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## DISCLAIMER

The contents of this report are protected in accordance with 23 USC Section 409: Discovery and Admission as Evidence of Certain Reports and Surveys.

## INTRODUCTION

## PURPOSE ANDNEED

The purpose of this study is to evaluate existing safety and traffic operations of US Route 422 and to identify potential countermeasures to reduce congestion and traffic crashes along US Route 422 from SLM 10.93 to SLM 13.31 in Geauga county, Ohio. The study area has several locations listed on the ODOT's safety program crash priority list (2013) as shown in Figure 1 below. Four (4), rural nonfreeway crash locations exist within the study area and range between \#77 and \#247 on the statewide ranking. Two (2) rural intersections of US Route 422 with Rapids Road and S.R. 700 also appear on the list ranked at 60 and 142 , respectively.

FIGURE1: ODOTS CRASH PRIORITY LOCATIONS (2013)


A review of crash data provided by the Ohio Department of Transportation (ODOT) yielded a total of 96 reported crashes within study area during a 3 -year period between 2011 and 2013. The following crash types and conditions are over represented at the study location compared to statewide averages (shown in parenthesis). Note the statewide crash averages are based on 2008-2012 data whereas the project data encompasses years 2011 to 2013.
> Total crashes: 96 total crashes
> Injury crashes: 30 crashes or 31.3 percent
> Rear end: 45 crashes or 46.9 percent
> Fixed Object: 24 crashes or 25.0 percent
(14.6 percent)

## BACKGROUND

US Route 422 is an east-west route that runs through Geauga County providing access to Cleveland to the west and Portage/Trumbull counties to the east and IR-80. US Route 422 is functionally classified as a rural principal arterial and also has an NHS route designation. Significant truck traffic is observed on US Route 422 within the study limits. Land uses are primarily rural undeveloped parcels with industrial land uses near the Great Lakes Parkway and the S.R. 700 intersections. A project location map is provided in Figure 2.
S.R. 700 is a north-south route that runs from the village of Burton at the north end to IR-80 to the south. S.R. 700 is a two lane roadway with a functional classification of a rural major collector and a posted speed limit of 45 miles per hour (MPH) within study limits.

Rapids Road (C.R. 1) is also a two lane north-south roadway, functionally classified as a rural local road.

## PREVIOUS STUDIES

An abbreviated safety study dated January 2013 was prepared for the section of US Route 422 from SLM 12.30 (Cuyahoga River) to SLM 12.60. There were 5 documented crashes during the $2009-2011$ analysis period with most attributed to the driveways of the Iron Horse Saloon property. The consolidation of driveways was recommended as a long term countermeasure. Appendix A includes excerpts from this safety study.

A technical memorandum dated June 2007 also was prepared by HNTB for the signalized intersection of US Route 422/S.R. 700. This memorandum summarized traffic operations under existing conditions (2007) and three alternatives.
$>$ Alternative 1 was the no build alternative
$>$ Alternative 2 added east/west left turn lanes in addition to a leading eastbound left phase.
$>$ Alternative 3 added left turn lanes on all four approaches in addition to a leading eastbound and northbound left turn phases.

Appendix A also includes excerpts from this capacity analysis technical memorandum.

AGURE 2: PROJECT LOCATION MAP



## EXISTING CONDITIONS

## ROADWAY CONDTIONS

US Route 422 is a two lane undivided roadway within the study limits. US Route 422 is functionally classified as a rural principal arterial with a posted speed limit of 45 MPH. Existing roadway conditions are summarized in Table 1 and described in additional detail below.

TABLE 1: EXISTING ROADWAY CONDITIONS

|  | USROUIE 422 <br> (SR 422) | RAPIDSRD (CR. 1) | S.R.700 | GREAT LAKES <br> PKWY |
| :--- | :---: | :---: | :---: | :---: |
| ODOT <br> Functional <br> Classification | Rural Principal Arterial | Rural Local | Rural Major Collector | Rural Local |
| Posted speed <br> limit | 45 MPH | $55 \mathrm{MPH}^{1}$ | 45 MPH | 25 MPH |
| 2012 ADT <br> (Source: TIMS) | $15,100 \mathrm{vpd}$ | $1,700 \mathrm{vpd}$ | $3,300 \mathrm{vpd}$ | NA |
| Daily Truck <br> percentage | $13 \%$ | NA | $3 \%$ | $18 \%^{2}$ |
| NHS Route | Yes | No | No | No |

Note 1: Speed limit (unposted) per ORC code 4511.21
Note 2: Source - 2014 Turn count (6AM-7PM) at US Route 422/GLP intersection, approach volume

