)	SSD (fig 201-1E)	ISD for passenger car turning left (Fig 201-5E)	ISD for passenger car turning right or crossing (Fig 201-5E)											
20	115'	225'	195'											
25	155'	280'	240'											
30	200'	335'	290'											
35	250'	390'	335'											
40	305'	445'	385'											
45	360'	500'	430'											
50	425'	555'	480'											
55	495'	610'	530'											
60	570'	665'	575'											

FORM 1296-5

### SPEED CHECK

COUNTY:	POR	R(		43	SLM:	3	3.93 L	OCATIC	N: SR 4	43 at Randolph R	d			
PAVEMENT	TYPE:	ASPH	AULT	DRY:	WET:	х	CONDITIC	ON:	Good	LANE WIDTH:	11'	NO. OF LANES	: 2	_
DATE:	11/12/	2021	DAY:	Frida	ay	v	VEATHER:		C	Clear	TE	MPERATURE:	39	
OBSERVE	<b>R:</b> K.	Kubus,	J. Durb	in										

North BOUND TIME: 8:15 AM TO 8:45 AM South BOUND TIME: 8:15 AM TO 8:45 AM MPH CUM. CUM. CUM. CUM. NO. VEHICLES VEHICLES NO. ΤΟΤΑ ΤΟΤΑ % % ≥ 66 100% 100% 98% 98% 97% 93% 88% 88% 86% 83% 77% 76% 74% 63% 73% 56% 64% 39% 53% 34% 39% 25% 30% 14% 7% 20% 3% 15% 9% 8% 2% 3% 2% ≤ 20 TOTALS 50<sup>TH</sup> %: 46 MPH 85<sup>TH</sup> %: **51** MPH PACE: 44 - 53 MPH 50<sup>TH</sup> %: 48 MPH 85<sup>TH</sup> %: **51** MPH PACE: 44 - 53 MPH

FORM 1296-5

### SPEED CHECK

COUNTY:	POR	R		43	SLM:	3	3.87 L	OCATIO	N: SR 4	43 at Trares Rd				
PAVEMENT	TYPE:	ASPH	AULT	DRY:	WET:	х	CONDITIO	ON:	Good	LANE WIDTH:	11'	NO. OF LANES	:	2
DATE:	11/12/	2021	DAY:	Frida	ау	v	VEATHER:		С	lear	TE	MPERATURE:	41	
OBSERVE	<b>R:</b> K.	Kubus,	J. Dubr	in										

North BOUND TIME: 7:40 AM TO 8:10 AM South BOUND TIME: 7:40 AM TO 8:10 AM MPH CUM. CUM. CUM. CUM. NO. VEHICLES VEHICLES NO. TOTA ΤΟΤΑ % % ≥ 66 100% 100% 98% 99% 97% 97% 92% 93% 87% 90% 79% 85% 69% 72% 59% 66% 49% 48% 39% 28% 23% 20% 16% 14% 7% 4% 1% 3% ≤ 20 TOTALS 50<sup>TH</sup> %: 47 MPH 85<sup>TH</sup> %: **51** MPH PACE: 44 - 53 MPH 50<sup>TH</sup> %: 47 MPH 85<sup>TH</sup> %: **50** MPH PACE: 44 - 53 MPH

## Appendix C Count Data and Volume Calculations



POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Lights

									Gr	oups Printed	d- Lights										
			SR-43				Ra	andolph I	Rd				SR-43								
		So	outhboun	nd		Westbound					Northbound										
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
07:00 AM	1	39	1	0	41	0	5	1	0	6	0	100	1	0	101	1	1	0	0	2	150
07:15 AM	0	49	2	0	51	2	9	3	0	14	1	109	0	0	110	0	0	2	0	2	177
07:30 AM	4	71	0	0	75	0	2	0	0	2	2	137	0	0	139	1	2	7	0	10	226
07:45 AM	7	76	0	0	83	0	3	2	0	5	3	69	1	0	73	2	0	3	0	5	166
Total	12	235	3	0	250	2	19	6	0	27	6	415	2	0	423	4	3	12	0	19	719
08:00 AM	1	44	0	0	45	0	6	4	0	10	0	54	1	0	55	0	2	1	0	3	113
08:15 AM	0	51	1	1	53	2	4	1	0	7	2	62	0	0	64	0	0	0	0	0	124
08:30 AM	5	42	0	0	47	0	0	1	0	1	3	80	0	0	83	2	1	1	0	4	135
08:45 AM	2	47	0	0	49	1	1	1	0	3	2	72	0	0	74	0	0	1	0	1	127
Total	8	184	1	1	194	3	11	7	0	21	7	268	1	0	276	2	3	3	0	8	499
1					1										1						
09:00 AM	5	36	0	0	41	0	6	1	0	7	0	56	0	0	56	0	1	0	0	1	105
09:15 AM	2	37	0	0	39	1	3	0	0	4	0	43	0	0	43	1	0	0	0	1	87
09:30 AM	2	40	1	0	43	0	2	3	0	5	4	44	0	0	48	0	1	0	0	1	97
09:45 AM	2	42	0	0	44	1	2	1	0	4	2	50	0	0	52	0	2	1	0	3	103
Total	11	155	1	0	167	2	13	5	0	20	6	193	0	0	199	1	4	1	0	6	392
					1					- 1					1		_				
10:00 AM	8	44	0	0	52	1	2	0	0	3	2	50	1	0	53	1	3	0	0	4	112
10:15 AM	2	50	0	0	52	0	3	0	0	3	0	47	0	0	47	0	2	0	0	2	104
10:30 AM	4	45	0	0	49	0	4	3	0	7	3	44	0	0	47	0	1	5	0	6	109
10:45 AM	6	33	1	0	40	0	3	4	0	7	3	46	0	0	49	0	0		0	0	96
I otal	20	172	1	0	193	1	12	7	0	20	8	187	1	0	196	1	6	5	0	12	421
11.00 414	-	50	0	0	<b>F7</b>		-		•	-	0			0		0	0		0	0	
11:00 AM	5	50	2	0	57	1	5	I	0	/	2	41	1	0	44	2	3	1	0	6	114
11:15 AM	2	40	0	0	42	0	3	0	0	3	1	50	0	0	51	0	1	5	0	6	102
11:30 AM	/	49	0	0	56	0	4	0	0	4	2	40	0	0	42	2	1	2	0	5	107
11:45 AM	0	37	0	0	37	1	4	2	0	/	3	54	0	0	5/	0	4	1	0	5	106
Iotal	14	176	2	0	192	2	16	3	0	21	8	185	1	0	194	4	9	9	0	22	429
10:00 DM	F	60	0	0	74	0	0	-	0	2	4	20	0	0	40	4	0	4	0	4	104
12:00 PM	5	69	0	0	74	0	2	1	0	3	4	39	0	0	43	1	2	1	0	4	124
12:15 PM	/	36	0	0	43		0	0	0	1	1	52	0	0	53	0	3	3	0	6	103
12:30 PM	2	53	0	0	55	1	3	2	0	6	2	48	0	0	50	0	I	5	0	6	117
12:45 PM	3	52	0	0	55	0	2	0	0	2	5	49	0	0	54	1	4	2	0	/	118
Iotal	1/	210	0	0	227	2	1	3	0	12	12	188	0	0	200	2	10	11	0	23	462
	0	46	0	0	40	4	0	0	0		0	FC	0	0	EO	0	0	~	0	4	110
	3	40	0	0	49	1	2	3	0	6	<u>র</u>	00 70	0	0	59	0	2	2	0	4	118
	9	51	0	0	60	1	5	0	0	6	2	/3	2	0	11	0	3	5	0	8	101
01:30 PM	9	51	U	U	60	1	3	3	0	1	1	65	U	0	66	U	2	3	U	5	138

Akron, OH 44306

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Lights

									Gr	oups Printer	d- Lights											
			SR-43			Randolph Rd SR-43											Randolph Rd					
		S	Southbound Westbound Northbound							Eastbound												
Start Time	e Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total	
01:45 PM	5	47	0	0	52	0	5	0	0	5	3	51	1	0	55	0	2	2	0	4	116	
Tota	1 26	195	0	0	221	3	15	6	0	24	9	245	3	0	257	0	9	12	0	21	523	
02:00 PM	5	61	0	0	66	1	3	2	0	6	4	55	2	0	61	1	4	1	0	6	139	
02:15 PM	2	73	0	0	75	1	1	2	0	4	1	75	1	0	77	1	6	6	0	13	169	
02:30 PM	11	77	1	0	89	1	0	0	0	1	3	78	2	0	83	0	1	6	0	7	180	
02:45 PM	8	89	0	0	97	0	6	1	0	7	3	67	0	0	70	2	2	5	0	9	183	
Tota	1 26	300	1	0	327	3	10	5	0	18	11	275	5	0	291	4	13	18	0	35	671	
03:00 PM	11	114	3	0	128	0	1	3	0	4	7	59	1	0	67	4	3	5	0	12	211	
03:15 PM	4	87	0	0	91	0	2	2	0	4	7	77	0	0	84	0	3	2	0	5	184	
03:30 PM	7	89	0	0	96	0	1	1	0	2	8	65	0	0	73	1	11	1	0	13	184	
03:45 PM	14	104	1	0	119	0	5	3	0	8	5	95	1	0	101	0	4	3	0	7	235	
Tota	36	394	4	0	434	0	9	9	0	18	27	296	2	0	325	5	21	11	0	37	814	
04:00 PM	7	86	0	0	93	1	1	0	0	2	1	90	0	0	91	0	8	2	0	10	196	
04:15 PM	5	148	0	0	153	1	1	1	0	3	5	74	1	0	80	3	5	1	0	9	245	
04:30 PM	8	111	0	0	119	0	4	1	0	5	6	101	1	0	108	4	5	4	0	13	245	
04:45 PM	3	135	2	0	140	0	5	1	0	6	4	90	0	0	94	0	6	1	0	7	247	
Tota	23	480	2	0	505	2	11	3	0	16	16	355	2	0	373	7	24	8	0	39	933	
05:00 PM	7	127	0	0	134	1	1	4	0	6	5	101	1	0	107	0	9	5	0	14	261	
05:15 PM	3	113	3	0	119	2	2	1	0	5	8	93	1	0	102	3	4	4	0	11	237	
05:30 PM	10	96	1	0	107	0	9	2	0	11	5	85	0	0	90	2	6	1	0	9	217	
05:45 PM	3	89	0	0	92	1	5	0	0	6	1	83	1	0	85	1	7	2	0	10	193	
Tota	I 23	425	4	0	452	4	17	7	0	28	19	362	3	0	384	6	26	12	0	44	908	
06:00 PM	4	70	0	0	74	0	5	0	0	5	5	51	0	0	56	4	2	1	0	7	142	
06:15 PM	0	67	0	0	67	1	4	0	0	5	3	69	0	0	72	0	6	1	0	7	151	
06:30 PM	2	74	2	0	78	0	3	4	0	7	0	65	0	0	65	2	1	2	0	5	155	
06:45 PM	1	48	2	0	51	2	4	2	0	8	8	32	0	0	40	1	3	2	0	6	105	
Tota	I 7	259	4	0	270	3	16	6	0	25	16	217	0	0	233	7	12	6	0	25	553	
Grand Tota	l  223	3185	23	1	3432	27	156	67	0	250	145	3186	20	0	3351	43	140	108	0	291	7324	
Apprch %	6.5	92.8	0.7	0		10.8	62.4	26.8	0		4.3	95.1	0.6	0		14.8	48.1	37.1	0			
Total %	5 J	43.5	0.3	0	46.9	0.4	2.1	0.9	0	3.4	2	43.5	0.3	0	45.8	0.6	1.9	1.5	0	4		

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Lights

			SR-43				Ra	andolph I	Rd				SR-43				R	andolph I	Rd		
		S	outhbour	d			V	/estbour	ld			N	lorthbour	d			E	Eastboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analys	is From 07	:00 AM to	o 11:45 A	M - Pea	k 1 of 1																
Peak Hour for Enti	ire Intersec	tion Begi	ns at 07:0	00 AM																	
07:00 AM	1	39	1	0	41	0	5	1	0	6	0	100	1	0	101	1	1	0	0	2	150
07:15 AM	0	49	2	0	51	2	9	3	0	14	1	109	0	0	110	0	0	2	0	2	177
07:30 AM	4	71	0	0	75	0	2	0	0	2	2	137	0	0	139	1	2	7	0	10	226
07:45 AM	7	76	0	0	83	0	3	2	0	5	3	69	1	0	73	2	0	3	0	5	166
Total Volume	12	235	3	0	250	2	19	6	0	27	6	415	2	0	423	4	3	12	0	19	719
% App. Total	4.8	94	1.2	0		7.4	70.4	22.2	0		1.4	98.1	0.5	0		21.1	15.8	63.2	0		
PHF	.429	.773	.375	.000	.753	.250	.528	.500	.000	.482	.500	.757	.500	.000	.761	.500	.375	.429	.000	.475	.795

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Lights

			SR-43				Ra	andolph	Rd				SR-43				R	andolph	Rd		
		S	outhboui	nd			V	Vestbour	nd			Ν	lorthboui	nd			E	Eastboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	s From 12	:00 PM t	o 06:45 F	PM - Pea	k 1 of 1																
Peak Hour for Enti	re Intersec	tion Begi	ins at 04:	15 PM																	
04:15 PM	5	148	0	0	153	1	1	1	0	3	5	74	1	0	80	3	5	1	0	9	245
04:30 PM	8	111	0	0	119	0	4	1	0	5	6	101	1	0	108	4	5	4	0	13	245
04:45 PM	3	135	2	0	140	0	5	1	0	6	4	90	0	0	94	0	6	1	0	7	247
05:00 PM	7	127	0	0	134	1	1	4	0	6	5	101	1	0	107	0	9	5	0	14	261
Total Volume	23	521	2	0	546	2	11	7	0	20	20	366	3	0	389	7	25	11	0	43	998
% App. Total	4.2	95.4	0.4	0		10	55	35	0		5.1	94.1	0.8	0		16.3	58.1	25.6	0		
PHF	.719	.880	.250	.000	.892	.500	.550	.438	.000	.833	.833	.906	.750	.000	.900	.438	.694	.550	.000	.768	.956

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Mediums

									Gro	ups Printed-	Mediums										
			SR-43				R	andolph	Rd				SR-43				R	andolph	Rd		
		Sc	outhbour	nd			V	Vestbou	nd			N	orthboun	d			E	Eastbour	ld		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
07:00 AM	0	1	0	0	1	0	0	1	0	1	0	4	0	0	4	0	0	0	0	0	6
07:15 AM	0	3	0	0	3	0	0	0	0	0	0	7	0	0	7	0	1	0	0	1	11
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	5	0	0	5	0	0	0	0	0	5
07:45 AM	0	5	0	0	5	0	0	1	0	1	0	4	0	0	4	0	0	0	0	0	10
Total	0	9	0	0	9	0	0	2	0	2	0	20	0	0	20	0	1	0	0	1	32
08.00 AM	0	2	0	0	2	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	6
08:15 AM	0 0	3	Ő	0	3	0	Ő	0	0	0	0	3	0	Ő	3	0 0	Ő	1	0	1	7
08:30 AM	1	1	0 0	0	2	0	Ő	0	0	0	0	2	0	0	2	0 0	0 0	0	0	0	4
08:45 AM	0	6	0	0	6	0	0	0	0	0	1	7	0	0	8	0	0	0	0	0	14
Total	1	12	0	0	13	0	0	0	0	0	1	16	0	0	17	0	0	1	0	1	31
			-				-			_	-		-			_		-	-		
09:00 AM	0	2	0	0	2	0	0	0	0	0	0	8	0	0	8	0	0	0	0	0	10
09:15 AM	0	0	0	0	0	0	0	0	0	0	1	4	0	0	5	0	0	0	0	0	5
09:30 AM	0	3	0	0	3	0	0	0	0	0	0	5	0	0	5	0	0	0	0	0	8
09:45 AM	0	2	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
Total	0	7	0	0	7	0	0	0	0	0	1	20	0	0	21	0	0	0	0	0	28
10:00 AM	1	2	0	0	3	0	0	0	0	0	0	3	0	0	3	0	0	1	0	1	7
10:15 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
10:30 AM	2	1	0	0	3	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	5
10:45 AM	0	3	0	0	3	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	6
Total	3	7	0	0	10	0	0	0	0	0	0	8	0	0	8	0	0	1	0	1	19
11:00 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
11:15 AM	1	0	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4
11:30 AM	1	1	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
11:45 AM	0	3	0	0	3	0	0	0	0	0	Ō	1	0	0	1	0	0	0	0	0	4
Total	2	5	0	0	7	0	0	0	0	0	0	8	0	0	8	0	0	0	0	0	15
12:00 PM	0	0	٥	0	٥	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	2
12:00 F M	0	2	0	0	3	0	0	0	0	0	0	2	0	0	2	0	0	1	0	1	2
12:13 F M	0	1	0	0	1	0	0	0	0	0	0	1	0	0	3	0	0	0	0	1	5
12:30 F M	0	2	0	0	2	0	0	0	0	0	0	4 0	0	0	4	0	0	0	0	0	5
Total	0	7	0			0	0	0	0	0	0	11	0	0		0	0	1	0	1	10
rolar	0	1	U	0	1	U	0	0	0	U	0	11	0	0	11	0	0	I	0	I	19
01:00 PM	0	2	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
01:15 PM	0	3	0	0	3	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	5
01:30 PM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4

Akron, OH 44306

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Mediums

									Gro	ups Printed-	Mediums										
			SR-43				Ra	andolph	Rd				SR-43				Ra	andolph F	}d		
		Sc	outhbound				N	/estbour	nd			N	orthboun	d			E	astbound	d		
Start Time	Right	Thru	Left U	-Turn A	pp. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn Ap	p. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
01:45 PM	0	1	0	0	1	0	0	0	0	0	0	5	0	0	5	0	0	0	0	0	6
Total	0	7	0	0	7	0	0	0	0	0	0	13	0	0	13	0	0	0	0	0	20
02:00 PM	0	4	0	0	4	0	0	1	0	1	0	1	0	0	1	0	0	0	0	0	6
02:15 PM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
02:30 PM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4
02:45 PM	0	7	0	0	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7
Total	0	13	0	0	13	0	0	1	0	1	0	5	0	0	5	0	0	0	0	0	19
03:00 PM	0	6	0	0	6	0	0	0	0	0	0	2	0	0	2	0	1	0	0	1	9
03:15 PM	0	2	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
03:30 PM	0	2	0	0	2	0	1	0	0	1	0	2	0	0	2	0	0	0	0	0	5
03:45 PM	0	2	0	0	2	0	0	0	0	0	1	3	0	0	4	0	0	0	0	0	6
Total	0	12	0	0	12	0	1	0	0	1	1	10	0	0	11	0	1	0	0	1	25
04:00 PM	0	3	0	0	3	0	0	0	0	0	1	4	0	0	5	0	0	0	0	0	8
04:15 PM	0	2	0	0	2	0	0	0	0	0	1	4	0	0	5	0	0	0	0	0	7
04:30 PM	0	0	0	0	0	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	3
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	5	0	0	5	0	0	0	0	0	2	11	0	0	13	0	0	0	0	0	18
05:00 PM	0	2	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	3
05:15 PM	0	1	0	0	1	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	3
05:30 PM	0	2	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	2
Total	0	5	0	0	5	0	0	0	0	0	0	5	0	0	5	0	0	0	0	0	10
'					1					'											1
06:00 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
06:15 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	Ō	0	0	1
06:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
06:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	Ō	0	0	0
Total	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
	-		-	-	1	-	-	-	•	- 1	-		-	-	1	-	-	-	2	-	_
Grand Total	6	90	0	0	96	0	1	3	0	4	5	128	0	0	133	0	2	3	0	5	238
Apprch %	6.2	93.8	0	0		0	25	75	0		3.8	96.2	0	0		0	40	60	0	-	_
Total %	2.5	37.8	0	0	40.3	0	0.4	1.3	0	1.7	2.1	53.8	0	0	55.9	0	0.8	1.3	0	2.1	

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Mediums

			SR-43				Ra	andolph	Rd				SR-43				Ra	andolph	Rd		
		S	outhboun	d			V	Vestbour	nd			N	orthboun	d			E	astboun	ld		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	is From 07	:00 AM to	o 11:45 A	M - Pea	k 1 of 1																
Peak Hour for Enti	re Intersec	tion Begi	ns at 08:4	15 AM																	
08:45 AM	0	6	0	0	6	0	0	0	0	0	1	7	0	0	8	0	0	0	0	0	14
09:00 AM	0	2	0	0	2	0	0	0	0	0	0	8	0	0	8	0	0	0	0	0	10
09:15 AM	0	0	0	0	0	0	0	0	0	0	1	4	0	0	5	0	0	0	0	0	5
09:30 AM	0	3	0	0	3	0	0	0	0	0	0	5	0	0	5	0	0	0	0	0	8
Total Volume	0	11	0	0	11	0	0	0	0	0	2	24	0	0	26	0	0	0	0	0	37
% App. Total	0	100	0	0		0	0	0	0		7.7	92.3	0	0		0	0	0	0		
PHF	.000	.458	.000	.000	.458	.000	.000	.000	.000	.000	.500	.750	.000	.000	.813	.000	.000	.000	.000	.000	.661

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Mediums

			SR-43				Ra	andolph I	Rd				SR-43				R	andolph F	Rd		
		So	outhboun	d			W	/estbour	nd			N	orthbour	nd			E	Eastboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	s From 12	:00 PM to	06:45 P	M - Pea	k 1 of 1																
Peak Hour for Enti	re Intersec	tion Begir	ns at 02:4	45 PM																	
02:45 PM	0	7	0	0	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7
03:00 PM	0	6	0	0	6	0	0	0	0	0	0	2	0	0	2	0	1	0	0	1	9
03:15 PM	0	2	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
03:30 PM	0	2	0	0	2	0	1	0	0	1	0	2	0	0	2	0	0	0	0	0	5
Total Volume	0	17	0	0	17	0	1	0	0	1	0	7	0	0	7	0	1	0	0	1	26
% App. Total	0	100	0	0		0	100	0	0		0	100	0	0		0	100	0	0		
PHF	.000	.607	.000	.000	.607	.000	.250	.000	.000	.250	.000	.583	.000	.000	.583	.000	.250	.000	.000	.250	.722

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Articulated Trucks

									Groups	Printed- Arti	culated Tru	ucks									
			SR-43				R	andolph	Rd				SR-43				Ra	andolph	Rd		]
		So	outhbou	nd			V	Vestbour	nd			N	orthbour	nd			E	astbour	nd		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
07:45 AM	1	1	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	3
Total	1	1	0	0	2	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	4
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:15 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
08:30 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	2	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	3
09:00 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
09:15 AM	0	2	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
09:30 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
09:45 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
Total	0	4	0	0	4	0	0	0	0	0	0	6	0	0	6	0	0	0	0	0	10
10:00 AM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	2
10:15 AM	0	1	0	0	1	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	3
10:30 AM	0	2	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	3
10:45 AM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	2
Total	0	3	0	0	3	0	0	0	0	0	0	7	0	0	7	0	0	0	0	0	10
11:00 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
11:15 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
11:30 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
11:45 AM	0	0	0	0	0	0	Õ	0	0	Ō	0	1	0	0	1	0	0	0	0	0	1
Total	0	2	0	0	2	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	6
12:00 PM	0	2	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
12:15 PM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
12:30 PM	Ő	1	Ő	Ő	1	Õ	Ő	Ő	Ő	Ő	Ő	3	Õ	Õ	3	Õ	Õ	Õ	Ő	Ő	4
12:45 PM	1	1	0	0	2	Ő	Ő	0	Ő	0	Ő	0	Ő	Ő	0	Ő	Õ	Ő	Ő	0	2
Total	1	5	0	0	6	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	10
01:00 PM	0	1	0	0	1	0	0	0	٥	٥l	0	3	0	0	3	0	0	0	٥	٥	4
01:15 PM	õ	0	0	0	0	0	õ	0	0	0	0	1	ő	0	1	0	õ	0	0	0	1
01:30 PM	õ	1	Ő	0	1	0	õ	0	Ő	0	0	2	Ő	Ő	2	0	õ	Ő	0	0	3

Akron, OH 44306

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Articulated Trucks

Groups Printed- Articulated Trucks	
SR-43 Randolph Rd SR-43 Randolph Rd	
Southbound Westbound Northbound Eastbound	
Start Time Right Thru Left U-Turn App. Total Right Thru Left U-Turn	App. Total Int. Total
01:45 PM 0 2 0 0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2
Total 0 4 0 0 4 0 0 0 0 0 0 0 6 0 0 6 0 0 0 0	0 10
02:00 PM 0 0 0 0 0 0 0 0 0 0 0 0 0 2 0 0 2 0 0 0 0 0	0 2
02:15 PM 0 2 0 0 2 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0	0 3
02:30 PM 0 1 0 0 1 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0 0	0 2
02:45 PM 0 2 0 0 2 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0	0 3
Total 0 5 0 0 5 0 0 0 0 0 0 0 5 0 0 5 0 0 0 0 0	0 10
03:00 PM 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1
03:15 PM 0 2 0 0 2 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0	0 3
03:30 PM 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1
03:45 PM 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1
Total 0 5 0 0 5 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0	0 6
04:00 PM 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0 0	0 1
04:15 PM 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1
04:30 PM 0 1 0 0 1 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0 0	0 2
04:45 PM 0 3 0 0 3 1 0 0 0 1 0 2 0 0 2 0 0 0 0	0 6
Total 0 5 0 0 5 1 0 0 0 1 0 4 0 0 4 0 0 0 0	0 10
	- 1
05:00 PM 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1
05:15 PM 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1
05:30 PM 0 0 0 0 0 0 0 0 0 0 0 0 3 0 0 3 0 0 0 0 0	0 3
05:45 PM 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 1 0 0 0 0 0	0 1
Total 0 2 0 0 2 0 0 0 0 0 0 0 4 0 0 4 0 0 0 0	0 6
	- 1
	0 1
	0 0
	0 1
Grand Total 2 38 0 0 40 1 0 0 0 1 0 45 0 0 45 0 0 0 0	0 86
Apprch % 5 95 0 0 100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
Total% 23 442 0 0 465 12 0 0 12 0 523 0 0 523 0 0 0 0	0

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Articulated Trucks

			SR-43				R	andolph	Rd				SR-43				Ra	andolph	Rd		
		S	outhboun	d			V	Vestbour	nd			N	lorthboun	d			E	astboun	ıd		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analys	is From 07	:00 AM to	o 11:45 A	M - Pea	k 1 of 1																
Peak Hour for Enti	ire Intersec	tion Begi	ns at 09:0	00 AM																	
09:00 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
09:15 AM	0	2	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
09:30 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
09:45 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
Total Volume	0	4	0	0	4	0	0	0	0	0	0	6	0	0	6	0	0	0	0	0	10
% App. Total	0	100	0	0		0	0	0	0		0	100	0	0		0	0	0	0		
PHF	.000	.500	.000	.000	.500	.000	.000	.000	.000	.000	.000	.500	.000	.000	.500	.000	.000	.000	.000	.000	.500

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Articulated Trucks

			SR-43				Ra	andolph I	Rd				SR-43				R	andolph	Rd		
		S	outhbour	nd			W	/estbour	nd			N	orthbour	d			E	Eastbour	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	s From 12	:00 PM to	06:45 F	PM - Pea	k 1 of 1																
Peak Hour for Enti	re Intersed	tion Begi	ns at 12:	15 PM																	
12:15 PM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
12:30 PM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4
12:45 PM	1	1	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
01:00 PM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4
Total Volume	1	4	0	0	5	0	0	0	0	0	0	7	0	0	7	0	0	0	0	0	12
% App. Total	20	80	0	0		0	0	0	0		0	100	0	0		0	0	0	0		
PHF	.250	1.00	.000	.000	.625	.000	.000	.000	.000	.000	.000	.583	.000	.000	.583	.000	.000	.000	.000	.000	.750

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Combined

							(	Groups P	rinted- Li	ights - Mediu	ums - Artic	ulated Tr	ucks								
			SR-43				R	andolph	Rd				SR-43				Ra	andolph	Rd		
		Sc	outhbour	nd			V	Vestbour	nd			N	orthbound	k			E	Eastbour	nd		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
07:00 AM	1	40	1	0	42	0	5	2	0	7	0	104	1	0	105	1	1	0	0	2	156
07:15 AM	0	52	2	0	54	2	9	3	0	14	1	116	0	0	117	0	1	2	0	3	188
07:30 AM	4	71	0	0	75	0	2	0	0	2	2	143	0	0	145	1	2	7	0	10	232
07:45 AM	8	82	0	0	90	0	3	3	0	6	3	74	1	0	78	2	0	3	0	5	179
Total	13	245	3	0	261	2	19	8	0	29	6	437	2	0	445	4	4	12	0	20	755
08:00 AM	1	46	0	0	47	0	6	4	0	10	0	58	1	0	59	0	2	1	0	3	119
08:15 AM	0	55	1	1	57	2	4	1	0	7	2	65	0	0	67	0	0	1	0	1	132
08:30 AM	6	44	0	0	50	0	0	1	0	1	3	83	0	0	86	2	1	1	0	4	141
08:45 AM	2	53	0	0	55	1	1	1	0	3	3	79	0	0	82	0	0	1	0	1	141
Total	9	198	1	1	209	3	11	7	0	21	8	285	1	0	294	2	3	4	0	9	533
09:00 AM	5	39	0	0	44	0	6	1	0	7	0	65	0	0	65	0	1	0	0	1	117
09:15 AM	2	39	0	0	41	1	3	0	0	4	1	50	0	0	51	1	0	0	0	1	97
09:30 AM	2	43	1	0	46	0	2	3	0	5	4	50	0	0	54	0	1	0	0	1	106
09:45 AM	2	45	0	0	47	1	2	1	0	4	2	54	0	0	56	0	2	1	0	3	110
Total	11	166	1	0	178	2	13	5	0	20	7	219	0	0	226	1	4	1	0	6	430
10:00 AM	9	46	0	0	55	1	2	0	0	3	2	55	1	0	58	1	3	1	0	5	121
10:15 AM	2	52	0	0	54	0	3	0	0	3	0	49	0	0	49	0	2	0	0	2	108
10:30 AM	6	48	0	0	54	0	4	3	0	7	3	47	0	0	50	0	1	5	0	6	117
10:45 AM	6	36	1	0	43	0	3	4	0	7	3	51	0	0	54	0	0	0	0	0	104
Total	23	182	1	0	206	1	12	7	0	20	8	202	1	0	211	1	6	6	0	13	450
11:00 AM	5	52	2	0	59	1	5	1	0	7	2	43	1	0	46	2	3	1	0	6	118
11:15 AM	3	41	0	0	44	0	3	0	0	3	1	54	0	0	55	0	1	5	0	6	108
11:30 AM	8	50	0	0	58	0	4	0	0	4	2	44	0	0	46	2	1	2	0	5	113
11:45 AM	0	40	0	0	40	1	4	2	0	7	3	56	0	0	59	0	4	1	0	5	111
Total	16	183	2	0	201	2	16	3	0	21	8	197	1	0	206	4	9	9	0	22	450
12:00 PM	5	71	0	0	76	0	2	1	0	3	4	41	0	0	45	1	2	1	0	4	128
12:15 PM	7	40	0	0	47	1	0	0	0	1	1	56	0	0	57	0	3	4	0	7	112
12:30 PM	2	55	0	0	57	1	3	2	0	6	2	55	0	0	57	0	1	5	0	6	126
12:45 PM	4	56	0	0	60	0	2	0	0	2	5	51	0	0	56	1	4	2	0	7	125
Total	18	222	0	0	240	2	7	3	0	12	12	203	0	0	215	2	10	12	0	24	491
[				-	- 1			-	-	1					- 1				-		
01:00 PM	3	49	0	0	52	1	2	3	0	6	3	62	0	0	65	0	2	2	0	4	127
01:15 PM	9	54	0	0	63	1	5	0	0	6	2	76	2	0	80	0	3	5	0	8	157
01:30 PM	9	53	0	0	62	1	3	3	0	7	1	70	0	0	71	0	2	3	0	5	145

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Combined

							0	Groups Pri	nted- Li	ights - Mediı	ums - Artio	culated Tr	ucks								
			SR-43				Ra	andolph R	d				SR-43				Ra	andolph I	Rd		
		So	outhboun	nd			V	Vestbound	1			N	lorthbour	nd			E	astboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left l	J-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
01:45 PM	5	50	0	0	55	0	5	0	0	5	3	56	1	0	60	0	2	2	0	4	124
Total	26	206	0	0	232	3	15	6	0	24	9	264	3	0	276	0	9	12	0	21	553
I					'					'											1
02:00 PM	5	65	0	0	70	1	3	3	0	7	4	58	2	0	64	1	4	1	0	6	147
02:15 PM	2	76	0	Ō	78	1	1	2	0	4	1	77	1	0	79	1	6	6	Ō	13	174
02:30 PM	11	79	1	0	91	1	0	0	0	1	3	82	2	0	87	0	1	6	0	7	186
02:45 PM	8	98	0	0	106	0	6	1	0	7	3	68	0	0	71	2	2	5	0	9	193
Total	26	318	1	0	345	3	10	6	0	19	11	285	5	0	301	4	13	18	0	35	700
. otal		0.0	•	°,	0.01	· ·		•	Ũ		••	-00	Ũ	· ·		•			°,		
03.00 PM	11	121	3	0	135	0	1	3	0	4	7	61	1	0	69	4	4	5	0	13	221
03.15 PM	4	91	0	0 0	95	0 0	2	2	ñ	4	7	81	0	0	88	n N	3	2	0	.0	192
03:30 PM	7	02	0	0	90	0	2	1	0	7	, 8	67	0	0	75	1	11	1	0	13	102
03.30 F M	1/	107	1	0	100	0	5	2	0	0	6	07	1	0	105	0	1	י ס	0	13	242
US.45 FIM	26	411	1	0	122	0	10		0	10	0	207	<u> </u>	0	227	5	- 4			/ 20	242
TOLAT	30	411	4	0	451	0	10	9	0	19	20	307	2	0	337	5	22		0	30	045
04:00 PM	7	80	0	0	96	1	1	0	0	2	2	05	0	0	07	0	Q	2	0	10	205
04.00 FM	/ E	151	0	0	150	1		1	0	2	2	95	1	0	97	0	0	2	0	10	203
04:15 PW	5	101	0	0	156	1	1		0	3	6	/8		0	85	3	5	1	0	9	253
04:30 PM	8	112	0	0	120	0	4	1	0	5	6	105	1	0	112	4	5	4	0	13	250
04:45 PM	3	138	2	0	143	1	5	1	0	1	4	92	0	0	96	0	6	1	0	/	253
Iotal	23	490	2	0	515	3	11	3	0	17	18	370	2	0	390	7	24	8	0	39	961
	_									- 1	_							_			
05:00 PM	7	130	0	0	137	1	1	4	0	6	5	102	1	0	108	0	9	5	0	14	265
05:15 PM	3	115	3	0	121	2	2	1	0	5	8	95	1	0	104	3	4	4	0	11	241
05:30 PM	10	98	1	0	109	0	9	2	0	11	5	88	0	0	93	2	6	1	0	9	222
05:45 PM	3	89	0	0	92	1	5	0	0	6	1	86	1	0	88	1	7	2	0	10	196
Total	23	432	4	0	459	4	17	7	0	28	19	371	3	0	393	6	26	12	0	44	924
06:00 PM	4	71	0	0	75	0	5	0	0	5	5	52	0	0	57	4	2	1	0	7	144
06:15 PM	0	67	0	0	67	1	4	0	0	5	3	70	0	0	73	0	6	1	0	7	152
06:30 PM	2	74	2	0	78	0	3	4	0	7	0	65	0	0	65	2	1	2	0	5	155
06:45 PM	1	48	2	0	51	2	4	2	0	8	8	32	0	0	40	1	3	2	0	6	105
Total	7	260	4	0	271	3	16	6	0	25	16	219	0	0	235	7	12	6	0	25	556
1				-	'	-	-	-	-	- 1	-	-	-	-				-	-	-	
Grand Total	231	3313	23	1	3568	28	157	70	0	255	150	3359	20	0	3529	43	142	111	0	296	7648
Apprch %	6.5	92.9	0.6	0		11	61.6	27.5	0		43	95.2	0.6	0		14.5	48	37.5	0		
Total %	3	43.3	0.3	Õ	46 7	04	21	0.9	Ő	33	2	43.9	0.3	Õ	46 1	0.6	19	1.5	Ő	39	
Lights	223	3185	23	1	3432	27	156	67	0	250	145	3186	20	0	3351	43	140	108	0	291	7324
% Lights	06.5	06 1	100	100	0402	06 /	00 /	05.7	0	200	06.7	0/ 0	100	0	0001	100	08.6	07.2	0	08.2	05.9
Mediume	6	<u> </u>	0	0	30.2 QG	0.4	1	30.7	0	30	50.7	128	001	0	132	0	20.0	37.5	0	30.3 F	239
% Modiuma	26	90 07	0	0		0	0 6	10	0	4		20	0	0	201	0	ے 1 ۸	07	0	17	200
	2.0	2.1	0	0	2.1	1	0.0	4.3	0	0.1	3.3	3.0	0	0	3.0 4E	0	0	2.1	0	1./	3.1
Articulated Trucks	2	38	0	0	40	1	0	0	0		0	45	0	0	45	0	0	0	0	0	00
O/ Autoritate d Tourslas				11	1 1 1				11	11/1	11	1.14	11		1.2			11	11	() ()	

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Combined

			SR-43				B	andolph	Rd				SR-43				r				
		S	outhboun	d			V	Vestbour	nd			N	orthboun	d			E	astboun	id		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analys	is From 07	':00 AM to	o 11:45 A	M - Pea	k 1 of 1					·											
Peak Hour for Enti	ire Intersed	ction Begi	ins at 07:0	00 AM																	
07:00 AM	1	40	1	0	42	0	5	2	0	7	0	104	1	0	105	1	1	0	0	2	156
07:15 AM	0	52	2	0	54	2	9	3	0	14	1	116	0	0	117	0	1	2	0	3	188
07:30 AM	4	71	0	0	75	0	2	0	0	2	2	143	0	0	145	1	2	7	0	10	232
07:45 AM	8	82	0	0	90	0	3	3	0	6	3	74	1	0	78	2	0	3	0	5	179
Total Volume	13	245	3	0	261	2	19	8	0	29	6	437	2	0	445	4	4	12	0	20	755
% App. Total	5	93.9	1.1	0		6.9	65.5	27.6	0		1.3	98.2	0.4	0		20	20	60	0		
PHF	.406	.747	.375	.000	.725	.250	.528	.667	.000	.518	.500	.764	.500	.000	.767	.500	.500	.429	.000	.500	.814

POR SR-43 at Randolph Rd 7:00AM-7:00PM 5/4/2022 Combined

			SR-43				Ra	andolph I	Rd				SR-43								
		S	outhbour	nd			W	/estbour	nd			N	lorthbour	nd			E	Eastbour	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	s From 12	:00 PM to	o 06:45 F	PM - Pea	k 1 of 1																
Peak Hour for Enti	re Intersec	ction Begi	ins at 04:	15 PM																	
04:15 PM	5	151	0	0	156	1	1	1	0	3	6	78	1	0	85	3	5	1	0	9	253
04:30 PM	8	112	0	0	120	0	4	1	0	5	6	105	1	0	112	4	5	4	0	13	250
04:45 PM	3	138	2	0	143	1	5	1	0	7	4	92	0	0	96	0	6	1	0	7	253
05:00 PM	7	130	0	0	137	1	1	4	0	6	5	102	1	0	108	0	9	5	0	14	265
Total Volume	23	531	2	0	556	3	11	7	0	21	21	377	3	0	401	7	25	11	0	43	1021
% App. Total	4.1	95.5	0.4	0		14.3	52.4	33.3	0		5.2	94	0.7	0		16.3	58.1	25.6	0		
PHF	.719	.879	.250	.000	.891	.750	.550	.438	.000	.750	.875	.898	.750	.000	.895	.438	.694	.550	.000	.768	.963

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Lights

	Groups Printed- Lights   SR-43 Trares Rd   Southbound Westbound Northbound														_						
			SR-43					Trares R	d				SR-43				-	Trares R	b		
		S	outhbou	nd			V	Vestbour	nd			N	orthbour	nd			E	astbour	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
07:00 AM	1	38	0	0	39	4	3	2	0	9	1	98	12	0	111	2	1	3	0	6	165
07:15 AM	5	49	0	0	54	4	8	0	0	12	0	95	27	0	122	10	1	10	0	21	209
07:30 AM	8	60	2	0	70	3	13	1	0	17	2	118	25	0	145	6	3	15	0	24	256
07:45 AM	7	67	5	0	79	1	8	0	0	9	0	69	28	0	97	3	2	6	0	11	196
Total	21	214	7	0	242	12	32	3	0	47	3	380	92	0	475	21	7	34	0	62	826
08:00 AM	2	43	1	0	46	1	4	2	0	7	1	57	19	0	77	1	3	1	0	5	135
08:15 AM	0	54	0	0	54	0	4	0	0	4	2	56	10	0	68	5	0	2	0	7	133
08:30 AM	2	42	0	0	44	2	3	2	0	7	1	82	22	0	105	4	2	1	0	7	163
08:45 AM	4	44	1	0	49	1	7	1	0	9	1	65	13	0	79	5	3	7	0	15	152
Total	8	183	2	0	193	4	18	5	0	27	5	260	64	0	329	15	8	11	0	34	583
1					1					1											
09:00 AM	2	34	1	0	37	2	7	0	0	9	3	54	13	0	70	7	1	2	0	10	126
09:15 AM	1	37	0	0	38	2	9	0	0	11	3	42	8	0	53	6	7	2	0	15	117
09:30 AM	2	40	1	0	43	1	7	0	0	8	0	42	10	0	52	8	4	6	0	18	121
09:45 AM	6	36	1	0	43	4	1	1	0	6	1	47	12	0	60	6	2	2	0	10	119
Total	11	147	3	0	161	9	24	1	0	34	7	185	43	0	235	27	14	12	0	53	483
1										1											
10:00 AM	5	41	0	0	46	1	5	1	0	7	1	45	5	0	51	2	5	5	0	12	116
10:15 AM	2	45	1	0	48	1	2	1	0	4	2	45	11	0	58	4	3	3	0	10	120
10:30 AM	3	44	1	0	48	0	4	0	0	4	1	41	4	0	46	6	2	8	0	16	114
10:45 AM	2	34	1	0	37	1	5	1	0	7	2	47	6	0	55	5	3	2	0	10	109
Iotal	12	164	3	0	179	3	16	3	0	22	6	178	26	0	210	17	13	18	0	48	459
	-	45		•	<b>E</b> 4	•			•	- 1	•		•	•	10	•		-	•	10	
11:00 AM	5	45	1	0	51	0	4	1	0	5	0	41	2	0	43	3	4	5	0	12	111
11:15 AM	1	39	2	0	42	1	2	0	0	3	0	40	/	0	4/	/	4	/	0	18	110
11:30 AM	2	46	0	0	48	3	5	1	0	9	3	34	13	0	50	/	3	6	0	16	123
11:45 AM	3	42	2	0	47	0	3	1	0	4	1	49	6	0	56	9	3	/		20	12/
Iotal	11	172	5	0	188	4	14	3	0	21	4	164	28	0	196	26	14	25	1	66	4/1
10.00 DM	-		0	0	<b>co</b>	0	0	0	0		4	05	10	0	50	0	4	-	0	17	140
12:00 PM	5	55	2	0	62	3	6	0	0	9	1	35	16	0	52	8 7	4	5	0	17	
12:15 PM	6	30	1	0	37	3	4	2	0	9	0	45	9	0	54	/	3	/	0	17	117
12:30 PM	4	49	2	0	55	2	2	2	0	6 7	0	45	9	0	54	14	4	5	0	23	138
12:45 PM	5	4/		0	52	3	4		0	/	2	40		0	49	9	3	9_	0	21	129
Iotal	20	181	5	0	206	11	16	4	0	31	3	165	41	U	209	38	14	26	0	78	524
	1	46	4	0	<b>E</b> 4	0	7	0	0	7	0	50	0	0	64	F	4	10	0	10	444
	4	40	1	0	21	1	( 6	0	0	7	2	53 60	9	0	04 76	5	4	10	0	19	141
	3	44	1	0	48		0	U 4	0	7	1	09	0	0	10	10	2	0 C	0	14	145
01:30 PM	Э	47	2	0	54	1	3	1	0	5	U	28	Э	U	63	13	2	ю	0	21	143

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Lights

File Name : POR-43\_at\_Trares\_Rd\_(3.867)\_956910\_05-04-2022 Site Code : Start Date : 5/4/2022

Page No : 2

										Gr	oups Printer	d- Lights										
				SR-43					Trares R	d				SR-43					Trares R	d		
			Sc	outhbou	nd			V	Vestbour	nd			N	lorthbour	nd				Eastbour	ld		
Sta	art Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn A	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
01	1:45 PM	5	44	1	0	50	0	2	1	0	3	2	51	11	0	64	9	6	4	0	19	136
	Total	17	181	5	0	203	2	18	2	0	22	5	231	31	0	267	33	14	26	0	73	565
						'																
02	2:00 PM	10	50	2	0	62	1	2	1	0	4	2	59	7	0	68	10	8	6	0	24	158
02	2:15 PM	5	70	1	Ō	76	3	2	0	0	5	2	55	11	0	68	13	8	11	0	32	181
02	2:30 PM	6	70	0	0	76	4	4	0	0	8	1	73	14	0	88	22	2	11	0	35	207
02	2:45 PM	10	88	3	0	101	2	1	0	0	3	0	63	7	0	70	6	6	6	0	18	192
-	Total	31	278	6	0	315	10	9	1	0	20	5	250	39	0	294	51	24	34	0	109	738
	1	-	-	-	-	1	-	-		-	- 1	-			-	- 1	-		-	-		
03	3:00 PM	15	93	2	0	110	1	3	0	0	4	3	56	7	0	66	9	6	11	0	26	206
03	3:15 PM	6	80	2	0	88	1	5	0	0	6	2	78	13	Ō	93	18	13	6	0	37	224
03	3:30 PM	4	88	3	0	95	1	3	1	0	5	2	71	12	0	85	15	10	4	0	29	214
03	3:45 PM	9	87	7	0	103	0	3	0	0	3	2	85	9	0	96	23	11	13	0	47	249
	Total	34	348	14	0	396	3	14	1	0	18	9	290	41	0	340	65	40	34	0	139	893
		•	• • •		•		•			•		•			•				•	•		
04	1:00 PM	4	86	3	0	93	1	6	0	0	7	4	81	9	0	94	28	10	9	0	47	241
04	1:15 PM	6	135	3	0	144	2	5	0	0	7	2	72	12	0	86	20	13	10	0	43	280
04	1:30 PM	8	101	6	0	115	3	6	1	0	10	0	96	12	0	108	13	9	8	0	30	263
04	1:45 PM	3	131	1	0	135	2	3	1	0	6	1	79	10	Ö	90	25	10	9	0	44	275
	Total	21	453	13	0	487	8	20	2	0	30	7	328	43	0	378	86	42	36	0	164	1059
					•		•			•					•					•		
05	5:00 PM	8	121	4	0	133	2	2	2	0	6	2	95	13	0	110	18	13	12	0	43	292
05	5:15 PM	5	106	5	0	116	3	7	3	0	13	0	88	9	0	97	26	16	14	0	56	282
05	5:30 PM	8	90	2	Ō	100	1	4	2	0	7	3	82	14	0	99	11	9	4	0	24	230
05	5:45 PM	3	79	6	0	88	4	0	2	0	6	1	81	7	0	89	10	11	5	0	26	209
	Total	24	396	17	0	437	10	13	9	0	32	6	346	43	0	395	65	49	35	0	149	1013
	1					- 1					- 1					1						
06	3:00 PM	3	67	3	0	73	2	3	2	0	7	1	46	4	0	51	7	6	5	0	18	149
06	6:15 PM	2	64	2	0	68	1	5	2	0	8	2	73	6	Ö	81	8	4	1	0	13	170
06	5:30 PM	5	70	3	0	78	2	1	1	0	4	4	62	14	0	80	8	1	5	0	14	176
06	6:45 PM	3	47	2	0	52	2	3	1	0	6	1	33	5	Ö	39	4	6	3	0	13	110
	Total	13	248	10	0	271	7	12	6	0	25	8	214	29	0	251	27	17	14	0	58	605
					2	=	-			· ·		5		_,	-	== •				· ·	50	
Gra	nd Total	223	2965	90	0	3278	83	206	40	0	329	68	2991	520	0	3579	471	256	305	1	1033	8219
A	oprch %	6.8	90.5	2.7	Ő		25.2	62.6	12.2	Ő		1.9	83.6	14.5	Ō		45.6	24.8	29.5	0.1		
	Total %	2.7	36.1	1.1	Ő	39.9	1	2.5	0.5	Õ	4	0.8	36.4	6.3	Ō	43.5	5.7	3.1	3.7	0	12.6	
						-			-	-						-				-	-	

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Lights

			SR-43				-	Trares R	d				SR-43					Trares Ro	b		
		S	outhboun	d			V	Vestbour	nd			Ν	lorthbou	nd			E	Eastboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	s From 07	:00 AM to	o 11:45 A	M - Pea	k 1 of 1																
Peak Hour for Enti	re Intersed	ction Begi	ns at 07:0	00 AM																	
07:00 AM	1	38	0	0	39	4	3	2	0	9	1	98	12	0	111	2	1	3	0	6	165
07:15 AM	5	49	0	0	54	4	8	0	0	12	0	95	27	0	122	10	1	10	0	21	209
07:30 AM	8	60	2	0	70	3	13	1	0	17	2	118	25	0	145	6	3	15	0	24	256
07:45 AM	7	67	5	0	79	1	8	0	0	9	0	69	28	0	97	3	2	6	0	11	196
Total Volume	21	214	7	0	242	12	32	3	0	47	3	380	92	0	475	21	7	34	0	62	826
% App. Total	8.7	88.4	2.9	0		25.5	68.1	6.4	0		0.6	80	19.4	0		33.9	11.3	54.8	0		
PHF	.656	.799	.350	.000	.766	.750	.615	.375	.000	.691	.375	.805	.821	.000	.819	.525	.583	.567	.000	.646	.807

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Lights

			SR-43					rares Ro	ł				SR-43								
		S	outhboun	ıd			N	/estboun	d			Ν	lorthbour	nd			E	Eastbour	nd		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	s From 12	2:00 PM to	06:45 P	M - Pea	k 1 of 1																
Peak Hour for Enti	re Intersed	ction Begi	ns at 04:3	30 PM																	
04:30 PM	8	101	6	0	115	3	6	1	0	10	0	96	12	0	108	13	9	8	0	30	263
04:45 PM	3	131	1	0	135	2	3	1	0	6	1	79	10	0	90	25	10	9	0	44	275
05:00 PM	8	121	4	0	133	2	2	2	0	6	2	95	13	0	110	18	13	12	0	43	292
05:15 PM	5	106	5	0	116	3	7	3	0	13	0	88	9	0	97	26	16	14	0	56	282
Total Volume	24	459	16	0	499	10	18	7	0	35	3	358	44	0	405	82	48	43	0	173	1112
% App. Total	4.8	92	3.2	0		28.6	51.4	20	0		0.7	88.4	10.9	0		47.4	27.7	24.9	0		
PHF	.750	.876	.667	.000	.924	.833	.643	.583	.000	.673	.375	.932	.846	.000	.920	.788	.750	.768	.000	.772	.952
POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Mediums

									Gro	ups Printed	Mediums	6									_
			SR-43					Trares R	ld				SR-43					Trares R	d		
		Sc	outhbound	d			<u>\</u>	Vestbou	nd			N	orthbound	k			E	Eastbour	ld		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
07:00 AM	0	2	0	0	2	0	0	0	0	0	0	4	2	0	6	0	0	0	0	0	8
07:15 AM	0	2	1	0	3	0	0	0	0	0	0	6	0	0	6	0	0	0	0	0	9
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	6	0	0	6	0	0	0	0	0	6
07:45 AM	2	4	0	0	6	0	0	0	0	0	0	3	2	0	5	0	0	0	0	0	11
Total	2	8	1	0	11	0	0	0	0	0	0	19	4	0	23	0	0	0	0	0	34
08:00 AM	0	1	0	0	1	0	0	0	0	0	0	3	2	0	5	0	0	0	0	0	6
08:15 AM	0	1	1	0	2	0	0	0	0	0	0	1	1	0	2	0	0	2	0	2	6
08:30 AM	0	1	0	0	1	0	0	1	0	1	0	2	0	0	2	1	0	0	0	1	5
08:45 AM	1	4	0	0	5	0	0	1	0	1	0	9	0	0	9	1	0	0	0	1	16
Total	1	7	1	0	9	0	0	2	0	2	0	15	3	0	18	2	0	2	0	4	33
09:00 AM	0	2	0	0	2	1	0	0	0	1	0	5	0	0	5	1	0	0	0	1	9
09:15 AM	0	0	0	0	0	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	4
09:30 AM	0	3	0	0	3	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	7
09:45 AM	0	2	0	0	2	0	0	0	0	0	0	2	1	0	3	0	0	0	0	0	5
Total	0	7	0	0	7	1	0	0	0	1	0	15	1	0	16	1	0	0	0	1	25
10:00 AM	0	2	0	0	2	0	0	0	0	0	0	2	2	0	4	0	0	1	0	1	7
10:15 AM	0	0	1	0	1	0	0	0	0	0	0	0	1	0	1	0	0	0	0	0	2
10:30 AM	0	1	0	0	1	1	0	0	0	1	0	1	0	0	1	0	0	0	0	0	3
10:45 AM	0	3	0	0	3	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	5
Total	0	6	1	0	7	1	0	0	0	1	0	5	3	0	8	0	0	1	0	1	17
11:00 AM	0	2	0	0	2	0	0	0	0	0	0	1	1	0	2	0	0	0	0	0	4
11:15 AM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	1	0	0	0	1	5
11:30 AM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4
11:45 AM	1	1	0	0	2	0	0	0	1	1	0	2	0	0	2	1	0	0	0	1	6
Total	1	5	0	0	6	0	0	0	1	1	0	9	1	0	10	2	0	0	0	2	19
12:00 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
12:15 PM	1	1	0	0	2	0	0	0	0	0	0	2	1	0	3	0	0	0	0	0	5
12:30 PM	0	1	0	0	1	0	0	0	0	0	0	2	2	0	4	0	0	1	0	1	6
12:45 PM	0	3	0	0	3	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	5
Total	1	5	0	0	6	0	0	0	0	0	0	7	3	0	10	0	0	1	0	1	17
01:00 PM	0	2	0	0	2	0	0	0	0	0	0	5	0	0	5	1	0	0	0	1	8
01:15 PM	0	3	0	0	3	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	4
01:30 PM	0	1	0	0	1	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	3

