

**FRA-161-15.80 NOISE WALLS  
PID NO. 117607  
FRANKLIN COUNTY, OHIO**

## **DRAFT GEOTECHNICAL EXPLORATION REPORT**

*Prepared For:*  
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**Rii Project No. W-23-107**

**January 2024**

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January 18, 2024 (Revised March 18, 2024)

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Planning  
Engineering  
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Technology

**Re: DRAFT Geotechnical Exploration Report  
FRA-161-15.80 Noise Walls  
PID No. 117607  
Franklin County, Ohio  
Rii Project No. W-23-107**

Mr. Hackenbracht:

Resource International, Inc. (Rii) is pleased to submit this revised Draft Geotechnical Exploration Report for the above referenced project. Engineering logs have been prepared and are attached to this report along with the results of laboratory testing. This revised report includes recommendations for the design and construction of eight (8) proposed noise walls and deep foundations for Noise Walls subgrade improvements along SR 161 between Ulry Road and US 62, Franklin County, Ohio. This revised report supersedes our previous submittal.

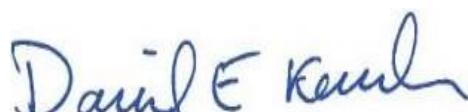
We sincerely appreciate the opportunity to be of continued service to you on this project. If you have any questions regarding the structure foundation exploration, or this report, please do not hesitate to contact us.

Sincerely,

**RESOURCE INTERNATIONAL, INC.**



Daniel K. Hayes, E.I.  
Staff Engineer



Daniel E. Karch, P.E.  
Project Manager - Geotechnical Services

Enclosure: DRAFT Geotechnical Exploration Report

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## EXECUTIVE SUMMARY

This report is a presentation of the subgrade exploration performed for the proposed construction of eight (8) new noise walls along SR 161 between Ulry Road and US 62 in Franklin County, Ohio. Based on the available project information, it is understood that the walls will range from 497 to 2,226 feet in length and will be 14 feet high. Noise Walls 3, 6, 8, 9, 11, 12 and 15, as designated and shown on the project documents, are included as part of this investigation. Details of the proposed noise walls are presented in the following table:

**Noise Wall Details**

Element	Detail
Noise Wall 3	576 feet long along the north side of SR 161 just east of Ulry Road. Maximum wall height of 14 feet.
Noise Wall 6	528 feet long along the north side of SR 161 just east of FRA-00161-19.090 L&R. Maximum wall height of 14 feet.
Noise Wall 8	1,018 feet long along the south side of SR 161 just east of FRA-00161-19.090 L&R. Maximum wall height of 14 feet.
Noise Wall 9	1,270 feet long along the north side of SR 161 just east of Harlem Rd. Maximum wall height of 14 feet.
Noise Wall 11	1,584 feet long along the south side of SR 161 just east of Harlem Rd. Maximum wall height of 14 feet.
Noise Wall 12	497 feet long along the south side of SR 161 just east of Harlem Rd. Maximum wall height of 14 feet.
Noise Wall 15	2,226 feet long along the south side of SR 161 east and west of New Albany Road. Maximum wall height of 14 feet.

The exploration was performed within general accordance of the Ohio Department of Transportation's (ODOT) Specifications for Geotechnical Explorations (SGE), revised January 2023.

## Exploration and Findings

Between October 23 and December 5, 2023, a total of 53 borings were performed for the noise walls as part of the overall FRA-161-16.80 project. The borings performed for noise walls were advanced to depths ranging between 15 and 27.5 feet below the existing ground surface

All borings except B-038-0-23 encountered topsoil thicknesses between 1 inch and 10 inches. Boring B-038-0-23 encountered 3.0 inches of asphalt overlaying 6.5 inches of concrete, overlaying 3.5 inches of aggregate base.

Underlying the surficial soils, the natural soils were encountered, consisting of both cohesive and granular deposits. The natural cohesive soils were described as sandy silt,

silt and clay, silty clay, and clay (ODOT A-4a, A-6a, A-6b, A-7-6). The granular soils were described as gravel, gravel with sand, gravel with sand and silt, gravel with sand and silt and clay, and coarse and fine sand (ODOT A-1-a, A-1-b, A-2-4, A-2-6, A-3a).

Bedrock was encountered in borings B-001-0-23, B-002-0-23, B-003-0-23, B-004-0-23, B-018-0-23, B-019-0-23, B-020-0-23, B-021-0-23, B-022-0-23, B-023-0-23, B-024-0-23, B-027-0-23, B-028-0-23, B-038-0-23, B-039-0-23, B-040-0-23, B-041-0-23, B-042-0-23, B-043-0-23, B-044-0-23, B-045-0-23, B-046-0-23, B-047-0-23, B-048-0-23, B-049-0-23, B-050-0-23, B-001-0-23, B-001-0-23, B-001-0-23, and B-001-0-23 at depths ranging from 4.3 to 23.0 feet beneath the existing ground surface. The bedrock was described as highly weathered gray and brown sandstone, highly weathered to severely weathered gray and black silt, and highly weathered gray shalestone.

Groundwater seepage was encountered in 3 of the borings at depths ranging from 14.0 to 22.4 feet below the ground surface. Significant groundwater flow was encountered during drilling (initial water level) in 26 of the borings at depths ranging from 12.0 to 21.0 feet below the existing ground surface. Measurable groundwater was observed at the completion of drilling in seventeen (17) of the borings at depths ranging from 7.8 to 20.5 feet below existing grade.

## **Analyses and Recommendations**

Data obtained from the subsurface exploration has been used to determine the foundation support capabilities for the soils and bedrock encountered at the site. These parameters have been used to provide guidelines for the design of foundation systems for the proposed noise walls, as well as the construction specifications related to the placement of foundation systems and general earthwork recommendations

Due to revisions in the proposed noise wall alignments after select borings were advanced, data from fifty (50) borings was utilized in the analysis.

The required shaft embedment for the proposed Noise Barriers 3, 6, 8, 9, 11, 12, and 15 was determined in accordance with Section 802.1.2 of the ODOT Bridge Design Manual (BDM). Per ODOT BDM Section 802.1.2, the required embedment depth for the supporting drilled shafts is determined using energy and depth corrected SPT values and selecting the required embedment depth based on either the average or critical corrected SPT value from Table 802.1.2-1 for granular soils or 802.1.2-2 for cohesive soils. Based on the plans and profile information provided, the anticipated panel heights and spacing for each noise barrier are as follows:

### Noise Walls 3, 6, 8, 9, 11, 12 and 15 – Panel Heights and Spacing Information

Noise Barrier	Noise Barrier 3	Noise Barrier 6	Noise Barrier 8	Noise Barrier 9	Noise Barrier 11	Noise Barrier 12	Noise Barrier 15
Panel Heights (feet)	14	14	14	14	14	14	14
Maximum Panel Spacing Center-to-Center of the Drilled Shaft (feet)	24	24	24	24	24	24	24

Based on cross section information provided, the transverse cross-slopes along the alignment of Noise Barrier 3 range from 3:1 and transition to level. The transverse cross-slopes along the Noise Barrier 6 range from 3:1 to 4:1. The transverse cross-slopes along the alignment of Noise Barrier 8 are considered to be generally level with a localized slope of 5:1. The transverse cross-slopes along the alignment of Noise Barrier 9 range from 3:1 to 5:1. The transverse cross-slopes along the alignment of Noise Barrier 11 range from level to 5:1. The transverse cross-slopes along the alignment of Noise Barrier 12 range from 2:1 to 5:1. Finally, the transverse cross-slopes along the alignment of Noise Barrier 15 range from 3:1 to level.

In general, the analysis indicates that 2.5-foot diameter drilled shafts excavated to depths ranging from 6.5 to 8.5 feet for Noise Barrier 3, 7.0 feet for Noise Barrier 6, from 6.5 to 7.0 feet for Noise Barrier 8, 7.0 feet for Noise Barrier 9, from 6.5 to 7.0 feet for Noise Barrier 11, from 7.0 to 8.5 feet for Noise Barrier 12, and from 6.5 to 9.5 feet for Noise Barrier 15 will be required for the support of the proposed noise walls. The following tables detail the required minimum drilled shaft depth for each panel along each of the proposed noise barrier wall alignment.

Please note that this executive summary does not contain all the information presented in the report. The unabridged subsurface exploration report should be read in its entirety to obtain a more complete understanding of the information presented.

## 1.0 INTRODUCTION

This report is a presentation of the geotechnical exploration performed for the proposed construction of eight (8) new noise walls along SR 161 between Ulry Road and US 62 in Franklin County, Ohio. Based on the available project information, it is understood that the walls will range from 497 to 2,226 feet in length and will be 14 feet high. Noise Walls 3, 6, 8, 9, 11, 12 and 15, as designated and shown on the project documents, are included as part of this investigation. Details of the proposed noise walls are presented in Table 1.

**Table 1. Noise Wall Details**

Element	Detail
Noise Wall 3	576 feet long along the north side of SR 161 just east of Ulry Road. Maximum wall height of 14 feet.
Noise Wall 6	528 feet long along the north side of SR 161 just east of FRA-00161-19.090 L&R. Maximum wall height of 14 feet.
Noise Wall 8	1,018 feet long along the south side of SR 161 just east of FRA-00161-19.090 L&R. Maximum wall height of 14 feet.
Noise Wall 9	1,270 feet long along the north side of SR 161 just east of Harlem Rd. Maximum wall height of 14 feet.
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Noise Wall 12	497 feet long along the south side of SR 161 just east of Harlem Rd. Maximum wall height of 14 feet.
Noise Wall 15	2,226 feet long along the south side of SR 161 east and west of New Albany Road. Maximum wall height of 14 feet.

The exploration was performed within general accordance of the Ohio Department of Transportation's (ODOT) Specifications for Geotechnical Explorations (SGE), revised January 2023. The project site and general location of the proposed retaining walls are as shown on the vicinity map and boring plan presented in Appendix I.

## 2.0 GEOLOGY AND OBSERVATIONS OF THE PROJECT

### 2.1 Site Geology

Physiographically, the project site falls within Galion Glaciated Low Plateau. This region is characterized by rolling uplands which are transitional between the gently rolling Till Plains and hill Glaciated Allegheny Plateau. The soils consist of thin to thick drift with moderate relief.

Based on bedrock geology and topography maps of the area from the Ohio Department of Natural Resources (ODNR), the underlying bedrock beneath the site is Mississippian-age shales and sandstones. The bedrock surface in the vicinity of the site ranges between approximately 5 to 25 feet below the existing surface grade.

## **2.2 Existing Conditions**

The proposed project site is located along SR 161 on the northeast side of Columbus in Franklin County, Ohio. The project limits stretching between Ulry Road and US 62. Land use in the project vicinity is predominantly residential with some commercial and/or industrial purpose.

## **3.0 EXPLORATION**

A total of fifty-three (53) borings were performed as part of the overall project. The borings were performed between October 23 and December 5, 2023. The borings performed were advanced to depths ranging between 15.0 and 27.5 feet below the existing ground surface.

Boring locations were selected and field located by Rii personnel prior to drilling operations. Ground surface elevations of the as drilled boring locations were interpolated from basemaps provided by Arcadis. A schedule of the borings performed is provided in Appendix II.

The borings performed were drilled with a track mounted Diedrich D-50 rotary drilling machine, utilizing 3.25-inch inside diameter hollow-stem augers to advance the holes between sampling attempts. Standard penetration testing (SPT) and split spoon sampling were performed at 2.5-foot intervals either to the boring completion depths or to auger refusal.

The SPT, per the American Society for Testing and Materials (ASTM) designation D1586, is conducted using a 140-pound hammer falling 30.0 inches to drive a 2.0-inch outside diameter split spoon sampler 18.0 inches. Driving resistance is recorded on the boring logs in terms of blows per 6-inch interval of the driving distance. The second and third intervals are added to obtain the number of blows per foot (N). Standard penetration blow counts aid in determining soil properties applicable in foundation system design. Measured blow count ( $N_m$ ) values are corrected to an equivalent (60%) energy ratio,  $N_{60}$ , by the following equation. Both values are represented on boring logs presented in Appendix IV.

$$N_{60} = N_m * (ER/60)$$

Where:

$N_m$  = measured N value

ER = drill rod energy ratio, expressed as a percent, for the system used

The hammer for the Diedrich D-50 rig operated by Rii on this project was calibrated on March 21, 2022 and has a drill rod energy ratio 86.4 percent.

In general, for instances of no recovery from standard split spoon sampling, a 2.5-inch outside diameter split spoon sampler was driven the full length of the standard split spoon interval plus an additional 6.0 inches to obtain a representative sample. These samples are designated with a "2S" preceding the sample number on the boring logs. Only the final 6.0 inches of sample were retained for classification.

Hand penetrometer readings, which provide a rough estimate of the unconfined compression strength (UCS) of the soil, were reported on the boring logs in units of tons per square foot (tsf) and were utilized to classify the consistency of the cohesive soil in each layer. An indirect estimate of the unconfined compressive strength of the cohesive split spoon samples can also be made from a correlation with the blow counts ( $N_{60}$ ). Please note that split spoon samples are considered to be disturbed and the laboratory determination of their shear strengths may vary from undisturbed conditions.

The depth to bedrock was determined by split spoon sampler refusal and/or auger refusal on bedrock. Where the borings were extended into the bedrock, an NQ2-sized, double-tube, diamond bit core barrel (utilizing wire line equipment) was used to core the bedrock. The rock cores obtained from the borings were logged in the field and visually classified in the laboratory. The retrieved cores were analyzed to identify the type of rock, color, mineral content, bedding planes and other geological and mechanical features of interest in this project. The Rock Quality Designation (RQD) for each rock core run was calculated according to the following equation:

$$RQD = \frac{\sum \text{segments equal to or longer than 4.0 inches}}{\text{core run length}} \times 100$$

The RQD value aids in estimating the general quality of the rock and is used in conjunction with other parameters to designate the quality of the rock mass.

Upon completion of field work, the borings were backfilled with either bentonite chips and soil cuttings or were sealed with cement-bentonite grout in accordance with ODOT policy. Where borings penetrated the existing pavement, an equivalent thickness of cold patch asphalt was used to repair the pavement surface.

During drilling, field personnel prepared field logs showing the encountered subsurface conditions. Soil samples obtained from the drilling operation were preserved and sealed in glass jars and delivered to the soil laboratory. In the laboratory, the recovered soil and rock samples were visually classified, and select samples from the borings performed for the subject structures were tested, as noted in Table 2.

**Table 2. Laboratory Test Schedule**

Laboratory Test	Test Designation	Number of Tests Performed
Natural Moisture Content	ASTM D 2216	439
Plastic and Liquid Limits	AASHTO T89, T90	83
Gradation – Sieve/Hydrometer	AASHTO T88	83
Unconfined Compressive Strength of Intact Rock	ASTM D7012, Method C	6
Point Load Strength Index	ASTM D5731	2

The tests performed are necessary to classify the existing soil and rock according to the Ohio Department of Transportation (ODOT) classification system and to estimate engineering properties of importance for foundation design and construction recommendations. Results of the laboratory testing are presented on the boring logs in Appendix IV and also in Appendix V.

## 4.0 FINDINGS

Interpreted engineering logs have been prepared based on the field logs, visual examination of samples and laboratory test results. Classification follows the version of the ODOT Specifications for Geotechnical Explorations (SGE) at the time the exploration borings were performed. The following is a summary of what was found in the test borings and what is represented on the boring logs. A description of the soil and rock terms used throughout this report is presented in Appendix III.

### 4.1 Surface Materials

The borings were generally performed in the vicinity of the proposed noise wall alignments. All borings, except B-038-0-23, encountered topsoil thicknesses between 1 inch and 10 inches. Boring B-038-0-23 encountered 3.0 inches of asphalt overlying 6.5 inches of concrete overlying 3.5 inches of aggregate base.

### 4.2 Subsurface Soils

Underlying the surficial soils, the natural soils were encountered, consisting of both cohesive and granular deposits. The natural cohesive soils were described as sandy silt, silt and clay, silty clay, and clay (ODOT A-4a, A-6a, A-6b, A-7-6). The granular soils were described as gravel, gravel with sand, gravel with sand and silt, gravel with sand and silt and clay, and coarse and fine sand (ODOT A-1-a, A-1-b, A-2-4, A-2-6, A-3a).

The shear strength and consistency of the cohesive soils are primarily derived from the hand penetrometer values (HP). The cohesive soils encountered ranged from medium

stiff ( $0.5 < HP \leq 1.0$  tsf) to hard ( $HP > 4.0$  tsf). The unconfined compressive strength of the cohesive soil samples tested, obtained from the hand penetrometer, ranged from 0.75 to over 4.5 tsf (limit of instrument). The relative density of granular soils is primarily derived from SPT blow counts ( $N_{60}$ ). Based on the SPT blow counts obtained, the granular soils encountered ranged from loose ( $5 < N_{60} \leq 10$  blows per foot [bpf]) to very dense ( $N_{60} > 50$  bpf). Blow counts recorded from the SPT sampling within the granular soil deposits ranged from 9 to 96 bpf.

Natural moisture contents of the soil samples tested ranged from 3 to 25 percent. The natural moisture contents of the cohesive soil samples tested for plasticity ranged from 14 percent below to 5 percent above their corresponding plastic limits. In general, the soil exhibited natural moisture contents considered to be significantly below to significantly above optimum moisture levels.

#### **4.3 Bedrock**

Bedrock was encountered in borings B-001-0-23 through B-004-0-23, B-018-0-23, through B-024-0-23, B-027-0-23, B-028-0-23, and B-038-0-23 through B-053-0-23 at depths ranging from 4.3 to 23.0 feet beneath the existing ground surface. The bedrock was described as highly weathered gray and brown sandstone, highly weathered to severely weathered gray and black silt, and highly weathered gray shalestone.

#### **4.4 Groundwater**

Groundwater seepage was encountered in three (3) of the borings at depths ranging from 14.0 to 22.4 feet below the ground surface. Significant groundwater flow was encountered during drilling (initial water level) in twenty-six (26) of the borings at depths ranging from 12.0 to 21.0 feet below the existing ground surface. Measurable groundwater was observed at the completion of drilling in seventeen (17) of the borings at depths ranging from 7.8 to 20.5 feet below existing grade.

Please note that short-term water level readings, especially in cohesive soils, are not necessarily an accurate indication of the actual groundwater level. In addition, groundwater levels or the presence of groundwater are considered to be dependent on seasonal fluctuations in precipitation.

A more comprehensive description of what was encountered during the drilling process may be found on the individual boring logs in Appendix IV.

### **5.0 ANALYSES AND RECOMMENDATIONS**

Data obtained from the subsurface exploration has been used to determine the foundation support capabilities for the soils and bedrock encountered at the site. These parameters have been used to provide guidelines for the design of foundation systems for the proposed noise walls, as well as the construction specifications related to the placement

of foundation systems and general earthwork recommendations, which are discussed in the following paragraphs.

Due to revisions in the proposed noise wall alignments after select borings were advanced, data from fifty (50) borings was utilized in the analysis.

### **5.1 Drilled Shaft Foundations (Noise Barriers 3, 6, 8, 9, 11, 12 and 15)**

The required shaft embedment for the proposed Noise Barriers 3, 6, 8, 9, 11, 12, and 15 was determined in accordance with Section 802.1.2 of the ODOT Bridge Design Manual (BDM). Per ODOT BDM Section 802.1.2, the required embedment depth for the supporting drilled shafts is determined using energy and depth corrected SPT values and selecting the required embedment depth based on either the average or critical corrected SPT value from Table 802.1.2-1 for granular soils or 802.1.2-2 for cohesive soils. Based on the plans and profile information provided, the anticipated panel heights and spacing for each noise barrier are as presented in Table 3.

**Table 3. Noise Walls 3, 6, 8, 9, 11, 12 and 15 – Panel Heights and Spacing Information**

Noise Barrier	Noise Barrier 3	Noise Barrier 6	Noise Barrier 8	Noise Barrier 9	Noise Barrier 11	Noise Barrier 12	Noise Barrier 15
Panel Heights (feet)	14	14	14	14	14	14	14
Maximum Panel Spacing Center-to-Center of the Drilled Shaft (feet)	24	24	24	24	24	24	24

Based on cross section information provided, the transverse cross-slopes along the alignment of Noise Barrier 3 range from 3:1 and transition to level. The transverse cross-slopes along the Noise Barrier 6 range from 3:1 to 4:1. The transverse cross-slopes along the alignment of Noise Barrier 8 are considered to be generally level with a localized slope of 5:1. The transverse cross-slopes along the alignment of Noise Barrier 9 range from 3:1 to 5:1. The transverse cross-slopes along the alignment of Noise Barrier 11 range from level to 5:1. The transverse cross-slopes along the alignment of Noise Barrier 12 range from 2:1 to 5:1. Finally, the transverse cross-slopes along the alignment of Noise Barrier 15 range from 3:1 to level.

In general, the analysis indicates that 2.5-foot diameter drilled shafts excavated to depths ranging from 6.5 to 8.5 feet for Noise Barrier 3, 7.0 feet for Noise Barrier 6, from 6.5 to 7.0 feet for Noise Barrier 8, 7.0 feet for Noise Barrier 9, from 6.5 to 7.0 feet for Noise Barrier 11, from 7.0 to 8.5 feet for Noise Barrier 12, and from 6.5 to 9.5 feet for Noise Barrier 15 will be required for the support of the proposed noise walls. The following tables detail the required minimum drilled shaft depth for each panel along each of the proposed

noise barrier wall alignment. Calculations for the noise barrier foundation depths are provided in Appendix VI.

**Table 4. Noise Barrier 3 Foundation Depth Requirements**

From Panel	To Panel	Length (feet)	Representative Boring	Post Spacing (feet)	Barrier Height (feet)	Transverse Ground Slope	Proposed Shaft Depth (feet)
1	5	96	B-001-0-23	24	14	3:1	7.0
6	13	168	B-002-0-23	24	14	4:1	8.5
14	21	168	B-003-0-23	24	14	5:1	7.0
22	25	72	B-004-0-23	24	14	Level	6.5

**Table 5. Noise Barrier 6 Foundation Depth Requirements**

From Panel	To Panel	Length (feet)	Representative Boring	Post Spacing (feet)	Barrier Height (feet)	Transverse Ground Slope	Proposed Shaft Depth (feet)
1	4	72	B-005-0-23	24	14	3:1	7.0
5	15	168	B-006-0-23	12 to 24	14	4:1	7.0
16	22	144	B-007-0-23	24	14	4:1	7.0
23	26	72	B-008-0-23	24	14	4:1	7.0

**Table 6. Noise Barrier 8 Foundation Depth Requirements**

From Panel	To Panel	Length (feet)	Representative Boring	Post Spacing (feet)	Barrier Height (feet)	Transverse Ground Slope	Proposed Shaft Depth (feet)
1	8	168	B-012-0-23	24	14	Level	6.5
9	16	168	B-013-0-23	24	14	Level	6.5
14	24	168	B-014-0-23	24	14	Level	6.5
25	33	192	B-015-0-23	24	14	Level	6.5
34	41	168	B-016-0-23	24	14	Level	6.5
42	52	188	B-017-0-23	14 to 24	14	Level	6.5
53	60	168	B-018-0-23	24	14	5:1	7.0
61	68	168	B-019-0-23	24	14	Level	6.5
69	75	144	B-020-0-23	24	14	Level	6.5
76	79	60	B-021-0-23	12 to 24	14	Level	6.5

**Table 7. Noise Barrier 9 Foundation Depth Requirements**

<b>From Panel</b>	<b>To Panel</b>	<b>Length (feet)</b>	<b>Representative Boring</b>	<b>Post Spacing (feet)</b>	<b>Barrier Height (feet)</b>	<b>Transverse Ground Slope</b>	<b>Proposed Shaft Depth (feet)</b>
1	5	88	B-031-0-23	16 to 24	14	3:1	7.0
6	14	168	B-032-0-23	16 to 24	14	3:1	7.0
15	23	192	B-033-0-23	24	14	4:1	7.0
24	31	168	B-034-0-23	24	14	3:1	7.0
32	39	168	B-035-0-23	24	14	5:1	7.0
40	48	192	B-036-0-23	24	14	4:1	7.0
49	57	150	B-037-0-23	17 to 24	14	3:1	7.0

**Table 8. Noise Barrier 11 Foundation Depth Requirements**

<b>From Panel</b>	<b>To Panel</b>	<b>Length (feet)</b>	<b>Representative Boring</b>	<b>Post Spacing (feet)</b>	<b>Barrier Height (feet)</b>	<b>Transverse Ground Slope</b>	<b>Proposed Shaft Depth (feet)</b>
1	5	96	B-022-0-23	24	14	Level	6.5
6	13	168	B-023-0-23	24	14	5:1	7.0
14	21	168	B-024-0-23	24	14	Level	6.5
22	30	192	B-025-0-23	24	14	Level	6.5
31	38	168	B-026-0-23	24	14	5:1	7.0
39	46	168	B-027-0-23	24	14	Level	6.5
47	55	192	B-028-0-23	24	14	Level	6.5
56	63	168	B-029-0-23	24	14	Level	6.5
64	67	72	B-030-0-23	24	14	Level	6.5

**Table 9. Noise Barrier 12 Foundation Depth Requirements**

<b>From Panel</b>	<b>To Panel</b>	<b>Length (feet)</b>	<b>Representative Boring</b>	<b>Post Spacing (feet)</b>	<b>Barrier Height (feet)</b>	<b>Transverse Ground Slope</b>	<b>Proposed Shaft Depth (feet)</b>
1	6	72	B-038-0-23	12 to 24	14	2:1	7.0
7	14	168	B-039-0-23	24	14	5:1	7.0
15	23	166	B-040-0-23	8 to 24	14	5:1	7.0
23	25	24	B-041-0-23	19 to 24	14	5:1	8.5

**Table 10. Noise Barrier 15 (Sta. 1500+00 to 1502+40) Foundation Depth Requirements**

From Panel	To Panel	Length (feet)	Representative Boring	Post Spacing (feet)	Barrier Height (feet)	Transverse Ground Slope	Proposed Shaft Depth (feet)
1	6	120	B-042-0-23	15 to 24	14	4:1	7.0
7	13	105	B-043-0-23	15 to 24	14	4:1	7.0

**Table 11. Noise Barrier 15 (Sta. 1504+27 to 1518+43) Foundation Depth Requirements**

From Panel	To Panel	Length (feet)	Representative Boring	Post Spacing (feet)	Barrier Height (feet)	Transverse Ground Slope	Proposed Shaft Depth (feet)
14	17	72	B-044-0-23	24	14	3:1	7.0
18	25	168	B-045-0-23	24	14	3:1	7.0
26	34	192	B-046-0-23	24	14	3:1	7.0
35	42	168	B-047-0-23	24	14	4:1	7.0
43	50	168	B-048-0-23	24	14	5:1	7.0
51	59	192	B-049-0-23	24	14	Level	6.5
60	67	168	B-050-0-23	24	14	Level	6.5
68	73	120	B-0051-23	24	14	5:1	8.5

**Table 12. Noise Barrier 15 (Sta. 1518+43 to 1522+26) Foundation Depth Requirements**

From Panel	To Panel	Length (feet)	Representative Boring	Post Spacing (feet)	Barrier Height (feet)	Transverse Ground Slope	Proposed Shaft Depth (feet)
74	77	72	B-051-0-23	24	14	5:1	8.5
78	84	144	B-052-0-23	24	14	5:1	7.0
85	88	72	B-053-0-23	24	14	Level	9.5

The drilled shaft excavations should be carefully observed by a geotechnical engineering representative as soon as possible following excavation to assure adequacy. If inadequate bearing soil is encountered, the shaft excavations should be continued into more suitable end bearing soils or to bedrock. Since water has an adverse effect on cohesive soil, drilled shaft concrete should be placed as soon as possible following

excavation, preferably the same day to reduce the potential for water related damage. Drilled shaft excavations should be kept dry and clean until concrete is placed to reduce damage to the bearing surfaces. For details about groundwater observations, refer to Section 4.4.

### **5.1.1 *Drilled Shaft Considerations***

The minimum requirements for proper inspection of drilled shaft construction are as follows:

- A qualified inspector should record the material types being removed from the hole as excavation proceeds.
- The use of casing for drilled shafts is recommended if caving material and/or groundwater is encountered at any time during the drilling of the shaft, or if groundwater seepage occurs in the drilled shaft.
- The placement of all concrete for the drilled shafts shall follow the American Concrete Institute's Design and Construction of Drilled Piers (ACI 336.3R-93).
- Concrete placed freefall should not be allowed to hit the sidewalls of the excavation and should not pass through any water. Therefore, concrete should be placed by tremie method if groundwater is encountered during construction of the drilled shafts.
- If concrete is placed by tremie method, it must be done so with an adequate head to displace water or slurry if groundwater has entered the drilled shaft (all tremie procedures shall follow applicable ACI specifications).
- The volume of concrete should be checked to ensure voids did not result during extraction of the casing.
- Pulling casing with insufficient concrete inside should be restricted.
- The bottom of drilled shaft excavations should be clean and free of loose material. Any loose material observed should be removed using a clean-out bucket (muck bucket).

In addition, it is recommended that, if casing is used, it be pulled after the concrete is poured, allowing for reuse of the casing, and eliminating reduction of side resistance (between soil and concrete).

## **5.2 Lateral Earth Pressure**

For the soil types encountered in the borings, the “in-situ” unit weight ( $\gamma$ ), cohesion ( $c$ ), effective angle of friction ( $\phi'$ ), and lateral earth pressure coefficients for at-rest conditions



$(k_o)$ , active conditions ( $k_a$ ), and passive conditions ( $k_p$ ) have been estimated and are provided in Table 13 and Table 14.

**Table 13. Estimated Undrained (Short-term) Soil Parameters for Design**

Soil Type	$\gamma$ (pcf) <sup>1</sup>	$c$ (psf)	$\phi$	$k_a$	$k_o$	$k_p$
Soft to Medium Stiff Cohesive Soil	110	500	0°	N/A	N/A	N/A
Stiff Cohesive Soil	120	1,500	0°	N/A	N/A	N/A
Very Stiff to Hard Cohesive Soil	125	2,500	0°	N/A	N/A	N/A
Very Loose to Loose Granular Soil	120	0	28°	0.36	0.53	2.77
Medium Dense to Dense Granular Soil	125	0	32°	0.31	0.47	3.25
Dense to Very Dense Granular Soil	130	0	35°	0.27	0.43	3.69
Compacted Cohesive Engineered Fill	120	2,000	0°	N/A	N/A	N/A
Compacted Granular Engineered Fill	125	0	32°	0.31	0.47	3.25

- When below groundwater table, use effective unit weight,  $\gamma' = \gamma - 62.4$  pcf and add hydrostatic water pressure.

**Table 14. Estimated Drained (Long-term) Soil Parameters for Design**

Soil Type	$\gamma$ (pcf) <sup>1</sup>	$c'$ (psf)	$\phi'$	$k_a$	$k_o$	$k_p$
Soft to Medium Stiff Cohesive Soil	120	0	22°	0.45	0.63	2.20
Stiff Cohesive Soil	125	0	26°	0.39	0.56	2.56
Very Stiff to Hard Cohesive Soil	125	0	28°	0.36	0.53	2.77
Very Loose to Loose Granular Soil	120	0	28°	0.36	0.53	2.77
Medium Dense to Dense Granular Soil	125	0	32°	0.31	0.47	3.25
Dense to Very Dense Granular Soil	130	0	35°	35°	0.27	0.43
Compacted Cohesive Engineered Fill	120	0	28°	0.36	0.53	2.77
Compacted Granular Engineered Fill	125	0	32°	0.31	0.47	3.25

- When below groundwater table, use effective unit weight,  $\gamma' = \gamma - 62.4$  pcf and add hydrostatic water pressure.

These parameters are considered appropriate for the design of all subsurface structures and any excavation support systems. Subsurface structures (where the top of the structure is restrained from movement) should be designed based on at-rest conditions ( $k_o$ ). For proposed temporary retaining structures (where the top of the structure is allowed to move), earth pressure distributions should be based on active ( $k_a$ ) and passive ( $k_p$ ) conditions.

These recommendations do not take into consideration the effect of any surcharge loading or a sloped ground surface (a flat surface is assumed). Earth pressures on excavation support systems will be dependent on the type of sheeting and method of bracing or anchorage. Surcharge loads, such as that imposed by traffic loading, will create additional lateral loading on the subsurface structures and excavation support systems. The resulting lateral earth pressure should be evaluated based on active ( $k_a$ ) and at-rest ( $k_o$ ) conditions and the anticipated magnitude of the loading.

Temporary retaining structures, such as sheet pile system, should be designed using the undrained soil parameters provided in Table 13, and the design should follow all applicable guidelines for the type of retaining structure utilized. Permanent retaining and subsurface structures should be designed using the drained soil parameters provided in Table 14. Regardless of whether the retaining structure is temporary or permanent, the effective unit weight ( $\gamma' = \gamma - 62.4 \text{pcf}$ ) plus the hydrostatic water pressure ( $\gamma_w * h_w$ , where  $h_w$  is the height of water behind the wall above the base of the wall) should be utilized below the design groundwater level. The lateral earth pressure coefficients should only be applied to the horizontal pressure resulting from the effective overburden pressure, and should not be applied to the hydrostatic water pressure.

## 5.3 Construction Considerations

All site work shall conform to local codes and to the latest ODOT Construction and Materials Specifications (CMS), including that all excavation and embankment preparation and construction should follow ODOT Item 200 (Earthwork).

### 5.3.1 Excavation Considerations

All excavations should be shored / braced or laid back at a safe angle in accordance with Occupational Safety and Health Administration (OSHA) guidelines. During excavation, if slopes cannot be laid back to OSHA Standards due to adjacent structures or other obstructions, temporary shoring may be required. The following table should be utilized as a general guide for implementing OSHA guidelines when estimating excavation back slopes at the various boring locations. Actual excavation back slopes must be field verified by qualified personnel at the time of excavation in strict accordance with OSHA guidelines.

**Table 15. Excavation Back Slopes**

Soil	Maximum Back Slope	Notes
Soft to Medium Stiff Cohesive	1.5 : 1.0	Above Ground Water Table and No Seepage
Stiff Cohesive	1.0 : 1.0	Above Ground Water Table and No Seepage
Very Stiff to Hard Cohesive	0.75 : 1.0	Above Ground Water Table and No Seepage
All Granular & Cohesive Soil Below Ground Water Table or with Seepage	1.5 : 1.0	None

### **5.3.2 Groundwater Considerations**

Based on the groundwater observations made during drilling, groundwater may be encountered during construction. Where groundwater is encountered, proper groundwater control should be employed and maintained to prevent disturbance to excavation bottoms consisting of cohesive soil, and to prevent the possible development of a quick or "boiling" condition where soft silts and/or fine sands are encountered. It is preferable that the groundwater level, if encountered, be maintained at least 36 inches below the deepest excavation. Any seepage or groundwater encountered within fine-grained or cohesive soils at this site should be able to be controlled by pumping from temporary sumps. Based on the recommended lengths of drilled shafts and proposed shaft elevations, it is not anticipated that groundwater will be encountered within granular soil layers. However, where excavations encounter groundwater within granular layers, more robust dewatering measures such as well points would be needed to control groundwater. Additional measures may be required depending on seasonal fluctuations of the groundwater level. Note that determining and maintaining actual groundwater levels during construction is the responsibility of the contractor.

## **6.0 LIMITATIONS OF STUDY**

The above recommendations are predicated upon construction inspection by a qualified soil technician under the direct supervision of a professional geotechnical engineer. Adequate testing and inspection during construction are considered necessary to assure an adequate foundation system and are part of these recommendations.

The recommendations for this project were developed utilizing soil and bedrock information obtained from the test borings that were made at the proposed site for the current investigation. Resource International is not responsible for the data, conclusions, opinions or recommendations made by others during previous investigations at this site. At this time we would like to point out that soil borings only depict the soil and bedrock conditions at the specific locations and time at which they were made. The conditions at other locations on the site may differ from those occurring at the boring locations.

The conclusions and recommendations herein have been based upon the available soil and bedrock information and the design details furnished by a representative of the owner of the proposed project. Any revision in the plans for the proposed construction from those anticipated in this report should be brought to the attention of the geotechnical engineer to determine whether any changes in the foundation or earthwork recommendations are necessary. If deviations from the noted subsurface conditions are encountered during construction, they should also be brought to the attention of the geotechnical engineer.

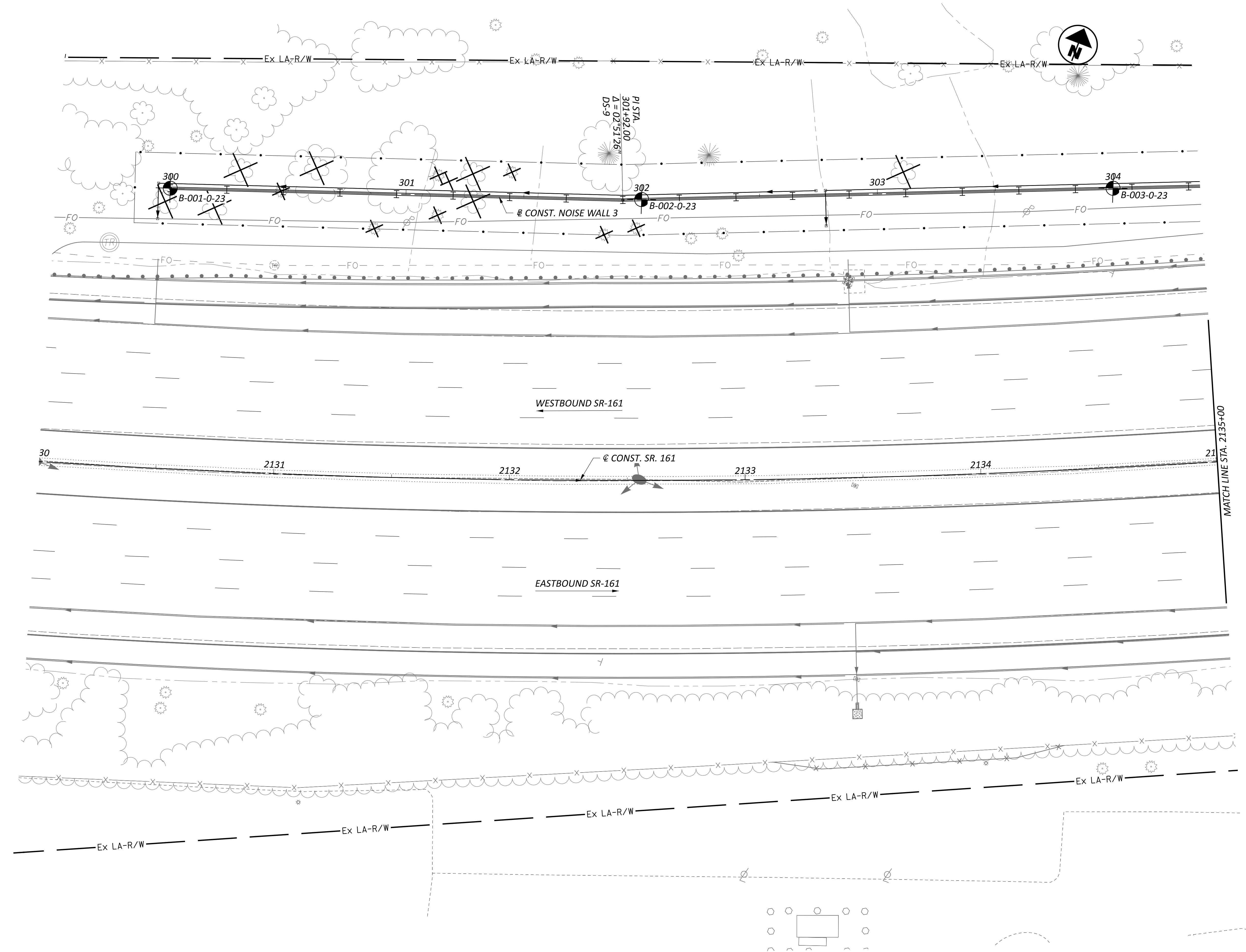
The scope of our services does not include any environmental assessment or investigation for the presence or absence of hazardous or toxic materials in the soil, groundwater or surface water within or beyond the site studied. Any statements in this report or on the test boring logs regarding odors, staining of soils or other unusual conditions observed are strictly for the information of our client.

Our professional services have been performed, our findings obtained and our recommendations prepared in accordance with generally accepted geotechnical engineering principles and practices. Resource International is not responsible for the conclusions, opinions or recommendations made by others based upon the data included.