## > US Route 422 (east/west)

- 2-lane roadway section comprised of one travel lane in each direction. Exclusive turn lanes exist at the intersection of Great Lakes Parkway. Turning maneuvers are made from shared lanes at other intersections within the study area.
- Center line rumble strips are installed on US Route 422 from east of Great Lakes Parkway (SLM 11.03) to 0.30 miles west of S.R. 700 (SLM 12.75).
- Guard rail is installed at various locations within study limits.
- Steep vertical grade of nearly 7 percent exists along US Route 422 approaching S.R. 700 in the eastbound direction. The steep grade affects trucks to have longer start up loss times from a stopped condition, resulting in much longer delays and travel times in that section of US Route 422.
- Reverse curves exist on the approach to the Cuyahoga River crossing near SLM 12.30


## > S.R. 700 (north/south)

- 2-lane roadway section comprised one travel lane in each direction with paved shoulder within study limits.
- The posted speed limit is 45 mph within the project limits and changes to $55 \mathrm{mph}, 0.30$ miles north of US Route 422 and 0.40 miles south of US Route 422.
- School zone exists along S.R. 700, 100 feet south of US Route 422 intersection associated with an Agape Christian Academy within 500 feet of the intersection.


## INIERSECTION CONDITIONS

Three primary intersections exist on US Route 422 corridor within study limits.

## Great Lakes Parkway

Great Lakes Parkway provides access to Great Lakes Cheese facility and a Saint Gobain Crystals facility. This T- intersection is under signal control. Exclusive turn lanes exist along US Route 422 and Great Lakes Parkway. Advance signal warning signs are mounted on US Route 422

## Rapids Road

Rapids Road is a local street and the intersection of US Route 422/Rapids Road is under two-way stop control. A flashing signal support is supplemented with dual stop signs on Rapids Road.

## S.R. 700

The intersection of S.R. 700 with US Route 422 is under signal control. Both roadways are two-lane roadways (one lane in each direction). Exclusive turn lanes are not provided on all four approaches.

## RELD OBSERVATIONS

Other observations made during the site visit have been listed below:
$>$ Extended queues were observed on US Route 422 during PM peak approaching S.R. 700 in the eastbound direction. These queues extended west of the Cuyahoga River crossing ( 5100 feet from the S.R. 700 intersection) between 4:25 pm and 5:10 pm. Picture 1 below shows eastbound queues (Source: ODOT's video log dated August 2012).

$>$ Significant truck traffic ( 15 percent) during peak hours
$>$ Turning radius is constrained at the intersection of US Route 422/S.R. 700. A northbound truck turning right onto US Route 422 (Picture 2 and 3 ) required westbound vehicles to backup 80-100 feet to accommodate the turning maneuver.




Picture 4 below depicts the southbound right turn manuever, where the turning path falls in the eastbound approach lane. Similarly, turning manuevers from other approaches are deficient in required turning radius for tractor trailer trucks.

> Chevron Alignment curve warning signs (W1-8) were found to be mounted at an approximate height of 7 feet in the reverse curve section near the Cuyahoga River crossing (SLM 12.05 to SLM 12.50). as shown in the picture to the right.



## LAND USE AND PROPERTY ACCESS

Land uses along US Route 422 are primarily rural undeveloped farm land. Some industrial land uses exist at Great Lakes Parkway intersection, single family residential is observed along the corridor between Highland Drive and the Cuyahoga River crossing. East of S.R. 700 intersection, the land uses are a mix of commercial and residential land uses.

## DATA COШECTION

Turning movement counts were conducted using Miovision technology at the three study intersections (Great Lakes Parkway, Rapids Road and S.R. 700) with US Route 422 on September 9, 2014 from 6 AM7 PM. Peak traffic volumes occur between 6:30 and 7:30 AM (morning peak hour) and between 4:45 and 5:45 PM (evening peak hour).

The turn count data was supplemented with field observation during the week of September 29, 2014. Significant queues were observed at the US-422/SR-700 intersection on the eastbound approach, the longest queue reaching about 5,100 feet from the S.R. 700 intersection during the afternoon peak hour. Traffic volume data was adjusted to account for the unserved demand. An additional 169 vehicles were added to the PM peak hour counted volume. The adjusted volumes were used in preparation of the detailed analyses contained in this report. Turn count data and manual adjustments are provided in Appendix B.