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Mediums

File Name : POR-43\_at\_Trares\_Rd\_(3.867)\_956910\_05-04-2022 Site Code : Start Date : 5/4/2022

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									Gro	ups Printed-	Mediums										
			SR-43					Trares R	d				SR-43					Trares R	d		
		Sc	outhboun	d			V	Vestboui	nd			N	lorthbour	nd			E	Eastbour	ıd		
Start Time	Right	Thru	Left	U-Turn A	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn A	pp. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
01:45 PM	0	1	0	0	1	0	0	0	0	0	0	5	1	0	6	0	0	0	0	0	7
Total	0	7	0	0	7	0	0	0	0	0	0	13	1	0	14	1	0	0	0	1	22
02:00 PM	0	5	0	0	5	0	0	0	0	0	0	1	1	0	2	0	0	0	0	0	7
02:15 PM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2	1	0	0	0	1	3
02:30 PM	0	0	0	0	0	0	0	0	0	0	0	1	2	0	3	0	0	0	0	0	3
02:45 PM	0	7	0	0	7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7
Total	0	12	0	0	12	0	0	0	0	0	0	4	3	0	7	1	0	0	0	1	20
03:00 PM	0	4	1	0	5	0	0	0	0	0	0	2	0	0	2	1	0	0	0	1	8
03:15 PM	1	2	0	0	3	0	0	1	0	1	0	2	0	0	2	0	0	0	0	0	6
03:30 PM	1	1	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	1	0	1	4
03:45 PM	0	2	0	0	2	0	0	1	0	1	1	3	0	0	4	0	0	0	0	0	7
Total	2	9	1	0	12	0	0	2	0	2	1	8	0	0	9	1	0	1	0	2	25
04:00 PM	0	3	0	0	3	1	0	0	0	1	0	2	0	0	2	2	0	2	0	4	10
04:15 PM	0	3	0	0	3	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	7
04:30 PM	0	0	0	0	0	1	0	0	0	1	0	3	0	0	3	0	0	0	0	0	4
04:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	1
Total	0	6	0	0	6	2	0	0	0	2	0	9	0	0	9	2	1	2	0	5	22
05:00 PM	0	2	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	3
05:15 PM	1	0	0	0	1	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	3
05:30 PM	0	3	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
05:45 PM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	2
Total	1	5	0	0	6	0	0	0	0	0	0	5	0	0	5	0	0	0	0	0	11
06:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
06:15 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
06:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
06:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
Grand Total	8	77	4	0	89	4	0	4	1	9	1	110	19	0	130	10	1	7	0	18	246
Apprch %	9	86.5	4.5	0		44.4	0	44.4	11.1		0.8	84.6	14.6	0		55.6	5.6	38.9	0		
Total %	3.3	31.3	1.6	0	36.2	1.6	0	1.6	0.4	3.7	0.4	44.7	7.7	0	52.8	4.1	0.4	2.8	0	7.3	

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Mediums

File Name : POR-43\_at\_Trares\_Rd\_(3.867)\_956910\_05-04-2022 Site Code : Start Date : 5/4/2022

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			SR-43				-	Frares R	d				SR-43				٦	Frares R	d		
		S	outhbour	nd			V	Vestbour	nd			N	orthboun	d			E	astboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	is From 07	:00 AM to	o 11:45 A	M - Pea	k 1 of 1																
Peak Hour for Enti	ire Intersec	tion Begi	ns at 08:	15 AM																	
08:15 AM	0	1	1	0	2	0	0	0	0	0	0	1	1	0	2	0	0	2	0	2	6
08:30 AM	0	1	0	0	1	0	0	1	0	1	0	2	0	0	2	1	0	0	0	1	5
08:45 AM	1	4	0	0	5	0	0	1	0	1	0	9	0	0	9	1	0	0	0	1	16
09:00 AM	0	2	0	0	2	1	0	0	0	1	0	5	0	0	5	1	0	0	0	1	9
Total Volume	1	8	1	0	10	1	0	2	0	3	0	17	1	0	18	3	0	2	0	5	36
% App. Total	10	80	10	0		33.3	0	66.7	0		0	94.4	5.6	0		60	0	40	0		
PHF	.250	.500	.250	.000	.500	.250	.000	.500	.000	.750	.000	.472	.250	.000	.500	.750	.000	.250	.000	.625	.563

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Mediums

			SR-43				T	rares Ro	b				SR-43				-	Trares Ro	b		
		So	outhboun	ld			W	/estbour	d			N	orthbour	nd			E	Eastboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysis	s From 12	:00 PM to	06:45 P	M - Pea	k 1 of 1				•			•									
Peak Hour for Entir	re Intersec	tion Begir	ns at 03:0	30 PM																	
03:30 PM	1	1	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	1	0	1	4
03:45 PM	0	2	0	0	2	0	0	1	0	1	1	3	0	0	4	0	0	0	0	0	7
04:00 PM	0	3	0	0	3	1	0	0	0	1	0	2	0	0	2	2	0	2	0	4	10
04:15 PM	0	3	0	0	3	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	7
Total Volume	1	9	0	0	10	1	0	1	0	2	1	10	0	0	11	2	0	3	0	5	28
% App. Total	10	90	0	0		50	0	50	0		9.1	90.9	0	0		40	0	60	0		
PHF	.250	.750	.000	.000	.833	.250	.000	.250	.000	.500	.250	.625	.000	.000	.688	.250	.000	.375	.000	.313	.700

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Articulated Trucks

									Groups	Printed- Artic	culated Tru	ucks									_
			SR-43					Trares R	d				SR-43				٦	Frares R	d		
		Sc	outhbou	nd			1	Vestbour	nd			No	orthbour	nd			E	astboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn Ap	p. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
07:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
07:30 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
07:45 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
Total	0	1	0	0	1	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	3
08:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
08:15 AM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
08:30 AM	1	0	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
08:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Total	1	1	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	3
					. 1					- 1					. 1						1
09:00 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
09:15 AM	0	2	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
09:30 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
09:45 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
Total	0	4	0	0	4	0	0	0	0	0	0	6	0	0	6	0	0	0	0	0	10
10.00 414	0	0	0	0		0	0	0	0		0	0	0	0		0	0	0	0	0	
10:00 AM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	2
10:15 AM	0		0	0		0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	3
10:30 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0		0	0	0	0	0	2
10:45 AM	0				0	0			0	0	0	- 2		0	2	0	0		0	0	2
Total	0	2	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	9
11.00 AM	٥	1	0	٥	1	0	٥	0	0	0	0	1	0	0	1	٥	0	0	0	0	2
11:15 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
11:30 AM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	2
11:45 AM	0	1	0	0	1	0	0	0	0	0	0	0	1	0	1	0	0	0	0	0	2
Total	0	3	0	0	3	0	0	0	0	0	0	4	1	0	5	0	0	0	0	0	8
1 otar	0	0	Ū	Ū	0	Ū	0	Ū	Ū	0	U	-		0	01	0	Ū	0	Ū	0	0
12:00 PM	0	2	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
12:15 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1	0	1	2
12:30 PM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	Ó	4
12:45 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	Ō	0	0	0	0	0	1
Total	0	5	0	0	5	0	0	0	0	0	0	3	0	0	3	0	0	1	0	1	9
	-	-	-	-	- 1	2	-	-	·	- 1	-	-		-	- 1	-	-		-	-	
01:00 PM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4
01:15 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
01:30 PM	0	1	0	0	1	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	3

Akron, OH 44306

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Articulated Trucks

									Groups F	Printed-Artic	culated Tru	ucks									
			SR-43				Т	rares R	d				SR-43				Т	rares Ro	d		
		So	outhbour	nd			W	estbour	nd			N	orthbour	nd			E	astboun	d		
Start Time	Right	Thru	Left	U-Turn A	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
01:45 PM	0	2	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	3
Total	0	4	0	0	4	0	0	0	0	0	0	7	0	0	7	0	0	0	0	0	11
02:00 PM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	2	0	0	0	0	0	2
02:15 PM	0	2	0	0	2	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	3
02:30 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
02:45 PM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
Total	0	4	0	0	4	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	8
03:00 PM	0	2	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
03:15 PM	0	3	0	0	3	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	4
03:30 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
03:45 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Total	0	7	0	0	7	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	8
04:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	1	1
04:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
04:30 PM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
04:45 PM	0	3	0	Ō	3	0	0	0	Ō	0	Ō	1	0	Ō	1	1	0	0	0	1	5
Total	0	4	0	0	4	0	0	0	0	0	0	2	0	0	2	1	0	1	0	2	8
	-		-	-		-	-	-	-	- 1	-		-	-	1		-		-	'	-
05:00 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
05:15 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
05:30 PM	Õ	0	Ő	Ő	0	Õ	Õ	Ő	Ő	Ő	Ő	3	Õ	Ő	3	Õ	Õ	Ő	Õ	Õ	3
05:45 PM	Õ	0 0	Ő	Ő	0	Õ	Ő	Ő	Ő	Ő	Ő	1	Ő	0	1	Ő	Ő	Ő	Ő	0	1
Total	0	2	0	0	2	0	0	0	0	0	0	4	0	0	4	0	0	0	0	0	6
· ota.	· ·	-	°,	· ·	= 1	Ũ	Ũ	•	U U	•	•	•	Ũ	°,	. 1	Ũ	Ũ	Ũ	· ·	Ū	•
06:00 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
06:15 PM	Õ	Ő	Õ	Õ	0	Õ	õ	õ	Ő	Ő	Ő	0	Ő	Ő	0	Õ	Ő	Ő	Õ	õ	Ó
06:30 PM	Õ	Ő	Õ	Õ	0	Õ	Õ	Õ	Ő	0	Ő	Ő	Ő	Ő	0	Õ	0 0	Ő	Ő	Õ	ů 0
06:45 PM	0 0	Ő	Ő	0	0	Ő	Ő	Ő	Ő	0	Ő	Ő	0	Ő	0	0	0	Ő	0 0	0	0
 Total	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
i otai	0	U	U	U	0	0	U	0	0	U	U		0	0	•	U	0	0	0	0	
Grand Total	1	37	0	0	38	0	0	0	0	٥l	0	42	1	0	43	1	0	2	0	3	84
Annrch %	26	974	0	0	00	0	0 0	0	0	U	0	97 7	23	0		33 3	0	66 7	0	5	04
Total %	1.0	44	0	0	45.2	0	0	0	0	0	0	50	2.3	0	51 2	1 2	0	24	0	36	
1 Utai /0	1.4		0	0	40.2	0	0	0	0	0	0	50	1.4	0	J1.2	1.4	0	<u> </u>	0	0.0	

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Articulated Trucks

			SR-43				٦	rares R	d				SR-43				-	Trares R	d		
		So	outhboun	d			W	/estbour	nd			N	orthbou	nd			E	Eastbour	d	1	l
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	is From 07	:00 AM to	) 11:45 A	M - Peak	(1 of 1																
Peak Hour for Enti	re Intersec	tion Begir	ns at 09:0	00 AM																	
09:00 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
09:15 AM	0	2	0	0	2	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	5
09:30 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	1
09:45 AM	0	1	0	0	1	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	2
Total Volume	0	4	0	0	4	0	0	0	0	0	0	6	0	0	6	0	0	0	0	0	10
% App. Total	0	100	0	0		0	0	0	0		0	100	0	0		0	0	0	0		L
PHF	.000	.500	.000	.000	.500	.000	.000	.000	.000	.000	.000	.500	.000	.000	.500	.000	.000	.000	.000	.000	.500

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Articulated Trucks

SR-43         Trares Rd         Trares Rd <th< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></th<>																						
Seat Time				SR-43				1	Trares R	d				SR-43				-	Trares Ro	b		
Start Time         Right         Thru         Left         U-Turn         App. Total         Right         Thru         Left         U-Turn         App. Total         Int. Total           Peak Hour Analysis From 12:00 PM to 06:45 PM - Peak 1 of 1         Peak 1 of 12:00 PM to 06:45 PM - Peak 1 of 1         U-Turn         App. Total         App. Tot			S	outhbour	nd			V	Vestbour	nd			N	lorthbour	nd			E	Eastboun	d		
Peak Hour Analysis From 12:00 PM to 06:45 PM - Peak 1 of 1         Peak Hour for Entire Intersection Begins at 12:15 PM       0       1       0       1       0       0       0       0       0       0       0       0       0       0       1       0       1       2         12:15 PM       0       1       0       0       0       0       0       0       0       0       0       0       1       0       1       2         12:30 PM       0       1       0       0       0       0       0       3       0       0       0       0       0       4         12:30 PM       0       1       0       0       0       0       0       0       3       0       0       0       0       4         12:45 PM       0       1       0       1       0       1       2       1       1       1       1       1       1       1       1       1       1 </td <td>Start Time</td> <td>Right</td> <td>Thru</td> <td>Left</td> <td>U-Turn</td> <td>App. Total</td> <td>Int. Total</td>	Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour for Entire Intersection Begins at 12:15 PM         12:15 PM       0       1       0       0       0       0       0       0       0       0       1       0       1       2         12:15 PM       0       1       0       0       0       0       0       0       0       0       0       0       1       0       1       2         12:30 PM       0       1       0       0       0       0       0       3       0       0       0       0       0       4         12:30 PM       0       1       0       0       0       0       0       0       3       0       0       0       0       0       4         12:45 PM       0       1       0       0       0       0       0       0       0       0       0       1       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       1       0       0       1       0       0       0       0       0       0       0       0       0       0       0<	Peak Hour Analysi	is From 12	2:00 PM to	o 06:45 F	PM - Pea	k 1 of 1																
12:15 PM       0       1       0       1       0       1       0       1       0       1       2         12:30 PM       0       1       0       0       1       0       1       0       1       0       1       0       1       2         12:30 PM       0       1       0       0       0       0       0       3       0       0       3       0       0       0       0       4         12:45 PM       0       1       0	Peak Hour for Enti	ire Intersed	ction Begi	ns at 12:	15 PM																	
12:30 PM       0       1       0       0       1       0       0       1       0       0       0       0       0       3       0       0       3       0<	12:15 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1	0	1	2
12:45 PM       0       1       0       0       0       0       0       0       0       0       0       0       0       0       0       1         01:00 PM       0       1       0	12:30 PM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4
01:00 PM       0       1       0       0       0       0       0       0       0       3       0       0       3       0       0       0       0       0       0       4         Total Volume       0       4       0       0       4       0       0       4       0       0       4       0       0       1       0       1       1         % App. Total       0       100       0       0       0       0       0       0       0       10       0       1       0       1       1         PHF       .000       1.00       .000	12:45 PM	0	1	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
Total Volume         0         4         0         0         4         0         0         0         0         0         0         0         0         0         1         0         1         1           % App. Total         0         100         0         0         0         0         0         0         0         0         0         1         0         1         1         1           PHF         .000         1.00         .0	01:00 PM	0	1	0	0	1	0	0	0	0	0	0	3	0	0	3	0	0	0	0	0	4
% App. Total         0         100         0	Total Volume	0	4	0	0	4	0	0	0	0	0	0	6	0	0	6	0	0	1	0	1	11
PHF         .000         1.00         .000         1.00         .000         .000         .000         .000         .500         .000         .500         .000         .000         .250         .000         .250         .688	% App. Total	0	100	0	0		0	0	0	0		0	100	0	0		0	0	100	0		
	PHF	.000	1.00	.000	.000	1.00	.000	.000	.000	.000	.000	.000	.500	.000	.000	.500	.000	.000	.250	.000	.250	.688

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Combined

							(	Groups P	rinted- L	ights - Mediu	ums - Artic	ulated Tr	ucks								
			SR-43					Trares R	d				SR-43				-	Trares R	d		
		Sc	outhbou	nd			V	Vestbour	nd			N	orthbour	nd			E	Eastbour	ıd		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn 🖌	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
07:00 AM	1	40	0	0	41	4	3	2	0	9	1	102	14	0	117	2	1	3	0	6	173
07:15 AM	5	51	1	0	57	4	8	0	0	12	0	101	27	0	128	10	1	10	0	21	218
07:30 AM	8	60	2	0	70	3	13	1	0	17	2	125	25	0	152	6	3	15	0	24	263
07:45 AM	9	72	5	0	86	1	8	0	0	9	0	73	30	0	103	3	2	6	0	11	209
Total	23	223	8	0	254	12	32	3	0	47	3	401	96	0	500	21	7	34	0	62	863
08:00 AM	2	44	1	0	47	1	4	2	0	7	1	60	21	0	82	1	3	1	0	5	141
08:15 AM	0	56	1	0	57	0	4	0	0	4	2	57	11	0	70	5	0	4	0	9	140
08:30 AM	3	43	0	0	46	2	3	3	0	8	1	85	22	0	108	5	2	1	0	8	170
08:45 AM	5	48	1	0	54	1	7	2	0	10	1	74	13	0	88	6	3	7	0	16	168
Total	10	191	3	0	204	4	18	7	0	29	5	276	67	0	348	17	8	13	0	38	619
09:00 AM	2	37	1	0	40	3	7	0	0	10	3	60	13	0	76	8	1	2	0	11	137
09:15 AM	1	39	0	0	40	2	9	0	0	11	3	49	8	0	60	6	7	2	0	15	126
09:30 AM	2	43	1	0	46	1	7	0	0	8	0	47	10	0	57	8	4	6	0	18	129
09:45 AM	6	39	1	0	46	4	1	1	0	6	1	50	13	0	64	6	2	2	0	10	126
Total	11	158	3	0	172	10	24	1	0	35	7	206	44	0	257	28	14	12	0	54	518
1										1											
10:00 AM	5	43	0	0	48	1	5	1	0	7	1	49	7	0	57	2	5	6	0	13	125
10:15 AM	2	46	2	0	50	1	2	1	0	4	2	47	12	0	61	4	3	3	0	10	125
10:30 AM	3	46	1	0	50	1	4	0	0	5	1	43	4	0	48	6	2	8	0	16	119
10:45 AM	2	37	1_	0	40	1	5	1	0	7	2	51	6	0	59	5	3	2	0	10	116
Total	12	172	4	0	188	4	16	3	0	23	6	190	29	0	225	17	13	19	0	49	485
	_				1					- 1			-			-		_			
11:00 AM	5	48	1	0	54	0	4	1	0	5	0	43	3	0	46	3	4	5	0	12	117
11:15 AM	1	41	2	0	44	1	2	0	0	3	0	44	7	0	51	8	4	7	0	19	117
11:30 AM	2	47	0	0	49	3	5	1	0	9	3	39	13	0	55	7	3	6	0	16	129
11:45 AM	4	44	2	0	50	0	3	1	1	5	1	51	7	0	59	10	3	7	1	21	135
Total	12	180	5	0	197	4	14	3	1	22	4	177	30	0	211	28	14	25	1	68	498
	_									- 1								_			
12:00 PM	5	57	2	0	64	3	6	0	0	9	1	36	16	0	53	8	4	5	0	17	143
12:15 PM	7	32	1	0	40	3	4	2	0	9	0	47	10	0	57	7	3	8	0	18	124
12:30 PM	4	51	2	0	57	2	2	2	0	6	0	50	11	0	61	14	4	6	0	24	148
12:45 PM	5	51	0	0	56	3	4	0	0	7	2	42	7	0	51	9	3	9	0	21	135
Total	21	191	5	0	217	11	16	4	0	31	3	175	44	0	222	38	14	28	0	80	550
					_ 1		_			1					_ 1						
01:00 PM	4	49	1	0	54	0	7	0	0	7	2	61	9	0	72	6	4	10	0	20	153
01:15 PM	3	47	1	0	51	1	6	0	0	7	1	71	6	0	78	6	2	6	0	14	150
01:30 PM	5	49	2	0	56	1	3	1	0	5	0	62	5	0	67	13	2	6	0	21	149

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Combined

							G	aroups Pr	inted- Lig	ghts - Mediu	ums - Artio	culated Tr	ucks								_
			SR-43				٦	Frares Rd					SR-43					Trares R	d		
		S	outhbou	nd			N	/estbound	d			N	lorthbound	, k			E	Eastbour	ıd		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left l	J-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
01:45 PM	5	47	1	0	53	0	2	1	0	3	2	57	12	0	71	9	6	4	0	19	146
Total	17	192	5	0	214	2	18	2	0	22	5	251	32	0	288	34	14	26	0	74	598
			_								_										
02:00 PM	10	55	2	0	67	1	2	1	0	4	2	62	8	0	72	10	8	6	0	24	167
02:15 PM	5	/2	1	0	/8	3	2	0	0	5	2	58	11	0	/1	14	8	11	0	33	187
02:30 PM	6	/1	0	0	//	4	4	0	0	8	1	/4	16	0	91	22	2	11	0	35	211
02:45 PM	10	96	3	0	109	2	1	0	0	3	0	64	/	0	/1	6	6	6	0	18	201
Iotal	31	294	6	0	331	10	9	1	0	20	5	258	42	0	305	52	24	34	0	110	/66
	15	00	0	0	447	4	0	0	0	4	0	EO	7	0	60	10	c	4.4	0	07	010
03.00 PNI	15	99	3	0	04	1	3 5	1	0	4	3	00 01	10	0	00	10	12	6	0	27	210
03.15 FIVI	/ E	00	2	0	94	1	0		0	7	2	70	10	0	90	10	10	5	0	37	234
03.30 PIVI	5	90	37	0	106	1	3	1	0	5	2	/2	12	0	100	10	10	10	0	30	219
U3.45 PIVI	9	90	15	0	100		14	<u> </u>	0		10	200	41		250	23	40	- 13	0	4/	237
TOLAT	30	304	15	0	415	3	14	3	0	20	10	299	41	0	350	00	40	35	0	141	920
04:00 PM	4	89	3	0	96	2	6	0	0	8	4	83	9	0	96	30	10	12	0	52	252
04:15 PM	6	138	3	0	147	2	5	0	0	7	2	76	12	0	90	20	13	10	0	43	287
04:30 PM	8	102	6	0	116	4	6	1	0	11	0	100	12	0	112	13	9	8	0	30	269
04:45 PM	3	134	1	0	138	2	3	1	0	6	1	80	10	0	91	26	11	9	0	46	281
Total	21	463	13	0	497	10	20	2	0	32	7	339	43	0	389	89	43	39	0	171	1089
05:00 PM	8	124	4	0	136	2	2	2	0	6	2	96	13	0	111	18	13	12	0	43	296
05:15 PM	6	107	5	0	118	3	7	3	0	13	0	90	9	0	99	26	16	14	0	56	286
05:30 PM	8	93	2	0	103	1	4	2	0	7	3	85	14	0	102	11	9	4	0	24	236
05:45 PM	3	79	6	0	88	4	0	2	0	6	1	84	7	0	92	10	11	5	0	26	212
Total	25	403	17	0	445	10	13	9	0	32	6	355	43	0	404	65	49	35	0	149	1030
				•	70					- 1		. –			50	_		_			
06:00 PM	3	67	3	0	73	2	3	2	0	7	1	47	4	0	52	7	6	5	0	18	150
06:15 PM	2	64	2	0	68	1	5	2	0	8	2	/4	6	0	82	8	4	1	0	13	1/1
06:30 PM	5	/0	3	0	/8	2	1	1	0	4	4	62	14	0	80	8	1	5	0	14	1/6
06:45 PM	3	4/	2	0	52	2	3	1	0	6	1	33	5	0	39	4	6	3		13	110
Iotal	13	248	10	0	2/1	/	12	6	0	25	8	216	29	0	253	27	17	14	0	58	607
Grand Total	232	3079	94	0	3405	87	206	44	1	338	69	3143	540	0	3752	482	257	314	1	1054	8549
Annrch %	6.8	90.4	28	0	0400	25.7	60.9	13	03	000	18	83.8	14 4	Ő	OTOL	45.7	24.4	29.8	01	1004	0040
Total %	27	36	11	0	39.8	20.7	24	0.5	0.0	4	0.8	36.8	6.3	0	43.9	5.6	27.7	37	0.1	12.3	
Lights	223	2965	90	0	3278	83	206	40	0	329	68	2991	520	0	3579	471	256	305	1	1033	8219
% Lights	96.1	96.3	95.7	0 0	96.3	95.4	100	90.9	õ	97.3	98.6	95.2	96.3	Ő	95.4	97.7	99.6	97.1	100		96.1
Mediums	8	77	4	0	89	4	0	4	1	9	1	110	19	0	130	10	1	7	0	18	246
% Mediums	3.4	2.5	4.3	õ	2.6	4.6	Õ	9.1	100	2.7	1.4	3.5	3.5	õ	3.5	2.1	0.4	2.2	Õ	1.7	2.9
Articulated Trucks	1	37	0	0	38	0	0	0	0	0	0	42	1	0	43	1	0	2	0	3	84
% Articulated Trucks	0.4	1.2	0	0	1.1	0	0	0	0	0	0	1.3	0.2	0	1.1	0.2	0	0.6	0	0.3	1

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Combined

			SR-43				1	Frares R	d				SR-43				-	Trares Ro	b		
		S	outhboun	d			V	Vestbour	nd			N	lorthboui	nd			E	astboun	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	is From 07	:00 AM to	o 11:45 A	M - Pea	k 1 of 1																
Peak Hour for Enti	re Intersec	tion Begi	ns at 07:0	00 AM																	
07:00 AM	1	40	0	0	41	4	3	2	0	9	1	102	14	0	117	2	1	3	0	6	173
07:15 AM	5	51	1	0	57	4	8	0	0	12	0	101	27	0	128	10	1	10	0	21	218
07:30 AM	8	60	2	0	70	3	13	1	0	17	2	125	25	0	152	6	3	15	0	24	263
07:45 AM	9	72	5	0	86	1	8	0	0	9	0	73	30	0	103	3	2	6	0	11	209
Total Volume	23	223	8	0	254	12	32	3	0	47	3	401	96	0	500	21	7	34	0	62	863
% App. Total	9.1	87.8	3.1	0		25.5	68.1	6.4	0		0.6	80.2	19.2	0		33.9	11.3	54.8	0		
PHF	.639	.774	.400	.000	.738	.750	.615	.375	.000	.691	.375	.802	.800	.000	.822	.525	.583	.567	.000	.646	.820

POR 43 at Trares Rd 5/4/2022 7:00AM-7:00PM Combined

			SR-43					Frares R	d				SR-43					Trares R	d		
		S	outhbour	nd			V	Vestbour	nd			Ν	lorthbour	nd			E	Eastbour	d		
Start Time	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Right	Thru	Left	U-Turn	App. Total	Int. Total
Peak Hour Analysi	s From 12	:00 PM to	06:45 F	PM - Pea	k 1 of 1																
Peak Hour for Enti	re Intersec	tion Begi	ns at 04:	15 PM																	
04:15 PM	6	138	3	0	147	2	5	0	0	7	2	76	12	0	90	20	13	10	0	43	287
04:30 PM	8	102	6	0	116	4	6	1	0	11	0	100	12	0	112	13	9	8	0	30	269
04:45 PM	3	134	1	0	138	2	3	1	0	6	1	80	10	0	91	26	11	9	0	46	281
05:00 PM	8	124	4	0	136	2	2	2	0	6	2	96	13	0	111	18	13	12	0	43	296
Total Volume	25	498	14	0	537	10	16	4	0	30	5	352	47	0	404	77	46	39	0	162	1133
% App. Total	4.7	92.7	2.6	0		33.3	53.3	13.3	0		1.2	87.1	11.6	0		47.5	28.4	24.1	0		
PHF	.781	.902	.583	.000	.913	.625	.667	.500	.000	.682	.625	.880	.904	.000	.902	.740	.885	.813	.000	.880	.957

For converting partial day turning movements counts to seasonally adjusted 24 hour (AADT) counts. Yellow boxes require user input. Scroll down for 24 hour diagrams. Use the Seasonal AdjuistmtFactors\_YYYY spreadsheet to lookup seasonal factor.

Use Avg TD by FC.xsl.	x to compute I	P&A B&C I	FACTORs.	Max									
PART 1	: INPUT PAR	TIAL DAY	P&A VEHI	ICLES					ROUTE	SR-43			
	PARTIAL C	OUNT * F/	ACTOR * S	EASONAL	FACTOR	= 24 HR F	P&A						
SOUTH LEG	SR-43	FC =	Rural Prin	ncipal Arter	northboun	d	APROACH	DEPART		0001700 0 00			
	IT	THRU	RT	20	3186	145	3351	3295	LT	THRU	RT	TOTAL	TOTAL
P&A FACTOR	1.281	1.281	1.281	25.62	4081.27	185.745	4292.63	4212.71	30	4080	190	4300	4210
SEASONAL FACTOR	0.922	0.922	0.922	23.6216	3762.93	171.257	3957.81	3876.55	20	3760	170	3950	3870
WEST LEG	Randolph R	FC =	Rural Maj	or Collecto	eastbound		APROACH	DEPART					
	FACTOR			LT	THRU	RT	TOTAL	TOTAL		WEST LEG		APROACH	DEPART
	LT 1 105	THRU 1 105	RT 1 105	108	140	43 51 295	291	399	LT 120	170	RT 50	TOTAL	TOTAL 510
SEASONAL E	0.865	0.865	0.865	111.637	144,715	44.448	300,799	450.82	110	140	40	290	440
NORTH LEG	SR-43	FC =	Rural Prin	ncipal Arter	southbour	d	APROACH	DEPART					
	FACTOR			LT	THRU	RT	TOTAL	TOTAL		NORTH LEG		APROACH	DEPART
	LT	THRU	RT	23	3185	223	3431	3321	LT	THRU	RT	TOTAL	TOTAL
P&A FACTOR	1.281	1.281	1.281	29.463	4079.99	285.663	4395.11	4243.1	30	4080	290	4400	4240
SEASUNAL F	0.922	0.922	0.922	27.1649	3/61./5	263.381	4052.29	3902.92	30	3760	260	4050	3900
EASTLEG	FACTOR	FC =	Rural Loc	al Road	THRI	PT	APROACH	DEPART		FASTIEG			DEDART
	LT	THRU	RT	67	156	27	250	308	LT	THRU	RT	TOTAL	TOTAL
P&A FACTOR	1.214	1.214	1.214	81.338	189.384	32.778	303.5	382.508	80	190	30	300	390
SEASONAL F	0.865	0.865	0.865	70.3574	163.817	28.353	262.528	343.136	70	160	30	260	340
PART 2:	INPUT PAR		B&C VEH						ROUTE	SR-43			
SOUTH LEG	SR-43	FC =	Rural Prin	ncipal Arte	northboun	d	APROACH	DEPART					
	FACTOR	<b>.</b>		LT	THRU	RT	TOTAL	TOTAL		SOUTH LEG		APROACH	DEPART
	LT	THRU	RT	0	173	5	178	131	LT	THRU	RT	TOTAL	TOTAL
B&C FACTOR	1.392	1.392	1.392	0	240.816	6.96	247.776	181.794		0 240	10	250	180
SEASONAL FACTOR	0.922	0.922	0.922	0	222.032	6.41712	228.449	167.408		220	10	230	160
WEST LEG	Randolph R	FC =	Rural Maj	or Collecto	eastbound	вт	APROACH	DEPART		WERTLEC			DEDADT
	IT	THRU	RT	3	2	KI 0	101AL 5	I U I AL	IТ	THRU	RT	TOTAI	TOTAL
B&C FACTOR	1.189	1.189	1.189	3.5661	2.3774	0	5.9435	12.342		0 0	0	0	10
SEASONAL FACTOR	0.865	0.865	0.865	3.08468	2.05645	0	5.14113	11.3106		0 0	0	0	10
NORTH LEG	SR-43	FC =	Rural Prin	ncipal Arter	southboun	d	APROACH	DEPART					
	FACTOR	-		LT	THRU	RT	TOTAL	TOTAL		NORTH LEG		APROACH	DEPART
	LT 1 202	THRU	RT 1 202	208	128	11 126	470 949	177	LT	THRU	RT	TOTAL	TOTAL
SEASONAL FACTOR	0.922	0.922	0.922	269.530	164 278	10 2674	4/0.040	240.000	29	0 160 0 160	10	400	240
FASTIEG	Randolph R	EC =	Rural Loc	al Road	westhound	1	APROACH	DEPART					
2307 220	FACTOR	1 .0	rtarar 200	LT	THRU	RT	TOTAL	TOTAL		EAST LEG		APROACH	DEPART
	LT	THRU	RT	3	1	1	5	215	LT	THRU	RT	TOTAL	TOTAL
B&C FACTOR	1.206	1.206	1.206	3.618	1.206	1.206	6.03	298.873		0 0	0	0	300
SEASONAL FACTOR	0.805	0.865	0.865	3.12957	1.04319	1.04319	5.21595	275.426		) 0	0	0	280
					1		SR-43						
P&A 24 HR						Ļ	7950	Ŷ					
					000	4050	20	3900					
-					260	3760	30			t 20	<b>`</b>		Pandolph P
		←	440			*	-			L 30 ← 16	, 50	260	←
		730		110	t					F 70	)		600
	_	. →	290	140	→ -								
-	Randolph R	oad		40	1		t⊓ 20	1	170			340	<b>→</b>
						3870	20	3950	170				
					1								
						т	7820	Ť					
						т	7820 SR-43	t					
						т	7820 SR-43 SR-43	¢					
B&C 24 HR						⊤ ↓ 440	7820 SR-43 SR-43 660	↓ ↑ 220					
B&C 24 HR					10	⊤ ↓ 440 160	7820 SR-43 SR-43 660 270	↓ ↑ 220					
B&C 24 HR			10		10 +	⊤ ↓ 440 160 ↓	7820 SR-43 SR-43 660 270 -	↓ ↑ 220		t O			Randolph Ro
B&C 24 HR		10	10		10 	⊤ 440 160 ↓	7820 SR-43 660 270	↓ ↑ 220		t 0 ← 0		0	Randolph Ro ← 280
B&C 24 HR		← 10 →	10	0	10 + 1 +	↑ 440 160 ↓	7820 SR-43 SR-43 660 270 L	↓ ↑ 220		t 0 ← 0 F 0		0	Randolph Ro ← 280
B&C 24 HR	Randolph R	← 10 → oad	10 0	0 0 0		⊤ 440 160 ↓	7820 SR-43 660 270 	↓ 1 220 ↑	r,	t 0 ← 0 F 0		0 280	Randolph Ro ← 280 →
B&C 24 HR	Randolph R	← 10 → oad	10 0	0 0 0	10 ↓ 1 1 1 1	T ↓ 440 160 ↓	7820 SR-43 660 270 ↓ 0	↓ ↑ 220 ↑ 220 220	r 10	t 0 ← 0 F 0		0 280	Randolph Ro ← 280 →
B&C 24 HR .	Randolph R	← 10 → oad	10 0	0 0 0	10 ↓ 1 1 1	⊤ ↓ 440 160 ↓ 160 ↑	7820 SR-43 660 270 ↓ 0 390	↓ ↑ 220 1 220 230 ↓	r 10	t 0 ← 0 F 0		0 280	Randolph Ro ← 280 →
B&C 24 HR	Randolph R	← 10 → oad	10 0	0 0 0		⊤ ↓ 440 160 ↓ 160 ↑	7820 SR-43 660 270 ↓ 0 390 SR-43	↓ 1 220 1 220 230 ↓	r+ 10	t 0 ← 0 F 0		0 280	Randolph Ro ← 280 →
B&C 24 HR	Randolph R	← 10 → oad	10 0	0 0 0	10 ↓ ↓ ↓ ↓ ↓	T ↓ 440 160 ↓ 160 ↑	7820 SR-43 660 270 - - 0 390 SR-43 SR-43	↓ 1 220 1 220 230 ↓	r• 10	t 0 ← 0 F 0		0 280	Randolph Ro ← 280 →
B&C 24 HR	Randolph R	← 10 → oad	10 0	0 0 0		T ↓ 440 160 ↓ 160 ↑	7820 SR-43 660 270 5 0 390 SR-43 8610	↓ ↑ 220 230 ↓ ↑	r+ 10	t 0 ← 0 F 0		0 280	Randolph Ro ← 280 →
B&C 24 HR	Randolph R	← 10 → oad	10 0	0 0 0	10 1 1 1 270	T ↓ 440 160 ↓ 160 ↑ 160 1 4490 3920	7820 <u>SR-43</u> 660 270 - 0 390 <u>SR-43</u> 8610 300	↓ <sup>↑</sup> 220 <sup>↑</sup> 220 230 ↓ <sup>↑</sup> 4120	r 10	L 0 ← 0 F 0		0 280	Randolph Ro ← 280 →
B&C 24 HR	Randolph R	← 10 → oad	10 0	0 0 0		T ↓ 440 160 ↓ 160 ↑ 160 ↑ ↓ 4490 3920 ↓	7820 SR-43 660 270 - - 0 390 SR-43 8610 300 -	↓ <sup>↑</sup> <sup>220</sup> <sup>230</sup> ↓ <sup>↑</sup> <sup>4120</sup>	r 10	L 0 ← 0 F 0		0 280	Randolph Ra ← 280 →
B&C 24 HR	Randolph R	← 10 → oad	10 0	0 0 0		T ↓ 440 160 ↓ 160 ↑ ↓ 4490 3920 ↓	7820 <u>SR-43</u> 660 270 <u>5</u> 0 <u>390</u> <u>SR-43</u> 8610 <u>300</u> <u>5</u>	↓ <sup>↑</sup> <sup>220</sup> <sup>230</sup> ↓ <sup>↑</sup> <sup>4120</sup>	r 10	t 0 ← 0 F 0 t 30 ← 16	)	280	Randolph Rα ← 280 → Randolph Rα ←
B&C 24 HR	Randolph R	← 10 → oad ~ 740	10 0 450	0000		T ↓ 440 160 ↓ 160 ↑ ↓ 4490 3920 ↓	7820 SR-43 660 270 0 390 SR-43 8610 300 1	↓ ↑ 220 230 ↓ ↑ 4120	r≠ 10	L 0 ← 0 F 0 L 33 ← 14	) 50 )	0 280 260	Randolph Ra ← 280 → Randolph Ra ← 880
B&C 24 HR	Randolph R	← 10 → oad 740 → oad	10 0 450 290	0 0 0 110 140 40		T ↓ 440 160 ↓ 160 ↑ 4490 3920 ↓	7820 SR-43 660 270 - - - - - - - - - - - - - - - - - - -	↓ ↑ 220 230 ↓ ↑ 4120 ↑	r 10	L 0 ← 0 F 0 L 33 ← 11 F 70	) 50 )	0 280 260	Randolph Ra ← 280 → Randolph Ra ← 880 →
B&C 24 HR TOTAL AADT	Randolph R Randolph R	← 10 → oad ← 740 → oad	10 0 450 290	0 0 0 110 140 40		T ↓ 440 160 ↓ 160 ↑ 160 ↑ 4490 3920 ↓	7820 SR-43 660 270 270 0 390 SR-43 8610 300 20	↓ ↑ 220 220 230 ↓ ↑ 4120 ↑ 3980	r 10 180	L 0 ← 0 F 0 L 33 ← 16 F 70	) 60	0 280 260 620	Randolph Ra ← 280 → Randolph Ra ← 880 →
B&C 24 HR	Randolph R Randolph R	10 → oad 740 → oad	10 0 450 290	0 0 0 110 140 40		T ↓ 440 160 ↓ 160 ↑ 160 ↑ ↓ 4490 3920 ↓ ↓	7820 SR-43 660 270 - 0 390 SR-43 8610 300 - 20 0 -	↓ ↑ 220 230 ↓ ↑ 4120 ↑ 3980 4180	г. 10 180	L 0 ← 0 F 0 L 33 ← 11 F 70	) 50 )	0 280 260 620	Randolph Ra ← 280 → Randolph Ra ← 880 →

For converting partial day turning movements counts to seasonally adjusted 24 hour (AADT) counts. Yellow boxes require user input. Scroll down for 24 hour diagrams. Use the Seasonal AdjuistmtFactors\_YYYY spreadsheet to lookup seasonal factor.

Use Avg TD by FC.xslx	to compute P	P&A B&C I	FACTORs.	May									
PART 1:	INPUT PAR	TIAL DAY	P&A VFHI	ICLES					ROUTE	SR-43			
	PARTIAL CO	OUNT * F/	ACTOR * S	EASONAL	FACTOR	= 24 HR I	P&A		HOULE	ore to			
SOUTH LEG	SR-43	FC =	Rural Prin	cipal Arter	northboun	d	APROACH	DEPART					
				LT	THRU	RT	TOTAL	TOTAL		SOUTH LEG		APROACH	DEPART
	LT	THRU	RT	520	2991	68	4504.7	3476	LT	THRU	RT	TOTAL	TOTAL
SEASONAL EACTOR	1.281	1.281	1.281	614 162	3831.47	87.108	4584.7	4418.52	610	3830	90	4590	4420
SEASONAL FACTOR	0.922	0.922	0.922	014.103	3552.62	00.3130	4227.09	4036.51	610	3530	80	4220	4030
WESTLEG	Trares Road	FC=	Rural Loc	al Road	eastbound	БТ	APROACH	DEPART		WERTLEC			DEDADT
	IT	THRU	RT	305	256	471	101AL	0/0	1.1	THRU	PT	TOTAL	TOTAL
P&A FACTOR	1.214	1.214	1.214	370.27	310,784	571.794	1252.85	1201.87	370	310	570	1250	1210
SEASONAL F	0.865	0.865	0.865	320.284	268.828	494.602	1083.71	1093.87	320	270	490	1080	1090
NORTH LEG	SR-43	EC =	Rural Prin	ncinal Arte	southhour	d	APROACH	DEPART		-			
	FACTOR			LT	THRU	RT	TOTAL	TOTAL		NORTH LEG		APROACH	DEPART
	LT	THRU	RT	90	2965	223	3278	3379	LT	THRU	RT	TOTAL	TOTAL
P&A FACTOR	1.281	1.281	1.281	115.29	3798.17	285.663	4199.12	4302.5	120	3800	290	4210	4300
SEASONAL F	0.922	0.922	0.922	106.297	3501.91	263.381	3871.59	3940.06	110	3500	260	3870	3940
EAST LEG	Trares Road	FC =	Rural Loc	al Road	westbound	i	APROACH	DEPART					
	FACTOR	•		LT	THRU	RT	TOTAL	TOTAL		EAST LEG		APROACH	DEPART
	LT	THRU	RT	40	206	83	329	414	LT	THRU	RT	TOTAL	TOTAL
P&A FACTOR	1.214	1.214	1.214	48.56	250.084	100.762	399.406	513.182	50	250	100	400	520
SEASONAL F	0.865	0.865	0.865	42.0044	216.323	87.1591	345.486	455.439	40	220	90	350	460
			D00	0.55					201	00.45	_		
PART 2:	PARTIAL CO		B&C VEH	ICLES					ROUTE	SR-43			
SOUTHIEG	ISR-43		Rural Prin	ncipal Arte	northboun	d	APROACH	DEPART					
000.11 220	FACTOR		. terer i fil	LT	THRU	RT	TOTAL	TOTAL		SOUTH LEG		APROACH	DEPART
	LT	THRU	RT	-451	152	472	173	129	LT	THRU	RT	TOTAL	TOTAL
B&C FACTOR	1.392	1.392	1.392	-627.79	211.584	657.024	240.816	176.778	-630	210	660	240	170
SEASONAL FACTOR	0.922	0.922	0.922	-578.82	195.08	605.776	222.032	161.958	-580	200	610	230	160
WEST LEG	Trares Road	FC =	Rural Loc	al Road	eastbound		APROACH	DEPART					
	FACTOR	-	-	LT	THRU	RT	TOTAL	TOTAL		WEST LEG		APROACH	DEPART
	LT	THRU	RT	9	1	11	21	-442	LT	THRU	RT	TOTAL	TOTAL
B&C FACTOR	1.206	1.206	1.206	10.854	1.206	13.266	25.326	-615.26	10	0 0	10	20	-620
SEASONAL FACTOR	0.865	0.865	0.865	9.38871	1.04319	11.4751	21.907	11.5508	10	0 0	10	20	-570
NORTH LEG	SR-43	FC =	Rural Prin	ncipal Arter	southbour	d	APROACH	DEPART					
	FACTOR			LT	THRU	RT	TOTAL	TOTAL		NORTH LEG		APROACH	DEPART
	LT	THRU	RT	7	114	9	130	165	LT	THRU	RT	TOTAL	TOTAL
B&C FACTOR	1.392	1.392	1.392	9.744	158.688	12.528	180.96	227.262	10	160	10	180	220
SEASONAL FACTOR	0.922	0.922	0.922	0.90397	140.31	11.5506	100.045	206.042	7.	150	10	170	210
EASTLEG	I rares Road	FC =	Rural Loc	al Road	westbound	1	APROACH	DEPART					
	EACTOR				TUDII	DT	TOTAL	TOTAL		EASTIEC		ADDOACH	DEDADT
	FACTOR	THRU	RT		THRU	RT 4	TOTAL 8	TOTAL 480	LT	EAST LEG THRU	RT	APROACH	DEPART
B&C FACTOR	FACTOR LT 1.206	THRU	RT 1.206	LT 4.824	THRU 0	RT 4.824	TOTAL 8 9.648	TOTAL 480 667.974	LT	EAST LEG THRU	<b>RT</b> 0	APROACH TOTAL 0	DEPART TOTAL 670
B&C FACTOR SEASONAL FACTOR	FACTOR LT 0.865	THRU 1.206 0.865	RT 1.206 0.865	LT 4.824 4.17276	THRU 0 0	RT 4.824 4.17276	TOTAL 8 9.648 8.34552	TOTAL 480 667.974 615.803	LT	EAST LEG THRU 0 0 0 0	RT 0 0	APROACH TOTAL 0 0	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR	FACTOR LT <u>1.206</u> 0.865	THRU 1.206 0.865	RT 1.206 0.865	LT 4.824 4.17276	<b>THRU</b> 0 0	RT 4.824 4.17276	TOTAL 8 9.648 8.34552	TOTAL 480 667.974 615.803	LT	EAST LEG THRU 0 0 0 0	RT 0 0	APROACH TOTAL 0 0	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR	FACTOR LT 1.206 0.865	THRU 1.206 0.865	RT 1.206 0.865	LT 4.824 4.17276	THRU 0 0	RT 4.824 4.17276	TOTAL 8 9.648 8.34552 SR-43	TOTAL 480 667.974 615.803	LT (	EAST LEG THRU 0 0 0 0	RT 0 0	APROACH TOTAL 0 0	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865	RT 1.206 0.865	LT 4.824 4.17276	THRU           0           0	RT 4.824 4.17276 ↓ 2870	TOTAL 8 9.648 8.34552 SR-43 7810	TOTAL 480 667.974 615.803		EAST LEG THRU 0 0 0 0	RT 0 0	APROACH TOTAL 0 0	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865	RT 1.206 0.865	LT 4.824 4.17276	260	RT 4.824 4.17276 ↓ 3870 3500	TOTAL 8 9.648 8.34552 SR-43 7810 110	TOTAL 480 667.974 615.803 1 3940		EAST LEG THRU 0 0 0 0	RT 0 0	APROACH TOTAL 0 0	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865	RT 1.206 0.865	LT 4.824 4.17276	THRU 0 0 260 ↓	RT 4.824 4.17276 ↓ 3870 3500 ↓	TOTAL 8 9.648 8.34552 SR-43 7810 110	TOTAL 480 667.974 615.803 ↑ 3940		EAST LEG THRU 0 0 0 0	RT 0 0	APROACH TOTAL 0 0	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865	RT 1.206 0.865 1090	LT 4.824 4.17276	U       0    <	RT 4.824 4.17276 ↓ 3870 3500 ↓	TOTAL 8 9.648 8.34552 SR-43 7810 110 4	TOTAL 480 667.974 615.803 ↑ 3940		EAST LEG THRU 0 0 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 350	DEPART TOTAL 670 620 Trares F
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 0.865	THRU 1.206 0.865	RT 1.206 0.865 1090	LT 4.824 4.17276	THRU       0       0       0       0       0       0       260       ↓	RT 4.824 4.17276 ↓ 3870 3500 ↓	TOTAL 8 9.648 8.34552 SR-43 7810 110 └	TOTAL 480 667.974 615.803 ↑ 3940		EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 350	DEPART TOTAL 670 620 Trares F ← 810
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 0.865	THRU 1.206 0.865 0.865 ← 2170 →	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270	THRU       0	RT 4.824 4.17276 ↓ 3870 3500 ↓	TOTAL 8 9.648 8.34552 SR-43 7810 110 ↓	TOTAL 480 667.974 615.803 ↑ 3940		EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	<b>APROACH</b> <b>TOTAL</b> 0 0 0 350	DEPART TOTAL 670 620 Trares F ← 810
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	THRU           0	RT 4.824 4.17276 ↓ 3870 3500 ↓	TOTAL 8 9.648 8.34552 SR-43 7810 110	TOTAL 480 667.974 615.803 ↑ 3940		EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	аргоасн ТОТАL 0 0 0 350 460	DEPART TOTAL 670 620 Trares F € 810 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 →	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	THRU           0           0           0           0           0           260           ⊥           1           1	RT 4.824 4.17276 ↓ 3870 3500 ↓ 4020	TOTAL 8 9.648 8.34552 SR-43 7810 110 - -	TOTAL 480 667.974 615.803 1 3940	LT (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	аркоасн ТОТАL 0 0 0 350 460	DEPART TOTAL 670 620 Trares F ← 810 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR -	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 →	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	THRU       0	RT 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑	TOTAL 8 9.648 8.34552 SR-43 7810 110 - -	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓	LT (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	аркоасн ТОТАL 0 0 0 350 460	DEPART TOTAL 670 620 Trares F ← 810 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 0.865	THRU 1.206 0.865 2170 ← 1	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	THRU 0 0 260 ↓ 1 1	RT 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑	TOTAL 8 9.648 8.34552 SR-43 7810 110 - - 610 8250 SR-43	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓	LT (2)	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	аркоасн ТОТАL 0 0 0 350 460	DEPART TOTAL 670 620 Trares F ← 810 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 ← 1	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	THRU           0           0           0           260           ↓           ↓           ↓	RT 4.824 4.17276 3870 3500 ↓ 4030 ↑	TOTAL 8 9.648 8.34552 SR-43 7810 110 - 610 82500 SR-43 SR-43	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓		EAST LEG THRU 0 0 0 0 0 1 99 ← 22 Γ 40	RT 0 0	<b>APROACH</b> <b>TOTAL</b> 0 0 0 350 460	DEPART TOTAL 670 620 Trares F ← 810 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 ← 1	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	THRU       0	RT 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ ↓	TOTAL 8 9.648 8.34552 SR-43 7810 110 - - 610 82500 SR-43 380	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓		EAST LEG THRU 0 0 0 1 0 1 0 1 0 0 0	RT 0 0	APROACH TOTAL 0 0 350 460	DEPART TOTAL 670 620 Trares F ← 810 →
B&C FACTOR SEASONAL FACTOR P8A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 →	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	Image: 1       0 </td <td>RT 4.824 4.17276 3870 3500 ↓ 4030 ↑ 4030 ↑</td> <td>TOTAL 8 9.6448 8.34552 SR-43 7810 110 4 610 8250 SR-43 380 4</td> <td>total 480 667.974 615.803 1 3940 ↑ 3530 4220 ↓ 1 210</td> <td></td> <td>EAST LEG THRU ) 0 0 (1) 0 (1)</td> <td>RT 0 0</td> <td>APROACH TOTAL 0 0 350 460</td> <td>DEPART TOTAL 670 620 Trares F € 810 →</td>	RT 4.824 4.17276 3870 3500 ↓ 4030 ↑ 4030 ↑	TOTAL 8 9.6448 8.34552 SR-43 7810 110 4 610 8250 SR-43 380 4	total 480 667.974 615.803 1 3940 ↑ 3530 4220 ↓ 1 210		EAST LEG THRU ) 0 0 (1)	RT 0 0	APROACH TOTAL 0 0 350 460	DEPART TOTAL 670 620 Trares F € 810 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 →	RT 1.206 0.865	LT 4.824 4.17276 320 270 490	THRU           0	RT 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ ↓ 170 150 ↓	TOTAL 8 9.6448 8.34552 SR-43 7810 110  610 82500 SR-43 380 10 	total 480 667.974 615.803 1 3940 ↑ 3530 4220 ↓ 1 210		EAST LEG THRU 0 0 0 0 0 1 0 1 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 350 460	DEPART TOTAL 670 620 Trares F ← 810 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 →	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	THRU           0           0           0           0           0           0           0           0           0           0           0           0           0           1           1           1           10	RT 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ ↓ 1700 150 ↓	TOTAL 8 9.648 8.34552 SR-43 7810 110 5 610 82500 SR-43 380 10 1	totaL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓ ↑ 210	LT (	EAST LEG THRU 0 0 0 0 0 1 9 4 22 7 40 1 40 1 0 0 1 90 4 22 7 40 1 0 0 1 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 350 460	DEPART TOTAL 670 620 Trares F € 810 →
B&C FACTOR SEASONAL FACTOR P8A 24 HR 	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 → 1 -550	RT 1.206 0.865 1090 1080	LT 4.824 4.17276 320 270 490	THRU       0       0       0       0       0       0       1       1       1       10       1	RT 4.824 4.7276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓	TOTAL 8 9.6448 8.34552 SR-43 7810 110 5 610 82500 SR-43 380 10 10	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓ 1 210	LT (	EAST LEG THRU → 0 	RT 0 0	APROACH TOTAL 0 0 0 350 460	DEPART TOTAL 670 620 ← Trares F 810 → Trares F 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 → -550 →	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490 10 0	THRU       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0       10       1       1	RT 4.824 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 1700 150 ↓	TOTAL 8 9.6448 8.34552 SR-43 7810 110 - 610 8250 SR-43 380 10 - -	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓ 10	LT (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0 0	аркоасн тотац 0 0 350 460 0	DEPART TOTAL 670 620 Trares F ← 810 → Trares F 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 → 4 -550 →	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490 10 0 10	THRU           0           0           0           0           0           0           0           0           0           0           0           0           0           10           110           12	RT 4.824 4.77276 ↓ 3870 3500 ↓ 4030 ↑ ↓ 170 150 ↓	TOTAL 8 9.6448 8.345522 SR-43 7810 110 5610 8250 SR-43 380 10 500	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3940 ↓ 1 210		EAST LEG THRU 0 0 0 0 0 1 9 4 22 Γ 40 Γ 40 Γ 0 Γ 0	RT 0 0 0	APROACH TOTAL 0 0 0 0 3550 460 460 0 0 620	DEPART TOTAL 670 620 → Trares F 810 → Trares F 620 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR 	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 → 1 -550 →	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490 10 0 10	THRU       0       10       1       1       1       1       1	RT 4.824 4.824 4.7276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160	TOTAL 8 9.648 9.648 8.34552 SR-43 7810 110 5610 82500 SR-43 380 10 58-43 380 10 58-43 380 10 58-43 58-43 58-43 58-43 58-43 58-43 58-43 58-43 58-43 58-43 58-43 58-43 59-58 59-	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓ 1 210		EAST LEG THRU 0 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1	RT 0 0	аркоасн тота 0 0 0 0 350 460 0 0 620	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR 	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 → 2170 → 4	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490	THRU       0       10       1       1       1	RT 4.824 4.824 4.824 4.824 4.824 4.824 3870 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑	TOTAL 8 9.6448 8.345522 SR-43 7810 110 4 610 82500 SR-43 380 10 4 5580 390	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3530 4220 ↓ ↑ 210 ↑ 210	LT ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	EAST LEG THRU 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	RT 0 0	APROACH TOTAL 0 0 0 350 460 0 620	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR 	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 → 1	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490 10 10	THRU       0	RT 4.824 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑	TOTAL 8 8.9.648 9.648 8.34552 SR-43 7810 110 5610 8250 SR-43 380 10 58-43 380 58-43 390 SR-43	TOTAL 480 667.974 615.803 ↑ 3530 4220 ↓ ↑ 210 ↑ 200 230 ↓	LT ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 0 3550 460 0 620	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR 	FACTOR LT 1.206 0.865	THRU 1 2006 0.865 2170 ↓ -550 ↓	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490	THRU         0]           0         0           260            J            J            J            J	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑	TOTAL 8 9.6448 8.34552 SR-43 7810 110 5610 82500 SR-43 380 10 58.43 380 10 58.43 380 390 SR-43 SR-43 SR-43 SR-43	TOTAL 460 67.974 615.803 † 3940 † 23530 4220 ↓ 1 210	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THU 0 0 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1	RT 0 0	APROACH TOTAL 0 0 0 350 460 0 620	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR 	FACTOR LT 1.206 0.865 Trares Road	1 THRU 1.206 0.865 2170 ↓ 	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490	THRU         0]         0]         0 </td <td>RT 4 4.824 4.824 4.824 4.824 4.824 4.824 4.824 4.824 1.827 ↓ 1.870 ↓ 1.870 ↓ 1.824 ↓ 1.80 ↑ 1.80 ↑ 1.80 ↑ 1.80 ↑ 1.80 ↓ 1.824 ↓ 1.824 ↓ 1.824 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.707 ↓</td> <td>TOTAL 8 9.648 9.648 8.34552 SR-43 7810 110 587 610 8250 SR-43 380 10 588 390 SR-43 SR-43 SR-43 8190</td> <td>TOTAL 480 667.974 615.803 ↑ 3940 ↑ 1 210 ↑ 210 ↑ 200 230 ↓</td> <td>LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (</td> <td>EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td> <td>RT 0 0</td> <td>APROACH TOTAL 0 0 0 350 460 0 620</td> <td>DEPART TOTAL 670 620</td>	RT 4 4.824 4.824 4.824 4.824 4.824 4.824 4.824 4.824 1.827 ↓ 1.870 ↓ 1.870 ↓ 1.824 ↓ 1.80 ↑ 1.80 ↑ 1.80 ↑ 1.80 ↑ 1.80 ↓ 1.824 ↓ 1.824 ↓ 1.824 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.827 ↓ 1.707 ↓	TOTAL 8 9.648 9.648 8.34552 SR-43 7810 110 587 610 8250 SR-43 380 10 588 390 SR-43 SR-43 SR-43 8190	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 1 210 ↑ 210 ↑ 200 230 ↓	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 350 460 0 620	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR 	FACTOR LT 1.206 0.865	1 THRU 1.206 0.865 2170 ↓ -550 ↓	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490 10 0 0	THRU         0]           0]         0           260	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 100 ↑ 160 ↑ ↓ 160 ↑ ↓ 160 ↑	TOTAL 8 8.9.648 8.34552 SR-43 7810 110 5610 8250 SR-43 380 10 58-43 380 38-43 8100 38-43 81000 8100 81000 81000 81000 8100 8100 8100 81000 8100	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 35530 4220 ↓ ↑ 210 ↑ 210	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 0 350 460 0 620	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR B&C 24 HR	FACTOR LT 1.206 0.865	1 HRU 1 2066 0.865 2170 ↓ -550 ↓	RT 1.206 0.865 1090 1080 -570 20	LT 4.824 4.17276 320 270 490	THRU         01           0         0           0         0           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑ 160 ↑ ↓	TOTAL 8 9.648 9.648 9.648 8.34552 SR-43 7810 110 580 8250 0 SR-43 380 10 580 390 SR-43 380 10 10 580 390 SR-43 381 10 10 10 10 10 10 10 10 10 1	TOTAL 480 667.974 615.803 1 3940 1 3940 1 1 200 230 2 1 1 1 210	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 3550 460 0 620	DEPART TOTAL 670 620 Trares F ← 810 → Trares F ← 620 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR B&C 24 HR	FACTOR LT 1.206 0.865	1 THRU 1.206 0.865 2170 ↓ 4 -550 ↓	RT 1.206 0.865 1090 1080 -570 20 520	LT 4.824 4.17276 320 270 490	THRU         0]           0]         0           260	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑ ↓ 4040 ↓ ↓ 4040 ↓ ↓ 150 ↓ ↓ 150 ↓	TOTAL 8 9.648 9.648 8.34552 SR-43 7810 110 5610 8250 SR-43 380 10 5884 380 10 5884 380 10 5884 380 10 10 5880 390 SR-43 8190 120 120 120	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 1 210 ↑ 210 ↑ 210 ↓ ↑ 1 210	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THRU 0 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 350 460 0 620	DEPART TOTAL 670 620 Trares F 610 → Trares F 620 → Trares F 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR 	FACTOR LT 1.206 0.865	THRU 1.206 0.865 2170 ← 1 -550 → 1 1620	RT 1.206 0.865 1090 1080 -570 20 520	LT 4.824 4.17276 320 270 490 10 0 10 330	THRU         0]           0]         0           260	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑ ↓ 4040 3850 ↓	TOTAL 8 8.34552 9.648 8.34552 SR-43 7810 110 5610 8250 SR-43 380 10 588-43 380 390 390 38-43 8190 120 L	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 35530 4220 ↓ ↑ 210 ↑ 210	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 0 0 460 0 620 0 620	DEPART TOTAL 670 620
B&C FACTOR SEASONAL FACTOR P&A 24 HR B&C 24 HR 	FACTOR LT 1.206 0.865	1 THRU 1 1206 0.865 2170 ↓ -550 ↓ 1620 ↓	RT 1.206 0.865 1090 1080 -570 20 520 1100	LT 4 4.824 4.17276 320 270 490 10 0 10	THRU         01           0         0           0         0           0         0           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑ ↓ 4040 3650 ↓	TOTAL 8 8.34552 SR-43 7810 110 - 610 8250 SR-43 380 10 - 580 390 SR-43 SR-43 380 10 - 580 390 SR-43 SR-43 SR-43 10 - 580 390 SR-43 SR-43 - 580 - - 580 - - 580 - - - - - - - - - - - - -	TOTAL 480 667.974 615.803 1 3940 1 3940 1 1 200 230 1 1 200 230 1 1 1 5 200 230 1 1 1 5 200 230 1 1 1 5 1 5 1 5 1 5 1 5 1 1 1 1 1 1 1	LT ( 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 350 460 0 620 350	DEPART TOTAL 670 620 Trares F 620 → Trares F 620 → Trares F 1430
B&C FACTOR SEASONAL FACTOR P&A 24 HR B&C 24 HR	FACTOR LT 1.206 0.865 Trares Road	1 THRU 1.206 0.865 2170 ← 4 -550 → 1 1620 →	RT 1.206 0.865 1090 1080 -570 20 520 1100	LT 4.824 4.824 4.17276 320 270 490 10 0 10	THRU         0]           0]         0]           260	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑ ↓ 160 ↑ ↓ 160 ↑ ↓	TOTAL 8 8.34552 8.34552 SR-43 7810 110 5610 82500 SR-43 380 10 58843 3800 SR-43 81900 120 5843 81900 120 5843 81900 120 5843 120 120 5843 120 120 120 120 120 120 120 120	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 3940 ↑ 210 ↑ 210 ↑ 210 ↓ ↑ 150 ↓	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THRU 0 0 0 0 0 1 99 ← 22 Γ 40 ← 0 Γ 0 1 99 ← 22 Γ 40 ← 1 99 ← 22 Γ 40 ← 1 99 ← 22 Γ 40 ← 1 99 ← 22 Γ 40 ← 1 99 ← 1 99 ← 2 9 ← 1 99 ← 1 99 ← 2 9 ← 1 99 ← 2 9 ← 1 99 ← 1 99	RT 0 0	APROACH TOTAL 0 0 0 350 460 0 620 0 620 0 1080	$\begin{array}{c} \text{DEPART}\\ \text{TOTAL}\\ \text{670}\\ 620 \end{array}$
B&C FACTOR SEASONAL FACTOR P8A 24 HR 	FACTOR LT 1.206 0.865 Trares Roac	THRU 1.206 0.865 2170 ← 1 -550 → 1 1620 → 1	RT 1.206 0.865 1090 1080 -570 20 520 1100	LT 4.824 4.17276 320 270 490 10 0 10 330 270 500	THRU         0]           0]         0           260            J            J            J            J            J            J            J            J            J            J	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 170 150 ↓ 160 ↑ 1 4040 3650 ↓ ↓ 4040 3650 ↓	TOTAL 8 8.34552 9.648 8.34552 SR-43 7810 110 5610 82500 SR-43 380 10 10 5800 3900 SR-43 8190 120 1 30	TOTAL 480 667.974 615.803 ↑ 3940 ↑ 23530 4220 ↓ ↑ 210 ↑ 210 ↑ 210 ↑ 15530 4250 ↓ ↑ 1550 ↓ 1550 ↑ 1550 1550 ↑	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THRU 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	RT 0 0	APROACH TOTAL 0 0 0 0 460 0 620 620 620 620 620 1080	DEPART TOTAL 670 620 → Trares F 810 → Trares F 620 → Trares F 620 →
B&C FACTOR SEASONAL FACTOR P&A 24 HR B&C 24 HR	FACTOR LT 1.206 0.865 Trares Roac	THRU 1.206 0.865 2170 → 1 1620 → 1	RT 1.206 0.865 1090 1080 -570 20 520 1100	LT 4.824 4.17276 320 270 490 10 0 10 0 10	THRU         01           0         0           0         0           0         0           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1           1         1	RT 4 4.824 4.17276 ↓ 3870 3500 ↓ 4030 ↑ 100 ↓ 100 ↑ 100 ↓ 10	TOTAL 8 9.648 9.648 8.34552 SR-43 7810 110 - 610 8250 SR-43 380 10 - 580 390 SR-43 SR-43 SR-43 38190 120 - 50 8250 SR-43 38190 120 - 50 50 50 50 50 50 50 50 50 50	TOTAL 480 667.974 515.803 1 3940 1 3940 1 1 35530 4220 230 4220 230 4150 1 1 1 1 5 7 3730 4450	LT ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	EAST LEG THRU 0 0 0 1 9 4 2 7 40 4 1 9 4 2 7 40 5 6 7 0 1 9 5 7 4 1 1 1 1 1 1 1 1 1 1 1 1 1	RT 0 0	APROACH TOTAL 0 0 0 350 460 0 620 0 620 0 1080	DEPART TOTAL 670 620

POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



#### POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations

	Year	Period	Scenario	Plate
CARPENTER		r chod	Peak Hour to	The second secon
MAKTY transportation	2022		Design Hour Factors	
A N	2022 Peak Hour to Randolph Road inte classified as Rural Lo this, they are utilizing	Design Hour Factors ob resection and both the e cal Roads and do not ha g the factor used for the classified as a	tained from ODOT. Note, the ea east and west legs of the Trares R ave defined Peak Hour to Design e west leg of the Randolph Road a Rural Major Collector.	st leg of the SR-43 & load intersection are Hour Factors. Due to intersection, which is
		SR-43		
	1.19 Randolph Road	1.19 1.19 1.19 1.19 1.1 1.1 1.1 1.1 1.19 1.19 1.19 1.19 1.19 1.19 1.19 1.19 1.1	1.19	
	1.19 Trares Road	1.19 1.19 1.1 1 1.1 1 1.1 1 1.1 1 1.1 1 1.19 1.19 1.19 1.19 1.19 1.19	1.19	

POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



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POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations


POR-SR-43 and Trares and Randolph Safety Study Traffic Volume Calculations



# Appendix D Crash Data



Fatalities	0
Total Serious Injuries	1
Total Non-Serious & Possible Injuries	10

Crash Severity	Crashes	%
(2) Serious Injury Suspected	1	4.76%
(3) Minor Injury Suspected	4	19.05%
(4) Injury Possible	4	19.05%
(5) PDO/No Injury	12	57.14%
Grand Total	21	100.00%

Day of Week	Crashes	%
(1) Sunday	3	14.29%
(2) Monday	1	4.76%
(3) Tuesday	4	19.05%
(4) Wednesday	4	19.05%
(5) Thursday	1	4.76%
(6) Friday	5	23.81%
(7) Saturday	3	14.29%
Grand Total	21	100.00%

Hour of Day	Crashes	%
7	1	4.76%
8	2	9.52%
9	1	4.76%
10	2	9.52%
12	2	9.52%
13	2	9.52%
14	4	19.05%
15	1	4.76%
16	1	4.76%
18	1	4.76%
19	2	9.52%
20	1	4.76%
22	1	4.76%
Grand Total	21	100.00%

Crashes Per Year	4.20
Fatal and All Injury Crashes	9
Percent Injury	42.9%
Equivalent PDO Index Value	4.82

Year	Crashes	%
2016	4	19.05%
2017	4	19.05%
2018	3	14.29%
2019	7	33.33%
2020	3	14.29%
Grand Total	21	100.00%

Crash Type	Crashes	%
Angle	15	71.43%
Rear End	3	14.29%
Left Turn	2	9.52%
Right Turn	1	4.76%
Grand Total	21	100.00%

Month	Crashes	%
1	2	9.52%
3	4	19.05%
6	2	9.52%
7	3	14.29%
8	1	4.76%
9	5	23.81%
10	3	14.29%
11	1	4.76%
Grand Total	21	100.00%

Weather Condition	Crashes	%
Clear	13	61.90%
Cloudy	7	33.33%
Rain	1	4.76%
Grand Total	21	100.00%

Light Condition	Crashes	%
Daylight	18	85.71%
Dawn/Dusk	1	4.76%
Dark - Lighted Roadway	1	4.76%
Dark - Roadway Not Lighted	1	4.76%
Grand Total	21	100.00%

ODOT Location	Crashes	%
Four-Way Intersection	21	100.00%
Grand Total	21	100.00%

Contour	Crashes	%
Straight Grade	19	90.48%
Straight Level	2	9.52%
Grand Total	21	100.00%

Roadway Departure	Crashes	%
No	19	90.48%
Yes	2	9.52%
Grand Total	21	100.00%
Intersection Related	Crashes	%
Yes	20	95.24%
No	1	4.76%
Grand Total	21	100.00%
Speed Related	Crashes	%
No	19	90.48%
Yes	2	9.52%
Grand Total	21	100 00%

Road Condition	Crashes	%
Dry	17	80.95%
Wet	4	19.05%
Grand Total	21	100.00%

Number of Units	Crashes	%
2	20	95.24%
3	1	4.76%
Grand Total	21	100.00%
Work Zone Related	Crashes	%
No	21	100.00%
Grand Total	21	100.00%
Alcohol Related	Crashes	%
No	21	100.00%
Grand Total	21	100.00%
Drug Related (Inc. Marijuana)	Crashes	%
No	21	100.00%
Grand Total	21	100.00%
Marijuana Related	Crashes	%
No	21	100.00%
Grand Total	21	100.00%
Older Driver (65+)	Crashes	%
No	15	71.43%
Yes	6	28.57%
Grand Total	21	100.00%
Young Driver (15-25)	Crashes	%
No	12	57.14%
Yes	9	42.86%
Grand Total	21	100.00%
Motorcycle Involved	Crashes	%
No	21	100.00%
Grand Total	21	100.00%

### POR-43 at Randolph Road & Trares Road Crash Summary Sheet Unit 1 Summary

Unit 1 Pre-Crash Action	Crashes	%
Straight Ahead	16	76.19%
Making Left Turn	3	14.29%
Entering Traffic Lane	1	4.76%
Leaving Traffic Lane	1	4.76%
Grand Total	21	100 00%

Unit 1 Object Struck	Crashes	%
Nothing Struck	20	95.24%
Ditch	1	4.76%
Grand Total	21	100.00%

Unit 1 Direction From	Crashes	%
Northeast	10	47.62%
South	5	23.81%
West	3	14.29%
East	2	9.52%
North	1	4.76%
Grand Total	21	100.00%

Unit 1 Direction To	Crashes	%
Southwest	10	47.62%
West	4	19.05%
East	3	14.29%
North	3	14.29%
South	1	4.76%
Grand Total	21	100.00%

Unit 1 Type	Crashes	%
Passenger Car	8	38.10%
Sport Utility Vehicle	7	33.33%
Pick up	5	23.81%
Unknown or Hit/Skip	1	4.76%
Grand Total	21	100.00%

Unit 1 Contributing Factor	Crashes	%
Failure to Yield	16	76.19%
Following Too Closely/ACDA	3	14.29%
Ran Stop Sign	1	4.76%
Improper Lane Change	1	4.76%
Grand Total	21	100.00%

Unit 1 Traffic Control	Crashes	%
Stop Sign	15	71.43%
No Control	6	28.57%
Grand Total	21	100.00%

Unit 1 Estimated Speed	Crashes	%
<15	12	57.14%
15-19	2	9.52%
20-24	3	14.29%
30-34	2	9.52%
40-44	2	9.52%
Grand Total	21	100.00%

Unit 1 Posted Speed	Crashes	%
0	1	4.76%
40	2	9.52%
45	18	85.71%
Grand Total	21	100.00%

Unit 1 Special Function	Crashes	%
None	21	100.00%
Grand Total	21	100.00%

### **Unit 2 Summary**

Unit 2 Pre-Crash Action	Crashes	%
Straight Ahead	20	95.24%
Slowing or Stopped In Traffic	1	4.76%
Grand Total	21	100 00%

Unit 2 Direction From	Crashes	%
North	13	61.90%
South	8	38.10%
Grand Total	21	100.00%

Unit 2 Contributing Factor	Crashes	%
None	21	100.00%
Grand Total	21	100.00%

Unit 2 Direction To	Crashes	%
North	8	38.10%
South	13	61.90%
Grand Total	21	100.00%

Unit 2 Type	Crashes	%
Passenger Car	14	66.67%
Sport Utility Vehicle	3	14.29%
Pick up	2	9.52%
Passenger Van (minivan)	2	9.52%
Grand Total	21	100.00%

Unit 2 Special Function	Crashes	%
None	21	100.00%
Grand Total	21	100.00%

Fatalities	0
Total Serious Injuries	2
Total Non-Serious & Possible Injuries	16

Crash Severity	Crashes	%
(2) Serious Injury Suspected	2	12.50%
(3) Minor Injury Suspected	7	43.75%
(4) Injury Possible	1	6.25%
(5) PDO/No Injury	6	37.50%
Grand Total	16	100.00%

Day of Week	Crashes	%
(2) Monday	3	18.75%
(3) Tuesday	3	18.75%
(4) Wednesday	2	12.50%
(5) Thursday	2	12.50%
(7) Saturday	6	37.50%
Grand Total	16	100.00%

Hour of Day	Crashes	%
8	1	6.25%
9	1	6.25%
10	1	6.25%
11	1	6.25%
12	2	12.50%
13	2	12.50%
14	1	6.25%
17	2	12.50%
18	3	18.75%
19	1	6.25%
20	1	6.25%
Grand Total	16	100.00%

Crashes Per Year	3.20
Fatal and All Injury Crashes	10
Percent Injury	62.5%
Equivalent PDO Index Value	9.17

Year	Crashes	%
2016	2	12.50%
2017	6	37.50%
2018	1	6.25%
2019	4	25.00%
2020	3	18.75%
Grand Total	16	100.00%

Crash Type	Crashes	%
Angle	6	37.50%
Rear End	4	25.00%
Left Turn	4	25.00%
Fixed Object	1	6.25%
Overturning	1	6.25%
Grand Total	16	100.00%

Month	Crashes	%
3	1	6.25%
5	2	12.50%
6	1	6.25%
7	2	12.50%
8	2	12.50%
9	4	25.00%
10	2	12.50%
11	2	12.50%
Grand Total	16	100.00%

Weather Condition	Crashes	%
Clear	11	68.75%
Cloudy	5	31.25%
Grand Total	16	100 00%

Light Condition	Crashes	%
Daylight	14	87.50%
Dark - Lighted Roadway	1	6.25%
Dark - Roadway Not Lighted	1	6.25%
Grand Total	16	100 00%

ODOT Location	Crashes	%
Four-Way Intersection	16	100.00%
Grand Total	16	100.00%

Contour	Crashes	%
Straight Grade	11	68.75%
Straight Level	5	31.25%
Grand Total	16	100.00%

Roadway Departure	Crashes	%
No	13	81.25%
Yes	3	18.75%
Grand Total	16	100.00%
Intersection Related	Crashes	%
Yes	15	93.75%
No	1	6.25%
Grand Total	16	100.00%
Speed Related	Crashes	%
No	16	100.00%
Grand Total	16	100.00%

Road Condition	Crashes	%
Drv	14	87.50%
Wet	1	6.25%
Snow	1	6.25%
Grand Total	16	100.00%

Number of Units	Crashes	%
2	13	81.25%
1	2	12.50%
3	1	6.25%
Grand Total	16	100.00%
Work Zone Related	Crashes	%
No	14	87.50%
Yes	2	12.50%
Grand Total	16	100.00%
Alcohol Polatod	Crachoc	0/_
No	16	100.00%
Grand Total	16	100.00%
Drug Related (Inc. Marijuana)	Crashes	%
No	16	100.00%
Grand Total	16	100.00%
Marijuana Related	Crashes	%
No	16	100.00%
Grand Total	16	100.00%
Older Driver (65+)	Crashes	%
No	11	68.75%
Yes	5	31.25%
Grand Total	16	100.00%
Young Driver (15-25)	Crashes	%
No	6	37.50%
Yes	10	62.50%
Grand Total	16	100.00%
Motorcycle Involved	Crashes	%
No	13	81.25%
Yes	3	18.75%
	40	TATATATATATA

### POR-43 at Randolph Road & Trares Road Crash Summary Sheet Unit 1 Summary

Unit 1 Pre-Crash Action	Crashes	%
Straight Ahead	8	50.00%
Making Left Turn	5	31.25%
Slowing or Stopped In Traffic	2	12.50%
Entering Traffic Lane	1	6.25%
Grand Total	16	100 00%

Unit 1 Object Struck	Crashes	%
Nothing Struck	15	93.75%
Traffic Sign Post	1	6.25%
Grand Total	16	100.00%

Unit 1 Direction From	Crashes	%
South	5	31.25%
East	5	31.25%
West	3	18.75%
North	3	18.75%
Grand Total	16	100.00%

Unit 1 Direction To	Crashes	%
West	7	43.75%
East	5	31.25%
North	3	18.75%
Southeast	1	6.25%
Grand Total	16	100.00%

Unit 1 Type	Crashes	%
Passenger Car	7	43.75%
Sport Utility Vehicle	4	25.00%
Pick up	3	18.75%
Motorcycle 2 Wheeled	2	12.50%
Grand Total	16	100.00%

Unit 1 Contributing Factor	Crashes	%
Failure to Yield	9	56.25%
Following Too Closely/ACDA	3	18.75%
Improper Lane Change	1	6.25%
Ran Stop Sign	1	6.25%
Other Improper Action	1	6.25%
Improper Start From a Parked Position	1	6.25%
Grand Total	16	100.00%

Unit 1 Traffic Control	Crashes	%
Stop Sign	8	50.00%
No Control	8	50.00%
Grand Total	16	100.00%

Unit 1 Estimated Speed	Crashes	%
<15	11	68.75%
15-19	1	6.25%
35-39	1	6.25%
40-44	1	6.25%
45-49	2	12.50%
Grand Total	16	100.00%

Unit 1 Posted Speed	Crashes	%
40	4	25.00%
45	12	75.00%
Grand Total	16	100.00%

Unit 1 Special Function	Crashes	%
None	16	100.00%
Grand Total	16	100.00%

### **Unit 2 Summary**

Unit 2 Pre-Crash Action	Crashes	%
Straight Ahead	9	56.25%
Slowing or Stopped In Traffic	3	18.75%
	2	12.50%
Making Left Turn	2	12.50%
Grand Total	16	100.00%

Unit 2 Direction From	Crashes	%
	2	12.50%
North	3	18.75%
South	9	56.25%
West	2	12.50%
Grand Total	16	100 00%

Unit 2 Type	Crashes	%
Passenger Car	7	43.75%
Sport Utility Vehicle	3	18.75%
	2	12.50%
Motorcycle 2 Wheeled	1	6.25%
Semi-Tractor	1	6.25%
Cargo Van	1	6.25%
Pick up	1	6.25%
Grand Total	16	100.00%

Unit 2 Contributing Factor	Crashes	%
None	13	81.25%
	2	12.50%
Swerving to Avoid	1	6.25%
Grand Total	16	100.00%

Unit 2 Direction To	Crashes	%
	2	12.50%
East	1	6.25%
North	9	56.25%
South	3	18.75%
West	1	6.25%
Grand Total	16	100.00%

Unit 2 Special Function	Crashes	%
None	13	81.25%
	2	12.50%
Farm	1	6.25%
Grand Total	16	100.00%



STATE OF ORD NOLANA	COLL POR SR	43 at Rai 51M 2016	NDIAGRAM ndolph Rd (CR 10) <sup>3.94</sup> -2020	
Randanan	tri trent pipe pipe pipe pipe pipe pipe pipe pip	FTV B-14-19/2P/D *Improper Turn		TRANSPACE OF THE REPORT OF THE
Vehicle Direction Backing Pedestrian Out of Control Overturn	<ul> <li>Injury</li> <li>Fatal</li> <li>Fixed Object</li> <li>Parked Vehicle</li> <li>TEXT Date/Time/Road/Egress Direct</li> </ul>	<u>Road:</u> D = Dry W = Wet I = Ice S = Snow tion	FTC = Failure To Control FTS = Failure To Stop FTY = Failure To Yield LOC = Left of Center RRL = Ran Red Light OVI = Operating Vehicle Impaired	TOTAL CRASHES ON PAGE           FREQUENCY         CRASH SEVERITY           4         2016           4         2017           3         2018           7         2019           3         2020

## Appendix E Existing and No Build Capacity Analysis







		ŀ	ICS 1	Гwo-'	Way	Stop	-Cor	ntrol	Repo	ort						
General Information	_	_	_	_		-	Site	Inforn	natio	1	_	_	_	_	_	
Analyst	VHD						Inters	ection		-	SR-43	at Ranc	lolph			
Agency/Co	Lanha	am Engir	eerina.				Jurisd	iction				District	4			
Date Performed			icening,				East/	Nest Stre	et		Rando	olph				
Analysis Year	2022						North	/South S	Street		SR-43	- F				
Time Analyzed	AM P	eak					Peak I	Hour Fac	tor		0.81					
Intersection Orientation	North	n-South					Analy	sis Time	Period (	hrs)	0.25					
Project Description	SR-43	3 at Rand	lolph Exi	isting AN	1											
Lanes	1															
Vehicle Volumes and Adjustments																
Vehicle Volumes and Adju	istme	nts														
Approach		Eastb	ound			West	ound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority		10	11	12		7	8	9	10	1	2	3	40	4	5	6
Number of Lanes	ļ	0	1	0		0	1	0	0	0	1	0	0	0	1	_
	ļ	12	LIR				I LIR I				I LIR I					0
volume (ven/h)		≺				0	21	2		2	520	7		4		0
Dercent Llenny Vahieles (9/)	1	- 13 - E	4	4		9	21	2		2	520	7		4	292	0 15
Percent Heavy Vehicles (%)		5	5	4		9 7	21 7	2 7		2	520	7		4	292	0
Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%)		5	4 5	4		9 7	21 7	2 7		2 5	520	7		4	292	0
Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Chappelized		5	4 5 0	4		9 7 (	21 7	2 7		2 5	520	7		4	292	0
Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Channelized Median Type   Storage		5	4 5 0	4 5 Undi	vided	9 7 (	21 7	2 7		2 5	520	7		4	292	0
Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Channelized Median Type   Storage Critical and Follow-up He	adwa	5 VS	4 5 0	4 5 Undi	vided	9 7 (	21 7	2 7		2 5	520	7		4	292	0
Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Channelized Median Type   Storage Critical and Follow-up He Base Critical Headway (sec)	adwa	<b>ys</b>	4 5 0	4 5 Undi	vided	9 7 ( 7 7 7 7 7 7 7 7 7 7 7 7 1	21 7 ) 6.5	2 7 6.2		2 5	520	7		4	292	0
Percent Heavy Vehicles (%) Proportion Time Blocked Percent Grade (%) Right Turn Channelized Median Type   Storage Critical and Follow-up He Base Critical Headway (sec) Critical Headway (sec)	adwa	<b>ys</b> 7.1 7.15	4 5 0 6.5 6.55	4 5 Undi	vided	9 7 ( 7.1 7.17	21 7 6.5 6.57	2 7 6.2 6.27		2 5 4.1 4.15	520	7		4 4 4 4 4.1 4.1		0
Percent Heavy Vehicles (%)         Proportion Time Blocked         Percent Grade (%)         Right Turn Channelized         Median Type   Storage         Critical and Follow-up He         Base Critical Headway (sec)         Critical Headway (sec)         Base Follow-Up Headway (sec)	adwa	<b>ys</b> 7.1 7.15 3.5	4 5 0 6.5 6.55 4.0	4 5 Undi 6.2 6.25 3.3	vided	9 7 ( 7.1 7.17 3.5	21 7 6.5 6.57 4.0	2 7 6.2 6.27 3.3		2 5 4.1 4.15 2.2	520	7		4 4 4.1 4.14 2.2	292	0

Delay, Queue Length, and	l Leve	l of Se	rvice										
Flow Rate, v (veh/h)			26			40		2			5		
Capacity, c (veh/h)			217			222		1163			926		
v/c Ratio			0.12			0.18		0.00			0.01		
95% Queue Length, Q <sub>95</sub> (veh)			0.4			0.6		0.0			0.0		
95% Queue Length, Q <sub>95</sub> (ft)			10.4			15.8							
Control Delay (s/veh)			23.8			24.7		8.1	0.0	0.0	8.9	0.1	0.1
Level of Service (LOS)			С			С		A	А	А	A	А	А
Approach Delay (s/veh)		23.	.8		24	4.7		0	.1		0	.2	
Approach LOS		C			(	2			4			4	

		ŀ	ICS <sup>-</sup>	Гwo-'	Way	Stop	-Cor	ntrol	Repo	ort						
General Information		_	_		_	_	Site	Inforr	natio	n		_	_		_	_
Analyst	VHD						Inters	ection			SR-43	3 at Rand	dolph			
Agency/Co.	Lanha	am Engir	neering,	LLC			Jurisc	liction			ODO	T District	t 4			
Date Performed	i						East/	West Stre	eet		Rand	olph				
Analysis Year	2022						North	n/South S	Street		SR-43	3				
Time Analyzed	PM P	eak					Peak	Hour Fac	ctor		0.96					
Intersection Orientation	North	n-South					Analy	sis Time	Period (	hrs)	0.25					
Project Description	SR-43	3 at Ranc	dolph Ex	isting PN	1											
Lanes																
Vehicle Volumes and Adjustments         Approach       Eastbound																
Vehicle Volumes and Adju	istme	nts											1			
Approach		Eastb	ound			West	bound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	T	R	U	L	T	R	U		Т	R
Priority	<u> </u>	10	11	12		7	8	9	10	1	2	3	40	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
	1	12	26	0		0	12	2		4	140	25		2	622	27
Percent Heavy Vehicles (%)		12	20	0		5	5	5		4	449	23		2	052	21
Proportion Time Blocked	1	0	0	0		5		5		5				-		
Percent Grade (%)	1		0				0									
Right Turn Channelized	1		-				-									
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	adwa	ys							<u> </u>							
Base Critical Headway (sec)	1	7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)	1	7.10	6.50	6.20		7.15	6.55	6.25		4.13				4.12		
Base Follow-Up Headway (sec)	i	3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)	l I	3.50	4.00	3.30		3.55	4.05	3.35		2.23				2.22		
			ervice													
Delay, Queue Length, and	Leve	101 30														

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Capacity, c (veh/h)

95% Queue Length, Q<sub>95</sub> (veh)

95% Queue Length, Q<sub>95</sub> (ft)

Control Delay (s/veh)

Level of Service (LOS)

Approach LOS

Approach Delay (s/veh)

v/c Ratio

28.1

D

180

0.13

0.5

13.0

28.1

D

903

0.00

0.0

9.0

А

0.1

А

0.1

А

0.1

А

200

0.24

0.9

22.5

28.7

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28.7

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А

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А

1070

0.00

0.0

8.4

А

		ŀ	ICS <sup>-</sup>	Гwo-	Way	Stop	-Cor	ntrol	Repo	ort						
General Information							Site	Inforr	natio	n						
Analyst	VHD						Inters	ection			SR-43	at Ranc	dolph			
Agency/Co.	Lanha	am Engir	neering,	LLC			Jurisd	iction			ODO	Γ District	4			
Date Performed	1						East/	Nest Stre	eet		Rand	olph				
Analysis Year	2027						North	/South S	Street		SR-43	3				
Time Analyzed	AM P	eak					Peak	Hour Fac	ctor		0.81					
Intersection Orientation	North	-South					Analy	sis Time	Period (	hrs)	0.25					
Project Description	SR-43	8 at Rand	lolph No	b Build C	Y AM											
Lanes																
Image: Street: North-South       Vehicle Volumes and Adjustments																
Approach	1	Facth	ound			Mostk	agund			North	hound		l .	Couth	hound	
Approach			т	D		vvesti	т	D		North	т	D		South	т	
Priority		10	11	12		7	8	9	111	1	2	3	411	4		6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration	1		LTR				LTR				LTR				LTR	
Volume (veh/h)		10	10	10		10	20	10		10	520	10		10	300	20
Percent Heavy Vehicles (%)	1	5	5	5		7	7	7		5				4		
Proportion Time Blocked	1															
Percent Grade (%)	i –	(	0			(	0									
Right Turn Channelized	i															
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	adwa	ys														
Base Critical Headway (sec)	1	7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.15	6.55	6.25		7.17	6.57	6.27		4.15				4.14		
	1															

Base Follow-Up Headway (sec)		3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
Follow-Up Headway (sec)		3.55	4.05	3.35	3.56	4.06	3.36	2.25			2.24		
Delay, Queue Length, and	Leve	l of Se	ervice										
Flow Rate, v (veh/h)			37			49		12			12		
Capacity, c (veh/h)			234			222		1147			923		
v/c Ratio			0.16			0.22		0.01			0.01		
95% Queue Length, Q <sub>95</sub> (veh)			0.6			0.8		0.0			0.0		
95% Queue Length, Q <sub>95</sub> (ft)			15.6			21.1							
Control Delay (s/veh)			23.2			25.8		8.2	0.1	0.1	9.0	0.2	0.2
Level of Service (LOS)			С			D		A	А	А	А	А	А
Approach Delay (s/veh)		23	3.2		25	5.8		0	.3		0	.4	
Approach LOS		(	2		[	2			4		1	4	

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		ŀ	ICS <sup>-</sup>	Гwo-'	Way	Stop	-Cor	ntrol	Repo	ort						
General Information	_	_	_	_		_	Site	Inforr	natio	n	_	_	_	_	_	
Analyst							Inters	ection			SR-//3	at Rand	dolph			
Anaport		m Engir	ooring				lurico	liction								
Date Performed		ani Liigii	leening,				Eact (	Noct Str	oot		Band		. 4			
Analysis Year	1 2027						East/	Vest Stre	Stroot			5 5				
		o o la					Deale		ster		0.06	)				
Intersection Orientation		edK					Peak		Deried (	hrs)	0.96					
Project Description		- south	lolph Nr	Puild O			Analy		Feriou (	1115)	0.23					
	31-43			bullu C												
Lanes																
/ehicle Volumes and Adjustments																
Vehicle Volumes and Adju	ustme	nts														
Approach		Eastb	ound			West	oound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1	10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes	1	0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration	1		LTR				LTR				LTR				LTR	
Volume (veh/h)	1	10	30	10		10	10	10		10	450	30		10	640	30
Percent Heavy Vehicles (%)	1	0	0	0		5	5	5		3				2		
Proportion Time Blocked	1															
Percent Grade (%)	1		0				0									
Right Turn Channelized	1															
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	eadwa	ys														
Base Critical Headway (sec)	1	7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.10	6.50	6.20		7.15	6.55	6.25		4.13				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)	1	3.50	4.00	3.30		3.55	4.05	3.35		2.23				2.22		
Delay, Queue Length, and	d Leve	l of Se	ervice													
Flow Rate, v (veh/h)	1		52				31			10				10		

Capacity, c (veh/h)

95% Queue Length, Q<sub>95</sub> (veh)

95% Queue Length, Q<sub>95</sub> (ft)

Control Delay (s/veh)

Level of Service (LOS)

Approach LOS

Approach Delay (s/veh)

v/c Ratio

28.0

D

188

0.17

0.6

15.6

28.0

D

894

0.01

0.0

9.1

А

0.3

А

0.1

А

0.1

А

189

0.28

1.1

27.5

31.1

D

31.1

D

0.3

0.1

А

0.1

А

1064

0.01

0.0

8.4

А

		ŀ	ICS T	Гwo-'	Way	Stop	-Cor	ntrol	Repo	ort						
General Information							Site	Inforr	natio	1						
Analyst	VHD						Inters	ection			SR-43	3 at Rand	dolph			
Agency/Co.	Lanha	am Engir	eering,	LLC			Jurisd	liction			ODO	T District	: 4			
Date Performed	İ						East/	Nest Stre	eet		Rand	olph				
Analysis Year	2047						North	/South S	Street		SR-43	3				
Time Analyzed	AM P	eak					Peak	Hour Fac	ctor		0.81					
Intersection Orientation	North	-South					Analy	sis Time	Period (	hrs)	0.25					
Project Description	SR-43	at Ranc	lolph No	Build D	Y AM											
Lanes																
Yehicle Volumes and Adjustments																
	Journe	1115														
Approach		Eastb	ound			West	bound			North	bound			South	oound	
Movement	U		T	R	U	L	Т	R	U		T	R	U			R
Priority	ļ	10	11	12		7	8	9	10	1	2	3	40	4	5	6
Number of Lanes	ļ	0	1	0		0	1	0	0	0	1	0	0	0		0
	1	20		10		10		10		10		10		10		20
Volume (veh/h)	1	20	10	10		10	30	10		10	560	10		10	310	20
Percent Heavy venicies (%)	1	5	5	5		/	1	1		5				4	<u> </u>	
Proportion Time Blocked	1		<u></u>				<u> </u>									
Percent Grade (%)	1		J				J									
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	adwa	vs		51101					I							
	l	71	65	6.2		71	65	6.2		A 1				4.1		
Critical Headway (sec)	1	7.1	6.55	6.25		7.1	6.57	6.27		4.1 1 15				4.1		
	-	7.15	0.55	0.25		7.17	0.57	0.27		4.15				4.14		

entical field way (see)		7.15	0.55	0.25	7.17	0.57	0.27	4.15			7.17		
Base Follow-Up Headway (sec)		3.5	4.0	3.3	3.5	4.0	3.3	2.2			2.2		
Follow-Up Headway (sec)		3.55	4.05	3.35	3.56	4.06	3.36	2.25			2.24		
Delay, Queue Length, and	Leve	l of Se	ervice										
Flow Rate, v (veh/h)			49			62		12			12		
Capacity, c (veh/h)			177			199		1135			885		
v/c Ratio			0.28			0.31		0.01			0.01		
95% Queue Length, Q <sub>95</sub> (veh)			1.1			1.3		0.0			0.0		
95% Queue Length, Q <sub>95</sub> (ft)			28.6			34.3							
Control Delay (s/veh)			33.0			31.0		8.2	0.1	0.1	9.1	0.2	0.2
Level of Service (LOS)			D			D		А	А	А	А	А	А
Approach Delay (s/veh)		33	3.0		31	1.0		0	.3		0.	.4	
Approach LOS		[	2		[	D			4		ļ	Ą	

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		ŀ	ICS 1	Гwo-'	Wav	Stop	-Cor	ntrol	Repo	ort						
General Information	_	_					Site	Inform	natio	n	_	_	_	_	_	
							pice		natio		CD 43		1 - 1 - 1-			
Analyst	VHD		•				Inters	ection			SR-43	at Rand	ioiph			
Agency/Co.	Lanha	am Engir	neering,	LLC			Jurisd	liction			ODO	「 District	. 4			
Date Performed							East/\	Nest Stre	eet		Rando	olph				
Analysis Year	2047						North	/South S	Street		SR-43	}				
Time Analyzed	PM P	eak					Peak	Hour Fac	tor		0.96					
Intersection Orientation	North	-South					Analy	sis Time	Period (	hrs)	0.25					
Project Description	SR-43	at Rand	dolph No	b Build D	Y PM											
Lanes																
A     A       A       A <t< th=""></t<>																
Vehicle Volumes and Adju	ustme	nts														
Approach		Eastb	ound			West	oound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1	10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes	1	0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration	1		LTR				LTR				LTR				LTR	
Volume (veh/h)	1	20	40	10		10	20	10		10	490	30		10	670	30
Percent Heavy Vehicles (%)	1	0	0	0		5	5	5		3				2		
Proportion Time Blocked	1															
Percent Grade (%)	1		0				0									
Right Turn Channelized	1															
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	adwa	ys														
Base Critical Headway (sec)	1	7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)	1	7.10	6.50	6.20		7.15	6.55	6.25		4.13				4.12		
Base Follow-Up Headway (sec)	1	3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.50	4.00	3.30		3.55	4.05	3.35		2.23				2.22		
Delay, Queue Length, and	d Leve	l of Se	ervice									•				
Flow Rate, v (veh/h)	1		73				42			10				10		

-												
Flow Rate, v (veh/h)		73			42		10			10		
Capacity, c (veh/h)		156			157		870			1027		
v/c Ratio		0.47			0.26		0.01			0.01		
95% Queue Length, Q <sub>95</sub> (veh)		2.2			1.0		0.0			0.0		
95% Queue Length, Q <sub>95</sub> (ft)		55.0			26.0							
Control Delay (s/veh)		47.0			35.9		9.2	0.2	0.2	8.5	0.1	0.1
Level of Service (LOS)		E			E		А	А	А	А	А	А
Approach Delay (s/veh)	47	7.0		35	5.9		0	.3		0	.3	
Approach LOS		E		I	E		/	4		A	4	

HCS Two-Way Stop-Control Report									
General Information		Site Information							
Analyst	VHD	Intersection	SR-43 at Trares						
Agency/Co.	Lanham Engineering, LLC	Jurisdiction	ODOT District 4						
Date Performed		East/West Street	Trares						
Analysis Year	2022	North/South Street	SR-43						
Time Analyzed	AM Peak	Peak Hour Factor	0.82						
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25						
Project Description	SR-43 at Trares Existing AM								
Lanes									
	7 4 + X 4 ★ ★	1 년 년 1 년 4 1 년 1 년 1 년 1 년 1 년 1 년 1 년 1 년 1 년 1 년							

					ብ ካ Major	t t treet: Nor Street: Nor	↑ ∱ ſ th-South										
Vehicle Volumes and Adj	ustme	nts															
Approach		Eastb	ound			West	bound			North	bound			South	bound		
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R	
Priority	1	10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes	1	0	1	0		0	1	0	0	0	1	0	0	0	1	0	
Configuration			LTR				LTR				LTR				LTR		
Volume (veh/h)		37	8	23		3	35	13		114	477	4		10	265	27	
Percent Heavy Vehicles (%)		0	0	0		0	0	0		5				5			
Proportion Time Blocked	]																
Percent Grade (%)	1		0			(	C										
Right Turn Channelized	]																
Median Type   Storage	1	Undivided															
Critical and Follow-up He	eadwa	ys															
Base Critical Headway (sec)	1	7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1			
Critical Headway (sec)		7.10	6.50	6.20		7.10	6.50	6.20		4.15				4.15			
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2			
Follow-Up Headway (sec)		3.50	4.00	3.30		3.50	4.00	3.30		2.25				2.25			
Delay, Queue Length, and	d Leve	l of Se	ervice														
Flow Rate, v (veh/h)	1		83				62			139				12			
Capacity, c (veh/h)	1		134				172			1186				974			
v/c Ratio	1		0.62				0.36			0.12				0.01			
95% Queue Length, Q <sub>95</sub> (veh)			3.2				1.5			0.4				0.0			
95% Queue Length, Q <sub>95</sub> (ft)			80.0				37.5										
Control Delay (s/veh)			68.4				37.3			8.4	1.5	1.5		8.7	0.1	0.1	
Level of Service (LOS)		F					E			А	A	А		A	А	А	
Approach Delay (s/veh)		68.4				37.3				2.8				0.4			

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Approach LOS

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HCS Two-Way Stop-Control Report									
General Information		Site Information							
Analyst	VHD	Intersection	SR-43 at Trares						
Agency/Co.	Lanham Engineering, LLC	Jurisdiction	ODOT District 4						
Date Performed		East/West Street	Trares						
Analysis Year	2022	North/South Street	SR-43						
Time Analyzed	PM Peak	Peak Hour Factor	0.96						
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25						
Project Description	SR-43 at Trares Existing PM								
Lanes									
	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	974 74 4 7 4 4 4							



Vehicle Volumes and Adju	stments															
Approach		Eastb	ound			West	bound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		43	51	85		1	18	11		56	419	6		17	593	30
Percent Heavy Vehicles (%)		1	1	1		3	3	3		3				2		
Proportion Time Blocked																
Percent Grade (%)	0 0															
Right Turn Channelized																
Median Type   Storage	Undivided															
Critical and Follow-up He	adwa	adways														
Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.11	6.51	6.21		7.13	6.53	6.23		4.13				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.51	4.01	3.31		3.53	4.03	3.33		2.23				2.22		
Delay, Queue Length, and	Leve	l of Se	ervice													
Flow Rate, v (veh/h)			186				31			58				18		
Capacity, c (veh/h)			209				203			932				1117		
v/c Ratio			0.89				0.15			0.06				0.02		
95% Queue Length, Q <sub>95</sub> (veh)			7.1				0.5			0.2				0.0		
95% Queue Length, Q <sub>95</sub> (ft)			178.9				12.8									
Control Delay (s/veh)			84.4				25.9			9.1	0.8	0.8		8.3	0.2	0.2
Level of Service (LOS)			F				D			А	А	А		А	А	А
Approach Delay (s/veh)		84	1.4			25	5.9		1.7				0.4			
Approach LOS	F D							Α				А				

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HCS Two-Way Stop-Control Report								
General Information		Site Information						
Analyst	VHD	Intersection	SR-43 at Trares					
Agency/Co.	Lanham Engineering, LLC	Jurisdiction	ODOT District 4					
Date Performed		East/West Street	Trares					
Analysis Year	2027	North/South Street	SR-43					
Time Analyzed	AM Peak	Peak Hour Factor	0.82					
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25					
Project Description	SR-43 at Trares No Build OY AM							
Lanes								
	A A A A A A A A A A A A A A A A A A A							

Vehicle Volumes and Adjustments																
Approach		Eastb	ound			West	oound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1	10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes	1	0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration	1		LTR				LTR				LTR				LTR	
Volume (veh/h)	1	40	10	30		10	40	10		120	490	10		10	280	30
Percent Heavy Vehicles (%)	1	0	0	0		0	0	0		5				5		
Proportion Time Blocked	1															
Percent Grade (%)	0 0															
Right Turn Channelized	1															
Median Type   Storage	Undivided															
Critical and Follow-up He	adwa	adways														
Base Critical Headway (sec)	1	7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)	1	7.10	6.50	6.20		7.10	6.50	6.20		4.15				4.15		
Base Follow-Up Headway (sec)	1	3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)	1	3.50	4.00	3.30		3.50	4.00	3.30		2.25				2.25		
Delay, Queue Length, and	l Leve	l of Se	ervice													
Flow Rate, v (veh/h)	1		98				73			146				12		
Capacity, c (veh/h)	1		119				139			1164				954		
v/c Ratio	1		0.82				0.53			0.13				0.01		
95% Queue Length, Q <sub>95</sub> (veh)	1		4.9				2.5			0.4				0.0		
95% Queue Length, Q <sub>95</sub> (ft)			122.5				62.5									
Control Delay (s/veh)	1		108.8				56.6			8.5	1.6	1.6		8.8	0.1	0.1
Level of Service (LOS)	1		F				F			А	А	А		А	А	А
Approach Delay (s/veh)		10	8.8			56	5.6		3.0				0.4			
Approach LOS	1	F F					A				А					

HCS Two-Way Stop-Control Report										
General Information		Site Inform	nation							
Analyst	VHD	Intersection	SR-43 at Trare	'S						
Agency/Co.	Lanham Engineering, LLC	Jurisdiction	ODOT District	4						
Date Performed		East/West Stre	eet Trares							
Analysis Year	2027	North/South	Street SR-43							
Time Analyzed	PM Peak	Peak Hour Fac	ctor 0.96							
Intersection Orientation	North-South	Analysis Time	Period (hrs) 0.25							
Project Description	SR-43 at Trares No Build OY PI	M								
Lanes										
	7 4 4 7 ↑ ¥ 7	A I A A A U A A A A A A A A A A A A A A A A								
Vehicle Volumes and Adju	istments									
Approach	Eastbound	Westbound	Northbound	Southbound						

Approach		Eastb	ound	Westbound				Northbound				Southbound				
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration			LTR				LTR				LTR				LTR	
Volume (veh/h)		50	60	90		10	20	10		60	430	10		20	610	30
Percent Heavy Vehicles (%)		1	1	1		3	3	3		3				2		
Proportion Time Blocked																
Percent Grade (%)		(	)			(	)									
Right Turn Channelized																
Median Type   Storage				Undiv	vided											
Critical and Follow-up He	adwa	ys														
Base Critical Headway (sec)		7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)		7.11	6.51	6.21		7.13	6.53	6.23		4.13				4.12		
Base Follow-Up Headway (sec)		3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)		3.51	4.01	3.31		3.53	4.03	3.33		2.23				2.22		
Delay, Queue Length, and	Leve	l of Se	ervice													
Flow Rate, v (veh/h)			208				42			63				21		
Capacity, c (veh/h)			188				118			918				1103		
v/c Ratio			1.11				0.35			0.07				0.02		
95% Queue Length, Q <sub>95</sub> (veh)			10.2				1.4			0.2				0.1		
95% Queue Length, Q <sub>95</sub> (ft)			257.0				35.8									
Control Delay (s/veh)			150.0				51.3			9.2	0.8	0.8		8.3	0.3	0.3
Level of Service (LOS)			F				F			А	А	А		А	А	А
Approach Delay (s/veh)	150.0 51.3						1.8				0.5					
Approach LOS	F F						AAA									

HCS Two-Way Stop-Control Report								
General Information		Site Information						
Analyst	VHD	Intersection	SR-43 at Trares					
Agency/Co.	Lanham Engineering, LLC	Jurisdiction	ODOT District 4					
Date Performed		East/West Street	Trares					
Analysis Year	2047	North/South Street	SR-43					
Time Analyzed	AM Peak	Peak Hour Factor	0.82					
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25					
Project Description	SR-43 at Trares No Build DY AM	· · · · · · · · · · · · · · · · · · ·						
Lanes								
	Image: state	► U ► ► ► ► ► ► ► ► ► ► ► ► ► ► ► ► ► ►						

Vehicle Volumes and Adju	ustments															
Approach		Eastb	ound			West	oound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	T	R	U	L	Т	R
Priority	1	10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes	1	0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration	1		LTR				LTR				LTR				LTR	
Volume (veh/h)	1	60	10	40		10	50	20		120	500	10		10	290	30
Percent Heavy Vehicles (%)	1	0	0	0		0	0	0		5				5		
Proportion Time Blocked	1															
Percent Grade (%)	1		0				0									
Right Turn Channelized	1															
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	eadways															
Base Critical Headway (sec)	1	7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)	1	7.10	6.50	6.20		7.10	6.50	6.20		4.15				4.15		
Base Follow-Up Headway (sec)	1	3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)	1	3.50	4.00	3.30		3.50	4.00	3.30		2.25				2.25		
Delay, Queue Length, and	l Leve	l of Se	ervice													
Flow Rate, v (veh/h)	1		134				98			146				12		
Capacity, c (veh/h)	1		90				145			1152				945		
v/c Ratio	1		1.49				0.67			0.13				0.01		
95% Queue Length, Q <sub>95</sub> (veh)	1		10.4				3.8			0.4				0.0		
95% Queue Length, Q <sub>95</sub> (ft)			260.0				95.0									
Control Delay (s/veh)			351.2				70.2			8.6	1.7	1.7		8.9	0.1	0.1
Level of Service (LOS)			F				F			А	А	А		А	А	А
Approach Delay (s/veh)		351.2 70.2							3	.0		0.4				
Approach LOS		F F					A				A					

HCS Two-Way Stop-Control Report								
General Information		Site Information						
Analyst	VHD	Intersection	SR-43 at Trares					
Agency/Co.	Lanham Engineering, LLC	Jurisdiction	ODOT District 4					
Date Performed		East/West Street	Trares					
Analysis Year	2047	North/South Street	SR-43					
Time Analyzed	PM Peak	Peak Hour Factor	0.96					
Intersection Orientation	North-South	Analysis Time Period (hrs)	0.25					
Project Description	SR-43 at Trares No Build DY PM							
Lanes								
		<ul> <li>↓</li> /ul>						
Vehicle Volumes and Adju	stments							

Approach		Eastb	ound			West	oound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1	10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes	1	0	1	0		0	1	0	0	0	1	0	0	0	1	0
Configuration	1		LTR				LTR				LTR				LTR	
Volume (veh/h)		70	80	130		10	30	10		60	440	10		20	640	30
Percent Heavy Vehicles (%)	1	1	1	1		3	3	3		3				2		
Proportion Time Blocked	1															
Percent Grade (%)	1		0			(	0									
Right Turn Channelized	1															
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	adwa	ys														
Base Critical Headway (sec)	1	7.1	6.5	6.2		7.1	6.5	6.2		4.1				4.1		
Critical Headway (sec)	1	7.11	6.51	6.21		7.13	6.53	6.23		4.13				4.12		
Base Follow-Up Headway (sec)	1	3.5	4.0	3.3		3.5	4.0	3.3		2.2				2.2		
Follow-Up Headway (sec)	1	3.51	4.01	3.31		3.53	4.03	3.33		2.23				2.22		
Delay, Queue Length, and	l Leve	l of Se	ervice													
Flow Rate, v (veh/h)	i		292				52			63				21		
Capacity, c (veh/h)	i		170				87			894				1093		
v/c Ratio	i –		1.71				0.60			0.07				0.02		
95% Queue Length, Q <sub>95</sub> (veh)	i i		20.5				2.7			0.2				0.1		
95% Queue Length, Q <sub>95</sub> (ft)			516.6				69.1									
Control Delay (s/veh)			391.6				94.4			9.3	0.9	0.9		8.4	0.3	0.3
Level of Service (LOS)			F				F			A	A	А		A	А	А
Approach Delay (s/veh)		39	1.6			94	1.4		1.9				0.5			
Approach LOS			F				F			/	4			/	4	

## Appendix F Signal, All-Way Stop-Control, and Turn Lane Warrants



STUDY AND ANALYSIS INFORMATION	TRAFFIC S	GNAL	WARR	ANT ANALYS
			Warrant	
Municipality: Traffic Volumes Obtained By	7	Applicable?	Satisfied?	Notes
Suffield Township ODOT	Warrant 1, Eight-Hour Vehicular Volume	Yes	No	Hote
County: Portage Analysis Date: 9/8/2022				
ODOT Engineering       4       Agency/ Company Name Performing       Lanham Engineering, LLC         District:       Map       Map	Warrant 2, Four-Hour Vehicular Volume	Yes	No	
Analysis Information	Warrant 3, Peak Hour	No		Signals installed under ac
Data Collection Date: 5/4/2022	For Warrants 1-3 new	ODOT signal	ls must be ba	sed off of 100% volume
Day of the Week: Wednesday	Warrant 4, Pedestrian Volume	No		If this warrant is met, and a tr engineering study, the traffic o pedestrian signal heads comp Chapter 4E
Is the intersection in a built-up area of an isolated community of <10,000 No No	Warrant 5, School Crossing	No		
Existing Traffic Signal at intersection: No	Warrant 6, Coordinated Signal System	No		(Shall not be use
Total Number of Approaches at Intersection: 4	Warrant 7, Crash Experience	Yes	No	If this is the sole warrant devices which provide pro within a coordinated s actuated if ins
Major Street Information	Warrant 8, Roadway Network	No		(Shall not be use
Major Street Name and Route Number: SR-43	Warrant 9, Intersection Near a Grade Crossing	No		
Major Street Approach Direction: N-Bound S-Bound	Multi-Way Stop Warrant	Yes	Yes	May be used as an int
Number of Thru Lanes on Each Major Street Approach: 1 LANE(S)	The satisfaction of a traffic sig	ınal warran	t or warrant control	s shall not in itself r signal.
Speed Limit or 85th Percentile Speed on the Major Street*: 45 MPH	If no warrants are satisfied, addition	onal options	may be con	sidered:
*Unknown assumes below 45 mph	1. An engineering study, performe	ed by a firm	prequalified	by ODOT for signal de
	district, may be used to justify a n	ew signal in	stallation or ı	etention of an existing
Minor Street Information	meet the published warrants. An e	example of s	such an insta	ince is a traffic signal
Mine Of a Characterized Data in Data in Data in Data in Data in the Data in th	that serves to reduce queuing acr	oss the trac	KS.	t counto fail to actiofy
	accentable to use traffic volumes	nroiected to	the second	vear after project com
Minor Street Approach Configuration:	Forecasting Section should prov	vide the proj	ected traffic	volumes.
	3. A pedestrian hybrid beacon ma	y be consid	ered for insta	allation to facilitate pe
	does not meet traffic signal warra	nts (see Cha	apter 4C of T	EM) or at a location t
	on PHB Score Sheet and submit	it to ODOT.	ision is made	e to not install a traffic
1 2 3 4 5	Considerations such as geometric	s and lack	of sight dista	nce generally have no
Number of Thru Lanes on Each Minor Street Approach: 1 LANE(S)	signal warrants. These considerat	ions may al	low an other	wise unwarranted traf
Apply Right Turn Lane Reduction*: Yes	percent local cost. Please review	TEM 402-4	for details.	
*Right Turn Lane Reduction Shall be used for Warrants 1, 2, & 3 for New ODOT Signals. Please refer to TEM 402-3.2 for clarification and criteria under which Right Turn Reduction is not required.	Notes:	Conclusion:	Do Not Insta	all New Traffic Signal

## **BIS FINDINGS**

### es and Comments:

er Warrant 3 should be traffic ctuated.