**APPENDIX I**  
**BORING PLAN**

FRA-161-15.80 NOISE WALLS

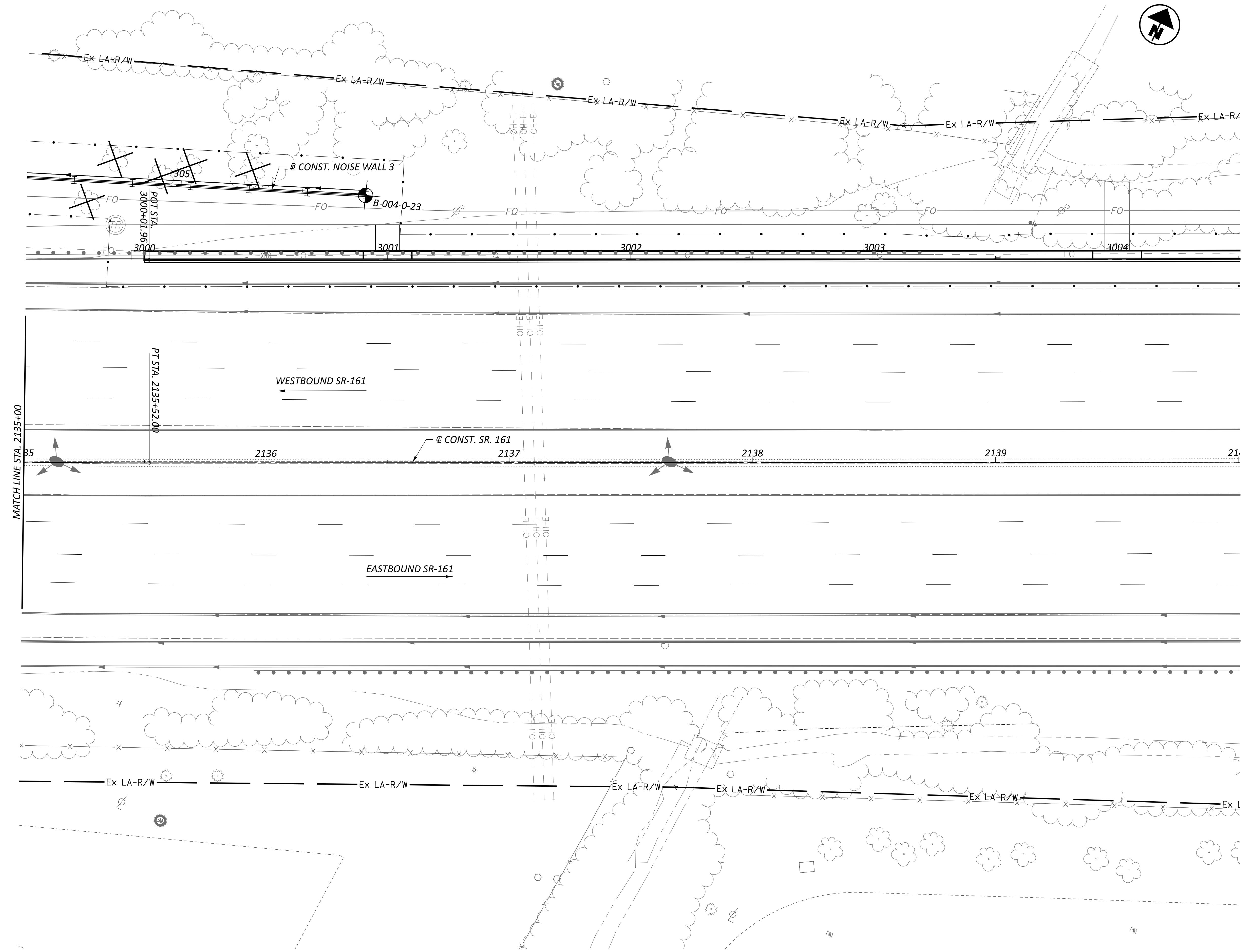
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DESIGN AGENCY	
	
350 PRESIDENTIAL GATEWAY COLUMBUS, OHIO 43231 (614) 823-4949	
DESIGNER	JAS
REVIEWER	
DEK MM-DD-YY	
PROJECT ID	
117607	
HEET	TOTAL
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STA. 2135+00.00 TO STA. 2140+00.00

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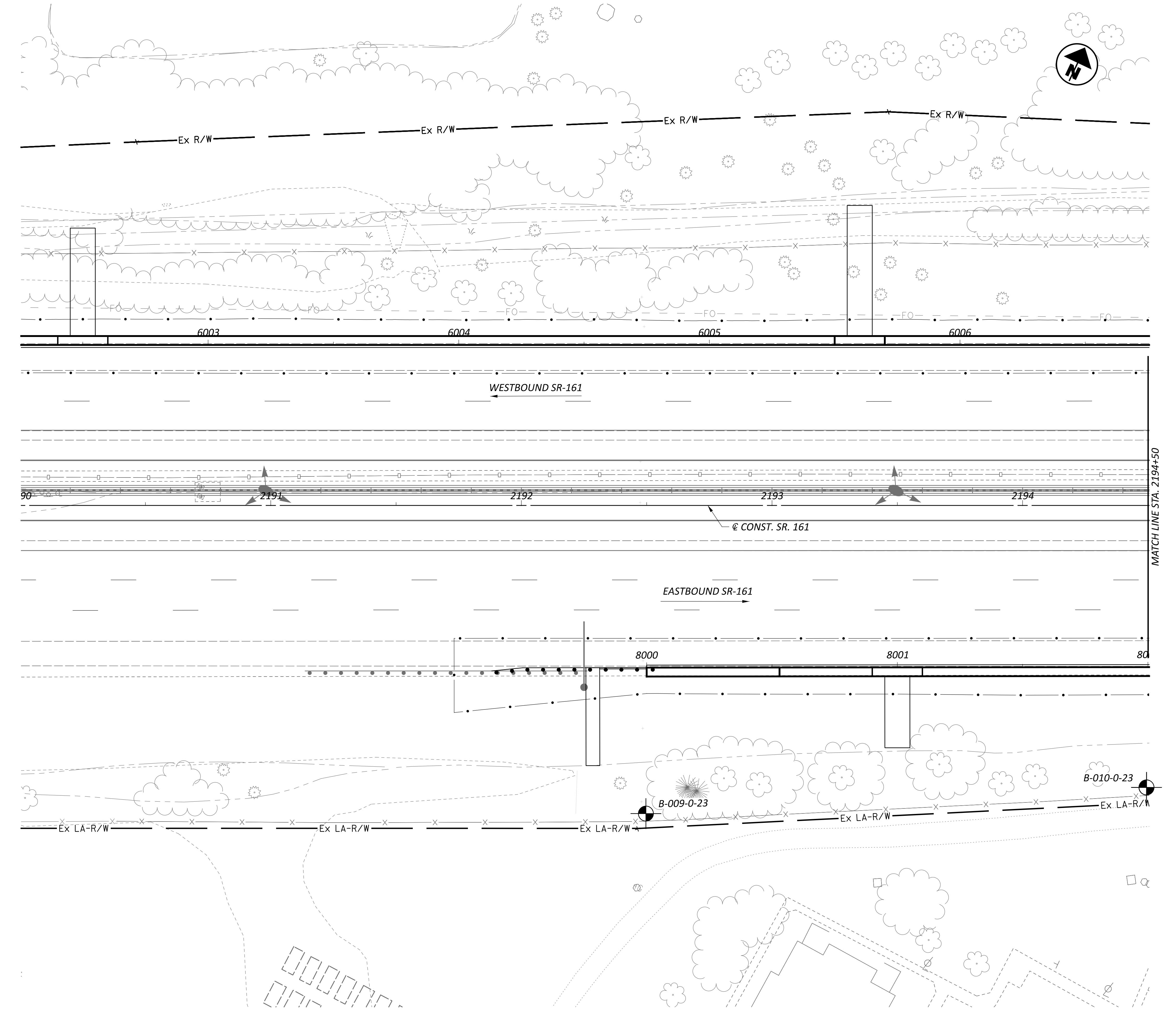
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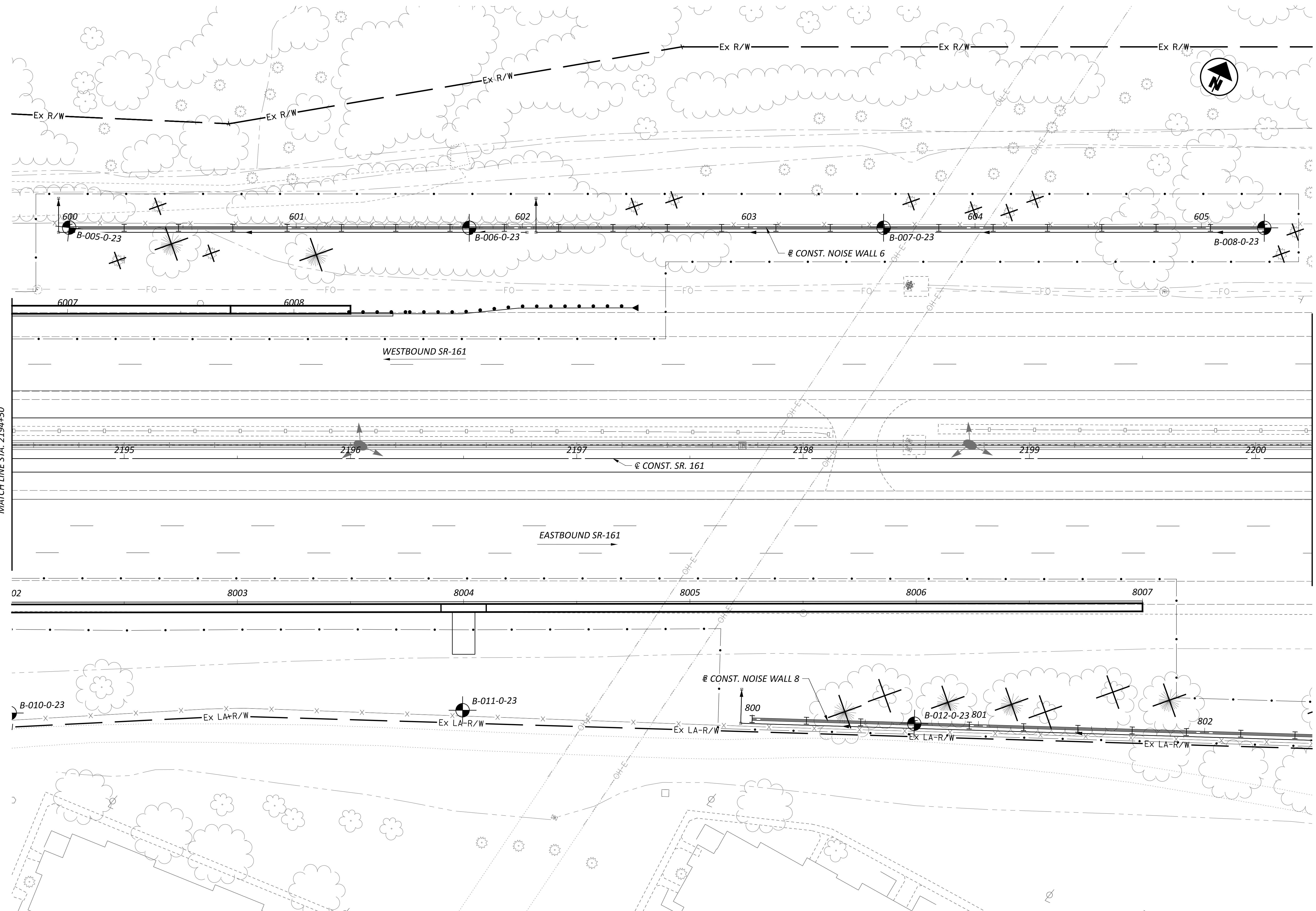
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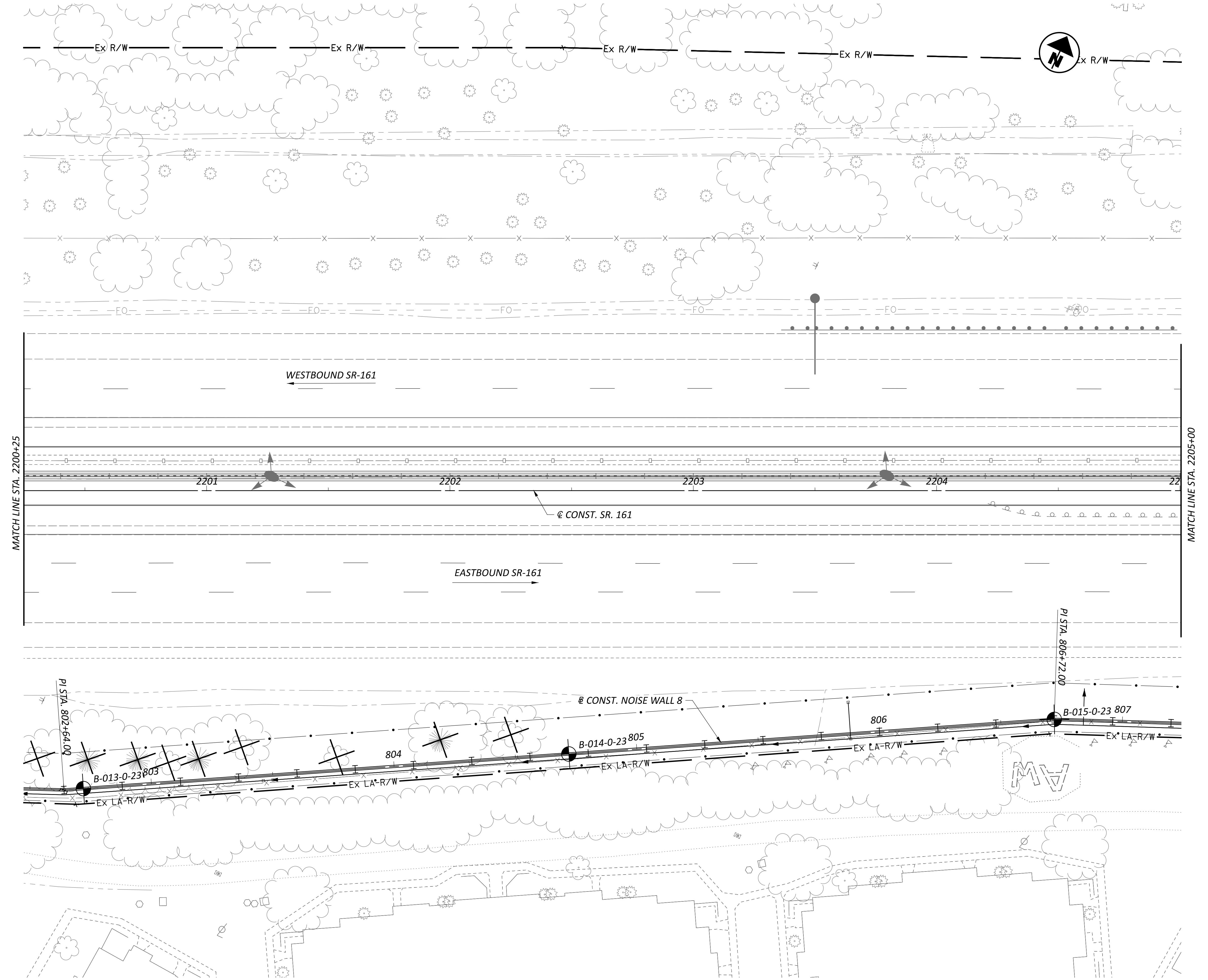
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MATCH LINE STA. 2200+25

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REVIEWER  
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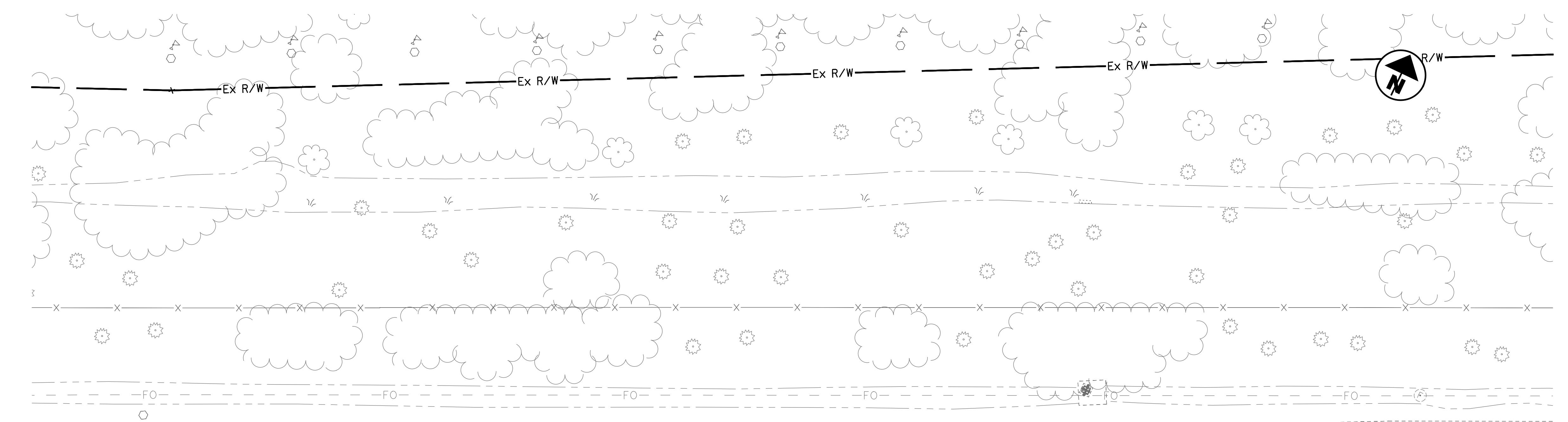


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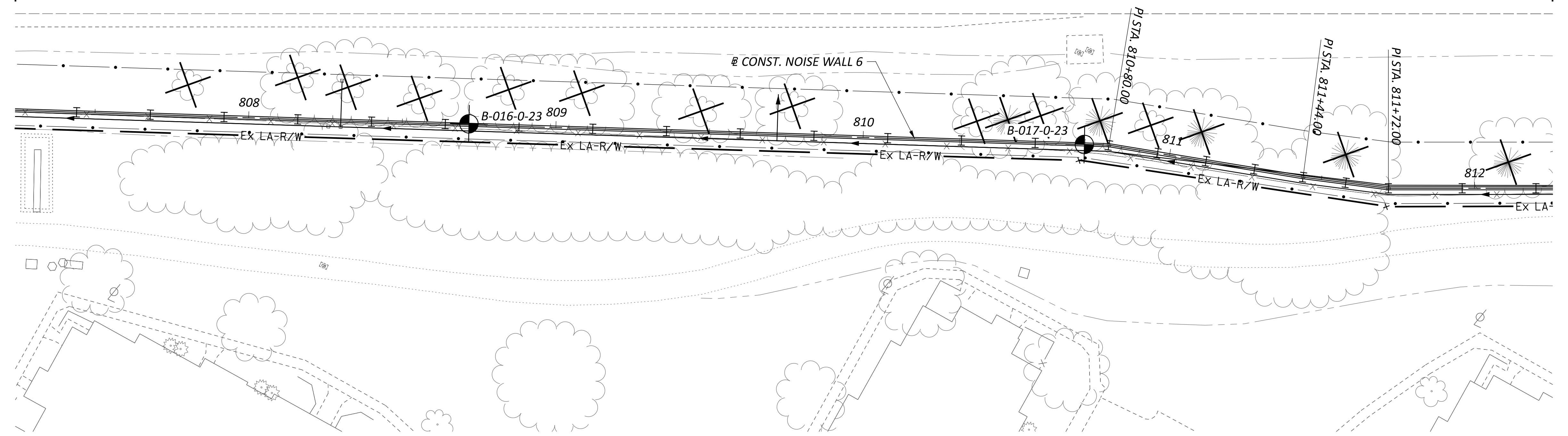
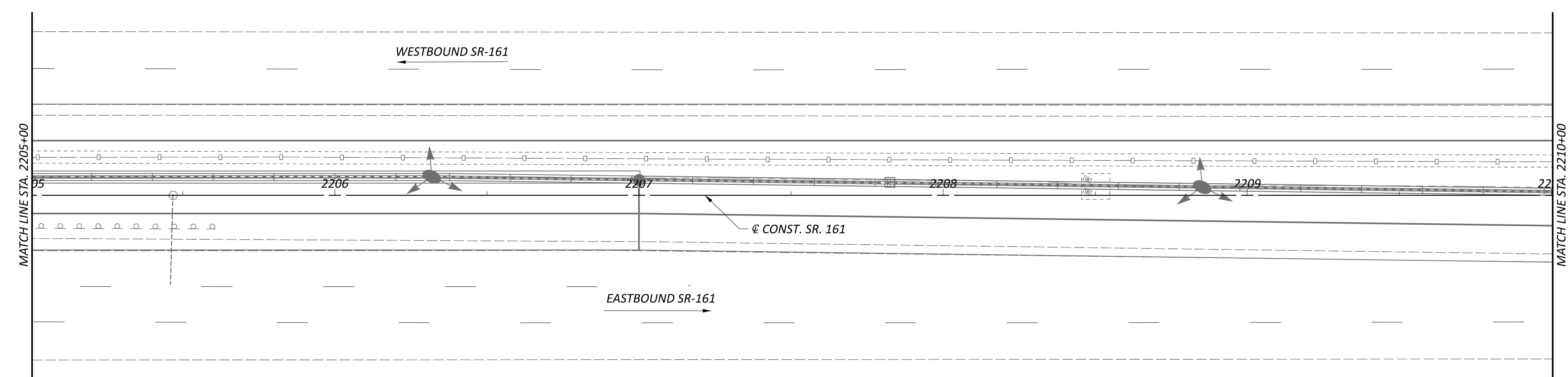
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BORING PLAN NOISE WALL 8  
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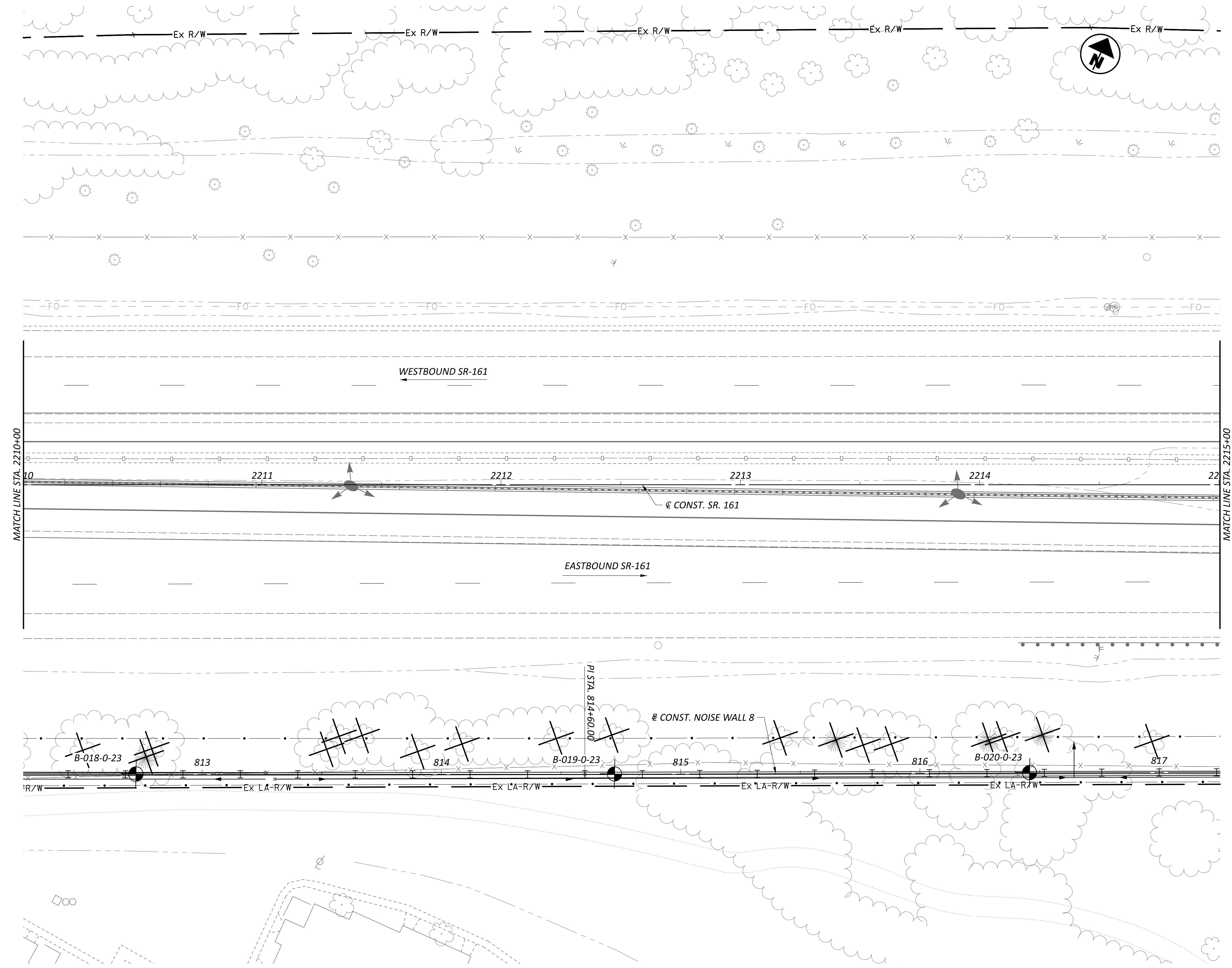


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DESIGNER  
JAS  
REVIEWER  
DEK MM-DD-Y  
PROJECT ID  
117507  
SHEET TOTAL  
P.O. 0

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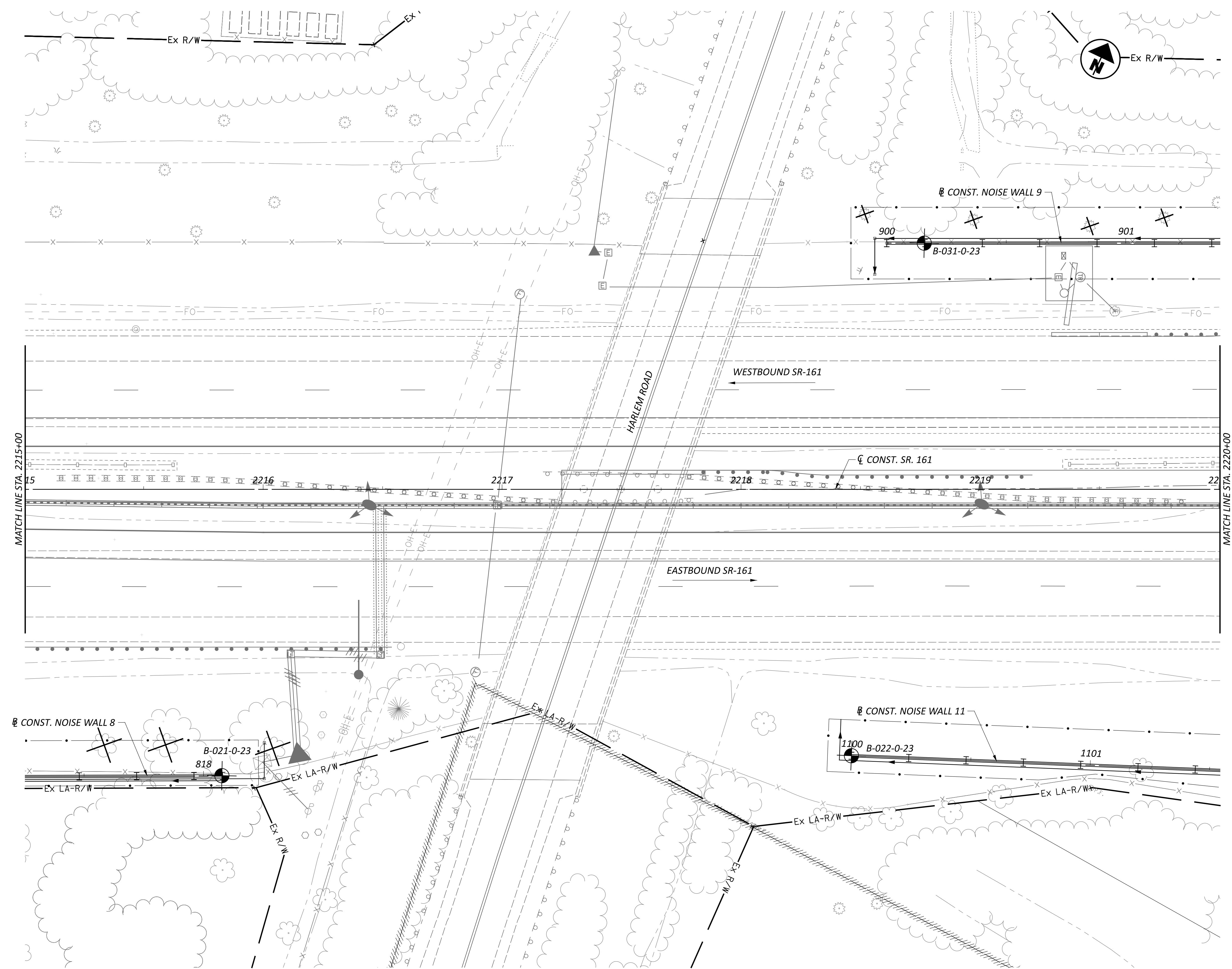


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**JAS**  
REVIEWER  
**DEK MM-DD-YN**  
PROJECT ID  
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SHEET TOTAL  
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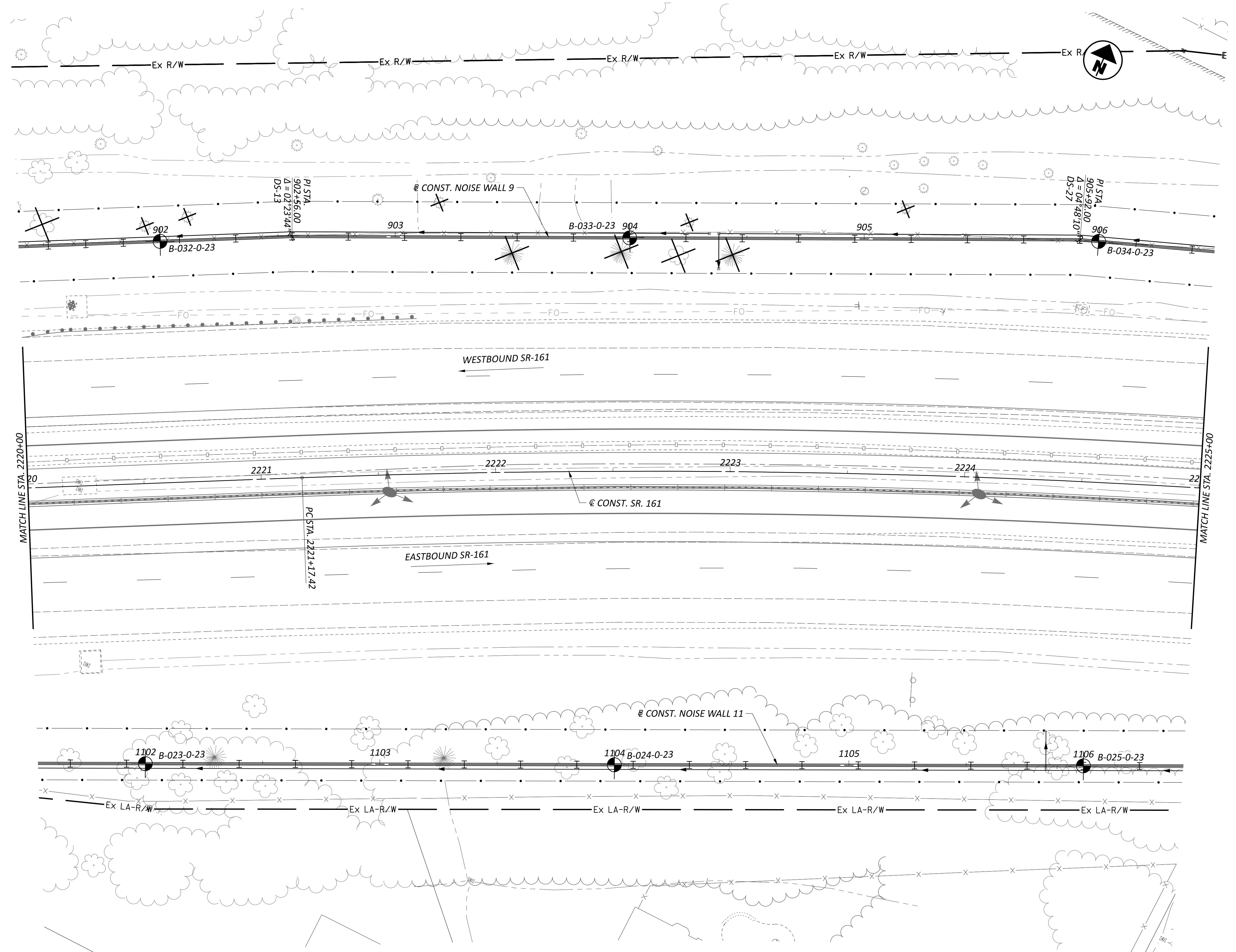
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REVIEWER DEK 1/1924  
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**BORING PLAN - NOISE WALLS 9 AND 11  
STA. 2220+00.00 TO STA. 2225+00.00**

HORIZONTAL  
SCALE IN FEET



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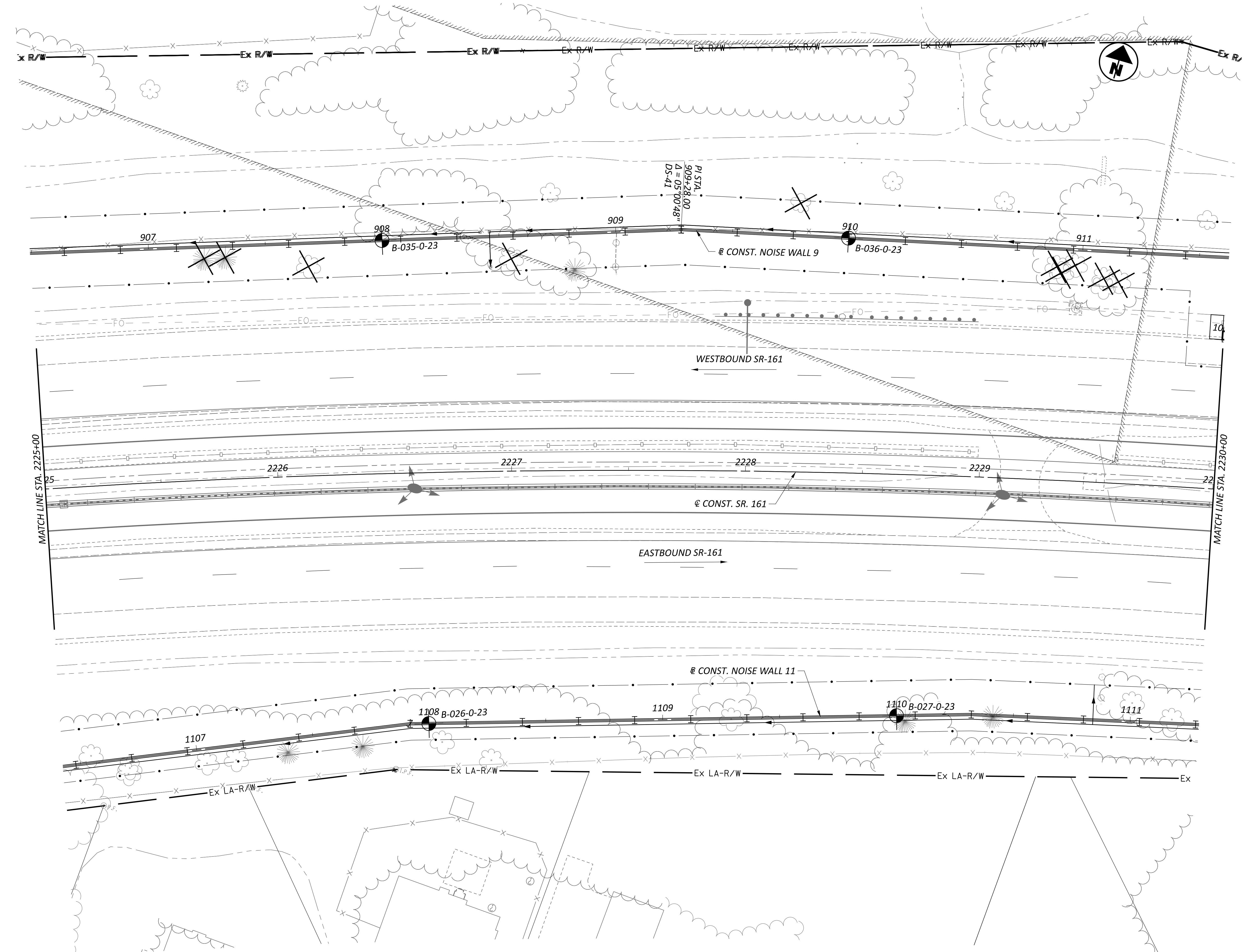
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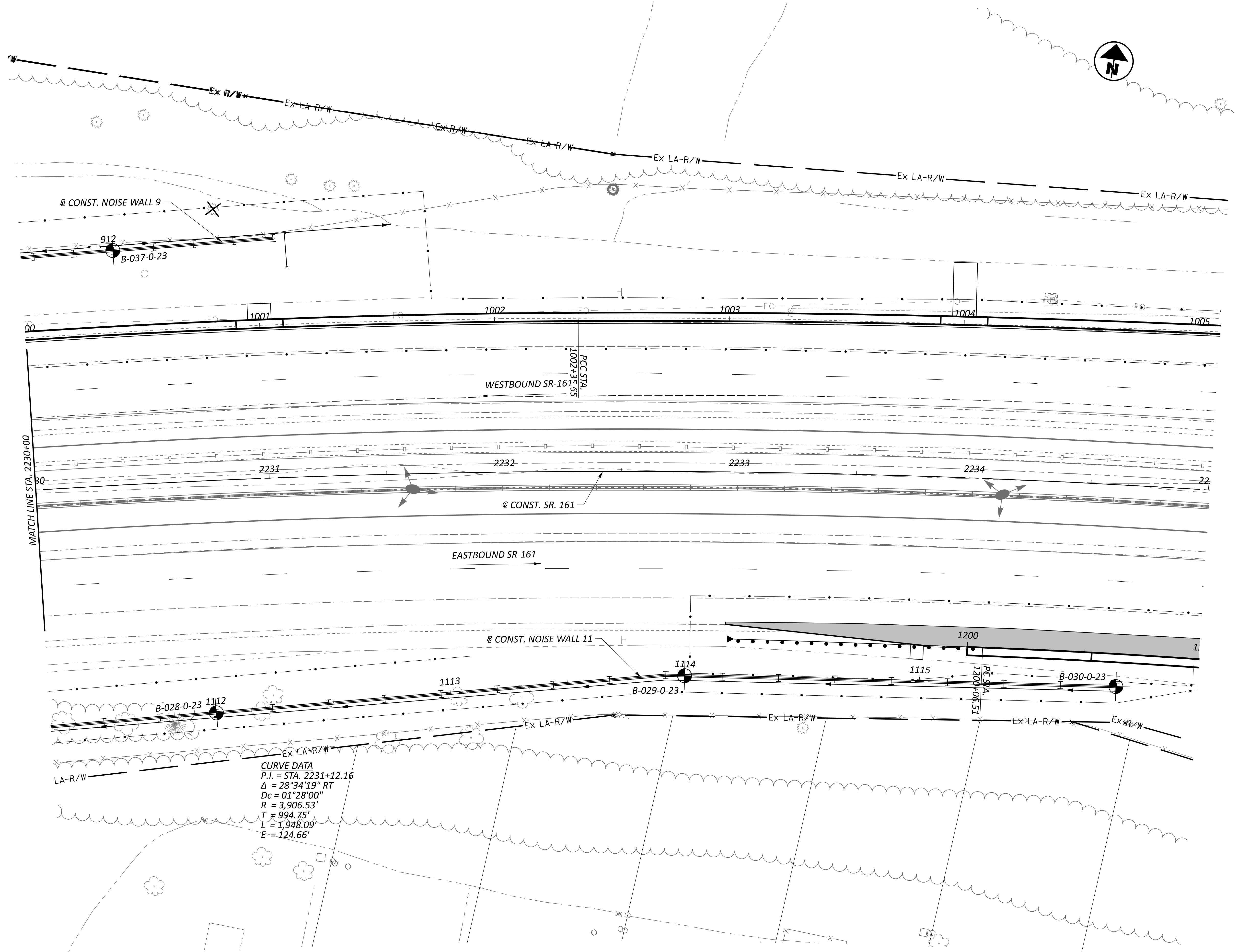
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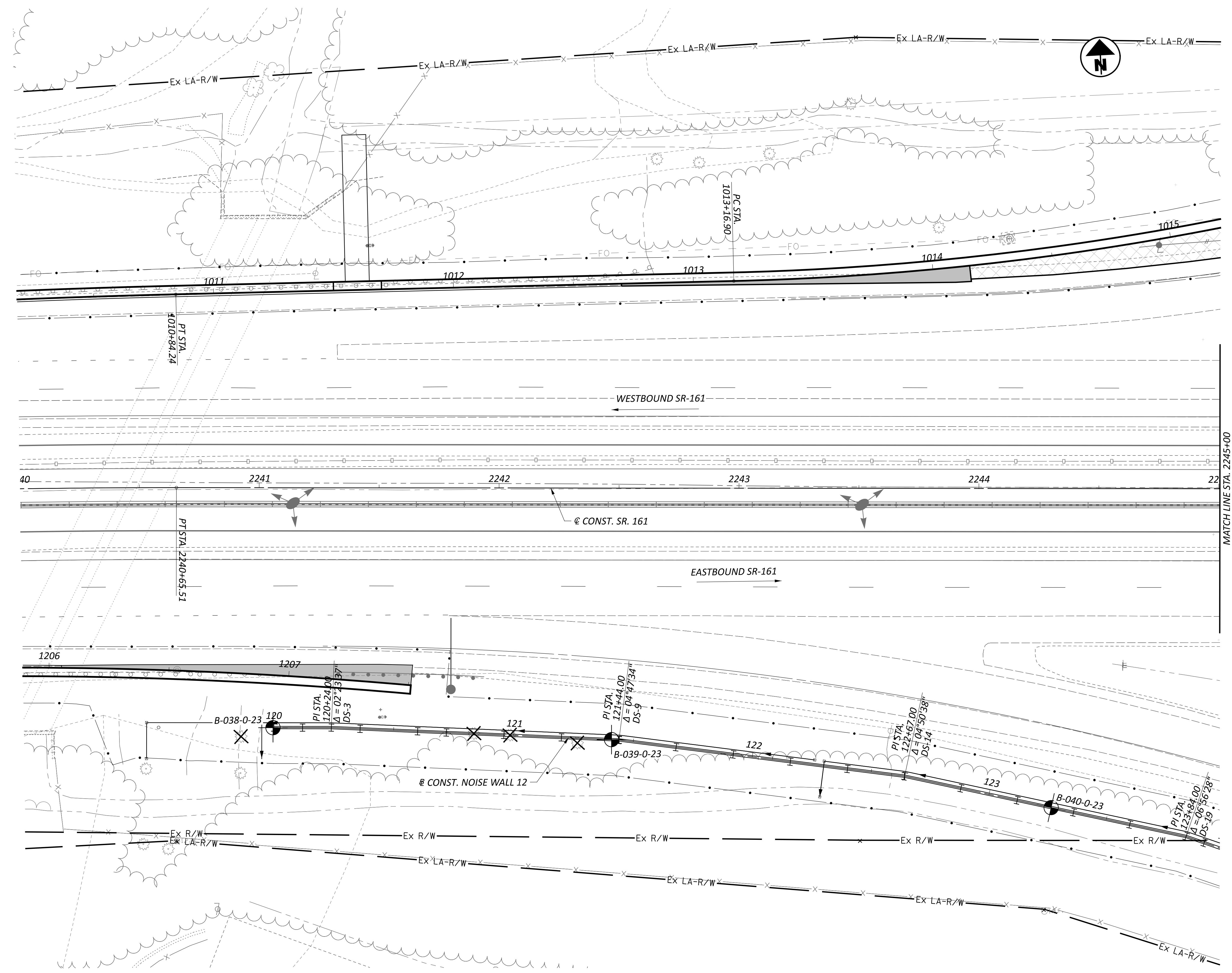
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REVIEWER  
**DEK MM-DD-Y**  
PROJECT ID  
**117607**  
SHEET TOTAL  
**P.O** 0

HORIZONTAL SCALE IN FEET  
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FRA-161-15.80 NOISE WALLS

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# BORING PLAN - NOISE WALL 12