The approach grades at the US-422/SR-700 intersection range from 4\% to 8\%. Approximated values were used in calculation of change and clearance intervals for each movement as detailed later in this report. The eastbound grade was found to be most severe at $+8 \%$ and the slope extends for approximately 2,400 feet approaching the intersection. The slope noticeably affected vehicle start-up time as observed during field visit. To account for this inefficiency, start-up time was modified to 3.0 seconds for the detailed capacity analysis contained in this report.

## CHANGE AND CLEARANCE INIERVALS

Vehicular change and clearance intervals were calculated for the study intersection based on guidelines published in the Ohio Manual of Uniform Traffic Control Devices and the ITE Proposed Recommended Practice. A summary of existing and calculated clearance intervals is provided in Table 2. Detailed calculations and methodology is provided in Appendix C. Calculated clearance times differ from the existing timings suggesting that signal timing modifications may be warranted based on current industry best practices and lower operating speeds during peak periods.

TABLE 2: CHANGE AND CLEARANCE INTERVAL SUMMARY

| Phase | Existing Yellow All Red [sec] | Existing <br> TOTAL <br> [sec] | Calculated Yellow All Red [sec] | Calculated TOTAL [sec] |
| :---: | :---: | :---: | :---: | :---: |
| US-422 and Great Lakes Pkwy |  |  |  |  |
| Phase 1: WB Left | 4.0 / 2.0 | 6.0 | 3.0 / 2.9 | 5.9 |
| Phase 2: EB Through | 4.0 / 2.0 | 6.0 | 4.3 / 1.4 | 5.7 |
| Phase 6: WB Through | 4.0 / 2.0 | 6.0 | 4.3 / 1.4 | 5.7 |
| Phase 8: NB All | 4.0 / 2.0 | 6.0 | 3.0 / 2.6 | 5.9 |
| US-422 and Papids Rd |  |  |  |  |
| Phase 2: EB Through | N/A <br> (Stop Control) |  | 4.3 / 1.0 | 5.3 |
| Phase 4: SB Through |  |  | $5.0 / 1.0$ | 6.0 |
| Phase 5: EB Left |  |  | 3.0 / 1.3 | 4.3 |
| Phase 6: WB Through |  |  | 4.3 / 1.0 | 5.3 |
| Phase 8: NB Through |  |  | 5.0 / 1.0 | 6.0 |


| US-42 and SR-700 |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Phase 2: EB Through | $4.0 / 2.0$ | 6.0 | $4.9 / 1.2$ | 6.1 |
| Phase 4: SB Through | $4.0 / 2.0$ | 6.0 | $4.8 / 1.4$ | 6.2 |
| Phase 5: EB Left | $4.0 / 2.0$ | 6.0 | $3.0 / 2.0$ | 5.0 |
| Phase 6: WB Through | $4.0 / 2.0$ | 6.0 | $4.9 / 1.2$ | 6.1 |
| Phase 8: NB Through | $4.0 / 2.0$ | 6.0 | $4.8 / 1.4$ | 6.2 |

Recommended intervals exceed the existing timings at SR-700 on the southbound and westbound approaches. This is attributed to the approach grades at the intersection. The negative approach grades are approximated at $-4 \%$ in the southbound direction and $-5 \%$ in the westbound direction.

## INIERSECTION CAPACITY

Intersection capacity was evaluated to assess existing operating conditions and to identify critical deficiencies that may contribute to safety issues. Analyses were prepared using existing (2014) peak hour volumes, adjusted for eastbound queues, and existing signal timing and phasing. Existing levels of service and vehicle delay are summarized in Table 3. Analysis methodology and detailed output reports are included in Appendix D.

Results indicate that under current conditions, there are capacity deficiencies at the US-422/Rapids Road intersection on the northbound and southbound approaches during the morning and afternoon peak hours.

Deficiencies are also present at the US-422/SR-700 intersection during the afternoon peak hour, especially in the eastbound direction. The volume to capacity ratio of the EB approach is 1.10 during the PM peak, which is $10 \%$ over capacity.