Peak Hour
4:15 PM
5:15 PM

e thresholds (TEM 402-3.2)

traffic control signal is justified by an control signal shall be equipped with plying with the provisions set forth in E of the OMUTCD.

Peak Hour
4:15 PM
5:15 PM

N/A

ed as the sole warrant in the analysis)

nt, signal must be semi-actuated with control oper coordination if installed at an intersection system and normally should be fully traffic stalled at an isolated intersection.

ed as the sole warrant in the analysis)

#### Figure 4C-9

terim measure if traffic signal warrants are satisfied.

### require the installation of a traffic

design, if approved by the ODOT ng signal that otherwise does not I in proximity to a railroad crossing

y a signal warrant, it may be mpletion. The **Modeling and** 

edestrian crossings at a location that that meets traffic signal warrants c control signal. **Please fill inputs** 

not been accepted in lieu of satisfying infinition of satisfying infinition of the set o



### **OMUTCD WARRANT 1, EIGHT-HOUR VEHICULAR VOLUME**

Number of La	nes for Moving Traffic
Major Street:	1 Lane
Minor Street:	1 Lane

Built up Isolated Community with Less Than 10,000 Population or Above 40 MPH on Major Street? Yes

Lanes Combination A/B\* Adjusted Condition A Condition B Volumes Major/ Cond. A Cond. B Cond. A Cond. B Minor 100% 100% 70% 70% 80% 56% 56% 80% Major Minor Maj. Min. 1/1 Х 2+/1 150 420 105 900 75 630 53 480 120 720 60 336 84 504 42 140 900 100 630 70 480 160 720 80 336 112 504 2+/2+ 160 600 280 112 1/2+ 12:00 AM 12:15 AM 12:30 AM 12:45 AM 1:00 AM 1:15 AM 1:30 AM 1:45 AM 2:00 AM 2:15 AM 2:30 AM 2:45 AM 3.00 AM 3:15 AM 3:30 AM 3.42 AM 4:00 AM 4:15 AM 4:30 AM 4:45 AM 5:00 AM 5:15 AM 5:30 AM 5:45 AM 6:00 AM 6:15 AM 6:30 AM 29 6:45 AM 7:00 AM 7:15 AM 7:30 AM 21 18 502 7:45 AM 8:00 AM 8:15 AM 8:30 AM 8:45 AM 9:00 AM 9:15 AM 9:30 AM 9:45 AM 10:00 AM 10:15 AM 10:30 AM 22 10:45 AM 11:00 AM 21 11:15 AM 11:30 AM 24 11:45 AM 12:00 PM 12:15 PM 12:30 PM 12:45 PM 1:00 PM 539 1:15 PM 1:30 PM 1:45 PM 2:00 PM 2:15 PM 2:30 PM 2:45 PM 3:00 PM 3:15 PM 3:30 PM 3:45 PM 4:00 PM 4:15 PM 

\*Only applicable after an adequate trial of other alternatives (See section 4C.02.06 of the 2012 OMUTCD)

4:30 PM	941	45													1			
4:45 PM	911	41	1		1						1							
5:00 PM	852	44					1						1					
5:15 PM	739	35							1								1	
5:30 PM	654	32													1			
5:45 PM	595	28	1		1						1							
6:00 PM	506	25																
6:15 PM	374	20																
6:30 PM	234	15																
6:45 PM	91	8																
7:00 PM	0	0																
7:15 PM	0	0																
7:30 PM	0	0																
7:45 PM	0	0																
8:00 PM	0	0																
8:15 PM	0	0																
8:30 PM	0	0																
8:45 PM	0	0																
9:00 PM	0	0																
9:15 PM	0	0																
9:30 PM	0	0																
9:45 PM	0	0																
HOURS MET			8	0	12	0	3	0	7	0	12	0	5	0	12	0	11	1
WARRANT S	ATISFIL	ED?	N	0	N	0	N	0	N	0		N	0			NO		

Warrant Met: No

Notes:



		S	outhbour	nd Approach			Wes	tbound Approa	ach			Noi	rthbound A	oproach			Ea	astbound	Approach	1		
Start Time	_	_	Sout	nbound	– App		_	Westbound		App		_	Nouthbou	nd	App		_	Eastbo	ound	Ap	n	NOTES:
12·00 AM	Right	Ihru	Left	U-Turn	Peds Total	Right	l hru	Left U-Turr	Peds	Total	Right	l hru	Left U	-Turn Peds	s Total	Right	Thru	Left	U-Turn	Peds Tot	al	
12:15 AM					õ					0										0		It should be noted that if data is copied overtop of the Hourly
12:30 AM 12:45 AM					0					0					0					0		Totals or Approach Totals, that the 'AutoSum' Formula will be
Hourly Total 1:00 AM	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		lost. This should not affect the
1:15 AM					0					0	-				0					0		copied from a program that
1:45 AM					<u>0</u>					0				<u> </u>	<u>0</u>					0		performs the calculations for the user.
2:00 AM	0	0	0	0	0 0		0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
2:15 AM 2:30 AM					0 0					0 0					0					0 0		
2:45 AM	0	0	0	0	0		0	0 0		0	0	0	0	0 0	0		0	0	0	0		
3:00 AM		0	0	0	0	Ļ,	0	0 0		0		Ū	0	0 0	0		0	0	0	0		
3:15 AM 3:30 AM					0					0					0					0		
3:45 AM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
4:00 AM					0					0					0	<u> </u>				0		
4:30 AM					0					0					0					0		
4:45 AM Hourly Total	0	0	0	0	0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
5:00 AM					0					0					0					0		
5:30 AM					ŏ					0										0		
5:45 AM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
6:00 AM 6:15 AM					0					0 0					0 0					0 0		
6:30 AM					0					0					0					0		
Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
7:00 AM 7:15 AM	1 0	40 52	1 2		42 54	0	5 9	3		7 14	0 1	104 116	1		105 117	1	1 1	2		23		
7:30 AM 7:45 AM	4	71 82	0 0		75	0	2 3	0		2 6	2	143 74	0		145 	1	2 0	7		10	D	
Hourly Total	13	245	3	0	0 261	2	19	8 0	0	29	6	437	2	0 0	445	4	4	12	0	0 20	D	
8:00 AM 8:15 AM	0	40 55	1		47	2	4	1		7	2	65	0		67	0	2	1		3		
8:30 AM 8:45 AM	6 2	44 53	0		50 55	0	0 1	1		1 3	3	83 79	0		86 82	2	1 0	1		4		
Hourly Total 9:00 AM	9 5	198 39	1	0	0 208	3	11 6	7 0	0	21 7	8	285 65	1	0 0	294	2	3	4	0	0 9		
9:15 AM	2	39	0		41	1	3	0		4	1	50	ŏ _		51	1	0	ŏ _		1		
9:30 AM 9:45 AM	2	43 45	0		40 47	1	2	1		э 4	4 2	50 54	0		54 56	0	2	1		3		
Hourly Total 10:00 AM	<u>11</u> 9	166 46	1 0	0	0 178 55	2	13 2	5 0 0	0	20 3	7	219 55	0	0 0	226 58	1	3	1	0	0 6		
10:15 AM	2	52 48	0		54	0	3	0		3	0	49 47	0		49	0	2	0		2		
10:45 AM	6	36	1		43	Ö	3	4		7	3	51	0		54	0	0	0		0		
Houriy Total 11:00 AM	5	52	2	0	<u> </u>	1	5	1	0	7	2	43	1	0 0	46	2	3	1	0	<u> </u>	3	
11:15 AM 11:30 AM	3 8	41 50	0 0		44 58	0	3 4	0		3 4	1	54 44	0		55 	0	1 1	5		6 5		
11:45 AM	0	40	0	0	40	1	4	2		7	3	56	0	0 0	59	0	4	1	0	5	2	
12:00 PM	5	71	0		76	0	2	1		3	4	41	0	0 0	45	1	2	1	0	4	2	
12:15 PM 12:30 PM	7 2	40 55	0		47 57	1	0 3	2		1 6	1	56 55	0		57 57	0	3 1	4 5		7 6		
12:45 PM Hourly Total	4	56 222	0	0	60 0 240	0	2	3 0	0	2	5	51 203	0	0 0	<u>56</u> 215	1	4	2	0	7	. 1	
1:00 PM	3	49	0		52	1	2	3		6	3	62	0		65	0	2	2		4		
1:15 PM 1:30 PM	9	53	0		62	1	3	3		7	1	70	0		71	0	2	3		5		
1:45 PM Hourly Total	26	206	0	0	0 232	3	5 15	6 0	0	5 24	3 9	56 264	3	0 0	60 276	0	2	2	0	4 0 2'	1	
2:00 PM 2:15 PM	5	65 76	0		70	1	3 1	3		7 4	4	58 77	2		64 	1	4	1		6 	3	
2:30 PM	11	79	1		91	1	0	0		1	3	82	2		87	0	1	6		7		
2:45 PM Hourly Total	26	318	1	0	0 345	3	10	6 0	0	7 19	11	285	5	0 0	301	4	13	5 18	0	0 35	5	
3:00 PM 3:15 PM	11 4	121 91	3 0		135 95	0	1 2	3		4 4	7	61 81	1		69 88	4	4 3	5 _		10	3	
3:30 PM	7	92 107	0		99	0	2	1		3	8	67 98	0		75	1	11 4	1		10	3	
Hourly Total	36	411	4	0	0 451	0	10	9 0	0	19	28	307	2	0 0	337	5	22	11	0	0 38	3	
4:00 PM 4:15 PM	5	151	0		156	1	1	1		23	6	95 78	1		85	3	5	1		9		
4:30 PM 4:45 PM	8 3	112 138	0 2		120 143	0	4 5	1		5 7	6 4	105 92	1		112 96	4	5 6	4		10 7	3	
Hourly Total	23	490 130	2	0	0 515	3	11	3 0	0	17	18	370 102	2	0 0	390 108	7	24 9	8	0	0 39	9 1	
5:15 PM	3	115	3		121	2	2	1		5	8	95	1		104	3	4	4		i <sup>-</sup>	1	
5:30 PM 5:45 PM	3	98 89	0		92	1	9 5	0		6	5	86 86	1		93 88	1	6 7	2		9 10	5	
Hourly Total 6:00 PM	23 4	432 71	<u>4</u> 0	0	0 459 75	4	17 5	7 0 0	0	28 5	19 5	371 52	3 0	0 0	393 57	6	26 2	12 1	0	0 44	4	
6:15 PM	0	67	0		67	1	4	0		5	3	70	0		73	0	6	1		7		
6:45 PM	1	48	2		51	2	4	2		8	8	32	0		40	1	3	2		6		
Hourly Total 7:00 PM		260	4	0	0 2/1	3	16	6 0	0	25 0	16	219	0	0 0	235		12	6	0	0 28		
7:15 PM 7:30 PM					0 0					0 0					0					0 0		
7:45 PM	0	0	0	0	0 0	0	0	0 0		0	0	0	0	0 0	0	0	0	0	0	0 0		
8:00 PM		0	0	0	0	Т, т	0	0 0		0		0	0	0 0	0		0	0	0	0		
8:15 PM 8:30 PM					0					0					0					0		
8:45 PM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
9:00 PM					0			Ŭ		0				, ,	0					0		
9:15 PM 9:30 PM					0					0					0					0		
9:45 PM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
10:00 PM 10:15 PM					0					0					0					0		
10:30 PM					0					0					0					0		
10:45 PM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
11:00 PM 11:15 PM					0					0 0					0					0		
11:30 PM					0					0					0					0		
Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0	1	

### **Multi-Way Stop Application**

### OMUTCD Section 2B.07

- A. Where traffic control signals are justified, the multi-way stop is an interim measure that can Warranted? be installed quickly to control traffic while arrangements are being made for the installation of the traffic control signal.
- B. Five or more reported crashes in a 12-month period that are susceptible to correction by a multiway stop installation. Such crashes include right-turn and left-turn collisions as well as right-angle collisions.
- C. Minimum Volumes:
  - 1 The vehicular volume entering the intersection from the major street approaches (total of both approaches) averages at least 300 vehicles per hour for any 8 hours of an average day.
  - 2 The combined vehicular, pedestrian, and bicycle volume entering the intersection from the minor street approaches (total of both approaches) averages at least 200 units per hour for the same 8 hours, with an average delay to minor-street vehicular traffic of at least 30 seconds per vehicle during the highest hour.\*

\*If this condition is satisfied, there must also be an average delay of at least 30 seconds per vehicle during the peak hour.

- 3 If the 85th-percentile approach speed of the major-street traffic exceeds 40 mph, the minimum volume warrants are 70 percent of the values provided in Items 1 and 2.
- D. Where no single criterion is satisfied, but where Criteria B, C.1, and C.2 are all satisfied to 80 percent of the minimum values. Criterion C.3 is excluded from this condition.

Other criteria that may be considered in an engineering study include:

- A. The need to control left-turn conflicts;
- B. The need to control vehicle/pedestrian conflicts near locations that generate high pedestrian volumes;
- C. Locations where a road user, after stopping, cannot see conflicting traffic and is not able to negotiate the intersection unless conflicting cross traffic is also required to stop; and
- D. An intersection of two residential neighborhood collector (through) streets of similar design and operating characteristics where multi-way stop control would improve traffic operational characteristics of the intersection.

Are the requirements for Multi-Way Stop Satisfied?: Yes



No

Yes

			A	UTOCALC	table			
		Each ho	our is indivi	dually chec	ked and talli	ed if "met"	•	
Lanes Major/	ADJU: VOLU	STED IMES	Condi	tion C.1	Condi	tion C.2	Cond	ition D
Minor	MALOD	MINOR	1	00%	7	0%	8	0%
	WAJUR	MINOR	MAJ.	MIN.	MAJ.	MIN.	MAJ.	MIN.
Re	quired Volu	imes	300	200	210	140	240	160
6:00 AM	0	0						
6:15 AM	147	7						
6:30 AM	318	21	1		1		1	
6:45 AM	538	23						
7:00 AM	706	29						
7:15 AM	665	32						
7:30 AM	617	25	1		1		1	
7:45 AM	533	24						
8:00 AM	502	21						
8:15 AM	505	18						
8:30 AM	474	15	1		1		1	
8:45 AM	438	19						
9:00 AM	404	20						
9:15 AM	408	16						
9:30 AM	419	15	1		1		1	
9:45 AM	423	17						
10:00 AM	417	20						
10:15 AM	409	24						
10:30 AM	405	24	1		1		1	
10:45 AM	405	21						
11:00 AM	407	22						
11:15 AM	423	20						
11:30 AM	428	21	1		1		1	
11:45 AM	438	22						
12:00 PM	455	24						
12:15 PM	451	24						
12:30 PM	490	25	1		1		1	
12:45 PM	509	24						
1:00 PM	508	24						
1:15 PM	525	25						
1:30 PM	539	28	1		1		1	
1:45 PM	584	30						
2:00 PM	646	35						
2:15 PM	716	41						
2:30 PM	742	33	1		1		1	
2:45 PM	738	39						
3:00 PM	788	38						
3:15 PM	777	35						
3:30 PM	835	39	1		1		1	
3:45 PM	893	38						
4:00 PM	905	38						
4:15 PM	957	43						
4:30 PM	941	45	1		1		1	
4:45 PM	911	41						
5:00 PM	852	44						
5:15 PM	739	35						
5:30 PM	654	32	1		1		1	

5:45 PM	595	28						
6:00 PM	506	25						
6:15 PM	374	20						
6:30 PM	234	15			1			
6:45 PM	91	8						
7:00 PM	0	0						
7:15 PM	0	0						
7:30 PM	0	0						
7:45 PM	0	0						
8:00 PM	0	0						
8:15 PM	0	0						
8:30 PM	0	0						
8:45 PM	0	0						
9:00 PM	0	0						
9:15 PM	0	0						
9:30 PM	0	0						
9:45 PM	0	0						
10:00 PM	0	0						
10:15 PM	0	0						
10:30 PM	0	0						
10:45 PM	0	0						
11:00 PM	0	0						
11:15 PM	0	0						
11:30 PM	0	0						
11:45 PM	0	0						
HOURS	MET		12	0	13	0	12	0
CONDIT	ION SATIS	FIED?	N	10	N	0	N	0

STUDY AND ANALYSIS INFORMAT	ION	TRAFFIC SI	GNAL	WARR	ANT ANALYS
				Warrant	
Municipality		1	Applicable?	Satisfied?	Notes
Suffield Township	ODOT	Warrant 1, Eight-Hour	Yes	No	Hole
County: Portage Analysis Date:	9/8/2022				
ODOT Engineering District: Google map link: <u>Map</u> Agency/ Company Name Performing Warrant Analysis:	Lanham Engineering, LLC	Warrant 2, Four-Hour Vehicular Volume	Yes	No	Fig
Analysis Information		Warrant 3, Peak Hour	No		Signals installed under ac
Data Collection Data: 5///2022		For Warrants 1-3 new	DDOT signa	ls must be ba	sed off of 100% volume
Day of the Week: Wednesday		Warrant 4, Pedestrian Volume	No		If this warrant is met, and a tr engineering study, the traffic of pedestrian signal heads comp Chapter 4E
Is the intersection in a built-up area of an isolated community of pop	<10,000 No	Warrant 5, School Crossing	No		
Existing Traffic Signal at intersection: No		Warrant 6, Coordinated Signal System	No		(Shall not be use
Total Number of Approaches at Intersection: 4		Warrant 7, Crash Experience	Yes	No	If this is the sole warrant devices which provide pro within a coordinated s actuated if ins
Major Street Information		Warrant 8, Roadway Network	No		(Shall not be use
Major Street Name and Route Number: SR-43		Warrant 9, Intersection Near a Grade Crossing	No		
Major Street Approach Direction: N-Bound S-Bound		Multi-Way Stop Warrant	Yes	Yes	May be used as an int
Number of Thru Lanes on Each Major Street Approach: 1	NE(S)	The satisfaction of a traffic sig	nal warran	it or warrant control	s shall not in itself r signal.
Speed Limit or 85th Percentile Speed on the Major Street*: 45	Н	If no warrants are satisfied, addition	onal options	s may be con	sidered:
*Unknown assumes below 45 mph		1. An engineering study, performe	ed by a firm	prequalified	by ODOT for signal de
		district, may be used to justify a ne	ew signal in	stallation or	etention of an existing
Minor Street Information		meet the published warrants. An e	example of	such an insta '	ince is a traffic signal
Minor Street Name and David Number Transp		that serves to reduce queuing acr	oss the trac	KS. na movemer	t counte fail to eatiefy
Minor Street Name and Route Number: Trates		accentable to use traffic volumes	nroiected to	the second	vear after project com
Minor Street Approach Configuration:		Forecasting Section should prov	ride the proj	ected traffic	volumes.
	T.	does not meet traffic signal warra	nts (see Ch	apter 4C of 1	EM) or at a location t
		under Sections 4C.05 and/or 4C.0 on PHB Score Sheet and submi	6 but a dec t to ODOT.	cision is made	e to not install a traffic
1 2 3 4	5	Considerations such as geometric	s and lack	of sight dista	nce generally have no
Number of Thru Lanes on Each Minor Street Approach: 1	NE(S)	signal warrants. These considerat	ions may a	llow an other	wise unwarranted traf
Apply Right Turn Lane Reduction*: Yes		percent local cost. Please review	TEM 402-4	for details.	
"Right Turn Lane Reduction Shall be used for Warrants 1, 2, & 3 for New ODOT Signals. Please refer to TEM 402-3.2 for clarification and criteria under which Right Turn Reduction is not required.		Notes:	Conclusion:	Do Not Inst	all New Traffic Signal

### **BIS FINDINGS**

### es and Comments:

gure 4C-2 (70% Factor)

er Warrant 3 should be traffic ctuated.

Peak Hour
4:15 PM
5:15 PM

e thresholds (TEM 402-3.2)

traffic control signal is justified by an control signal shall be equipped with plying with the provisions set forth in E of the OMUTCD.

Peak Hour
4:15 PM
5:15 PM

N/A

ed as the sole warrant in the analysis)

nt, signal must be semi-actuated with control oper coordination if installed at an intersection system and normally should be fully traffic stalled at an isolated intersection.

ed as the sole warrant in the analysis)

#### Figure 4C-9

terim measure if traffic signal warrants are satisfied.

### require the installation of a traffic

design, if approved by the ODOT ng signal that otherwise does not I in proximity to a railroad crossing

y a signal warrant, it may be mpletion. The **Modeling and** 

edestrian crossings at a location that that meets traffic signal warrants c control signal. **Please fill inputs** 

not been accepted in lieu of satisfying infinition of satisfying infinition of the set o



### **OMUTCD WARRANT 1, EIGHT-HOUR VEHICULAR VOLUME**

Number of Lanes for Moving Traffi on Each Approach								
Major Street:	1 Lane							
Minor Street:	1 Lane							

Built up Isolated Community with Less Than 10,000 Population or Above 40 MPH on Major Street? Yes

\*Only applicable after an adequate trial of other alternatives (See section 4C.02.06 of the 2012 OMUTCD)

4:30 PM	921	146							1	1					1	1		
4:45 PM	898	141			1	1												
5:00 PM	849	127	1				1	1			1	1	1	1				
5:15 PM	727	103															1	1
5:30 PM	660	67							1	1					1			
5:45 PM	613	58			1													
6:00 PM	524	48	1								1							
6:15 PM	399	32																
6:30 PM	249	23																
6:45 PM	91	13																$\square$
7:00 PM	0	0																$\square$
7:15 PM	0	0																$\square$
7:30 PM	0	0																$\square$
7:45 PM	0	0																$\square$
8:00 PM	0	0																$\square$
8:15 PM	0	0																$\square$
8:30 PM	0	0																$\square$
8:45 PM	0	0																$\square$
9:00 PM	0	0																
9:15 PM	0	0																
9:30 PM	0	0																
9:45 PM	0	0																
HOURS MET			8	0	12	2	4	3	7	5	12	2	5	4	12	3	11	10
WARRANT SATISFIED?		NO NO		NO		NO		NO				NO						

Warrant Met: No

Notes:

Published Jan. 2022


		Sou	thbound	Approach			Wes	tbound Ap	proach			No	orthbound	Approach			E	astbound	Approact	h		
Start Time	Right	Thru	Left	U-Turn P	eds App Total	Right	Thru	Left U-	u Turn Peds	App Total	Right	Thru	Left	U-Turn Pe	ds App Total	Right	Thru	Left	U-Turn	Peds A	pp otal	NOTES:
12:00 AM 12:15 AM					0	·				0 0					0 0	·					0	It should be noted that if data is
12:30 AM 12:45 AM					0 0										0 0						0	Totals or Approach Totals, that
Hourly Total 1:00 AM	0	0	0	0	0 0	0	0	0	0 0	0	0	0	0	0 0	0 0	0	0	0	0	0	0 0	lost. This should not affect the
1:15 AM 1:30 AM					0					0					0						0 0	copied from a program that
1:45 AM Hourly Total	0	0	0	0	0	0	0	0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0 0	user.
2:00 AM 2:15 AM					0					0					0						0 0	
2:30 AM 2:45 AM					0 0					- 0 0					0						0	
3:00 AM	0	0	0	0	0 0		0	0	0 0	0	0	0	0	0 0	0		0	0	0		0	
3:30 AM																					0	
Hourly Total	0	0	0	0	0 0	0	0	0	0 0	0	0	0	0	0 0	) 0	0	0	0	0	0	0	
4:00 AM 4:15 AM																					0	
4:45 AM	0	0	0	0	0		0	0	0 0			0	0	0 0	0		0	0	0		0	
5:00 AM	Ŭ			0	0	Ļ,	0	•	0 0	- 0				0 0	0	Ļ					0	
5:30 AM																					0	
Hourly Total 6:00 AM	0	0	0	0	0 0	0	0	0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0	
6:15 AM 6:30 AM					0 0					0					0 0						0	
6:45 AM Hourly Total	0	0	0	0	0	0	0	0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0	
7:00 AM 7:15 AM	1 5	40 51	0		41 57	4 4	3 8	2		9 12	1 0	102 101	14 27		117 128	2 10	1	3 10		2	6 21	
7:30 AM 7:45 AM	8 9	60 72	2		70 86	3	13 8	1		17 9	2	125 <u>7</u> 3	25 <u>3</u> 0		152 103	6 3	3 2	15 6		2	24  1	
Hourly Total 8:00 AM	23 2	223 44	8 1	0	0 254 47	12 1	32 4	3	0 0	47 7	3	401 60	96 21	0 0	) 500 82	21	7	34 1	0	0 6	5 5	
8:15 AM 8:30 AM	0 3	56 43	1 0		57 46	0 2	4 3	0 3		4	2 1	57 85	11 22		70 108	5 5	0 2	4 1			9 8	
8:45 AM Hourly Total	5 10	48 191	1 3	0	54 0 204	1 4	7	2 7	0 0	10 29	1 5	74 276	13 67	0 0	88 ) 348	6 17	3	7	0	0 3	16 38	
9:00 AM 9:15 AM	2 1	37 39	1		40 40	3 2	7 9	0		10 11	3 3	60 49	13 8		76 60	8	1 7	2 2		1 1	1 15	
9:30 AM 9:45 AM	2 6	43 39	1		46 46	1	7 1	0		- 8 6	0	47 50	10 13		57 64	8 6	4 2	6 2		1 1	18 10	
Hourly Total 10:00 AM	11 5	158 43	3 0 _	0	0 <u>172</u> 48	10 1	24 5	1	0 0		7	206 49	44 7	0 0	) <u>257</u> 57	28	14 5	12 6	0	<u>    0     5</u> 1	54 13	
10:15 AM 10:30 AM	2 3	46 46	2		50 50	1	2 4	1		4 5	2 1	47 43	12 4		61 48	4	3 2	3 8		1 1	10 16	
10:45 AM Hourly Total	2 12	37 172	1	0	40 0 188	4	5 16	1 3	0 0	7 23	2	51 190	6 29	0 0	59 ) 225	5 17	3 13	2 19	0	0 4	10 19	
11:00 AM 11:15 AM	5 1	48 41	1 2		54 44	0	4	1		3	0	43 44	7		46 51	3	4	5		1	12 19	
11:30 AM 11:45 AM	2 4	47 44 190	2	0	49 50	0	5	1	0 0	- 9 4	1	39 51	7	0 0	55 59	10	3	6 7	0	2	20	
12:00 PM	5	57	2	0	<u>64</u> 64	3	6	0	0 0	- 9	1	36	16	0 0	53	8	4	5	0	1	17	
12:30 PM	4	52 51	2		57	2	2	2		6	0	50 42	11		61	14	3 4 3	6		2	24	
Hourly Total	21 4	191 49	5	0	0 217	11	4 16 7	4	0 0	31	3	175	44	0 0	) 222	38	14 4	28	0	0 8	30	
1:15 PM 1:30 PM	3	47 49	1		51	1	6 3	0		- 7 5	1	71 62	6		78	6 13	2 2	6		1	14 21	
1:45 PM Hourly Total	5	47	1 5	0	53 0 214	0	2	1	0 0	- <u>3</u> 22	2	57 251	12	0 0	71	9	6	4	0	<u>1</u> 0 7	19 74	
2:00 PM 2:15 PM	10 5	55 72	2		67 78	1	2	1		- 4 5	2 2	62 58	8 11		72	10 14	8 8	6 11		2	24 33	
2:30 PM 2:45 PM	6 10	71 96	0 3		77 109	4	4 1	0		8 3	1 0	74 64	16 7		91 71	22 6	2 6	11 6		3	85 18	
Hourly Total 3:00 PM	31 15	294 99	6 3	0	0 <u>331</u> 117	10 1	9 3	1	0 0	20 4	5	258 58	42 7	0 0	) <u>305</u> 68	52 10	24 6	34 11	0	0 1	10 27	
3:15 PM 3:30 PM	7 5	85 90	2 3		94 98	1	5 3	1		7	2 2	81 72	13 12		96 86	18 15	13 10	6 5		3	87 80	
3:45 PM Hourly Total	9 36	90 364	7 15	0	106 0 415	0	3 14	1 3	0 0	4 20	3 10	88 299	9 41	0 0	100 ) 350	23 66	11 40	13 35	0	4 0 14	17 41	
4:00 PM 4:15 PM	4	89 138	3		96 	2	6 5	0		- <sup>8</sup> 7	4	83 76	9		96 90	30 20	10 13	12 10		5	52 13	
4:30 PM 4:45 PM	8	102 134	6 1	0	116 138	4	6 3	1	0 0	- 11 6	0	100 80	12	0	112 91	13 26	9	8	0	3	80 16	
5:00 PM	8	403 124	4	U	<u>497</u> 136	2	20	2	0 0	- 6 - 10	2	96 00	13	0 0	<u>389</u> 111	18	43 13	12	0	4	13	
5:30 PM	8	93 70	2		103	3 1 4	4	3 2 2		- 7	3	90 85 84	9 14 7		102	26 11 10	9 11	14 4 5		2	24	
Hourly Total	25 3	403 67	17 3	0	0 445	10 2	13 3	9	0 0	32	6	355 47	43	0 0	) <u>404</u> 52	65	49	35 5	0	0 1	49	
6:15 PM 6:30 PM	2	64 70	2		68	1	5	2		8	2	74 62	6		82	8	4	1		1	13  4	
6:45 PM Hourly Total	3	47	2	0	<u> </u>	2	3	1	0 0	 6 25	1	33	5	0 0	39	27	6	3	0	1	13	
7:00 PM 7:15 PM					0					- 0					0				-		0	
7:30 PM 7:45 PM					0					0					0						0 0	
Hourly Total 8:00 PM	0	0	0	0	0 0	0	0	0	0 0	0	0	0	0	0 0	00	0	0	0	0	0	0 0	
8:15 PM 8:30 PM					0					0					0						0 0	
8:45 PM Hourly Total	0	0	0	0	0 0	0	0	0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0 0	
9:00 PM 9:15 PM					0 0					0					0						0	
9:30 PM 9:45 PM					0					- 0					0						0	
Hourly Total 10:00 PM	0	0	0	0	0 0	0	0	0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0	
10:15 PM 10:30 PM					0					0					0						0	
10:45 PM Hourly Total	0	0	0	0	0 0	0	0	0	0 0	0	0	0	0	0 0	0	0	0	0	0	0	0	
11:00 PM 11:15 PM					0										0						0	
11:45 PM Hourly Total	0	0	0	0	0 0 0	0	0	0	0 0	- 0	0	0	0	0 0	0	0	0	0	0	0	0	

## **Multi-Way Stop Application**

#### OMUTCD Section 2B.07

- A. Where traffic control signals are justified, the multi-way stop is an interim measure that can Warranted? be installed quickly to control traffic while arrangements are being made for the installation of the traffic control signal.
- B. Five or more reported crashes in a 12-month period that are susceptible to correction by a multiway stop installation. Such crashes include right-turn and left-turn collisions as well as right-angle collisions.
- C. Minimum Volumes:
  - 1 The vehicular volume entering the intersection from the major street approaches (total of both approaches) averages at least 300 vehicles per hour for any 8 hours of an average day.
  - 2 The combined vehicular, pedestrian, and bicycle volume entering the intersection from the minor street approaches (total of both approaches) averages at least 200 units per hour for the same 8 hours, with an average delay to minor-street vehicular traffic of at least 30 seconds per vehicle during the highest hour.\*

\*If this condition is satisfied, there must also be an average delay of at least 30 seconds per vehicle during the peak hour.

- 3 If the 85th-percentile approach speed of the major-street traffic exceeds 40 mph, the minimum volume warrants are 70 percent of the values provided in Items 1 and 2.
- D. Where no single criterion is satisfied, but where Criteria B, C.1, and C.2 are all satisfied to 80 percent of the minimum values. Criterion C.3 is excluded from this condition.

Other criteria that may be considered in an engineering study include:

- A. The need to control left-turn conflicts;
- B. The need to control vehicle/pedestrian conflicts near locations that generate high pedestrian volumes;
- C. Locations where a road user, after stopping, cannot see conflicting traffic and is not able to negotiate the intersection unless conflicting cross traffic is also required to stop; and
- D. An intersection of two residential neighborhood collector (through) streets of similar design and operating characteristics where multi-way stop control would improve traffic operational characteristics of the intersection.

Are the requirements for Multi-Way Stop Satisfied?: Yes No

Yes

Yes

No

Yes

No

No

No

No

No

			A	UTOCALC	table			
		Each ho	our is indivi	dually chec	ked and talli	ed if "met"		
Lanes Major/	ADJU: VOLU	STED JMES	Condi	tion C.1	Condi	tion C.2	Cond	ition D
Minor		MINOD	1	00%	7	0%	8	0%
	WAJUR	WINOR	MAJ.	MIN.	MAJ.	MIN.	MAJ.	MIN.
Re	equired Volu	imes	300	200	210	140	240	160
6:00 AM	0	0						
6:15 AM	158	8						
6:30 AM	343	23	1		1		1	
6:45 AM	565	44						
7:00 AM	754	58						
7:15 AM	725	57						
7:30 AM	667	46	1		1		1	
7:45 AM	599	28						
8:00 AM	552	32						
8:15 AM	539	35						
8:30 AM	512	40	1		1		1	
8:45 AM	461	49						
9:00 AM	429	43						
9:15 AM	418	48						
9:30 AM	429	43	1		1		1	
9:45 AM	424	42						
10:00 AM	413	46						
10:15 AM	408	41						
10:30 AM	392	49	1		1		1	
10:45 AM	398	48						
11:00 AM	408	56						
11:15 AM	425	59						
11:30 AM	427	59	1		1		1	
11:45 AM	441	64						
12:00 PM	439	65						
12:15 PM	448	69						
12:30 PM	480	65	1		1		1	
12:45 PM	485	63						
1:00 PM	502	61						
1:15 PM	515	63						
1:30 PM	535	79	1		1		1	
1:45 PM	580	89						
2:00 PM	636	90						
2:15 PM	682	93			<u> </u>			
2:30 PM	723	95	1		1		1	
2:45 PM	739	93			-			
3:00 PM	765	115						
3:15 PM	//2	132						
3:30 PM	819	142	1			1	1	
3:45 PM	863	142						
4:00 PM	886	140						
4:15 PM	941	139						
4:30 PM	921	146	1				1	
4:45 PM	898	141						
5:00 PM	849	127						
5:15 PM	727	103						
5:30 PM	660	67	1	1	1		1 1	

5:45 PM	613	58						
6:00 PM	524	48						
6:15 PM	399	32						
6:30 PM	249	23			1		1	
6:45 PM	91	13						
7:00 PM	0	0						
7:15 PM	0	0						
7:30 PM	0	0						
7:45 PM	0	0						
8:00 PM	0	0						
8:15 PM	0	0						
8:30 PM	0	0						
8:45 PM	0	0						
9:00 PM	0	0						
9:15 PM	0	0						
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9:45 PM	0	0						
10:00 PM	0	0						
10:15 PM	0	0						
10:30 PM	0	0						
10:45 PM	0	0						
11:00 PM	0	0						
11:15 PM	0	0						
11:30 PM	0	0						
11:45 PM	0	0						
HOURS	MET		12	0	13	2	13	0
CONDIT	ION SATIS	FIED?	N	10	N	0	N	0

STUDY AND ANALYSIS INFORMATION		TRAFFIC SI	GNAL	WARRA	ANT ANALYS
				Warrant	
Municipality: Traffic Volumes Obtained By:			Applicable?	Satisfied?	Notes
Suffield Township	ODOT	Warrant 1, Eight-Hour Vehicular Volume	Yes	No	
County: Portage Analysis Date:	9/8/2022				
ODOT Engineering <u>4</u> Agency/ Company Name Performing Lanhar District: Warrant Analysis: Coogle map link: Map	m Engineering, LLC	Warrant 2, Four-Hour Vehicular Volume	Yes	No	Fig
Analysis Information		Warrant 3, Peak Hour	No		Signals installed under
		-			au
Data Collection Date: 5/4/2022		For Warrants 1-3, new	ODOT signa	ls must be ba	sed off of 100% volume
Day of the Week: Wednesday		Warrant 4, Pedestrian Volume	No		If this warrant is met, and a tr engineering study, the traffic o pedestrian signal heads comp Chapter 4E
ls the intersection in a built-up area of an isolated community of <10,000 population	No	Warrant 5, School Crossing	No		
Existing Traffic Signal at intersection: No		Warrant 6, Coordinated Signal System	No		(Shall not be use
Total Number of Approaches at Intersection: 4		Warrant 7, Crash Experience	No		If this is the sole warran devices which provide pro within a coordinated s actuated if ins
Major Street Information		Warrant 8, Roadway Network	No		(Shall not be use
Major Street Name and Route Number: SR-43		Warrant 9, Intersection Near a	No		
N-Bound		Grade Crossing			May be used as an int
Major Street Approach Direction: S-Bound		Multi-Way Stop Warrant	No		
Number of Thru Lanes on Each Major Street Approach: 1 LANE(S)		The satisfaction of a traffic sig	inal warran	t or warrant control	s shall not in itself i signal.
Speed Limit or 85th Percentile Speed on the Major Street*: 45 MPH		If no warrants are satisfied, addition	onal options	may be con	sidered:
*Unknown assumes below 45 mph		1. An engineering study, performe	ed by a firm	prequalified	by ODOT for signal d
		district, may be used to justify a ne	ew signal in	stallation or ı	retention of an existin
Minor Street Information		thet serves to reduce queuing cor	example of s	such an Insta	ance is a traffic signal
Minor Street Name and Route Number: Trares		2. According to TEM 402-2. If the	actual turnii	na movemen	t counts fail to satisfy
		acceptable to use traffic volumes	projected to	the second	vear after project con
Minor Street Approach Configuration:		Forecasting Section should prov	vide the proj	ected traffic	volumes.
		3. A pedestrian hybrid beacon ma	y de consid nts (see Ch	ered for insta	EM) or at a location f
		under Sections 4C 05 and/or 4C 0	)6 but a dec	ision is made	e to not install a traffic
		on PHB Score Sheet and submi	it to ODOT.		
1 2 3 4 5		Considerations such as geometric	s and lack	of sight dista	nce generally have no
Number of Thru Lanes on Each Minor Street Approach: 1 LANE(S)		signal warrants. These considerat	ions may al	low an other	wise unwarranted traf
Apply Right Turn Lane Reduction*: Yes		percent local cost. Please review	IEM 402-4	tor details.	
ODOT Signals. Please refer to TEM 402-3.2 for clarification and criteria		(	Conclusion:	Do Not Insta	all New Traffic Signal
under which Right Turn Reduction is not required.		Notes:			

# SIS FINDINGS

#### es and Comments:

gure 4C-2 (70% Factor)

er Warrant 3 should be traffic ctuated.

Peak Hour
4:30 PM
5:30 PM

e thresholds (TEM 402-3.2)

traffic control signal is justified by an control signal shall be equipped with plying with the provisions set forth in E of the OMUTCD.

Peak Hour
4:15 PM
5:15 PM

N/A

ed as the sole warrant in the analysis)

nt, signal must be semi-actuated with control oper coordination if installed at an intersection system and normally should be fully traffic installed at an isolated intersection.

ed as the sole warrant in the analysis)

#### Figure 4C-9

terim measure if traffic signal warrants are satisfied.

#### require the installation of a traffic

design, if approved by the ODOT ng signal that otherwise does not I in proximity to a railroad crossing

y a signal warrant, it may be mpletion. The **Modeling and** 

edestrian crossings at a location that that meets traffic signal warrants c control signal. **Please fill inputs** 

not been accepted in lieu of satisfying infinition of satisfying infinition of the set o



## **OMUTCD WARRANT 1, EIGHT-HOUR VEHICULAR VOLUME**

Number of La	nes for Moving Traffic												
on Ea	on Each Approach												
Major Street:	1 Lane												
Minor Street:	1 Lane												

Built up Isolated Community with Less Than 10,000 Population or Above 40 MPH on Major Street?