## STA. 2240+00.00 TO STA. 2245+00.00

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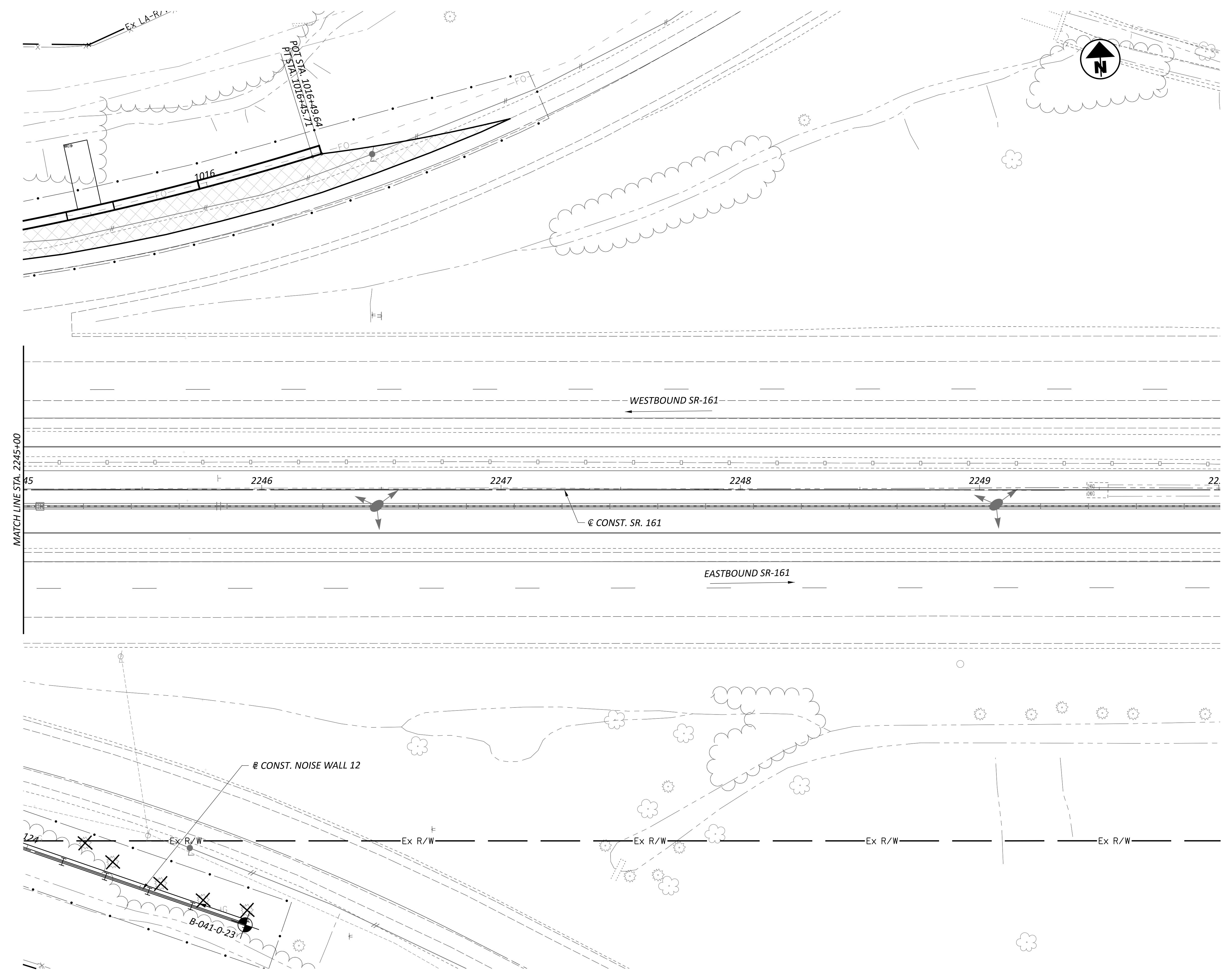
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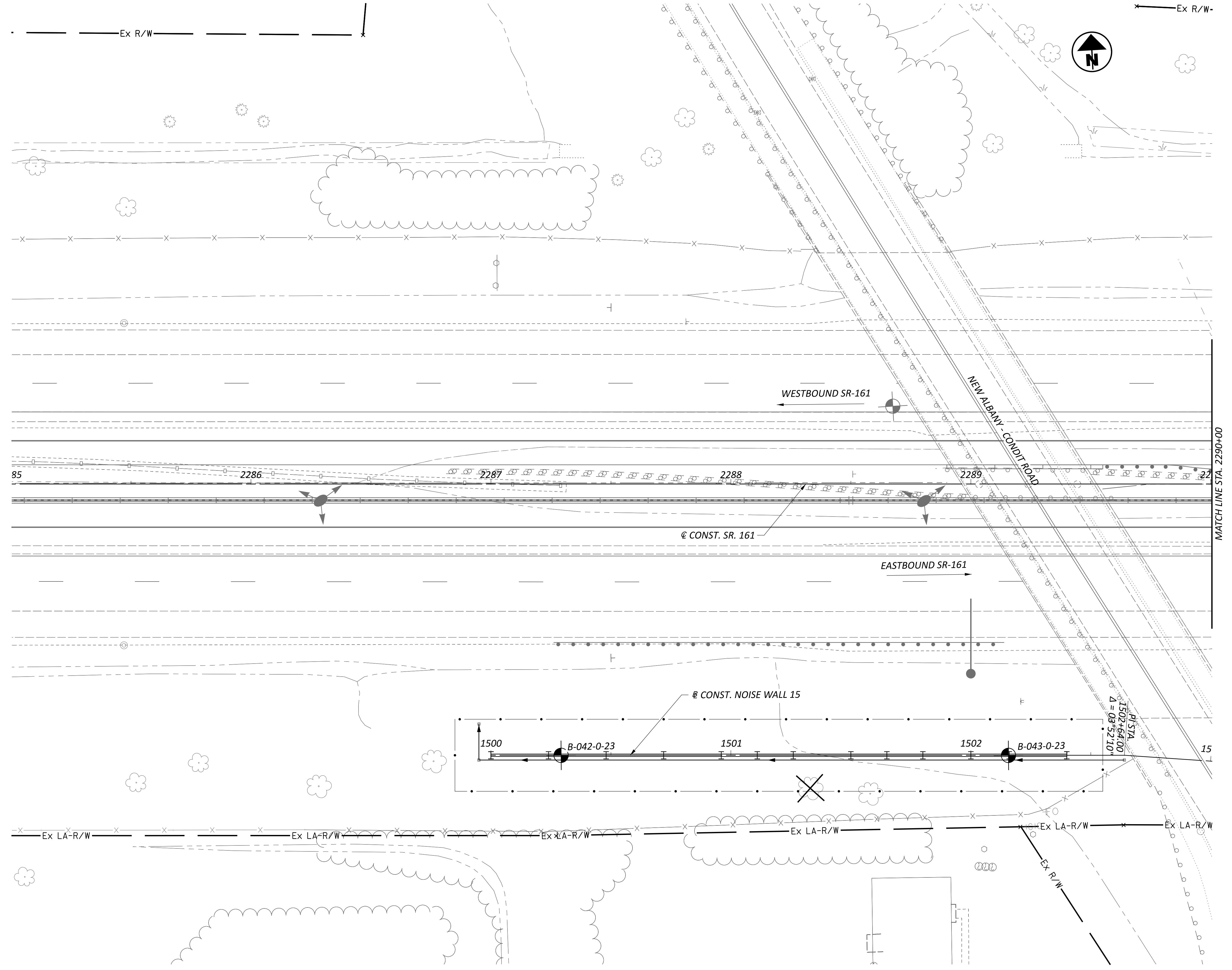


DESIGN AGENCY  
**Rii**  
RESOURCE INTERNATIONAL  
6350 PRESIDENTIAL GATEWAY  
COLUMBUS, OHIO 43231  
(614) 823-8489  
DESIGNER  
**JAS**  
REVIEWER  
**DEK MM-DD-YW**  
PROJECT ID  
**117607**  
SHEET TOTAL  
**P.O.** 0

**BORING PLAN - NOISE WALL 12**  
STA. 2245+00.00 TO STA. 2250+00.00

# FRA-161-15.80 NOISE WALLS

MODEL: GCP\_SR161 - Plan 32 PAPER SIZE: 34x22 (in) DATE: 1/18/2024 TIME: 3:58:56 PM USER: kevinj J:\\GEOTECH\\Connect\\Projects\\2023\\W-23-107\\FRA-161-15.80 NOISE WALLS\\117607\_BPW15-11.dgn



BORING PLAN - NOISE WALL 15  
STA. 2285+00.00 TO STA. 2290+00.00

DESIGN AGENCY



6350 PRESIDENTIAL GATEWAY  
COLUMBUS, OHIO 43231  
(614) 823-3499

DESIGNER

JAS

REVIEWER

DEK MM-DD-Y

PROJECT ID

117607

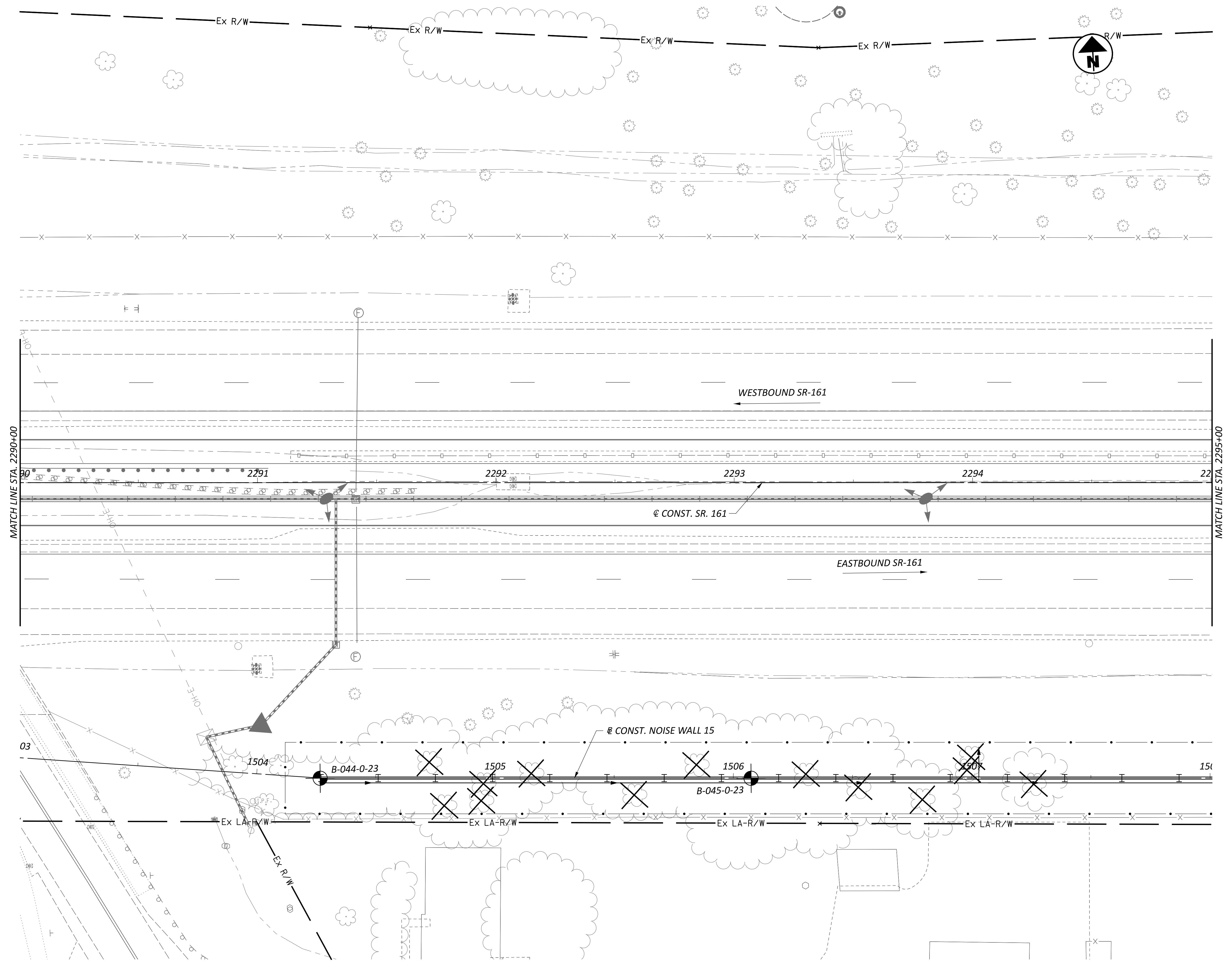
SHEET TOTAL

P.O. 0

HORIZONTAL SCALE IN FEET  
0 10 20 30 40

FRA-161-15.80 NOISE WALLS

MODEL: CLP\_SR161 - Plan 33 PAPER SIZE: 34x22 (in.) DATE: 1/18/2024 TIME: 3:59:03 PM USER: kevinj J:\GEOTECH\Geotech Connect Projects\2023\W-23-107 FRA-161-15.80 NOISE WALLS\117607\400-Engineering\Geotechnical\Sheets\117607\_BPLW15-12.dgn



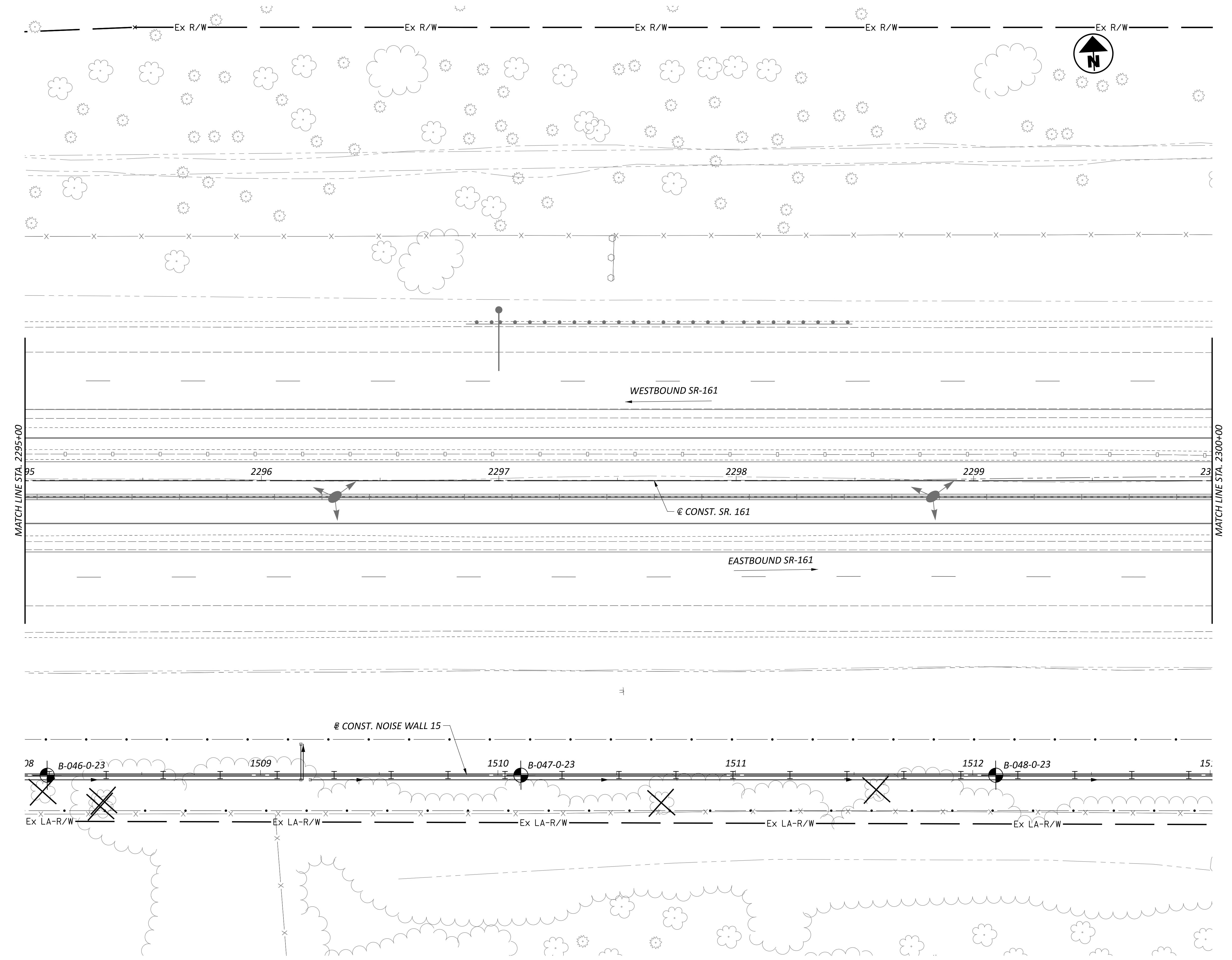
BORING PLAN - NOISE WALL 15  
STA. 2290+00.00 TO STA. 2295+00.00

BORING PLAN - NOISE WALL 15  
STA. 2290+00.00 TO STA. 2295+00.00

DESIGN AGENCY	
	
50 PRESIDENTIAL GATEWAY COLUMBUS, OHIO 43231 (614) 823-4949	
DESIGNER	
JAS	
REVIEWER	
EK MM-DD-YY	
OBJECT ID	
117607	
STREET	TOTAL
P.O.	0

# FRA-161-15.80 NOISE WALLS

MODEL: CLP\_SR161 - Plan 34 PAPER SIZE: 34x22 (in) DATE: 1/18/2024 TIME: 3:59:07 PM USER: kevinj J:\\GEOTECH\\Connect\\Projects\\2023\\W-23-107 FRA-161-15.80 NOISE WALLS\\117607\_BPW15-13.dgn

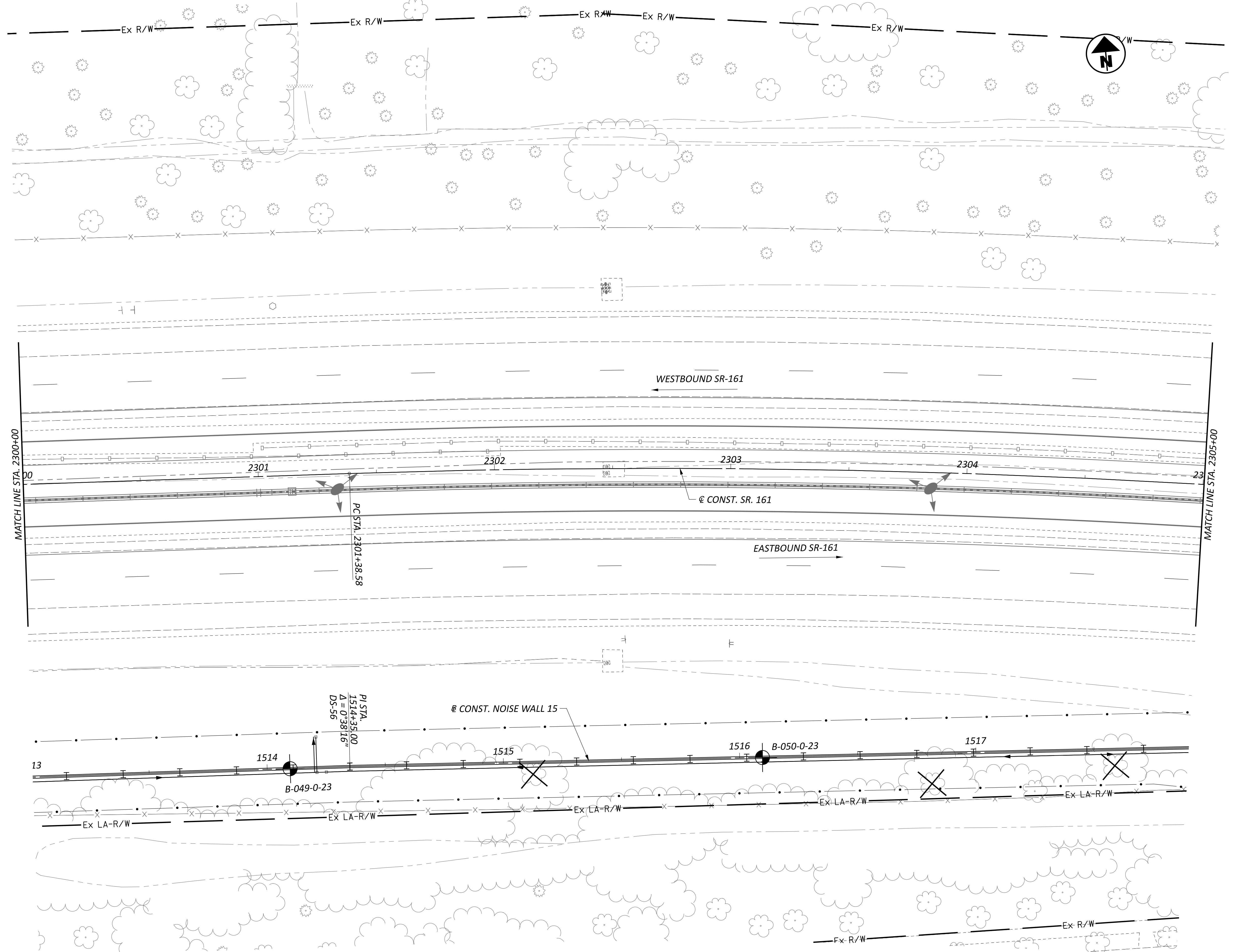


DESIGN AGENCY  
**Rii**  
RESOURCE INTERNATIONAL  
6350 PRESIDENTIAL GATEWAY  
COLUMBUS, OHIO 43231  
(614) 823-8489  
DESIGNER  
JAS  
REVIEWER  
DEK MM-DD-Y  
PROJECT ID  
117607  
SHEET TOTAL  
P.O. 0

BORING PLAN - NOISE WALL 15  
STA. 2295+00.00 TO STA. 2300+00.00

FRA-161-15.80 NOISE WALLS

MODEL: CLP\_SR161 - Plan 35 PAPER SIZE: 34x22 (in.) DATE: 1/18/2024 TIME: 3:59:10 PM USER: kevinj I:\GEOOTECH\Gootoch Connect Projects\2023\W\_22\_107\_EPA\_161\_15\_80\_NOISE WALLS\117607\100\_Engineering\Gootochchnical\Shoots\117607\_BDI\W115\_11.dwg



**BORING PLAN - NOISE WALL 15  
STA. 2300+00.00 TO STA. 2305+00.00**

BORING PLAN - NOISE WALL 15  
SSTA. 2300+00.00 TO STA. 2305+00.00

IGN AGENCY



PRESIDENTIAL GATE  
COLUMBUS, OHIO 43233  
(614) 823-4949

IGNER  
IAS

REVIEWER

EK MM-DD

## PROJECT ID

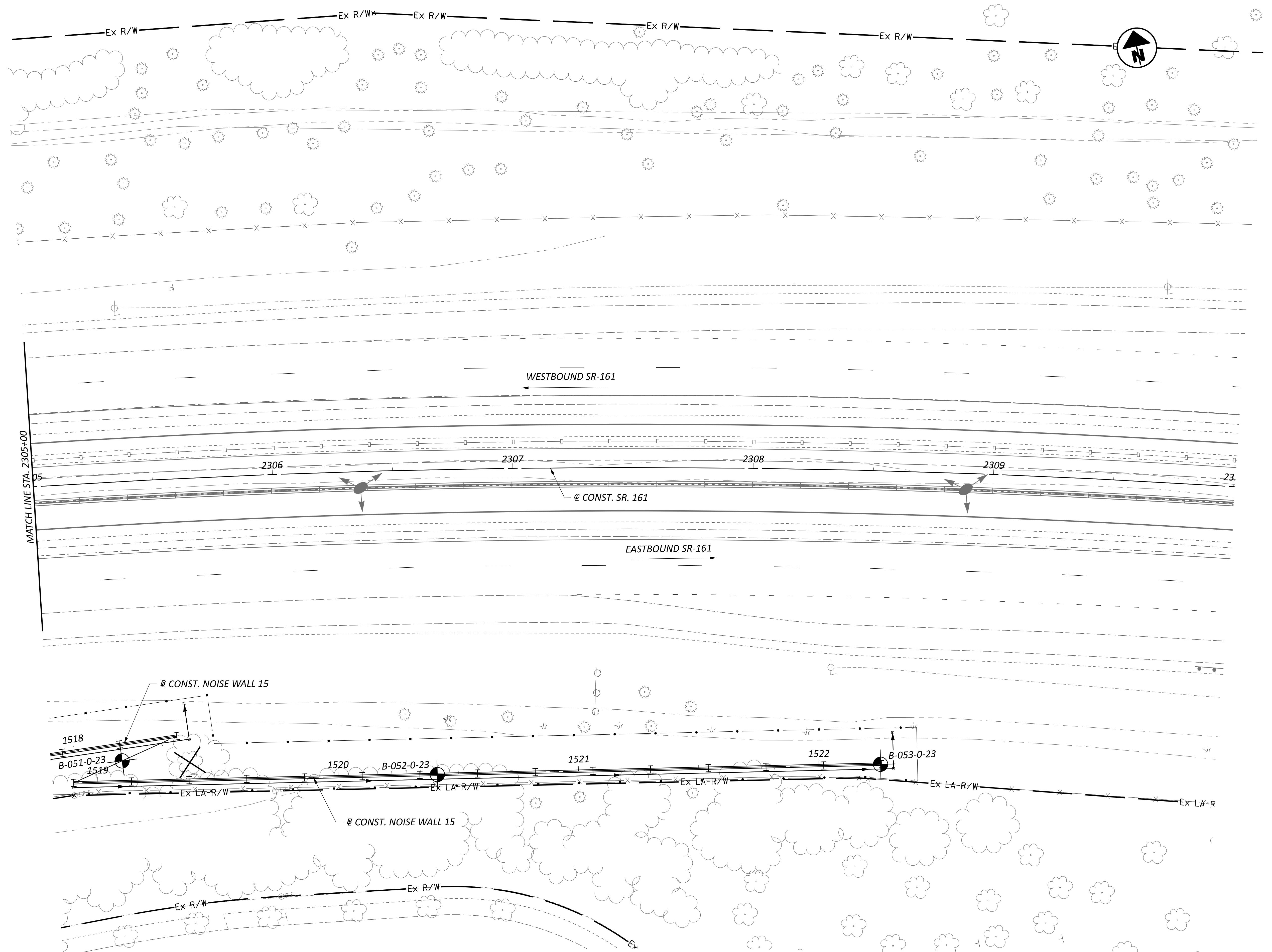
117607

ET TOTAL  
20 | 0

0.0 0

# FRA-161-15.80 NOISE WALLS

MODEL: CLP\_SR161 - Plan 36 PAPERSIZE: 34x22 (in) DATE: 1/18/2024 TIME: 3:59:14 PM USER: kevinj J:\GEOTECH\Connect\Projects\2031\W-23-107\FRA-161-15.80 NOISE WALLS\117607\_BPW15.15.dgn



BORING PLAN - NOISE WALL 15  
STA. 2305+00.00 TO STA. 2310+00.00



Rii  
RESOURCE  
INTERNATIONAL

6350 PRESIDENTIAL GATEWAY  
COLUMBUS, OHIO 43231  
(614) 823-9499

DESIGNER

JAS

REVIEWER

DEK MM-DD-Y

PROJECT ID

117607

SHEET TOTAL

P.O 0

**APPENDIX II**  
**SUMMARY OF BORINGS**

## FRA-161-15.80 Noise Walls

PID No. 117607

Rii Project No. W-23-107

Boring	Element	Latitude	Longitude	Elevation	Alignment	Station	Offset
B-001-0-23	Wall 3	40.080429	-82.864610	966.3	CL Wall 3	300+00	0
B-002-0-23		40.080609	-82.863925	968.1		302+00	0
B-003-0-23		40.080806	-82.863307	969.1		304+00	0
B-004-0-23		40.081003	-82.862692	969.2		305+76	0
B-005-0-23	Wall 6	40.087831	-82.843714	961.5	CL Wall 6	600+00	0
B-006-0-23		40.088035	-82.843136	968.1		601+77	0
B-007-0-23		40.088248	-82.842572	969.0		603+60	0
B-008-0-23		40.088448	-82.842015	970.0		605+28	0
B-009-0-23	Wall 8	40.086999	-82.844104	960.9	CL SR 161	2192+50	123' RT
B-010-0-23		40.087252	-82.843476	961.8		2194+50	113' RT
B-011-0-23		40.087493	-82.842814	964.3		2196+50	111' RT
B-012-0-23		40.087734	-82.842176	967.1		2198+50	117' RT
B-013-0-23		40.087953	-82.841539	967.4	CL Wall 8	808+00	0
B-014-0-23		40.088209	-82.840922	966.4		810+00	0
B-015-0-23		40.088482	-82.840308	966.5		812+00	0
B-016-0-23		40.088693	-82.839666	968.4		814+00	0
B-017-0-23		40.088908	-82.839020	970.7		816+00	0
B-018-0-23		40.089106	-82.838365	975.5		818+00	0
B-019-0-23		40.089329	-82.837734	974.9		820+00	0
B-020-0-23		40.089531	-82.837178	974.3		821+73	0
B-021-0-23		40.089729	-82.836617	974.1		823+48	0
B-022-0-23	Wall 11	40.090031	-82.835839	975.0	CL Wall 11	1100+00	0
B-023-0-23		40.090244	-82.835195	977.0		1102+00	0
B-024-0-23		40.090471	-82.834551	979.6		1104+00	0
B-025-0-23		40.090688	-82.833893	980.2		1106+00	0
B-026-0-23		40.090906	-82.833225	979.8		1108+00	0
B-027-0-23		40.091062	-82.832539	981.5		1110+00	0
B-028-0-23		40.091197	-82.831841	982.2		1112+00	0
B-029-0-23		40.091321	-82.831138	983.0		1114+00	0
B-030-0-23		40.091378	-82.830480	983.0		1115+84	0
B-031-0-23	Wall 9	40.090580	-82.836109	974.5	CL Wall 9	900+16	0
B-032-0-23		40.090809	-82.835481	975.2		902+00	0
B-033-0-23		40.091043	-82.834836	977.2		904+00	0
B-034-0-23		40.091273	-82.834170	979.3		906+00	0
B-035-0-23		40.091443	-82.833496	981.4		908+00	0
B-036-0-23		40.091597	-82.832807	983.2		910+00	0
B-037-0-23		40.091724	-82.832101	984.9		912+00	0
B-038-0-23	Wall 12	40.091445	-82.828386	979.3	CL Wall 12	120+00	0
B-039-0-23		40.091317	-82.827731	986.4		121+89	0
B-040-0-23		40.091207	-82.827079	987.0		123+75	0
B-041-0-23		40.091033	-82.826474	988.2		125+52	0
B-042-0-23	Wall 15	40.090577	-82.811738	1030.3	CL Wall 15	1500+29	0
B-043-0-23		40.090545	-82.811039	1035.0		1502+16	0
B-044-0-23		40.090479	-82.810313	1038.3		1504+27	0
B-045-0-23		40.090452	-82.809651	1038.9		1506+08	0
B-046-0-23		40.090415	-82.808921	1039.1		1508+10	0
B-047-0-23		40.090391	-82.808171	1039.2		1510+10	0
B-048-0-23		40.090360	-82.807478	1037.4		1512+10	0
B-049-0-23		40.090327	-82.806756	1038.9		1514+10	0
B-050-0-23		40.090286	-82.806054	1038.0		1516+10	0
B-051-0-23		40.090226	-82.805330	1038.1		1518+19.3	7' RT
B-052-0-23		40.090130	-82.804859	1038.6		1520+41	0
B-053-0-23		40.090039	-82.804245	1036.5		1522+26	0

**APPENDIX III**  
**DESCRIPTION OF SOIL AND ROCK TERMS**

## DESCRIPTION OF SOIL TERMS

The following terminology was used to describe soils throughout this report and is generally adapted from ASTM 2487/2488.

**Granular Soils** – USCS GW, GP, GM, GC, SW, SP, SM, SC, ML (non-plastic)  
The relative compactness of granular soils is described as:

Description	Blows per foot – SPT (N <sub>60</sub> )		
Very Loose	Below	5	
Loose	5	-	10
Medium Dense	11	-	30
Dense	31	-	50
Very Dense	Over		50

**Cohesive Soils** – USCS ML, CL, OL, MH, CH, OH, PT

The relative consistency of cohesive soils is described as:

Description	Unconfined Compression (tsf)		
Very Soft	Less than	0.25	
Soft	0.25	-	0.5
Medium Stiff	0.5	-	1.0
Stiff	1.0	-	2.0
Very Stiff	2.0	-	4.0
Hard	Over		4.0

**Gradation** - The following size-related denominations are used to describe soils:

Soil Fraction	Size		
Boulders	Larger than 12"		
Cobbles	12" to 3"		
Gravel	coarse	3" to $\frac{3}{4}$ "	
	fine	$\frac{3}{4}$ " to 4.75 mm ( $\frac{3}{4}$ " to #4 Sieve)	
Sand	coarse	4.75 mm to 2.0 mm (#4 to #10 Sieve)	
	medium	2.0 mm to 0.42 mm (#10 to #40 Sieve)	
	fine	0.42 mm to 0.074 mm (#40 to #200 Sieve)	
Silt		0.074 mm to 0.005 mm (#200 to 0.005 mm)	
Clay		Smaller than 0.005 mm	

**Modifiers of Components** – The following modifiers indicate the range of percentages of the minor soil components:

Term	Range		
Trace	0%	-	10%
Little	10%	-	20%
Some	20%	-	35%
And	35%	-	50%

**Moisture Table** - The following moisture-related denominations are used to describe cohesive soils:

Term	Range		
Dry	0% to 10%		
Damp	>2% below Plastic Limit		
Moist	2% below to 2% above Plastic Limit		
Very Moist	>2% above Plastic Limit		
Wet	$\geq$ Liquid Limit		

**Organic Content** – The following terms are used to describe organic soils:

Term	Organic Content (%)		
Slightly organic	2-4		
Moderately organic	4-10		
Highly organic	>10		

**Bedrock** – The following terms are used to describe bedrock hardness:

Term	Parameter
Very Weak	Can be carved with knife and scratched by fingernail.
Weak	Can be grooved or gouged with knife readily.
Slightly Strong	Can be grooved or gouged 0.05 in deep with knife.
Moderately Strong	Can be scratched with knife or pick.
Strong	Can be scratched with knife or pick with difficulty.
Very Strong	Cannot be scratched by knife or pick. Hard repeated blows of hammer to detach specimen.
Extremely Strong	Cannot be scratched by knife or pick. Hard repeated blows of hammer to chip hand specimen.

## DESCRIPTION OF ROCK TERMS

The following terminology was used to describe the rock throughout this report and is generally adapted from ASTM D5878 and the ODOT Specifications for Geotechnical Explorations.

**Weathering** – Describes the degree of weathering of the rock mass:

<u>Description</u>	<u>Field Parameter</u>
Unweathered	No evidence of any chemical or mechanical alteration of the rock mass. Mineral crystals have a right appearance with no discoloration. Fractures show little or not staining on surfaces.
Slightly Weathered	Slight discoloration of the rock surface with minor alterations along discontinuities. Less than 10% of the rock volume presents alteration.
Moderately Weathered	Portions of the rock mass are discolored as evident by a dull appearance. Surfaces may have a pitted appearance with weathering "halos" evident. Isolated zones of varying rock strengths due to alteration may be present. 10 to 15% of the rock volume presents alterations.
Highly Weathered	Entire rock mass appears discolored and dull. Some pockets of slightly to moderately weathered rock may be present and some areas of severely weathered materials may be present.
Severely Weathered	Majority of the rock mass reduced to a soil-like state with relic rock structure discernable. Zones of more resistant rock may be present but the material can generally be molded and crumbled by hand pressures.

**Strength of Bedrock** – The following terms are used to describe the relative strength of bedrock:

<u>Description</u>	<u>Field Parameter</u>
Very Weak	Can be carved with knife and scratched by fingernail. Pieces 1 in. thick can be broken by finger pressure.
Weak	Can be grooved or gouged with knife readily. Small, thin pieces can be broken by finger pressure.
Slightly Strong	Can be grooved or gouged 0.05 in deep with knife. 1 in. size pieces from hard blows of geologist hammer.
Moderately Strong	Can be scratched with knife or pick. 1/4 in. size grooves or gouges from blows of geologist hammer.
Strong	Can be scratched with knife or pick with difficulty. Hard hammer blows to detach hand specimen.
Very Strong	Cannot be scratched by knife or pick. Hard repeated blows of geologist hammer to detach hand specimen.
Extremely Strong	Cannot be scratched by knife or pick. Hard repeated blows of geologist hammer to chip hand specimen.

**Bedding Thickness** – Description of bedding thickness as the average perpendicular distances between bedding surfaces:

<u>Description</u>	<u>Thickness</u>
Very Thick	Greater than 36 inches
Thick	18 to 36 inches
Medium	10 to 18 inches
Thin	2 to 10 inches
Very Thin	0.4 to 2 inches
Laminated	0.1 to 0.4 inches
Thinly Laminated	Less than 0.1 inches

**Fracturing** – Describes the degree and condition of fracturing (fault, joint, or shear):

<b>Degree of Fracturing</b>	
<u>Description</u>	<u>Spacing</u>
Unfractured	Greater than 10 feet
Intact	3 to 10 feet
Slightly Fractured	1 to 3 feet
Moderately Fractured	

<b>Aperture Width</b>		<b>Surface Roughness</b>	
<u>Description</u>	<u>Width</u>	<u>Description</u>	<u>Criteria</u>
Open	Greater than 0.2 inches	Very Rough	Near vertical steps and ridges occur on surface
Narrow	0.05 to 0.2 inches	Slightly Rough	Asperities on the surfaces distinguishable
Tight	Less than 0.05 inches	Slickensided	Surface has smooth, glassy finish, evidence of striations

**RQD** – Rock Quality Designation (calculation shown in report) and Rock Quality (ODOT, GB 3, January 13, 2006):

<u>RQD %</u>	<u>Rock Index Property Classification (based on RQD, not slake durability index)</u>
0 – 25%	Very Poor
26 – 50%	Poor
51 – 70%	Fair
71 – 85%	Good
86 – 100%	Very Good

**APPENDIX IV**

**BORING LOGS: B-001-0-23 THROUGH B-053-0-23  
ROCK CORE PHOTOGRAPHS**

# BORING LOGS

## Definitions of Abbreviations

AS	=	Auger sample
GI	=	Group index as determined from the Ohio Department of Transportation classification system
HP	=	Unconfined compressive strength as determined by a hand penetrometer (tons per square foot)
LL <sub>o</sub>	=	Oven-dried liquid limit as determined by ASTM D4318. Per ASTM D2487, if LL <sub>o</sub> /LL is less than 75 percent, soil is classified as "organic".
LOI	=	Percent organic content (by weight) as determined by ASTM D2974 (loss on ignition test)
PID	=	Photo-ionization detector reading (parts per million)
QR	=	Unconfined compressive strength of intact rock core sample as determined by ASTM D2938 (pounds per square inch)
QU	=	Unconfined compressive strength of soil sample as determined by ASTM D2166 (pounds per square foot)
RC	=	Rock core sample
REC	=	Ratio of total length of recovered soil or rock to the total sample length, expressed as a percentage
RQD	=	Rock quality designation – estimate of the degree of jointing or fracture in a rock mass, expressed as a percentage:

$$\frac{\sum \text{ segments equal to or longer than 4.0 inches}}{\text{core run length}} \times 100$$

S	=	Sulfate content (parts per million)
SPT	=	Standard penetration test blow counts, per ASTM D1586. Driving resistance recorded in terms of blows per 6-inch interval while letting a 140-pound hammer free fall 30 inches to drive a 2-inch outer diameter (O.D.) split spoon sampler a total of 18 inches. The second and third intervals are added to obtain the number of blows per foot (N <sub>m</sub> ).
N <sub>60</sub>	=	Measured blow counts corrected to an equivalent (60 percent) energy ratio (ER) by the following equation: N <sub>60</sub> = N <sub>m</sub> * (ER/60)
SS	=	Split spoon sample
2S	=	For instances of no recovery from standard SS interval, a 2.5 inch O.D. split spoon is driven the full length of the standard SS interval plus an additional 6.0 inches to obtain a representative sample. Only the final 6.0 inches of sample is retained. Blow counts from 2S sampling are not correlated with N <sub>60</sub> values.
3S	=	Same as 2S, but using a 3.0 inch O.D. split spoon sampler.
TR	=	Top of rock
W	=	Initial water level measured during drilling
▽	=	Water level measured at completion of drilling

### Classification Test Data

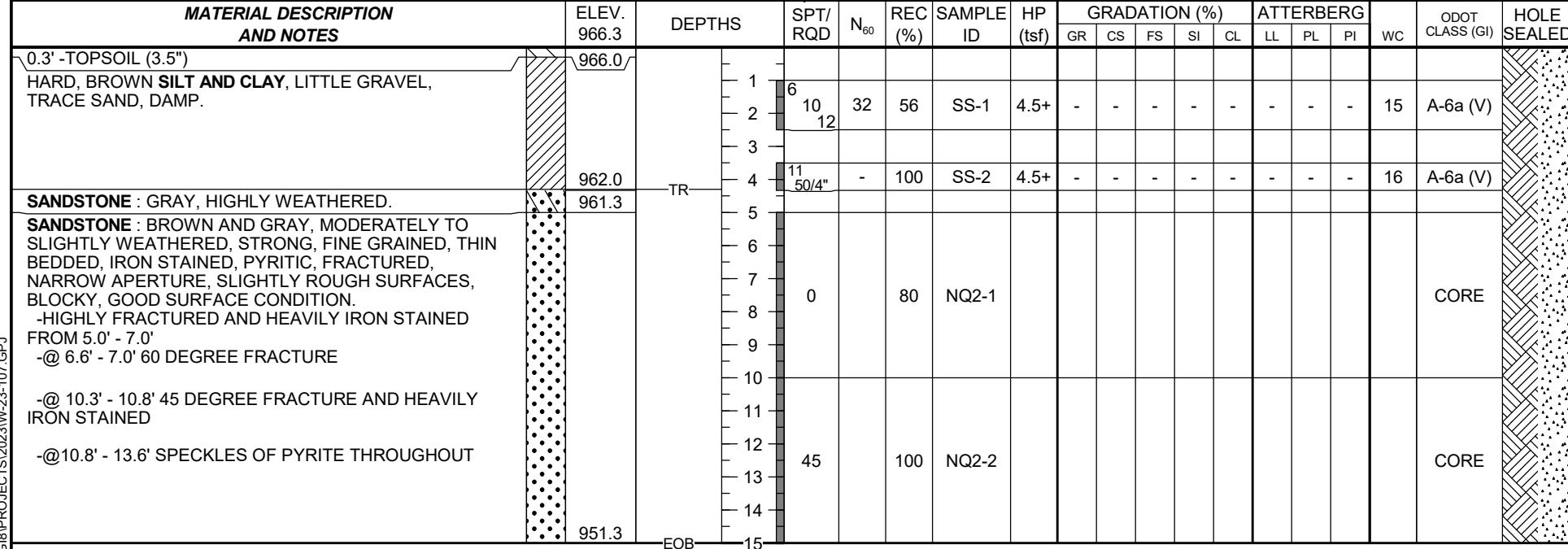
Gradation (as defined on Description of Soil Terms):

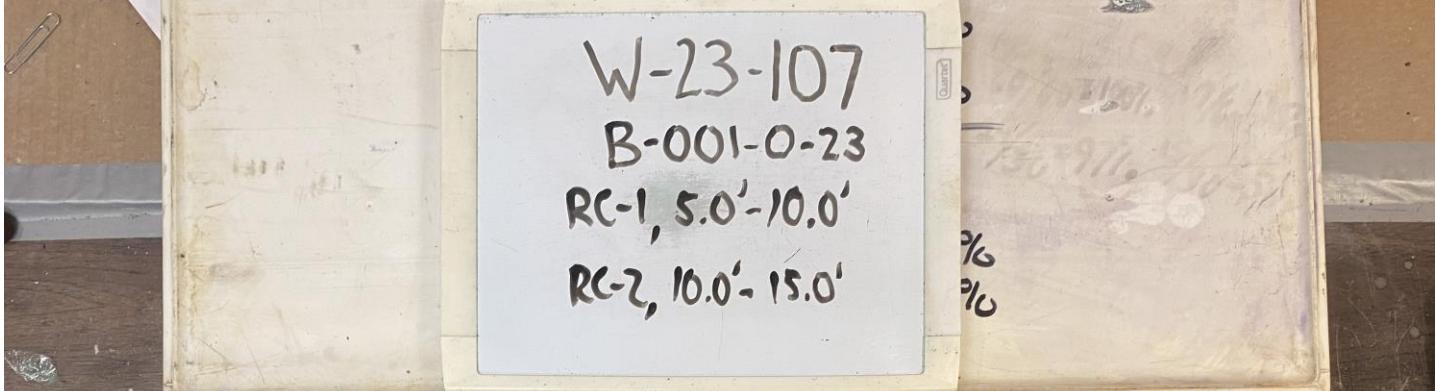
GR	=	% Gravel
SA	=	% Sand
SI	=	% Silt
CL	=	% Clay

Atterberg Limits:

LL	=	Liquid limit
PL	=	Plastic limit
PI	=	Plasticity Index
WC	=	Water content (%)

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/22/23 END: 11/22/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 300+00 / 0' ALIGNMENT: CL WALL 3 ELEVATION: 966.3 (MSL) EOB: 15.0 ft. LAT / LONG: 40.080429, -82.864610	EXPLORATION ID <b>B-001-0-23</b>
				PAGE 1 OF 1

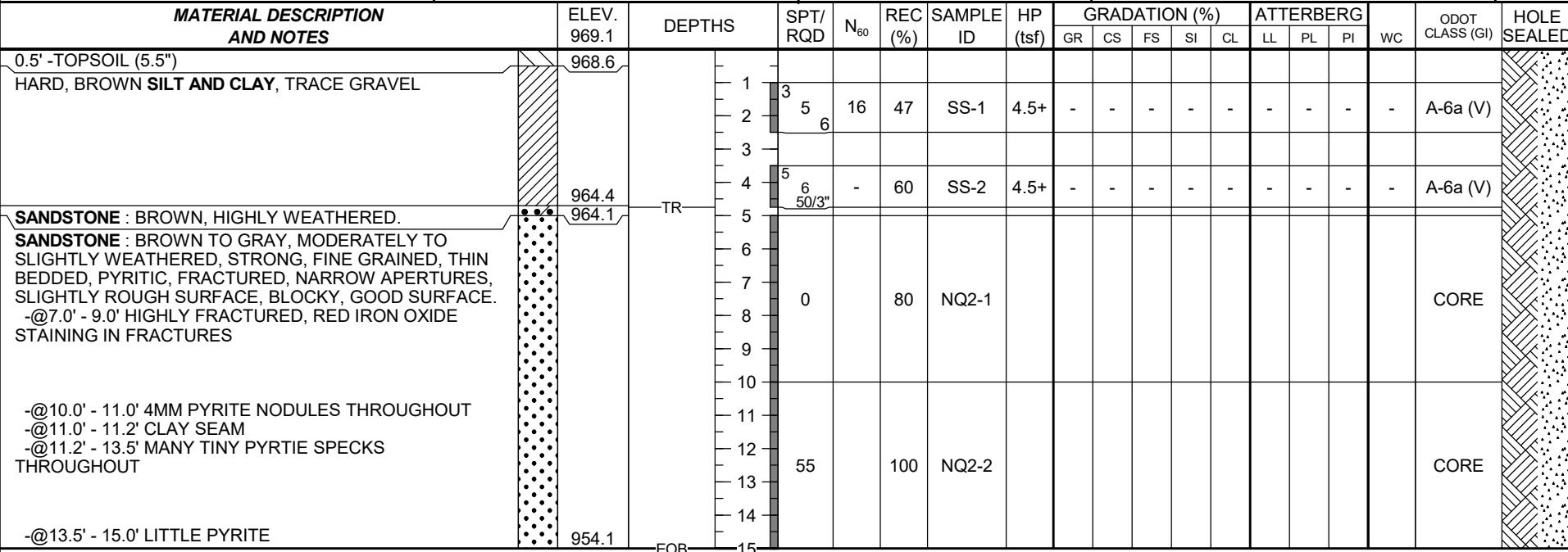


<p><b>Project Name:</b> FRA-161-15.80</p>	<p><b>Location:</b> Franklin County, Ohio</p>
<p><b>Photo No.</b> <b>1</b></p>	 <p>W-23-107 B-001-0-23 RC-1, 5.0'-10.0' RC-2, 10.0'-15.0'</p>
<p><b>Boring:</b> B-001-0-23</p>	
<p>RC-1: 5.0-10.0' REC (%):80 RQD (%):0</p>	
<p>RC-2: 10.0-15.0' REC (%):100 RQD (%):45</p>	