TABLE 3: EXISTING INIERSECTION CAPACITY SUMMARY

|  |  | 7 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 |  | $T$ 0 0 0 0 0 0 $\frac{1}{1}$ 0 0 | $z$ 6 II 4 0 1 2 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| US-422 \& Great Lakes Pkwy |  |  |  |  |  |
| 2014 AM Peak - Existing (Signal) | B/14.2 | B/19.2 | D/38.2 | - | C/21.4 |
| 2014 PM Peak - Existing (Signal) | D/45.3 | A/5.2 | D/36.4 | - | C/33.5 |
| US-422 \& Rapids Rd |  |  |  |  |  |
| 2014 AM Peak - Existing (Stop) | A/1.0 | A/0.1 | F/261.2 | F/52.4 | B/13.3 |
| 2014 PM Peak - Existing (Stop) | A/1.4 | A/0.3 | F/208.2 | F/107.0 | A/9.7 |
| US-422 \& SR-700 |  |  |  |  |  |
| 2014 AM Peak - Existing (Signal) | D/47.5 | D/46.2 | D/41.7 | C/27.4 | D/44.1 |
| 2014 PM Peak - Existing (Signal) | F/289.5 | B/11.4 | E/77.7 | E/77.2 | F/190.9 |

[^0]
## CRASH ANALYSIS

CRASH DATA
Crash data was furnished by the Ohio Department of Transportation for US Route 422 corridor from SLM 10.93 to SLM 13.31, encompassing a three-year study period between 2011 and 2013. The OH-1 report for each documented crash was reviewed to confirm accuracy and to locate crashes properly within the study limits. Crash diagrams are provided in Appendix E.

Noteworthy crash statistics for the three-year period are summarized below and shown graphically in Graphs 1, 2 and 3. Statewide averages for crashes on state system, non-freeway locations are shown in parentheses based on data for years 2008 through 2012.
> Total crashes: 96 total crashes
> Injury: 30 crashes or 31.3 percent
(25.4 percent)
> Rear end: 45 crashes or 46.9 percent
(30.9 percent)
> Fixed Object: 24 crashes or 25.0 percent
(14.6 percent)

General crash observations include:
> Rear end, fixed object and angle crashes represent the top 3 crash types observed within study area as shown in Graph 1, accounting for over 80 percent of the total crashes.
$>$ Seventy percent of crashes were recorded between the hours of 6AM-9AM and 2PM-7PM (Graph 2).
> Nineteen percent of crashes were recorded under dark - roadway not lighted conditions as shown in Graph 3.

GRAPH1: PREQUENCY OF CRASHESBY CRASH TYPE


GRAPH 2: PREQUENCY OF CRASHESBY TIME OF DAY


GRAPH 3: PREQUENCY OF CRASHES BY LGHT CONDITION


Crashes recorded within the study area have been summarized by location and crash type in Table 4.
TABLE4: CRASH SUMMARY

| CRASH TYPE | DIRECTION | $\begin{gathered} \text { GREAT } \\ \text { LAKES } \\ \text { PARKWAY } \end{gathered}$ | $\begin{aligned} & \text { SECNENT } \\ & \text { (GLP TO } \\ & \text { RAPIDS) } \end{aligned}$ | RAPIDS ROAD | $\begin{gathered} \text { SEGMENT } \\ \text { (RAPIDS } \\ \text { TOSRR } \\ 700) \end{gathered}$ | $\begin{aligned} & \text { S.R. } \\ & 700 \end{aligned}$ | $\begin{aligned} & \text { SEGMENT } \\ & \text { EAST OF } \\ & \text { SR. } 700 \end{aligned}$ | $\begin{aligned} & \text { NASH } \\ & \text { ROAD } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rear <br> End | Eastbound | 4 | 2 | 7 | 11 | 5 | 1 | 3 |
|  | Westbound | 2 | 1 | 3 | 1 | 4 | -- | -- |
| Angle |  | -- | -- | $\begin{aligned} & 3-\mathrm{EB} / \mathrm{NB} \\ & 2-\mathrm{EB} / \mathrm{SB} \end{aligned}$ | -- | 4 | 1 | -- |
| Fixed Object | Eastbound | -- | 4 | 1 | 7 | - | 1 | -- |
|  | Westbound | -- | 3 | - | 5 | 1 | -- | -- |
|  | Cross street | -- | -- | 1 | - | -- | -- | -- |
| LeftTurn |  | -- | -- | -- | 1 | 2 | -- | -- |
| Other |  | 2 | 2 | -- | 5 | 2 | 1 | 2 |
| Injury Crashes |  | 0 | 5 | 5 | 9 | 7 | 1 | 1 |
| Total |  | 8 | 12 | 17 | 30 | 18 | 4 | 5 |

## REAREND CRASHES

A total of 45 rear end crashes were reported within the study area with 38 percent resulting in injury. A review of crashes by hour of day indicates that rear end crash patterns peak between 6AM and 9AM (24 percent) and between 3PM and 6PM (49 percent). Seventy three percent of the rear end crashes occurred during these six hours, indicating congestion as a contributing factor.