	Lanes	Adju	sted		Condi	ition A			Condi	tion B	Cond. A Cond. B Cond				VB*				
	Major/	Volu	imes									Con	d. A	Cor	id. B	Cor	nd. A	Con	nd. B
	Minor	Major	Minor	10 Mai	00% Min	70 Moi	)% Min	10 Moi	00% Min	70 Moi	)% Min	80 Mai	)% Min	80 Moi	)%   Min	56 Moi	5% Min	56 Moi	5% Min
	1/1		i X	500	150	350	105	750	75	525	53	400	120	600	60	280	84	420	42
	2+/1		-	600	150	420	105	900	75	630	53	480	120	720	60	336	84	504	42
	2+/2+			600	200	420	140	900	100	630	70	480	160	720	80	336	112	504	56
	1 / 2+			500	200	350	140	750	100	525	70	400	160	600	80	280	112	420	56
	12:00 AM	0	0																
	12:15 AM	0	0																
	12:30 AM	0	0																
	1:00 AM	0	0																
	1:15 AM	0	0																
	1:30 AM	0	0																
	1:45 AM	0	0																
	2:00 AM 2:15 AM	0	0																
	2:30 AM	0	0																
	2:45 AM	0	0																
	3:00 AM	0	0																
	3:15 AM	0	0																
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$\vdash$	4:00 AM	0	0																
	4:15 AM	0	0																
	4:30 AM	0	0																
⊨	4:45 AM	0	0						<b> </b>										<b> </b>
├──	5:00 AM 5:15 AM	0	0																
	5:30 AM	0	0																
	5:45 AM	0	0																
$\vdash$	6:00 AM	0 157	0						<u> </u>										<u> </u>
F	6:30 AM	341	39													1			
	6:45 AM	563	61	1		1				1	1	1						1	1
	7:00 AM 7:15 AM	749	74											1	1				
<u> </u>	7:30 AM	660	62													1			
	7:45 AM	591	50	1		1				1		1						1	1
	8:00 AM	546	47																
<u> </u>	8:30 AM	509	40 51													1			
	8:45 AM	457	55			1						1						1	1
	9:00 AM	425	51																
<u> </u>	9:15 AM 9:30 AM	415	60 57													1			
	9:45 AM	420	61			1						1						1	1
	10:00 AM	407	58																
	10:15 AM	403	57 69													1			
<u> </u>	10:30 AM	396	66			1										-			
	11:00 AM	407	80									1							
	11:15 AM	422	76													1		1	1
-	11:45 AM	436	85			1													
	12:00 PM	436	87									1							
	12:15 PM	443	99															1	1
<u> </u>	12:30 PM	473	90			1													
	1:00 PM	496	82									1							
	1:15 PM	509	85	1						4								1	1
$\vdash$	1:45 PM	527 576	105			1	1		-	1	1								-
	2:00 PM	631	121			Ė	Ŀ					1	1	1	1				
$\vdash$	2:15 PM	680	128	1														1	1
$\vdash$	2:30 PM 2:45 PM	735	123			1	1		-	1	1								-
	3:00 PM	760	148					1	1			1	1	1	1				
$\vdash$	3:15 PM	767	166	1	1													1	1
$\vdash$	3:45 PM	815 859	174			1	1		-	1	1								-
	4:00 PM	885	172					1	1			1	1	1	1				
$\vdash$	4:15 PM	936	175	1	1													1	1
$\vdash$	4:30 PM 4:45 PM	919 896	184			1	1			1	1								
F	5:00 PM	846	178				Ľ	1	1			1	1	1	1				
	5:15 PM	728	130	1														1	1
┣—	5:30 PM	659	100 80			1		<u> </u>	<u> </u>	1									
$\vdash$	6:00 PM	522	66			<u> </u>						1			-	<u> </u>			
	6:15 PM	397	47																
$\vdash$	6:30 PM	247	33									<u> </u>					<u> </u>		
	7:00 PM	0	18																
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$\vdash$	7:30 PM	0	0																<u> </u>
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	8:30 PM	0	0																
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	9:30 PM	0	0																
	9:45 PM	0	0	7	2	10	4	2	2	7	6	10	4	F	F	10	6	44	14
Uno		ATICE	502		4			J N	0			12	4 N	0	5	12			

\*Only applicable after an adequate trial of other alternatives (See section 4C.02.06 of the 2012 OMUTCD)

Warrant Met: No Notes:

Published Jan. 2022



		Southbo	und Approach			Westbou	nd Approach			Northbound	Approach			East	bound Appro	ach		
Start Time	Right T	hru Left	U-Turn P	eds App	Right	Thru Left	U-Turn Peds	App Total	Right Thru	Left	U-Turn Peds	App Total	Right	Thru I	Left U-Turr	Peds	App Total	NOTES:
12:00 AM 12:15 AM				0 0				0 0				0					0 0	It should be noted that if data is
12:30 AM 12:45 AM				0 0													0	Totals or Approach Totals, that
Hourly Total 1:00 AM	0	0 0	0	0 0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	lost. This should not affect the
1:15 AM 1:30 AM				0				0				0					0 0	copied from a program that
1:45 AM Hourly Total	0	0 0	0	0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	user.
2:00 AM 2:15 AM				0				0				0					0	
2:30 AM 2:45 AM				0	<u> </u>			0				<u> </u>					0	
3:00 AM	0	0 0	U	0	0	0 0	0 0	0	0 0	0	0 0	0		0	0 0	0	0	
3:30 AM																	0	
Hourly Total	0	0 0	0	0 0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	
4:15 AM																	0	
4:45 AM Hourly Total	0	0 0	0	0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	
5:00 AM 5:15 AM		<u> </u>		0				0				0					0	
5:30 AM 5:45 AM																	0 0	
Hourly Total 6:00 AM	0	0 0	0	0 0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	
6:15 AM 6:30 AM				0				0				0					0 0	
6:45 AM Hourly Total	0	0 0	0	0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	
7:00 AM 7:15 AM	1 3 5 4	18 1 18 3		40 56	4 4	8 4 17 3		16 24	1 101 0 101	15 27		117 128	2 10	1	4		7 24	
7:30 AM 7:45 AM	8696	0 2 9 5		70 83	3 1	15 1 11 3		19 15	2 125 0 72	25 31		152 103	6 3	3 2	24 9		33 14	
Hourly Total 8:00 AM	23 2 2 4	15 11 0 1	0	0 <u>249</u> 43	12	51 11 10 6	0 0	74	3 399 1 59	98 22	0 0	500 82	21	7 3	50 0 4	0	78 8	
8:15 AM 8:30 AM	0 5	i5 2 2 0		57 45	0 2	8 1 3 4		9	2 57 1 85	11 22		70 108	5	0 2	5		10 10	
8:45 AM Hourly Total	5 4 10 1	84 4	0	53 0 198	4	8 3 29 14	0 0	12 47	1 74 5 275	13 68	0 0	88 348	17	3	8 20 0	0	1/ 45	
9:00 AM 9:15 AM	2 3	6 1 9 0		39 40	3	13 1 12 0		17 14	3 60 3 49	13 8			6	1 7	3		12 15	
9:30 AM 9:45 AM	2 4	0 2 18 1		44 45	1	9 3 <u>3 2</u>		13 9	0 47 1 50	10 13		<u>57</u>	8	4	5		19 13	
10:00 AM	5 4	3 0		48	1	7 1	0 0	9	1 48	8	0 0	57	28	5	10		59 17	
10:15 AM 10:30 AM	3 4	6 2 3 1		47	1	5 1 8 3		12	2 47	4		48	6	3	5 14		12 22	
Hourly Total	12 1 12 1	65 5 7 2	0	0 182 55	4	8 5 28 10	0 0	42	6 189	30	0 0	225	17	3 13	2 31 0	0	61 16	
11:15 AM	1 4	1 2		44	1	9 2 5 0		6	0 42 0 44	4 7 13		51	8	4	13		25	
11:45 AM Hourly Total	4 4	12 2 77 7	0	49 48 0 196	0	7 3 30 6	0 0	10 	1 51 4 176	7	0 0	59 	10	3	12 43 0		25	
12:00 PM 12:15 PM	5 5	i6 2 12 1		63 40	3	8 1 4 2		12 9	1 36	16 10		53 57	8	4	8		20 25	
12:30 PM 12:45 PM	4 4	9 2		55	2	5 4		11 9	0 50	11 7		61 51	14 9	4	12		30 27	
Hourly Total 1:00 PM	21 1 4 4	88 5 6 1	0	0 <u>214</u> 51	11	23 7 9 3	0 0	41 12	3 175 2 61	44 9	0 0	222 72	38 6	14 4	50 0 14	0	102 24	
1:15 PM 1:30 PM	3 4 5 4	7 1 6 2		51 53	1	11 0 6 4		12 11	1 69 0 62	8		78 67	6 13	2 2	14		22 26	
1:45 PM Hourly Total	5 4 17 1	17 1 86 5	0	53 0 208	0	7 1 33 8	0 0	<u>8</u> 43	2 56 5 248	13 35	0 0	71 288	9 34	6 14	8 47 0	0	23 95	
2:00 PM 2:15 PM	10 5 5 7	62 2 70 1		64 76	1 3	5 4 3 2		10 8	2 60 2 57	10 12		72 71	10 14	8 8	11 23		29 45	
2:30 PM 2:45 PM	6 7 10 9	1 1 15 3		78 108	4 2	4 0 7 1		8 10	1 72 0 64	18 7		91 71	22 6	2 6	18 13		42 25	
Hourly Total 3:00 PM	31 2 15 9	88 7 16 6	0	0 <u>326</u> 117	10	<u>19 7</u> 4 3	0 0	<u>36</u> 8	5 253 3 57	47 8	0 0	<u>305</u> 68	52 10	24 6	65 0 20	0	141 36	
3:15 PM 3:30 PM	7 8	13 2 19 3		92 97	1	7 3 5 2		11 8	2 81 2 72	13 12		96 86	18 15	13 10	11		42 42	
3:45 PM Hourly Total	9 8 36 3	55 19	0	104 0 410	3	8 4 24 12	0 0	12 39	3 87 10 297	10 43	0 0	100 350	23 66	11 40	20 68 0	0	54 174	
4:00 PM 4:15 PM	4 8 6 1	19 3 37 3		96	2	7 0 6 1		9	4 83 2 75	9 13		96	30 20	10 13 0	16		02 49 30	
4:30 PM 4:45 PM	3 1	33 3 60 15	0	139	4 2	8 2	0 0	10 12	1 80	10	0 0	91	26	9 11 42	16		53 202	
5:00 PM	8 1	20 4		<u>490</u> 132 120	2	3 6 9 4	0 0	11 16	2 95	14	0 0		18	13	26		203 57 64	
5:30 PM	8 9	11 3 19 6		102	1	5 4 13 4 5 2			3 85 1 83	14 8		102	11	9	11		31 35	
Hourly Total 6:00 PM	25 3 3 6	96 <u>21</u> 7 3	0	0 442 73	10	30 16 8 2	0 0	56 12	6 352 1 47	46 4	0 0	404 52	65 7	49 6	73 0 8	0	187 21	
6:15 PM 6:30 PM	2 6	i4 2 i6 5		68 76	1	9 2 4 5		12 11	2 74 4 62	6 14		82 80	8	4	8		20 17	
6:45 PM Hourly Total	3 4 13 2	5 4 42 14	0	52 0 269	2	7 <u>3</u> 28 12	0 0	<u>12</u> 47	1 33 8 216	5 29	0 0	39 253	4 27	6 17	8 32 0	0	18 76	
7:00 PM 7:15 PM				0				0				0					0 0	
7:30 PM 7:45 PM				0 0				0				0					0 0	
Hourly Total 8:00 PM	0	0 0	0	0 0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	
8:15 PM 8:30 PM				0				0				0					0	
8:45 PM Hourly Total	0	0 0	0	0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	
9:00 PM 9:15 PM				0								0					0	
9:30 PM 9:45 PM	0	0	0	0 0		0	0	0 0		0	0	0		0	0		0	
10:00 PM	U	0 0	U	0	0	0 0	0 0	0	0 0	U	0 0	0		U	0 0	0	0	
10:15 PM 10:30 PM				0													0	
Hourly Total	0	0 0	0	0 0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	
11:15 PM 11:15 PM				0													0	
11:45 PM Hourly Total	0	0 0	0	0	0	0 0	0 0	0	0 0	0	0 0	0	0	0	0 0	0	0	
			v v		~			0	- 0	~	- 1	0				v v	-	

		S	outhboun	d Approach	1		West	bound Appre	oach			North	bound Ap	proach			3	astbound	Approach	1		
Start Time	Pight	Thru	South		Reds App	Pight	Thru	Westbound	Irp Bodo	Арр	Piaht	Thru	Nouthboun	d Furn Bode	Арр	Pight	Thru	Eastbo	ound	Pode A	рр	NOTES:
12:00 AM	right	mu	Leit	- o naiii	Total 0	Right				Total 0	- Ngin			reds	Total 0	Right	nina	Lon	e-runi	T	otal 0	It should be noted that if data
12:15 AM 12:30 AM					0					0					0						0	copied overtop of the Hourly
12:45 AM					Ő					0		_			<u>0</u>	E					0	Totals or Approach Totals, that the 'AutoSum' Formula will be
Hourly Total 1:00 AM	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	lost. This should not affect the actual totals if the data was
1:15 AM 1:30 AM					0					0					0						0	copied from a program that
1:45 AM	0	0	0	0	0		0	0 0		0	0	0	0	0 0	0		0	0	0		0	user.
2:00 AM	0	0	0	0	0		0	0 0		0		0	0	0 0	0		0	0	0		0	
2:15 AM 2:30 AM					0					0 0					— 0 0						0 0	
2:45 AM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	
3:00 AM					0					0		•	<u> </u>		0						0	
3:15 AM 3:30 AM					0					0					0						0	
3:45 AM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	
4:00 AM					0		-			0		-	-		0	-					0	
4:15 AM 4:30 AM					0					0					0						0	
4:45 AM Hourly Total	0	0	0	0	0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	
5:00 AM					0					0					0						0	
5:30 AM					0					0					0						0	
5:45 AM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	
6:00 AM					0			0		0				Ŭ	0	-					0	
6:15 AM 6:30 AM					0					0					0						0	
6:45 AM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0	0	
7:00 AM	1	40	0		41	4	3	2		9	1	102	14		117	2	1	3			6	
7:30 AM	э 8	60	2		70	3	13	1		17	2	125	25		128	6	3	15			24	
7:45 AM Hourly Total	9 23	72 223	5	0	86 0 254	1	8 32	0 3 0	0	9 47	0 3	73 401	30 96	0 0	103 500	21 21	2 7	6 34	0	0	11 52	
8:00 AM	2	44	1		47	1	4	2		7	1	60 57	21		82	1	3	1			5	
8:15 AM 8:30 AM	3	43	0		46	2	3	3		8	1	85	22		108	5	2	1			8	
8:45 AM Hourly Total	5 10	48	1	0	0 204	4	7 18	2 0	0	10 29	1 5	74 276	13 67	0 0	88 348	17	3	7 13	0	0	16 38	
9:00 AM	2	37	1		40	3	7	0		10	3	60 40	13		76	8	1	2			11	
9:30 AM	2	39 43	1		40	1	9 7	0		8	0	49 47	10		57	8	4	6			18	
9:45 AM Hourly Total	6 11	39 158	1	0	<u>46</u> 0 172	10	1 24	1 1 0	0	6 35	7	50 206	13 44	0 0	64 257	6 28	2	2 12	0	0	10 54	
10:00 AM	5	43	0		48	1	5	1		7	1	49	7		57	2	5	6			13	
10:15 AM 10:30 AM	3	46	2		50	1	4	0		4 5	1	47	4		48	6	2	8			16	
10:45 AM Hourly Total	2	37	1 4	0	<u>40</u> 0 188	4	5	3 0	0	23	2	51 190	29	0 0	59 225	17	3	2	0	0 4	10 19	
11:00 AM	5	48	1		54	0	4	1		5	0	43	3		46	3	4	5			12	
11:15 AM 11:30 AM	2	41	2		44 49	3	5	1		9	3	44 39	13		55	7	4 3	6			16	
11:45 AM Hourly Total	4	44	2	0	50 0 197	0 4	3	1 3 0	0	4 21	4	51 177	30	0 0	59 211	10 28	3	25	0	0	20 37	
12:00 PM	5	57	2		64	3	6	0		9	1	36	16		53	8	4	5			17	
12:30 PM	4	32 51	2		57	2	4	2		6	0	47 50	11		61	14	4	6		:	24	
12:45 PM Hourly Total	5 21	51 191	0	0	<u>56</u> 0 217	3	4	0 4 0	0	7 31	2	42	44	0 0	<u>51</u> 222	9	3	9 28	0	0	<u>21</u> 30	
1:00 PM	4	49	1	_	54	0	7	0		7	2	61	9		72	6	4	10			20	
1:30 PM	5	49	2		56	1	3	1		5	0	62	5		67	13	2	6		:	21	
1:45 PM Hourly Total	5 17	47	1 5	0	53 0 214	2	2	2 0	0	3 22	2	57 251	32	0 0	288	9 34	6 14	26	0	0	19 74	
2:00 PM	10	55 72	2		67	1	2	1		4	2	62 58	8		72 71	10 14	8	6			24	
2:30 PM	6	71	0		77	4	4	0		8	1	74	16		91	22	2	11			35	
2:45 PM Hourly Total	10 31	96 294	3	0	0 331	10	1 9	0 1 0	0	3 20	0 5	64 258	42	0 0	71 305	6 52	6 24	6 34	0	0 1	18 10	
3:00 PM 3:15 PM	15 7	99 85	3		117 	1	3	0		4	3	58 81	7		68 	10	6 13	11			27	
3:30 PM	5	90	3		98	1	3	1		5	2	72	12		86	15	10	5			30	
3:45 PM Hourly Total	36	364	15	0	0 415	3	3 14	3 0	0	20	10	299	41	0 0	350	66	40	35	0	0 1	41	
4:00 PM 4:15 PM	4 6	89 138	3 3		96	2 2	6 5	0		8 7	4 2	83 76	9		96 90	30 20	10 13	12 10			52 13	
4:30 PM	8	102	6		116	4	6	1		11	0	100	12		112	13	9	8		:	30 16	
Hourly Total	21	463	13	0	0 497	10	20	2 0	0	32	7	339	43	0 0	389	89	43	39	0	0 1	71	
5:00 PM 5:15 PM	8 6	124 107	4 5		136 118	23	2 7	2		6 13	2 0	96 90	13 9		111 99	18 26	13 16	12 14			13 56	
5:30 PM	8	93 70	2		103	1	4	2		7	3	85 84	14		102	11	9 11	4		;	24	
Hourly Total	25	403	17	0	0 445	10	13	9 0	0	32	6	355	43	0 0	404	65	49	35	0	0 1	49	
6:00 PM 6:15 PM	3	67 64	3		73 68	2	3 5	2		8	1 2	47 74	6		52 82	8	6 4	5			18	
6:30 PM	5	70	3		78	2	1	1		4	4	62	14		80	8	1	5			14	
Hourly Total	13	248	10	0	0 271	7	12	6 0	0	25	8	216	29	0 0	253	27	17	14	0	0	58	
7:00 PM 7:15 PM					0					0					— 0 0						0	
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		S	outhbour	nd Approach			Wes	tbound Approa	ach			Noi	rthbound A	oproach			Ea	astbound	Approach	1		
Start Time	_	_	Sout	nbound	– App		_	Westbound		App		_	Nouthbou	nd	App		_	Eastbo	ound	Ap	n	NOTES:
12·00 AM	Right	Ihru	Left	U-Turn	Peds Total	Right	l hru	Left U-Turr	Peds	Total	Right	l hru	Left U	-Turn Peds	s Total	Right	Thru	Left	U-Turn	Peds Tot	al	
12:15 AM					ő					0										0		It should be noted that if data is copied overtop of the Hourly
12:30 AM 12:45 AM					0					0					0					0		Totals or Approach Totals, that the 'AutoSum' Formula will be
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1:15 AM					0					0	-				0					0		copied from a program that
1:45 AM					<u>0</u>					0				<u> </u>	<u>0</u>					0		performs the calculations for the user.
2:00 AM	0	0	0	0	0 0		0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
2:15 AM 2:30 AM					0 0					0 0					0					0 0		
2:45 AM	0	0	0	0	0		0	0 0		0	0	0	0	0 0	0		0	0	0	0		
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6:30 AM					0					0					0					0		
Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
7:00 AM 7:15 AM	1 0	40 52	1 2		42 54	0	5 9	3		7 14	0 1	104 116	1		105 117	1	1 1	2		23		
7:30 AM 7:45 AM	4	71 82	0 0		75	0	2 3	0		2 6	2	143 74	0		145 	1	2 0	7		10	D	
Hourly Total	13	245	3	0	0 261	2	19	8 0	0	29	6	437	2	0 0	445	4	4	12	0	0 20	D	
8:00 AM 8:15 AM	0	40 55	1		47	2	4	1		7	2	65	0		67	0	2	1		3		
8:30 AM 8:45 AM	6 2	44 53	0		50 55	0	0 1	1		1 3	3	83 79	0		86 82	2	1 0	1		4		
Hourly Total 9:00 AM	9 5	198 39	1	0	0 208	3	11 6	7 0	0	21 7	8	285 65	1	0 0	294	2	3	4	0	0 9		
9:15 AM	2	39	0		41	1	3	0		4	1	50	ŏ _		51	1	0	ŏ _		1		
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Hourly Total 10:00 AM	<u>11</u> 9	166 46	1 0	0	0 178 55	2	13 2	5 0 0	0	20 3	7	219 55	0	0 0	226 58	1	3	1	0	0 6		
10:15 AM	2	52 48	0		54	0	3	0		3	0	49 47	0		49	0	2	0		2		
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11:15 AM 11:30 AM	3 8	41 50	0 0		44 58	0	3 4	0		3 4	1	54 44	0		55 	0	1 1	5		6 5		
11:45 AM	0	40	0	0	40	1	4	2		7	3	56	0	0 0	59	0	4	1	0	5	2	
12:00 PM	5	71	0		76	0	2	1		3	4	41	0	0 0	45	1	2	1	0	4	2	
12:15 PM 12:30 PM	7 2	40 55	0		47 57	1	0 3	2		1 6	1	56 55	0		57 57	0	3 1	4 5		7 6		
12:45 PM Hourly Total	4	56 222	0	0	60 0 240	0	2	3 0	0	2	5	51 203	0	0 0	<u>56</u> 215	1	4	2	0	7	. 1	
1:00 PM	3	49	0		52	1	2	3		6	3	62	0		65	0	2	2		4		
1:15 PM 1:30 PM	9	53	0		62	1	3	3		7	1	70	0		71	0	2	3		5		
1:45 PM Hourly Total	26	206	0	0	0 232	3	5 15	6 0	0	5 24	3 9	56 264	3	0 0	60 276	0	2	2	0	4 0 2'	1	
2:00 PM 2:15 PM	5	65 76	0		70	1	3 1	3		7 4	4	58 77	2		64	1	4	1		6 	3	
2:30 PM	11	79	1		91	1	0	0		1	3	82	2		87	0	1	6		7		
2:45 PM Hourly Total	26	318	1	0	0 345	3	10	6 0	0	7 19	11	285	5	0 0	301	4	13	5 18	0	0 35	5	
3:00 PM 3:15 PM	11 4	121 91	3 0		135 95	0	1 2	3		4 4	7	61 81	1		69 88	4	4 3	5 2		10	3	
3:30 PM	7	92 107	0		99	0	2	1		3	8	67 98	0		75	1	11 4	1		10	3	
Hourly Total	36	411	4	0	0 451	0	10	9 0	0	19	28	307	2	0 0	337	5	22	11	0	0 38	3	
4:00 PM 4:15 PM	5	151	0		156	1	1	1		23	6	95 78	1		85	3	5	1		9		
4:30 PM 4:45 PM	8 3	112 138	0 2		120 143	0	4 5	1		5 7	6 4	105 92	1		112 96	4	5 6	4		10 7	3	
Hourly Total	23	490 130	2	0	0 515	3	11	3 0	0	17	18	370 102	2	0 0	390 108	7	24 9	8	0	0 39	9 1	
5:15 PM	3	115	3		121	2	2	1		5	8	95	1		104	3	4	4		i <sup>-</sup>	1	
5:30 PM 5:45 PM	3	98 89	0		92	1	9 5	0		6	5	86 86	1		93 88	1	6 7	2		9 10	5	
Hourly Total 6:00 PM	23 4	432 71	<u>4</u> 0	0	0 459 75	4	17 5	7 0 0	0	28 5	19 5	371 52	3	0 0	393 57	6	26 2	12 1	0	0 44	4	
6:15 PM	0	67	0		67	1	4	0		5	3	70	0		73	0	6	1		7		
6:45 PM	1	48	2		51	2	4	2		8	8	32	0		40	1	3	2		6		
Hourly Total 7:00 PM		260	4	0	0 2/1	3	16	6 0	0	25 0	16	219	0	0 0	235		12	6	0	0 28		
7:15 PM 7:30 PM					0 0					0 0					0					0 0		
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10:45 PM Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0		
11:00 PM 11:15 PM					0					0 0					0					0		
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Hourly Total	0	0	0	0	0 0	0	0	0 0	0	0	0	0	0	0 0	0	0	0	0	0	0 0	1	

		So	uthbound	d Approach			We	stbound A	pproach			No	thbound App	proach			Ea	stbound A	pproach			
Start Time	Right	Thru	Left	U-Turn	Peds App Tota	Right	Thru	Left l	U-Turn Peds	App Total	Right	Thru	Left U-T	urn Peds	App Total	Right	Thru	Left L	J-Turn F	Peds App		NOTES:
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12:30 AM 12:45 AM					0 0															0 0		Totals or Approach Totals, that
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7:15 AM 7:30 AM	5 8	48 60	3 2		56 70	4	17 15	3		24 19	0 2	101 125	27 25		128 152	10 6	1 3	13 24		24		
7:45 AM Hourly Total	9 23	69 215	5 11	0	83 0 249	1	11 51	3	0 0	15 74	0	72 399	31 98 (	0	103 500	3 21	2 7	9 50	0	14 0 78		
8:00 AM 8:15 AM	2 0	40 55	1 2		43 57	1 0	10 8	6 1		17 9	1 2	59 57	22 11		82 70	1 5	3 0	4 5		8 10		
8:30 AM 8:45 AM	3 5	42 47	0 1		45 53	2	3 8	4 3		9 12	1 1	85 74	22 13		108 88	5 6	2 3	3 8		10 17		
Hourly Total 9:00 AM	10 2	184 36	4	0	0 198 39	4	29 13	14 1 _	0 0	47	5	275 60	68 ( 13	0	<u>348</u> 76	17 8	8	20 3	0	0 45		
9:15 AM 9:30 AM	1 2	39 40	0 2		40	2	12 9	0 3		14 13	3 0	49 47	8		60 57	6 8	7 4	2 7		15		
9:45 AM Hourly Total	6 11	38 153	1	0	45 0 168	4	3 37	2 6	0 0	9 53	1 7	50 206	13 44 (	0	64 257	6 28	2 14	5 17	0	13 0 59		
10:00 AM 10:15 AM	5 2	43 46	0 2		48 50	1	7 5	1		9 7	1 2	48 47	8		57 61	2 4	5 3	10 5		17 12		
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11:15 AM 11:30 AM	1 2	41 47	2 0		44 49	1	5 9	0		6 13	0 3	44 39	7 13		51 55	8 7	4 3	13 9		25 19		
11:45 AM Hourly Total	4	42 177	2 7	0	48 0 196	0	7 30	3 6	0 0	10 40	1 4	51 176	7 31 (	0	59 211	10 28	3 14	12 43	0	25 0 85		
12:00 PM 12:15 PM	5 7	56 32	2 1		63 40	3	8 4	1 _		12 9	1 0	36 47	16 10		53 57	8 7	4 3	8 15		20 25		
12:30 PM 12:45 PM	4 5	49 51	2 0		55 56	2	5	4 0		- 11 - 9	0 2	50 42	11 7		61 51	14 9	4	12 15		30		
Hourly Total 1:00 PM	21 4	188 46	5	0	0 214	0	23 9	3	0 0	41	2	175 61	9	0	222	38 6	14 4	50 14	0	0 102		
1:15 PM 1:30 PM	3	47 46	1		51	1	11 6	4		12	1	69 62	5		78 67	6 13	2	14		22 26		
1:45 PM Hourly Total	5 17	47	1	0	0 208	2	33	8	0 0	43	5	248	13 35 (	0	288	34	6 14	8 47	0	0 95		
2:00 PM 2:15 PM	10 5	52 70	2		76	3	3	2		8	2	60 57	10		71	10	8	23		45		
2:30 PM 2:45 PM	6 10	95	3		/8 	4	4 7	1		- 8 10	1	72 64	18		91 71	22 6	2 6	18		42 25		
Houriy Total 3:00 PM	31 15	96	6	U	0 326	10	4	3	0 0	8	3	57	4/ ( 8	0	68	10	6	20	0	<u> </u>		
3:15 PM 3:30 PM	5	89 87	2		92 97	1	5	2		11 8	2	81 72	13		96 86	18	13	11 17 20		42		
3:45 PM Hourly Total	36	355	0 19 2	0	0 410	3	24	12	0 0	39	10	87 297	43 (	0	350	66 20	40	20 68	0	0 174		
4:00 PM 4:15 PM	6	137	3		146	2	6	1		9	2	75	13		90	20	13	16		49		
4:30 PM 4:45 PM	3	133	3	0	115	4 2 10	8	2	0 0	12	1	80 337	10	0	91	26	11 43	16	0	39 53 202		
5:00 PM	8	120	4	0	132	2	3	6 _	0 0	- 11 - 16	2	95 89	14	. 0		18	13	26	0	57		
5:30 PM	8	91 79	3		102	1	13	4		- 18 - 11	3	85	14		102	11	9	11		31		
Hourly Total 6:00 PM	25 3	396 67	21	0	0 442	10	<u>30</u>	16 2	0 0	56	6	352 47	46 (	0	404	65 7	<u>49</u> 6	73	0	0 187		
6:15 PM	2	64 66	2		68	1	9	2		12	2	74 62	6		82	8	4	8		20		
6:45 PM	3	45	4	0	52 	2	7	3	0 0	<u>12</u>	1	33	5	. 0	- 39 253	4	6	8	0	18		
7:00 PM 7:15 PM					0		20			- 0 0		210	20 (		- 0					0		
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## **Multi-Way Stop Application**

#### OMUTCD Section 2B.07

- A. Where traffic control signals are justified, the multi-way stop is an interim measure that can Warranted? be installed quickly to control traffic while arrangements are being made for the installation of the traffic control signal.
- B. Five or more reported crashes in a 12-month period that are susceptible to correction by a multiway stop installation. Such crashes include right-turn and left-turn collisions as well as right-angle collisions.
- C. Minimum Volumes:
  - 1 The vehicular volume entering the intersection from the major street approaches (total of both approaches) averages at least 300 vehicles per hour for any 8 hours of an average day.
  - 2 The combined vehicular, pedestrian, and bicycle volume entering the intersection from the minor street approaches (total of both approaches) averages at least 200 units per hour for the same 8 hours, with an average delay to minor-street vehicular traffic of at least 30 seconds per vehicle during the highest hour.\*

\*If this condition is satisfied, there must also be an average delay of at least 30 seconds per vehicle during the peak hour.

- 3 If the 85th-percentile approach speed of the major-street traffic exceeds 40 mph, the minimum volume warrants are 70 percent of the values provided in Items 1 and 2.
- D. Where no single criterion is satisfied, but where Criteria B, C.1, and C.2 are all satisfied to 80 percent of the minimum values. Criterion C.3 is excluded from this condition.

Other criteria that may be considered in an engineering study include:

- A. The need to control left-turn conflicts;
- B. The need to control vehicle/pedestrian conflicts near locations that generate high pedestrian volumes;
- C. Locations where a road user, after stopping, cannot see conflicting traffic and is not able to negotiate the intersection unless conflicting cross traffic is also required to stop; and
- D. An intersection of two residential neighborhood collector (through) streets of similar design and operating characteristics where multi-way stop control would improve traffic operational characteristics of the intersection.

Are the requirements for Multi-Way Stop Satisfied?: Yes No

Yes

Yes

No

Yes

No

No

No

No

No

AUTOCALC table								
Lanos				Juany chec	ked and taili T	ea il met	1	
Major/	VOLU	JMES	Condit	tion C.1	Condi	tion C.2	Condi	ition D
Minor	MAJOR	MINOR	10	00%	7	0%	80	)%
			MAJ.	MIN.	MAJ.	MIN.	MAJ.	MIN.
Re	equired Volu	imes	300	200	210	140	240	160
6:00 AM	0	0						
6:15 AM	157	16						
6:30 AM	341	39	1		1		1	
6:45 AM	563	61						
7:00 AM	749	74						
7:15 AM	717	75						
7:30 AM	660	62	1		1		1	
7:45 AM	591	50						
8:00 AM	546	47						
8:15 AM	536	46						
8:30 AM	509	51	1		1		1	
8:45 AM	457	55						
9:00 AM	425	51						
9:15 AM	415	60						
9:30 AM	426	57	1		1		1	
9:45 AM	420	61						
10:00 AM	407	58						
10:15 AM	403	57						
10:30 AM	387	69	1		1		1	
10:45 AM	396	66						
11:00 AM	407	80						
11:15 AM	422	76						
11:30 AM	424	77	1		1		1	
11:45 AM	436	85						
12:00 PM	436	87						
12:15 PM	443	99						
12:30 PM	475	96	1		1		1	
12:45 PM	479	93						
1:00 PM	496	82						
1:15 PM	509	85						
1:30 PM	527	105	1		1		1	
1:45 PM	576	117						
2:00 PM	631	121						
2:15 PM	680	128						
2:30 PM	721	123	1		1		1	
2:45 PM	735	136						
3:00 PM	760	148						
3:15 PM	767	166						
3:30 PM	815	177	1		1	1	1	1
3:45 PM	859	174						
4:00 PM	885	172						
4:15 PM	936	175						
4:30 PM	919	184	1		1	1	1	1
4:45 PM	896	177						
5:00 PM	846	178						
5:15 PM	728	130						
5:30 PM	659	100	1		1		1	

5:45 PM	611	80						
6:00 PM	522	66						
6:15 PM	397	47						
6:30 PM	247	33			1		1	
6:45 PM	91	18						
7:00 PM	0	0						
7:15 PM	0	0						
7:30 PM	0	0						
7:45 PM	0	0						
8:00 PM	0	0						
8:15 PM	0	0						
8:30 PM	0	0						
8:45 PM	0	0						
9:00 PM	0	0						
9:15 PM	0	0						
9:30 PM	0	0						
9:45 PM	0	0						
10:00 PM	0	0						
10:15 PM	0	0						
10:30 PM	0	0						
10:45 PM	0	0						
11:00 PM	0	0						
11:15 PM	0	0						
11:30 PM	0	0						
11:45 PM	0	0						
HOURS	MET		12	0	13	2	13	2
CONDIT	ION SATIS	FIED?	N	0	N	0	N	0





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
	Cycles Per Hour	60	Assume 60	
Ť	Turn Lane Volume	10	VPH	
ä	Advancing Traffic	580	VPH	
പ്	Opposing Volume	340	VPH	
_	Left Turn Percentage	2%		
2	Location Type	Through Road		
	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Offset Width	12		includes 50 ft diverging
	Approach Taper	600		taper
	Design Speed	50	mph	
	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
	Cycles Per Hour	60	Assume 60	
- <del>- </del>	Turn Lane Volume	10	VPH	
	Advancing Traffic	530	VPH	
õ	Opposing Volume	710	VPH	
	Left Turn Percentage	2%		
>	Location Type	Through Road		
Ы	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Offset Width	12		includes 50 ft diverging
	Approach Taper	600		taper
ls Left Turn Warrant Met		Yes	See Above	





	Design Speed	50	mph	
×	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
g	Cycles Per Hour	60	Assume 60	
e O	Turn Lane Volume	10	VPH	
Δ.	Advancing Traffic	580	VPH	
V	Right Turn Percentage	2%		
4	Location Type	Through Road		
$\triangleleft$	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Design Speed	50	mph	includes 50 ft diverging
	Traffic Control	Unsignalized		taper
×	Cycle Length	Unsignalized		
а	Cycles Per Hour	60	Assume 60	
G	Turn Lane Volume	30	VPH	
<b>d</b>	Advancing Traffic	530	VPH	
V	Right Turn Percentage	6%		
РЛ	Location Type	Through Road		
	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
le Pight Turn Warrant Mat		No	No Right Turn Lane	includes 50 ft diverging
is Right Turn Warrant Met		NO	Required	taper





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
×	Cycle Length	Unsignalized		
g	Cycles Per Hour	60	Assume 60	
e O	Turn Lane Volume	20	VPH	
<b>D</b>	Advancing Traffic	600	VPH	
7	Right Turn Percentage	3%		
4	Location Type	Through Road		
$\triangleleft$	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Design Speed	50	mph	includes 50 ft diverging
	Traffic Control	Unsignalized		taper
×	Cycle Length	Unsignalized		
В	Cycles Per Hour	60	Assume 60	
e	Turn Lane Volume	70	VPH	
<b>d</b>	Advancing Traffic	580	VPH	
V	Right Turn Percentage	12%		
РЛ	Location Type	Through Road		
	Condition	B or C		
	Vehicles/Cycle	2		
	Turn Lane Length	See Column to Right	245	* Turn Lane Length
Is Right Turn Warrant Met		Yes	See Above	includes 50 ft diverging taper





	Design Speed	35	mph	
	Traffic Control	Unsignalized		
×	Cycle Length	Unsignalized		
g	Cycles Per Hour	60	Assume 60	
e O	Turn Lane Volume	20	VPH	
Δ.	Advancing Traffic	600	VPH	
V	Right Turn Percentage	3%		
4	Location Type	Through Road		
$\triangleleft$	Condition	А		
	Vehicles/Cycle	1		
	Turn Lane Length	100		* Turn Lane Length
	Design Speed	35	mph	includes 50 ft diverging
	Traffic Control	Unsignalized		taper
×	Cycle Length	Unsignalized		
а	Cycles Per Hour	60	Assume 60	
G	Turn Lane Volume	70	VPH	
<b>d</b>	Advancing Traffic	580	VPH	
V	Right Turn Percentage	12%		
ΡV	Location Type	Through Road		
	Condition	А		
	Vehicles/Cycle	2		
	Turn Lane Length	150		* Turn Lane Length
Is Right Turn Warrant Met		Yes	See Above	includes 50 ft diverging taper





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
	Cycles Per Hour	60	Assume 60	
Ť	Turn Lane Volume	10	VPH	
ä	Advancing Traffic	340	VPH	
പ്	Opposing Volume	580	VPH	
	Left Turn Percentage	3%		
2	Location Type	Through Road		
	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Offset Width	12		includes 50 ft diverging
	Approach Taper	600		taper
	Design Speed	50	mph	
	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
	Cycles Per Hour	60	Assume 60	
Ť	Turn Lane Volume	10	VPH	
	Advancing Traffic	710	VPH	
ď	Opposing Volume	530	VPH	
	Left Turn Percentage	1%		
2	Location Type	Through Road		
Ы	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Offset Width	12		includes 50 ft diverging
	Approach Taper	600		taper
Is Left Turn Warrant Met		Yes	See Above	





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
$\mathbf{X}$	Cycle Length	Unsignalized		
a	Cycles Per Hour	60	Assume 60	
e	Turn Lane Volume	20	VPH	
<b>D</b>	Advancing Traffic	340	VPH	
V	Right Turn Percentage	6%		
4	Location Type	Through Road		
4	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Design Speed	50	mph	includes 50 ft diverging
	Traffic Control	Unsignalized		taper
×	Cycle Length	Unsignalized		
g	Cycles Per Hour	60	Assume 60	
G	Turn Lane Volume	30	VPH	
<b>d</b>	Advancing Traffic	710	VPH	
V	Right Turn Percentage	4%		
РΛ	Location Type	Through Road		
	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
Is Right Turn Warrant Met		Yes	See Above	includes 50 ft diverging taper





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
$\mathbf{X}$	Cycle Length	Unsignalized		
<b>D</b>	Cycles Per Hour	60	Assume 60	
e O	Turn Lane Volume	20	VPH	
Δ.	Advancing Traffic	340	VPH	
7	Right Turn Percentage	6%		
4	Location Type	Through Road		
A	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Design Speed	50	mph	includes 50 ft diverging
	Traffic Control	Unsignalized		taper
$\mathbf{X}$	Cycle Length	Unsignalized		
σ	Cycles Per Hour	60	Assume 60	
G	Turn Lane Volume	30	VPH	
<b>D</b>	Advancing Traffic	710	VPH	
V	Right Turn Percentage	4%		
	Location Type	Through Road		
<b>D</b>	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
Is Right Turn Warrant Met		Yes	See Above	includes 50 ft diverging taper





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
	Cycles Per Hour	60	Assume 60	
Ť	Turn Lane Volume	120	VPH	
ä	Advancing Traffic	630	VPH	
ď	Opposing Volume	330	VPH	
_	Left Turn Percentage	19%		
2	Location Type	Through Road		
	Condition	B or C		
	Vehicles/Cycle	2		
	Turn Lane Length	See Column to Right	245	* Turn Lane Length
	Offset Width	12		includes 50 ft diverging
	Approach Taper	600		taper
	Design Speed	50	mph	
	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
	Cycles Per Hour	60	Assume 60	
Ť	Turn Lane Volume	60	VPH	
	Advancing Traffic	510	VPH	
ď	Opposing Volume	690	VPH	
_	Left Turn Percentage	12%		
PM	Location Type	Through Road		
	Condition	B or C		
	Vehicles/Cycle	1		
	Turn Lane Length	See Column to Right	225	* Turn Lane Length
	Offset Width	12		includes 50 ft diverging
	Approach Taper	600		taper
ls Left Turn Warrant Met		Yes	See Above	





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
×	Cycle Length	Unsignalized		
g	Cycles Per Hour	60	Assume 60	
e O	Turn Lane Volume	10	VPH	
Δ.	Advancing Traffic	630	VPH	
V	Right Turn Percentage	2%		
4	Location Type	Through Road		
$\triangleleft$	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Design Speed	50	mph	includes 50 ft diverging
	Traffic Control	Unsignalized		taper
×	Cycle Length	Unsignalized		
а	Cycles Per Hour	60	Assume 60	
G	Turn Lane Volume	10	VPH	
<b>d</b>	Advancing Traffic	510	VPH	
V	Right Turn Percentage	2%		
PN	Location Type	Through Road		
	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
Is Pight Turn Warrant Mat		No	No Right Turn Lane	includes 50 ft diverging
is Right Turn Warrant Met		NO	Required	taper





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
	Cycles Per Hour	60	Assume 60	
Ť	Turn Lane Volume	10	VPH	
ä	Advancing Traffic	330	VPH	
പ്	Opposing Volume	630	VPH	
=	Left Turn Percentage	3%		
2	Location Type	Through Road		
⊿	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Offset Width	12		includes 50 ft diverging
	Approach Taper	600		taper
	Design Speed	50	mph	
	Traffic Control	Unsignalized		
	Cycle Length	Unsignalized		
	Cycles Per Hour	60	Assume 60	
	Turn Lane Volume	20	VPH	
	Advancing Traffic	690	VPH	
õ	Opposing Volume	510	VPH	
	Left Turn Percentage	3%		
>	Location Type	Through Road		
Ы	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Offset Width	12		includes 50 ft diverging
	Approach Taper	600		taper
ls Left Turn Warrant Met		Yes	See Above	





	Design Speed	50	mph	
	Traffic Control	Unsignalized		
×	Cycle Length	Unsignalized		
g	Cycles Per Hour	60	Assume 60	
e O	Turn Lane Volume	30	VPH	
Δ.	Advancing Traffic	330	VPH	
7	Right Turn Percentage	9%		
4	Location Type	Through Road		
$\triangleleft$	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
	Design Speed	50	mph	includes 50 ft diverging
	Traffic Control	Unsignalized		taper
×	Cycle Length	Unsignalized		
а	Cycles Per Hour	60	Assume 60	
G	Turn Lane Volume	30	VPH	
<b>d</b>	Advancing Traffic	690	VPH	
V	Right Turn Percentage	4%		
	Location Type	Through Road		
<b>D</b>	Condition	В		
	Vehicles/Cycle	1		
	Turn Lane Length	225		* Turn Lane Length
Is Right	Turn Warrant Met	Yes	See Above	includes 50 ft diverging taper

# Appendix G Proposed Capacity Analysis



## **Capacity Analysis for Planning of Junctions**

Summary Report

Project Name:	POR-SR-43 at Trares and Randolph Road Safety Study
Project Number:	0
Location:	SR-43 & Trares Road
Date:	2047 PM
Number of Intersection Legs:	4
Major Street Direction	North-South

				Tra	ffic Volume D	emand			
				Volume	(Veh/hr)			Perce	ent (%)
	U-T	urn	Le	əft	Thru	Right			
			<b>+</b>	]		ſ	Heavy \	/ehicles	Volume Growth
Eastbound	(	)	1:	30	80	130	1.0	0%	0.00%
Westbound	(	)	2	0	50	20	3.0	0%	0.00%
Southbound	(	)	3	0	630	30	2.0	0%	0.00%
Northbound	(	)	7	0	430	10	3.0	0%	0.00%
Adjustment Factor	0.	80	0.	95	$\sim$	0.85			
Suggested	0.	80	0.	95		0.85		$\sim$	
		Truck to	PCE Fa	ctor		Suggested =	2.00		2.00
Multin	nodal Ac	tivity Lev	el			0			
E-W / Cro	ssing Ea	ast-West	Legs		Low	Low			Low
N-S / Cros	sing No	rth-South	n Legs		Low	Low			Low
		2-phas	e signal	Sug	gested = 1800 (	Urban), 1650 (Ru	ıral)		1620
Critical L Volume Th	ane reshold	3-phas	e signal	Sug	gested = 1750 (	Urban), 1600 (Ru	iral)		1600
		4-phas	e signal	Sug	ggested = 1700 (	Urban), 1550 (Ru	ıral)		1550

## **Capacity Analysis for Planning of Junctions**

Summary Report

				#############
TYPE OF INTERSECTION	Overall v/c Ratio	V/C Ranking	Pedestrian Accommodations	Bicycle Accommodations
1 X 1 Roundabout	0.60	1	5.36	4.75
All-Way Stop Control	1.44	2	4.12	4.79
Two-Way Stop Control N-S	2.37	3	2.94	4.08

					HC	S Rou	nda	bou	uts R	ер	ort								
General Information				_				Sit	e Info	orn	natio	n			_				
Analyst	VHD				_		4				Inters	ection			SF	R-43 at	Rand	lolph R	 ≀d
Agency or Co.	Lanha	m Engir	neering	g, LLC	С			÷			E/W S	Street Na	ame		Rá	andolp	h Rd		
Date Performed										¢	N/S S	itreet Na	me		SF	R-43			
Analysis Year	2027					<b>\</b>	W	↑ F S	) î		Analy	rsis Time	Period, ł	rs	0.	25			
Time Analyzed	OY AN	Л				Ť.					Peak	Hour Fa	ctor		0.	81			
Project Description	SR-43	Alt 1						→ ▼ *	1		Jurisd	liction			0	DOT D	istrict	4	
Volume Adjustments	and S	ite Cł	nara	cter	ristic	s													
Approach		E	EB				V	NB				٦	IB		Γ		S	В	
Movement	U	L	Т	Т	R	U	L	Т	F	ł	U	L	Т	R	ι	J	L	Т	R
Number of Lanes (N)	0	0	1	T	0	0	0	1	C	)	0	0	1	0	C	)	0	1	0
Lane Assignment				LTR					LTR				LT	R	$\square$				LTR
Volume (V), veh/h	0	10	10	Т	10	0	10	20	) 1	C	0	10	520	10	C	)	10	300	20
Percent Heavy Vehicles, %	0	5	5	+	5	0	7	7	7	,	0	5	5	5	C	)	4	4	4
Flow Rate (VPCE), pc/h	0	13	13		13	0	13	26	5 1	3	0	13	674	13	C	)	13	385	26
Right-Turn Bypass		No	one				N	one				N	one				Nc	one	
Conflicting Lanes			1					1					1					1	
Pedestrians Crossing, p/h			0					0					0				(	)	
Proportion of CAVs, %										(	)								
Critical and Follow-U	p Hea	dway	Adj	ust	men	t													
Approach		E	EB	_			V	NB	_			1	IB		Γ		S	В	
Lane	Left	Ri	ght	By	pass	Left	Ri	ight	Вура	ss	Left	Ri	ght E	ypass	L	_eft	Rig	ght	Bypass
Critical Headway, s		4.9	763				4.9	9763				4.9	763				4.9	763	
Follow-Up Headway, s		2.6	6087				2.6	5087				2.6	087				2.6	087	
Flow Computations, (	Capaci	ity an	d v/	c R	atios	5									-				
Approach	•	• E	EB		_		V	NB				1	IB		<u> </u>		S	В	
Lane	Left	Ri	aht	By	pass	Left	Ri	ight	Вура	ss	Left	Ri	aht E	vpass		_eft	Ric	aht	Bypass
Entry Flow (v₀), pc/h		3	39					52				7	00		1		42	24	
Entry Volume, veh/h		3	37					49				6	67				4(	08	
Circulating Flow (v <sub>c</sub> ), pc/h		4	11				7	700				:	39				5	2	
Exiting Flow (vex), pc/h		Э	39				(	65				7	00				4	11	
Capacity (cpce), pc/h		9	07				6	576				13	326				13	09	
Capacity (c), veh/h		8	64				6	32				12	263				12	58	
v/c Ratio (x)		0.	.04				0	.08				0.	53				0.	32	
Delay and Level of Se	rvice						1		<u> </u>										
Approach			_		EB		Т	_	WB				NB	_		_	_	SB	
Lane			Left	t	Right	Bypas	5 L	.eft	Right	1	Bypass	Left	Right	Вур	ass	Left	F	Right	Bypass
Lane Control Delay (d), s/veh					4.6				6.6	T			8.6					5.8	
Lane LOS					А				А				А					А	
95% Queue Length, Q <sub>95</sub> (veh)					0.1				0.2	T			3.2					1.4	
95% Queue Length, Q <sub>95</sub> (ft)					2.6				5.3				83.2					36.1	
Approach Delay, s/veh   LOS			4	1.6		A		6.6			A	8.6	5	A		5	5.8		A
Intersection Delay, s/veh   LOS							<b>G3</b> 7.4	ot 28	- 1						A	۱			

					HC	S Rou	nda	boı	uts Re	ep	ort								
General Information				_				Sit	e Info	rn	natio	n			_				
Analyst	VHD						*				Inters	ection			S	R-43 a	t Rand	dolph F	 ≀d
Agency or Co.	Lanha	m Engir	neering	g, LLC	С			⊢ `		ľ	E/W S	Street Na	ame		R	andolp	oh Rd		
Date Performed										÷	N/S S	itreet Na	me		S	R-43			
Analysis Year	2027					<b>  ↓</b>	W	Ω Ω E S	†		Analy	rsis Time	Period, I	nrs	0	.25			
Time Analyzed	OY PN	Л				<b>*</b>					Peak	Hour Fa	ctor		0.	.96			
Project Description	SR-43	Alt 1						→ ▼ *	1	ľ	Jurisd	liction			С	DOT E	District	: 4	
Volume Adjustments	and S	ite Cł	nara	cter	ristic	S													
Approach		E	EB				V	VB		Τ		1	١B		Г		S	БВ	
Movement	U	L	Т	Т	R	U	L	Т	R		U	L	Т	R	L I	J	L	Т	R
Number of Lanes (N)	0	0	1	T	0	0	0	1	0	T	0	0	1	0	(	0	0	1	0
Lane Assignment				LTR					LTR				Ľ	R					LTR
Volume (V), veh/h	0	10	30	Т	10	0	10	10	10	,	0	10	450	30	(	0	10	640	30
Percent Heavy Vehicles, %	0	0	0		0	0	5	5	5		0	3	3	3	(	0	2	2	2
Flow Rate (VPCE), pc/h	0	10	31		10	0	11	11	11		0	11	483	32	(	0	11	680	32
Right-Turn Bypass		No	one				No	one				N	one				No	one	_
Conflicting Lanes			1					1					1					1	
Pedestrians Crossing, p/h			0					0					0					0	
Proportion of CAVs, %										0	)								
Critical and Follow-U	p Hea	dway	Adj	ust	men	t													
Approach		-	EB				v	VB	_	Т		1	١B		Τ		S	БB	
Lane	Left	Ri	ght	By	pass	Left	Ri	ght	Bypas	s	Left	Ri	ght l	Sypass		Left	Ri	ght	Bypass
Critical Headway, s		4.9	763				4.9	763				4.9	763				4.9	763	
Follow-Up Headway, s		2.6	6087				2.6	087				2.6	087				2.6	087	
Flow Computations,	Capaci	ity an	d v/	c Ra	atios	5											· · ·		
Approach	•		EB				v	VB		Т		1	1B		Т			B	
Lane	Left	Ri	aht	Byr	pass	Left	Ri	aht	Bypas	s	Left	Ri	ght I	Sypass		Left	Ri	ght	Bypass
Entry Flow (v₀), pc/h			51				3	33				5	26				7	23	
Entry Volume, veh/h			51				3	31				5	11				7	09	
Circulating Flow (v <sub>c</sub> ), pc/h		7	02				5	04					52				3	3	
Exiting Flow (vex), pc/h		-	74				5	54				5	04				7	01	
Capacity (cpce), pc/h		6	74				8	25				13	309				13	34	
Capacity (c), veh/h		6	74				7	86				12	271				13	808	
v/c Ratio (x)		0.	.08		_		0.	.04				0	40				0.	54	
Delay and Level of Se	rvice						1		1				1					1	
Approach				-	EB		Т		WB				NB					SB	
Lane			Left	t	Right	Bypass	; L	eft	Right	E	Bypass	Left	Righ	Вур	bass	Lef	t	Right	Bypass
Lane Control Delay (d), s/veh					6.2		T		5.0	T			6.7				1	8.7	
Lane LOS				+	А				А	t			А				+	А	
95% Queue Length, Q <sub>95</sub> (veh)					0.2		T		0.1	t			2.0					3.4	
95% Queue Length, Q <sub>95</sub> (ft)				+	5.0				2.6	t			51.2				+	86.4	
Approach Delay, s/veh   LOS			e	5.2		A	<u>.</u>	5.0		4	A	6.	7	A		8	3.7		A
Intersection Delay, s/veh   LOS					_			ot 28					I		F	4			

					HC	S Rou	nda	bοι	uts Re	por	t								
General Information								Site	e Info	rmat	tion	1			_				
Analyst	VHD						4			In	nterse	ection			SR	R-43 at	Rando	olph R	
Agency or Co.	Lanha	m Engir	neering	g, LLC			•	- `		E/	/W St	treet Na	ime		Ra	andolpl	h Rd		
Date Performed						$\square$				> N	I/S St	reet Na	me		SR	R-43			
Analysis Year	2047					<b>∢</b> ↓ (	w	Ω † E S	) † >	A	nalys	sis Time	Period, h	rs	0.2	25			
Time Analyzed	DY AN	Л				<b>₹</b>				Pe	eak ⊦	lour Fac	tor		0.8	81			
Project Description	SR-43	Alt 1						→ ▼ *		Ju	urisdi	ction			0	DOT Di	istrict ·	4	
Volume Adjustments	and S	ite Cł	nara	cteri	istic	s													
Approach		E	B				W	/B		Т		N	IB				SE	3	
Movement	U	L	Т		R	U	L	Т	R	ι	U	L	Т	R	U	J	L	Т	R
Number of Lanes (N)	0	0	1		0	0	0	1	0	(	0	0	1	0	0		0	1	0
Lane Assignment				LTR					LTR				LT	R		_			LTR
Volume (V), veh/h	0	20	10	· ·	10	0	10	30	10	(	0	10	560	10	0		10	310	20
Percent Heavy Vehicles, %	0	5	5		5	0	7	7	7	(	0	5	5	5	0	,	4	4	4
Flow Rate (VPCE), pc/h	0	26	13	-	13	0	13	40	13	(	0	13	726	13	0	,	13	398	26
Right-Turn Bypass		No	one				Nc	one				Nc	one				No	ne	
Conflicting Lanes			1					1					1				1		
Pedestrians Crossing, p/h			0				(	0				(	)				0		
Proportion of CAVs, %										0									
Critical and Follow-U	p Hea	dway	Adj	ustn	nen	t													
Approach		-	EB				W	/B	_	Т		N	IB				SE	3	
Lane	Left	Ri	ght	Вура	ass	Left	Rig	ght	Bypass	1	Left	Rig	ght B	ypass	L	.eft	Rig	ht	Bypass
Critical Headway, s		4.9	763				4.9	763		+-		4.9	763				4.97	63	
Follow-Up Headway, s		2.6	087				2.6	087		+		2.6	087				2.60	87	
Flow Computations, (	Capaci	ity an	d v/	c Ra	tios	;				_		_							
Approach	•		B				W	/B		Т		N	IB				SE	3	
Lane	Left	Ri	ght	Вура	ass	Left	Ric	aht	Bypass		Left	Ric	aht B	vpass	L	.eft	Riq	ht	Bypass
Entry Flow (v₀), pc/h			52				6	6		1		7	52			_	43	7	
Entry Volume, veh/h			50				6	2		+		7	16				42	0	
Circulating Flow (v <sub>c</sub> ), pc/h		4	24				76	65				5	2				66	5	
Exiting Flow (vex), pc/h		3	39				7	'9		+		70	65				42	4	
Capacity (cpce), pc/h		8	95				63	32		+		13	09				129	90	
Capacity (c), veh/h		8	53				59	91		+		12	46				124	41	
v/c Ratio (x)		0.	.06				0.	10		+-		0.	57				0.3	4	
Delay and Level of Se	rvice			<u> </u>						-		1					<u> </u>	1	
Approach			_	_	EB			_	WB	_	Т		NB		Т	_	_	SB	
Lane			Left	F	Right	Bypass	Le	eft	Right	Вура	ass	Left	Right	Вур	ass	Left	R	ight	Bypass
Lane Control Delay (d), s/veh					4.8				7.3				9.6					6.1	
Lane LOS					А				А		+		А					А	
95% Queue Length, Q <sub>95</sub> (veh)					0.2				0.3				3.8					1.5	
95% Queue Length, Q <sub>95</sub> (ft)					5.2				7.9				98.8				3	38.7	
Approach Delay, s/veh   LOS			4	1.8	Τ	A	6-	7.3		A		9.6		A		6	.1	Γ	A
Intersection Delay, s/veh   LOS							<b>G5 c</b> 8.1	ot 28							A				

					HC	S Roui	ndal	bou	its Re	port									
General Information								Site	e Infor	mati	on				_				
Analyst	VHD						*			Int	erse	ction			SR	k-43 at	Rand	olph R	d
Agency or Co.	Lanha	m Engir	neering	g, LLC			•	- `		E/\	N Sti	reet Na	me		Ra	indolp	h Rd		
Date Performed										N/	S Str	reet Na	me		SR	k-43			
Analysis Year	2047					<b>∢</b> ↓	w 4	E	) ↑ >	An	alysi	is Time	Period, h	rs	0.2	25			
Time Analyzed	DY PN	1				÷				Pe	ak H	our Fac	tor		0.9	96			
Project Description	SR-43	Alt 1					_	+   *		Jui	risdic	ction			O	DOT D	istrict	4	
Volume Adjustments	and S	ite Cł	nara	cteri	istic	S													
Approach		E	B				W	′B		Τ		N	В				S	В	
Movement	U	L	Т	Т	R	U	L	Т	R	U		L	Т	R	U		L	Т	R
Number of Lanes (N)	0	0	1		0	0	0	1	0	0	T	0	1	0	0		0	1	0
Lane Assignment		<u> </u>		LTR					LTR				LT	र		_			LTR
Volume (V), veh/h	0	20	40		10	0	10	20	10	0		10	490	30	0		10	670	30
Percent Heavy Vehicles, %	0	0	0		0	0	5	5	5	0		3	3	3	0		2	2	2
Flow Rate (VPCE), pc/h	0	21	42		10	0	11	22	11	0		11	526	32	0		11	712	32
Right-Turn Bypass		No	one				No	ne				No	ne				No	ne	
Conflicting Lanes			1				1					1	1				1		
Pedestrians Crossing, p/h	Crossing, p/h 0						C	)				(	)				(	)	
Proportion of CAVs, %										0									
<b>Critical and Follow-U</b>	р Неа	dway	Adj	ustr	nen	t													
Approach		E	B				W	'B		1		N	В				S	В	
Lane	Left	Ri	ght	Вур	ass	Left	Rig	jht	Bypass	L	eft	Rig	jht B	ypass	L	eft	Ric	jht	Bypass
Critical Headway, s		4.9	763				4.97	763				4.9	763				4.97	763	
Follow-Up Headway, s		2.6	087				2.60	087				2.60	087				2.60	087	
Flow Computations, (	Capaci	ity an	d v/	c Ra	atios	5													
 Approach	-	E	B				W	′B	_		_	N	В				S	B	
Lane	Left	Ri	ght	Вур	ass	Left	Rig	jht	Bypass	L	eft	Ric	ght B	ypass	L	eft	Ric	jht	Bypass
Entry Flow (ve), pc/h		7	73				4	4				56	59				75	55	
Entry Volume, veh/h		7	73				4	2				55	52				74	40	
Circulating Flow (v <sub>c</sub> ), pc/h		7	34				55	58				7	4				4	4	
Exiting Flow (v <sub>ex</sub> ), pc/h		8	35				6	5				55	58				73	33	
Capacity (cpce), pc/h		6	53				78	31				12	80				13	19	
Capacity (c), veh/h		6	53				74	4				12	42				12	94	
v/c Ratio (x)		0.	.11				0.0	06				0.4	44				0.5	57	
Delay and Level of Se	rvice											1							
Approach			_	_	EB		Γ	_	WB	_	Т		NB	_	Т	_	_	SB	
Lane			Left	:	Right	Bypass	Le	ft	Right	Bypas	s	Left	Right	Вур	ass	Left	F	Right	Bypass
Lane Control Delay (d), s/veh					6.8				5.4		T		7.4					9.3	
Lane LOS					А				А		+		A					А	
95% Queue Length, Q <sub>95</sub> (veh)					0.4				0.2		╈		2.3					3.8	
95% Queue Length, Q <sub>95</sub> (ft)					10.0				5.2		+		58.9					96.5	
Approach Delay, s/veh   LOS			6	5.8		A	<u> </u>	5.4		А	T	7.4		А		9	.3		A
Intersection Delay, s/veh   LOS								×-∠8			╈				A				