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/22/23 END: 11/22/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 302+00 / 0' ALIGNMENT: CL WALL 3 ELEVATION: 968.1 (MSL) EOB: 15.3 ft. LAT / LONG: 40.080609, -82.863925	EXPLORATION ID <b>B-002-0-23</b>															
				PAGE 1 OF 1															
	<b>MATERIAL DESCRIPTION AND NOTES</b>	ELEV. 968.1	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	<b>GRADATION (%)</b>					<b>ATTERBERG</b>			ODOT CLASS (GI)	HOLE SEALED	
		967.7		1	3				GR	CS	FS	SI	CL	LL	PL	PI	WC		
0.4' -TOPSOIL (4.5") HARD, BROWN-GRAY CLAY, SOME SILT, LITTLE COARSE TO FINE SAND, TRACE SAND AND GRAVEL, MOIST. -@2.8' - 3.4' COBBLES		965.1		2	5	17	56	SS-1	4.5+	3	5	8	34	50	55	21	34	20	A-7-6 (19)
VERY DENSE, GRAY GRAVEL WITH SAND AND SILT, DAMP.		963.5	TR	3															
SANDSTONE : GRAY, HIGHLY WEATHERED.  SANDSTONE : GRAY, SLIGHTLY WEATHERED, STRONG, FINE GRAINED, THIN BEDDED, PYRITIC, FRACTURED, NARROW APERTURES, SLIGHTLY ROUGH SURFACES, BLOCKY, GOOD SURFACE. -@6.0' - 9.7' APPROXIMATELY 4MM PYRITE NODULES THROUGHOUT -@9.7' CLAY SEAM -@10.25' - 12.0' MANY PYRITE FLECKS THROUGHOUT -@11.0' - 15.75' FEW PYRITE FLECKS		962.1		4	14	17	-	100	SS-2	4.5+	-	-	-	-	-	-	-	7	A-2-4 (V)
		952.9	EOB	5															
				6															
				7															
				8	0		68	NQ2-1											CORE
				9															
				10															
				11															
				12															
				13	53		96	NQ2-2											CORE
				14															
				15															

Project Name: FRA-161-15.80	Location: Franklin County, Ohio
Photo No. <b>2</b>	 <p> <b>W-23-107</b>  <b>B-002-0-23</b>  <b>RC-1, 6.0'-10.25'</b>  <b>RC-2, 10.25'-15.25'</b> </p> <p style="text-align: right;">     %      4%      %   </p>
Boring: <b>B-002-0-23</b>	
RC-1: 6.0-10.25' REC (%):68 RQD (%):0	
RC-2: 10.25-15.25' REC (%):96 RQD (%):53	

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/20/23 END: 11/22/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 304+00 / 0' ALIGNMENT: CL WALL 3 ELEVATION: 969.1 (MSL) EOB: 15.0 ft. LAT / LONG: 40.080806, -82.863307	EXPLORATION ID <b>B-003-0-23</b>
				PAGE 1 OF 1



**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
**3**

**Boring:**  
B-003-0-23

RC-1: 5.0-10.0'  
REC (%):80  
RQD (%):0



**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

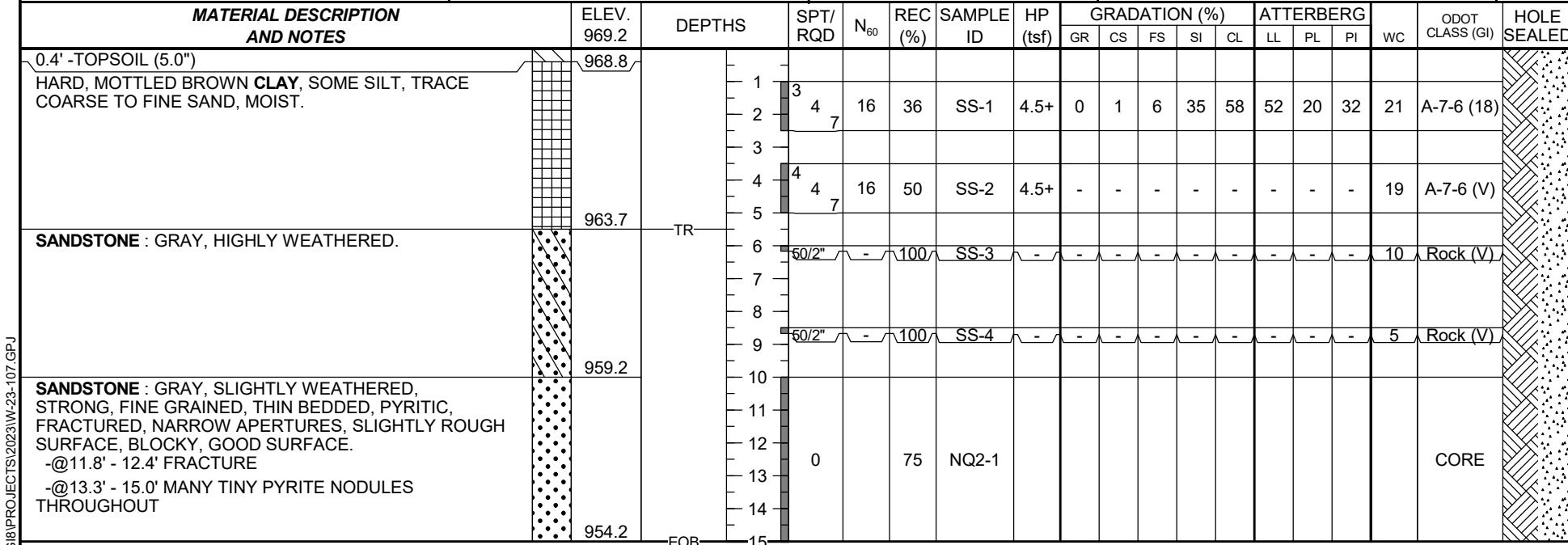
**Photo No.**  
**4**

**Boring:**  
B-003-0-23

RC-2: 10.0-15.0'  
REC (%):100  
RQD (%):55



 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/20/23 END: 11/20/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 305+76 / 0' ALIGNMENT: CL WALL 3 ELEVATION: 969.2 (MSL) EOB: 15.0 ft. LAT / LONG: 40.081003, -82.862692	EXPLORATION ID <b>B-004-0-23</b>
				PAGE 1 OF 1



**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

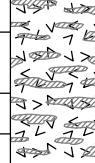
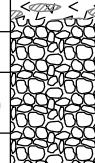
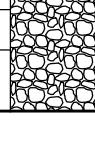
**Photo No.**  
**5**

**Boring:**  
B-004-0-23

RC-1: 10.0-15.0'  
REC (%):75  
RQD (%):0



 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/20/23 END: 11/20/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 600+00 / 0' ALIGNMENT: CL WALL 6	EXPLORATION ID <b>B-005-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 961.5 (MSL) EOB: 25.0 ft. LAT / LONG: 40.087831, -82.843714	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 961.5	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.4' -TOPSOIL (5.0") VERY STIFF TO HARD, DARK BROWN TO BROWNISH GRAY SILT AND CLAY, LITTLE COARSE TO FINE SAND, TRACE GRAVEL, DAMP TO MOIST.	961.1			1 2 3 4 5 6 7 8 9 10 11 12	6 8 8 23 23 56 16 23 22 56 4 4 5	SS-1 SS-2 SS-3 SS-4 SS-5 SS-6 SS-7 SS-8 SS-9 SS-10	4.5+ 4.5+ 4.5+ 4.5+ 2.50 -	-	-	-	-	-	-	-	14	A-6a (V)			
MEDIUM DENSE, DARK GRAY COARSE AND FINE SAND, LITTLE SILT, TRACE GRAVEL, WET.	948.5			13 14 15 16 17 18 19 20 21 22 23 24 25	7 7 8 22 19 47 53 50 SS-7 37 53 8 12 18			9 11 16 31 33 28 16 12 13								14	A-6a (7)		
DENSE TO VERY DENSE, DARK GRAY GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, WET.	946.0			W 946.0	5 5 8	SS-6	-	-	-	-	-	-	-	-	-	14	A-3a (V)		
DENSE, DARK GRAY COARSE AND FINE SAND, TRACE FINE GRAVEL, TRACE SILT, WET.	938.5			EOB	21 21 16 31 15 25 9 10 16 8 12 18	SS-7 SS-8 SS-9 SS-10	- -	51 17 10 13 9	NP NP NP	NP NP NP	NP NP NP	13	12	11	13	A-1-b (V)			
																18	A-1-b (0)		
																			
																			

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 15.5' AND UPON COMPLETION @ 14.7'; CAVE-IN DEPTH @ 11.8'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/20/23 END: 11/20/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 601+77 / 0' ALIGNMENT: CL WALL 6	EXPLORATION ID <b>B-006-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 968.1 (MSL) EOB: 25.0 ft. LAT / LONG: 40.088035, -82.843136	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 968.1	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.5' -TOPSOIL (5.5") HARD, BROWN SILT AND CLAY, SOME CLAY, TRACE FINE GRAVEL, DAMP.	967.6			1															
			2	6 10 12	32	78	SS-1	4.5+	-	-	-	-	-	-	-	11	A-6a (V)		
			3																
			4	7 12 13	36	75	SS-2	4.5+	7	11	16	32	34	29	17	12	14	A-6a (7)	
			5																
			6																
			7	7 9 11	29	100	SS-3	4.5+	-	-	-	-	-	-	-	-	13	A-6a (V)	
			8																
			9	6 11 16	39	72	SS-4	-	-	-	-	-	-	-	-	-	11	A-2-4 (V)	
			10																
			11																
			12	7 17 16	48	33	SS-5	-	-	-	-	-	-	-	-	-	7	A-2-4 (V)	
			13																
			14	9 15 16	45	0	SS-6	-	-	-	-	-	-	-	-	-			
			15	13	-	67	2S-6A	-	-	-	-	-	-	-	-	-	15	A-2-4 (V)	
			16	21 18 15	48	44	SS-7	-	36	19	14	19	12	24	17	7	11	A-2-4 (0)	
			17																
			18																
			19	16 12 8	29	64	SS-8	-	-	-	-	-	-	-	-	-	10	A-2-4 (V)	
			20																
			21	10 12 12	35	83	SS-9	-	-	-	-	-	-	-	-	-	12	A-3a (V)	
			22																
			23																
			24	16 15 15	43	97	SS-10	-	-	-	-	-	-	-	-	-	10	A-1-b (V)	
			25																
		EOB																	

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 13.5' AND UPON COMPLETION @ 15.5'; CAVE-IN DEPTH @ 12.2'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

**RESOURCE INTERNATIONAL, INC.**



PROJECT: FRA-161-15.80  
TYPE: NOISE WALLS  
PID: 117607 SFN: NA  
START: 11/17/23 END: 11/

DRILLING FIRM / OPERATOR: \_\_\_\_\_ R  
SAMPLING FIRM / LOGGER: \_\_\_\_\_ RI  
DRILLING METHOD: \_\_\_\_\_ 3.25" HS  
SAMPLING METHOD: \_\_\_\_\_ SPT

DRILL RIG: DIEDRICH D-50 (# 313)  
HAMMER: AUTOMATIC  
CALIBRATION DATE: 3/21/22  
ENERGY RATIO (%): 86.4

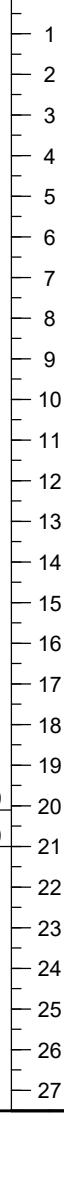
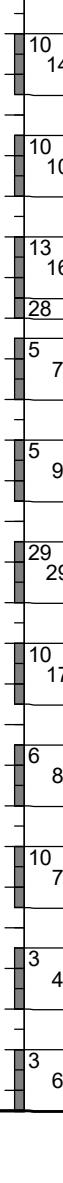
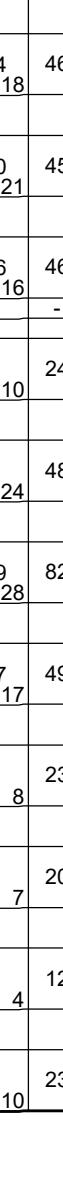
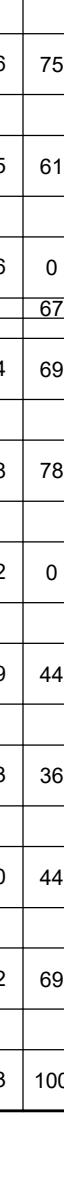
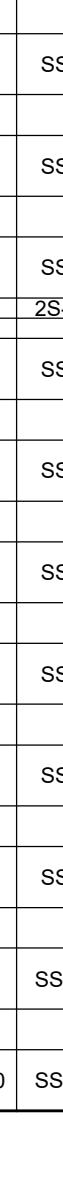
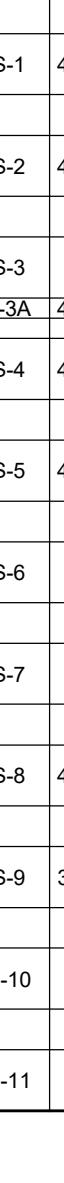
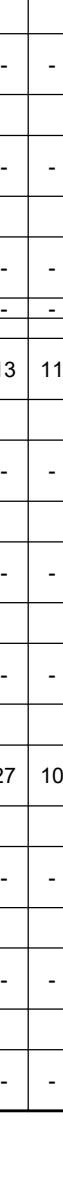
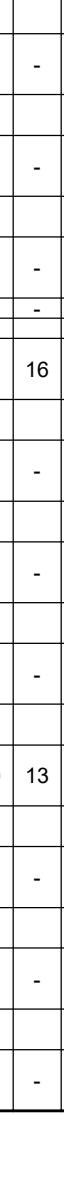
STATION / OFFSET: 603+60 / 0' EXP  
ALIGNMENT: CL WALL 6 B-  
ELEVATION: 969.0 (MSL) EOB: 25.0 ft.  
LAT / LONG: 40.088248, -82.842572

**EXPLORATION ID  
B-007-0-23**

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 21.0' AND UPON COMPLETION @ 20.5'; CAVE-IN DEPTH @ 13.1'.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/17/23 END: 11/17/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 605+28 / 0' ALIGNMENT: CL WALL 6	EXPLORATION ID <b>B-008-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 970.0 (MSL) EOB: 27.5 ft. LAT / LONG: 40.088448, -82.842015	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 970.0	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.3' -TOPSOIL (4.0") HARD, BROWN TO BROWN/GRAY SANDY SILT, SOME CLAY, LITTLE FINE GRAVEL, DAMP.	969.7			1 10 14 18	46	75	SS-1	4.5+	-	-	-	-	-	-	-	11	A-4a (V)		
				2 3 4 10 10 21	45	61	SS-2	4.5+	-	-	-	-	-	-	-	11	A-4a (V)		
				5 6 13 16 16	46	0	SS-3	-	-	-	-	-	-	-	-				
				7 28 28	13 16 16	67	2S-3A	4.5+	-	-	-	-	-	-	-	10	A-4a (V)		
				9 10 5 7 10	24	69	SS-4	4.5+	13	11	16	30	30	16	14	2	10	A-4a (5)	
				11 12 5 9 24	48	78	SS-5	4.5+	-	-	-	-	-	-	-	11	A-4a (V)		
VERY DENSE TO DENSE, GRAY GRAVEL WITH SAND, LITTLE SILT, MOIST.	957.0			13 14 29 29 28	29	82	0	SS-6	-	-	-	-	-	-	-	-			
				15 16 10 17 17	29	82	0	SS-6	-	-	-	-	-	-	-	-			
VERY STIFF TO HARD, GRAY SANDY SILT, SOME CLAY, SOME FINE GRAVEL, DAMP. -COBBLES FROM 18.0' - 18.5'	952.0			17 18 19 6 8 8	17 17 17	49	44	SS-7	-	-	-	-	-	-	-	9	A-1-b (V)		
				20 21 10 7 7	20	44	SS-8	4.5+	27	10	13	27	23	24	14	10	10	A-4a (3)	
				22 23 10 3 4 4	20	44	SS-9	3.50	-	-	-	-	-	-	-	12	A-4a (V)		
MEDIUM DENSE, BROWN TO BROWNISH GRAY COARSE AND FINE SAND, TRACE FINE GRAVEL, TRACE SILT, WET.	947.0			24 25 3 4 4	12	69	SS-10	-	-	-	-	-	-	-	-	17	A-3a (V)		
				26 27 3 6 10	23	100	SS-11	-	-	-	-	-	-	-	-	20	A-3a (V)		
		EOB																	

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 21.0' AND UPON COMPLETION @ 20.1'; CAVE-IN DEPTH @ 13.1'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.



PROJECT: FRA-161-15.80

TYPE: NOISE WALL

BID: 1

FID.

DRILLING FIRM / OPERATOR: RII A

SAMPLING FIRM / LOGGER: BII /

DRILLING METHOD: 3.25" USA

SAMPLING METHOD: SPT

DRILL RIG: DIEDRICH D-50 (# 313)

HAMMER: AUTOMATIC

CALIBRATION DATE: 3/21/23

ENERGY RATIO (%) 63.4

STATION / OFFSET: 2192+50 / 123' RT

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CL SB 161

EL ELEVATION: 060.0 (MSL) FOR:

AT / LONG. 12.333333 - 02.244444

## **EXPLORATION ID**

B-009-0-23

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 12.0' AND UPON COMPLETION @ 10.3'; CAVE-IN DEPTH @ 19.1'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

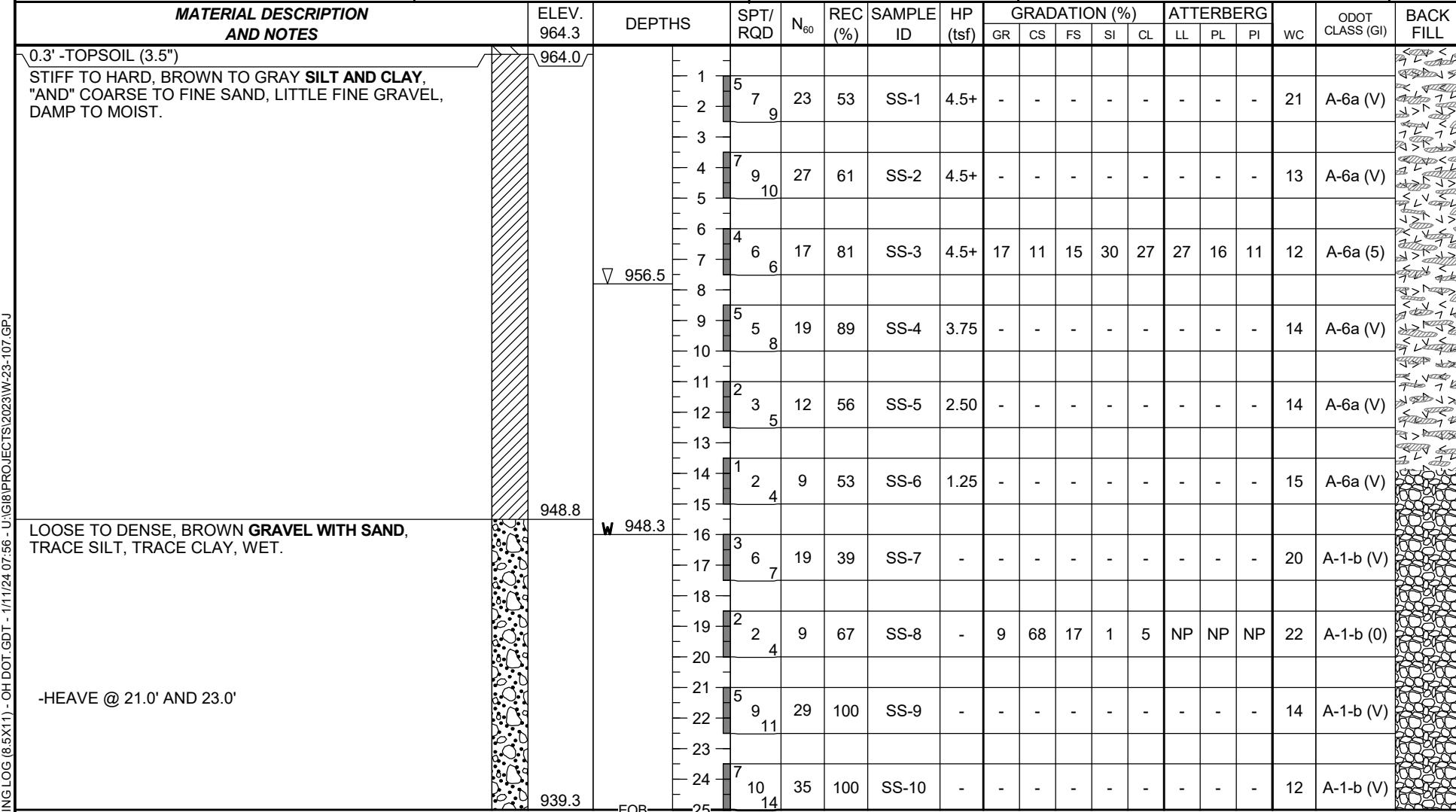
 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/3/23 END: 11/3/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 2194+49 / 112' RT ALIGNMENT: CL SR 161	EXPLORATION ID <b>B-010-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 961.8 (MSL) EOB: 25.0 ft. LAT / LONG: 40.087252, -82.843476	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 961.8	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.3' -TOPSOIL (4.0") HARD, BROWN SILT AND CLAY, LITTLE COARSE TO FINE SAND, TRACE GRAVEL, DAMP TO MOIST. -COBBLES FROM 3.8' - 4.5'	961.5			1 8 2 12 12 3 4 15 45 18 5 6 11 9 9 7 8 9 11 12 10 11 6 8 11 12 13 14 10 10 10 15 5 7 8 10 16 17 18 19 5 8 13 20 21 9 16 17 22 23 10 15 13 24 25					-	-	-	-	-	-	-	-	16	A-6a (V)	
MEDIUM DENSE TO DENSE, BROWN GRAVEL WITH SAND AND SILT, WET.	956.3																		
HARD, BROWN SANDY SILT, LITTLE CLAY, TRACE FINE GRAVEL, DAMP.	946.1																		
	936.8																		
	EOB																		

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 12.5' AND UPON COMPLETION @ 11.2'; CAVE-IN DEPTH @ 13.1'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/3/23 END: 11/3/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 2196+50 / 111' RT ALIGNMENT: CL SR 161	EXPLORATION ID <b>B-011-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 964.3 (MSL) EOB: 25.0 ft. LAT / LONG: 40.087493, -82.842814	PAGE 1 OF 1



 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/3/23 END: 11/3/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 800+72 / 117' RT ALIGNMENT: CL SR 161	EXPLORATION ID <b>B-012-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 967.1 (MSL) EOB: 25.0 ft. LAT / LONG: 40.087734, -82.842176	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 967.1	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI			
0.3' -TOPSOIL (4.0") HARD, LIGHT BROWN SILT AND CLAY, SOME COARSE TO FINE SAND, TRACE FINE GRAVEL, DAMP TO MOIST. -COBBLES FROM 4.8' - 5.2' -AUGER REFUSAL @ 5.2'. OFFSET 7.0' SW, CONTINUED SAMPLING AT 6.0'	966.8			1 5 6 9 2 3 4 14 16 28 5 6 7 11 13 16 8 9 20 28 16 10 11 12 13 14 7 14 18 15 18 10 16 17 18 19 17 18 18 20 21 18 22 34 26 23 6 9 12 24 25				-	-	-	-	-	-	-	-	18	A-6a (V)	
DENSE TO VERY DENSE, DARK GRAY GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, MOIST.	954.1			1 5 18 12 13 14 15 16 17 18 19 20 21 22 23 24 25				8	10	15	33	34	30	17	13	11	A-6a (8)	
HARD, BROWN SANDY SILT, LITTLE CLAY, TRACE FINE GRAVEL, MOIST.	946.6			1 5 18 12 13 14 15 16 17 18 19 20 21 22 23 24 25				-	-	-	-	-	-	-	-	10	A-6a (V)	
	942.1			1 5 18 12 13 14 15 16 17 18 19 20 21 22 23 24 25				46	21	8	18	7	NP	NP	NP	8	A-1-b (0)	
	EOB			1 5 18 12 13 14 15 16 17 18 19 20 21 22 23 24 25				-	-	-	-	-	-	-	-	8	A-1-b (V)	
				1 5 18 12 13 14 15 16 17 18 19 20 21 22 23 24 25				-	-	-	-	-	-	-	-	11	A-1-b (V)	
				1 5 18 12 13 14 15 16 17 18 19 20 21 22 23 24 25				-	-	-	-	-	-	-	-	11	A-4a (V)	
				1 5 18 12 13 14 15 16 17 18 19 20 21 22 23 24 25				-	-	-	-	-	-	-	-	11	A-4a (V)	

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 18.5' AND UPON COMPLETION @ 14.9'; CAVE-IN DEPTH @ 18.5'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.



PROJECT: FRA-161-15.80

TYPE: NOISE WALL

BID: 1

11

STAR

DRILLING FIRM / OPERATOR: RII

SAMPLING FIRM / LOGGER: BII /

DRILLING METHOD: 3.25" HS/

SAMPLING METHOD: SPT

SAMPLING METHOD: SPI

DRILL RIG: DIEDRICH D-50 (# 313)

HAMMER AUTOMATIC

CALIBRATION DATE: 3/31/23

ENERGY RATIO (%): 86.4

ENERGY RATIO (%). 80.4

STATION / OFFSET: 802+72 / 0'

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ALIGNMENT CI WALL 8

ELEVATION: 867.4 (MSL) EOB:

LAT / LONG: 40.087053 -82.8

LAT / LONG. 40.087953, -82.84

EXPLORATION

B-013-0-23

PAGE

1 OF

NOTES: GROUNDWATER INITIALLY ENCOUNTERED @ 16.0' AND UPON COMPLETION @ 14.2'.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.



PROJECT: FRA-161-15.80

**TYPE:** NOISE WALLS

PID: 1

FID.

**START:** \_\_\_\_\_

**DRILLING FIRM / OPERATOR:** RII

SAMPLING FIRM / LOGGER: RII /

DRILLING METHOD: 3.25" HS/

SAMPLING METHOD: SPT

SAMPLING METHOD: \_\_\_\_\_

DRILL RIG: DIEDRICH D-50 (# 313)

HAMMER: AUTOMATIC

CALIBRATION DATE: 3/31/23

ENERGY RATIO (%): 86.4

ENERGY RATIO (%): 86.4

STATION / OFFSET: 804+72 / 0'

ALIGNMENT: CL WALL 8

ELEVATION: 066.4 (MSL) EOB:

LAT / LONG: 46.0882200 -82.3

LAT / LUNG: 40.088209, -82.84

EXPLORATION ID

B-014-0-23

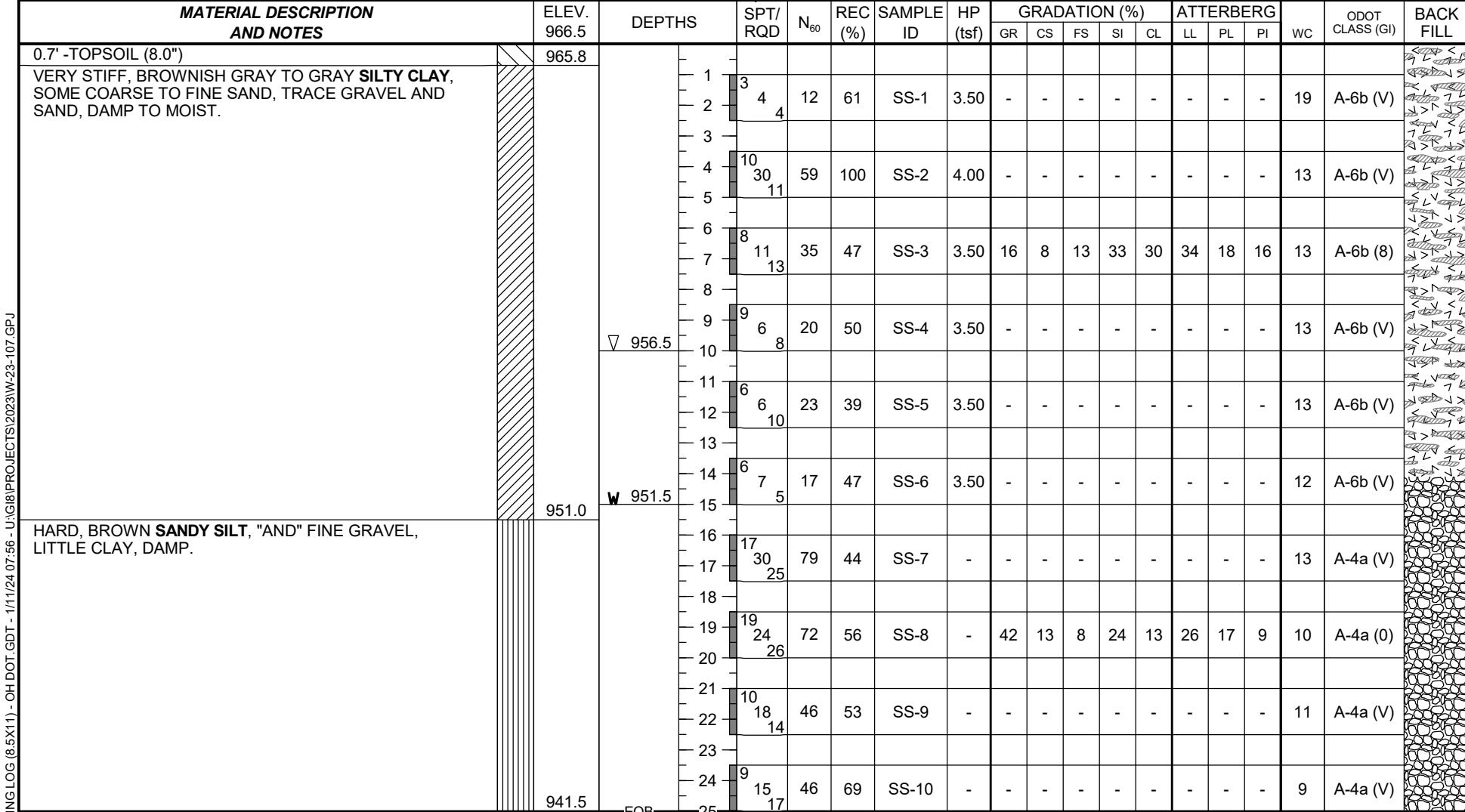
PAGE

1 OF 1

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 13.5' AND UPON COMPLETION @ 11.8'; CAVE-IN DEPTH @ 12.3'.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/23/23 END: 10/23/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 806+72 / 0' ALIGNMENT: CL WALL 8	EXPLORATION ID <b>B-015-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 966.5 (MSL) EOB: 25.0 ft. LAT / LONG: 40.088482, -82.840308	PAGE 1 OF 1



NOTES: SEEPAGE @ 14.0'; GROUNDWATER INTIALLY ENCOUNTERED @ 15.0' AND UPON COMPLETION @ 10.0'; CAVE-IN DEPTH @ 14.1'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/23/23 END: 10/23/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 808+72 / 0' ALIGNMENT: CL WALL 8	EXPLORATION ID <b>B-016-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 968.4 (MSL) EOB: 25.0 ft. LAT / LONG: 40.088693, -82.839666	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 968.4	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI		
0.6' -TOPSOIL (7.0") VERY STIFF TO HARD, LIGHT BROWN TO BROWN SILT AND CLAY, SOME COARSE TO FINE GRAVEL, LITTLE FINE GRAVEL, DAMP TO MOIST.	968.4	967.8	1	5				-	-	-	-	-	-	-	-	15	A-6a (V)
		954.6	2	5 5	14	50	SS-1	4.5+	-	-	-	-	-	-	-	13	A-6a (V)
		952.9	3														
		950.4	4	8 8 9	24	100	SS-2	4.5+	-	-	-	-	-	-	-	12	A-6a (V)
		943.4	5														
MEDIUM DENSE TO VERY DENSE, GRAY GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, MOIST.	943.4	943.4	6														
		943.4	7	11 11 12	33	58	SS-3	4.5+	-	-	-	-	-	-	-	10	A-6a (V)
		943.4	8														
		943.4	9	13 13	37	56	SS-4	4.5+	14	11	15	33	27	28	16	10	A-6a (6)
		943.4	10														
		943.4	11														
		943.4	12	7 7	20	78	SS-5	3.00	-	-	-	-	-	-	-	13	A-6a (V)
		943.4	13														
		943.4	14	5 11 9	29	44	SS-6	3.00	-	-	-	-	-	-	-	13	A-6a (V)
		943.4	15														
		943.4	16														
		943.4	17	12 12 12	35	61	SS-7	-	50	23	9	12	6	23	17	10	A-1-b (0)
		943.4	18														
		943.4	19	11 9 9	26	56	SS-8	-	-	-	-	-	-	-	-	14	A-1-b (V)
		943.4	20														
		943.4	21														
		943.4	22	16 16 17	48	83	SS-9	-	-	-	-	-	-	-	-	10	A-1-b (V)
		943.4	23														
		943.4	24	13 31 32	91	89	SS-10	-	-	-	-	-	-	-	-	8	A-1-b (V)
		943.4	25														
		943.4	EOB														

NOTES: SEEPAGE @ 17.5'; GROUNDWATER INITIALLY ENCOUNTERED @ 18.0' AND UPON COMPLETION @ 13.8'; CAVE-IN DEPTH @ 21.0'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/23/23 END: 10/23/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 810+72 / 0' ALIGNMENT: CL WALL 8	EXPLORATION ID <b>B-017-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 970.7 (MSL) EOB: 25.0 ft. LAT / LONG: 40.088908, -82.839020	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 970.7	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI			
0.4' -TOPSOIL (5.0") HARD TO VERY STIFF, BROWN TO GRAY SILT AND CLAY, SOME COARSE TO FINE SAND, TRACE FINE GRAVEL, DAMP TO MOIST.	970.3			1														
			6	9	30	81	SS-1	4.5+	-	-	-	-	-	-	-	17	A-6a (V)	
			2	12														
			3															
			4	20	60	36	SS-2	4.5+	-	-	-	-	-	-	-	11	A-6a (V)	
			5	22	20													
			6															
			7	12	32	89	SS-3	4.5+	9	10	16	37	28	28	17	10	A-6a (6)	
			8	11	11													
			9	11														
			10	7	36	86	SS-4	4.5+	-	-	-	-	-	-	-	13	A-6a (V)	
			11	10	15													
			12															
			13															
			14	5	36	86	SS-4	4.5+	-	-	-	-	-	-	-	10	A-6a (V)	
			15	5	12													
DENSE TO VERY DENSE, GRAY GRAVEL WITH SAND AND SILT, TRACE CLAY, DAMP TO MOIST.	955.2		16															
			17	10	39	53	SS-7	-	-	-	-	-	-	-	-	7	A-2-4 (V)	
			18	12	15													
			19	15	20	50	78	SS-8	-	45	15	12	22	6	NP	NP	11	A-2-4 (0)
			20															
			21	15														
			22	30	28	84	100	SS-9	-	-	-	-	-	-	-	9	A-2-4 (V)	
			23															
			24	13	17	62	69	SS-10	-	-	-	-	-	-	-	7	A-2-4 (V)	
			25	26														
		EOB																

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 18.0'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/23/23 END: 10/23/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 812+76 / 0' ALIGNMENT: CL WALL 8	EXPLORATION ID <b>B-018-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 975.5 (MSL) EOB: 25.0 ft. LAT / LONG: 40.089106, -82.838365	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 975.5	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.4' -TOPSOIL (5.0") VERY STIFF TO HARD, BROWN TO GRAY SANDY SILT, SOME CLAY, LITTLE FINE GRAVEL, DAMP TO MOIST.	975.1			1				-	-	-	-	-	-	-	-				
			6	10	32	58	SS-1	4.5+	-	-	-	-	-	-	-	14	A-4a (V)		
			2	12															
			3																
			4	12	13	46	SS-2	4.5+	-	-	-	-	-	-	-	10	A-4a (V)		
			5	19															
			6																
			7	17	13	40	SS-3	4.5+	-	-	-	-	-	-	-	13	A-4a (V)		
			8	15															
			9																
			10	8	9	29	SS-4	4.5+	-	-	-	-	-	-	-	11	A-4a (V)		
			11																
			12	7	8	23	SS-5	3.25	13	11	15	35	26	24	15	9	12	A-4a (5)	
			13																
			14	6	8	24	SS-6	3.25	-	-	-	-	-	-	-	-	12	A-4a (V)	
			15																
			16																
			17	3	4	13	SS-7	2.50	-	-	-	-	-	-	-	-	12	A-4a (V)	
			18	5															
			19																
DENSE TO VERY DENSE, BROWN-GRAY TO GRAY GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, MOIST.	957.5		8	13	14	39	SS-8	-	61	15	8	11	5	26	20	6	8	A-1-b (0)	
			20																
			21	11	29	91	0	SS-9	-	-	-	-	-	-	-	-			
			22	34															
			23		38	-	100	2S-9A	-	-	-	-	-	-	-	-	8	Rock (V)	
			24		28	50/3"		SS-10	-	-	-	-	-	-	-	-	5	Rock (V)	
			25																

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING; CAVE-IN DEPTH @ 16.4'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/23/23 END: 10/23/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 814+72 / 0' ALIGNMENT: CL WALL 8	EXPLORATION ID <b>B-019-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 974.9 (MSL) EOB: 25.0 ft. LAT / LONG: 40.089329, -82.837734	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 974.9	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.3' - TOPSOIL (4.0") HARD, BROWN SILT AND CLAY, LITTLE COARSE TO FINE SAND, TRACE FINE GRAVEL, DAMP TO MOIST.	974.6			1 7 9 9	26	83	SS-1	4.5+	-	-	-	-	-	-	-	16	A-6a (V)		
MEDIUM DENSE, BROWN GRAVEL WITH SAND AND SILT, MOIST.	969.4			4 8 12 16	40	94	SS-2	4.5+	-	-	-	-	-	-	-	10	A-6a (V)		
VERY STIFF TO HARD, GRAY SANDY SILT, SOME CLAY, LITTLE FINE GRAVEL, DAMP TO MOIST.	966.9			6 4 7 3	14	61	SS-3	-	-	-	-	-	-	-	-	10	A-2-4 (V)		
MEDIUM DENSE TO DENSE, GRAY GRAVEL WITH SAND, LITTLE SILT, TRACE CLAY, MOIST.	956.9			9 3 5 6	16	100	SS-4	4.25	12	11	17	35	25	24	14	10	11	A-4a (5)	
SHALE : GRAY, HIGHLY WEATHERED.	951.9	TR		11 4 5 6	16	56	SS-5	2.50	-	-	-	-	-	-	-	12	A-4a (V)		
	949.9	EOB		14 6 8 10	26	44	SS-6	2.50	-	-	-	-	-	-	-	12	A-4a (V)		
				15 19 10 12 15	39	47	SS-8	-	53	18	10	13	6	24	18	6	9	A-1-b (0)	
				21 22 8 9 8	24	56	SS-9	-	-	-	-	-	-	-	-	10	A-1-b (V)		
				23 24 50/5"	-	100	SS-10	-	-	-	-	-	-	-	-	9	Rock (V)		
				25															

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/27/23 END: 10/27/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 816+46 / 0' ALIGNMENT: CL WALL 8	EXPLORATION ID <b>B-020-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 974.3 (MSL) EOB: 25.0 ft. LAT / LONG: 40.089531, -82.837178	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 974.3	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI			
0.4' -TOPSOIL (4.5") HARD, BROWN TO GRAY SILT AND CLAY, SOME COARSE TO FINE SAND, TRACE TO LITTLE FINE GRAVEL, DAMP TO MOIST.	973.9			1														
			5	5	17	44	SS-1	4.5+	-	-	-	-	-	-	-	16	A-6a (V)	
			7															
			3															
			4	6	10	36	SS-2	4.5+	-	-	-	-	-	-	-	13	A-6a (V)	
			15															
			5															
			6															
			10															
			10															
			14															
			7															
			8															
			9															
			9															
			10															
			11															
			12															
			13															
			14															
			15															
			16															
			17															
			18															
			19	50/5"	-	67	SS-8	-	-	-	-	-	-	-	-	9	Rock (V)	
			20															
			21	50/5"	-	56	SS-9	-	-	-	-	-	-	-	-	4	Rock (V)	
			22															
			23															
			24	50/6"	-	73	SS-10	-	-	-	-	-	-	-	-	4	Rock (V)	
			25															
<b>SHALE : GRAY, HIGHLY WEATHERED.</b>																		

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING; CAVE-IN DEPTH @ 17.2'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

RESOURCE INTERNATIONAL, INC.