Of the 45 crashes, 33 crashes involved eastbound vehicles and the remaining 12 were related to westbound vehicles. These crashes resonate with field observations, where significant queues were observed in the eastbound direction approaching S.R. 700 intersection.

## FXED OBJECT CRASHES

Twenty four fixed object crashes were reported within study area with 21 percent resulting in injury. Thirteen of the fixed object crashes occurred under cloudy/rain/snow weather condition. A contributing factor for some of the fixed object crashes involved a vehicle leaving the roadway to avoid striking a stopped/slowing vehicle.

Roadway geometry elements that adversely impact fixed object/out-of control crashes include horizontal curvature and steep vertical grades along US Route 422, lack of safety grading of shoulders, and the presence of guard rail.

## ANGLECRASHES

Ten angle crashes were reported within the study area, nine of them reported at an intersection and one crash driveway related.
> Of the nine intersection related crashes, five crashes were reported at Rapids Road intersection and four crashes at the S.R. 700 intersection.
$>$ Four of the five angle crashes at Rapids Road intersection involved a side street motorist at fault.
> Two of the four angle crashes at S.R. 700 intersection involved red light violation crashes.

## INJURY CRASHES

The study area experienced thirty injury crashes, equivalent to 31 percent of all crashes recorded within the study period. Rear-end crashes and fixed object/out-of control crashes accounted for 77 percent of injuries.

## CRASH SUMMARY BY LOCATION

## US Route 422/Great Lakes Parkway - Intersection (SLM11.03)

Eight crashes have been documented at the Great Lakes parkway intersection within the study period. These include six rear-end crashes (four eastbound and two westbound), one each of a backing and of a head-on crash.

## US Route 422 - GLP to Rapids Road (SLM11.08-SLM1150)

Within this section of US Route 422, twelve crashes have been documented. Prevalent crash types include rear-end ( 3 crashes), four eastbound out of control crashes, and three westbound out of control crashes.

## US Route 422/Rapids Road - Intersection (SLM1155)

Seventeen crashes have been recorded at the Rapids road intersection within the study period. The most prevalent patterns are seven eastbound rear end crashes involving through vehicles stopped behind left turning vehicles and four angle crashes attributed to stop sign violations.

## US Route 422 -Rapids Road to S.R. 700 (SLM1160-1299)

Within this section of US Route 422 between Rapids road and S.R. 700, thirty crashes have been recorded. Rear-end and fixed object/out-of-control crashes, twelve crashes each are the prevalent crash types observed in this section.

Of the twelve rear-end crashes, ten crashes involve eastbound vehicles. A majority of these eastbound rear-end crashes were recorded between 3 pm and 7 pm , consistent with the PM peak extended queues in the eastbound direction of US Route 422 approaching S.R. 700 intersection as observed during site visit.

Fixed object/out of control crashes were concentrated (6 crashes), east of Cuyahoga River crossing on a curved section of US Route 422 (Crash Diagram - Sheet 9). In this section, 3 out of control crashes along with a rear-end crash involved eastbound vehicles and were also driveway related crashes. No contributing factor $s$ were noted for the other 3 out of control crashes in the westbound direction.

## US Route 422IS.R. 700 (SLM13.04)

Eighteen crashes have been recorded at the S.R. 700 intersection within the study period. Most prevalent crash types include nine rear-end (5 - eastbound, 4 - westbound), angle (4 crashes) and left turn (2 crashes).

## US Route 422 -East of S.R. 700 (SLM13.09 - SLM13.31)

This section of US Route 422 experienced nine crashes within the study period. Prevalent crash types include three eastbound rear end crashes and two westbound sideswipe passing crashes near the unsignalized intersection of Nash road.

Nash road is under stop control, and intersects with US Route 422 at an oblique angle. Westbound vehicles on Nash road approaching US Route 422 have limited intersection sight distance. Also, two other factors that contribute to crashes include horizontal curvature on this section of US Route 422 and wide pavement (access) to the Marathon gas station on the north side.

## COUNTERMEASURES

The following section addresses contributing factors associated with the prevalent crashes patterns along the US Route 422 corridor and possible countermeasures to mitigate those crashes. Additional countermeasures are recommended to minimize potential safety issues that may not be directly attributed to historical crash trends. Detailed technical analyses including intersection clearance interval calculations, signal warrants, capacity analyses, signal warrants and turn lane sizing calculations are summarized in Appendix C, D, F and G, respectively.