					HC	S Roui	ndal	bou	uts Re	рс	ort								
General Information				_				Site	e Info	rma	atior	ı			_		_		
Analyst	VHD						*			Т	Inters	ection			S	R-43 a	t Trare	es Rd	
Agency or Co.	Lanha	ım Engir	neering	g, LLC	С		+	- `		F	E/W S	Street Na	ame		Tr	rares R	d		
Date Performed						$\left[ \right]$				2	N/S S	treet Na	me		S	R-43			
Analysis Year	2027					<b>▼</b> +	w 4	Ē	) † >		Analy	sis Time	Period, h	rs	0.	.25			
Time Analyzed	OY AI	M				Ê.					Peak I	Hour Fa	ctor		0.	.82			
Project Description	SR-43	Alt 1						→ / *			Jurisd	iction			0	DOT E	District	: 4	
Volume Adjustments	and S	ite Cl	nara	ctei	ristic	S													
Approach		E	EB				W	/B		Т		1	1B				S	SB	
Movement	U	L	Т	Τ	R	U	L	Т	R	Ť	U	L	Т	R	l	J	L	Т	R
Number of Lanes (N)	0	0	1	T	0	0	0	1	0	T	0	0	1	0	(	)	0	1	0
Lane Assignment				LTR					LTR	Ť			LT	R					LTR
Volume (V), veh/h	0	40	10	Τ	30	0	10	40	10	T	0	120	490	10	(	D	10	280	30
Percent Heavy Vehicles, %	0	0	0		0	0	0	0	0		0	5	5	5	(	)	5	5	5
Flow Rate (VPCE), pc/h	0	49	12		37	0	12	49	12	T	0	154	627	13	(	)	13	359	38
Right-Turn Bypass		N	one				No	ne		T		N	one				No	one	
Conflicting Lanes			1				1	1		T			1					1	
Pedestrians Crossing, p/h			0				C	)					0					0	
Proportion of CAVs, %										0									
<b>Critical and Follow-U</b>	p Hea	dway	Adj	ust	men	t													
Approach		E	EB				W	/B		Т		٦	IB		Γ		ç	БB	
Lane	Left	Ri	ght	Ву	pass	Left	Rig	ght	Bypass		Left	Ri	ght E	ypass		Left	Ri	ght	Bypass
Critical Headway, s		4.9	763				4.97	763		T		4.9	763				4.9	763	
Follow-Up Headway, s		2.6	6087				2.60	087				2.6	087		$\square$		2.6	087	
Flow Computations,	Capaci	ity an	d v/	c R	atios	5													
Approach		E	EB				W	/B		Т		٦	IB		Γ		S	SB	
Lane	Left	Ri	ght	Ву	pass	Left	Rig	ght	Bypass		Left	Ri	ght E	ypass		Left	Ri	ght	Bypass
Entry Flow (ve), pc/h			98				7	3		T		7	94		1		4	10	
Entry Volume, veh/h		9	98				7	3		$^{+}$		7	56				3	90	
Circulating Flow (v <sub>c</sub> ), pc/h		3	84				83	30		T			74				2	15	
Exiting Flow (vex), pc/h		3	38				24	41				6	88				4	08	
Capacity (dece), pc/h		9	33				59	92		T		12	280				11	08	
Capacity (c), veh/h		9	33				59	92				12	219		$\square$		10	)55	
v/c Ratio (x)		0.	.11				0.1	12		T		0	62				0.	37	
Delay and Level of Se	ervice														1				
Approach					EB		Τ		WB				NB					SB	
Lane			Left	:	Right	Bypass	Le	eft	Right	Ву	ypass	Left	Right	Вур	ass	Lef	t	Right	Bypass
Lane Control Delay (d), s/veh					4.8				7.6				10.8					7.2	
Lane LOS					А				А				В					А	
95% Queue Length, Q <sub>95</sub> (veh)					0.4				0.4				4.5					1.7	
95% Queue Length, Q <sub>95</sub> (ft)					10.0				10.0				117.0					44.2	
Approach Delay, s/veh   LOS			4	1.8		А	67.0	7.6 of 28		А		10.	8	В		-	7.2		А
Intersection Delay, s/veh   LOS	5						9.1	7 20							A	4			

					HC	S Rou	ndal	bou	ıts Re	ро	rt								
General Information								Site	e Info	rma	ation	n			_				
Analyst	VHD						4			1	Interse	ection			SR	R-43 at	Trares	s Rd	
Agency or Co.	Lanha	m Engir	neering	g, LLC			•	- `		E	E/W S	treet Na	ime		Tra	ares Ro	ł		
Date Performed										1	N/S St	treet Na	me		SR	R-43			
Analysis Year	2027					<b>∢</b> ↓	w	₽ ₽ S	) † >	E	Analys	sis Time	Period, h	rs	0.2	25			
Time Analyzed	OY PN	Л				*				F F	Peak H	Hour Fac	tor		0.9	96			
Project Description	SR-43	Alt 1						→ / *∲	1	7	Jurisdi	iction			O	DOT Di	istrict	4	
Volume Adjustments	and S	ite Cł	nara	cteri	istic	S	Distance Careta												
Approach		E	B				W	/B		Т		N	IB				SI	В	
Movement	U	L	Т	Τ	R	U	L	Т	R	+	U	L	Т	R	U		L	Т	R
Number of Lanes (N)	0	0	1		0	0	0	1	0		0	0	1	0	0		0	1	0
Lane Assignment				LTR					LTR				LT	२					LTR
Volume (V), veh/h	0	50	60		90	0	10	20	10		0	60	430	10	0		20	610	30
Percent Heavy Vehicles, %	0	1	1		1	0	3	3	3		0	3	3	3	0		2	2	2
Flow Rate (VPCE), pc/h	0	53	63		95	0	11	21	11		0	64	461	11	0		21	648	32
Right-Turn Bypass		N	one	_			No	one	_			Nc	one			_	No	ne	<u> </u>
Conflicting Lanes			1				1	1					1				1		
Pedestrians Crossing, p/h			0				(	)				(	0				C	)	
Proportion of CAVs, %										0									
Critical and Follow-U	p Hea	dway	Adj	ustr	nen	t													
 Approach	-		EB				W	/B		Т		N	IB				SI	B	
Lane	Left	Ri	ght	Вур	ass	Left	Ric	ght	Bypass		Left	Rio	ght B	ypass	L	eft	Rig	ht	Bypass
Critical Headway, s		4.9	763		_		4.9	763		1		4.9	763			_	4.97	763	
Follow-Up Headway, s		2.6	087				2.60	087		┢		2.6	087				2.60	)87	
Flow Computations, (	Capaci	itv an	d v/	c Ra	itios	;													
Approach			B				W	/B		Т		N	IB				S	3	
Lane	Left	Ri	aht	Bvp	ass	Left	Ric	aht	Bypass	+	Left	Ric	aht B	vpass	L	eft	Rig	ht	Bypass
Entry Flow (ve), pc/h		2	5 11	51	_		4	.3	51	+		53	36	, i			70	)1	
Entry Volume, veh/h		2	09				4	2		+		52	20				68	57	
Circulating Flow (v <sub>c</sub> ), pc/h		6	80		_		57	78		+		13	37				9	6	
Exiting Flow (vex), pc/h		Q	95				11	17		+		52	25				75	4	
Capacity (care), pc/h		6	90				76	65		+		12	.00				12	51	
Capacity (c), veh/h		6	83				74	43		┢		11	65				12	27	
v/c Ratio (x)		0.	.31		_		0.0	06				0.4	45				0.5	56	
Delay and Level of Se	rvice														I				
Approach					EB		Т		WB				NB		Т			SB	
Lane			Left		Right	Bypass	Le	eft	Right	Вур	oass	Left	Right	Вура	ass	Left	R	light	Bypass
Lane Control Delay (d), s/veh					9.1				5.4				7.8					9.4	
Lane LOS					А				А				A					А	
95% Queue Length, Q <sub>95</sub> (veh)					1.3				0.2				2.4					3.6	
95% Queue Length, Q <sub>95</sub> (ft)					32.8			$\neg$	5.1		$\neg$		61.4				9	91.4	
Approach Delay, s/veh   LOS			ç	9.1	Τ	A	6.5	5.4		A		7.8		A		9.	.4	Τ	A
Intersection Delay, s/veh   LOS							<b>G8-c</b> 8.7	ot 28							A				

					HC	S Rou	nda	boı	uts Re	ep	ort								
General Information				_				Sit	e Info	orm	natio	n			_				
Analyst	VHD						*				Inters	ection			S	R-43 a	t Trare	es Rd	
Agency or Co.	Lanha	ım Engir	neering	g, LLC	2			⊢ `		ľ	E/W S	Street Na	ame		Tr	rares R	d		
Date Performed					_					÷	N/S S	treet Na	me		S	R-43			
Analysis Year	2047					<b>  ↓</b>	W	Ω Ω E S	) † }		Analy	sis Time	Period, ł	rs	0.	.25			
Time Analyzed	DY AN	Л				<b>*</b>					Peak	Hour Fa	ctor		0.	.82			
Project Description	SR-43	Alt 1						→ ▼ *	1	ĺ	Jurisd	liction			0	DOT E	Distric	t 4	
Volume Adjustments	and S	ite Cł	nara	cter	ristic	s													
Approach		E	B				V	VB				٦	١B		Γ		9	SB	
Movement	U	L	Т	Т	R	U	L	Т	R		U	L	Т	R	ι	J	L	Т	R
Number of Lanes (N)	0	0	1		0	0	0	1	0		0	0	1	0	(	0	0	1	0
Lane Assignment				LTR					LTR				LT	R	$\square$	_			LTR
Volume (V), veh/h	0	60	10		40	0	10	50	20	,	0	120	500	10	(	0	10	290	30
Percent Heavy Vehicles, %	0	0	0		0	0	0	0	0		0	5	5	5	(	0	5	5	5
Flow Rate (VPCE), pc/h	0	73	12		49	0	12	61	24		0	154	640	13	(	0	13	371	38
Right-Turn Bypass		No	one				No	one				N	one				N	one	
Conflicting Lanes			1					1					1		$\square$			1	
Pedestrians Crossing, p/h			0					0					0		$\square$			0	
Proportion of CAVs, %										0	)								
Critical and Follow-U	p Hea	dway	Adj	usti	men	t													
Approach	-	-	EB				v	VB	_			1	١B		Τ		9	SB	
Lane	Left	Ri	ght	Byp	pass	Left	Ri	ght	Bypas	s	Left	Ri	ght E	ypass		Left	Ri	ght	Bypass
Critical Headway, s		4.9	763				4.9	763				4.9	763				4.9	763	
Follow-Up Headway, s		2.6	087				2.6	087				2.6	087		$\vdash$		2.6	087	
Flow Computations, (	Capaci	ity an	d v/	c Ra	atios	5	1					_					1		
Approach			B				v	VB				1	1B		Г			SB	
Lane	Left	Ri	ght	Byr	pass	Left	Ri	aht	Bypas	s	Left	Ri	aht E	vpass		Left	Ri	aht	Bypass
Entry Flow (v₀), pc/h		1	34				9	97				8	07	-			4	22	
Entry Volume, veh/h		1	34				9	97				7	69				4	02	
Circulating Flow (v <sub>c</sub> ), pc/h		3	96				8	67				9	98				2	27	
Exiting Flow (vex), pc/h		3	38				2	53				7	37		$\vdash$		4	32	
Capacity (cpce), pc/h		9	21				5	70				12	249				1(	)95	
Capacity (c), veh/h		9	21				5	70				1'	189		$\vdash$		1(	)43	
v/c Ratio (x)		0.	.15		_		0.	.17				0.	.65		1		0	.39	
Delay and Level of Se	rvice	_																1	
Approach					EB		Т		WB				NB					SB	
Lane			Left	t	Right	Bypass	; L	eft	Right	E	Bypass	Left	Right	Вур	ass	Lef	t	Right	Bypass
Lane Control Delay (d), s/veh				1	5.3		T		8.5	T			11.6					7.5	
Lane LOS				+	А				А	$\uparrow$			В				+	А	
95% Queue Length, Q <sub>95</sub> (veh)					0.5		T		0.6	T			5.0					1.8	
95% Queue Length, Q <sub>95</sub> (ft)				+	12.5				15.0	$\uparrow$			130.0				+	46.8	
Approach Delay, s/veh   LOS			5	5.3		A		8.5		4	A	11.	6	В			7.5		A
Intersection Delay, s/veh   LOS							9.6	ot 28							A	4			

					HC	S Rou	nda	bou	uts Re	ep	ort								
General Information				_				Sit	e Info	orn	natio	n			_				
Analyst	VHD						*				Inters	ection			S	R-43 a	t Trare	es Rd	
Agency or Co.	Lanha	m Engir	neering	g, LLC	C		-	+ `			E/W S	Street Na	ame		Tr	rares R	d		
Date Performed										÷	N/S S	itreet Na	me		S	R-43			
Analysis Year	2047					< ↓	w	↑ ↑ S	) † }		Analy	rsis Time	Period, ł	rs	0.	.25			
Time Analyzed	DY PN	1				Ť.					Peak	Hour Fa	ctor		0.	.96			
Project Description	SR-43	Alt 1						→ ▼ *		ĺ	Jurisd	liction			0	DOT E	Distric	t 4	
Volume Adjustments	and S	ite Cł	nara	cter	ristic	S													
Approach		E	EB				V	VB		Π		1	١B		Γ		9	SB	
Movement	U	L	Т	Т	R	U	L	Т	R		U	L	Т	R	ι	J	L	Т	R
Number of Lanes (N)	0	0	1		0	0	0	1	0		0	0	1	0	(	0	0	1	0
Lane Assignment				LTR					LTR				LT	R		_			LTR
Volume (V), veh/h	0	70	80	Τ	130	0	10	30	20	,	0	60	440	10	(	0	20	640	30
Percent Heavy Vehicles, %	0	1	1		1	0	3	3	3		0	3	3	3	(	0	2	2	2
Flow Rate (VPCE), pc/h	0	74	84		137	0	11	32	21		0	64	472	11	(	0	21	680	32
Right-Turn Bypass		No	one				N	one				N	one			_	N	one	
Conflicting Lanes			1					1					1		$\square$			1	
Pedestrians Crossing, p/h			0					0					0					0	
Proportion of CAVs, %										C	)								
Critical and Follow-U	p Hea	dway	Adj	usti	men	t													
Approach		-	EB				V	VB	_			1	١B		Г		9	SB	
Lane	Left	Ri	ght	Вур	pass	Left	Ri	ght	Bypas	s	Left	Ri	ght E	ypass		Left	Ri	ght	Bypass
Critical Headway, s		4.9	763				4.9	763				4.9	763				4.9	763	
Follow-Up Headway, s		2.6	6087				2.6	6087				2.6	087		$\vdash$		2.6	087	
Flow Computations, (	Capaci	ity an	d v/	c Ra	atios	5	-		<u> </u>						-		· · ·		
Approach			EB				v	VB				1	1B		1			SB	
Lane	Left	Ri	aht	Bvr	pass	Left	Ri	aht	Bypas	s	Left	Ri	aht E	vpass		Left	Ri	aht	Bypass
Entry Flow (ve), pc/h		2	95	51			e	5 64	51			5	47	<u> </u>	-		7	33	
Entry Volume, veh/h		2	92				e	52				5	31		-		7	19	
Circulating Flow (v <sub>c</sub> ), pc/h		7	12				6	10				1	79				1	07	
Exiting Flow (vex), pc/h		1	16				1	28				5	67		$\vdash$		8	28	
Capacity (care), pc/h		6	68				7	41				1	150				12	237	
Capacity (c), veh/h		6	61				7	19				1	116		-		12	213	
v/c Ratio (x)		0.	.44				0.	.09				0	48				0	.59	
Delay and Level of Se	rvice						<u> </u>		<u> </u>	_							I		
Approach				_	EB		Т		WB	_	_		NB					SB	
Lane			Left	:	Right	Bypass	; L	eft	Right	E	Bypass	Left	Right	Вур	ass	Lef	t	Right	Bypass
Lane Control Delay (d), s/veh					11.9		1		5.9	t			8.5			-		10.1	
Lane LOS				+	В				А	+			А					В	
95% Queue Length, Q <sub>95</sub> (veh)				+	2.3				0.3	t			2.6					4.1	<u> </u>
95% Queue Length, Q <sub>95</sub> (ft)				+	58.0		+		7.7	+			66.6				+	104.1	
Approach Delay, s/veh   LOS			1	1.9		В		5.9		/	A	8.	5	A		1	0.1		В
Intersection Delay, s/veh   LOS							<b>G10</b> 9.8	of 28							A	4			

		ŀ	ICS -	Two-'	Way	Stop	-Cor	ntrol	Repo	ort							
General Information								Site Information									
Analyst	VHD						Inters	ection	SR-43 at Randolph								
Agency/Co.	Lanham Engineering, LLC						Jurisdiction				ODOT District 4						
Date Performed	i						East/West Street				Randolph						
Analysis Year	2027						North/South Street				SR-43						
Time Analyzed	AM Peak						Peak Hour Factor				0.81						
Intersection Orientation	North-South						Analysis Time Period (hrs) 0.25										
Project Description	SR-43 at Randolph Alt 2																
Lanes																	
Image: State of the state o																	
Vehicle Volumes and Adju																	
Approach		Eastb	ound			West	bound			North	bound			South	bound		
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R	
Priority	1	10	11	12		7	8	9	1U	1	2	3	4U	4	5	6	
Number of Lanes	1	0	0	1		0	0	1	0	0	1	1	0	0	1	0	
Configuration	1			R				R			Т	R				TR	
Volume (veh/h)	1			10				10			530	20			310	20	
Percent Heavy Vehicles (%)	1			5				7									
Proportion Time Blocked	1																
Percent Grade (%)	0					0											
Right Turn Channelized	No					No				No							
Median Type   Storage	Undivided																
Critical and Follow-up He	adwa	ys															
Base Critical Headway (sec)	1			6.2				6.2									
Critical Headway (sec)	1			6.25				6.27									
Base Follow-Up Headway (sec)	1			3.3				3.3									
Follow-Up Headway (sec)	1			3.35				3.36									
Delay, Queue Length, and	l Leve	l of Se	ervice	•													
Flow Rate, v (veh/h)	1			12				12									
Capacity, c (veh/h)	1			648				458									
v/c Ratio	1			0.02				0.03									
95% Queue Length, Q <sub>95</sub> (veh)				0.1				0.1									
95% Queue Length, Q <sub>95</sub> (ft)				2.6				2.6									
Control Delay (s/veh)				10.7				13.1									
Level of Service (LOS)				В				В									
Approach Delay (s/veh)		1(	).7			13.1											

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В

Approach LOS

В
		ŀ	HCS <sup>-</sup>	Two-'	Way	Stop	o-Cor	ntrol	Repo	ort						
General Information	_			_			Site	Inforr	natio	n				_		
Analyst	VHD						Inters	section			SR-43	3 at Rand	dolph			
Agency/Co.	Lanha	am Engir	neering,	LLC			Jurisc	diction			ODO	T Distric	t 4			
Date Performed							East/	West Str	eet		Rand	olph				
Analysis Year	2027						North	n/South :	Street		SR-43	3				
Time Analyzed	PM P	eak					Peak	Hour Fac	ctor		0.96					
Intersection Orientation	North	n-South					Analy	sis Time	Period (	(hrs)	0.25					
Project Description	SR-43	3 at Rand	dolph Al	t 2							1					
Lanes																
					٩٦ Major	↑ ſ <b>↑</b> ſ <b>↑</b> Y Street: No	th-South	24 4 X 4 4 5								
Vehicle Volumes and Adj	Adjustments															
Approach	Eastbound Westbound									North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	1		0	0	1	0	0	1	1	0	0	1	0
Configuration				R				R			Т	R				TR
Volume (veh/h)				10				10			460	60			650	30
Percent Heavy Vehicles (%)				0				5								
Proportion Time Blocked																
Percent Grade (%)			0				0									
Right Turn Channelized		Ν	10			١	10			١	10					
Median Type   Storage				Undi	vided											
Critical and Follow-up He	eadwa	ys														
Base Critical Headway (sec)	1			6.2				6.2								
Critical Headway (sec)				6.20				6.25								
Base Follow-Up Headway (sec)				3.3				3.3								
Follow-Up Headway (sec)				3.30				3.35								
Delay, Queue Length, and	d Leve	l of S	ervice	)			<u> </u>	<u> </u>		<u> </u>	<u> </u>					
Flow Rate, v (veh/h)	1			10				10								
Capacity, c (veh/h)				447				580								<u> </u>
v/c Ratio	1			0.02				0.02								<u> </u>
95% Queue Length, Q <sub>95</sub> (veh)				0.1				0.1								
95% Queue Length, Q <sub>95</sub> (ft)				2.5				2.6								
Control Delay (s/veh)				13.2				11.3								
Level of Service (LOS)				В				В								
Approach Delay (s/veh)	B							<u> </u>		<u>I</u>		<u>I</u>			L	<u>I</u>

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В

Approach LOS

В

		ŀ	ICS -	Гwo-	Way	Stop	-Cor	ntrol	Repo	ort						
General Information							Site	Inforr	natio	n						
Analyst	VHD						Inters	ection			SR-43	at Rand	dolph			
Agency/Co.	Lanha	ım Engir	neering,	LLC			Jurisc	liction				۲ District	: 4			
Date Performed							East/	West Str	eet		Rand	olph				
Analysis Year	2047						North	n/South :	Street		SR-43	3				
Time Analyzed	AM P	eak					Peak	Hour Fac	ctor		0.81					
Intersection Orientation	North	-South					Analy	sis Time	Period (	hrs)	0.25					
Project Description	SR-43	at Rand	dolph Al	t 2												
Lanes																
					ብ ጉ Major	1 1 Street: Nor	th-South	74 + 74 + 7 7								
Vehicle Volumes and Adju	ustments															
Approach		Eastb	ound			West	bound			North	bound			South	bound	
Movement	U	L	Т	R	U	L	Т	R	U	L	T	R	U	L	Т	R
Priority		10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes		0	0	1		0	0	1	0	0	1	1	0	0	1	0
Configuration				R				R			Т	R				TR
Volume (veh/h)	1			10				10			580	20			320	20
Percent Heavy Vehicles (%)	1			5				7								
Proportion Time Blocked	1															
Percent Grade (%)	1		0				0									
Right Turn Channelized	1	Ν	lo			Ν	10			Ν	10					
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	adwa	ys														
Base Critical Headway (sec)	1			6.2				6.2								
Critical Headway (sec)	1			6.25				6.27								
Base Follow-Up Headway (sec)	1			3.3				3.3								
Follow-Up Headway (sec)	1			3.35				3.36								
Delay, Queue Length, and	d Leve	l of Se	ervice													
Flow Rate, v (veh/h)	1			12				12								
Capacity, c (veh/h)	1			637				422								
v/c Ratio	]			0.02				0.03								
95% Queue Length, Q <sub>95</sub> (veh)				0.1				0.1								
95% Queue Length, Q <sub>95</sub> (ft)				2.6				2.6								
Control Delay (s/veh)				10.8				13.8								
Level of Service (LOS)	1			В				В								

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10.8

В

Approach Delay (s/veh)

Approach LOS

13.8

В

		ŀ	HCS <sup>-</sup>	Two-'	Way	Stop	-Cor	ntrol	Repo	ort						
General Information	_	_	_	_	_	_	Site	Inforr	natio	n	_	_	_	_		
Analyst	VHD						Inters	ection			SR-43	3 at Ran	dolph			
Agency/Co.	Lanha	am Engir	neering,	LLC			Jurisc	liction			ODO <sup>.</sup>	T Distric	t 4			
Date Performed	1						East/	West Stre	eet		Rand	olph				
Analysis Year	2047						North	n/South S	Street		SR-43	3				
Time Analyzed	PM P	eak					Peak	Hour Fac	ctor		0.96					
Intersection Orientation	North	n-South					Analy	sis Time	Period (	hrs)	0.25					
Project Description	SR-43	3 at Rand	dolph Al	t 2							1					
Lanes																
					ብ ኪ Major	↑ ſ ↑ ↓ Street: Noi	th-South	しょ 1 7 全 と C								
Vehicle Volumes and Adju	ustme	Istments														
Approach	Eastbound W						bound			North	bound			South	bound	
Movement	U	L	T	R	U	L	Т	R	U	L	Т	R	U	L	Т	R
Priority	1	10	11	12		7	8	9	1U	1	2	3	4U	4	5	6
Number of Lanes	1	0	0	1		0	0	1	0	0	1	1	0	0	1	0
Configuration	1			R				R			Т	R				TR
Volume (veh/h)	1			10				10			510	70			680	30
Percent Heavy Vehicles (%)	1			0				5								
Proportion Time Blocked																
Percent Grade (%)	1		0				0							·		
Right Turn Channelized		Ν	10			Ν	lo			Ν	10					
Median Type   Storage	1			Undi	vided											
Critical and Follow-up He	eadwa	ys														
Base Critical Headway (sec)	1			6.2				6.2								
Critical Headway (sec)	1			6.20				6.25								
Base Follow-Up Headway (sec)	1			3.3				3.3								
Follow-Up Headway (sec)	1			3.30				3.35								
Delay, Queue Length, and	d Leve	l of S	ervice				<u> </u>	<u> </u>			<u> </u>					
Flow Rate, v (veh/h)	1			10				10								
Capacity, c (veh/h)	1			429				542								
v/c Ratio	1			0.02				0.02								
95% Queue Length, Q <sub>95</sub> (veh)	1			0.1				0.1								
95% Queue Length, Q <sub>95</sub> (ft)				2.5				2.6								
Control Delay (s/veh)	1			13.6				11.8								
Level of Service (LOS)				В				В								
Approach Delay (s/veh)	B 13.6 11.8															

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В

Approach LOS

В

HCS Roundabouts Report																			
General Information				_				Sit	e Info	orn	natio	n							
Analyst	VHD						*				Inters	ection			S	R-43	at Trar	es Rd	
Agency or Co.	Lanha	m Engir	neering	g, LLC	С			← ``			E/W S	Street N	ame		Т	rares l	Rd		
Date Performed										¢	N/S S	Street Na	ime		S	R-43			
Analysis Year	2027					<b>\</b>	W	↑ F S			Analy	vsis Time	Period,	nrs	] 0	.25			
Time Analyzed	OY AN	Л				Ϋ́,					Peak	Hour Fa	ctor		0	.82			
Project Description	SR-43	Alt 2						→ ▼ *	1		Jurisc	liction			C	DOT	Distric	t 4	
Volume Adjustments	and S	ite Cł	nara	ctei	ristic	S													
Approach		E	B				\	VB				1	١B		Т			SB	
Movement	U	L	Т		R	U	L	Т	R		U	L	Т	R		U	L	Т	R
Number of Lanes (N)	0	0	1	T	0	0	0	1	0		0	0	1	0		0	0	1	0
Lane Assignment		<u> </u>		LTR	1				LTR				Ľ	R	$\top$				LTR
Volume (V), veh/h	0	60	10	Τ	30	0	20	60	) 10	)	0	130	480	10		0	20	270	30
Percent Heavy Vehicles, %	0	0	0	T	0	0	0	0	0		0	5	5	5		0	5	5	5
Flow Rate (VPCE), pc/h	0	73	12	T	37	0	24	73	12	2	0	166	615	13		0	26	346	38
Right-Turn Bypass		No	one				N	one				N	one				N	one	
Conflicting Lanes			1					1					1					1	
Pedestrians Crossing, p/h			0					0					0					0	
Proportion of CAVs, %								C	)										
Critical and Follow-U	p Hea	dway	Adj	ust	men	t													
 Approach		E	B	_			\	NB				r	NB		T			SB	
Lane	Left	Ri	ght	By	pass	Left	Ri	ight	Bypas	s	Left	R	ght	Bypass	s	Left	R	ight	Bypass
Critical Headway, s		4.9	763				4.9	9763				4.9	763		-		4.9	9763	
Follow-Up Headway, s		2.6	087				2.6	5087				2.6	087		+		2.0	5087	
Flow Computations, (	Capaci	itv an	d v/	c R	atios	5									_				
Approach			B					WB			_		JB		-			SB	
lane	Left	Ri	aht	Bv	mass	Left	Ri	iaht	Bypas	s	l eft	Ri	aht	Bypass	5	l eft	R	iaht	Bypass
Entry Flow (ve), pc/h		1	22	,			1	09	71	-		7	94	71				10	71
Entry Volume, veh/h		1	22				1	09				7	56		+			90	
Circulating Flow (v <sub>c</sub> ), pc/h		3	96		_			354				1	11		+			263	
Exiting Flow (Vex), pc/h		[	51				2	277				7	00		+		2	07	
Capacity (cpce), pc/h		9	21		_		5	78				1.	232		+		1	055	
Capacity (c), veh/h		9	21				5	578				1	174		+		1	005	
v/c Ratio (x)		0.	13		_		0	.19				0	.64		+		C	.39	
Delay and Level of Se	rvice		-						<u> </u>										
Approach					FB		Т		WB				NB					SB	
Lane	EB Left Righ					Bypas	5 1	eft	Right	TF	Bypass	Left	Righ	B	vpass	le <sup>.</sup>	ft	Right	Bypass
Lane Control Delay (d), s/veh		Left Right				Jpas			86	+	5)pass		11.7	. 5,	)   0.00			7.8	Jpass
Lane LOS		5.2					+		A.	+			В					A	
95% Queue Length. Oss (veh)		A 0.5					+		0.7	+			5.0	+				1.9	
95% Queue Length, O <sub>65</sub> (ft)				+	12.5		+		17.5	+			130 (	)				49.4	
Approach Delay, s/veh   LOS	95% Queue Length, Q <sub>95</sub> (ft)					A	1	8.6			A	11	7	В			7.8		A
Intersection Delay, s/veh   LOS					<b>G15</b> 9.7	of 28								Ą					

	S Roui	ndal	oou	its Re	pori	t													
General Information				_				Site	e Infor	mat	ion	1			_		_		
Analyst	VHD						*			In	terse	ection			SF	R-43 at	Trare	s Rd	
Agency or Co.	Lanha	m Engir	neering	g, LLC	C		+	- `		E/	W St	treet Na	ime		Tr	ares Ro	d		
Date Performed						$\left[ \right]$				N,	/S Sti	reet Na	me		SF	R-43			
Analysis Year	2027					<b>▼</b> + (	w †	E	) ↑ >	A	nalys	is Time	Period, h	rs	0.	25			
Time Analyzed	OY PN	Л				Ê				Pe	eak H	lour Fac	tor		0.	96			
Project Description	SR-43	Alt 2						•		Ju	risdi	ction			0	DOT D	istrict	4	
Volume Adjustments	and S	ite Cł	narae	cter	ristic	S													
Approach		E	ΕB				W	В		Т		N	IB				S	В	
Movement	U	L	Т		R	U	L	Т	R	ι	J	L	Т	R	ι	J	L	Т	R
Number of Lanes (N)	0	0	1		0	0	0	1	0	0	,	0	1	0	C	)	0	1	0
Lane Assignment				LTR					LTR				LT	R					LTR
Volume (V), veh/h	0	90	60		90	0	20	30	10	0	)	70	420	10	C	)	30	600	30
Percent Heavy Vehicles, %	0	1	1		1	0	3	3	3	0	)	3	3	3	C	)	2	2	2
Flow Rate (VPCE), pc/h	0	95	63		95	0	21	32	11	0	)	75	451	11	C	)	32	638	32
Right-Turn Bypass		No	one				No	ne				No	one				No	one	-
Conflicting Lanes			1				1						1					1	
Pedestrians Crossing, p/h			0				0	)				(	)				(	D	
Proportion of CAVs, %										0									
<b>Critical and Follow-U</b>	p Hea	dway	Adj	usti	men	t													
Approach	-	E	EB	_			W	B		T	_	N	IB		Γ		S	В	
Lane	Left	Ri	ght	Вур	pass	Left	Rig	Iht	Bypass	L	.eft	Rig	ght E	ypass	L	_eft	Rig	ght	Bypass
Critical Headway, s		4.9	763				4.97	763				4.9	763				4.9	763	
Follow-Up Headway, s		2.6	087				2.60	)87				2.6	087				2.6	087	
Flow Computations, (	Capaci	ity an	d v/	c Ra	atios	5													
Approach		E	B	_			W	B		Т	_	N	IB		Γ		S	В	
Lane	Left	Ri	ght	Byp	pass	Left	Rig	ht	Bypass		.eft	Rio	ght E	ypass		_eft	Rio	ght	Bypass
Entry Flow (v₂), pc/h		2	53				64	4				53	37		1		7	02	
Entry Volume, veh/h		2	50				62	2				52	21				6	88	
Circulating Flow (v <sub>c</sub> ), pc/h		6	91				62	1				19	90				12	28	
Exiting Flow (vex), pc/h		1	06				13	9		+		5	57				7	54	
Capacity (cpca), pc/h		6	82				73	2				11	37				12	11	
Capacity (c), veh/h		6	75				71	1				11	04				11	87	
v/c Ratio (x)		0.	.37				0.0	)9				0.4	47				0.	58	
Delay and Level of Se	rvice	0.37															1		
Approach					EB		Γ		WB		Т		NB					SB	
Lane		Left Righ					Le	ft	Right	Вура	ss	Left	Right	Вур	ass	Left	6	Right	Bypass
Lane Control Delay (d), s/veh		10.3							6.0				8.5					10.0	
Lane LOS		B							А				А					В	
95% Queue Length, Q <sub>95</sub> (veh)		в 1.7							0.3				2.6					3.9	
95% Queue Length, Q <sub>95</sub> (ft)				$\uparrow$	42.8				7.7				66.6					99.1	
Approach Delay, s/veh   LOS	5% Queue Length, Q <sub>95</sub> (ft) pproach Delay, s/veh   LOS					В	040	6.0		А		8.5		А		1(	0.0		В
Intersection Delay, s/veh   LOS							9.4	ot 28			+		1		A	۱			

					HC	S Rou	nda	bοι	uts Re	ep	ort								
General Information				_				Sit	e Info	rn	natio	n			_		_		
Analyst	VHD						4				Inters	ection			S	R-43 a	at Trar	es Rd	
Agency or Co.	Lanha	ım Engir	neering	g, LL(	.C		•				E/W S	Street N	ame		Т	rares I	Rd		
Date Performed						$\square$				÷	N/S S	itreet Na	ime		S	R-43			
Analysis Year	2047					<b>∢</b> ↓ (	w	¢ F S	†		Analy	rsis Time	Period, I	irs	0	.25			
Time Analyzed	DY AN	N				Ê					Peak	Hour Fa	ctor		0	.82			
Project Description	SR-43	Alt 2						→ ▼ *			Jurisd	liction			С	DOT	Distric	t 4	
Volume Adjustments	and S	ite Cł	narae	cte	ristic	s													
Approach		E	B				W	/B				1	١B		Т			SB	
Movement	U	L	Т		R	U	L	Т	R		U	L	Т	R	1	U	L	Т	R
Number of Lanes (N)	0	0	1		0	0	0	1	0	Ĩ	0	0	1	0		0	0	1	0
Lane Assignment				LTR	R				LTR				1	R					LTR
Volume (V), veh/h	0	90	10	Τ	40	0	20	80	20		0	130	490	10		0	20	280	30
Percent Heavy Vehicles, %	0	0	0	Τ	0	0	0	0	0	Τ	0	5	5	5		0	5	5	5
Flow Rate (VPCE), pc/h	0	110	12	Τ	49	0	24	98	24		0	166	627	13		0	26	359	38
Right-Turn Bypass		No	one				No	one				N	one		Τ		N	one	
Conflicting Lanes			1					1					1		Τ			1	
Pedestrians Crossing, p/h			0				(	0		Τ			0		Τ			0	
Proportion of CAVs, %										0	)								
<b>Critical and Follow-U</b>	p Hea	dway	Adj	ust	tmen	t													
Approach		E	B				W	/B				1	١B		Т			SB	
Lane	Left	Ri	ght	Ву	/pass	Left	Rig	ght	Bypas	s	Left	Ri	ght I	sypass		Left	R	ight	Bypass
Critical Headway, s		4.9	763				4.9	763				4.9	763		$\top$		4.	9763	
Follow-Up Headway, s		2.6	087				2.6	087				2.6	087				2.	5087	
Flow Computations, (	Capaci	ity an	d v/	c R	atios	5													
Approach		E	B	_	_		W	/B		Τ		1	١B	_	Т	_	_	SB	
Lane	Left	Ri	ght	By	/pass	Left	Rig	ght	Bypas	s	Left	Ri	ght l	Sypass		Left	R	ight	Bypass
Entry Flow (ve), pc/h		1	71				14	46				8	06		1		4	123	
Entry Volume, veh/h		1	71				14	46				7	68				4	103	
Circulating Flow (v <sub>c</sub> ), pc/h		4	09				90	03		T		1	48				2	288	
Exiting Flow (v <sub>ex</sub> ), pc/h		5	51				30	02				7	61		$\top$		4	132	
Capacity (coce), pc/h		9	09				54	49				1	187				1	029	
Capacity (c), veh/h		9	09				54	49				1	130		$\top$		ģ	980	
v/c Ratio (x)		0.	.19				0.	27				0	.68		$\top$		(	.41	
Delay and Level of Se	rvice																		
Approach					EB		Τ		WB				NB					SB	
Lane	Left Righ					Bypass	Le	eft	Right	B	Bypass	Left	Right	Ву	oass	Lef	ťt	Right	Bypass
Lane Control Delay (d), s/veh		5.8							10.2	T			13.0					8.3	
Lane LOS		A							В	T			В					А	
95% Queue Length, Q <sub>95</sub> (veh)		A 0.7							1.1	T			5.6					2.0	
95% Queue Length, Q <sub>95</sub> (ft)				$\uparrow$	17.5				27.5	T			145.6					52.0	
Approach Delay, s/veh   LOS	15% Queue Length, Q <sub>95</sub> (ft)					A	C 4 7	10.2		E	В	13	0	В			8.3		A
Intersection Delay, s/veh   LOS							<b>617</b> 10.6	01-28							E	B			

HCS Roundabouts Report																			
General Information								Sit	e Info	rn	natior	n			_				
Analyst	VHD						*				Inters	ection			S	R-43 a	t Trare	es Rd	
Agency or Co.	Lanha	m Engir	neering	g, LLC				+ `		ľ	E/W S	Street N	ame		Т	rares F	d		
Date Performed										÷	N/S S	treet Na	me		S	R-43			
Analysis Year	2047					< ↓	w	↑ F S	†		Analy	sis Time	Period, I	nrs	0	.25			
Time Analyzed	DY PN	1				<u></u>					Peak	Hour Fa	ctor		0.	.96			
Project Description	SR-43	Alt 2						→ ▼ *	1	ľ	Jurisd	liction			С	DOT [	Distric	t 4	
Volume Adjustments	and S	ite Ch	nara	cteri	istic	S													
Approach		E	B				V	VB		Τ		1	١B		Г		9	SB	
Movement	U	L	Т		R	U	L	Т	R		U	L	Т	R	L I	J	L	Т	R
Number of Lanes (N)	0	0	1		0	0	0	1	0		0	0	1	0	(	0	0	1	0
Lane Assignment		<u> </u>		LTR					LTR				Ľ	R					LTR
Volume (V), veh/h	0	130	80	1	130	0	20	50	20		0	70	430	10	(	0	30	630	30
Percent Heavy Vehicles, %	0	1	1		1	0	3	3	3		0	3	3	3	(	0	2	2	2
Flow Rate (VPCE), pc/h	0	137	84	1	137	0	21	54	21		0	75	461	11	(	0	32	669	32
Right-Turn Bypass		No	one				N	one				N	one				N	one	
Conflicting Lanes			1					1					1					1	
Pedestrians Crossing, p/h			0					0					0					0	
Proportion of CAVs, %								0	)										
Critical and Follow-U	p Hea	dway	ustn	t															
Approach		E	B				V	VB	_	Т		1	١B		Τ		9	SB	
Lane	Left	Rie	ght	Вур	ass	Left	Ri	ght	Bypas	s	Left	Ri	ght l	Sypass		Left	Ri	ght	Bypass
Critical Headway, s		4.9	763		_		4.9	763				4.9	763				4.9	763	
Follow-Up Headway, s		2.6	087				2.6	6087				2.6	087				2.6	087	
Flow Computations, (	Capaci	ity an	d v/	c Ra	ntios	5											1		
Approach	•	• E	B				v	VB		Т		1	1B		Т			SB	
Lane	Left	Rie	ght	Вур	ass	Left	Ri	aht	Bypas	s	Left	Ri	ght I	Sypass		Left	Ri	aht	Bypass
Entry Flow (v₀), pc/h		3	58				9	96				5	47				7	33	
Entry Volume, veh/h		3	54				9	93				5	31				7	19	
Circulating Flow (v <sub>c</sub> ), pc/h		7.	22				6	73				2	53				1	50	
Exiting Flow (vex), pc/h		1	27				1	61				6	19				8	27	
Capacity (cpce), pc/h		6	61				6	95				1	066				1	184	
Capacity (c), veh/h		6	54				6	74				1	)35				1	161	
v/c Ratio (x)		0.	54		_		0.	.14				0	.51				0	.62	
Delay and Level of Se	rvice	0.54					1		1										
Approach					EB		Т		WB	_			NB					SB	
Lane		Left Righ					; L	eft	Right	E	Bypass	Left	Righ	Вур	bass	Lef	t	Right	Bypass
Lane Control Delay (d), s/veh		Leπ         Kign           14.5							6.9	T			9.6					11.1	
Lane LOS		14.5 B					+		А	$\dagger$			А				+	В	
95% Queue Length, Q <sub>95</sub> (veh)		З.3							0.5	t			3.0					4.5	
95% Queue Length, Q <sub>95</sub> (ft)					83.2				12.8	$\dagger$			76.8				+	114.3	
Approach Delay, s/veh   LOS	25% Queue Length, Q₀₅ (ft) vpproach Delay, s/veh   LOS 14					В	<b>.</b>	6.9		-	Ą	9.	5	A		1	1.1		B
Intersection Delay, s/veh   LOS		14.5					<b>-G18</b> 11.1	of 28							E	3			

		HCS	All-W	'ay Sto	p Con	trol Re	eport					
General and Site Informat	ion				Lanes							
Analyst	VHD						-					
Agency/Co.	Lanham	Engineerii	ng, LLC		1			<u>*</u>	┶┢	⊾ L <u>_</u>		
Date Performed					1			×	•			
Analysis Year	2027				1	_*					K	
Analysis Time Period (hrs)	0.25				1	<u>~</u>					<u> </u>	
Time Analyzed	AM Pea	k				*	*			*	k k	
Project Description	SR-43 a	t Randolph	AWSC				T			Y		
Intersection	SR-43 a	t Randolph	ı								*	
Jurisdiction	ODOT D	District 4			]							
East/West Street	Randolp	oh Road			]			×	₽			
North/South Street	SR-43						ካ	ন ক	╵ ⋎ <b>┦</b> ┣┣	<u>م</u> ،		
Peak Hour Factor	0.81											
Turning Movement Dema	nd Volum	nes										
Approach		Eastbound	1		Westbound	b	1	Northboun	d	9	Southboun	ıd
Movement	L	Т	R	L	Т	R	L	Т	R	L	Т	R
Volume (veh/h)	10	10	10	10	20	10	10	520	10	10	300	20
% Thrus in Shared Lane												
Lane Flow Rate and Adjust	tments											
Approach		Eastbound	1		Westbound	b		Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	37			49			667			407		
Percent Heavy Vehicles	5			7			5			4		
Initial Departure Headway, hd (s)	3.20			3.20			3.20			3.20		
Initial Degree of Utilization, x	0.033			0.044			0.593			0.362		
Final Departure Headway, hd (s)	6.47			6.50			4.78			5.02		
Final Degree of Utilization, x	0.067			0.089			0.885			0.568		
Move-Up Time, m (s)	2.0			2.0			2.0			2.0		
Service Time, ts (s)	4.47			4.50			2.78			3.02		
Capacity, Delay and Level	of Servic	e										
Approach		Eastbound	1		Westbound	d		Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	37			49			667			407		
Capacity (veh/h)	556			554			753			717		
95% Queue Length, Q₃₅ (veh)	0.2			0.3			11.3			3.6		
95% Queue Length, Q₃₅ (ft)	5.2			7.9			293.8			92.9		
Control Delay (s/veh)	9.9			10.1			32.6			14.4		
Level of Service, LOS	А			В			D			В		
Approach Delay (s/veh)   LOS	9.9		A	10.1		В	32.6		D	14.4		В
Intersection Delay (s/veh)   LOS			24	4.5						С		

		HCS	All-W	'ay Sto	p Con	trol Re	eport					
General and Site Informat	ion				Lanes							
Analyst	VHD											
Agency/Co.	Lanham	Engineerii	ng, LLC		1			<u></u>	┶┶┝	د ل <u>ه</u>		
Date Performed					1				•			
Analysis Year	2027				1	_*					<b>K</b>	
Analysis Time Period (hrs)	0.25				1	4					<u> </u>	
Time Analyzed	PM Pea	k			1	*					<b>←</b>	
Project Description	SR-43 a	t Randolph	n AWSC		1		7			7		
Intersection	SR-43 a	t Randolph	ו		1						<u>▼</u> ←	
Jurisdiction	ODOT D	District 4			1	× 						
East/West Street	Randolp	oh Road			1				<b>t</b>			
North/South Street	SR-43				1		ሻ	<u>र्</u> र् र र	╵ ⋎ <b>∕│</b> ╋│ ╋	• <b>•</b>		
Peak Hour Factor	0.96											
Turning Movement Demai	nd Volum	nes										
Approach		Eastbound	ł		Westbound	d		Northboun	d	9	Southboun	d
Movement	L	Т	R	L	Т	R	L	Т	R	L	Т	R
Volume (veh/h)	10	30	10	10	10	10	10	450	30	10	640	30
% Thrus in Shared Lane												
Lane Flow Rate and Adjust	ments											
Approach		Eastbound	ł		Westbound	d		Northboun	d	9	Southboun	d
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	52			31			510			708		
Percent Heavy Vehicles	0			5			3			2		
Initial Departure Headway, hd (s)	3.20			3.20			3.20			3.20		
Initial Degree of Utilization, x	0.046			0.028			0.454			0.630		
Final Departure Headway, hd (s)	6.69			6.80			5.06			4.84		
Final Degree of Utilization, x	0.097			0.059			0.717			0.952		
Move-Up Time, m (s)	2.0			2.0			2.0			2.0		
Service Time, ts (s)	4.69			4.80			3.06			2.84		
Capacity, Delay and Level	of Servic	e										
Approach		Eastbound	ł		Westbound	d	1	Northboun	d	9	Southboun	d
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	52			31			510			708		
Capacity (veh/h)	538			529			712			744		
95% Queue Length, Q <sub>95</sub> (veh)	0.3			0.2			6.1			14.2		
95% Queue Length, Q₃₅ (ft)	7.5			5.2			156.2			360.7		
Control Delay (s/veh)	10.4			10.2			19.8			43.9		
Level of Service, LOS	В			В			С			E		
Approach Delay (s/veh)   LOS	10.4		В	10.2		В	19.8		С	43.9		E
Intersection Delay (s/veh)   LOS			3	2.3						D		

		HCS	All-W	'ay Sto	p Con	trol Re	eport					
General and Site Informat	ion				Lanes							
Analyst	VHD						-					
Agency/Co.	Lanham	Engineerii	ng, LLC		1			<u></u>	L III I	د ل <u>ه</u>		
Date Performed					1			4	4			
Analysis Year	2047				1	_*					<b>K</b>	
Analysis Time Period (hrs)	0.25				1	4					<u> </u>	
Time Analyzed	AM Pea	k			1	*					<b>←</b>	
Project Description	SR-43 a	t Randolph	NAWSC		1	$\prec$	4			<b>*</b>		
Intersection	SR-43 a	t Randolph	ı		1						¥ +	
Jurisdiction	ODOT D	District 4			1	× – – – – – – – – – – – – – – – – – – –						
East/West Street	Randolp	oh Road			1			×				
North/South Street	SR-43				1		ሻ	*	▎ ↗│╀│₺			
Peak Hour Factor	0.81				1							
Turning Movement Dema	nd Volum	nes			<u> </u>							
Approach		Eastbound	1		Westbound	b		Northboun	d	9	Southboun	ıd
Movement	L	Т	R	L	Т	R	L	Т	R	L	Т	R
Volume (veh/h)	20	10	10	10	30	10	10	560	10	10	310	20
% Thrus in Shared Lane												
Lane Flow Rate and Adjus	tments		<u> </u>									
Approach		Eastbound	1		Westbound	d		Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	49			62			716			420		
Percent Heavy Vehicles	5			7			5			4		
Initial Departure Headway, hd (s)	3.20			3.20			3.20			3.20		
Initial Degree of Utilization, x	0.044			0.055			0.636			0.373		
Final Departure Headway, hd (s)	6.87			6.83			4.94			5.25		
Final Degree of Utilization, x	0.094			0.117			0.983			0.612		
Move-Up Time, m (s)	2.0			2.0			2.0			2.0		
Service Time, t <sub>s</sub> (s)	4.87			4.83			2.94			3.25		
Capacity, Delay and Level	of Servic	e										
Approach		Eastbound	1		Westbound	b		Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	49			62			716			420		
Capacity (veh/h)	524			527			728			685		
95% Queue Length, Q <sub>95</sub> (veh)	0.3			0.4			15.6			4.2		
95% Queue Length, Q <sub>95</sub> (ft)	7.8			10.6			405.6			108.4		
Control Delay (s/veh)	10.6			10.7			51.0			16.2		
Level of Service, LOS	В			В			F			С		
Approach Delay (s/veh)   LOS	10.6		В	10.7		В	51.0		F	16.2		С
Intersection Delay (s/veh)   LOS			3	5.7						E		

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		HCS	All-W	'ay Sto	p Con	trol Re	eport					
General and Site Informat	ion				Lanes							
Analyst	VHD						_					
Agency/Co.	Lanham	Engineerii	ng, LLC		1			*				
Date Performed					1			Ľ	*			
Analysis Year	2047				1	_*					K	
Analysis Time Period (hrs)	0.25				1	4					_ <u>↓</u>	
Time Analyzed	PM Pea	k			1	*	*				<b>←</b> ĸ	
Project Description	SR-43 a	t Randolph	NAWSC		1	<b>1</b>	<b>T</b>			, T		
Intersection	SR-43 a	t Randolph	ı		1							
Jurisdiction	ODOT D	District 4			1							
East/West Street	Randolp	oh Road			1			×				
North/South Street	SR-43				1		ሻ	<b>N</b>	▎ ↗ ↑ ∱	<u>م</u> ا		
Peak Hour Factor	0.96				1							
Turning Movement Dema	nd Volum	nes										
Approach		Eastbound	1		Westbound	k	l i	Northboun	d	9	Southboun	ıd
Movement	L	Т	R	L	Т	R	L	Т	R	L	Т	R
Volume (veh/h)	20	40	10	10	20	10	10	490	30	10	670	30
% Thrus in Shared Lane												
Lane Flow Rate and Adjus	tments		<u> </u>		<u> </u>					-		
Approach		Eastbound	1		Westbound	k	1	Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	73			42			552			740		
Percent Heavy Vehicles	0			5			3			2		
Initial Departure Headway, hd (s)	3.20			3.20			3.20			3.20		
Initial Degree of Utilization, x	0.065			0.037			0.491			0.657		
Final Departure Headway, hd (s)	6.88			7.03			5.22			5.06		
Final Degree of Utilization, x	0.139			0.081			0.800			1.040		
Move-Up Time, m (s)	2.0			2.0			2.0			2.0		
Service Time, t <sub>s</sub> (s)	4.88			5.03			3.22			3.06		
Capacity, Delay and Level	of Servic	e										
Approach		Eastbound	1		Westbound	ł	1	Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	73			42			552			740		
Capacity (veh/h)	523			512			690			711		
95% Queue Length, Q <sub>95</sub> (veh)	0.5			0.3			8.1			18.5		
95% Queue Length, Q <sub>95</sub> (ft)	12.5			7.8			207.4			469.9		
Control Delay (s/veh)	11.0			10.6			25.7			66.7		
Level of Service, LOS	В			В			D			F		
Approach Delay (s/veh)   LOS	11.0		В	10.6		В	25.7		D	66.7		F
Intersection Delay (s/veh)   LOS			4	6.0						E		