PROJECT: FRA-161-15.80  
TYPE: NOISE WALLS  
PID: 117607 SFN: NA  
START: 10/27/23 END: 10/

DRILLING FIRM / OPERATOR: \_\_\_\_\_ R  
SAMPLING FIRM / LOGGER: \_\_\_\_\_ RI  
DRILLING METHOD: \_\_\_\_\_ 3.25" HS  
SAMPLING METHOD: \_\_\_\_\_ SPT

DRILL RIG: DIEDRICH D-50 (# 313)  
HAMMER: AUTOMATIC  
CALIBRATION DATE: 3/21/22  
ENERGY RATIO (%): 86.4

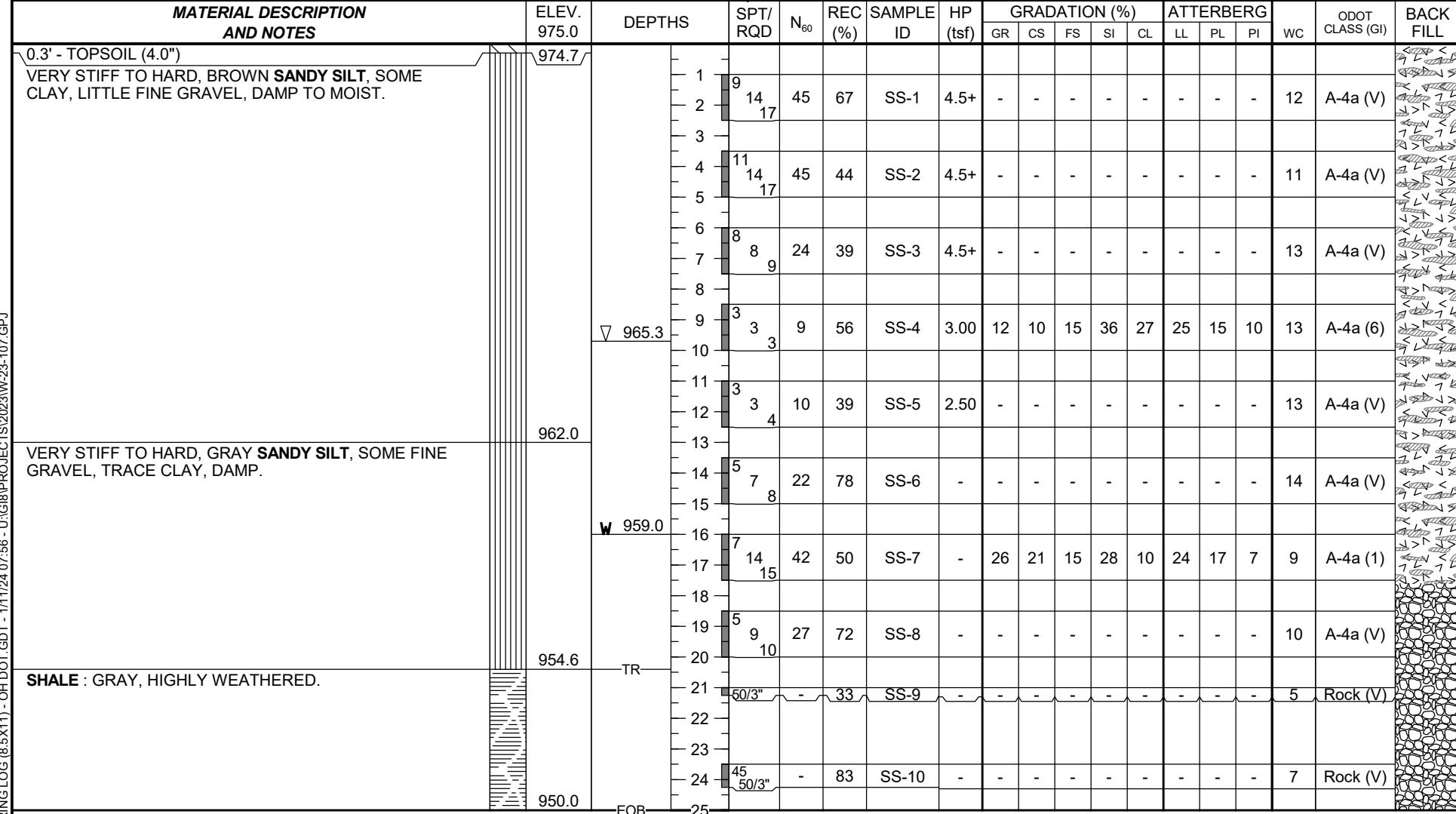
STATION / OFFSET: 818+03 / 0' EXP  
ALIGNMENT: CL WALL 8 B  
ELEVATION: 974.1 (MSL) EOB: 25.0 ft.  
LAT / LONG: 40.089729, -82.836617

**EXPLORATION ID  
B-021-0-23**

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING; CAVE-IN DEPTH @ 19.7'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/30/23 END: 10/30/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1100+00 / 0' ALIGNMENT: CL WALL 11	EXPLORATION ID <b>B-022-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 975.0 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090031, -82.835839	PAGE 1 OF 1



RESOURCE INTERNATIONAL, INC.



PROJECT: FRA-161-15.80  
TYPE: NOISE WALLS  
PID: 117607 SFN: NA  
START: 10/30/23 END: 10/3

DRILLING FIRM / OPERATOR: \_\_\_\_\_ F  
SAMPLING FIRM / LOGGER: \_\_\_\_\_ R  
DRILLING METHOD: \_\_\_\_\_ 3.25" HSA  
SAMPLING METHOD: \_\_\_\_\_ SPT / I

DRILL RIG: DIEDRICH D-50 (# 313)  
HAMMER: AUTOMATIC  
CALIBRATION DATE: 3/21/22  
ENERGY RATIO (%): 86.4

STATION / OFFSET: 1102+00 / 0'  
ALIGNMENT: CL WALL 11  
ELEVATION: 977.0 (MSL) EOB: 24.5 ft.  
LAT / LONG: 40.090244, -82.835195

EXPLORATION ID  
B-023-0-23

NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 16.11'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

**Project Name:** FRA-161-15.80

**Location:**

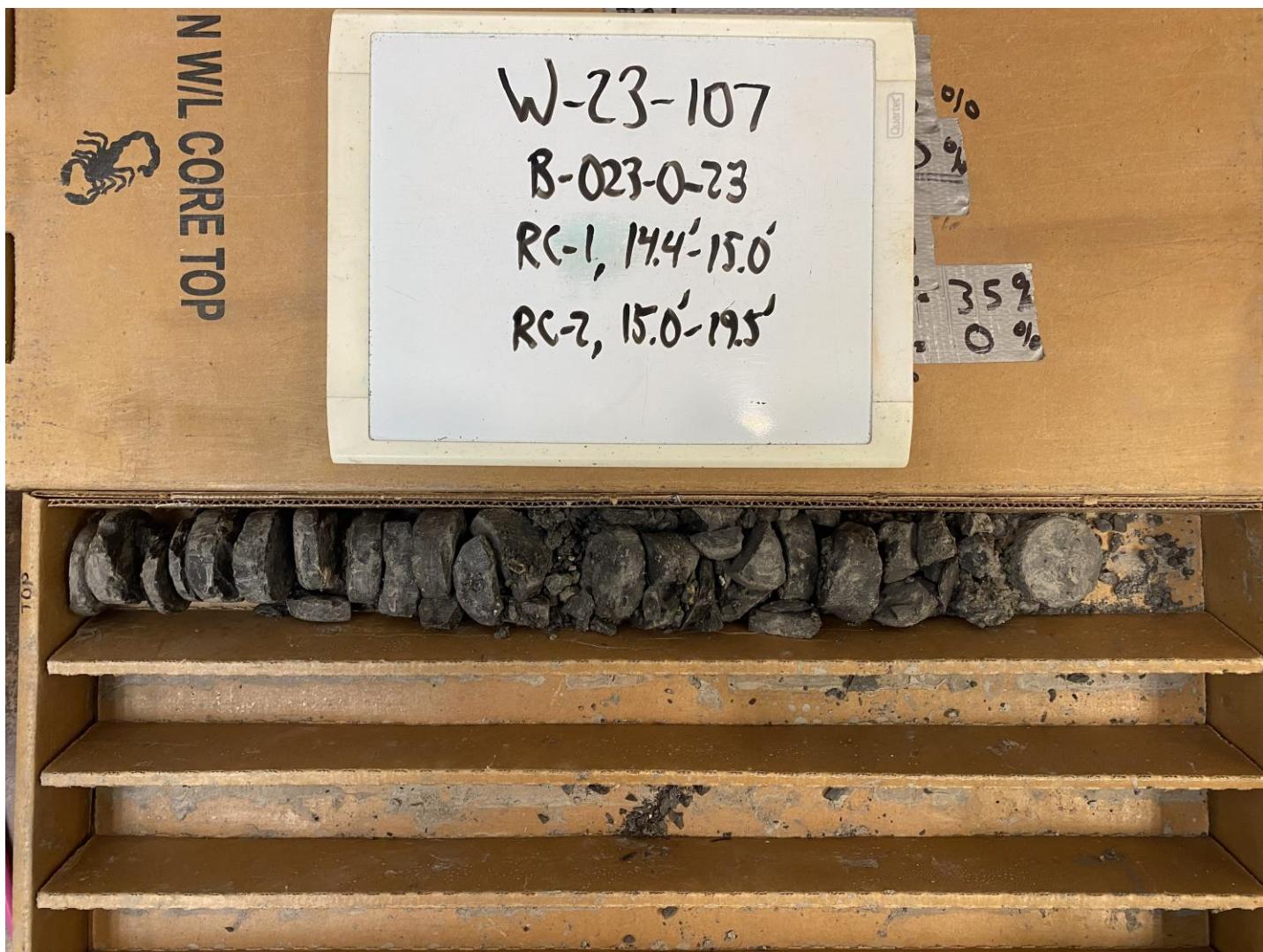
Franklin County, Ohio

**Photo No.**  
**6**

**Boring:**  
B-023-0-23

RC-1: 14.4-15.0'  
REC (%):0  
RQD (%):0

RC-2: 15.0-19.5'  
REC (%):35  
RQD (%):0



**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
7

**Boring:**  
B-023-0-23

RC-3: 19.5-24.5'  
REC (%):100  
RQD (%):0



 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/31/23 END: 10/31/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1104+00 / 0' ALIGNMENT: CL WALL 11	EXPLORATION ID <b>B-024-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 979.6 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090471, -82.834551	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 979.6	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL																	
								GR	CS	FS	SI	CL	LL	PL	PI																				
0.1' -TOPSOIL (1.0") HARD, BROWN CLAY, SOME SILT, LITTLE COARSE TO FINE SAND, TRACE FINE GRAVEL, DAMP TO MOIST.	979.5			1 5 2 8 3 4 8 10 16 5 6 17 28 26 7 8 9 28 18 12 10 11 12 13 14 10 17 21 15 16 10 14 15 17 18 19 6 14 17 20 21 22 23 24 25					-	-	-	-	-	-	-	-	19	A-7-6 (V)	< /> < /> < /> > < /> < /> < />																
VERY STIFF TO HARD, BROWN SILT AND CLAY, LITTLE COARSE TO FINE SAND, TRACE FINE GRAVEL, DAMP.	974.1																9	A-6a (V)	< /> < /> < /> > < /> < /> < />																
DENSE TO VERY DENSE, GRAY TO BLACK GRAVEL WITH SAND AND SILT, LITTLE CLAY, MOIST.	966.6																13	A-6a (V)	< /> < /> < /> > < /> < /> < />																
SHALE : GRAY, HIGHLY WEATHERED.	956.6	TR															10	A-2-4 (V)	< /> < /> < /> > < /> < /> < />																
	954.6	EOB															3	Rock (V)	< /> < /> < /> > < /> < /> < />																

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING; CAVE-IN DEPTH @ 18.5'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/31/23 END: 10/31/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1106+00 / 0' ALIGNMENT: CL WALL 11	EXPLORATION ID <b>B-025-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 980.2 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090688, -82.833893	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 980.2	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.2' -TOPSOIL (1.5") HARD, BROWN SILT AND CLAY, LITTLE GRAVEL AND SAND, DAMP.	980.0			1															
			4	5	17	50	SS-1	4.5+	-	-	-	-	-	-	-	20	A-6a (V)		
			5	7															
			3																
			4	8	12	61	SS-2	4.5+	-	-	-	-	-	-	-	14	A-6a (V)		
			17	17															
			5																
			6	12	17	55	SS-3	4.5+	10	10	16	34	30	27	16	11	8	A-6a (6)	
			21																
			7	17	21														
			8																
			9	10	13	39	SS-4	4.5+	-	-	-	-	-	-	-	10	A-6a (V)		
			14																
			10	18	21	69	SS-5	-	-	-	-	-	-	-	-	8	A-2-4 (V)		
			27																
			11																
			12	18	21	83	SS-6	-	38	23	12	17	10	27	20	7	6	A-2-4 (0)	
			27																
			13																
			14	9	12	39	SS-7	-											
			15																
			15	12	15														
			16	14	21	71	SS-8	-											
			28																
			17	14	21	71	SS-9	-											
			28																
			18																
			19	12	22	75	SS-10	-											
			30																
			20																
			21	12	16	42	SS-11	-											
			22	16	13														
			23																
			24	8	15	46	SS-12	-											
			25	17															
			EOB																

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 21.0' AND DRY UPON COMPLETION; CAVE-IN DEPTH @ 15.3'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 10/31/23 END: 10/31/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1108+00 / 0' ALIGNMENT: CL WALL 11	EXPLORATION ID <b>B-026-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 979.8 (MSL) EOB: 25.5 ft. LAT / LONG: 40.090906, -82.833225	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 979.8	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.3' -TOPSOIL (4.0") VERY STIFF TO HARD, LIGHT BROWN SILTY CLAY, "AND" FINE TO COARSE SAND, LITTLE FINE GRAVEL, DAMP TO MOIST.	979.5			1 4 5 13	26	67	SS-1	4.5+	-	-	-	-	-	-	-	17	A-6b (V)		
				3															
				4 18 18 16	49	39	SS-2	4.5+	-	-	-	-	-	-	-	19	A-6b (V)		
				5															
				6															
				7 9 13 15	40	89	SS-3	4.5+	-	-	-	-	-	-	-	12	A-6b (V)		
				8															
				9 4 4 4	12	50	SS-4	4.00	19	24	12	23	22	36	19	17	14	A-6b (4)	
				10															
				11 3 4 5	13	56	SS-5	-	-	-	-	-	-	-	-	20	A-2-4 (V)		
				12															
				13															
				14 14 15 16	45	0	SS-6	-	-	-	-	-	-	-	-				
				15 7	-	100	2S-6A	-	-	-	-	-	-	-	-	11	A-2-4 (V)		
				16															
				17 14 14 10	35	72	SS-7	-	-	-	-	-	-	-	-	10	A-2-4 (V)		
				18															
				19 9 9 14	33	0	SS-8	-	-	-	-	-	-	-	-				
				20 14 -	100	2S-8A	-	-	-	-	-	-	-	-	-	14	A-1-b (V)		
				21 12 15 17	46	75	SS-9	-	50	20	11	11	8	24	18	6	10	A-1-b (0)	
				22															
				23															
				24 11 14 13	39	0	SS-10	-	-	-	-	-	-	-	-	-			
				25 8	-	100	2S-10A	-	-	-	-	-	-	-	-	15	A-1-b (V)		
		EOB																	

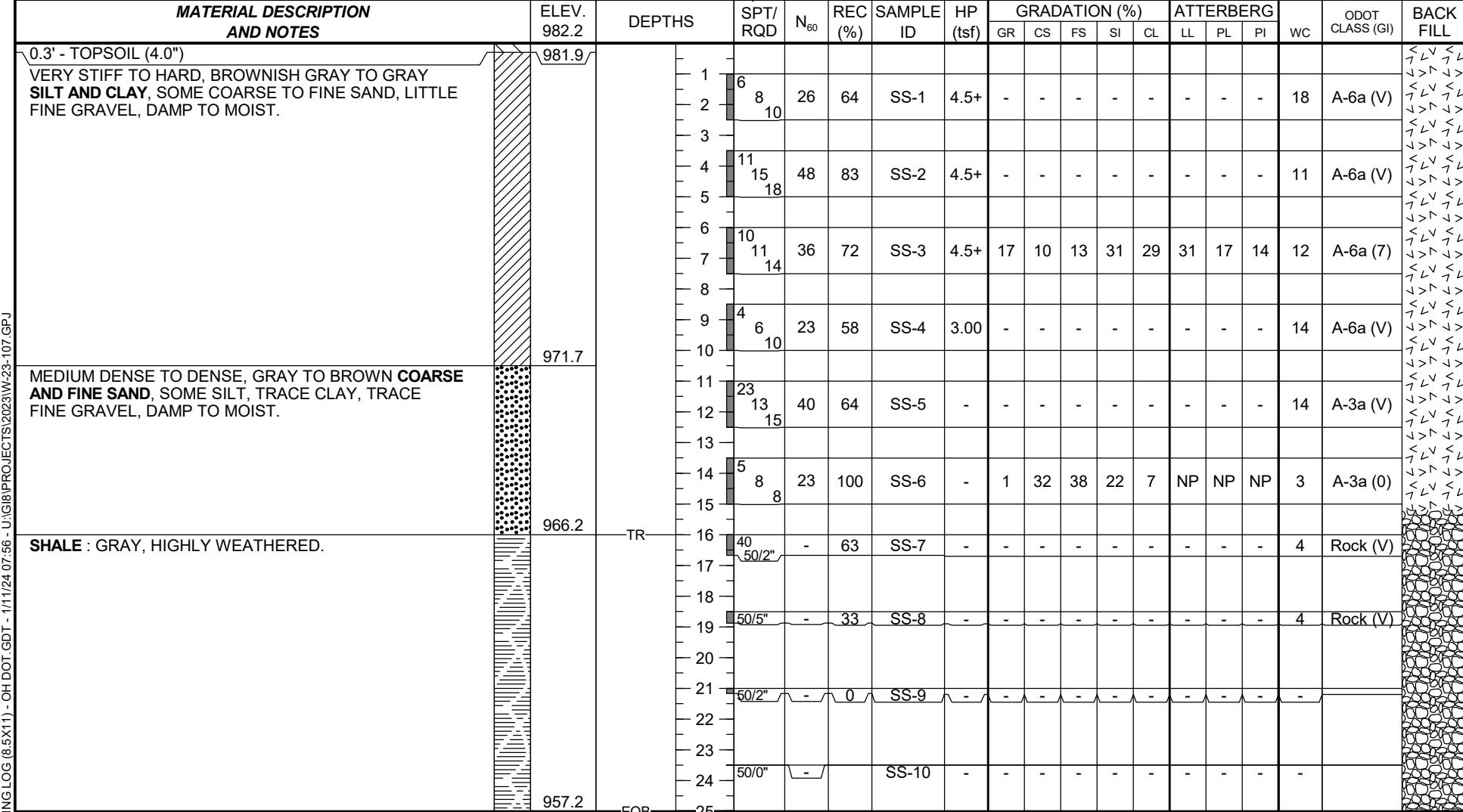
NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 18.5' AND DRY UPON COMPLETION; CAVE-IN DEPTH @ 13.5'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/1/23 END: 11/1/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1110+00 / 0' ALIGNMENT: CL WALL 11	EXPLORATION ID <b>B-027-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 981.5 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091062, -82.832539	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 981.5	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI			
0.3' -TOPSOIL (3.5") HARD, LIGHT BROWN SILT AND CLAY, LITTLE COARSE TO FINE SAND, TRACE GRAVEL, DAMP.	981.2			1 7 13 19	46 61	SS-1	4.5+	-	-	-	-	-	-	-	-	11	A-6a (V)	< /> < /> < /> > < /> < /> < />
				2 3 4 11 13 15	40 67	SS-2	4.5+	-	-	-	-	-	-	-	-	12	A-6a (V)	< /> < /> < /> > < /> < /> < />
				5 6 13 16 15	45 64	SS-3	4.5+	-	-	-	-	-	-	-	-	11	A-6a (V)	< /> < /> < /> > < /> < /> < />
				7 8 9 17 5 7	17	SS-4	4.5+	-	-	-	-	-	-	-	-	12	A-6a (V)	< /> < /> < /> > < /> < /> < />
LOOSE TO VERY DENSE, GRAY GRAVEL WITH SAND AND SILT, TRACE TO LITTLE CLAY, DAMP.	971.0			11 12 3 3 3	9 67	SS-5	-	-	-	-	-	-	-	-	-	14	A-2-4 (V)	< /> < /> < /> > < /> < /> < />
				13 14 4 4 5	13 58	SS-6	-	35	20	14	19	12	29	19	10	14	A-2-4 (0)	< /> < /> < /> > < /> < /> < />
				15 16 7 16 18	49 67	SS-7	-	-	-	-	-	-	-	-	-	8	A-2-4 (V)	< /> < /> < /> > < /> < /> < />
				17 18 19 6 9 12	30 67	SS-8	-	54	20	8	13	5	28	18	10	10	A-2-4 (0)	< /> < /> < /> > < /> < /> < />
				20 21 12 14 24	55 78	SS-9	-	-	-	-	-	-	-	-	-	12	A-2-4 (V)	< /> < /> < /> > < /> < /> < />
				22 23 24 23 50/5"	27	SS-10	-	-	-	-	-	-	-	-	-	4	Rock (V)	< /> < /> < /> > < /> < /> < />
				TR 958.5 956.5 EOB														

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/1/23 END: 11/1/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1112+00 / 0' ALIGNMENT: CL WALL 11	EXPLORATION ID <b>B-028-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 982.2 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091197, -82.831841	PAGE 1 OF 1



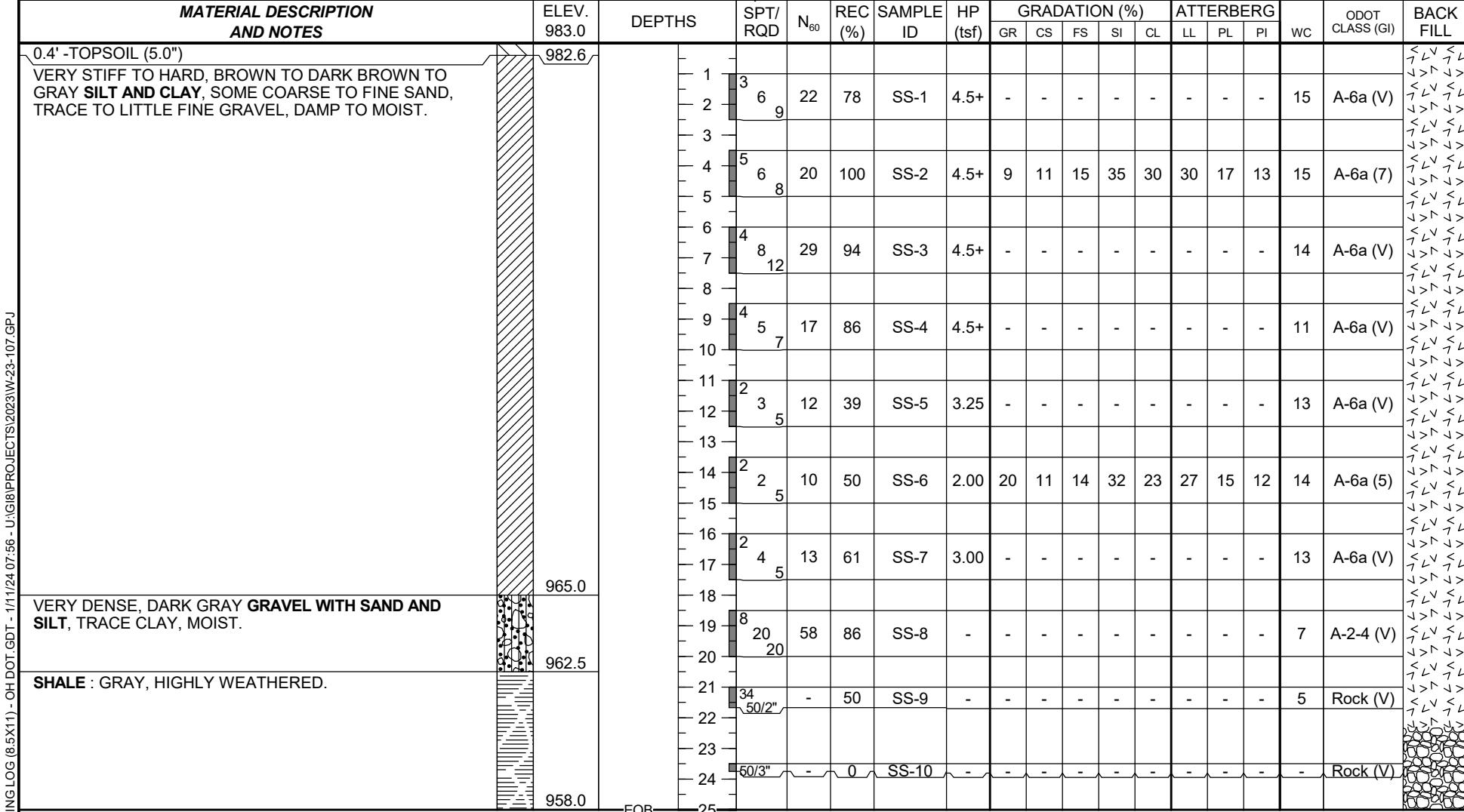
 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/1/23 END: 11/1/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1114+00 / 0' ALIGNMENT: CL WALL 11	EXPLORATION ID <b>B-029-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 983.0 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091321, -82.831138	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 983.0	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI			
0.3' - TOPSOIL (4.0") HARD TO VERY STIFF, BROWN TO GRAY SILT AND CLAY, SOME COARSE TO FINE SAND, LITTLE FINE GRAVEL, DAMP TO MOIST.	982.7			1														
			3	5	20	53	SS-1	4.5+	-	-	-	-	-	-	-	17	A-6a (V)	
			9															
			3															
			4	6	20	81	SS-2	4.5+	-	-	-	-	-	-	-	16	A-6a (V)	
			8															
			5															
			6															
			4	7	24	89	SS-3	4.5+	-	-	-	-	-	-	-	14	A-6a (V)	
			10															
			7															
			8															
			9	4	17	61	SS-4	4.5+	19	11	14	34	22	26	15	11	11	A-6a (5)
			5	7														
			10															
			11															
			3	3	14	81	SS-5	2.50	-	-	-	-	-	-	-	14	A-6a (V)	
			7	7														
			12															
			13															
			14	2	10	42	SS-6	2.00	-	-	-	-	-	-	-	14	A-6a (V)	
			3	4														
			15															
			16															
			17	4	23	56	SS-7	3.00	-	-	-	-	-	-	-	9	A-4a (V)	
			7	9														
			18															
			19	2	7	56	SS-8	2.25	12	15	16	34	23	25	15	10	13	A-4a (4)
			3	2														
			20															
			21	1														
			22	1	4	33	SS-9	0.75	-	-	-	-	-	-	-	14	A-4a (V)	
			2															
			23															
			24	8	19	60	SS-10	-	-	-	-	-	-	-	-	10	A-2-4 (V)	
			25	23														
		EOB																

NOTES: SEEPAGE @ 22.4' - 25.0' AND DRY UPON COMPLETION; CAVE-IN DEPTH @ 13.0'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/1/23 END: 11/1/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1115+84 / 0' ALIGNMENT: CL WALL 11	EXPLORATION ID <b>B-030-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 983.0 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091378, -82.830480	PAGE 1 OF 1



NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING; CAVE-IN DEPTH @ 22.3'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/16/23 END: 11/16/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 900+16 / 0' ALIGNMENT: CL WALL 9	EXPLORATION ID <b>B-031-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 974.5 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090580, -82.836109	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 974.5	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI			
0.5' -TOPSOIL (5.5") HARD, BROWN TO GRAY SANDY SILT, SOME CLAY, LITTLE FINE GRAVEL, DAMP TO MOIST.	974.0			1														
			4	5	17	78	SS-1	4.5+	-	-	-	-	-	-	-	19	A-4a (V)	
			5	7														
			3															
			4	18	23	0	SS-2	-	-	-	-	-	-	-	-			
			9	7														
			5	9	-	0	2S-2A	-	-	-	-	-	-	-	-			
			6															
			7	30	16	40	SS-3	4.5+	-	-	-	-	-	-	-	10	A-4a (V)	
			12	12														
			8															
			9	13	10	29	78	SS-4	4.5+	-	-	-	-	-	-	11	A-4a (V)	
			10	10														
			11															
			12	6	6	19	83	SS-5	4.5+	11	10	16	36	27	25	15	12	A-4a (6)
			13															
			14	6	7	22	0	SS-6	-	-	-	-	-	-	-			
			15	8	12	-	100	2S-6A	4.5+	-	-	-	-	-	-	13	A-4a (V)	
			16															
			17	4	5	14	75	SS-7	4.5+	-	-	-	-	-	-	12	A-4a (V)	
			18	5														
			19	3	4	20	83	SS-8	4.5+	-	-	-	-	-	-	13	A-4a (V)	
			20	10														
MEDIUM DENSE, DARK GRAY GRAVEL WITH SAND, TRACE SILT, TRACE CLAY, MOIST. -SHALE FRAGMENTS PRESENT THROUGHOUT -1.5' OF HEAVING SANDS @23.5'	954.0		21	4	8	26	78	SS-9	-	39	35	11	9	6	NP	NP	16	A-1-b (0)
			22	10														
			23															
			24	8	8	29	92	SS-10	-	-	-	-	-	-	-	16	A-1-b (V)	
			25	12														
			EOB															

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 19.8' AND UPON COMPLETION @ 20.5'; CAVE-IN DEPTH @ 13.8'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .



PROJECT: FRA-161-15.80  
TYPE: NOISE WALLS  
PID: 117607 SFN: NA  
START: 11/16/23 END: 11/

DRILLING FIRM / OPERATOR: \_\_\_\_\_ R  
SAMPLING FIRM / LOGGER: \_\_\_\_\_ RI  
DRILLING METHOD: \_\_\_\_\_ 3.25" HS  
SAMPLING METHOD: \_\_\_\_\_ SPT

DRILL RIG: DIEDRICH D-50 (# 313)  
HAMMER: AUTOMATIC  
CALIBRATION DATE: 3/21/22  
ENERGY RATIO (%): 86.4

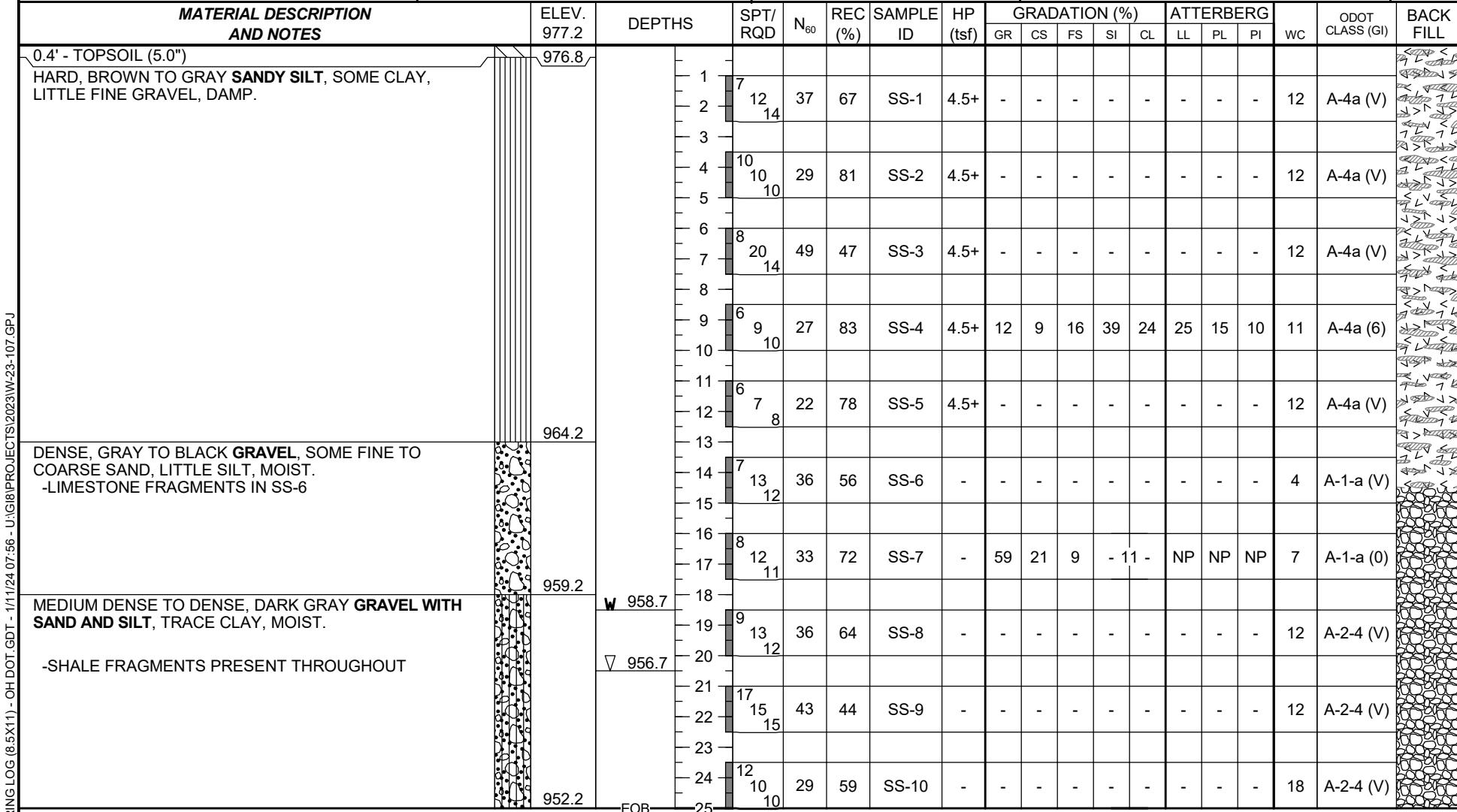
STATION / OFFSET: 902+00 / 0'  
ALIGNMENT: CL WALL 9  
ELEVATION: 975.2 (MSL) EO: \_\_\_\_\_  
LAT / LONG: 40.090809, -82.8

**EXPLORATION ID**  
**B-032-0-23**

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 18.5' AND UPON COMPLETION @ 20.5'; CAVE-IN DEPTH @ 15.1'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/16/23 END: 11/16/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 904+00 / 0' ALIGNMENT: CL WALL 9	EXPLORATION ID <b>B-033-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 977.2 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091043, -82.834836	PAGE 1 OF 1



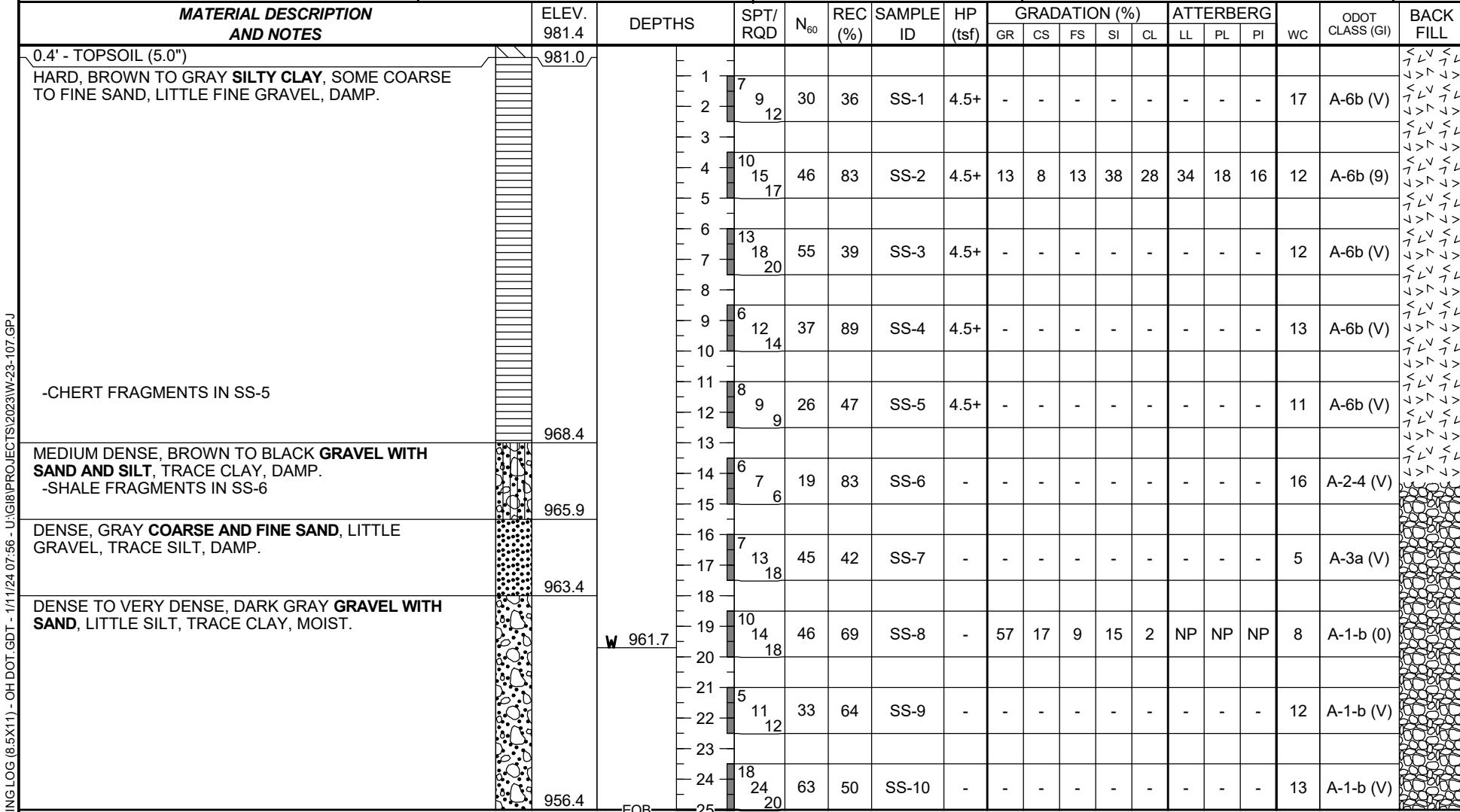
 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/16/23 END: 11/16/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 906+00 / 0' ALIGNMENT: CL WALL 9	EXPLORATION ID <b>B-034-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 979.3 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091273, -82.834170	PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 979.3	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI			
0.4 - TOPSOIL (5.0") HARD, BROWN SILT AND CLAY, LITTLE GRAVEL AND SAND, DAMP.	978.9			1 6 2 10 13 3 4 7 8 10 12 14 5 6 10 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25				-	-	-	-	-	-	-	-	12	A-6a (V)	< /> < /> < /> > < /> < /> < />
-ROOT FIBERS IN SS-4	968.8															17	A-6a (V)	
DENSE TO VERY DENSE, GRAY GRAVEL, LITTLE COARSE TO FINE SAND, TRACE SILT, DAMP.																15	A-6a (V)	
MEDIUM DENSE TO VERY DENSE, BLACK GRAVEL WITH SAND AND SILT, MOIST. -SHALE FRAGMENTS PRESENT THROUGHOUT	958.8															6	A-1-a (V)	
																20	A-1-a (0)	
																6	A-1-a (V)	
																6	A-1-a (V)	
																16	A-2-4 (V)	
																11	A-2-4 (V)	

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 21.0' AND DRY UPON COMPLETION; CAVE-IN DEPTH @ 14.0'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/15/23 END: 11/15/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 908+00 / 0' ALIGNMENT: CL WALL 9	EXPLORATION ID <b>B-035-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 981.4 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091443, -82.833496	PAGE 1 OF 1



NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 19.7' AND DRY UPON COMPLETION; CAVE-IN DEPTH @ 14.3'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.



PROJECT: FRA-161-15.80  
TYPE: NOISE WALLS  
PID: 117607 SFN: NA  
START: 11/15/23 END: 11/

DRILLING FIRM / OPERATOR: R  
SAMPLING FIRM / LOGGER: RIM  
DRILLING METHOD: 3.25" HS  
SAMPLING METHOD: SPT

DRILL RIG: DIEDRICH D-50 (# 313)  
HAMMER: AUTOMATIC  
CALIBRATION DATE: 3/21/22  
ENERGY RATIO (%): 86.4

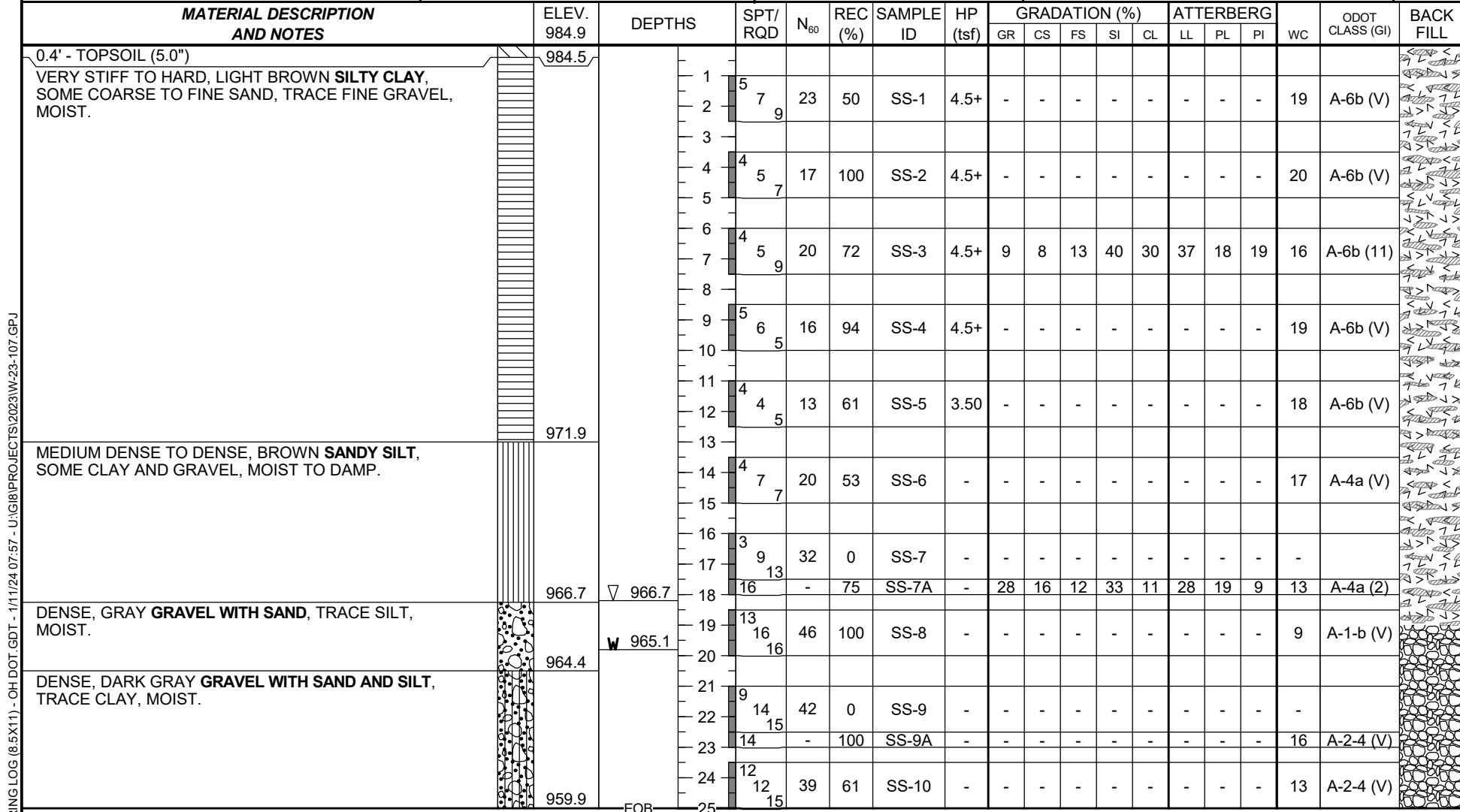
STATION / OFFSET: 910+00 / 0'  
ALIGNMENT: CL WALL 9  
ELEVATION: 983.2 (MSL) EOB:  
LAT / LONG: 40.091597, -82.83

EXPLORATION ID <b>B-036-0-23</b>	PAGE 1 OF 1
5.0 ft.	

NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 21.0' AND DRY UPON COMPLETION; CAVE-IN DEPTH @ 14.3'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

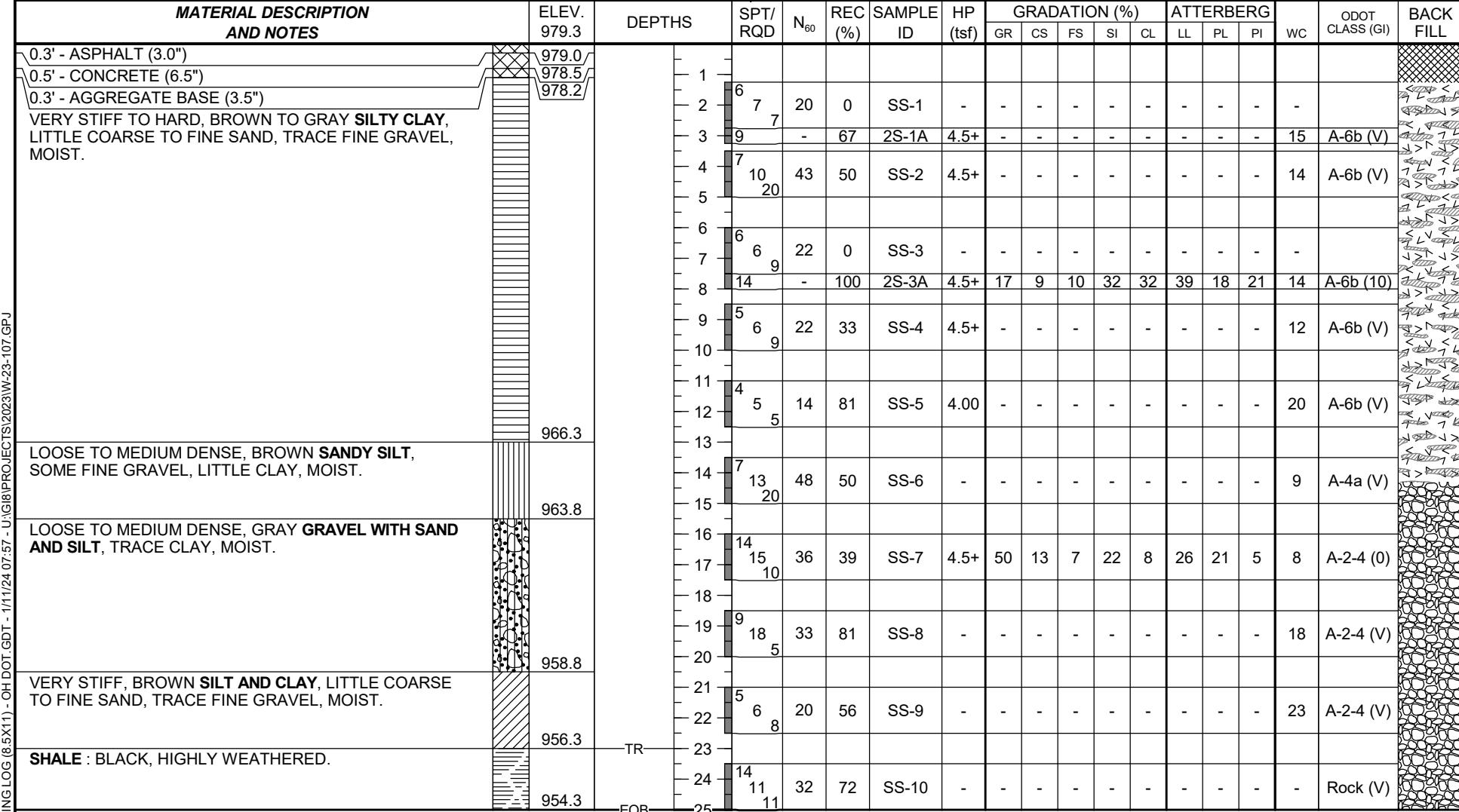
 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/15/23 END: 11/15/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 912+00 / 0' ALIGNMENT: CL WALL 9	EXPLORATION ID <b>B-037-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 984.9 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091724, -82.832101	PAGE 1 OF 1



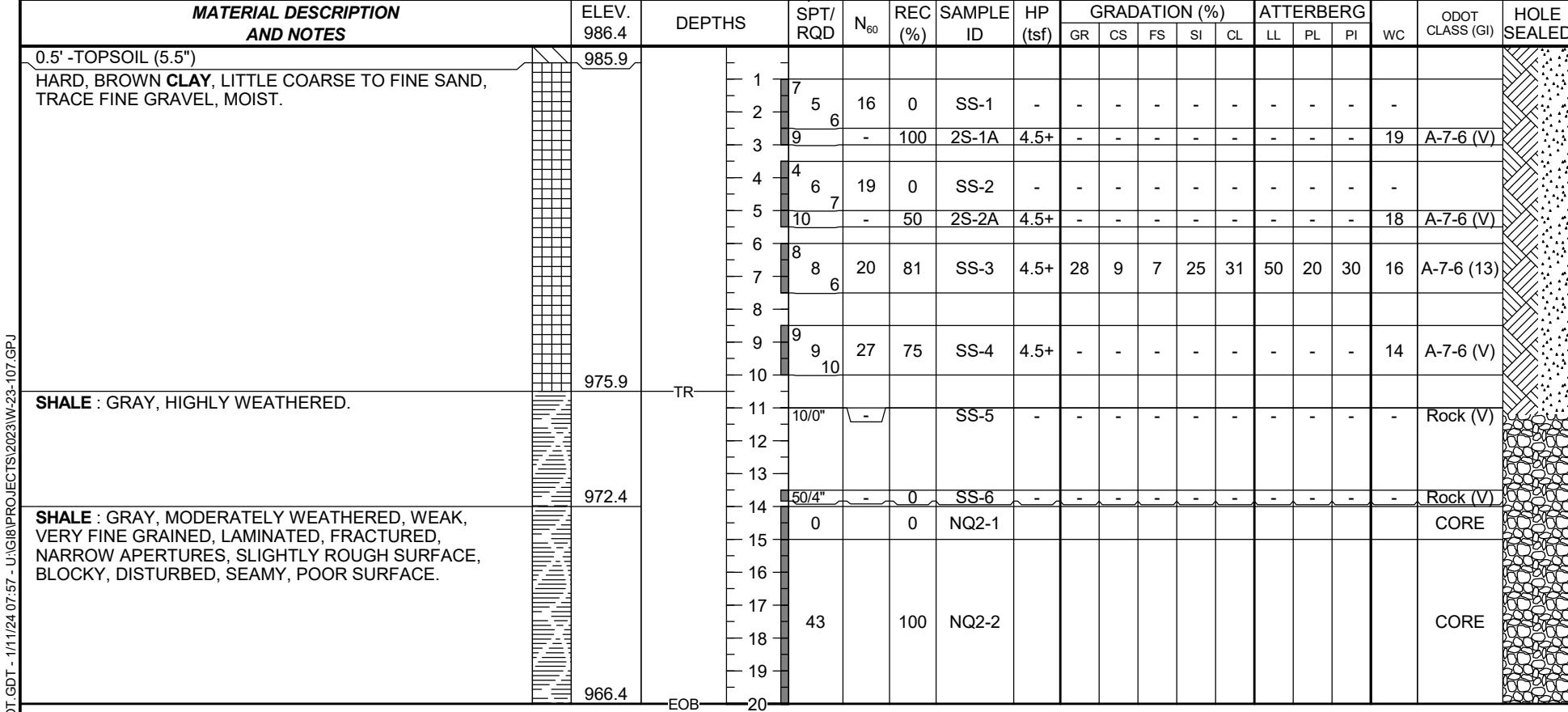
NOTES: GROUNDWATER INTIALLY ENCOUNTERED @ 19.8' AND UPON COMPLETION @ 18.2'; CAVE-IN DEPTH @ 19.0'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 12/5/23 END: 12/5/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 120+00 / 0' ALIGNMENT: CL WALL 12 ELEVATION: 979.3 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091445, -82.828386	EXPLORATION ID <b>B-038-0-23</b>
				PAGE 1 OF 1



 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 12/4/23 END: 12/4/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 121+41.21 / 0' ALIGNMENT: CL WALL 12 ELEVATION: 986.4 (MSL) EOB: 20.0 ft. LAT / LONG: 40.091317, -82.827731	EXPLORATION ID <b>B-039-0-23</b>
				PAGE 1 OF 1



NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 11.2'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
**8**

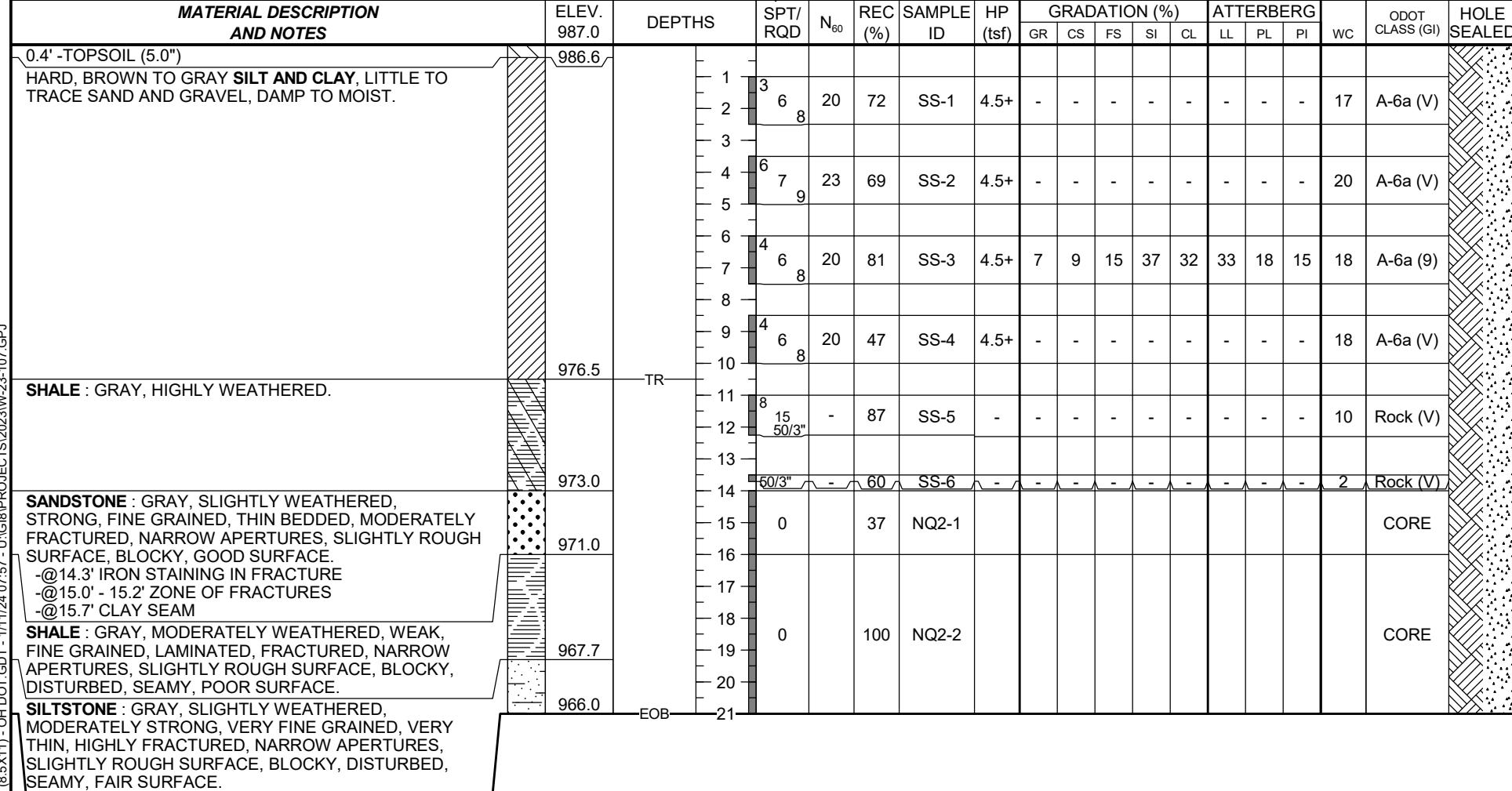
**Boring:**  
B-039-0-23

RC-1: 14.0-15.0'  
REC (%):0  
RQD (%):0

RC-2: 15.0-20.0'  
REC (%):100  
RQD (%):43

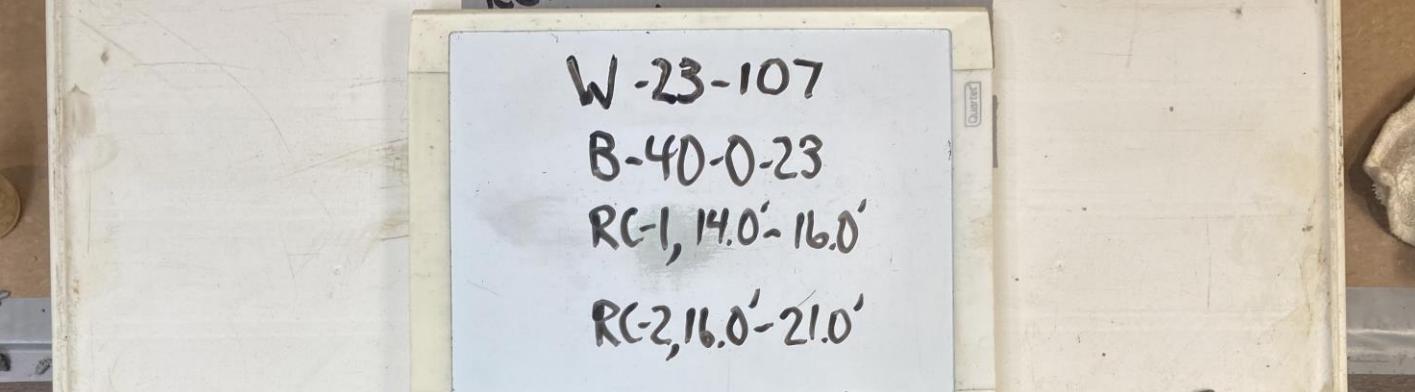


 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 12/4/23 END: 12/4/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 123+26.79 / 0' ALIGNMENT: CL WALL 12 ELEVATION: 987.0 (MSL) EOB: 21.0 ft. LAT / LONG: 40.091207, -82.827079	EXPLORATION ID <b>B-040-0-23</b>
				PAGE 1 OF 1

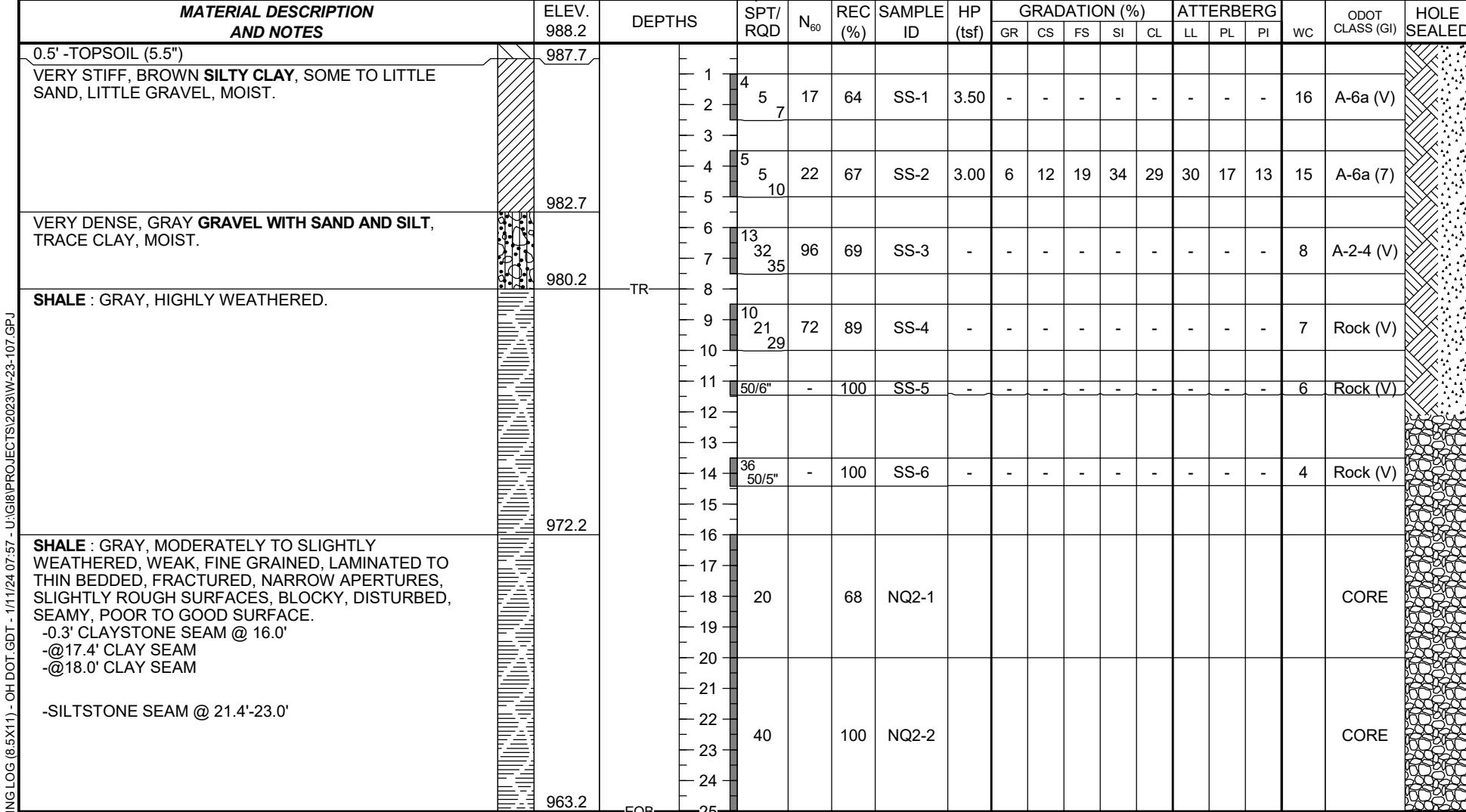


NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 94 LBS CEMENT / 25 LBS BENTONITE POWDER / 40 GAL WATER.

<p><b>Project Name:</b> FRA-161-15.80</p>	<p><b>Location:</b> Franklin County, Ohio</p>
<p><b>Photo No.</b> <b>9</b></p>	
<p><b>Boring:</b> B-040-0-23</p>	
<p>RC-1: 14.0-16.0' REC (%):37 RQD (%):0</p>	
<p>RC-2: 16.0-21.0' REC (%):100 RQD (%):0</p>	

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 12/4/23 END: 12/4/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 124+97.00 / 0' ALIGNMENT: CL WALL 12 ELEVATION: 988.2 (MSL) EOB: 25.0 ft. LAT / LONG: 40.091033, -82.826474	EXPLORATION ID <b>B-041-0-23</b>
				PAGE 1 OF 1



NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 12.1'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 94 LBS CEMENT / 25 LBS BENTONITE POWDER / 40 GAL WATER.

**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
**10**

**Boring:**  
B-041-0-23

RC-1: 16.0-20.0'  
REC (%):68  
RQD (%):20

RC-2: 20.0-25.0'  
REC (%):100  
RQD (%):40



 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/9/23 END: 11/9/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 1500+29 / 0' ALIGNMENT: CL WALL 15 ELEVATION: 1030.3 (MSL) EOB: 24.0 ft. LAT / LONG: 40.090577, -82.811738	EXPLORATION ID <b>B-042-0-23</b>
				PAGE 1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 1030.3	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	HOLE SEALED	
								GR	CS	FS	SI	CL	LL	PL	PI				
0.6' -TOPSOIL (6.5") HARD, BROWN SILT AND CLAY, SOME COARSE TO FINE SAND, TRACE FINE GRAVEL, DAMP TO MOIST.	1029.7			1															
			3	8	23	44	SS-1	4.5+	-	-	-	-	-	-	-	14	A-6a (V)		
			8																
			3																
			4	14	39	0	SS-2	-	-	-	-	-	-	-	-	13	A-6a (V)		
			14	13															
			5	17	-	100	2S-2A	4.5+	-	-	-	-	-	-	-	13	A-6a (V)		
			17																
			6																
			7	4	16	58	SS-3	4.5+	9	11	16	37	27	27	16	11	15	A-6a (6)	
			5	6															
			8																
			9	4	23	58	SS-4	4.5+	-	-	-	-	-	-	-	12	A-6a (V)		
			8	8															
			10																
SANDSTONE : GRAY, HIGHLY WEATHERED.	1019.3	TR	11	40	-	100	SS-5	-	-	-	-	-	-	-	-	6	Rock (V)		
			12	42	50/2"	-													
			13																
			14	50/0"			SS-6	-	-	-	-	-	-	-	-	Rock (V)			
			15																
			16	50/3"	-	67	SS-7	-	-	-	-	-	-	-	-	5	Rock (V)		
			17																
			18														CORE		
			19	58		75	NQ2-1												
			20																
			21														CORE		
			22	68		92	NQ2-2												
			23																
			24																

NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 16.9'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
**11**

**Boring:**  
B-042-0-23

RC-1: 18.0-19.0'  
REC (%):75  
RQD (%):58

RC-2: 19.0-24.0'  
REC (%):92  
RQD (%):68





PROJECT: FRA-161-15.80  
TYPE: NOISE WALLS  
PID: 117607 SFN: NA  
START: 11/9/23 END: 11/

DRILLING FIRM / OPERATOR: \_\_\_\_\_ R  
SAMPLING FIRM / LOGGER: \_\_\_\_\_ RI  
DRILLING METHOD: \_\_\_\_\_ 3.25" HSA  
SAMPLING METHOD: \_\_\_\_\_ SPT / N

DRILL RIG: DIEDRICH D-50 (# 313)  
HAMMER: AUTOMATIC  
CALIBRATION DATE: 3/21/22  
ENERGY RATIO (%): 86.4

STATION / OFFSET: 1502+16 / 0'  
ALIGNMENT: CL WALL 15  
ELEVATION: 1035.0 (MSL) EOB:  
LAT / LONG: 40.090545, -82.81

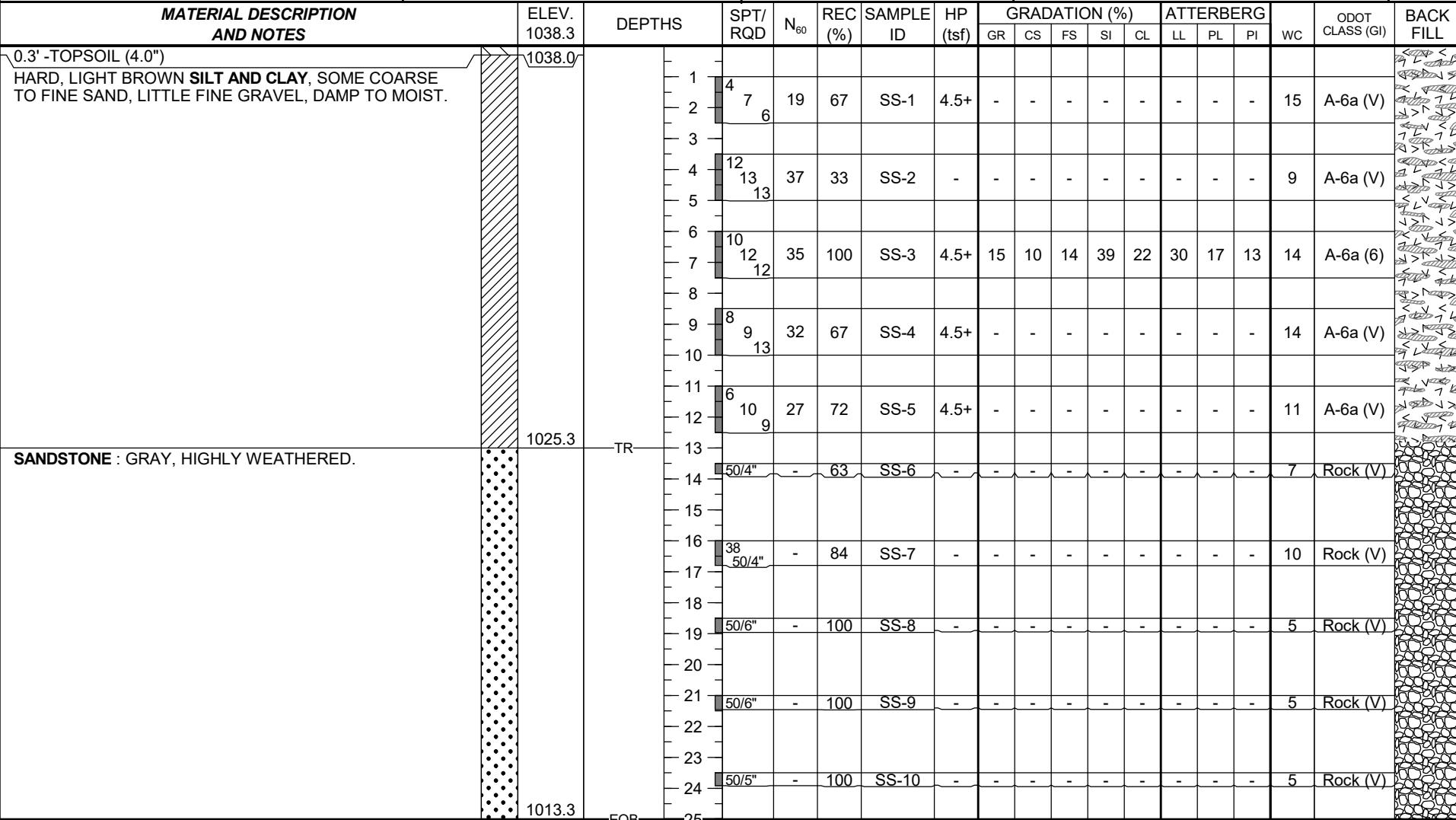
**EXPLORATION ID**  
**B-043-0-23**

NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 15.2'.

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER

<b>Project Name:</b> FRA-161-15.80	<b>Location:</b> Franklin County, Ohio
<b>Photo No.</b> <b>12</b>	
<b>Boring:</b> B-043-0-23	
RC-1: 18.5-19.5' REC (%):75 RQD (%):0	
RC-2: 19.5-24.5' REC (%):68 RQD (%):33	

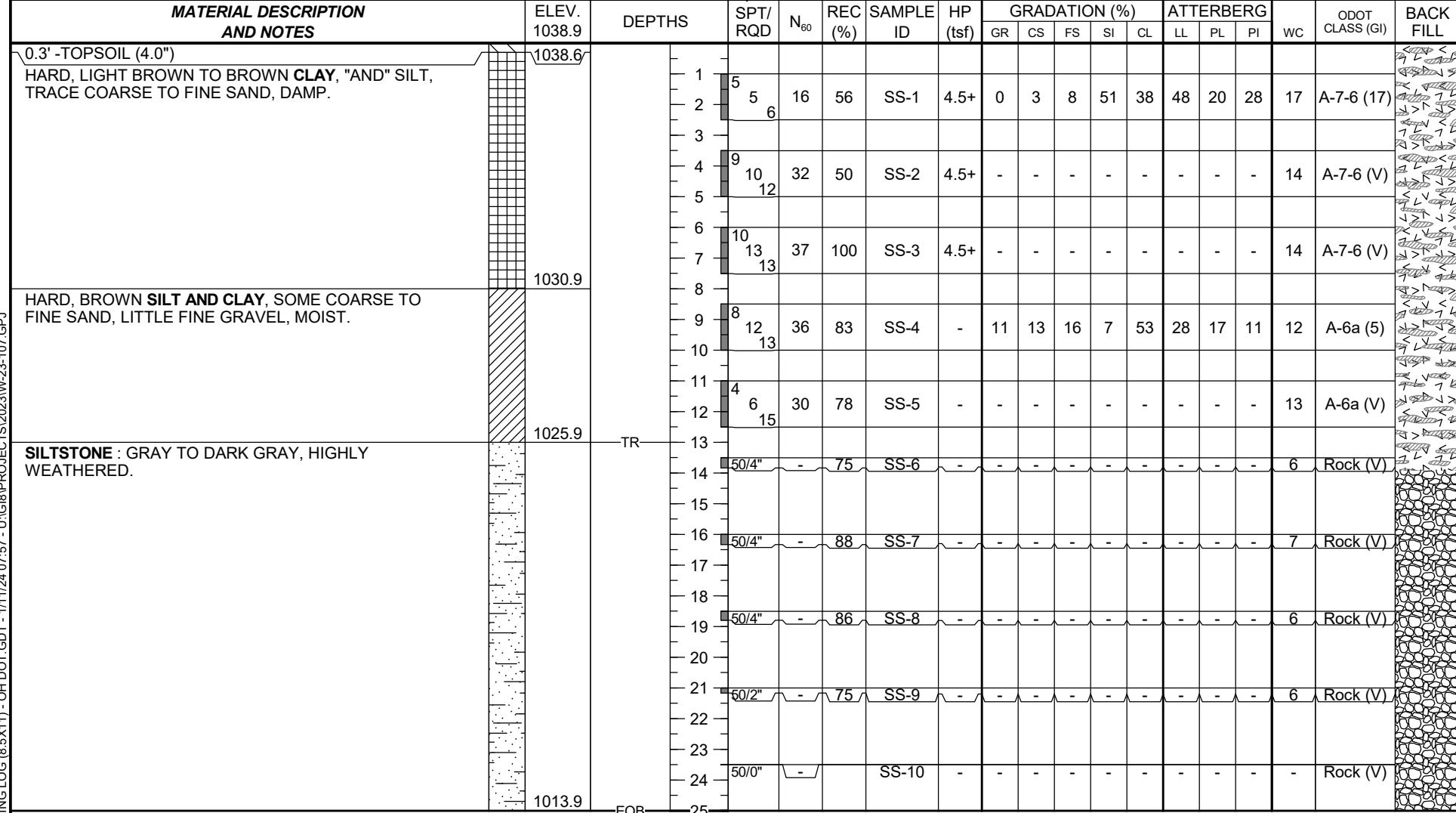
PROJECT: FRA-161-15.80	DRILLING FIRM / OPERATOR: RII / TG	DRILL RIG: DIEDRICH D-50 (# 313)	STATION / OFFSET: 1504+27 / 0'	EXPLORATION ID B-044-0-23
TYPE: NOISE WALLS	SAMPLING FIRM / LOGGER: RII / MJ	HAMMER: AUTOMATIC	ALIGNMENT: CL WALL 15	
PID: 117607 SFN: NA	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 3/21/22	ELEVATION: 1038.3 (MSL) EOB: 25.0 ft.	PAGE
START: 11/14/23 END: 11/14/23	SAMPLING METHOD: SPT	ENERGY RATIO (%): 86.4	LAT / LONG: 40.090479, -82.810313	1 OF 1



NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING; CAVE-IN DEPTH @ 12.8'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS.

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/14/23 END: 11/14/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1506+08 / 0' ALIGNMENT: CL WALL 15	EXPLORATION ID <b>B-045-0-23</b>
	DRILLING METHOD: 3.25" HSA SAMPLING METHOD: SPT	CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	ELEVATION: 1038.9 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090452, -82.809651	PAGE 1 OF 1



NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 13.9'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/10/23 END: 11/10/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 1508+10 / 0' ALIGNMENT: CL WALL 15 ELEVATION: 1039.1 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090415, -82.808921	EXPLORATION ID <b>B-046-0-23</b>
				PAGE 1 OF 1

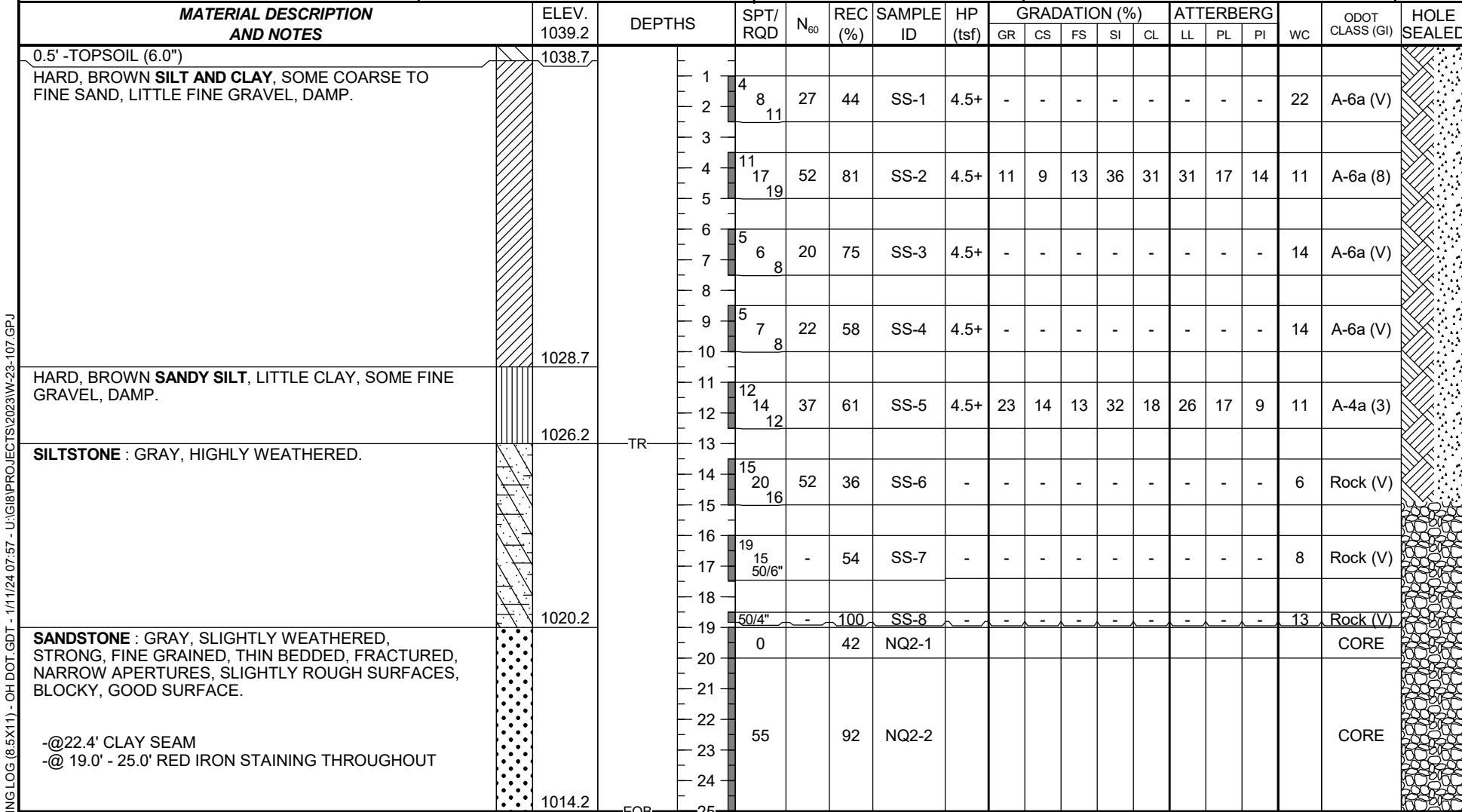
MATERIAL DESCRIPTION AND NOTES	ELEV. 1039.1	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	HOLE SEALED
								GR	CS	FS	SI	CL	LL	PL	PI			
0.5' -TOPSOIL (5.5") HARD, BROWNISH GRAY CLAY, "AND" SILT, LITTLE FINE GRAVEL, LITTLE COARSE TO FINE SAND, DAMP.	1038.6			1 5 7 8 2 3 4 12 14 14 5 6 15 16 16 7 8 10 12 15 9 11 11 18 16 16 12 15 10 11 12 13 14 6 16 32 16 16 15 16 50/4" 100 SS-7 50/4" 50 SS-8 0 33 NQ2-1 37 93 NQ2-2														
HARD, BROWNISH GRAY SILT AND CLAY, SOME COARSE TO FINE SAND, SOME FINE GRAVEL, MOIST.	1033.6																	
SANDSTONE : GRAY, HIGHLY WEATHERED.	1028.6	TR																
SANDSTONE : GRAY, SLIGHTLY WEATHERED, STRONG, FINE GRAINED, THIN BEDDED, MODERATELY FRACTURED, NARROW APERTURES, SLIGHTLY ROUGH SURFACES, BLOCKY, GOOD SURFACE. -@21.3' - 21.5' SHALE -@22.5' CLAY SEAM -@ 24.5'-25.0' SHALE	1020.1 1014.6																	
		EOB																

NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 15.2'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

<b>Project Name:</b> FRA-161-15.80		<b>Location:</b> Franklin County, Ohio
<b>Photo No.</b> <b>13</b>		
<b>Boring:</b> B-046-0-23		<p>W-23-107      B-046-0-23      RC-1, 19.0'-20.0'      RC-2, 20.0'-25.0'</p> 
RC-1: 19.0-20.0' REC (%):33 RQD (%):0		
RC-2: 20.0-25.0' REC (%):93 RQD (%):37		

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/10/23 END: 11/10/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 1510+10 / 0' ALIGNMENT: CL WALL 15 ELEVATION: 1039.2 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090391, -82.808171	EXPLORATION ID <b>B-047-0-23</b>
				PAGE 1 OF 1



NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 14.9'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
**14**

**Boring:**  
B-047-0-23

RC-1: 19.0-20.0'  
REC (%):42  
RQD (%):0

RC-2: 20.0-25.0'  
REC (%):92  
RQD (%):55



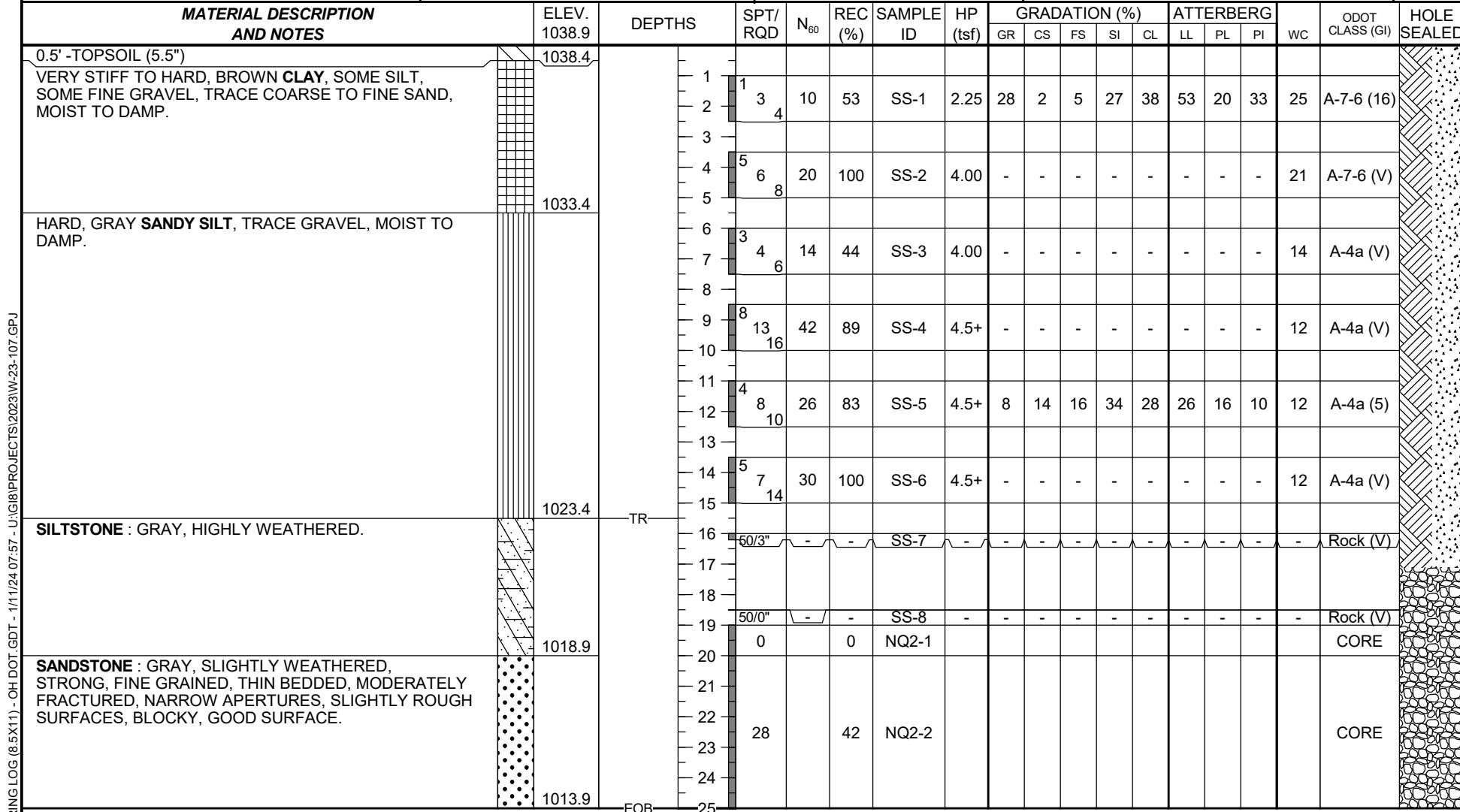
 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/10/23 END: 11/10/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC	STATION / OFFSET: 1512+10 / 0' ALIGNMENT: CL WALL 15	EXPLORATION ID <b>B-048-0-23</b>
	DRILLING METHOD: 3.25" HSA	CALIBRATION DATE: 3/21/22	ELEVATION: 1037.4 (MSL) EOB: 25.0 ft.	PAGE
	SAMPLING METHOD: SPT	ENERGY RATIO (%): 86.4	LAT / LONG: 40.090360, -82.807478	1 OF 1

MATERIAL DESCRIPTION AND NOTES	ELEV. 1037.4	DEPTHs	SPT/ RQD	N <sub>60</sub>	REC (%)	SAMPLE ID	HP (tsf)	GRADATION (%)					ATTERBERG			WC	ODOT CLASS (GI)	BACK FILL
								GR	CS	FS	SI	CL	LL	PL	PI			
0.5' -TOPSOIL (6.0") HARD, BROWN TO GRAY SILTY CLAY, SOME COARSE TO FINE SAND, TRACE FINE GRAVEL, DAMP TO MOIST.	1036.9			1														
			3	12	39	SS-1	4.5+	-	-	-	-	-	-	-	-	19	A-6b (V)	
			5															
			6	20	100	SS-2	4.5+	10	5	19	32	34	36	17	19	14	A-6b (10)	
			7															
			6	24	33	SS-3	4.5+	-	-	-	-	-	-	-	-	17	A-6b (V)	
			11															
			8															
			6	26	69	SS-4	4.5+	-	-	-	-	-	-	-	-	12	A-6b (V)	
			8															
			10															
VERY STIFF TO HARD, GRAY SANDY SILT, SOME CLAY, LITTLE FINE GRAVEL, DAMP.	1026.9			11														
			5	22	83	SS-5	4.5+	18	11	14	33	24	26	16	10	11	A-4a (4)	
			6															
			9															
			13															
			14	13	64	SS-6	3.00	-	-	-	-	-	-	-	-	12	A-4a (V)	
			3															
			4															
			5															
SHALE : BROWN, SEVERELY WEATHERED.	1021.4	TR	16															
			28															
			35	-	40	SS-7	-									0	Rock (V)	
			50/3"															
			17															
			18															
			19	72	83	SS-8	-									13	Rock (V)	
			24															
			26															
			21	50/3"	0	SS-9	-											
			22															
			23															
			24	11	36	SS-10	-									20	Rock (V)	
			10															
			15															
			EOB															
			25															

NOTES: GROUNDWATER NOT ENCOUNTERED DURING DRILLING; CAVE-IN DEPTH @ 16.1'

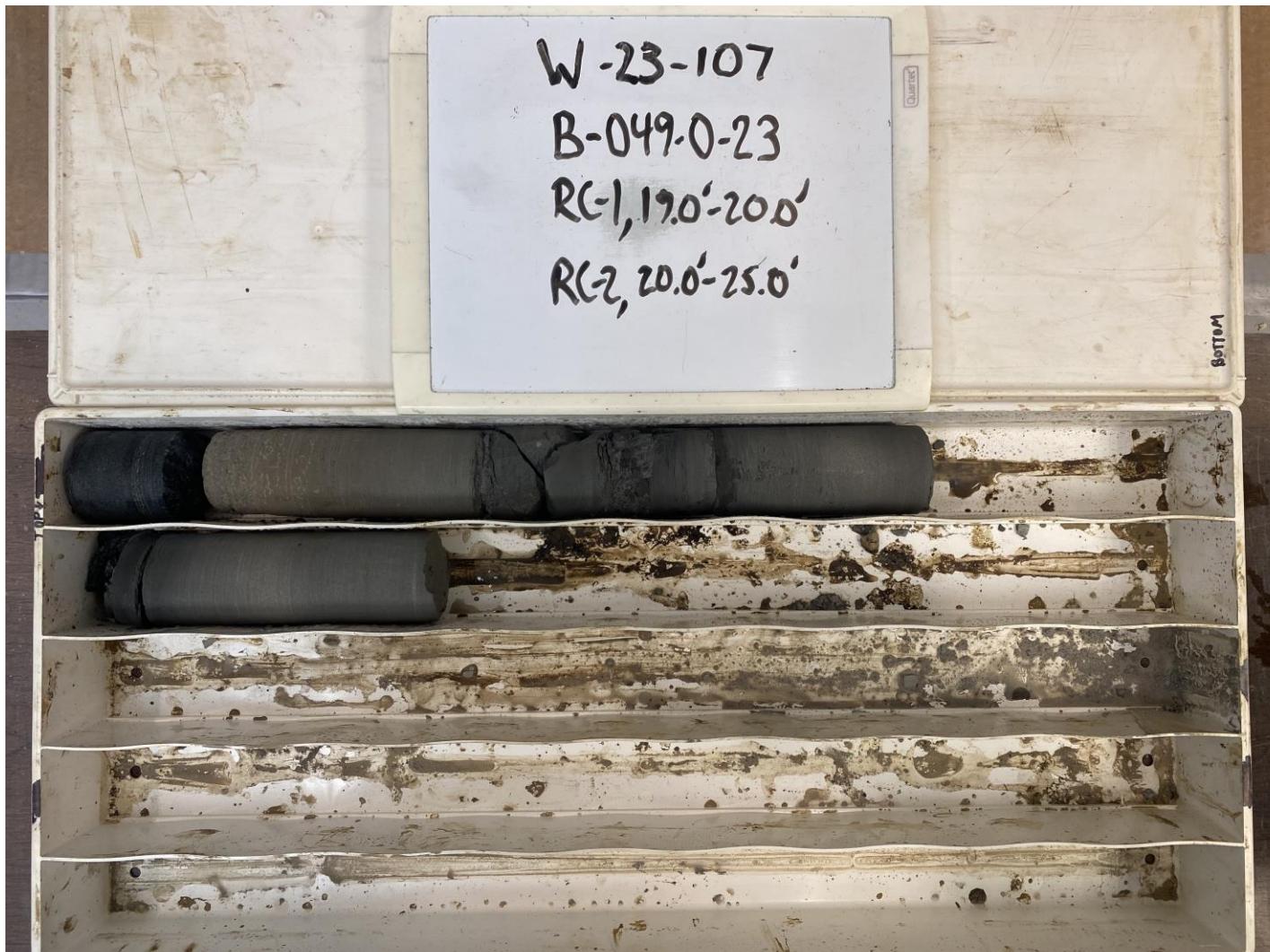
ABANDONMENT METHODS, MATERIALS, QUANTITIES: BACKFILLED WITH 50 LBS. BENTONITE CHIPS AND SOIL CUTTINGS. .