The following are key factors that contribute to the most prevalent crash patterns observed along US Route 422 corridor and intersections: Countermeasure recommendations are intended to address these factors.
> Absence of left turn lanes. There are no exclusive turn lanes at the intersections of Rapids Road and of S.R. 700. Exclusive left turn lanes allow separation of turning vehicles from the through traffic and provide a dedicated space for turning vehicle before executing the desired movements. Auxiliary turn lane reduces the need for a through vehicle to slow or stop to avoid a rear end crash with a turning vehicle and thereby mitigate rear end crashes.
> Fixed object/out of control crashes. A contributing factor of some fixed object/out of control crashes include presence of shoulders and stopped vehicles in shared lanes.
> Traffic control at the US Route 422/Rapids Road intersection. Contributing factor of angle crashes and rear end crashes is extended delays for minor street approaches due to twoway stop control (i.e., stop condition for Rapids Road). Contributing factor of rear end crashes on US Route 422 is left turning vehicles blocking through vehicles. US Route 422 is free flow and drivers do not anticipate stop conditions resulting in crashes. Similarly, angle crashes can be attributed to infrequent gaps in mainline traffic for drivers on Rapids Road to identify a safe gap.

## SHORT TERM COUNIERMEASURES

The following countermeasures are recommended to mitigate all crashes at the US Route 422/Rapids Road intersection.
> Install traffic signal: The installation of a traffic signal at the US Route 422/Rapids Road intersection is warranted based on existing traffic volumes. A traffic signal will decrease vehicle delay and mitigate angle crashes at the intersection. Recommended features of the proposed signal operation include three phase operation with an eastbound lead left turn movement to reduce queues on US Route 422. Warrants are contained in Appendix F.
> Clear sight triangles. Sight distance on the Rapids Road approaches is restricted due to poles and a telephone junction box (northwest quadrant). Vehicles on Rapids Road are obscured by vegetation. Measures to maintain clear sight triangles by removing vegetation, relocating telephone junction box are recommended along with traffic signal installation.
> Revised centerline width. Revise the centerline pavement marking on US Route 422 to be a standard solid, double yellow centerline. Increased shoulder width would mitigate the fixed object crashes within the study area by providing for a wider paved shoulder.
> Upgrade clearance intervals. Modification of the yellow change and all red clearance times is recommended. Calculations have been prepared in accordance with the ODOT Traffic Engineering Manual and ITE recommended practices, as summarized in Appendix F.

## MEDIUM TERMCOUNIERMEASURES

The following countermeasures are recommended to mitigate all crashes at the US Route 422/S.R. 700 intersection.
> Install left turn lanes on US Route 422. Widening of US Route 422 is recommended to provide dedicated lanes for left turning vehicles at the S.R. 700 intersection. Left turn lane sizing calculations are provided in Appendix G. A conceptual layout of the left turn lane improvement is shown in Figure 4 assuming pavement widening on the south side of US Route 422.

The eastbound left turn volume of 108 vph is only 11 percent of the approach volume during the PM peak hour, however for every stopped car waiting for a safe gap in opposing through volume, the through and right turning vehicles queue behind the stopped car, resulting in very long queues on an already congested segment. Separating through movements from left turning vehicles can decrease the headway between vehicles and improve the flow rate through the signal for both movements.

The high traffic volumes on eastbound approach suggests that further delay to EB through traffic may be attributed to queues that form as a result of vehicles slowing or stopping to turn left to S.R. 700. The benefit of physically separating turning vehicles from through traffic removes slow or decelerating vehicles from the through lane, thus reducing the potential for rear end crashes. Dedicated left turn lanes on westbound US Route 422 will also likely mitigate the westbound rear end crash pattern.

The FHWA publication titled Signalized Intersections: Informational Guide states that a left turn lane can be expected to decrease rear-end, left turn and red light running crashes. The crash reduction potential will depend on whether left turn phasing is provided, ranging from 15 to 35 percent. The FHWA signalized intersection guide provides eight criteria for justification of left turn phasing (protected-permissive, permissive-protected, or protected only). Left turn phasing should be considered if any one of the eight criteria is satisfied. The US Route 422/S.R. 700 intersection does not satisfy any of the left turn phasing criteria.

Cost estimates for this improvement is included in Appendix H.
> Interconnection of Signals. The traffic signals at Great Lakes Parkway, Rapids Road and S.R. 700 are recommended to be interconnected as part of a coordinated signal system. Interconnection of signals on US Route 422 will reduce the number of stops. Near perfect progression can be achieved between the signalized intersections within the study area (based on a 90 second cycle length and operating speeds of 45 MPH ).
> Curve signing. Existing warning signs on US Route 422 for the reverse curve section near Cuyahoga River crossing (SLM 12.05 to SLM 12.50) include a reverse curve sign (W1-4) on the tangent section and chevron warning signs (W1-8) are mounted on the outside of the curve.