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		HCS	All-W	'ay Sto	p Con	trol Re	eport					
General and Site Informat	ion				Lanes							
Analyst	VHD											
Agency/Co.	Lanham	Engineerii	ng, LLC		1			<u>x</u> ]	└╺┢			
Date Performed					1			4				
Analysis Year	2027				1	_*					<b>K</b>	
Analysis Time Period (hrs)	0.25				1						<u> </u>	
Time Analyzed	AM Pea	k			1	*					<b>←</b>	
Project Description	SR-43 a	t Trares AV	/SC		1		<b>T</b>			7		
Intersection	SR-43 a	t Trares			1						<u>▼</u> ←	
Jurisdiction	ODOT D	District 4			1							
East/West Street	Trares R	load			1	•		×				
North/South Street	SR-43				1		ሻ	ন ক	ĭ ĭ∕™ † †	<u>م</u> ا		
Peak Hour Factor	0.82				1							
Turning Movement Dema	nd Volum	nes										
Approach		Eastbound	1		Westbound	d	1	Northboun	d	9	Southboun	ıd
Movement	L	Т	R	L	Т	R	L	Т	R	L	Т	R
Volume (veh/h)	40	10	30	10	40	10	120	490	10	10	280	30
% Thrus in Shared Lane												
Lane Flow Rate and Adjus	tments											
Approach		Eastbound	1		Westbound	d	1	Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	98			73			756			390		
Percent Heavy Vehicles	0			0			5			5		
Initial Departure Headway, hd (s)	3.20			3.20			3.20			3.20		
Initial Degree of Utilization, x	0.087			0.065			0.672			0.347		
Final Departure Headway, hd (s)	6.63			6.77			5.19			5.45		
Final Degree of Utilization, x	0.180			0.138			1.089			0.591		
Move-Up Time, m (s)	2.0			2.0			2.0			2.0		
Service Time, ts (s)	4.63			4.77			3.19			3.45		
Capacity, Delay and Level	of Servic	e								-		
Approach		Eastbound	1		Westbound	d	1	Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	98			73			756			390		
Capacity (veh/h)	543			532			694			660		
95% Queue Length, Q <sub>95</sub> (veh)	0.6			0.5			21.2			3.9		
95% Queue Length, Q <sub>95</sub> (ft)	15.0			12.5			551.2			101.4		
Control Delay (s/veh)	11.1			10.8			82.5			16.0		
Level of Service, LOS	В			В			F			С		
Approach Delay (s/veh)   LOS	11.1		В	10.8		В	82.5		F	16.0		С
Intersection Delay (s/veh)   LOS			5	3.6						F		

		HCS	All-W	'ay Sto	p Con	trol Re	eport					
General and Site Informat	ion				Lanes							
Analyst	VHD						-					
Agency/Co.	Lanham	Engineerii	ng, LLC		1			<u></u>	Lata b	د ل <u>ه</u>		
Date Performed					1			×	*			
Analysis Year	2027				1	_*					K	
Analysis Time Period (hrs)	0.25				1	4					<u> </u>	
Time Analyzed	PM Pea	k			1	*					<b>←</b>	
Project Description	SR-43 a	t Trares AV	/SC		1	$\prec$				Ŷ		
Intersection	SR-43 a	t Trares			1							
Jurisdiction	ODOT D	District 4			1	* ~						
East/West Street	Trares R	oad			1	•	$\sim$	×				
North/South Street	SR-43				1		ካ	মা মাদা≍	╷ ╱╸╡╴╊			
Peak Hour Factor	0.96				1							
Turning Movement Dema	nd Volum	nes			-							
Approach		Eastbound	1		Westbound	d		Northboun	d	9	Southbour	ıd
Movement	L	Т	R	L	Т	R	L	Т	R	L	Т	R
Volume (veh/h)	50	60	90	10	20	10	60	430	10	20	610	30
% Thrus in Shared Lane												
Lane Flow Rate and Adjust	tments											
Approach		Eastbound	1		Westbound	d		Northboun	d	9	Southbour	nd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	208			42			521			688		
Percent Heavy Vehicles	1			3			3			2		
Initial Departure Headway, hd (s)	3.20			3.20			3.20			3.20		
Initial Degree of Utilization, x	0.185			0.037			0.463			0.611		
Final Departure Headway, hd (s)	6.80			7.68			5.87			5.73		
Final Degree of Utilization, x	0.393			0.089			0.849			1.094		
Move-Up Time, m (s)	2.0			2.0			2.0			2.0		
Service Time, ts (s)	4.80			5.68			3.87			3.73		
Capacity, Delay and Level	of Servic	e										
Approach		Eastbound	1		Westbound	d		Northboun	d	9	Southbour	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	208			42			521			688		
Capacity (veh/h)	530			469			614			629		
95% Queue Length, Q <sub>95</sub> (veh)	1.9			0.3			9.3			20.2		
95% Queue Length, Q₃₅ (ft)	47.9			7.7			238.1			513.1		
Control Delay (s/veh)	14.1			11.4			33.1			86.9		
Level of Service, LOS	В			В			D			F		
Approach Delay (s/veh)   LOS	14.1		В	11.4		В	33.1		D	86.9		F
Intersection Delay (s/veh)   LOS			5	5.2				F				

		HCS	All-W	'ay Sto	p Con	trol Re	eport					
General and Site Informat	ion				Lanes							
Analyst	VHD						-					
Agency/Co.	Lanham	Engineerii	ng, LLC		1			<u></u>	Lata b			
Date Performed					1			×	*			
Analysis Year	2047				1	_*					<b>K</b>	
Analysis Time Period (hrs)	0.25				1	-*					<u>*</u>	
Time Analyzed	AM Pea	k			1	*					<b>←</b>	
Project Description	SR-43 a	t Trares AV	/SC		1	$\prec$	4			7		
Intersection	SR-43 a	t Trares			1						¥ +	
Jurisdiction	ODOT D	District 4			1	× 						
East/West Street	Trares R	oad			1			×	<b>*</b>			
North/South Street	SR-43				1		ሻ	<u>र्</u> र र र	╷ ╱┥ <b>╀</b> ╞╊	<u>م</u> ا		
Peak Hour Factor	0.82				1							
Turning Movement Dema	nd Volum	nes										
Approach		Eastbound	1		Westbound	d		Northboun	d	9	Southboun	ıd
Movement	L	Т	R	L	Т	R	L	Т	R	L	Т	R
Volume (veh/h)	60	10	40	10	50	20	120	500	10	10	290	30
% Thrus in Shared Lane												
Lane Flow Rate and Adjus	tments		<u> </u>	-	-	<u> </u>	<u> </u>			-		
Approach		Eastbound	1		Westbound	d		Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	134			98			768			402		
Percent Heavy Vehicles	0			0			5			5		
Initial Departure Headway, hd (s)	3.20			3.20			3.20			3.20		
Initial Degree of Utilization, x	0.119			0.087			0.683			0.358		
Final Departure Headway, hd (s)	6.83			6.95			5.52			5.76		
Final Degree of Utilization, x	0.255			0.188			1.179			0.643		
Move-Up Time, m (s)	2.0			2.0			2.0			2.0		
Service Time, t <sub>s</sub> (s)	4.83			4.95			3.52			3.76		
Capacity, Delay and Level	of Servic	e										
Approach		Eastbound	1		Westbound	d	1	Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	134			98			768			402		
Capacity (veh/h)	527			518			652			625		
95% Queue Length, Q <sub>95</sub> (veh)	1.0			0.7			25.8			4.6		
95% Queue Length, Q <sub>95</sub> (ft)	25.0			17.5			670.8			119.6		
Control Delay (s/veh)	12.1			11.6			116.3			18.5		
Level of Service, LOS	В			В			F			С		
Approach Delay (s/veh)   LOS	12.1		В	11.6		В	116.3	;	F	18.5		С
Intersection Delay (s/veh)   LOS			7	1.0				F				

		HCS	All-W	'ay Sto	p Con	trol Re	eport					
General and Site Informat	ion				Lanes							
Analyst	VHD						-					
Agency/Co.	Lanham	Engineerii	ng, LLC		1			<u></u>	L III I	د ل <u>ه</u>		
Date Performed					1			×				
Analysis Year	2047				1	_*					<b>K</b>	
Analysis Time Period (hrs)	0.25				1	4					<b>▲</b>	
Time Analyzed	PM Pea	k			1	*					<b>←</b>	
Project Description	SR-43 a	t Trares AV	/SC		1	$\prec$	4			<b>*</b>		
Intersection	SR-43 a	t Trares			1							
Jurisdiction	ODOT D	District 4			1	× –						
East/West Street	Trares R	oad			1			×				
North/South Street	SR-43				1		ሻ	xt xtx *	▎ ↗│╀│₺			
Peak Hour Factor	0.96				1							
Turning Movement Dema	nd Volum	nes										
Approach		Eastbound	l		Westbound	b		Northboun	d	9	Southboun	ıd
Movement	L	Т	R	L	Т	R	L	Т	R	L	Т	R
Volume (veh/h)	70	80	130	10	30	20	60	440	10	20	640	30
% Thrus in Shared Lane												
Lane Flow Rate and Adjus	tments				<u> </u>			<u> </u>				
Approach		Eastbound	1		Westbound	d		Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	292			63			531			719		
Percent Heavy Vehicles	1			3			3			2		
Initial Departure Headway, hd (s)	3.20			3.20			3.20			3.20		
Initial Degree of Utilization, x	0.259			0.056			0.472			0.639		
Final Departure Headway, h₄ (s)	7.05			8.22			6.41			6.38		
Final Degree of Utilization, x	0.571			0.143			0.946			1.275		
Move-Up Time, m (s)	2.0			2.0			2.0			2.0		
Service Time, t <sub>s</sub> (s)	5.05			6.22			4.41			4.38		
Capacity, Delay and Level	of Servic	e										
Approach		Eastbound	l		Westbound	b		Northboun	d	9	Southboun	ıd
Lane	L1	L2	L3	L1	L2	L3	L1	L2	L3	L1	L2	L3
Configuration	LTR			LTR			LTR			LTR		
Flow Rate, v (veh/h)	292			63			531			719		
Capacity (veh/h)	511			438			562			564		
95% Queue Length, Q <sub>95</sub> (veh)	3.5			0.5			12.3			28.7		
95% Queue Length, Q95 (ft)	88.2			12.8			314.9			729.0		
Control Delay (s/veh)	19.0			12.6			50.9			157.6		
Level of Service, LOS	С			В			F			F		
Approach Delay (s/veh)   LOS	19.0		C	12.6		В	50.9		F	157.6	;	F
Intersection Delay (s/veh)   LOS			9	1.4						F		



D4 SAFETY STUDY - POR-SR 43 & TRARES & RANDOLPH MODEL Vertical Sight Distance Sheet PAPERSIZE 17X11 (In.) DATE: 1/29/2025 TIME: 3:20:37 PM USER: NATES



D4 SAFETY STUDY - POR-SR 43 & TRARES & RANDOLPH MODEL: Vertical Sight Distance Sheet - 2 PAPERSIZE: 1/2/11 (In.) DATE: 1/29/2025 TIME: 3.20:38 PM USER: lyates P: NOTVETY0035\_ D4 Shery Studies (Task 4) POR-SR 43 & Trares & Randolph/Analysis/Sight Distance Analysis/Sight Distance den

## Appendix H HSM Analysis



ECAT	Project Informati								
Economic Crash Analysis Tool	General Information								
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com						
Project Description	SR-43 Safety Study: Existing	Contact Phone	614-656-2429						
Reference Number	ODOT PID 1147572	Date Performed	10/28/2024						
Analyst	GMB	Analysis Year	2022						
Agency/Company	Carpenter Marty Transportation								
Perform Benefit Cost Analysis?	Yes								
Do the proposed in									

Do the proposed improvements fundamentally change the conditions of the base safety perform Or is crash data unavailable for the analysis condition, Or is only predicted (and not expected) analysis needed for the existing or proposed condition?

(Examples: unsignalized to signalized, undivided to divided, increase or decrease in the number of lanes, change the number of approaches to an intersection, significant realignment of the roadway)

If Yes, are you analyzing the existing or proposed conditions?

Existing

Yes

Project Elements Description Table									
			Location Information						
Project Element ID (Must be Unique)	Site Type	Intersection Control Type	NLFID	Begin Logpoint/ Intersection Midpoint	End Logpoint (Leave blank for Intersection)	Length (mi) OR Intersection Radius Buffer (mi)	Cross Route NLFID(s)	Common Name	
SR43; 3.868-3.936	Rural Two-Lane Two Way Segment		SPORSR00043**C	3.868	3.936	0.068		SR-43 (Cleveland Canton Road)	
SR43; 3.868	Rural Two-Lane Two Way Intersection	Unsignalized	SPORSR00043**C	3.868		0.05	CPORCR0002	SR-43 @ Trares Road	
SR43; 3.936	Rural Two-Lane Two Way Intersection	Unsignalized	SPORSR00043**C	3.936		0.05	CPORCR0001	SR-43 @ Randolph Road	

Traffic Volume Growth Rate Calculation For Benefit Cost Analysis									
	Year	AADT							
Present ADT (PADT)			veh / day						
Future ADT (FADT)			veh / day						
Annual Linear Growth Rate									



ECAT	Project Safety Performance Report							
Economic Crash Analysis Tool	General							
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com					
Project Description	SR-43 Safety Study: Existing	Contact Phone	614-656-2429					
Reference Number	ODOT PID 1147572	Date Performed	10/28/2024					
Analyst	GMB	Analysis Year	2022					
Agency/Company	Carpenter Marty Transportation							



Project Summary Results (Without Animal Crashes)										
KA B C O Total										
N <sub>predicted</sub> - Existing Conditions	0.4736	1.1505	0.7602	4.0919	6.4762					
N <sub>expected</sub> - Existing Conditions	0.5335	1.2954	0.8573	3.8484	6.5346					
$\mathbf{N}_{\text{potential for improvement}}$ - Existing Conditions	0.0599	0.1449	0.0971	-0.2435	0.0584					



ECAT	Project Safety Performance Report							
Economic Crash Analysis Tool	Genera	General Information						
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com					
Project Description	SR-43 Safety Study: Existing	Contact Phone	614-656-2429					
Reference Number	ODOT PID 1147572	Date Performed	10/28/2024					
Analyst	GMB	Analysis Year	2022					
Agency/Company	Carpenter Marty Transportation							

Existing Conditions Project Element Predicted Crash Summary (Without Animal Crashes)										
Broject Floment ID	Common Nomo		Crash Severity Level							
Project Element ID	Common Name	KA	В	C	0	Total				
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	0.0125	0.0325	0.0158	0.0912	0.152				
SR43; 3.868	SR-43 @ Trares Road	0.2727	0.6613	0.4404	2.3665	3.7409				
SR43; 3.936	SR-43 @ Randolph Road	0.1884	0.4567	0.304	1.6342	2.5833				

Existing Conditions Project Element Expected Crash Summary (Without Animal Crashes)										
Droject Floment ID	Common Name		Crash Severity Level							
Project Element ID	Common Name	KA	В	С	0	Total				
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	0.0102	0.0268	0.0125	0.0546	0.1041				
SR43; 3.868	SR-43 @ Trares Road	0.3036	0.7359	0.4901	1.9438	3.4734				
SR43; 3.936	SR-43 @ Randolph Road	0.2197	0.5327	0.3547	1.85	2.9571				

Existing Conditions Project Element Potential for Safety Improvement Summary (Without Animal Crashes)										
Project Element ID	Common Nomo		Crash Severity Level							
	Common Name	KA	В	C	0	Total				
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	-0.0023	-0.0057	-0.0033	-0.0366	-0.0479				
SR43; 3.868	SR-43 @ Trares Road	0.0309	0.0746	0.0497	-0.4227	-0.2675				
SR43; 3.936	SR-43 @ Randolph Road	0.0313	0.076	0.0507	0.2158	0.3738				

Summary by Crash Type								
		Existing		Proposed				
Crash Type	Predicted Crash	Expected Crash	PSI	Expected Crash				
	Frequency	Frequency	FSI	Frequency				
Unknown	0.0325	0.0306	-0.0019					
Head On	0.0716	0.0709	-0.0007					
Rear End	1.7720	1.6568	-0.1152					
Backing	0.3309	0.2953	-0.0356					
Sideswipe - Meeting	0.2481	0.2341	-0.0140					
Sideswipe - Passing	0.3768	0.3463	-0.0305					
Angle	3.1254	3.0244	-0.1010					
Parked Vehicle	0.2925	0.2639	-0.0286					
Pedestrian	0.0406	0.0416	0.0010					
Animal	0.1063	0.0645	-0.0418					
Train	0.0014	0.0014	0.0000					
Pedalcycles	0.0304	0.0307	0.0003					
Other Non-Vehicle	0.0006	0.0007	0.0001					
Fixed Object	1.4494	1.3343	-0.1151					
Other Object	0.0510	0.0452	-0.0058					
Overturning	0.0892	0.0865	-0.0027					
Other Non-Collision	0.1125	0.1017	-0.0108					
Left Turn	0.2999	0.2888	-0.0111					
Right Turn	0.0000	0.0000	0.0000					



Existing Conditions: General Information and Data for Rural Two-Lane Two-Way Intersection								
General Information					Location Information			
Analyst	GMB				Route		SR43	
Agency or Company	Carpenter Marty T	ransportation			Logpoint		3.936	
Date Performed	10/28/24				Common Name		SR-43 @ Randolp	h Road
Intersection	SR43; 3.936				Analysis Year		2022	
Signalized/Unsignalized	Unsignalized							
Input Data					Existing Conditions		HSM Base Conditions	
Intersection type (3ST, 4ST, 4SG)					4ST			
AADT <sub>major</sub> (veh/day)		AADT <sub>MAX</sub> =	14,700	(veh/day)		8,670		
AADT <sub>minor</sub> (veh/day)		AADT <sub>MAX</sub> =	3,500	(veh/day)		650		
Intersection skew angle (degrees) Skew Angle Help Does skew differ for minor legs? Else, No. Yes			Skew for Leg 1 (All): 20	Skew for Leg 2 (4ST only)	20	0		
Number of uncontrolled approaches	with a left-turn lane	(0, 1, 2, 3, 4)			0		0	
Number of uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4)				0		0		
Intersection lighting (present/not present)				Present		Not Present		
Calibration Factor, C <sub>i</sub>				1.01		1.00		
Locality:						State System		

Existing Conditions: Crash Modification Factors (CMFs) for Rural Two-Lane Two-Way Intersection						
(1)	(2)	(3)	(4)	(5)		
CMF for Intersection Skew Angle	CMF for Left-Turn Lanes	CMF for Right-Turn Lanes	CMF for Lighting	Combined CMF		
CMF 1i	CMF 2i	CMF 3i	CMF <sub>4i</sub>	CMF COMB		
from Equations 10-22 or 10-23	from Table 10-13	from Table 10-14	from Equation 10-24	(1)*(2)*(3)*(4)		
1,1140	1.0000	1.0000	0.9996	1,1136		

Existing Conditions: Predicted Crash Summary for Rural Two-Lane Two-Way Intersection							
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Croch Soverity Lovel	N spf 3ST, 4ST or 4SG	Overdispersion	Crash Severity	N spf 3ST, 4ST or 4SG by Severity	Combined		Predicted average crash frequency,
		Parameter, k	Distribution	Distribution	CMFs	Calibration Factor, C <sub>i</sub>	N predicted int
Clash Seventy Level	from Equations 10-8, 10-9, or 10-	from Section	from Section from Table (2)	(2) * (4)	from (5) of		(5)*(6)*(7)
	10	10.6.2	10-5	(Z)TOTAL (4)	Worksheet 2B		
Total	2.297	0.24	1.000	2.297	1.11	1.01	2.583
Fatal and Injury (FI)		-	0.367	0.844	1.11	1.01	0.949
Property Damage Only (PDO)			0.633	1.453	1.11	1.01	1.634

Existing Conditions: General Information and Data for Rural Two-Lane Two-Way Intersection								
General Information					Location Information			
Analyst	GMB				Route		SR43	
Agency or Company	Carpenter Marty Tr	ransportation			Logpoint		3.868	
Date Performed	10/28/24				Common Name		SR-43 @ Trares R	oad
Intersection	SR43; 3.868				Analysis Year		2022	
Signalized/Unsignalized	Unsignalized							
Input Data					Existing Conditions		HSM Base Conditions	
Intersection type (3ST, 4ST, 4SG)	_				4ST		-	
AADT <sub>major</sub> (veh/day)		AADT <sub>MAX</sub> =	14,700	(veh/day)		8,510		-
AADT <sub>minor</sub> (veh/day)		AADT <sub>MAX</sub> =	3,500	(veh/day)		1,450		
Intersection skew angle (degrees) Skew Angle Help	Does skew differ fo	or minor legs? Else,	No.	Yes	Skew for Leg 1 (All):	Skew for Leg 2 (4ST only):	0	0
Number of uncontrolled approaches	with a left-turn lane	(0, 1, 2, 3, 4)			0		0	
Number of uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4)					0		0	
Intersection lighting (present/not present)				Present		Not Present		
Calibration Factor, C <sub>i</sub>				1.01		1.00		
Locality:						State System		

Existing Conditions: Crash Modification Factors (CMFs) for Rural Two-Lane Two-Way Intersection						
(1) CME for Intersection Skew Angle	(2) CME for Left-Turn Lanes	(3) CME for Right-Turn Lanes	(4) CME for Lighting	(5) Combined CME		
CMF 1i	CMF <sub>2i</sub>	CMF 3i	CMF 4i	CMF COMB		
from Equations 10-22 or 10-23	from Table 10-13	from Table 10-14	from Equation 10-24	(1)*(2)*(3)*(4)		
1.0000	1.0000	1.0000	0.9996	0.9996		

Existing Conditions: Predicted Crash Summary for Rural Two-Lane Two-Way Intersection								
(1)	(1) (2) (3) (4) (5) (6) (7) (8)							
Creek Severity Level	N spf 3ST, 4ST or 4SG	Overdispersion	Crash Severity	N spf 3ST, 4ST or 4SG by Severity	Combined		Predicted average crash frequency,	
		Parameter, k	Distribution	Distribution	CMFs	Calibration Eactor C	N predicted int	
Crash Seventy Lever	from Equations 10-8, 10-9, or 10-	from Section	from Table	(2) * (4)	from (5) of	(5)*(6)*(7)		
	10	10.6.2	10-5	(2)TOTAL (4)	Worksheet 2B		(3) (0) (7)	
Total	3.705	0.24	1.000	3.705	1.00	1.01	3.741	
Fatal and Injury (FI)			0.367	1.361	1.00	1.01	1.374	
Property Damage Only (PDO)			0.633	2.344	1.00	1.01	2.366	

	eneral Infor	mation and	d Data for Ru	ral Two-La	ne Two-Wa	y Roadway S	egment		
General Information					Location Information				
Analyst	GMB				Route			SR43	
Agency or Company	Carpenter Mart	y Transportation			Logpoints			3.868 to 3.936	
Date Performed	10/28/24				Common Name	e		SR-43 (Clevela	and Canton Road)
Segment for Analysis	SR43; 3.868-3.	936			Analysis Year			2022	
Input Data						Existing (	Conditions		HSM Base Conditions
Length of segment, L (mi)						0.0	068		
AADT (veh/day)		AADT <sub>MAX</sub> =	17,800 (v	eh/day)		8,2	210		
Lane width (ft)						1	1		12
Shoulder width (ft)					Right Shld:	5	Left Shld:	5	6
Shoulder type					Right Shld:	Paved	Left Shld:	Paved	Paved
Length of horizontal curve (mi)					0.0			0	
Radius of curvature (ft)					0				0
Spiral transition curve (present/r	not present)				Not Present			Not Present	
Superelevation variance (ft/ft)					0			< 0.01	
Grade (%)					4.7			0	
Driveway density (driveways/mil	le)					16.24	616184		5
Centerline rumble strips (presen	nt/not present)				Not Present			Not Present	
Passing lanes [present (1 lane)	/present (2 lane	) / not present)]				Not P	resent		Not Present
Two-way left-turn lane (present/not present)						Not P	resent		Not Present
Roadside hazard rating (1-7 scale)							4		3
Segment lighting (present/not present)					Not Present			Not Present	
Auto speed enforcement (present/not present)				Not Present			Not Present		
Calibration Factor, Cr						1.	20		1
Locality:						State	System		

ECAT	Project Inform	ation						
Economic Crash Analysis Tool	General Information							
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com					
Project Description	SR-43 Safety Study: Alt 1	Contact Phone	614-656-2429					
Reference Number	ODOT PID 1147572	Date Performed	2/6/2025					
Analyst	GMB	Analysis Year	2022					
Agency/Company	Carpenter Marty Transportation							
Perform Benefit Cost Analysis?	Yes							
Do the proposed improvements fundamentally change the conditions of the base safety performance function (SDE)								

Or is crash data unavailable for the analysis condition, Or is only predicted (and not expected) analysis needed for the existing or proposed condition?

(Examples: unsignalized to signalized, undivided to divided, increase or decrease in the number of lanes, change the number of approaches to an intersection, significant realignment of the roadway)

If Yes, are you analyzing the existing or proposed conditions?

Proposed

Yes

Project Elements Description Table								
			Location Information					
Project Element ID (Must be Unique)	Site Type	Intersection Control Type	NLFID         Begin Logpoint/ Intersection Midpoint         End Logpoint (Leave blank for Intersection)         Length (mi) OR Intersection Radius Buffer (mi)         Cross Route NLFID(s)         Common Name					
SR43; 3.868-3.936	Rural Two-Lane Two Way Segment		SPORSR00043**C	3.868	3.936	0.068		SR-43 (Cleveland Canton Road)
SR43; 3.868	Roundabout	Unsignalized	SPORSR00043**C	3.868		0.05	CPORCR0002	SR-43 @ Trares Road
SR43; 3.936	Roundabout	Unsignalized	SPORSR00043**C	3.936		0.05	CPORCR0001	SR-43 @ Randolph Road

Traffic Volume Growth Rate Calculation For Benefit Cost Analysis							
	Year	AADT					
Present ADT (PADT)			veh / day				
Future ADT (FADT)			veh / day				
Annual Linear Growth Rate		0.0025					

ECAT	Project Safety Performance Report								
Economic Crash Analysis Tool	General								
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com						
Project Description	SR-43 Safety Study: Alt 1	Contact Phone	614-656-2429						
Reference Number	ODOT PID 1147572	Date Performed	2/6/2025						
Analyst	GMB	Analysis Year	2022						
Agency/Company	Carpenter Marty Transportation								



Project Summary Results (Without Animal Crashes)												
KA B C O Total												
N <sub>predicted</sub> - Existing Conditions	0.4736	1.1505	0.7602	4.0919	6.4762							
N <sub>expected</sub> - Existing Conditions	0.5335	1.2954	0.8573	3.8484	6.5346							
$\mathbf{N}_{\text{potential for improvement}}$ - Existing Conditions	0.0599	0.1449	0.0971	-0.2435	0.0584							
N <sub>expected</sub> - Proposed Conditions	0.0255	0.1416	0.1510	2.8440	3.1621							





ECAT	Project Safety Performance Report									
Economic Crash Analysis Tool	General									
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com							
Project Description	SR-43 Safety Study: Alt 1	Contact Phone	614-656-2429							
Reference Number	ODOT PID 1147572	Date Performed	2/6/2025							
Analyst	GMB	Analysis Year	2022							
Agency/Company	Carpenter Marty Transportation									

Existing Conditions Project Element Predicted Crash Summary (Without Animal Crashes)											
Project Element ID	Common Nomo			Crash Severity Level							
	Common Name	KA	В	C	0	Total					
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	0.0125	0.0325	0.0158	0.0912	0.152					
SR43; 3.868	SR-43 @ Trares Road	0.2727	0.6613	0.4404	2.3665	3.7409					
<u>SR43; 3.936</u>	SR-43 @ Randolph Road	0.1884	0.4567	0.304	1.6342	2.5833					

Existing Conditions Project Element Expected Crash Summary (Without Animal Crashes)											
Project Element ID	Common Nama		Crash Severity Level								
Project Element ID	Common Name	KA	В	С	0	Total					
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	0.0102	0.0268	0.0125	0.0546	0.1041					
SR43; 3.868	SR-43 @ Trares Road	0.3036	0.7359	0.4901	1.9438	3.4734					
<u>SR43; 3.936</u>	SR-43 @ Randolph Road	0.2197	0.5327	0.3547	1.85	2.9571					

Existing Conditions Project Element Potential for Safety Improvement Summary (Without Animal Crashes)											
Droject Floment ID	Common Nomo			Crash Severity Level							
Project Element ID	Common Name	KA	В	C	0	Total					
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	-0.0023	-0.0057	-0.0033	-0.0366	-0.0479					
SR43; 3.868	SR-43 @ Trares Road	0.0309	0.0746	0.0497	-0.4227	-0.2675					
SR43; 3.936	SR-43 @ Randolph Road	0.0313	0.076	0.0507	0.2158	0.3738					

Proposed Conditions Project Element Predicted Crash Summary (Without Animal Crashes)											
Droject Element ID	Common Nomo	Crash Severity Level									
Project Element ID	Common Name	KA	В	C	0	Total					
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	0.0125	0.0325	0.0158	0.0912	0.152					
SR43; 3.868	SR-43 @ Trares Road	0.007	0.0581	0.0719	1.4653	1.6023					
SR43; 3.936	SR-43 @ Randolph Road	0.006	0.051	0.0633	1.2875	1.4078					

	Sum	mary by Crash	Туре	
		Existing		Proposed
Crash Type	Predicted Crash Frequency	Expected Crash Frequency	PSI	Predicted Crash Frequency
Unknown	0.0325	0.0306	-0.0019	0.0864
Head On	0.0716	0.0709	-0.0007	0.0040
Rear End	1.7720	1.6568	-0.1152	0.4859
Backing	0.3309	0.2953	-0.0356	0.0300
Sideswipe - Meeting	0.2481	0.2341	-0.0140	0.0108
Sideswipe - Passing	0.3768	0.3463	-0.0305	0.9529
Angle	3.1254	3.0244	-0.1010	0.8574
Parked Vehicle	0.2925	0.2639	-0.0286	0.0018
Pedestrian	0.0406	0.0416	0.0010	0.0034
Animal	0.1063	0.0645	-0.0418	0.1367
Train	0.0014	0.0014	0.0000	0.0000
Pedalcycles	0.0304	0.0307	0.0003	0.0030
Other Non-Vehicle	0.0006	0.0007	0.0001	0.0000
Fixed Object	1.4494	1.3343	-0.1151	0.3832
Other Object	0.0510	0.0452	-0.0058	0.0033
Overturning	0.0892	0.0865	-0.0027	0.0090
Other Non-Collision	0.1125	0.1017	-0.0108	0.0624
Left Turn	0.2999	0.2888	-0.0111	0.0690
Right Turn	0.0000	0.0000	0.0000	0.2053



	Propose	d Conditions: (	General Infor	mation an	nd Data for Rural Two-Lane Two-Way Roadway Segment						
General Information					Location Information						
Analyst	GMB				Route			SR43			
Agency or Company	Carpenter Mart	y Transportation			Logpoints			3.868 to 3.936			
Date Performed	02/06/25				Common Name	e		SR-43 (Clevela	and Canton Road)		
Segment for Analysis	SR43; 3.868-3.	936			Analysis Year			2022			
Input Data				Proposed	Conditions		HSM Base Conditions				
Length of segment, L (mi)			0.0	068							
AADT (veh/day)		AADT <sub>MAX</sub> =	17,800 (v	eh/day)		8,2	210		-		
Lane width (ft)						1	1		12		
Shoulder width (ft)					Right Shld:	5	Left Shld:	5	6		
Shoulder type					Right Shld:	Paved	Left Shld:	Paved	Paved		
Length of horizontal curve (mi)						0	.0		0		
Radius of curvature (ft)							0	0			
Spiral transition curve (present/	not present)					Not P	resent	Not Present			
Superelevation variance (ft/ft)							0	< 0.01			
Grade (%)						4	.7		0		
Driveway density (driveways/mi	ile)					16.246	616184		5		
Centerline rumble strips (preser	nt/not present)					Not P	resent		Not Present		
Passing lanes [present (1 lane)	/present (2 lane	) / not present)]				Not P	resent		Not Present		
Two-way left-turn lane (present/	/not present)					Not P	resent		Not Present		
Roadside hazard rating (1-7 sca	ale)						4		3		
Segment lighting (present/not p	resent)					Not P	resent		Not Present		
Auto speed enforcement (prese	ent/not present)					Not P	resent		Not Present		
Calibration Factor, Cr						1.	20		1		
Locality:						State	System				

	Proposed Conditions: Crash Modification Factors (CMFs) for Rural Two-Lane Two-Way Roadway Segment													
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)		
CMF for Lane Width	CMF for Shoulder Width and Type	CMF for Horizontal Curves	CMF for Super- elevation	CMF for Grades	CMF for Driveway Density	CMF for Centerline Rumble Strips	CMF for Passing Lanes	CMF for Two- Way Left-Turn Lane	CMF for Roadside Design	CMF for Lighting	CMF for Automated Speed Enforcement	Combined CMF		
CMF 1r	CMF 2r	CMF 3r	CMF 4r	CMR 5r	CMF 6r	CMF 7r	CMF 8r	CMF 9r	CMF 10r	CMF 11r	CMF 12r	CMF comb		
from Equation 10-11	from Equation 10-12	from Equation 10-13	from Equations 10- 14, 10-15, or 10-16	from Table 10- 11	from Equation 10-17	from Section 10.7.1	from Section 10.7.1	from Equation 10-18 & 10-19	from Equation 10-20	from Equation 10-21	from Section 10.7.1	(1)x(2)x x(11)x(12)		
1.0195	1.0312	1.0000	1.0000	1.1000	1.1601	1.0000	1.0000	1.0000	1.0691	1.0000	1.0000	1.4341		

Proposed Conditions: Predicted Crash Summary for Rural Two-Lane Two-Way Roadway Segment												
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)					
Crash Severity Level	N spf rs	Overdispersion Parameter, k	Crash Severity Distribution	N spf rs by Severity Distribution	Combined CMFs	Calibration Factor, Cr	Predicted average crash frequency, N predicted rs (crashes/year)					
Crash Severity Level	from Equation 10-6	from Equation 10-7	from Table 10-3 (proportion)	(2)total x (4)	(13) from Worksheet 1B		(5)x(6)x(7)					
Total	0.1492	3.4706	1.0000	0.1492	1.4341	1.2000	0.256696					
Fatal and Injury (FI)			0.2549	0.0380	1.4341	1.2000	0.065432					
Property Damage Only (PDO)			0.7451	0.1111	1.4341	1.2000	0.191264					

		Propos	sed Condi	itions: Genera	al Information and I	Data for Roundabout Inte	rsection		
	General Info	mation					Location Informati	on	
Analyst	GMB				Route		SR43		
Agency or Compar	ny Carpenter Mar	ty Transportation			Logpoint		3.868		
Date Performed	02/06/25				Common Name		SR-43 @ Trares Ro	Road	
Intersection	SR43; 3.868				Analysis Year		2022		
Signalized/Unsigna	alized Unsignalized	ato.				Proposed Conditions	L	HSM Page Conditions	
Area Type (Rural, I	Urban)	ita				Rural			
Number of Legs (3	3 or 4)					4			
Single-Lane or Mul	lti-lane Roundabout					Single-Lane			
Total Entering AAD	DT (veh/day)					9,960		-	
								0	
Presence of Outbound Only Leg (present/not present)						Not Present		Not Present	
Calibration Factor,	Calibration Factor, C <sub>i</sub>					Varies, See Below		1.00	
Locality:						State System			
	Leg 1 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		4,470			
	Bypass lane (present/not present)	Bypass lane (present/not present) - Leg 1				Not Present			
Leg 1 Ni	Number of driveways or unsignaliz	ed access points - L	.eg 1			1		-	
	Entry width (feet) - Leg 1	eet) - Leg 1				23		16-25 ft	
	Number of entering lanes (1 lane,	2 lanes) - Leg 1			1		-		
	Leg 2 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		350			
	Bypass lane (present/not present)	- Leg 2				Not Present			
Leg 2	Number of driveways or unsignaliz	ed access points - L	eg 2			1			
	Entry width (feet) - Leg 2					23		16-25 ft	
	Number of entering lanes (1 lane,	2 lanes) - Leg 2				1		-	
	Leg 3 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		4,040			
	Bypass lane (present/not present)	- Leg 3				Not Present			
Leg 3	Number of driveways or unsignaliz	ed access points - L	eg 3			1			
	Entry width (feet) - Leg 3					21		16-25 ft	
	Number of entering lanes (1 lane,	2 lanes) - Leg 3				1			
	Leg 4 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		1,100			
	Bypass lane (present/not present)	- Leg 4				Not Present		-	
Leg 4	Number of driveways or unsignaliz	ed access points - L	eg 4		1				
	Entry width (feet) - Leg 4					23		16-25 ft	
	Number of entering lanes (1 lane,	2 lanes) - Leg 4				1			

Proposed Conditions: Crash Modification Factors (CMFs) for Roundabout Intersection											
Crash Severity	Inscribed Circle	Outbound Only			Leg CMFs			Combined CME			
Level	CMF	Leg CMF	Leg 1 CMF	Leg 2 CMF	Leg 3 CMF	Leg 4 CMF	Total CMF Legs	Combined CIVIF			
Fatal and Injury (FI)	1.00	0.43	1.07	1.07	1.07	1.07	1.07	0.46			
Property Damage Only (PDO)	1.00	1.00	1.09	1.09	1.09	1.09	1.09	1.09			

Proposed Conditions: Predicted Crash Summary for Roundabout Intersection									
(1)		(2)		(3)	(4)	(5)	(6)	(7)	
Crash Severity Level	SI	PF Coefficient	efficients N spf int		Overdispersion Parameter, k	Combined CMFs	Calibration	Predicted average crash frequency,	
orasin ocvernty Lever	from Table 11-7 or 11-8				from (6) of	Factor, C <sub>i</sub>	- · predicted inc		
	а	b	С	from Equation 11-11 or 11-12	from Table 11-7 or 11-8	Worksheet 2B		(3)*(5)*(6)	
Total								1.618	
Fatal and Injury (FI)	-3.503	0.915	0.206	0.303	0.33	0.46	1.00	0.138	
Property Damage Only (PDO)	-1.475	0.702	0.168	1.36	0.80	1.09	1.00	1.480	

		Propos	sed Condi	itions: Genera	al Information and	Data for Roundabout Inte	ersection		
	General Infor	mation					Location Informati	on	
Analyst	GMB				Route		SR43		
Agency or Compar	ny Carpenter Mart	y Transportation			Logpoint		3.936		
Date Performed	02/06/25				Common Name		SR-43 @ Randolph	Road	
Intersection	SR43; 3.936				Analysis Year		2022		
Signalized/Unsigna	alized Unsignalized	<b>1</b> -				Drenses d Conditions		USM Pass Canditians	
Area Type (Rural,	Urban)	ld				Rural			
Number of Legs (3	3 or 4)					4			
Single-Lane or Mu	Iti-lane Roundabout					Single-Lane		-	
Total Entering AAD	DT (veh/day)					9,320			
								0	
Presence of Outbo	ound Only Leg (present/not present)					Not Present		Not Present	
Calibration Factor,	, C <sub>i</sub>					Varies, See Below		1.00	
Locality:		-				State System			
	Leg 1 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		4,170			
	Bypass lane (present/not present) - Leg 1			Not Present					
Leg 1	Number of driveways or unsignalized access points - Leg 1				0				
	Entry width (feet) - Leg 1				23		16-25 ft		
	Number of entering lanes (1 lane, 2	lanes) - Leg 1			1			-	
	Leg 2 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)	360				
	Bypass lane (present/not present)	Leg 2				Not Present			
Leg 2	Number of driveways or unsignalize	ed access points - L	.eg 2			0			
	Entry width (feet) - Leg 2					27		16-25 ft	
	Number of entering lanes (1 lane, 2	lanes) - Leg 2				1			
	Leg 3 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		4,500			
	Bypass lane (present/not present)	Leg 3				Not Present			
Leg 3	Number of driveways or unsignalize	ed access points - L	eg 3			0			
	Entry width (feet) - Leg 3			24		16-25 ft			
	Number of entering lanes (1 lane, 2	lanes) - Leg 3				1			
	Leg 4 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		290			
	Bypass lane (present/not present)	Leg 4				Not Present			
Leg 4	Number of driveways or unsignalize	ed access points - L	eg 4			1		-	
	Entry width (feet) - Leg 4					23		16-25 ft	
	Number of entering lanes (1 lane, 2	lanes) - Leg 4				1			

Proposed Conditions: Crash Modification Factors (CMFs) for Roundabout Intersection								
Crash Severity	Inscribed Circle	Outbound Only			Leg CMFs			Combined CMF
Level	CMF	Leg CMF	Leg 1 CMF	Leg 2 CMF	Leg 3 CMF	Leg 4 CMF	Total CMF Legs	Combined CMF
Fatal and Injury (FI)	1.00	0.43	1.00	1.00	1.00	1.07	1.00	0.43
Property Damage Only (PDO)	1.00	1.00	1.00	1.00	1.00	1.09	1.00	1.00

Proposed Conditions: Predicted Crash Summary for Roundabout Intersection									
(1)		(2)		(3)	(4)	(5)	(6)	(7)	
Crash Severity Level	SPF Coefficients		N spf int	N spf int Overdispersion Parameter, k		Calibration	Predicted average crash frequency,		
orasir ocverny Lever	from Table 11-7 or 11-8				from (6) of	Factor, C <sub>i</sub>	predicted int		
	а	b	С	from Equation 11-11 or 11-12	from Table 11-7 or 11-8	Worksheet 2B		(3)*(5)*(6)	
Total			-					1.422	
Fatal and Injury (FI)	-3.503	0.915	0.206	0.285	0.33	0.43	1.00	0.122	
Property Damage Only (PDO)	-1.475	0.702	0.168	1.30	0.80	1.00	1.00	1.301	

ECAT	Project Informati	on					
Economic Crash Analysis Tool	General Information						
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com				
Project Description	SR-43 Safety Study: Alt 2	Contact Phone	614-656-2429				
Reference Number	ODOT PID 1147572	Date Performed	10/28/2024				
Analyst	GMB	Analysis Year	2022				
Agency/Company	Carpenter Marty Transportation						
Perform Benefit Cost Analysis?	Yes						
Do the proposed im	Do the proposed improvements fundamentally change the conditions of the base safety performance function (SPF).						

Or is crash data unavailable for the analysis condition, Or is only predicted (and not expected) analysis needed for the existing or proposed condition?

Yes

(Examples: unsignalized to signalized, undivided to divided, increase or decrease in the number of lanes, change the number of approaches to an intersection, significant realignment of the roadway)

If Yes, are you analyzing the existing or proposed conditions?

Proposed

Project Elements Description Table								
			Location Information					
Project Element ID (Must be Unique)	Site Type	Intersection Control Type	NLFID	Begin Logpoint/ Intersection Midpoint	End Logpoint (Leave blank for Intersection)	Length (mi) OR Intersection Radius Buffer (mi)	Cross Route NLFID(s)	Common Name
SR43; 3.868-3.936	Rural Two-Lane Two Way Segment		SPORSR00043**C	3.868	3.936	0.068		SR-43 (Cleveland Canton Road)
SR43; 3.868	Roundabout	Unsignalized	SPORSR00043**C	3.868		0.05	CPORCR0002	SR-43 @ Trares Road
SR43; 3.936	Rural Two-Lane Two Way Intersection	Unsignalized	SPORSR00043**C	3.936		0.05	CPORCR0001	SR-43 @ Randolph Road

Traffic Volume Growth Rate C	alculation For Bene	efit Cost Analysis	5
	Year	AADT	
Present ADT (PADT)			veh / day
Future ADT (FADT)			veh / day
Annual Linear Growth Rate		0.0025	

	Select Other Non-Site Characteristic Based Countermeasures For Entire Project						
CMF Nbr	Countermeasure	CMF KA Value	CMF B Value	CMF C Value	CMF O Value	CMF Valid for the Following Site Types	
CMF 1	Install right-in-right-out (RIRO) operations at stop-controlled intersections	0.2	0.32	0.32	0.32	2	



ECAT	Project Safety P	Project Safety Performance Report					
Economic Crash Analysis Tool	Genera	I Information					
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com				
Project Description	SR-43 Safety Study: Alt 2	Contact Phone	614-656-2429				
Reference Number	ODOT PID 1147572	Date Performed	10/28/2024				
Analyst	GMB	Analysis Year	2022				
Agency/Company	Carpenter Marty Transportation						



Project Summary Results (Without Animal Crashes)								
	KA	В	C	0	Total			
N <sub>predicted</sub> - Existing Conditions	0.4736	1.1505	0.7602	4.0919	6.4762			
N <sub>expected</sub> - Existing Conditions	0.5335	1.2954	0.8573	3.8484	6.5346			
$\mathbf{N}_{\text{potential for improvement}}$ - Existing Conditions	0.0599	0.1449	0.0971	-0.2435	0.0584			
N <sub>expected</sub> - Proposed Conditions	0.0352	0.1524	0.1300	1.8350	2.1526			



ECAT	Project Safety P	Project Safety Performance Report					
Economic Crash Analysis Tool	Genera	Information					
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com				
Project Description	SR-43 Safety Study: Alt 2	Contact Phone	614-656-2429				
Reference Number	ODOT PID 1147572	Date Performed	10/28/2024				
Analyst	GMB	Analysis Year	2022				
Agency/Company	Carpenter Marty Transportation						

	Existing Conditions Project Element Predicted Crash Summary (Without Animal Crashes)								
Project Element ID	Common Nomo		Crash Severity Level						
	Common Name	KA	В	C	0	Total			
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	0.0125	0.0325	0.0158	0.0912	0.152			
SR43; 3.868	SR-43 @ Trares Road	0.2727	0.6613	0.4404	2.3665	3.7409			
SR43; 3.936	SR-43 @ Randolph Road	0.1884	0.4567	0.304	1.6342	2.5833			

Existing Conditions Project Element Expected Crash Summary (Without Animal Crashes)									
Project Element ID	Common Nama	Crash Severity Level	Severity Level						
Project Element ID	Common Name	KA	В	С	0	Total			
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	0.0102	0.0268	0.0125	0.0546	0.1041			
SR43; 3.868	SR-43 @ Trares Road	0.3036	0.7359	0.4901	1.9438	3.4734			
<u>SR43; 3.936</u>	SR-43 @ Randolph Road	0.2197	0.5327	0.3547	1.85	2.9571			

Existing Conditions Project Element Potential for Safety Improvement Summary (Without Animal Crashes)										
Droject Element ID	Common Nomo		Crash Severity Level							
Project Element ID	Common Name	KA	В	C	0	Total				
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	-0.0023	-0.0057	-0.0033	-0.0366	-0.0479				
SR43; 3.868	SR-43 @ Trares Road	0.0309	0.0746	0.0497	-0.4227	-0.2675				
SR43; 3.936	SR-43 @ Randolph Road	0.0313	0.076	0.0507	0.2158	0.3738				

Proposed Conditions Project Element Predicted Crash Summary (Without Animal Crashes)										
Project Element ID	Common Namo	Crash Severity Level								
Project Element ID	Common Name	KA	В	С	0	Total				
SR43; 3.868-3.936	SR-43 (Cleveland Canton Road)	0.0133	0.0343	0.0162	0.0955	0.1593				
SR43; 3.868	SR-43 @ Trares Road	0.0074	0.0618	0.0763	1.5379	1.6834				
SR43; 3.936	SR-43 @ Randolph Road	0.0145	0.0563	0.0375	0.2016	0.3099				

Summary by Crash Type											
		Proposed									
Crash Type	Predicted Crash Frequency Frequency		PSI	Predicted Crash Frequency							
Unknown	0.0325	0.0306	-0.0019	0.0528							
Head On	0.0716	0.0709	-0.0007	0.0155							
Rear End	1.7720	1.6568	-0.1152	0.6137							
Backing	0.3309	0.2953	-0.0356	0.0818							
Sideswipe - Meeting	0.2481	0.2341	-0.0140	0.0554							
Sideswipe - Passing	0.3768	0.3463	-0.0305	0.5883							
Angle	3.1254	3.0244	-0.1010	1.0531							
Parked Vehicle	0.2925	0.2639	-0.0286	0.0587							
Pedestrian	0.0406	0.0416	0.0010	0.0092							
Animal	0.1063	0.0645	-0.0418	0.1227							
Train	0.0014	0.0014	0.0000	0.0003							
Pedalcycles	0.0304	0.0307	0.0003	0.0073							
Other Non-Vehicle	0.0006	0.0007	0.0001	0.0001							
Fixed Object	1.4494	1.3343	-0.1151	0.5067							
Other Object	0.0510	0.0452	-0.0058	0.0126							
Overturning	0.0892	0.0865	-0.0027	0.0230							
Other Non-Collision	0.1125	0.1017	-0.0108	0.0565							
Left Turn	0.2999	0.2888	-0.0111	0.0945							
Right Turn	0.0000	0.0000	0.0000	0.1106							



	Proposed	d Conditions: 0	General Information a	nd Data for R	ural Two-La	ane Two-Wa	y Roadway	Segment
General Information		Location Information						
Analyst	Analyst GMB						SR43	
Agency or Company	Carpenter Mart	y Transportation		Logpoints			3.868 to 3.936	
Date Performed	10/28/24			Common Name	e		SR-43 (Clevela	and Canton Road)
Segment for Analysis	SR43; 3.868-3.	936		Analysis Year			2022	
Input Data					Proposed	Conditions		HSM Base Conditions
Length of segment, L (mi)					0.0	068		
AADT (veh/day)		AADT <sub>MAX</sub> =	17,800 (veh/day)		8,6	670		
Lane width (ft)					1	1		12
Shoulder width (ft)				Right Shld:	5	Left Shld:	5	6
Shoulder type				Right Shld:	Paved	Left Shld:	Paved	Paved
Length of horizontal curve (mi)					0	.0		0
Radius of curvature (ft)				0			0	
Spiral transition curve (present/	not present)				Not Present			Not Present
Superelevation variance (ft/ft)						0		< 0.01
Grade (%)					4.7			0
Driveway density (driveways/mi	le)				16.246	616184		5
Centerline rumble strips (preser	nt/not present)				Not P	resent		Not Present
Passing lanes [present (1 lane)	/present (2 lane	) / not present)]			Not P	resent		Not Present
Two-way left-turn lane (present/			Not P	resent		Not Present		
Roadside hazard rating (1-7 sca				4		3		
Segment lighting (present/not p	resent)				Not Present			Not Present
Auto speed enforcement (prese	nt/not present)				Not P	resent		Not Present
Calibration Factor, Cr					1.	20		1
Locality:					State	System		

Proposed Conditions: Crash Modification Factors (CMFs) for Rural Two-Lane Two-Way Roadway Segment												
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)
CMF for Lane Width	CMF for Shoulder Width and Type	CMF for Horizontal Curves	CMF for Super- elevation	CMF for Grades	CMF for Driveway Density	CMF for Centerline Rumble Strips	CMF for Passing Lanes	CMF for Two- Way Left-Turn Lane	CMF for Roadside Design	CMF for Lighting	CMF for Automated Speed Enforcement	Combined CMF
CMF 1r	CMF 2r	CMF 3r	CMF 4r	CMR 5r	CMF 6r	CMF 7r	CMF 8r	CMF 9r	CMF 10r	CMF 11r	CMF 12r	CMF comb
from Equation 10-11	from Equation 10-12	from Equation 10-13	from Equations 10- 14, 10-15, or 10-16	from Table 10- 11	from Equation 10-17	from Section 10.7.1	from Section 10.7.1	from Equation 10-18 & 10-19	from Equation 10-20	from Equation 10-21	from Section 10.7.1	(1)x(2)x x(11)x(12)
1.0195	1.0312	1.0000	1.0000	1.1000	1.1518	1.0000	1.0000	1.0000	1.0691	1.0000	1.0000	1.4239

Proposed Conditions: Predicted Crash Summary for Rural Two-Lane Two-Way Roadway Segment										
(1)	(2)	(2) (3) (4) (5) (6) (7) (8)								
Crash Severity Level	N spf rs	Overdispersion Parameter, k	Crash Severity Distribution	N spf rs by Severity Distribution	Combined CMFs	Calibration Factor, Cr	Predicted average crash frequency, N predicted rs (crashes/year)			
Clash Seventy Level	from Equation 10-6	from Equation 10-7	from Table 10-3 (proportion)	(2)total x (4)	(13) from Worksheet 1B		(5)x(6)x(7)			
Total	0.1575	3.4706	1.0000	0.1575	1.4239	1.2000	0.269151			
Fatal and Injury (FI)			0.2549	0.0402	1.4239	1.2000	0.068606			
Property Damage Only (PDO)			0.7451	0.1174	1.4239	1.2000	0.200545			