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/10/23 END: 11/10/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 1514+10 / 0' ALIGNMENT: CL WALL 15 ELEVATION: 1038.9 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090327, -82.806756	EXPLORATION ID <b>B-049-0-23</b>
				PAGE 1 OF 1

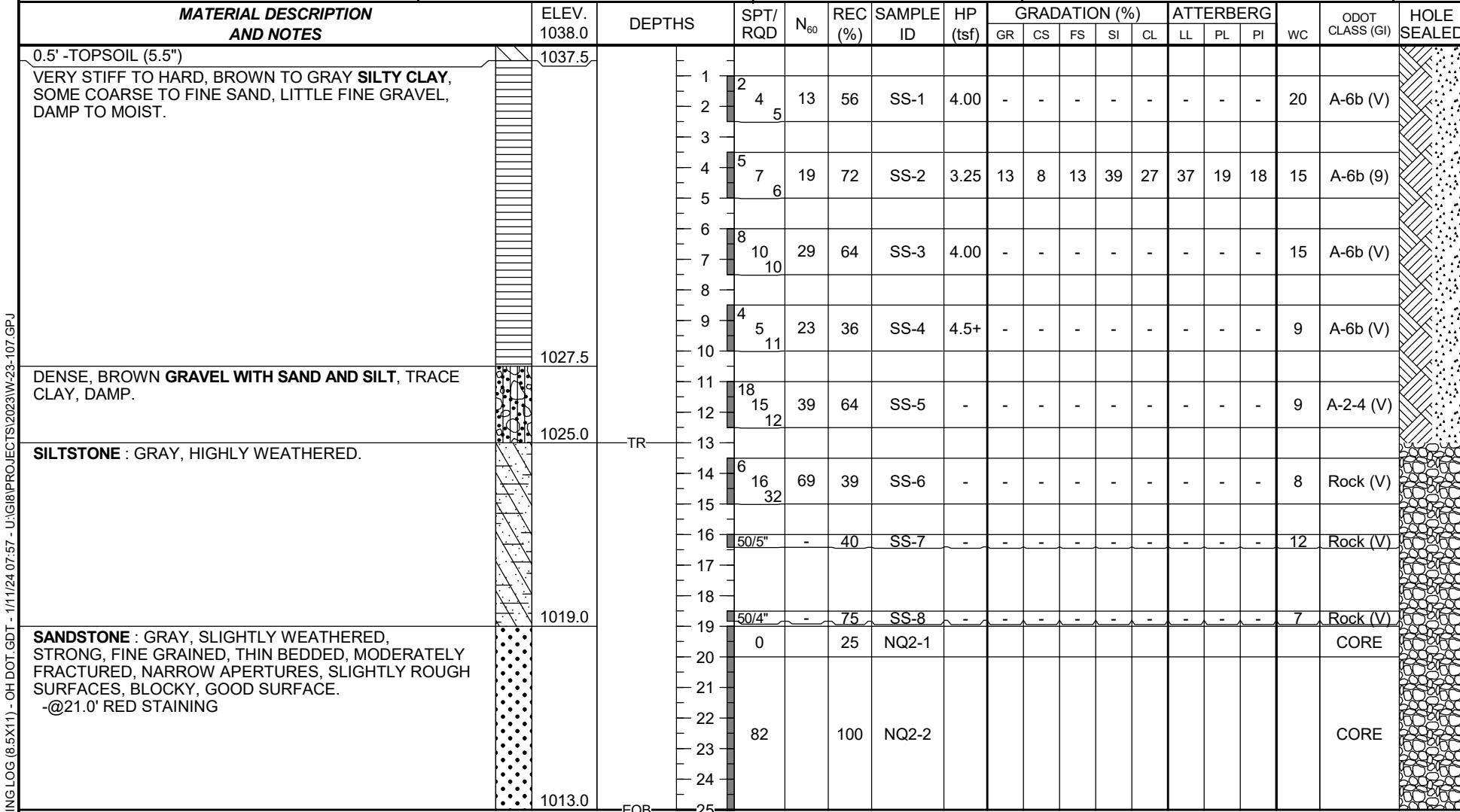


NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 17.1'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

<b>Project Name:</b> FRA-161-15.80		<b>Location:</b> Franklin County, Ohio
<b>Photo No.</b> <b>15</b>		
<b>Boring:</b> B-049-0-23		
RC-1: 19.0-20.0' REC (%):0 RQD (%):0		
RC-2: 20.0-25.0' REC (%):42 RQD (%):28		

 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/13/23 END: 11/13/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 1516+10 / 0' ALIGNMENT: CL WALL 15 ELEVATION: 1038.0 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090286, -82.806054	EXPLORATION ID <b>B-050-0-23</b>
				PAGE 1 OF 1



NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 13.0'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
**16**

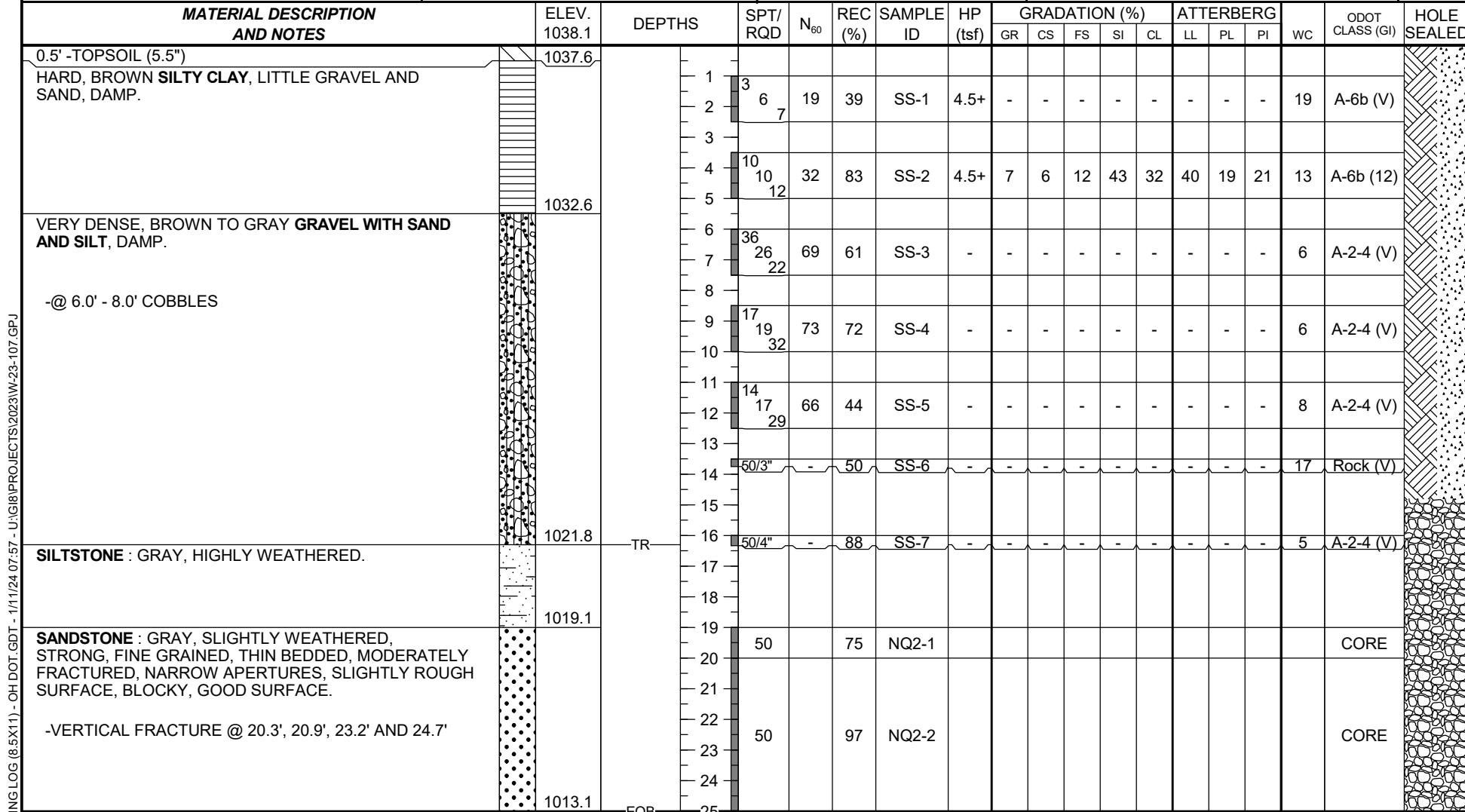
**Boring:**  
B-050-0-23

RC-1: 19.0-20.0'  
REC (%):0  
RQD (%):25

RC-2: 20.0-25.0'  
REC (%):100  
RQD (%):82



 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/13/23 END: 11/13/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 1519+10.6 / 8.77' LT ALIGNMENT: CL WALL 15 ELEVATION: 1038.1 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090226, -82.805330	EXPLORATION ID <b>B-051-0-23</b>
				PAGE 1 OF 1



**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
**17**

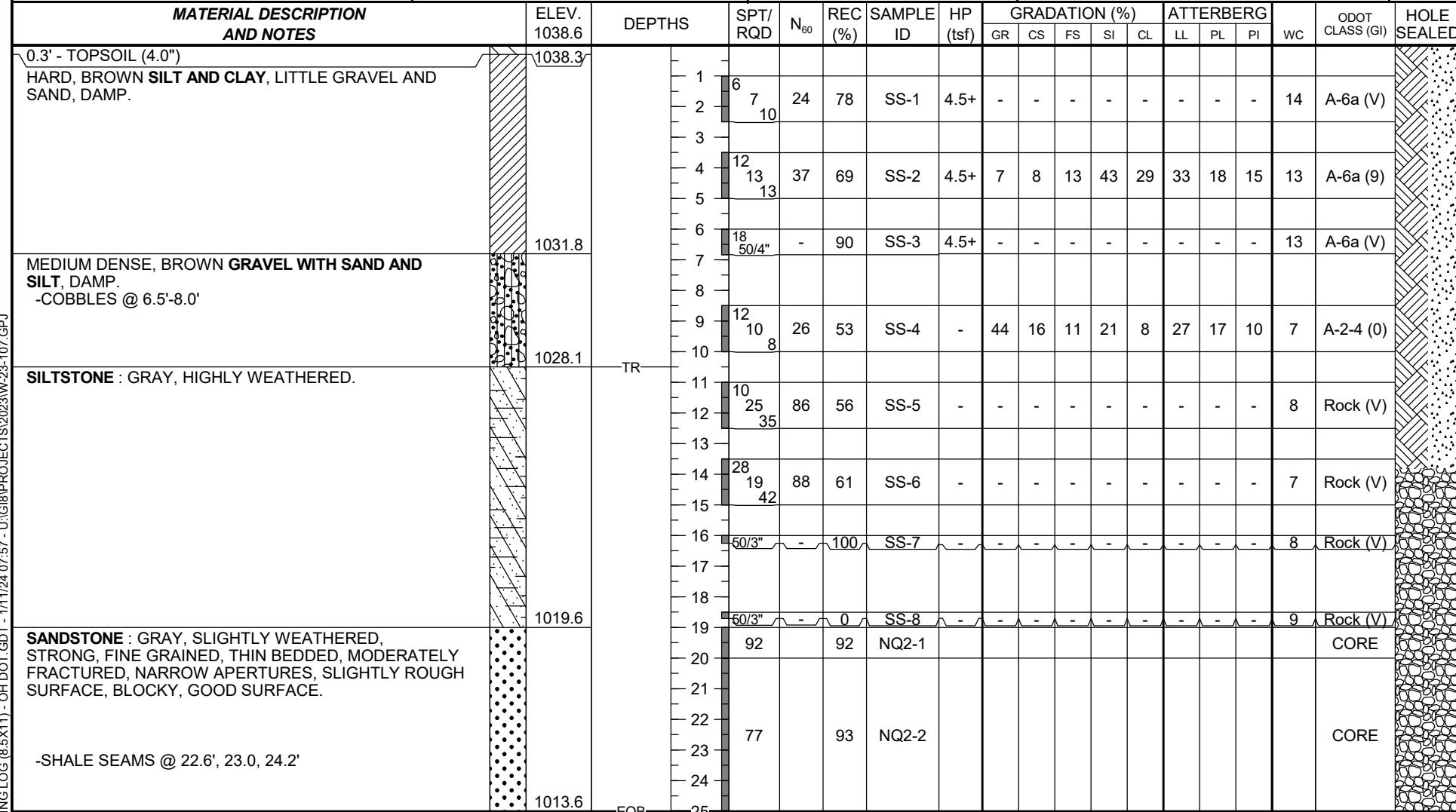
**Boring:**  
B-051-0-23

RC-1: 19.0-20.0'  
REC (%):75  
RQD (%):50

RC-2: 20.0-25.0'  
REC (%):97  
RQD (%):50



 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/13/23 END: 11/13/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 1520+41 / 0' ALIGNMENT: CL WALL 15 ELEVATION: 1038.6 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090130, -82.804859	EXPLORATION ID <b>B-052-0-23</b>
				PAGE 1 OF 1



NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 13.8'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

**Project Name:** FRA-161-15.80

**Location:**

Franklin County, Ohio

**Photo No.**  
**18**

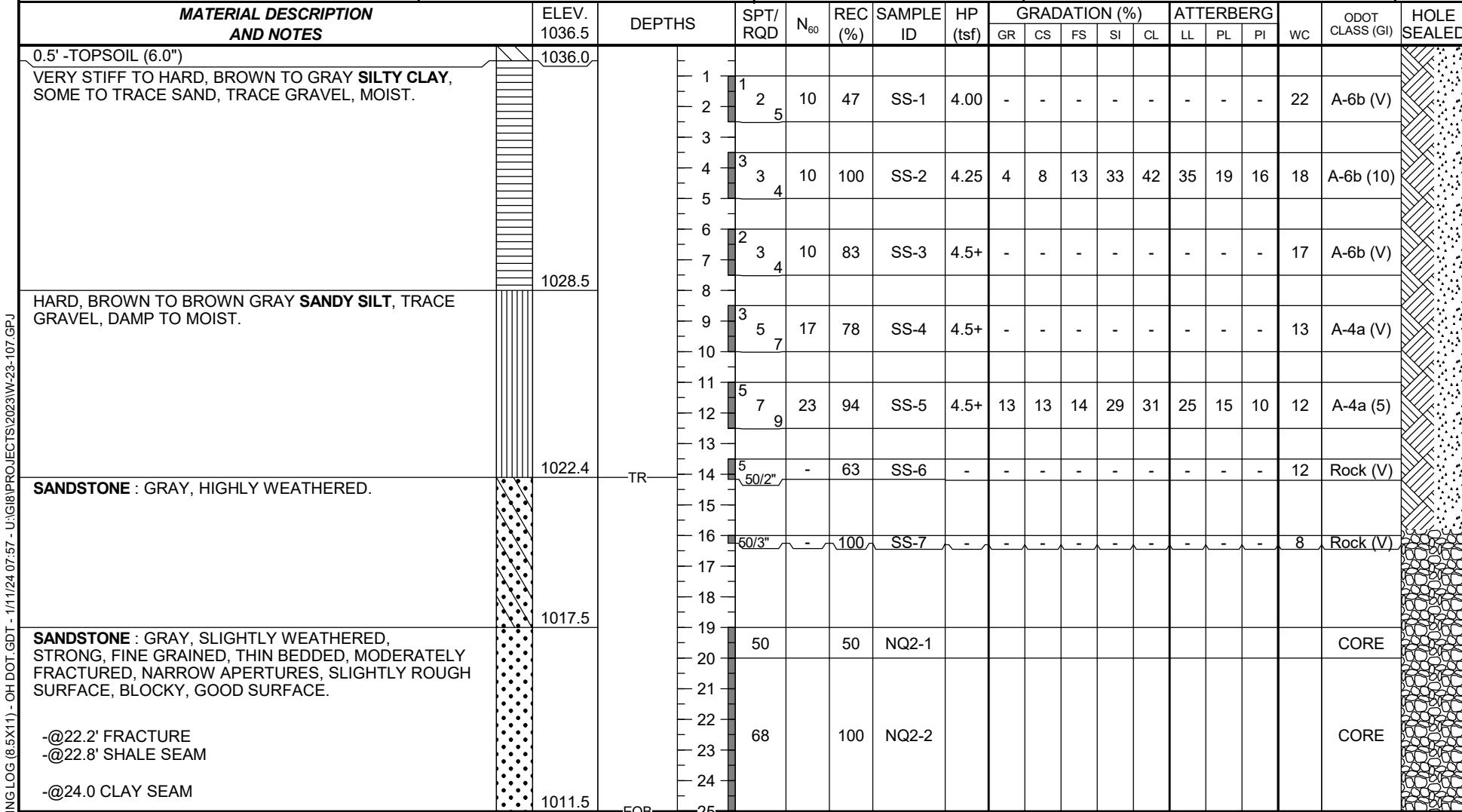
**Boring:**  
B-052-0-23

RC-1: 19.0-20.0'  
REC (%):92  
RQD (%):92

RC-2: 20.0-25.0'  
REC (%):93  
RQD (%):77

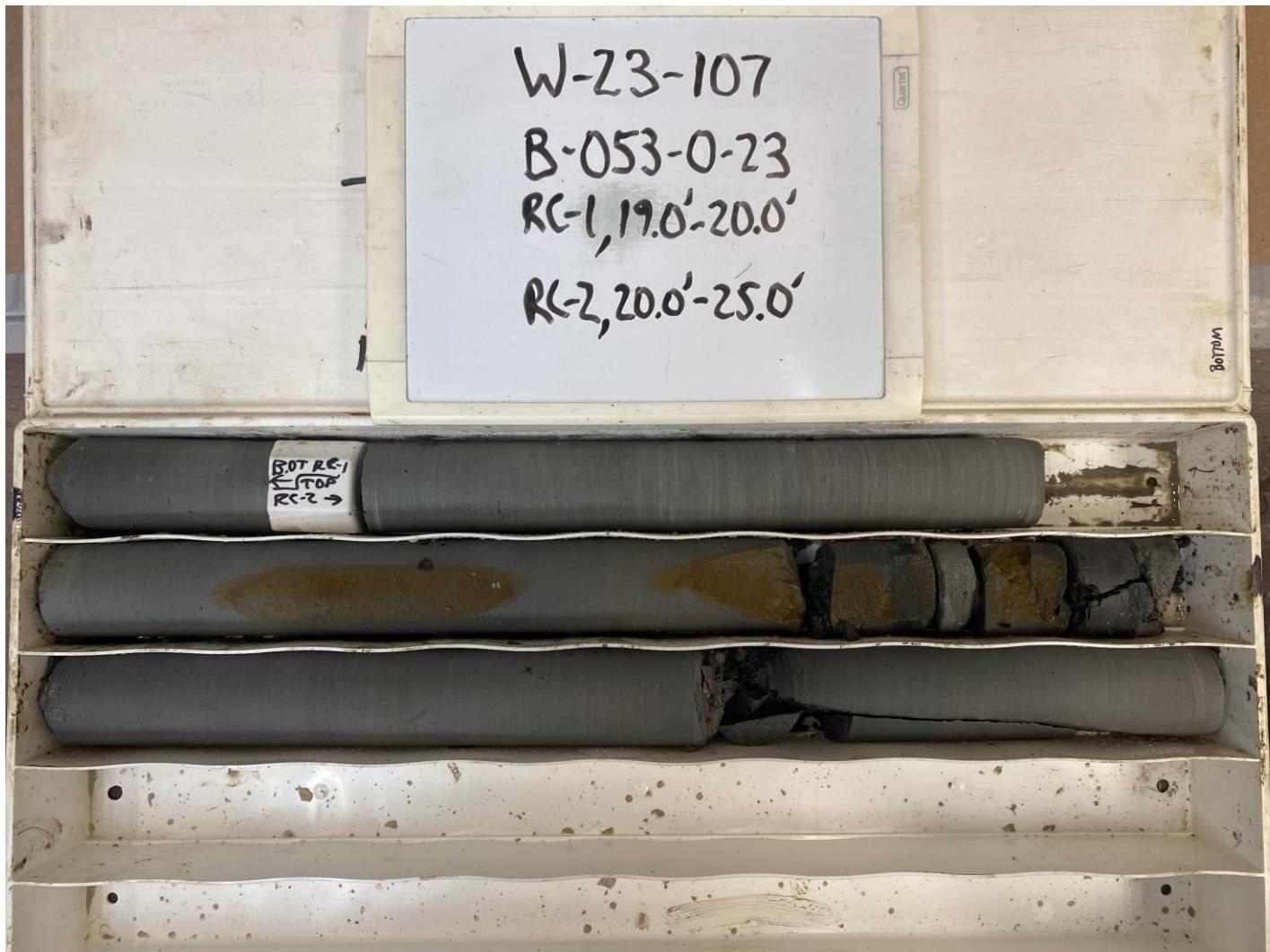


 <p>PROJECT: FRA-161-15.80 TYPE: NOISE WALLS PID: 117607 SFN: NA START: 11/14/23 END: 11/14/23</p>	DRILLING FIRM / OPERATOR: RII / TG SAMPLING FIRM / LOGGER: RII / MJ DRILLING METHOD: 3.25" HSA / NQ2 SAMPLING METHOD: SPT / NQ2	DRILL RIG: DIEDRICH D-50 (# 313) HAMMER: AUTOMATIC CALIBRATION DATE: 3/21/22 ENERGY RATIO (%): 86.4	STATION / OFFSET: 1522+26 / 0' ALIGNMENT: CL WALL 15 ELEVATION: 1036.5 (MSL) EOB: 25.0 ft. LAT / LONG: 40.090039, -82.804245	EXPLORATION ID <b>B-053-0-23</b>
				PAGE 1 OF 1



NOTES: GROUNDWATER NOT MEASURED UPON COMPLETION DUE TO INFLUENCE OF CORE WATER; CAVE-IN DEPTH @ 15.8'

ABANDONMENT METHODS, MATERIALS, QUANTITIES: PUMPED 47 LBS CEMENT, 25 LBS BENTONITE POWDER AND 40 GAL WATER .

<b>Project Name:</b> FRA-161-15.80		<b>Location:</b> Franklin County, Ohio
<b>Photo No.</b> <b>19</b>		
<b>Boring:</b> B-053-0-23		<p>W-23-107      B-053-0-23      RC-1, 19.0'-20.0'      RC-2, 20.0'-25.0'</p> 
RC-1: 19.0-20.0' REC (%):50 RQD (%):50		
RC-2: 20.0-25.0' REC (%):100 RQD (%):68		

**APPENDIX V**  
**LABORATORY TEST RESULTS**



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## Unconfined Compressive Strength of Intact Rock Core Specimens (ASTM D 7012-14)

Project: FRA-161-15.80

Project No.: W-23-107

Date of Testing: 1/8/2024

Test Performed by: KL/EM

Rock Description: Gray Sandstone

Rock Formation:

Boring No.: B-001-0-23

Sample No.: RC-2

Depth (ft): 14.0' feet

Moisture condition: As received

Sample Mass: 470.86 grams

Testing Temperature: 23 °C

Rate of Loading: 62.1 lbs/sec

Testing Time: 221 sec

(Rate 2-15 min.)

Average Length: 4.030 in

Average Diameter: 1.993 in

Length to diameter ratio: 2.022

Cross Sectional Area: 3.120 in<sup>2</sup>

Volume: 0.0073 ft<sup>3</sup>

Unit Weight (sample specimen)\*: 142.68 lbs/ft<sup>3</sup>

Failure Load: 13,727 lbs

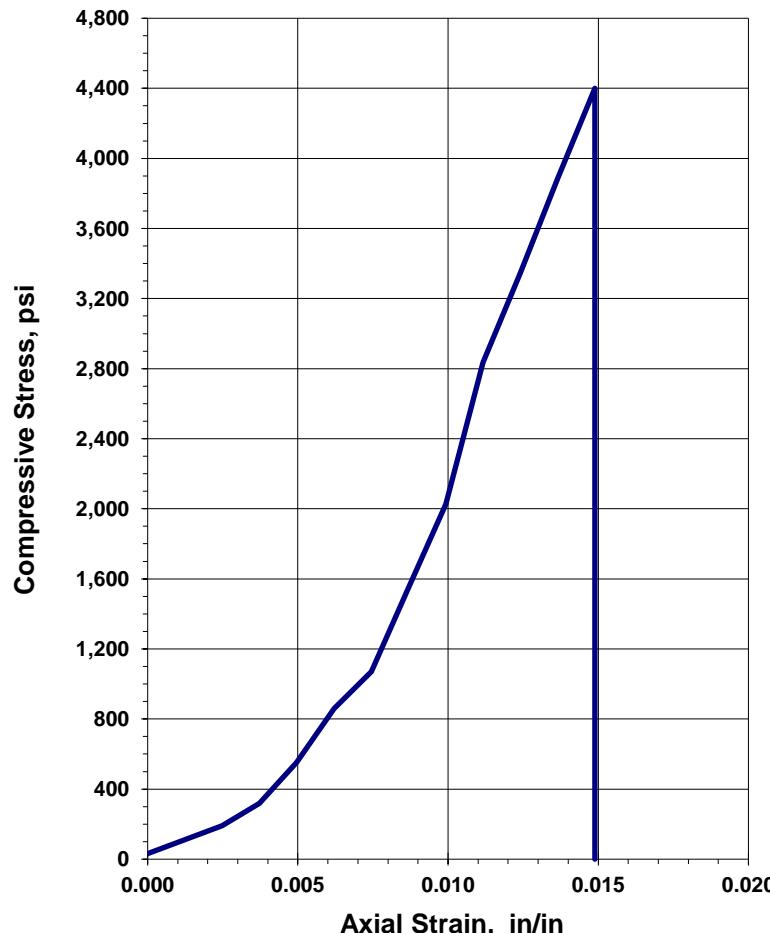
Axial Strain at Failure: 0.0149 in/in

Compressive Strength: 4,400 psi

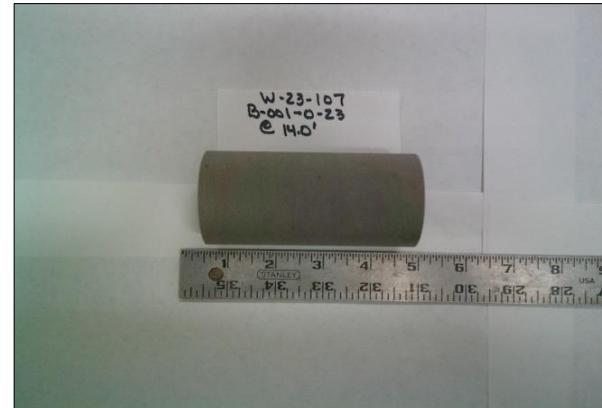
Sample Preparation: Per ASTM D4543

\*Actual test sample used for unit weight prior to testing.

### Unconfined Compression Test



### Before Testing



### After Failure



REMARKS:



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## Unconfined Compressive Strength of Intact Rock Core Specimens

(ASTM D 7012-14)

Project: FRA-161-15.80

Project No.: W-23-107

Date of Testing: 1/8/2024

Test Performed by: KL/EM

Rock Description: Gray Sandstone

Rock Formation: \_\_\_\_\_

Boring No.: B-003-0-23

Sample No.: RC-2

Depth (ft): 13.8' feet

Moisture condition: As received

Sample Mass: 480.55 grams

Testing Temperature: 23 °C

Rate of Loading: 75.1 lbs/sec

Testing Time: 287 sec  
(Rate 2-15 min)

Average Length: 4.028 in

Average Diameter: 1.995 in

Length to diameter ratio: 2.019

Cross Sectional Area: 3.126 in<sup>2</sup>

Volume: 0.0073 ft<sup>3</sup>

Unit Weight (sample specimen)\*: 145.39 lbs/ft<sup>3</sup>

Failure Load: 21,542 lbs

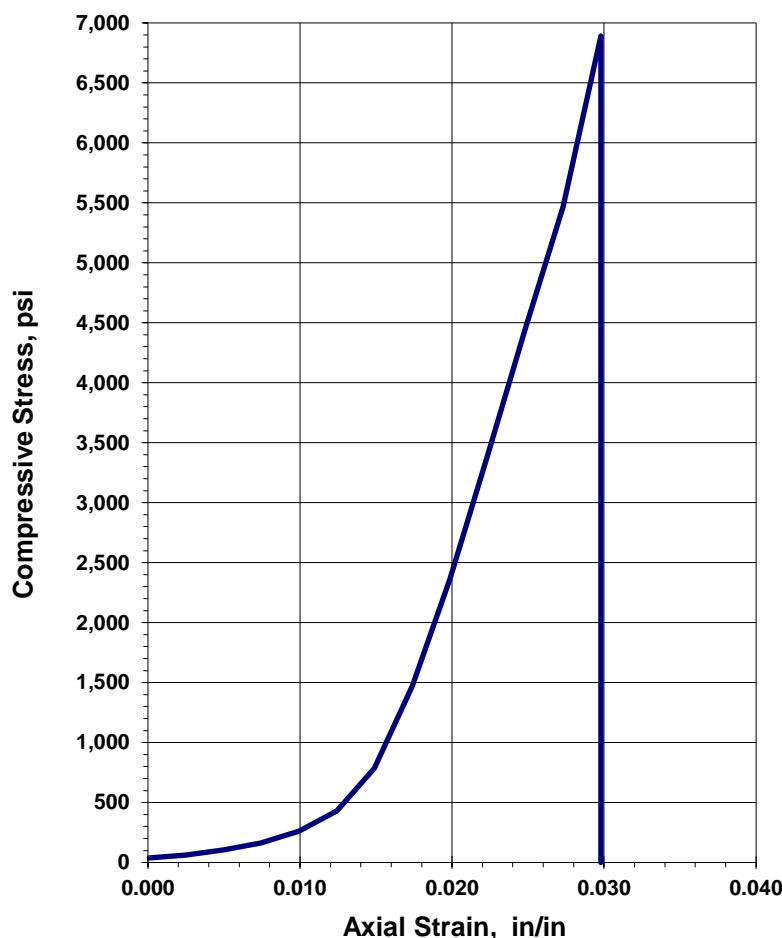
Axial Strain at Failure: 0.0298 in/in

Compressive Strength: 6,891 psi

Sample Preparation: Per ASTM D4543

\*Actual test sample used for unit weight prior to testing.

### Unconfined Compression Test



### Before Testing



### After Failure



REMARKS: \_\_\_\_\_



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## Unconfined Compressive Strength of Intact Rock Core Specimens

(ASTM D 7012-14)

Project: FRA-161-15.80

Project No.: W-23-107

Date of Testing: 1/8/2024

Test Performed by: KL/EM

Rock Description: Gray Sandstone

Rock Formation: \_\_\_\_\_

Boring No.: B-043-0-23

Sample No.: RC-2

Depth (ft): 21.00 feet

Moisture condition: As received

Sample Mass: 460.53 grams

Testing Temperature: 23 °C

Rate of Loading: 87.2 lbs/sec

Testing Time: 221 sec  
(Rate 2-15 min)

Average Length: 4.000 in

Average Diameter: 1.988 in

Length to diameter ratio: 2.012

Cross Sectional Area: 3.104 in<sup>2</sup>

Volume: 0.0072 ft<sup>3</sup>

Unit Weight (sample specimen)\*: 141.30 lbs/ft<sup>3</sup>

Failure Load: 19,269 lbs

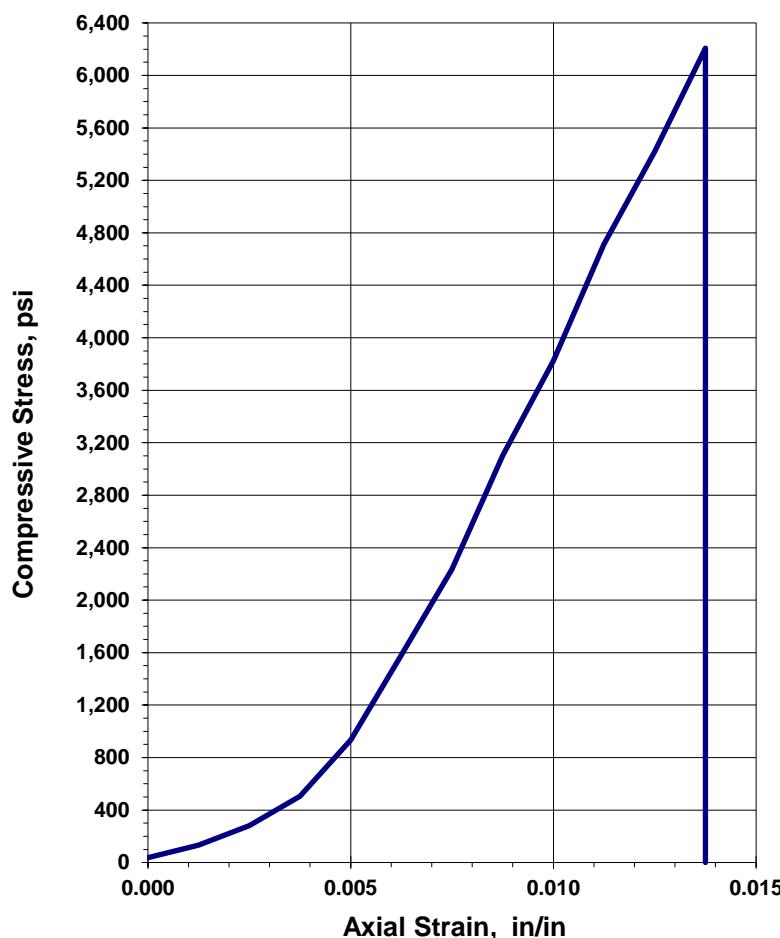
Axial Strain at Failure: 0.0138 in/in

Compressive Strength: 6,208 psi

Sample Preparation: Per ASTM D4543

\*Actual test sample used for unit weight prior to testing.

### Unconfined Compression Test



### Before Testing



### After Failure



REMARKS: \_\_\_\_\_



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## Unconfined Compressive Strength

### of Intact Rock Core Specimens

#### (ASTM D 7012-14)

Project: FRA-161-15.80

Project No.: W-23-107

Date of Testing: 1/8/2024

Test Performed by: KL/EM

Rock Description: Gray Sandstone

Rock Formation: \_\_\_\_\_

Boring No.: B-046-0-23

Average Length: 3.992 in

Sample No.: RC-2

Average Diameter: 1.995 in

Depth (ft): 22.0' feet

Length to diameter ratio: 2.001

Moisture condition: As received

Cross Sectional Area: 3.126 in<sup>2</sup>

Sample Mass: 519.17 grams

Volume: 0.0072 ft<sup>3</sup>

Testing Temperature: 23 °C

Unit Weight (sample specimen)\*: 158.49 lbs/ft<sup>3</sup>

Rate of Loading: 101.9 lbs/sec

Failure Load: 24,655 lbs

Testing Time: 242 sec  
(Rate 2-15 min)

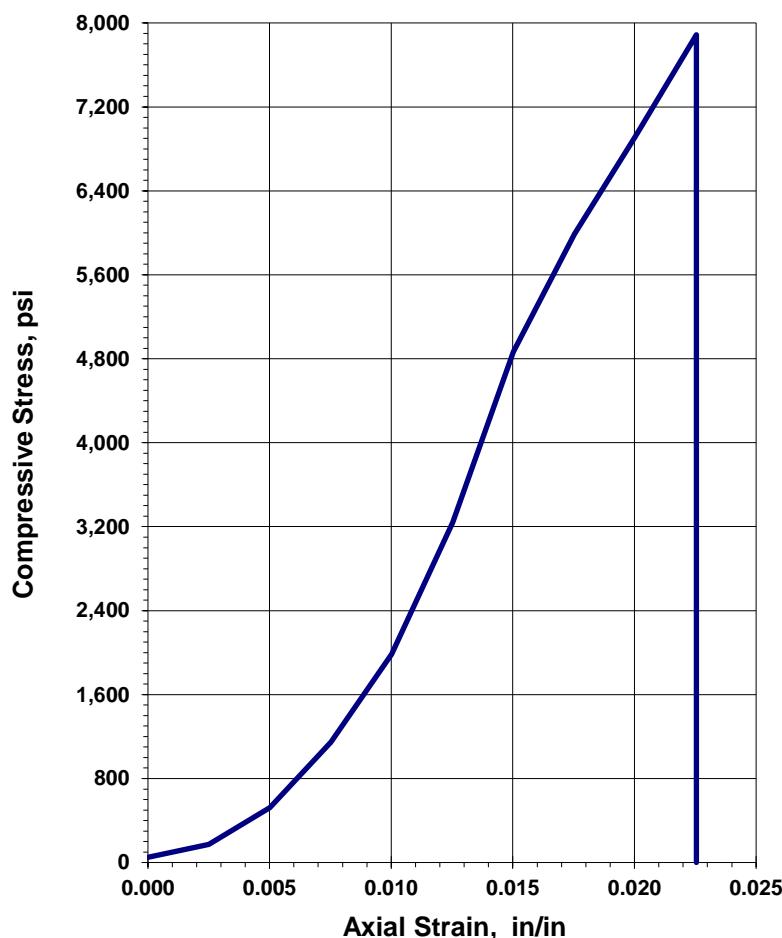
Axial Strain at Failure: 0.0225 in/in

Compressive Strength: 7,887 psi

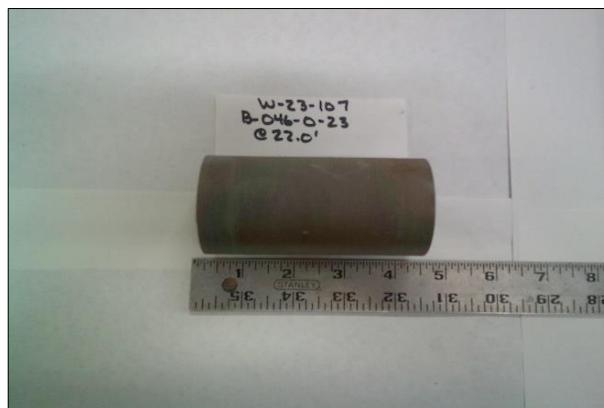
Sample Preparation: Per ASTM D4543

\*Actual test sample used for unit weight prior to testing.

#### Unconfined Compression Test



#### Before Testing



#### After Failure



REMARKS: \_\_\_\_\_



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## Unconfined Compressive Strength of Intact Rock Core Specimens

(ASTM D 7012-14)

Project: FRA-161-15.80

Project No.: W-23-107

Date of Testing: 1/8/2024

Test Performed by: KL/EM

Rock Description: Gray Sandstone

Rock Formation: \_\_\_\_\_

Boring No.: B-050-0-23

Sample No.: RC-2

Depth (ft): 21.0' feet

Moisture condition: As received

Sample Mass: 455.36 grams

Testing Temperature: 23 °C

Rate of Loading: 108.5 lbs/sec

Testing Time: 242 sec

(Rate 2-15 min)

Average Length: 3.988 in

Average Diameter: 1.985 in

Length to diameter ratio: 2.009

Cross Sectional Area: 3.095 in<sup>2</sup>

Volume: 0.0071 ft<sup>3</sup>

Unit Weight (sample specimen)\*: 140.56 lbs/ft<sup>3</sup>

Failure Load: 26,255 lbs

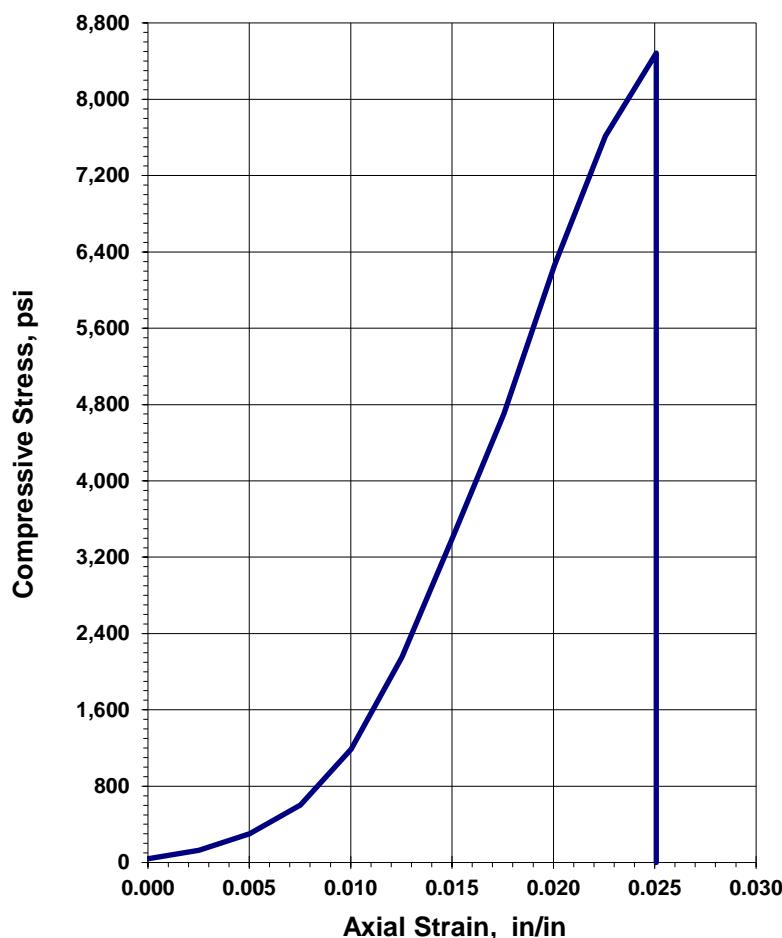
Axial Strain at Failure: 0.0251 in/in

Compressive Strength: 8,484 psi

Sample Preparation: Per ASTM D4543

\*Actual test sample used for unit weight prior to testing.