- Relocate the existing warning signs (350 feet in advance of the curve) to a distance in advance of the curves consistent with OMUTCD guidelines (175 feet) for no deceleration and a 45 MPH posted speed.
- Replacement of W1-4 signs with winding road (W1-5) signs is recommended at a distance between 100 feet and 175 feet in advance of the curves.
- The existing chevron warning signs (W1-8) mounted at a height of 7 feet in both directions are recommended to be lowered/replaced to a maximum height of 5 feet for improved visibility.



## LONG TERMCOUNTERMEASURES

> Install left turn lanes on US Route 422 at Rapids Road. The eastbound left turn demand at Rapids Road intersection is 145 vph ( 14 percent of approach volume) during PM peak hour. Even with a traffic signal installation at the intersection, delay to eastbound through traffic is expected due to queues that form as a result of vehicles slowing or stopping to turn left.

Separate left-turn lanes provide a refuge while waiting for a gap and also reduce conflict between stopped left turning vehicles and through vehicles, thus reducing the potential for rear end crashes.

## OTHER COUNIERMEASURES

## Great Lakes Parkway Intersection

Following improvements to signal operation are recommended for improved efficiency at the intersection of US Route 422 and Great Lakes parkway intersection
> Implement right turn overlap phase for eastbound approaches: Right turn overlap phases will allow right turn movements from US Route 422 to utilize green time allotted to the minor street split phase on Great Lakes Parkway. This countermeasure would require installation of 5 -section signal heads on eastbound approach.
> Install advance detection on Great Lakes Parkway: Green phase on Great Lakes Parkway has full extension time resulting in wasted green time. Install advance detection on Great Lakes parkway approach to reduce lost time on side street.

## Nash Road

The following access management improvements are recommended to mitigate drivewayrelated/minor street related rear-end and sideswipe crashes on US Route 422 near Nash Road.
$>$ Extend left turn lane at the S.R. 700 intersection as a two-way left turn lane to Nash Road. A number of driveways exist within this section of US Route 422, and this improvement will improve safety and operations by separating turning vehicles from through lanes along the corridor. This countermeasure may require additional right of way.


| FORMAL SAFETY STUDY |  |  |  |
| :---: | :---: | :---: | :---: |
| District: 12 | County: Geauga | Route: US-422 | Section: 12.3-12.6 |
| GEA-422 (12.3-12.6) |  |  |  | 2011 Safety Study Analyst Rank \#12 Rural Non-Freeway.

## Background:

Between the years of 2009-2011, there were a total of nine crashes recorded to this section of US-422 causing it to be ranked $12^{\text {th }}$ in the state on the 2011 rural non-freeway list. This high ranking has caused this section of US-422 to be flagged for possible safety concerns. The average daily traffic (ADT) for this section of US-422 is 14,795 . For a visual of the site, see below.


## Existing Conditions:

A crash analysis has been performed to review possible safety concerns associated with Main Market Rd (US-422) between log points 12.3 and 12.6. This section of US-422 begins right after a bridge over the Cuyahoga River and ends almost a half mile west of Claridon Troy Rd (SR-700). At the beginning of this section is the Iron Horse Saloon restaurant. Immediately after the restaurant there is a small curve in the roadway due to a previous realignment of US-422. The previous project added centerline rumble strips and created 12' lanes with 10 ' shoulders. Congestion due to the signal at SR 700 is a suspected contributing factor for crashes that occurred during weekday PM peak hours. See below for a visual of existing sign locations.


## Crash Data:

A crash data analysis was performed to determine if the crashes showed any trends relating to a possible safety concern. The study period used for this crash analysis was 2009-2011. Using the GIS Crash Analysis Tool (GCAT), a query was run from log point 12.3 to log point 12.6 along US-422. The crash rate was then determined using the GCAT Rate Calc Sheet.