		Propos	sed Condi	tions: Genera	al Information and	Data for Roundabout Inte	rsection		
	General Infor	mation					Location Information	on	
Analyst	GMB				Route		SR43		
Agency or Compar	ny Carpenter Mart	y Transportation			Logpoint		3.868		
Date Performed	10/28/24				Common Name SR-43 @ Trares R			load	
Intersection	SR43; 3.868				Analysis Year		2022		
Signalized/Unsigna	alized Unsignalized	<b>1</b> 0				Drenses d Conditions		USM Deep Conditions	
Area Type (Rural,	Urban)	ld			Proposed Conditions				
Number of Legs (3	3 or 4)					4			
Single-Lane or Multi-lane Roundabout						Single-Lane			
Total Entering AADT (veh/day)						10,670			
								0	
Presence of Outbound Only Leg (present/not present)						Not Present		Not Present	
Calibration Factor, C <sub>i</sub>						Varies, See Below		1.00	
Locality:		-				State System			
	Leg 1 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		4,570			
	Bypass lane (present/not present) - Leg 1				Not Present				
Leg 1	Number of driveways or unsignalized access points - Leg 1				1				
	Entry width (feet) - Leg 1				23			16-25 ft	
	Number of entering lanes (1 lane, 2	lanes) - Leg 1			1				
	Leg 2 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		350			
	Bypass lane (present/not present) -	Leg 2				Not Present		-	
Leg 2	Number of driveways or unsignalize	ed access points - L	.eg 2			1			
	Entry width (feet) - Leg 2					23		16-25 ft	
	Number of entering lanes (1 lane, 2	lanes) - Leg 2				1		-	
	Leg 3 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		4,120			
	Bypass lane (present/not present) -	Leg 3				Not Present		-	
Leg 3	Number of driveways or unsignalize	ed access points - L	.eg 3			1			
	Entry width (feet) - Leg 3					21		16-25 ft	
	Number of entering lanes (1 lane, 2 lanes) - Leg 3					1		-	
	Leg 4 Entering AADT (veh/day)	AADT <sub>MAX</sub> =	19,733	(veh/day)		1,110		-	
Bypass lane (present/not present) - Leg 4		Not Present							
Leg 4 Number of driveways or unsignalized access points - Leg 4			1						
	Entry width (feet) - Leg 4					23		16-25 ft	
	Number of entering lanes (1 lane, 2	lanes) - Leg 4				1			

	Proposed Conditions: Crash Modification Factors (CMFs) for Roundabout Intersection										
Crash Severity	Inscribed Circle	Outbound Only			Leg CMFs			Combined CMF			
Level	CMF	Leg CMF	Leg 1 CMF	Leg 2 CMF	Leg 3 CMF	Leg 4 CMF	Total CMF Legs	Combined CMF			
Fatal and Injury (FI)	1.00	0.43	1.07	1.07	1.07	1.07	1.07	0.46			
Property Damage Only (PDO)	1.00	1.00	1.09	1.09	1.09	1.09	1.09	1.09			

Proposed Conditions: Predicted Crash Summary for Roundabout Intersection										
(1)		(2)		(3)	(4)	(5)	(6)	(7)		
Crash Severity Level	SPF Coefficients from Table 11-7 or 11-8			N spf int	Overdispersion Parameter, k	Combined CMFs	Calibration	Predicted average crash frequency,		
orash oeventy Leven						from (6) of Factor, C <sub>1</sub>		•• predicted int		
	a b c		from Equation 11-11 or 11-12	from Table 11-7 or 11-8	Worksheet 2B		(3)*(5)*(6)			
Total								1.700		
Fatal and Injury (FI)	-3.503	0.915	0.206	0.323	0.33	0.46	1.00	0.147		
Property Damage Only (PDO)	-1.475	0.702	0.168	1.43	0.80	1.09	1.00	1.553		

Proposed Conditions: General Information and Data for Rural Two-Lane Two-Way Intersection											
General Information					Location Information						
Analyst	GMB				Route		SR43				
Agency or Company	Carpenter Marty Tr	ransportation			Logpoint		3.936				
Date Performed	10/28/24				Common Name		SR-43 @ Randolp	h Road			
Intersection	SR43; 3.936				Analysis Year		2022				
Signalized/Unsignalized	Unsignalized										
Input Data					Proposed Conditions		HSM Base Conditions				
Intersection type (3ST, 4ST, 4SG)	-					4ST					
AADT <sub>major</sub> (veh/day)		AADT <sub>MAX</sub> =	14,700	(veh/day)	8,900						
AADT <sub>minor</sub> (veh/day)		AADT <sub>MAX</sub> =	3,500	(veh/day)	170						
Intersection skew angle (degrees) Skew Angle Help	Does skew differ fo	or minor legs? Else,	No.	Yes	Skew for Leg 1 (All): 20	Skew for Leg 2 (4ST only):	20	0			
Number of uncontrolled approaches	with a left-turn lane	(0, 1, 2, 3, 4)			0		0				
Number of uncontrolled approaches with a right-turn lane (0, 1, 2, 3, 4)					1		0				
Intersection lighting (present/not present)					Present		Not Present				
Calibration Factor, C <sub>i</sub>					1.01			1.00			
Locality:					Sta	te System					

Proposed Conditions: Crash Modification Factors (CMFs) for Rural Two-Lane Two-Way Intersection										
(1)	(2)	(3)	(4)	(5)						
CMF for Intersection Skew Angle	CMF for Left-Turn Lanes	CMF for Right-Turn Lanes	CMF for Lighting	Combined CMF						
CMF 1i	CMF 2i	CMF 3i	CMF <sub>4i</sub>	CMF COMB						
from Equations 10-22 or 10-23	from Table 10-13	from Table 10-14	from Equation 10-24	(1)*(2)*(3)*(4)						
1,1140	1.0000	0.8600	0.9996	0.9577						

Proposed Conditions: Predicted Crash Summary for Rural Two-Lane Two-Way Intersection							
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)
Crash Severity Level	N spf 3ST, 4ST or 4SG	Overdispersion	Crash Severity	N spf 3ST, 4ST or 4SG by Severity	Combined	Calibration Factor, C <sub>i</sub>	Predicted average crash frequency,
		Parameter, k	Distribution	Distribution	CMFs		N predicted int
	from Equations 10-8, 10-9, or 10-	from Section	from Table	(2) <sub>TOTAL</sub> * (4)	from (5) of		(5)*(6)*(7)
	10	10.6.2	10-5		Worksheet 2B		
Total	1.030	0.24	1.000	1.030	0.96	1.01	0.996
Fatal and Injury (FI)			0.367	0.378	0.96	1.01	0.366
Property Damage Only (PDO)			0.633	0.651	0.96	1.01	0.630
Proposed Conditions: Summary of Other CMFs (Without Animal Crashes)							
---	---	----------	---------	---------	---------	---------	
CMF Nbr	Countermeasure	KA Value	B Value	C Value	O Value	Total	
CMF 1	Install right-in-right-out (RIRO) operations at stop-controlled intersections	-0.0582	-0.1196	-0.0798	-0.4284	-0.6860	
		0.0000	0.0000	0.0000	0.0000	0.0000	
		0.0000	0.0000	0.0000	0.0000	0.0000	
		0.0000	0.0000	0.0000	0.0000	0.0000	
		0.0000	0.0000	0.0000	0.0000	0.0000	
		0.0000	0.0000	0.0000	0.0000	0.0000	
		0.0000	0.0000	0.0000	0.0000	0.0000	
		0.0000	0.0000	0.0000	0.0000	0.0000	
		0.0000	0.0000	0.0000	0.0000	0.0000	
		0.0000	0.0000	0.0000	0.0000	0.0000	
Total		-0.0582	-0.1196	-0.0798	-0.4284	-0.6860	



# **CMF / CRF Details**

CMF ID: 9822

CMF Name: Install right-in-right-out (RIRO) operations at stop-controlled interse

**Description:** 

**Prior Condition: No Prior Condition(s)** 

**Category: Access management** 

Study ID: <u>Safety Effects of Turning Movement Restrictions at Stop-Controlled</u> <u>Intersections, Le et al. 2018</u>

Star Quality Rating		
Star Quality Rating:	3 Stars	
Crash Modification Factor (CMF)		
Value:	0.32	
Adjusted Standard Error:		
Unadjusted Standard Error:	0.08	

Crash Reduction Factor		
Value:	68	
Adjusted Standard Error:		
Unadjusted Standard Error:	8	

Applicability		
Crash Type:	Other	
Crash Severity:	All	
Roadway Types:	Not specified	
Minimum Number of Lanes:	4	
Maximum Number of Lanes:	6	
Number of Lanes Direction:		
Number of Lanes Comment:	4 and 6 Lanes	
Road Division Type:	Divided by Median	
Minimum Speed Limit:		
Maximum Speed Limit:		
Speed Unit:		
Speed Limit Comment:		
Area Type:	Urban	
Traffic Volume:		
Average Traffic Volume:		
Time of Day:	All	
	If countermeasure is intersection-based.	
Intersection Type:	Roadway/roadway (not interchange related)	
Intersection Geometry:	3-leg	
Traffic Control:	Stop-controlled	
Major Road Traffic Volume:	Minimum of 13433 to Maximum of 75000 Annual Average Daily Traffic (AADT)	
Minor Road Traffic Volume:	Minimum of 51 to Maximum of 2600 Annual Average Daily Traffic (AADT)	

Average Major Road Volume:	38724 Annual Average Daily Traffic (AADT)
Average Minor Road Volume:	519 Annual Average Daily Traffic (AADT)

Development Details	
Date Range of Data Used:	
Municipality:	
State:	CA
Country:	USA
Type of Methodology Used:	Regression cross-section
Sample Size (crashes):	199 crashes
Sample Size (sites):	138 sites

Other Details		
Included in HSM:	No	
Date Added to Clearinghouse:	Oct 27, 2018	
Comments:	This CMF compares urban, three-legged, stop-controlled intersections with RIRO operation to full movement. This CMF looks at Intersection-related	
	intersection defined as 'intersection-related' by the reporting officer (all types and severities combined)	

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# **CMF / CRF Details**

CMF ID: 9823

CMF Name: Install right-in-right-out (RIRO) operations at stop-controlled interse

**Description:** 

Prior Condition: No Prior Condition(s)

**Category: Access management** 

Study ID: <u>Safety Effects of Turning Movement Restrictions at Stop-Controlled</u> <u>Intersections, Le et al. 2018</u>

Star Quality Rating		
Star Quality Rating:	3 Stars	
Crash Modification Factor (CMF)		
Value:	0.2	
Adjusted Standard Error:		
Unadjusted Standard Error:	0.07	

Crash Reduction Factor		
Value:	80	
Adjusted Standard Error:		
Unadjusted Standard Error:	7	

Applicability		
Crash Type:	Other	
Crash Severity:	K (fatal),A (serious injury),B (minor injury),C (possible injury)	
Roadway Types:	Not specified	
Minimum Number of Lanes:	4	
Maximum Number of Lanes:	6	
Number of Lanes Direction:		
Number of Lanes Comment:	4 and 6 Lanes	
Road Division Type:	Divided by Median	
Minimum Speed Limit:		
Maximum Speed Limit:		
Speed Unit:		
Speed Limit Comment:		
Area Type:	Urban	
Traffic Volume:		
Average Traffic Volume:		
Time of Day:	All	
	If countermeasure is intersection-based.	
Intersection Type:	Roadway/roadway (not interchange related)	
Intersection Geometry:	3-leg	
Traffic Control:	Stop-controlled	
Major Road Traffic Volume:	Minimum of 13433 to Maximum of 75000 Annual Average Daily Traffic (AADT	
Minor Road Traffic Volume:	Minimum of 51 to Maximum of 2600 Annual Average Daily Traffic (AADT)	

Average Major Road Volume:	38724 Annual Average Daily Traffic (AADT)
Average Minor Road Volume:	519 Annual Average Daily Traffic (AADT)

Development Details	
Date Range of Data Used:	
Municipality:	
State:	CA
Country:	USA
Type of Methodology Used:	Regression cross-section
Sample Size (crashes):	101 crashes
Sample Size (sites):	138 sites

Other Details								
Included in HSM:	No							
Date Added to Clearinghouse:	Oct 27, 2018							
Comments:	This CMF compares urban, three-legged, stop-controlled intersections with RIRO operation to full movement. This CMF looks at Fatal and Injury, Intersection-related crashes. Intersection-related crashes are defined as all crashes within 100 ft of intersection defined as 'intersection-related' by the reporting officer (K, A, B, and C injuries on KABCO scale)							

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## **Appendix I** Cost Estimates, Benefit Cost Analysis, and Design Parameters







EASTBOUND RANDOLPH ROAD: RIGHT TURN MOVEMENT





WESTBOUND RANDOLPH ROAD: RIGHT TURN MOVEMENT





NORTHBOUND SR-43: RIGHT TURN MOVEMENT





SOUTHBOUND SR-43: RIGHT TURN MOVEMENT





EASTBOUND RANDOLPH ROAD: RIGHT TURN MOVEMENT



EASTBOUND RANDOLPH ROAD: THROUGH MOVEMENT





NOTE: THE DESIGN VEHICLE USED FOR THE GEOMETRIC LAYOUT OF THE ROUNDABOUTS IS A WB-62.



WESTBOUND RANDOLPH ROAD: RIGHT TURN MOVEMENT



WESTBOUND RANDOLPH ROAD: THROUGH MOVEMENT



WESTBOUND RANDOLPH ROAD: LEFT TURN MOVEMENT

025 TIME: 5:36:07 PM USER: cflac \Site plan\SR-da Transe בהשלטובר

DATE: 3/10,

(AB\_002\_WestBound PAPERSIZE: 17x11 (in.) C D4 Safety Studies (Tack 41) D0P\_CR 43 & Trar





NORTHBOUND SR-43: LEFT TURN MOVEMENT



NORTHBOUND SR-43: RIGHT TURN MOVEMENT



NOTE: THE DESIGN VEHICLE USED FOR THE GEOMETRIC LAYOUT OF THE ROUNDABOUTS IS A WB-62.

0 HEET TOTAL



SOUTHBOUND SR-43: RIGHT TURN MOVEMENT



SOUTHBOUND SR-43: LEFT TURN MOVEMENT



NOTE: THE DESIGN VEHICLE USED FOR THE GEOMETRIC LAYOUT OF THE ROUNDABOUTS IS A WB-62.

HEET TOTAL



EASTBOUND RANDOLPH ROAD: RIGHT TURN MOVEMENT





WESTBOUND TRARES ROAD: RIGHT TURN MOVEMENT





NORTHBOUND SR-43: RIGHT TURN MOVEMENT





SOUTHBOUND SR-43: RIGHT TURN MOVEMENT





EASTBOUND RANDOLPH ROAD: RIGHT TURN MOVEMENT



EASTBOUND RANDOLPH ROAD: LEFT TURN MOVEMENT



EASTBOUND RANDOLPH ROAD: THROUGH MOVEMENT



0

HEET TOTAL 10 13



WESTBOUND TRARES ROAD: RIGHT TURN MOVEMENT







SOUTHBOUND SR-43: RIGHT TURN MOVEMENT



SOUTHBOUND SR-43: LEFT TURN MOVEMENT



SOUTHBOUND SR-43: THROUGH MOVEMENT



NOTE: THE DESIGN VEHICLE USED FOR THE GEOMETRIC LAYOUT OF THE ROUNDABOUTS IS A WB-62.

0

HEET TOTAL 12 13



NORTHBOUND SR-43: RIGHT TURN MOVEMENT



NORTHBOUND SR-43: LEFT TURN MOVEMENT



NORTHBOUND SR-43: THROUGH MOVEMENT



NOTE: THE DESIGN VEHICLE USED FOR THE GEOMETRIC LAYOUT OF THE ROUNDABOUTS IS A WB-62.

SHEET TOTAL

## **Roundabout Critical Design Parameters** North Roundabout (SR-43 and Randolph)

Dosign Baramotors	Leg 1	Leg 2	Leg 3	Leg 4			
Design Parameters	(North)	(West)	(South)	(East)			
Inscribed Circle Diameter, FT		14	40				
Entry Width, FT	19.9	18.7	18.4	22.6			
Entry Angle PHI φ, DEG	10	20	6	20			
Exit Width, FT	18.9	16.2	16.9	16.7			
Circulatory Roadway Width Upstream of Entry, FT	18	18	18	18			
- 							
Fastest Path Speed	(North)	(Wost)	(South)	(East)			
P Padius/Speed ET/MPH	158 17	(West)	(30util)	(Last) 82.01			
P Spood MDH	24.54	97.03 20.40	137.73	10.24			
R <sub>1</sub> , speed, MFT	02 78	20.49	23.33	01 01			
R <sub>2</sub> , Radius/ speed, 11/MPTT	10.0	17.02	18.7	18.05			
R <sub>2</sub> , speed, MFT	246.60	255.62	214 46	277 11			
R <sub>3</sub> , Radius/ speed, FT/MPH	240.09	300.02	214.40	377.11			
R <sub>3</sub> , speed, MPH	28.94	33.Z	27.5	33.98			
R <sub>4</sub> , Radius/Speed, FT/MPH	57.00	57.00	57.00	57.00			
R <sub>4</sub> , Speed, MPH	15.8	15.8	15.8	15.8			
$R_5$ , Radius/Speed, FT/MPH	N/A	N/A	N/A	80.27			
$R_5$ , Speed, MPH	N/A	N/A	N/A	19			
R <sub>5</sub> , Bypass Radius/Speed, FT/MPH							
-	leg 1	leg 2	leg 3	leg 4			
Minimum Sight Parameters	(North)	(West)	(South)	(East)			
Approach Design Speed, MPH	24.5	20.5	23.3	19.2			
Approach Stopping Sight Distance, FT/MPH							
Circulatory Stopping Sight Distance, FT/MPH							
Exit (Crosswalk) Stopping Sight Distance, FT/MPH	N/A	N/A	N/A	N/A			
Intersection Sight Distance, FT/MPH							
General							
Design Vehicle(s)	WB-62						
Truck Apron Width, FT		2	.0				

#### Designer: Colleen Flach

Signature:

Date: 2/4/2025

## Roundabout Critical Design Parameters South Roundabout (SR-43 and Trares)

Dosign Paramotors	Leg 1	Leg 2	Leg 3	Leg 4			
Design Parameters	(North)	(West)	(South)	(East)			
Inscribed Circle Diameter, FT		14	40				
Entry Width, FT	16.7	19.0	18.5	18.7			
Entry Angle PHI φ, DEG	14	15	18	18			
Exit Width, FT	15.8	17.0	17.1	16.6			
Circulatory Roadway Width Upstream of Entry, FT	18	18	18	18			
	Leg 1	Leg 2	Leg 3	Leg 4			
Fastest Path Speed	(North)	(West)	(South)	(East)			
R1, Radius/Speed, FT/MPH	103.86	122.05	116.79	116.17			
R <sub>1</sub> , Speed, MPH	20.97	22.30	21.93	21.89			
R <sub>2</sub> , Radius/Speed, FT/MPH	78.63	89.89	96.05	84.01			
R <sub>2</sub> , Speed, MPH	17.89	18.80	19.26	18.33			
R <sub>3</sub> , Radius/Speed, FT/MPH	394.18	407.30	347.80	404.93			
R <sub>3</sub> , Speed, MPH	34.54	34.97	32.96	34.89			
R <sub>4</sub> , Radius/Speed, FT/MPH	57.00	57.00	57.00	57.00			
R <sub>4</sub> , Speed, MPH	15.80	15.80	15.80	15.80			
R <sub>5</sub> , Radius/Speed, FT/MPH	136.98	N/A	N/A	N/A			
R <sub>5</sub> , Speed, MPH	23.28	N/A	N/A	N/A			
R <sub>5</sub> , Bypass Radius/Speed, FT/MPH							
- 							
Minimum Sight Parameters	(North)	(West)	(South)	(East)			
Approach Design Speed, MPH	21.0	22.3	21.9	21.9			
Approach Stopping Sight Distance, FT/MPH							
Circulatory Stopping Sight Distance, FT/MPH							
Exit (Crosswalk) Stopping Sight Distance, FT/MPH	N/A	N/A	N/A	N/A			
Intersection Sight Distance, FT/MPH							
General							
Design Vehicle(s)	WB-62						
Truck Apron Width, FT		2	.0				

#### Designer: Colleen Flach

Signature:

Date: 2/4/2025



#### **Roadway Improvements**

Item	Description	Quantity	Units		Unit Cost		Total Cost
	Clearing and Grubbing						
201	Clearing of trees and overgrowth in	1	LUMP	\$	25,000.00	\$	25,000.00
	wooded areas		FACIL		(	<i>.</i>	(
202	Building Demolished	1	EACH	\$	60,000.00	\$	60,000.00
202	Farthwark	7770	51	\$	22.50	\$	174,825.00
	Earthwork Required for leveling vertical						
203	alignments of roadways and grading	1	LUMP	\$	650,000.00	\$	650,000.00
	beyond the limits of new pavement						
204	Subgrade Compaction	11630	SY	\$	3.25	\$	37,797.50
441	Asphalt Drive	260	SY	\$	115.00	\$	29,900.00
441	Full Depth Pavement (Asphalt)	9165	SY	\$	115.00	\$	1,053,975.00
452	Concrete Truck Apron	1090	SY	\$	125.00	\$	136,250.00
452	Concrete Drive	235	SY	\$	105.00	\$	24,675.00
609	Concrete Curb	4640	FT	\$	45.00	\$	208,800.00
609	Concrete Traffic Island	840	SY	\$	150.00	\$	126,000.00
	Drainage						
611	Installation of closed storm sewer (catch	1	LUMP	\$	500,000.00	\$	500,000.00
	basins, manholes, conduits, BMP, etc.)				- ·		- ·
	Lighting						
605		1	TIMD	¢	200,000,00	¢	200,000,00
025	Installation of two (2) light poles per leg	1	LUMI	φ	200,000.00	φ	200,000.00
	Signage						
(22	Flat sheet sian installations along leas		LUMD		10 000 00		
630	and within the central island and	1	LUMP	\$	10,000.00	\$	10,000.00
	splitter islands						
	Pavement Markings						
644	Installation of edge lines, center lines,	1	LUMP	\$	15,000.00	\$	15,000.00
	and yield lines						
	Seeding and Mulching						
659	Restoration of disturbed areas within 1	LUMP	\$	50,000.00	\$	50,000.00	
	The project limits						
822	Assumed based on the size and elements	1	LUMP	\$	20,000,00	\$	20,000,00
0.02	of the project	-	LOMI	Ψ	20,000.00	Ψ	20,000.00
		T	temized	Subto	tal	¢	2 222 220 00
			.emizeu i	Subt	Jui	Ψ	3,322,230.00
	Iı	ncidentals					
614	Maintenance of Traffic	1	LUMP	\$	150,000.00	\$	150,000.00
623	Construction Layout Stakes	1	LUMP	\$	25,000.00	\$	25,000.00
624	Mobilization	1	LUMP	\$	100,000.00	\$	100,000.00
		In	cidentals	s Sub	total	\$	275,000.00
			(	Conti	ngency (30%)	\$	1,079,200.00
		Cor	nstructio	n Sul	ototal	\$	4,676,430.00
	\$	701,500.00					
	\$	467,700.00					
	\$	87,474.00					
	\$	5,933,200.00					
					•		_
				Infla	ation* (13.5%)	\$	801,000.00
					Total	\$	6,734,200.00

Note: Cost estimate does not include utility relocation costs.

\*Inflation based on 2027 Construction. Note, inflation rates have been irregularly high recently. If the proposed project is not immediately moved forward, this cost estimate will likely need revised as time passes.



#### Right-of-Way Cost Estimate - Roundabouts - Combined Alternate 1 SR-43 at Trares Road and Randolph Road

		11-14	0	O de textest			Subtotal	Tetel Mars Labor	Derrol	<b>T</b> . 4 . 1	Destinat	
Acquisition	Parcel	Unit	Cost/Unit	Subtotal	Structure Value	Damages (Loss In	Structures &	I otal Non-Labor	Parcel	Total	Partial	No. of Structures Impacted
		(Acreage)	(\$\$/Acre)	Land value	(if Taken)	value to the Residue)	Damages	Acquisition Costs	Count	Takes	Takes	
	36-024-00-00-007-002	0.033	\$15,000	\$495	\$0	\$0	\$0	\$495				
	36-024-00-00-024-000	0.022	\$30,000	\$660	\$0	\$0	\$0	\$660				
	36-024-00-00-025-005	0.663	\$8,000	\$5,304	\$0	\$0	\$0	\$5,304				
	36-024-00-00-038-001	0.105	\$35,000	\$3,675	\$0	\$0	\$0	\$3,675				
Posidontial	36-027-00-00-011-000	0.337	\$15,000	\$5,055	\$0	\$0	\$0	\$5,055	10	1	0	1
Residential	36-027-00-00-028-001	0.170	\$20,000	\$3,400	\$0	\$0	\$0	\$3,400		'	9	1
	36-027-00-00-029-000	0.006	\$20,000	\$120	\$0	\$0	\$0	\$120				
	36-027-00-00-029-001	0.001	\$20,000	\$20	\$0	\$0	\$0	\$20				
	36-027-00-00-030-000	0.253	\$20,000	\$5,060	\$0	\$0	\$0	\$5,060				
	36-027-00-00-031-000	0.034	\$55,000	\$1,870	\$0	\$0	\$0	\$1,870				
Commercial			\$0	\$0	\$0	\$0	\$0	\$0				0
Industrial			\$0	\$0	\$0	\$0	\$0	\$0				0
Agricultural			\$0	\$0	\$0	\$0	\$0	\$0				0
Relocation	Unit (Dienla	comont)			Move Cost	Po ostablishmont		Total Non-Labor	Estimate	amount of	time nece	ssary to relocate all RAP
Residential	Unit (Displa	cement)	KHF/KJF	_	WOVE COSt	-		RAP Costs	Estimated	d number o	of years un	til project wide R/W
Owner Occupant	1		\$34,000		\$6,000			\$40,000	acquisitio	n begins =	3	
Tenant	0		\$10,000	]	\$1750			\$0				
Commercial/Farm/NPO			_				_					
Owner	0		]		\$15,000	\$10,000		\$0				
Tenant	0				\$15,000	\$10,000		\$0				
Personal Property	0				\$1,000			\$0				
[[(total of acquisition cost) x 0.09]x0.025] + [[(total of acquisition cost) x 0.15] x 1.20] + [[(total of acquisition		total of acquisition	cost) x 0.10] x 1.50	] =	Continger (Incidentals, Admin, Review	CY Appropriation)	\$21,815	RHP - Re	placement	t Housing I	Payment /ment	
						Total Non-Labor	R/W Costs	\$87.474	NPO - No	n-Profit O	roanization	
Labor (External)	Unit (Par	cels)	Unit Price	Total Cost	1						3	-
Titles	0		\$1.000	\$0				This R/W Co	ost Estimate	Prepared	bv	Date
Appraisals								Carpenter	Marty Tran	sportation		10/23/2023
Simple	0		\$750	\$0								
Detailed	0		\$4,500	\$0								
Appraisal Review												
Simple	0		\$500	\$0	1							
Detailed	0		\$2,000	\$0	1							
					1							
Negotiations	0		\$1,800	\$0								
Relocations												
Personal Property	0		\$2,000	\$0								
Residential	0		\$8,000	\$0								
Commericial/Farm/NPO	0		\$6,000	\$0								
Closings	0		\$500	\$0								
Package Billing & Review	0		\$500	\$0						Total La	bor Costs	
Project Management	0		\$4,000	\$0					Total No	n-Labor R	R/W Costs	\$87,474
Asbestos Testing & Abatement	0		\$5,000	\$0	ļ					Cor	ntingency	
	Tot	al Labor Costs		\$0					тот	AL R/W	COSTS	\$87,474

Item	Description	Quantity	Units		Unit Cost		Total Cost
Item	Clearing and Grubbing	Qualitity			Chiteost		Total Cost
201	Clearing of trees and overgrowth in wooded areas	1	LUMP	\$	15,000.00	\$	15,000.00
202	Building Demolished	1	EACH	\$	60,000.00	\$	60,000.00
202	Pavement Removed	3900	SY	\$	22.50	\$	87,750.00
203	Earthwork Required for leveling vertical alignments of roadways and grading beyond the limits of new pavement	1	LUMP	\$	350,000.00	\$	350,000.00
204	Subgrade Compaction	6210	SY	\$	3.25	\$	20,182.50
441	Asphalt Drive	20	SY	\$	115.00	\$	2,300.00
441	Full Depth Pavement (Asphalt)	4950	SY	\$	115.00	\$	569,250.00
452	Concrete Truck Apron	535	SY	\$	125.00	\$	66,875.00
452	Concrete Drive	30	SY	\$	105.00	\$	3,150.00
609	Concrete Curb	2510	FT	\$	45.00	\$	112,950.00
609	Concrete Traffic Island	410	SY	\$	150.00	\$	61,500.00
611	Drainage Installation of closed storm sewer (catch basins, manholes, conduits, BMP, etc.)	1	LUMP	\$	250,000.00	\$	250,000.00
625	Lighting Installation of two (2) light poles per leg	1	LUMP	\$	100,000.00	\$	100,000.00
630	Signage Flat sheet sign installations along legs and within the central island and splitter islands	1	LUMP	\$	5,000.00	\$	5,000.00
644	Pavement Markings Installation of edge lines, center lines, and yield lines	1	LUMP	\$	7,500.00	\$	7,500.00
659	Seeding and Mulching Restoration of disturbed areas within the project limits	1	LUMP	\$	25,000.00	\$	25,000.00
832	Erosion Control Assumed based on the size and elements of the project	1	LUMP	\$	10,000.00	\$	10,000.00
		I	temized	Subt	otal	\$	1,746,460.00
r	-	• 1 • 1					
(	Meintenen of Traffic	ncidentals	LIDER	¢	100	¢	10.5
614	Construction Levout Stolag	1		\$	100,000.00	\$	100,000.00
623	Construction Layout Stakes	1		\$	12,500.00	\$	12,500.00
624	Modilization	1	LUMP	\$	100,000.00	4	100,000.00
		In	cidental	s Sub	total	\$	212,500.00
				Conti	ingency (30%)	\$	587,700.00
	\$	2,546,660.00					
	Environmental, Geotechnical, Miso Rig	cellaneous F ht-of-Way* (	Engine ederal Ro Includes	ering equir 30%	g Design (15%) rements (10%) Contingency)	\$ \$ \$	382,000.00 254,700.00 71,064.00
					Subtotal	\$	3,254,500.00

#### **Roadway Improvements**

Note: Cost estimate does not include utility relocation costs.

\*Inflation based on 2027 Construction. Note, inflation rates have been irregularly high recently. If the proposed project is not immediately moved forward, this cost estimate will likely need revised as time passes.

Inflation\* (13.5%) \$

Total \$

439,400.00

3,693,900.00



#### Right-of-Way Cost Estimate - North Roundabout SR-43 and Randolph Road

Acquisition	Parcel	Unit (Acreage)	Cost/Unit (\$\$/Acre)	Subtotal Land Value	Structure Value (If Taken)	Damages (Loss in Value to the Residue)	Subtotal Structures & Damages	Total Non-Labor Acquisition Costs	Parcel Count	Total Takes	Partial Takes	No. of Structures Impacted
	36-024-00-00-007-002	0.033	\$15,000	\$495	\$0	\$0	\$0	\$495				
	36-024-00-00-024-000	0.022	\$30,000	\$660	\$0	\$0	\$0	\$660				
	36-024-00-00-025-005	0.442	\$8,000	\$3,536	\$0	\$0	\$0	\$3,536				
Residential	36-027-00-00-028-001	0.080	\$20,000	\$1,600	\$0	\$0	\$0	\$1,600	7	1	6	1
	36-027-00-00-029-000	0.006	\$20,000	\$120	\$0	\$0	\$0	\$120				
	36-027-00-00-030-000	0.253	\$20,000	\$5,060	\$0	\$0	\$0	\$5,060				
	36-027-00-00-031-000	0.034	\$55,000	\$1,870	\$0	\$0	\$0	\$1,870				
Commercial			\$0	\$0	\$0	\$0	\$0	\$0				0
Industrial			\$0	\$0	\$0	\$0	\$0	\$0				0
Agricultural			\$0	\$0	\$0	\$0	\$0	\$0				0
Relocation	Unit (Displa	acomont)	PHD/DCD		Move Cost	Ro-ostablishment		Total Non-Labor	Estimate	amount of	time neces	ssary to relocate all RAP
Residential	Offic (Dispic	acementy		_	wove oost	Re-establishment		RAP Costs	Estimated	l number o	of years un	til project wide R/W
Owner Occupant	1		\$34,000	]	\$6,000			\$40,000	acquisitio	n begins =	3	
Tenant	0		\$10,000		\$1750			\$0				
Commercial/Farm/NPO				-		— —						
Owner	0		]		\$15,000	\$10,000	1	\$0	1			
Tenant	0				\$15,000	\$10,000		\$0	1			
Personal Property	0				\$1.000		•	\$0	1			
[[(total of acquisition cost) x 0.09]x0.025] + [[(total of acquisition cost) x 0.15] x 1.20] + [[(total of		total of acquisition	cost) x 0.10] x 1.50	] =	Continger (Incidentals, Admin. Review	ncy	\$17,723	RHP - Replacement Housing Payment - RSP - Rent Supplemental Payment			Payment /ment	
						I otal Non-Labor	R/W Costs	\$71,064	NPO - No	n-Profit O	rganizatior	1
Labor (External)	Unit (Pa	rcels)	Unit Price	Total Cost				n				
Titles	0		\$1,000	\$0				This R/W Co	st Estimate	Preparec	by	Date
Appraisals								Carpenter	Marty Tran	sportation		1/31/2025
Simple	0		\$750	\$0								
Detailed	0		\$4,500	\$0								
Appraisal Review	1			1	-							
Simple	0		\$500	\$0	-							
Detailed	0		\$2,000	\$0								
Negotiations	0		\$1.800	\$0	-							
Relocations			÷.,	1								
Personal Property	0		\$2 000	\$0	1							
Residential	0		\$8,000	\$0								
Commericial/Farm/NPO	0		\$6,000	\$0	1							
Closings	0		\$500	\$0	1							
Package Billing & Review	0		\$500	\$0	1					Total I a	or Costs	
Project Management	0		\$4,000	\$0	1				Total No	n-l abor F	W Costs	\$71.064
Aspestos Testing & Abatement	0		\$5,000	\$0	1					Co	ntingency	
	To	tal Labor Costs		\$0	Ĩ				тот	AL R/W	COSTS	\$71.064

Roadway	Improvements
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Item	Description	Quantity	Units		Unit Cost		Total Cost
201	Clearing and Grubbing Clearing of trees and overgrowth in wooded areas	1	LUMP	\$	10,000.00	\$	10,000.00
202	Pavement Removed	3870	SY	\$	22.50	\$	87,075.00
203	Earthwork Required for leveling vertical alignments of roadways and grading beyond the limits of new pavement	1	LUMP	\$	300,000.00	\$	300,000.00
204	Subgrade Compaction	5420	SY	\$	3.25	\$	17,615.00
441	Asphalt Drive	240	SY	\$	115.00	\$	27,600.00
441	Full Depth Pavement (Asphalt)	4215	SY	\$	115.00	\$	484,725.00
452	Concrete Truck Apron	555	SY	\$	125.00	\$	69,375.00
452	Concrete Drive	205	SY	\$	105.00	\$	21,525.00
609	Concrete Curb	2130	FT	\$	45.00	\$	95,850.00
609	Concrete Traffic Island	430	SY	\$	150.00	\$	64,500.00
611	Drainage Installation of closed storm sewer (catch basins, manholes, conduits, BMP, etc.)	1	LUMP	\$	250,000.00	\$	250,000.00
625	Lighting Installation of two (2) light poles per leg	1	LUMP	\$	100,000.00	\$	100,000.00
630	Signage Flat sheet sign installations along legs and within the central island and splitter islands	1	LUMP	\$	5,000.00	\$	5,000.00
644	Pavement Markings Installation of edge lines, center lines, and yield lines	1	LUMP	\$	7,500.00	\$	7,500.00
659	Seeding and Mulching Restoration of disturbed areas within the project limits	1	LUMP	\$	25,000.00	\$	25,000.00
832	Erosion Control Assumed based on the size and elements of the project	1	LUMP	\$	10,000.00	\$	10,000.00
		I	temized	Subt	otal	\$	1,575,770.00
	I	ncidentals					
614	Maintenance of Traffic	1	LUMP	\$	100,000.00	\$	100,000.00
623	Construction Layout Stakes	1	LUMP	\$	12,500.00	\$	12,500.00
624	Mobilization	1	LUMP	\$	100,000.00	\$	100,000.00
		In	cidentals	s Sub	ototal	\$	212,500.00
			(	Conti	ingency (30%)	\$	536,500.00
		Сог	istructio	n Su	btotal	\$	2.324.770.00
			1511 40110	nou	Stotal	Ψ	<b>_,3_,</b> /0100
			Engine	ering	g Design (15%)	\$	348,800.00
	Environmental, Geotechnical, Misc	ellaneous Fe	ederal Re	equir	rements (10%)	\$	232,500.00
	Rigl	nt-of-Way* (1	Includes	- 30%	Contingency)	\$	16,384.00
		• •			Subtotal	\$	2,922,500.00
				Infl	ation* (13.5%)	\$	394,600.00
					Total	\$	3,317,100.00

Note: Cost estimate does not include utility relocation costs.

\*Inflation based on 2027 Construction. Note, inflation rates have been irregularly high recently. If the proposed project is not immediately moved forward, this cost estimate will likely need revised as time passes.



#### Right-of-Way Cost Estimate - South Roundabout SR-43 and Trares Road

Acquisition	Parcel	Unit (Acreage)	Cost/Unit (\$\$/Acre)	Subtotal Land Value	Structure Value (If Taken)	Damages (Loss in Value to the Residue)	Subtotal Structures & Damages	Total Non-Labor Acquisition Costs	Parcel Count	Total Takes	Partial Takes	No. of Structures Impacted
	36-024-00-00-025-005	0.221	\$8,000	\$1,768	\$0	\$0	\$0	\$1,768				
	36-024-00-00-038-001	0.105	\$35,000	\$3,675	\$0	\$0	\$0	\$3,675	1	0	4	0
	36-027-00-00-011-000	0.337	\$15,000	\$5,055	\$0	\$0	\$0	\$5,055	1 4	0	4	0
	36-027-00-00-028-001	0.090	\$20,000	\$1,800	\$0	\$0	\$0	\$1,800				
Commercial			\$0	\$0	\$0	\$0	\$0	\$0				0
Industrial			\$0	\$0	\$0	\$0	\$0	\$0				0
Agricultural			\$0	\$0	\$0	\$0	\$0	\$0				0
Relocation	Unit (Dionk	acomant)			Move Cost	Be establishment		Total Non-Labor	Estimate	amount of	time nece	ssary to relocate all RAP
Residential		icement)	KHF/KOF	KHP/KSP		Re-establishment		RAP Costs	Estimated	I number o	of years un	til project wide R/W
Owner Occupant	0		\$34,000	]	\$6,000			\$0	acquisitio	n begins =	3	
Tenant	0		\$10,000	1	\$1750	1		\$0				
Commercial/Farm/NPO			•	•		-						
Owner	0		1		\$15,000	\$10.000		\$0				
Tenant	0				\$15,000	\$10,000		\$0				
Personal Property	0				\$1,000		-	\$0				
[[(total of acquisition cost) x 0.09]x0.025] + [[(total of acquisition cost) x 0.15] x 1.20] + [[(total of acquisition cost)				cost) x 0.10] x 1.50	] =	Continger	ncy « & Appropriation)	\$4,086	RHP - Re	placemen	t Housing	Payment
						Total Non-Labor	R/W Costs	\$16,384	NPO - No	n-Profit O	rganizatior	)
Labor (External)	Unit (Pa	rcels)	Unit Price	Total Cost					_			
Titles	0		\$1,000	\$0				This R/W Co	st Estimate	Prepared	l by	Date
Appraisals								Carpenter I	Marty Tran	sportation		1/31/2025
Simple	0		\$750	\$0								
Detailed	0		\$4,500	\$0								
Appraisal Review												
Simple	0		\$500	\$0								
Detailed	0		\$2,000	\$0								
Negotiations	0		\$1,800	\$0								
Relocations	•											
Personal Property	0		\$2,000	\$0								
Residential	0		\$8,000	\$0								
Commericial/Farm/NPO	0		\$6,000	\$0								
Closings	0		\$500	\$0								
Package Billing & Review	0		\$500	\$0	1					Total La	bor Costs	
Project Management	0		\$4,000	\$0	1				Total No	n-Labor R	R/W Costs	\$16.384
Asbestos Testing & Abatement	0		\$5,000	\$0	1					Cor	ntingency	
	To	al Labor Costs		\$0					тот	AL R/W	COSTS	\$16,384

Project Cost Estimate										
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com							
Project Description	SR-43 Safety Study: Alt 1	Contact Phone	614-656-2429							
Reference Number	ODOT PID 1147572	Date Performed	2/6/2025							
Analyst	GMB	Analysis Year	2022							
Agency/Company	Carpenter Marty Transportation									

#### Engineering Design % 25% Contingency % 30%

Countermeasures	Construction Costs	Right of Way Costs	Engineering Design Costs	Contingency Amount	Total Cost of Countermeasure	Annual Maintenance & Energy Costs	Salvage Value
Install Roundabouts	\$3,740,408.00	\$87,474.00	\$956,970.50	\$1,148,364.60	\$5,933,217.10		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
Totals	\$3,740,408.00	\$87,474.00	\$956,970.50	\$1,148,364.60	\$5,933,217.10	\$0.00	\$0.00

	Inflation %	14%
Final Costruction Cost:	\$6,734,201.41	

\*Final construction cost should match the Project Cost Estimate

ECAT	Safety B		
And Antonio Contraction	C		
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com
Project Description	SR-43 Safety Study: Alt 1	Contact Phone	614-656-2429
Reference Number	ODOT PID 1147572	Date Performed	2/6/2025
Analyst	GMB	Analysis Year	2022
Agency/Company	Carpenter Marty Transportation		
		·	<u>.</u>
	Comments:		

Select Site Types to be used in Benefit-Cost Analysis:								
All Sites								
Countermeasure Service Lives, Costs, and Safety Benefits								
Countermeasures	Service Life (Years)	Initial Cost of Countermeasure	Annual Maintenance & Energy Costs	Salvage Value	Net Present Cost of Countermeasure	Total Cost of Countermeasures	Summary of Annual Crash Modifications	Net Present Value of Safety Benefits
Install Roundabouts	20	\$5,933,217.10			\$5,933,217.10	\$5,933,217.10		
		\$0.00			\$0.00	\$0.00	2.214	\$4.559.660
		\$0.00			\$0.00	\$0.00	-3.314	\$4,558,662
		\$0.00			\$0.00	\$0.00		
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
Totals		\$5,933,217.10	\$0.00	\$0.00	\$5,933,217.10	\$5,933,217.10	-3.314	\$4,558,662

\$5,955,217.10	\$0.00	\$0.00	\$5,955,217.10	\$5,955,217.1
	Expected Annual	Crash Adjustment		Comments:
Number of Fa	tal & Incapacitating Injury Crashes	-0.448		
Numb	er of Injury Crashes	-2.066		
Numb	per of Total Crashes	-3.314		

Net Benefit (\$1,374,555.27)

Benefit - Cost Calculator

 Net Present Value of Project
 \$5,933,217.10

 Net Present Value of Safety Benefits
 \$4,558,661.83

Benefit / Cost Ratio 0.77



# SR-43, RANDOLPH ROAD, AND TRARES ROAD MODEL:

tic Plan - RIRO PAPERSIZE: 17x11 (in.) DATE: 3/10/2025 TIME: 5:39:53 PM USER: cflach D4 Safety Studies (Task 4)\POR-SR 43 & Trares & Randolph/Site plan\SR-43 Trares Ranc



HORIZONTAL SCALE IN FEET 。 RANDERROAD SR-43 AND RANDOLPH ROAD RIGHT-IN/RIGHT-OUT TRUCK TURNS ESIGNER CEF REVIEWER BAA 02-04-25 NOTE: THE DESIGN VEHICLE USED FOR THE GEOMETRIC LAYOUT OF THE RIGHT-IN/RIGHT-OUT IS AN SU-30. 0 SHEET TOTAL



#### **Roadway Improvements**

Item	Description	Quantity	Units		Unit Cost	Total Cost		
	Clearing and Grubbing							
201	Clearing of trees and overgrowth in	1	LUMP	\$	25,000.00	\$	25,000.00	
	wooded areas							
202	Pavement Removed	6250	SY	\$	22.50	\$	140,625.00	
202	Guardrail Removed	150	FT	\$	4.00	\$	600.00	
	Earthwork							
203	Required for leveling vertical	1	LUMP	\$	400.000.00	\$	400.000.00	
-0	alignments of roadways and grading		-	1			1	
	beyond the limits of new pavement							
204	Subgrade Compaction	7000	SY	\$	3.25	\$	22,750.00	
441	Asphalt Drive	240	SY	\$	115.00	\$	27,600.00	
441	Full Depth Pavement (Asphalt)	6120	SY	\$	115.00	\$	703,800.00	
452	Concrete Truck Apron	555	SY	\$	125.00	\$	69,375.00	
452	Concrete Drive	205	SY	\$	105.00	\$	21,525.00	
606	Guardrail	150	FT	\$	30.00	\$	4,500.00	
608	Concrete Curb	2470	FT	\$	45.00	\$	111,150.00	
609	Concrete Traffic Island	595	SY	\$	150.00	\$	89,250.00	
	Drainage							
611	Installation of closed storm sewer (catch	1	LUMP	\$	325,000.00	\$	325,000.00	
	basins, manholes, conduits, BMP, etc.)							
	Lishting							
605			TIMD	¢	100 000 00	¢	100 000 00	
025	Installation of two (2) light poles per leg	1	LUMP	¢	120,000.00	ф	120,000.00	
	Signage							
630	Flat sheet sign installations along legs	1	LUMP	\$	8,500.00	\$	8,500.00	
	splitter islands							
	Pavement Markings							
	Installation of odge lines, conton lines							
644	uiald lines stop lines chappelizing lines	1	LUMP	\$	12,500.00	\$	12,500.00	
	and lane arrows							
	Seeding and Mulching							
659	Restoration of disturbed areas within	1	LUMP	\$	38,000.00	\$	38,000.00	
0,	the project limits				0,		0 /	
	Erosion Control							
832	Assumed based on the size and elements	1	LUMP	\$	16,000.00	\$	16,000.00	
	of the project							
		I	temized	Subto	otal	\$	2.136.180.00	
							, • ,	
	I	ncidentals						
614	Maintenance of Traffic	1	LUMP	\$	75,000.00	\$	75,000.00	
623	Construction Layout Stakes	1	LUMP	\$	12,500.00	\$	12,500.00	
624	Mobilization	1	LUMP	\$	20,000.00	\$	20,000.00	
		In	cidental	s Sub	total	\$	107,500.00	
				Conti	ngency (30%)	\$	673,200.00	
		Cor	nstructio	n Sul	ototal	\$	2.916.880.00	
	*	_,,,000.00						
			Engine	ering	Design (15%)	\$	437,600.00	
	\$	291,700.00						
	Rig	ht-of-Way* (	Includes	30%	Contingency)	\$	50,162.00	
					Subtotal	\$	3.696.400.00	
					Jantotai	Ψ	3,090,400.00	
				Infl	ation* (13.5%)	\$	499,100.00	
					Total	\$	4,195,500.00	

Note: Cost estimate does not include utility relocation costs.

\*Inflation based on 2027 Construction. Note, inflation rates have been irregularly high recently. If the proposed project is not immediately moved forward, this cost estimate will likely need revised as time passes.



#### Right-of-Way Cost Estimate - Right-In/Right Out and South Roundabout Alternate 2 SR-43 at Trares Road and Randolph Road

Acquisition	Parcel	Unit (Acreage)	Cost/Unit (\$\$/Acre)	Subtotal Land Value	Structure Value (If Taken)	Damages (Loss in Value to the Residue)	Subtotal Structures & Damages	Total Non-Labor Acquisition Costs	Parcel Count	Total Takes	Partial Takes	No. of Structures Impacted
	36-027-00-00-011-000	0.337	\$15,000	\$5,055	\$0	\$0	\$0	\$5,055				
Posidontial	36-027-00-00-028-001	0.980	\$20,000	\$19,600	\$0	\$0	\$0	\$19,600		0	4	0
Residentia	36-024-00-00-038-001	0.105	\$35,000	\$3,675	\$0	\$0	\$0	\$3,675	-	0	4	0
	36-024-00-00-025-005	0.229	\$8,000	\$1,832	\$0	\$0	\$0	\$1,832				
Commercial			\$0	\$0	\$0	\$0	\$0	\$0				0
Industrial			\$0	\$0	\$0	\$0	\$0	\$0				0
Agricultural			\$0	\$0	\$0	\$0	\$0	\$0				0
Relocation	Unit (Dionk	nont)			Maya Coat	Be establishment		Total Non-Labor	Estimate	amount of	time nece	ssary to relocate all RAP
Residential		icement)	KHF/KSF		WOVE COSt	Re-establishment		RAP Costs	Estimated	I number o	of years un	til project wide R/W
Owner Occupant	0		\$34,000	]	\$6,000	1		\$0	acquisitio	n begins =	3	
Tenant	0		\$10,000	1	\$1750			\$0				
Commercial/Farm/NPO				-		-			1			
Owner	0				\$15,000	\$10,000	7	\$0				
Tenant	0				\$15,000	\$10,000		\$0				
Personal Property	0				\$1,000		-	\$0				
[[(total of acquisition cost) x 0.09]x0.025] + [[(total of acquisition cost) x 0.15] x 1.20] + [[(total of a			total of acquisition	cost) x 0.10] x 1.50	] =	Continge (Incidentals, Admin, Review	ncy w. & Appropriation)	\$20,000	RHP - Re RSP - Re	placemen nt Suppler	t Housing mental Pay	Payment /ment
						Total Non-Labor	R/W Costs	\$50,162	NPO - No	n-Profit O	rganizatior	1
Labor (External)	Unit (Pa	rcels)	Unit Price	Total Cost				P	-			
Titles	0		\$1,000	\$0				This R/W Co	st Estimate	Prepared	l by	Date
Appraisals								Carpenter	Marty Tran:	sportation		11/01/2024
Simple	0		\$750	\$0								
Detailed	0		\$4,500	\$0								
Appraisal Review				•								
Simple	0		\$500	\$0								
Detailed	0		\$2,000	\$0								
Negotiations	0		\$1,800	\$0								
Relocations												
Personal Property	0		\$2,000	\$0	1							
Residential	0		\$8,000	\$0								
Commericial/Farm/NPO	0		\$6,000	\$0	1							
Closings	0		\$500	\$0	1							
Package Billing & Review	0		\$500	\$0	1					Total La	bor Costs	
Project Management	0		\$4,000	\$0	1				Total No	n-Labor R	R/W Costs	\$50.162
Asbestos Testing & Abatement	0		\$5,000	\$0	1					Cor	ntingencv	
	To	tal Labor Costs		\$0					тот	AL R/W	COSTS	\$50,162

Project Cost Estimate								
Project Name	SR-43 at Randolph Road & Trares Road	Contact Email	gbalsamo@cmtran.com					
Project Description	SR-43 Safety Study: Alt 2	Contact Phone	614-656-2429					
Reference Number	ODOT PID 1147572	Date Performed	10/28/2024					
Analyst	GMB	Analysis Year	2022					
Agency/Company	Carpenter Marty Transportation							

#### Engineering Design % 25% Contingency % 30%

Countermeasures	Construction Costs	Right of Way Costs	Engineering Design Costs	Contingency Amount	Total Cost of Countermeasure	Annual Maintenance & Energy Costs	Salvage Value
Roundabout at Trares	\$1,879,252.00	\$16,384.00	\$473,909.00	\$568,690.80	\$2,938,235.80		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
CMF 1 - Install right-in-right-out (RIRO) operations at stop- controlled intersections	\$455,410.00	\$33,778.00	\$122,297.00	\$146,756.40	\$758,241.40		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
			\$0.00	\$0.00	\$0.00		
Totals	\$2,334,662.00	\$50,162.00	\$596,206.00	\$715,447.20	\$3,696,477.20	\$0.00	\$0.00

	Inflation %	14%
Final Costruction Cost:	\$4,195,501.62	

\*Final construction cost should match the Project Cost Estimate
FCAT		S	afety Benef	it - Cost An	alysis					
Contraction in the local data			Genera	I Information						
Project Name	SR-43 at Randolph Road & Trares Road				Contact Email		gbalsamo@cmtran.com			
Project Description	SR-43 Safety Study: Alt 2				Contact Phone		614-656-2429			
Reference Number	ODOT PID 1147572				Date Performed		10/28/2024			
Analyst	GMB				Analysis Year		2022			
Agency/Company	Carpenter Marty Transportation									
		Comm	Comments:							
Select Site Types to be used in Benefit-Cost Analysis:										
All Sites										
Countermeasure Service Lives, Costs, and Safety Benefits										
	Countermeasures	Service Life (Years)	Initial Cost of Countermeasure	Annual Maintenance & Energy Costs	Salvage Value	Net Present Cost of Countermeasure	Total Cost of Countermeasures	Summary of Annual Crash Modifications	Net Present Value of Safety Benefits	
Roundabout at Trares		20	\$2,938,235.80			\$2,938,235.80	\$2,938,235.80			
			\$0.00			\$0.00	\$0.00	3.638	\$3,913,190	
			\$0.00			\$0.00	\$0.00			
			\$0.00			\$0.00	\$0.00			
CMF 1 - Install right-in-right-out (RIRO) operations at stop-controlled intersections		20	\$758,241.40			\$758,241.40	\$758,241.40	-0.686	\$581,082	
			\$0.00			\$0.00	\$0.00	0.000	\$0	
			\$0.00			\$0.00	\$0.00	0.000	\$0	

Totals		\$3,696,477.20	\$0.00	\$0.00	\$3,696,477.20	\$3,696,477.20	-4.324	\$4,494,272
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0
		\$0.00			\$0.00	\$0.00	0.000	\$0

Expected Annual Crash Adjustment							
Number of Fatal & Incapacitating -0.438 Injury Crashes							
Number of Injury Crashes -2.067							
Number of Total Crashes -4.324							

Comments:

Net Present Value of Project \$3,696,477.20

Benefit - Cost Calculator

Net Present Value of Safety Benefits \$4,494,271.66

Net Benefit \$797,794.46

Benefit / Cost Ratio 1.22