### Unconfined Compression Test



### Before Testing



### After Failure



REMARKS: \_\_\_\_\_



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## Unconfined Compressive Strength of Intact Rock Core Specimens

(ASTM D 7012-14)

Project: FRA-161-15.80

Project No.: W-23-107

Date of Testing: 1/8/2024

Test Performed by: KL/EM

Rock Description: Gray Sandstone

Rock Formation: \_\_\_\_\_

Boring No.: B-052-0-23

Sample No.: RC-2

Depth (ft): 21.20 feet

Moisture condition: As received

Sample Mass: 505.98 grams

Testing Temperature: 23 °C

Rate of Loading: 112.4 lbs/sec

Testing Time: 234 sec  
(Rate 2-15 min)

Average Length: 4.024 in

Average Diameter: 1.993 in

Length to diameter ratio: 2.019

Cross Sectional Area: 3.120 in<sup>2</sup>

Volume: 0.0073 ft<sup>3</sup>

Unit Weight (sample specimen)\*: 153.55 lbs/ft<sup>3</sup>

Failure Load: 26,295 lbs

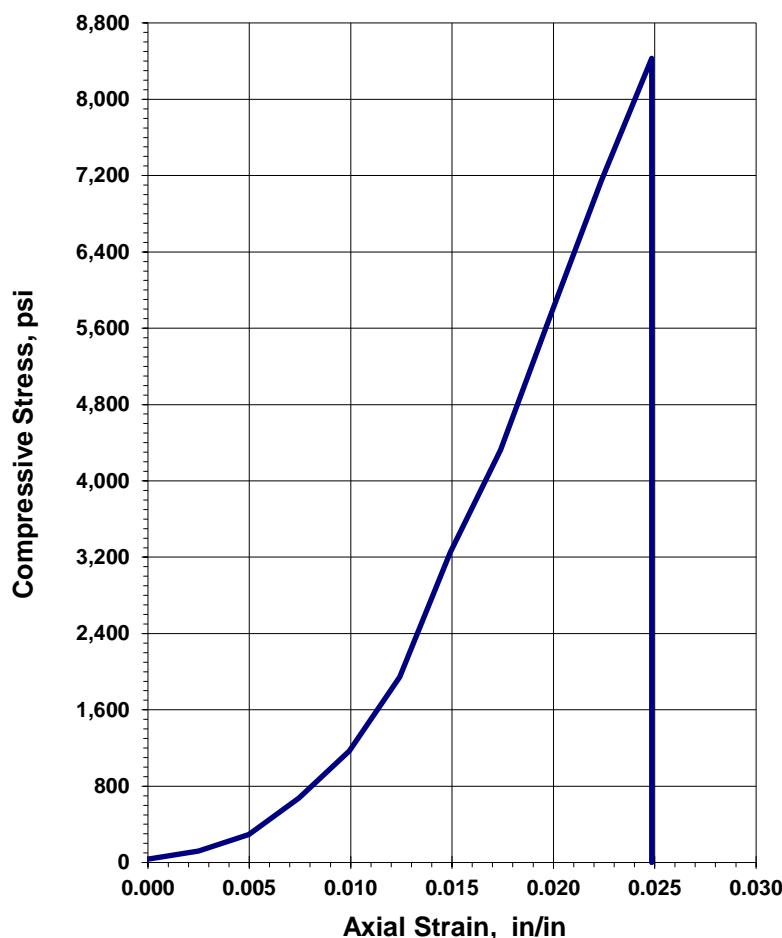
Axial Strain at Failure: 0.0249 in/in

Compressive Strength: 8,429 psi

Sample Preparation: Per ASTM D4543

\*Actual test sample used for unit weight prior to testing.

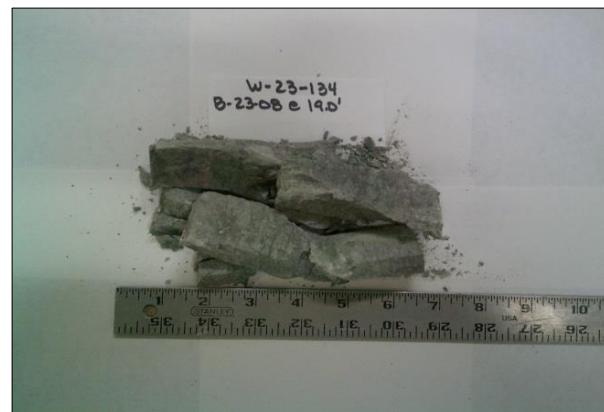
### Unconfined Compression Test



### Before Testing



### After Failure



REMARKS: \_\_\_\_\_



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*Engineering Consultants*

**Point Load Strength Index  
of Rock Specimens  
(ASTM D 5731-08)**

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Project: FRA-161-15.80  
Project No.: W-23-107  
Date of Testing: 1/8/2024  
Test Performed by: EM/KL

Rock Description: Gray Shale

Boring No.: B-23-0-23  
Station / Offset: RC-3  
Sample No. / Depth: 21.5'-23.5'

Test Apparatus: Forney-LA 0080  
Serial Number: A125/AZ/0014  
Date of Calibration: 4/25/2023

Sample No.	Test Type	Depth (ft)	Width (mm)	Diameter (mm)	Load (N)	$D_e^2$ (mm <sup>2</sup> )	$D_e$ (mm)	F	Is (MPa)	Is <sub>(50)</sub> (MPa)	$\sigma_c$ (MPa)
1	a <sup>⊥</sup>	21.5-23.5	49.7	21.1	503	1,336	36.5	0.87	0.38	0.33	4.52
2	a <sup>⊥</sup>	21.5-23.5	49.6	25.8	783	1,631	40.4	0.91	0.48	0.44	5.76
3	a <sup>⊥</sup>	21.5-23.5	49.7	23.1	525	1,463	38.3	0.89	0.36	0.32	4.31
4	a <sup>⊥</sup>	21.5-23.5	49.7	28.5	814	1,802	42.5	0.93	0.45	0.42	5.42
5	a <sup>⊥</sup>	21.5-23.5	49.7	30.0	854	1,895	43.5	0.94	0.45	0.42	5.41
6	a <sup>⊥</sup>	21.5-23.5	49.7	25.1	916	1,589	39.9	0.90	0.58	0.52	6.92
7	a <sup>⊥</sup>	21.5-23.5	49.7	24.6	816	1,555	39.4	0.90	0.52	0.47	6.30
8	a <sup>⊥</sup>	21.5-23.5	49.7	22.6	798	1,429	37.8	0.88	0.56	0.49	6.70
9	a <sup>⊥</sup>	21.5-23.5	49.7	21.5	789	1,361	36.9	0.87	0.58	0.51	6.96
10	a <sup>⊥</sup>	21.5-23.5	49.7	22.5	801	1,427	37.8	0.88	0.56	0.49	6.73

## STATISTICS

Mean Is <sub>(50)</sub> <sup>⊥</sup>	0.44 MPa (64 psi)
Mean Is <sub>(50)</sub> <sup>  </sup>	
la <sub>(50)</sub>	

### Specific Specimen Shape:

### Estimated Unaxial Compression, $\sigma_c = K * Is$

d = diametrical

K = 12

\*Per Section 206.1.3 of 2011 ODOT  
Rock Slope Design Guide

a = axial

b = block

i = irregular lump

Mean  $\sigma_c$  = 5.90 MPa (0.856 psi)

⊥ = perpendicular to bedding plane

|| = parallel to bedding plane

Remarks: \_\_\_\_\_



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## Point Load Strength Index of Rock Specimens (ASTM D 5731-08)

Project: FRA-161-15.80

Project No.: W-23-107

Date of Testing: 1/8/2024

Test Performed by: EM/KL

Rock Description: Gray Shale

Boring No.: B-39-0-23

Station / Offset: RC-2

Sample No. / Depth: 15.0-20.0

Test Apparatus: Forney-LA 0080

Serial Number: A125/AZ/0014

Date of Calibration: 4/25/2023

Sample No.	Test Type	Depth (ft)	Width (mm)	Diameter (mm)	Load (N)	$D_e^2$ (mm <sup>2</sup> )	$D_e$ (mm)	F	$Is$ (MPa)	$Is_{(50)}$ (MPa)	$\sigma_c$ (MPa)
1	a <sup>⊥</sup>	17.5-18.5	49.9	21.7	50	1,381	37.2	0.88	0.04	0.03	0.43
2	a <sup>⊥</sup>	17.5-18.5	49.5	24.4	45	1,539	39.2	0.90	0.03	0.03	0.35
3	a <sup>⊥</sup>	17.5-18.5	50.5	20.4	40	1,309	36.2	0.86	0.03	0.03	0.37
4	a <sup>⊥</sup>	17.5-18.5	50.6	23.9	48	1,538	39.2	0.90	0.03	0.03	0.37
5	a <sup>⊥</sup>	17.5-18.5	50.6	22.3	49	1,440	38.0	0.88	0.03	0.03	0.41
6	a <sup>⊥</sup>	17.5-18.5	50.6	21.1	49	1,362	36.9	0.87	0.04	0.03	0.43
7	a <sup>⊥</sup>	17.5-18.5	50.6	22.6	53	1,455	38.1	0.89	0.04	0.03	0.44
8	a <sup>⊥</sup>	17.5-18.5	50.6	22.6	48	1,456	38.2	0.89	0.03	0.03	0.40
9	a <sup>⊥</sup>	17.5-18.5	50.6	35.0	51	2,255	47.5	0.98	0.02	0.02	0.27
10	a <sup>⊥</sup>	17.5-18.5	50.6	22.2	52	1,429	37.8	0.88	0.04	0.03	0.44

### STATISTICS

Mean $Is_{(50)}$ <sup>⊥</sup>	0.03 MPa (4 psi)
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Mean $Is_{(50)}$ <sup>  </sup>
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$la_{(50)}$
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Specific Specimen Shape:

Estimated Unaxial Compression,  $\sigma_c = K * Is$

d = diametrical

K = 12

\*Per Section 206.1.3 of 2011 ODOT  
Rock Slope Design Guide

a = axial

b = block

i = irregular lump

Mean  $\sigma_c$  = 0.39 MPa (0.057 psi)

⊥ = perpendicular to bedding plane

|| = parallel to bedding plane

Remarks: \_\_\_\_\_

**APPENDIX VI**

**CALCULATIONS – NOISE BARRIER  
FOUNDATION DEPTHS**

**OHIO DEPARTMENT OF TRANSPORTATION****OFFICE OF GEOTECHNICAL ENGINEERING****Noise Wall Design****FRA-161-15.80  
117607****Noise Wall Along SR 161 Sta. 300+00.00 to 305+76.00****Noise Wall 3****Rii**

**Prepared By:** Dan Hayes, E.I.  
**Date prepared:** Thursday, January 18, 2024

**Checked By:** Daniel E. Karch, P.E.  
**Date Checked:** Thursday, January 18, 2024

**No. of Borings:****4**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
300+00.00	1	14.00	24.00	965.50
300+24.00	2	14.00	24.00	965.50
300+48.00	3	14.00	24.00	966.50
300+72.00	4	14.00	24.00	966.50
300+96.00	5	14.00	24.00	966.50
301+20.00	6	14.00	24.00	966.50
301+44.00	7	14.00	24.00	967.00
301+68.00	8	14.00	24.00	967.00
301+92.00	9	14.00	24.00	967.00
302+16.00	10	14.00	24.00	967.50
302+40.00	11	14.00	24.00	967.50
302+64.00	12	14.00	24.00	967.50
302+88.00	13	14.00	24.00	968.00
303+12.00	14	14.00	24.00	968.00
303+36.00	15	14.00	24.00	968.50
303+60.00	16	14.00	24.00	968.50
303+84.00	17	14.00	24.00	968.50
304+08.00	18	14.00	24.00	968.50
304+32.00	19	14.00	24.00	968.50
304+56.00	20	14.00	24.00	968.50
304+80.00	21	14.00	24.00	968.50
305+04.00	22	14.00	24.00	968.50
305+28.00	23	14.00	24.00	968.50
305+52.00	24	14.00	24.00	968.50
305+76.00	25	14.00	24.00	968.50

**Noise Wall ID: Noise Wall 3**

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev. (ft)	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height (ft)	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)
B-001-0-23	300+00.00	301+00.00	966.30	965.50	966.30	962.00		24	14.00	3.0   3:1	300+00.00	300+96.00	1	5	7.00	958.50
B-002-0-23	302+00.00	303+00.00	968.10	967.00	968.10	963.50		24	14.00	4.0   4:1	301+20.00	302+88.00	6	13	8.50	958.50
B-003-0-23	304+00.00	304+88.00	969.10	968.50	969.10	964.40		24	14.00	7.0   5:1	303+12.00	304+80.00	14	21	7.00	961.50
B-004-0-23	305+76.00	305+76.00	969.20	968.50	969.20	963.70		24	14.00	0.0   Level	305+04.00	305+76.00	22	25	6.50	962.00

**OHIO DEPARTMENT OF TRANSPORTATION****OFFICE OF GEOTECHNICAL ENGINEERING****Noise Wall Design****FRA-161-15.80  
117607****Noise Wall Along SR 161 Sta. 600+00.00 to 605+28.00****Noise Wall 6****Rii**

**Prepared By:** Dan Hayes, E.I.  
**Date prepared:** Thursday, January 18, 2024

**Checked By:** 1/18/2024  
**Date Checked:** Thursday, January 18, 2024

**No. of Borings:** **4**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
600+00.00	1	14.00	24.00	960.50
600+24.00	2	14.00	24.00	960.50
600+48.00	3	14.00	24.00	960.50
600+72.00	4	14.00	24.00	960.50
600+96.00	5	14.00	12.00	961.50
601+08.00	6	14.00	12.00	962.50
601+20.00	7	14.00	12.00	963.50
601+32.00	8	14.00	12.00	964.50
601+44.00	9	14.00	12.00	965.50
601+56.00	10	14.00	12.00	966.00
601+68.00	11	14.00	24.00	966.50
601+92.00	12	14.00	24.00	967.00
602+16.00	13	14.00	24.00	968.00
602+40.00	14	14.00	24.00	968.00
602+64.00	15	14.00	24.00	968.00
602+88.00	16	14.00	24.00	968.50
603+12.00	17	14.00	24.00	968.50
603+36.00	18	14.00	24.00	968.50
603+60.00	19	14.00	24.00	968.50
603+84.00	20	14.00	24.00	968.50
604+08.00	21	14.00	24.00	968.50
604+32.00	22	14.00	24.00	968.50
604+56.00	23	14.00	24.00	969.00
604+80.00	24	14.00	24.00	969.00
605+04.00	25	14.00	24.00	969.00
605+28.00	26	14.00	24.00	969.00

**Boring Information and  
Design Recommendation**

FRA-161-15.80

PID: 117607

**Foundation Design**

**Noise Wall ID: Noise Wall 6**

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev. (ft)	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height (ft)	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)	
B-005-0-23	600+00.00	600+88.50	961.50	960.50	961.50			24	14.00	3.0   3:1	600+00.00	600+72.00		1	4	7.00	953.50
B-006-0-23	601+77.00	602+68.50	968.10	966.50	968.10			24	14.00	4.0   4:1	600+96.00	602+64.00		5	15	7.00	959.50
B-007-0-23	603+60.00	604+44.00	969.00	968.50	969.00			24	14.00	4.0   4:1	602+88.00	604+32.00		16	22	7.00	961.50
B-008-0-23	605+28.00	605+28.00	970.00	969.00	970.00			24	14.00	4.0   4:1	604+56.00	605+28.00		23	26	7.00	962.00

**OHIO DEPARTMENT OF TRANSPORTATION****OFFICE OF GEOTECHNICAL ENGINEERING****Noise Wall Design****FRA-161-15.80  
117607****Noise Wall Along SR 161 Sta. 800+00.00 to 823+48.00****Noise Wall 8****Rii**

**Prepared By:** Dan Hayes, E.I.  
**Date prepared:** Thursday, January 18, 2024

**Checked By:** Daniel E. Karch, P.E.  
**Date Checked:** Thursday, January 18, 2024

**No. of Borings:** **10**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
800+00.00	1	14.00	24.00	966.00
800+24.00	2	14.00	24.00	966.00
800+48.00	3	14.00	24.00	966.00
800+72.00	4	14.00	24.00	966.00
800+96.00	5	14.00	24.00	966.50
801+20.00	6	14.00	24.00	966.50
801+44.00	7	14.00	24.00	966.50
801+68.00	8	14.00	24.00	966.50
801+92.00	9	14.00	24.00	966.50
802+16.00	10	14.00	24.00	966.50
802+40.00	11	14.00	24.00	966.50
802+64.00	12	14.00	24.00	966.50
802+88.00	13	14.00	24.00	966.50
803+12.00	14	14.00	24.00	966.50
803+36.00	15	14.00	24.00	966.50
803+60.00	16	14.00	24.00	966.50
803+84.00	17	14.00	24.00	966.50
804+08.00	18	14.00	24.00	966.00
804+32.00	19	14.00	24.00	966.00
804+56.00	20	14.00	24.00	965.50
804+80.00	21	14.00	24.00	965.50
805+04.00	22	14.00	24.00	965.50
805+28.00	23	14.00	24.00	964.50
805+52.00	24	14.00	24.00	964.50
805+76.00	25	14.00	24.00	964.50
806+00.00	26	14.00	24.00	964.50
806+24.00	27	14.00	24.00	964.50
806+48.00	28	14.00	24.00	964.50
806+72.00	29	14.00	24.00	965.50
806+96.00	30	14.00	24.00	965.50
807+20.00	31	14.00	24.00	966.00
807+44.00	32	14.00	24.00	966.50

Noise Wall: Noise Wall 8

FRA-161-15.80  
PID: 117607

**Design Data Sheet**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
807+68.00	33	14.00	24.00	966.50
807+92.00	34	14.00	24.00	967.00

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
808+16.00	35	14.00	24.00	967.00
808+40.00	36	14.00	24.00	967.00
808+64.00	37	14.00	24.00	967.50
808+88.00	38	14.00	24.00	967.50
809+12.00	39	14.00	24.00	967.50
809+36.00	40	14.00	24.00	967.50
809+60.00	41	14.00	24.00	968.00
809+84.00	42	14.00	24.00	968.50
810+08.00	43	14.00	24.00	968.50
810+32.00	44	14.00	24.00	969.00
810+56.00	45	14.00	24.00	969.50
810+80.00	46	14.00	16.00	970.00
810+96.00	47	14.00	16.00	970.00
811+12.00	48	14.00	16.00	970.50
811+28.00	49	14.00	16.00	971.00
811+44.00	50	14.00	14.00	971.00
811+58.00	51	14.00	14.00	971.50
811+72.00	52	14.00	24.00	972.00
811+96.00	53	14.00	24.00	972.50
812+20.00	54	14.00	24.00	973.00
812+44.00	55	14.00	24.00	974.00
812+68.00	56	14.00	24.00	975.00
812+92.00	57	14.00	24.00	975.00
813+16.00	58	14.00	24.00	975.00
813+40.00	59	14.00	24.00	975.00
813+64.00	60	14.00	24.00	975.00
813+88.00	61	14.00	24.00	975.00
814+12.00	62	14.00	24.00	974.50
814+36.00	63	14.00	24.00	974.50
814+60.00	64	14.00	24.00	974.00
814+84.00	65	14.00	24.00	974.00
815+08.00	66	14.00	24.00	974.00

Noise Wall: Noise Wall 8

FRA-161-15.80  
PID: 117607

**Design Data Sheet**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
815+32.00	67	14.00	24.00	974.00
815+56.00	68	14.00	24.00	974.00

<b>STA. (FT)</b>	<b>Post No.</b>	<b>Barrier Height (FT)</b>	<b>Post Spacing (FT)</b>	<b>Top of Shaft Elev. (MSL FT)</b>
815+80.00	69	14.00	24.00	974.00
816+04.00	70	14.00	24.00	974.00
816+28.00	71	14.00	24.00	973.50
816+52.00	72	14.00	24.00	973.50
816+76.00	73	14.00	24.00	973.50
817+00.00	74	14.00	24.00	973.50
817+24.00	75	14.00	24.00	973.50
817+48.00	76	14.00	24.00	973.50
817+72.00	77	14.00	24.00	973.50
817+96.00	78	14.00	12.00	973.50
818+08.00	79	14.00	24.00	973.50

**Boring Information and  
Design Recommendation**

FRA-161-15.80

PID: 117607

**Foundation Design**

**Noise Wall ID: Noise Wall 8**

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev. (ft)	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height (ft)	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)	
B-012-0-23	800+72.00	801+72.00	967.10	966.00	967.10			24	14.00	0.0	Level	800+00.00	801+68.00	1	8	6.50	959.50
B-013-0-23	802+72.00	803+72.00	967.40	966.50	967.40			24	14.00	0.0	Level	801+92.00	803+60.00	9	16	6.50	960.00
B-014-0-23	804+72.00	805+72.00	966.40	965.50	966.40			24	14.00	0.0	Level	803+84.00	805+52.00	17	24	6.50	959.00
B-015-0-23	806+72.00	807+72.00	966.50	965.50	966.50			24	14.00	0.0	Level	805+76.00	807+68.00	25	33	6.50	959.00
B-016-0-23	808+72.00	809+72.00	968.40	967.50	968.40			24	14.00	0.0	Level	807+92.00	809+60.00	34	41	6.50	961.00
B-017-0-23	810+72.00	811+74.00	970.70	969.50	970.70	953.00		24	14.00	0.0	Level	809+84.00	811+72.00	42	52	6.50	963.00
B-018-0-23	812+76.00	813+74.00	975.50	975.00	975.50	953.00		24	14.00	6.0	5:1	811+96.00	813+64.00	53	60	7.00	968.00
B-019-0-23	814+72.00	815+59.00	974.90	974.00	974.90	951.90		24	14.00	0.0	Level	813+88.00	815+56.00	61	68	6.50	967.50
B-020-0-23	816+46.00	817+24.50	974.30	973.50	974.30	956.30		24	14.00	0.0	Level	815+80.00	817+24.00	69	75	6.50	967.00
B-021-0-23	818+03.00	818+03.00	974.10	973.50	974.10	955.90		24	14.00	0.0	Level	817+48.00	818+08.00	76	79	6.50	967.00



## OHIO DEPARTMENT OF TRANSPORTATION

### OFFICE OF GEOTECHNICAL ENGINEERING

#### Noise Wall Design

**FRA-161-15.80  
117607**

**Noise Wall Along SR 161 Sta. 900+00.00 to 912+70.00**

**Noise Wall 9**

**Rii**

**Prepared By:** Dan Hayes, E.I.

**Date prepared:** Thursday, January 18, 2024

**Checked By:** Daniel E. Karch, P.E.

**Date Checked:** Thursday, January 18, 2024

**of Borings:**

**7**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
900+00.00	1	14.00	16.00	973.50
900+16.00	2	14.00	24.00	973.50
900+40.00	3	14.00	24.00	973.50
900+64.00	4	14.00	24.00	973.50
900+88.00	5	14.00	24.00	974.00
901+12.00	6	14.00	24.00	974.00
901+36.00	7	14.00	16.00	974.00
901+52.00	8	14.00	16.00	974.00
901+68.00	9	14.00	16.00	974.00
901+84.00	10	14.00	24.00	974.50
902+08.00	11	14.00	24.00	974.50
902+32.00	12	14.00	24.00	974.50
902+56.00	13	14.00	24.00	974.50
902+80.00	14	14.00	24.00	975.00
903+04.00	15	14.00	24.00	975.50
903+28.00	16	14.00	24.00	976.00
903+52.00	17	14.00	24.00	976.00
903+76.00	18	14.00	24.00	976.00
904+00.00	19	14.00	24.00	976.00
904+24.00	20	14.00	24.00	976.50
904+48.00	21	14.00	24.00	976.50
904+72.00	22	14.00	24.00	977.00
904+96.00	23	14.00	24.00	977.00
905+20.00	24	14.00	24.00	977.50
905+44.00	25	14.00	24.00	977.50
905+68.00	26	14.00	24.00	978.00
905+92.00	27	14.00	24.00	978.50
906+16.00	28	14.00	24.00	978.50
906+40.00	29	14.00	24.00	978.50
906+64.00	30	14.00	24.00	978.50
906+88.00	31	14.00	24.00	979.00
907+12.00	32	14.00	24.00	979.50
907+36.00	33	14.00	24.00	979.50
907+60.00	34	14.00	24.00	980.00

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
907+84.00	35	14.00	24.00	980.50
908+08.00	36	14.00	24.00	980.50
908+32.00	37	14.00	24.00	980.50
908+56.00	38	14.00	24.00	981.00
908+80.00	39	14.00	24.00	981.00
909+04.00	40	14.00	24.00	981.50
909+28.00	41	14.00	24.00	981.50
909+52.00	42	14.00	24.00	981.50
909+76.00	43	14.00	24.00	982.00
910+00.00	44	14.00	24.00	982.00
910+24.00	45	14.00	24.00	982.00
910+48.00	46	14.00	24.00	982.50
910+72.00	47	14.00	24.00	983.00
910+96.00	48	14.00	24.00	983.00
911+20.00	49	14.00	24.00	983.50
911+44.00	50	14.00	24.00	983.50
911+68.00	51	14.00	24.00	983.50
911+85.00	52	14.00	17.00	984.00
912+02.00	53	14.00	17.00	984.00
912+19.00	54	14.00	17.00	983.00
912+36.00	55	14.00	17.00	982.00
912+53.00	56	14.00	17.00	981.00
912+70.00	57	14.00	17.00	981.00

### Noise Wall ID: Noise Wall 9

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev.	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)	
B-031-0-2	900+16.00	901+08.00	974.50	973.50	974.50			24	14.00	3.0	3:1	900+00.00	900+88.00	1	5	7.00	966.50
B-032-0-2	902+00.00	903+00.00	975.20	974.50	975.20			24	14.00	3.0	3:1	901+12.00	902+80.00	6	14	7.00	967.50
B-033-0-2	904+00.00	905+00.00	977.20	976.00	977.20			24	14.00	4.0	4:1	903+04.00	904+96.00	15	23	7.00	969.00
B-034-0-2	906+00.00	907+00.00	979.30	978.50	979.30			24	14.00	3.0	3:1	905+20.00	906+88.00	24	31	7.00	971.50
B-035-0-2	908+00.00	909+00.00	981.40	980.50	981.40			24	14.00	5.0	5:1	907+12.00	908+80.00	32	39	7.00	973.50
B-036-0-2	910+00.00	911+00.00	983.20	982.00	983.20			24	14.00	4.0	4:1	909+04.00	910+96.00	40	48	7.00	975.00
B-037-0-2	912+00.00	912+00.00	984.90	984.00	984.90			24	14.00	3.0	3:1	911+20.00	912+70.00	49	57	7.00	####

**OHIO DEPARTMENT OF TRANSPORTATION****OFFICE OF GEOTECHNICAL ENGINEERING****Noise Wall Design****FRA-161-15.80  
117607****Noise Wall Along SR 161 Sta. 1100+00.00 to 1115+84.00****Noise Wall 11****Rii**

**Prepared By:** Dan Hayes, E.I.  
**Date prepared:** Thursday, January 18, 2024

**Checked By:** Daniel E. Karch, P.E.  
**Date Checked:** Thursday, January 18, 2024

**No. of Borings:** **9**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
1100+00.00	1	14.00	24.00	975.00
1100+24.00	2	14.00	24.00	975.00
1100+48.00	3	14.00	24.00	975.50
1100+72.00	4	14.00	24.00	976.00
1100+96.00	5	14.00	24.00	976.00
1101+20.00	6	14.00	24.00	976.00
1101+44.00	7	14.00	24.00	976.00
1101+68.00	8	14.00	24.00	976.50
1101+92.00	9	14.00	24.00	976.50
1102+16.00	10	14.00	24.00	976.50
1102+40.00	11	14.00	24.00	976.50
1102+64.00	12	14.00	24.00	976.50
1102+88.00	13	14.00	24.00	976.50
1103+12.00	14	14.00	24.00	977.00
1103+36.00	15	14.00	24.00	977.50
1103+60.00	16	14.00	24.00	978.00
1103+84.00	17	14.00	24.00	978.50
1104+08.00	18	14.00	24.00	979.00
1104+32.00	19	14.00	24.00	979.50
1104+56.00	20	14.00	24.00	979.50
1104+80.00	21	14.00	24.00	979.50
1105+04.00	22	14.00	24.00	979.50
1105+28.00	23	14.00	24.00	979.50
1105+52.00	24	14.00	24.00	980.00
1105+76.00	25	14.00	24.00	980.00
1106+00.00	26	14.00	24.00	980.00
1106+24.00	27	14.00	24.00	980.00
1106+48.00	28	14.00	24.00	980.00
1106+72.00	29	14.00	24.00	980.00
1106+96.00	30	14.00	24.00	980.00
1107+20.00	31	14.00	24.00	980.00
1107+44.00	32	14.00	24.00	979.50

Noise Wall: Noise Wall 11

FRA-161-15.80  
PID: 117607

**Design Data Sheet**

<b>STA. (FT)</b>	<b>Post No.</b>	<b>Barrier Height (FT)</b>	<b>Post Spacing (FT)</b>	<b>Top of Shaft Elev. (MSL FT)</b>
1107+68.00	33	14.00	24.00	979.50
1107+92.00	34	14.00	24.00	979.50

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
1108+16.00	35	14.00	24.00	979.50
1108+40.00	36	14.00	24.00	979.50
1108+64.00	37	14.00	24.00	980.00
1108+88.00	38	14.00	24.00	980.00
1109+12.00	39	14.00	24.00	980.50
1109+36.00	40	14.00	24.00	981.00
1109+60.00	41	14.00	24.00	981.00
1109+84.00	42	14.00	24.00	981.00
1110+08.00	43	14.00	24.00	981.00
1110+32.00	44	14.00	24.00	981.00
1110+56.00	45	14.00	24.00	981.00
1110+80.00	46	14.00	24.00	981.50
1111+04.00	47	14.00	24.00	981.50
1111+28.00	48	14.00	24.00	981.50
1111+52.00	49	14.00	24.00	981.50
1111+76.00	50	14.00	24.00	981.50
1112+00.00	51	14.00	24.00	982.00
1112+24.00	52	14.00	24.00	982.00
1112+48.00	53	14.00	24.00	982.00
1112+72.00	54	14.00	24.00	982.00
1112+96.00	55	14.00	24.00	982.00
1113+20.00	56	14.00	24.00	982.00
1113+44.00	57	14.00	24.00	982.00
1113+68.00	58	14.00	24.00	982.00
1113+92.00	59	14.00	24.00	982.50
1114+16.00	60	14.00	24.00	982.50
1114+40.00	61	14.00	24.00	982.50
1114+64.00	62	14.00	24.00	982.50
1114+88.00	63	14.00	24.00	982.50
1115+12.00	64	14.00	24.00	982.50
1115+36.00	65	14.00	24.00	982.50
1115+60.00	66	14.00	24.00	982.50

Noise Wall: Noise Wall 11

FRA-161-15.80  
PID: 117607

**Design Data Sheet**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
1115+84.00	67	14.00	24.00	982.50

**Boring Information and Design Recommendation**

FRA-161-15.80

PID: 117607

**Foundation Design**

**Noise Wall ID: Noise Wall 11**

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev. (ft)	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height (ft)	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)	
B-022-0-23	1100+00.00	1101+00.00	975.00	975.00	975.00	954.60		24	14.00	0.0 Level	1100+00.00	1100+96.00		1	5	6.50	968.50
B-023-0-23	1102+00.00	1103+00.00	977.00	976.50	977.00	966.50		24	14.00	6.0 5:1	1101+20.00	1102+88.00		6	13	7.00	969.50
B-024-0-23	1104+00.00	1105+00.00	979.60	978.50	979.60	956.60		24	14.00	0.0 Level	1103+12.00	1104+80.00		14	21	6.50	972.00
B-025-0-23	1106+00.00	1107+00.00	980.20	980.00	980.20			24	14.00	0.0 Level	1105+04.00	1106+96.00		22	30	6.50	973.50
B-026-0-23	1108+00.00	1109+00.00	979.80	979.50	979.80			24	14.00	6.0 5:1	1107+20.00	1108+88.00		31	38	7.00	972.50
B-027-0-23	1110+00.00	1111+00.00	981.50	981.00	981.50	958.50		24	14.00	10.0 Level	1109+12.00	1110+80.00		39	46	6.50	974.50
B-028-0-23	1112+00.00	1113+00.00	982.20	982.00	982.20	966.20		24	14.00	0.0 Level	1111+04.00	1112+96.00		47	55	6.50	975.50
B-029-0-23	1114+00.00	1114+92.00	983.00	982.50	983.00			24	14.00	0.0 Level	1113+20.00	1114+88.00		56	63	6.50	976.00
B-030-0-23	1115+84.00	1115+84.00	983.00	982.50	983.00	962.50		24	14.00	0.0 Level	1115+12.00	1115+84.00		64	67	6.50	976.00

**OHIO DEPARTMENT OF TRANSPORTATION****OFFICE OF GEOTECHNICAL ENGINEERING****Noise Wall Design**

**FRA-161-15.80  
117607**

**Noise Wall Along SR 161 Sta. 120+00.00 to 125+52.00**

**Noise Wall 12**

**Rii**

**Prepared By:** Dan Hayes, E.I.

**Date prepared:** Thursday, January 18, 2024

**Checked By:** Daniel E. Karch, P.E.

**Date Checked:** Thursday, January 18, 2024

**No. of Borings:**

**4**

<b>STA. (FT)</b>	<b>Post No.</b>	<b>Barrier Height (FT)</b>	<b>Post Spacing (FT)</b>	<b>Top of Shaft Elev. (MSL FT)</b>
120+00.00	1	14.00	12.00	981.50
120+12.00	2	14.00	12.00	982.00
120+24.00	3	14.00	12.00	982.50
120+36.00	4	14.00	24.00	983.00
120+60.00	5	14.00	12.00	983.50
120+72.00	6	14.00	24.00	984.00
120+96.00	7	14.00	24.00	984.50
121+20.00	8	14.00	24.00	985.50
121+44.00	9	14.00	24.00	985.50
121+68.00	10	14.00	24.00	985.50
121+92.00	11	14.00	24.00	985.50
122+16.00	12	14.00	24.00	985.50
122+40.00	13	14.00	24.00	984.50
122+64.00	14	14.00	24.00	984.50
122+88.00	15	14.00	24.00	985.50
123+12.00	16	14.00	24.00	986.00
123+36.00	17	14.00	24.00	986.50
123+60.00	18	14.00	24.00	986.50
123+84.00	19	14.00	24.00	986.50
123+92.00	20	14.00	8.00	986.50
124+16.00	21	14.00	24.00	986.50
124+35.00	22	14.00	19.00	986.50
124+54.00	23	14.00	19.00	986.50
124+73.00	24	14.00	19.00	986.50
124+97.00	25	14.00	24.00	986.50

**Noise Wall ID: Noise Wall 12**

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev. (ft)	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height (ft)	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)	
B-038-0-23	120+00.00	120+94.50	979.30	981.50	979.30	956.30		24	14.00	2.0	2:1	120+00.00	120+72.00	1	6	7.00	974.50
B-039-0-23	121+89.00	122+82.00	986.40	985.50	986.40	975.90		24	14.00	7.0	5:1	120+96.00	122+64.00	7	14	7.00	978.50
B-040-0-23	123+75.00	124+63.50	987.00	986.50	987.00	976.50		24	14.00	5.0	5:1	122+88.00	124+54.00	15	23	7.00	979.50
B-041-0-23	125+52.00	125+52.00	988.20	986.50	988.20	980.20		24	14.00	5.0	5:1	124+73.00	124+97.00	24	25	8.50	978.00

**OHIO DEPARTMENT OF TRANSPORTATION****OFFICE OF GEOTECHNICAL ENGINEERING****Noise Wall Design****FRA-161-15.80  
117607****Noise Wall Along SR 161 Sta. 1500+00.00 to 1502+40.00****Noise Wall 15****Rii****Prepared By:** Dan Hayes, E.I.**Date prepared:** Thursday, January 18, 2024**Checked By:** Daniel E. Karch, P.E.**Date Checked:** Thursday, January 18, 2024**No. of Borings:****2**

<b>STA. (FT)</b>	<b>Post No.</b>	<b>Barrier Height (FT)</b>	<b>Post Spacing (FT)</b>	<b>Top of Shaft Elev. (MSL FT)</b>
1500+00.00	1	14.00	24.00	1029.00
1500+24.00	2	14.00	24.00	1029.00
1500+48.00	3	14.00	24.00	1029.50
1500+72.00	4	14.00	24.00	1030.00
1500+96.00	5	14.00	24.00	1030.50
1501+20.00	6	14.00	15.00	1031.00
1501+35.00	7	14.00	15.00	1032.00
1501+50.00	8	14.00	24.00	1032.00
1501+74.00	9	14.00	15.00	1032.50
1501+89.00	10	14.00	15.00	1032.50
1502+04.00	11	14.00	20.00	1033.00
1502+24.00	12	14.00	16.00	1034.00
1502+40.00	13	14.00	24.00	1034.50

### Noise Wall ID: Noise Wall 15

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev. (ft)	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height (ft)	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)	
B-042-0-23	1500+29.00	1501+22.50	1030.30	1029.00	1030.30	1019.30		24	14.00	3.5   4:1	1500+00.00	1501+20.00		1	6	7.00	1022.00
B-043-0-23	1502+16.00	1502+16.00	1035.00	1033.00	1035.00	1024.50		24	14.00	4.0   4:1	1501+35.00	1502+40.00		7	13	7.00	1026.00

**OHIO DEPARTMENT OF TRANSPORTATION****OFFICE OF GEOTECHNICAL ENGINEERING****Noise Wall Design****FRA-161-15.80  
117607****Noise Wall Along SR 161 Sta. 1504+27.00 to 1518+43.00****Noise Wall 15****Rii**

**Prepared By:** Dan Hayes, E.I.  
**Date prepared:** Thursday, January 18, 2024

**Checked By:** Daniel E. Karch, P.E.  
**Date Checked:** Thursday, January 18, 2024

**No. of Borings:** **8**

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
1504+27.00	14	14.00	24.00	1038.00
1504+51.00	15	14.00	24.00	1038.00
1504+75.00	16	14.00	24.00	1038.00
1504+99.00	17	14.00	24.00	1038.00
1505+23.00	18	14.00	24.00	1038.00
1505+47.00	19	14.00	24.00	1038.00
1505+71.00	20	14.00	24.00	1038.00
1505+95.00	21	14.00	24.00	1038.00
1506+19.00	22	14.00	24.00	1038.00
1506+43.00	23	14.00	24.00	1038.00
1506+67.00	24	14.00	24.00	1038.50
1506+91.00	25	14.00	24.00	1038.50
1507+15.00	26	14.00	24.00	1038.50
1507+39.00	27	14.00	24.00	1038.50
1507+63.00	28	14.00	24.00	1038.50
1507+87.00	29	14.00	24.00	1038.50
1508+11.00	30	14.00	24.00	1038.50
1508+35.00	31	14.00	24.00	1038.50
1508+59.00	32	14.00	24.00	1038.50
1508+83.00	33	14.00	24.00	1038.50
1509+07.00	34	14.00	24.00	1038.50
1509+31.00	35	14.00	24.00	1038.50
1509+55.00	36	14.00	24.00	1038.50
1509+79.00	37	14.00	24.00	1038.50
1510+03.00	38	14.00	24.00	1038.50
1510+27.00	39	14.00	24.00	1038.50
1510+51.00	40	14.00	24.00	1038.50
1510+75.00	41	14.00	24.00	1037.50
1510+99.00	42	14.00	24.00	1037.50
1511+23.00	43	14.00	24.00	1037.00
1511+47.00	44	14.00	24.00	1037.00
1511+71.00	45	14.00	24.00	1036.50

Noise Wall: Noise Wall 15

FRA-161-15.80  
PID: 117607

**Design Data Sheet**

<b>STA. (FT)</b>	<b>Post No.</b>	<b>Barrier Height (FT)</b>	<b>Post Spacing (FT)</b>	<b>Top of Shaft Elev. (MSL FT)</b>
1511+95.00	46	14.00	24.00	1036.50
1512+19.00	47	14.00	24.00	1036.50

STA. (FT)	Post No.	Barrier Height (FT)	Post Spacing (FT)	Top of Shaft Elev. (MSL FT)
1512+43.00	48	14.00	24.00	1036.50
1512+67.00	49	14.00	24.00	1036.50
1512+91.00	50	14.00	24.00	1036.50
1513+15.00	51	14.00	24.00	1036.50
1513+39.00	52	14.00	24.00	1036.50
1513+63.00	53	14.00	24.00	1036.50
1513+87.00	54	14.00	24.00	1036.50
1514+11.00	55	14.00	24.00	1036.50
1514+35.00	56	14.00	24.00	1036.50
1514+59.00	57	14.00	24.00	1036.50
1514+83.00	58	14.00	24.00	1036.50
1515+07.00	59	14.00	24.00	1036.50
1515+31.00	60	14.00	24.00	1036.50
1515+55.00	61	14.00	24.00	1036.50
1515+79.00	62	14.00	24.00	1037.00
1516+03.00	63	14.00	24.00	1037.00
1516+27.00	64	14.00	24.00	1037.00
1516+51.00	65	14.00	24.00	1037.50
1516+75.00	66	14.00	24.00	1037.50
1516+99.00	67	14.00	24.00	1038.00
1517+23.00	68	14.00	24.00	1038.00
1517+47.00	69	14.00	24.00	1037.50
1517+71.00	70	14.00	24.00	1036.50
1517+95.00	71	14.00	24.00	1035.50
1518+19.00	72	14.00	24.00	1034.50
1518+43.00	73	14.00	24.00	1034.50

**Boring Information and  
Design Recommendation**

FRA-161-15.80

PID: 117607

**Foundation Design**

**Noise Wall ID: Noise Wall 15**

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev. (ft)	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height (ft)	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)		
B-044-0-23	1504+27.00	1505+17.50	1038.30	1038.00	1038.30	1025.30		24	14.00	3.0	3:1			#REF!	17	7.00	1031.00	
B-045-0-23	1506+08.00	1507+09.00	1038.90	1038.00	1038.90	1025.90		24	14.00	3.0	3:1	1505+23.00	1506+91.00		18	25	7.00	1031.00
B-046-0-23	1508+10.00	1509+10.00	1039.10	1038.50	1039.10	1028.60		24	14.00	3.0	3:1	1507+15.00	1509+07.00		26	34	7.00	1031.50
B-047-0-23	1510+10.00	1511+10.00	1039.20	1038.50	1039.20	1026.20		24	14.00	4.0	4:1	1509+31.00	1510+99.00		35	42	7.00	1031.50
B-048-0-23	1512+10.00	1513+10.00	1037.40	1036.50	1037.40	1021.40		24	14.00	7.0	5:1	1511+23.00	1512+91.00		43	50	7.00	1029.50
B-049-0-23	1514+10.00	1515+10.00	1038.90	1036.50	1038.90	1023.40		24	14.00	0.0	Level	1513+15.00	1515+07.00		51	59	6.50	1030.00
B-050-0-23	1516+10.00	1517+14.65	1038.00	1037.00	1038.00	1025.00		24	14.00	8.0	Level	1515+31.00	1516+99.00		60	67	6.50	1030.50
B-051-0-23	1518+19.30	1518+19.30	1038.10	1034.50	1038.10	1021.80		24	14.00	7.0	5:1	1517+23.00	1518+43.00		68	73	8.50	1026.00

**OHIO DEPARTMENT OF TRANSPORTATION****OFFICE OF GEOTECHNICAL ENGINEERING****Noise Wall Design****FRA-161-15.80  
117607****Noise Wall Along SR 161 Sta. 1518+90.00 to 1522+26.00****Noise Wall 15****Rii****Prepared By:** Dan Hayes, E.I.**Date prepared:** Thursday, January 18, 2024**Checked By:** Daniel E. Karch, P.E.**Date Checked:** Thursday, January 18, 2024**No. of Borings:****3**

<b>STA. (FT)</b>	<b>Post No.</b>	<b>Barrier Height (FT)</b>	<b>Post Spacing (FT)</b>	<b>Top of Shaft Elev. (MSL FT)</b>
1518+90.00	74	14.00	24.00	1037.50
1519+14.00	75	14.00	24.00	1037.50
1519+38.00	76	14.00	24.00	1037.50
1519+62.00	77	14.00	24.00	1037.50
1519+86.00	78	14.00	24.00	1037.50
1520+10.00	79	14.00	24.00	1037.50
1520+34.00	80	14.00	24.00	1037.50
1520+58.00	81	14.00	24.00	1037.50
1520+82.00	82	14.00	24.00	1037.50
1521+06.00	83	14.00	24.00	1037.00
1521+30.00	84	14.00	16.00	1036.50
1521+46.00	85	14.00	24.00	1036.50
1521+70.00	86	14.00	24.00	1036.50
1521+94.00	87	14.00	24.00	1036.00
1522+18.00	88	14.00	24.00	1036.00

### Noise Wall ID: Noise Wall 15

Boring ID	Boring STA. (ft)	Mid-Boring STA. (ft)	Boring Elev. (ft)	Shaft Elev. (ft)	Ex. Ground Elev. (ft)	Rock Elev. (ft)	Rock UCS (psi)	Post Spacing (ft)	Barrier Height (ft)	Cross Slope	From DS STA.	To DS STA.	From Post No.	To Post No.	DS Length (ft)	Bottom of DS Elev. (ft)
B-051-0-23	1519+10.60	1519+75.80	1038.10	1037.50	1038.10	1021.80		24	14.00	5.0   5:1	1518+90.00	1519+62.00	74	77	8.50	1029.00
B-052-0-23	1520+41.00	1521+33.50	1038.60	1037.50	1038.60	1028.10		24	14.00	5   5:1	1519+86.00	1521+30.00	78	84	7.00	1030.50
B-053-0-23	1522+26.00	1522+26.00	1036.50	1036.00	1036.50	1022.40		24	14.00	0   Level	1521+46.00	1522+18.00	85	88	9.50	1026.50