The query resulted in nine crashes, which were all reviewed to determine if they were logged correctly. After reviewing the crash reports it was determined that none of the crashes were logged in the correct locations. Of the nine crashes, five were logged to the Iron Horse Saloon driveway and four were logged to a location 0.4 miles east of mile marker 12. Two of the crashes logged to a location of 0.4 miles east of mile marker 12 didn't even occur within the 12.3 to 12.6 search query so they were pulled out of the safety study. Due to the fact that the Iron Horse Saloon has three driveways, it was difficult to determine which driveway the five crashes actually occurred in front of. Therefore, four of the five crashes logged to the Iron Horse Saloon driveway were given the revised log point of the middle driveway. All of the hand logged revisions made in this crash analysis were submitted for review.

| CRASH_SEVERITY | Number | $\%$ |
| :--- | :---: | :---: |
| Injury Crash | 2 | $28.6 \%$ |
| Property Damage Crash | 5 | $71.4 \%$ |
| Grand Total | 7 | $100.0 \%$ |


| TRAFFIC_CRASH_YEAR | Number |  |  |
| :--- | :---: | :---: | :---: |
|  | 2009 | 1 | $14.3 \%$ |
|  | 2010 | 3 | $42.9 \%$ |
|  | 2011 | 3 | $42.9 \%$ |
| Grand Total |  | 7 | $100.0 \%$ |


| DAY_OF_WEEK | Number | $\%$ |
| :--- | :---: | :---: |
| Friday | 4 | $57.1 \%$ |
| Sunday | 2 | $28.6 \%$ |
| Tuesday | 1 | $14.3 \%$ |
| Grand Total | 7 | $100.0 \%$ |


| HOUR_OF_DAY | Number |  |  |
| :--- | ---: | :---: | :---: |
|  | $\mathbf{1}$ | \% |  |
|  | 14 | $\mathbf{2}$ | $14.3 \%$ |
|  | 16 | $\mathbf{1}$ | $14.3 \%$ |
|  | 19 | 2 | $28.6 \%$ |
|  | 20 | $\mathbf{1}$ | $14.3 \%$ |
| Grand Total |  | $\mathbf{7}$ | $\mathbf{1 0 0 . 0 \%}$ |


| TYPE_OF_CRASH | Number | $\%$ |
| :--- | :---: | :---: |
| Rear End | 4 | $57.1 \%$ |
| Fixed Object | 3 | $42.9 \%$ |
| Grand Total | 7 | $100.0 \%$ |


| ROAD_CONDITION | Number | $\%$ |
| :--- | :---: | :---: |
| Road - Dry | 5 | $71.4 \%$ |
| Road - Wet | 2 | $28.6 \%$ |
| Grand Total | 7 | $100.0 \%$ |


| LOCATION | Number | $\%$ |
| :--- | :---: | :---: |
| Driveway/Alley Access | 4 | $57.1 \%$ |
| Not An Intersection | 3 | $42.9 \%$ |
| Grand Total | 7 | $100.0 \%$ |


(See Appendix A for the complete 6 page CAM Tool Data Analysis Summary)

## Observations:

- Crash Type
o 4 (57.1\%) Rear end collisions.
o 3 (42.9\%) Fixed object collisions.
- 2 of the 3 fixed object crashes involved guardrail.
- Road Condition

$$
\begin{array}{ll}
\mathrm{o} & 5 \text { (71.4\%) Dry. } \\
\mathrm{o} & 2 \text { (28.6\%) Wet. }
\end{array}
$$

- Direction
o 5 (71.4\%) East.
o 2 (28.6\%) West.


## Results:

- While using pathweb and going west on US-422, congestion was observed on US-422 East. The backup went from the intersection of US-422 and SR-700 all the way back to the Iron Horse Saloon. This distance is greater than a half mile and could cause problems with the curve visibility.
- Both of the crashes in the westbound direction occurred at the end of the curve and involved a guardrail. There is a curve warning sign and chevrons currently in place for westbound traffic approaching this curve. Therefore, lack of adequate warning does not appear to have been the cause of the westbound crashes.
- Of the crashes going eastbound, one crash occurred during peak hour traffic and the crash report mentions the presence of congestion. However, this is the only crash that occurred during the evening peak hours, so congestion does not appear to play a big role in these crashes.
- All four of the eastbound crashes logged to the middle driveway of the Iron Horse Saloon involved left turns into the restaurants parking lot. One driver made a bad turn and ended up in a ditch. Two of the crashes happened as a result of drivers not slowing down enough when a vehicle in front of them was making a left turn into the Iron Horse Saloon. One of the crashes happened because a driver did not slow down fast enough after one of the previously mentioned crashes occurred. Therefore, two of the crashes actually refer to the same incident. Sight distance should not play a role in these crashes because they occur on a straight and flat section of roadway and they did not occur during a time when the queue from SR-700 may have been a contributing factor.
- Due to the small number of crashes within the initial query, no trends were identifed. In order to gain a better idea of what is happening on this section of US-422, another query was run from the bridge all the way to the intersection of SR-700. A total of 25 crashes occurred between the bridge and the intersection with SR-700. Of the 25 crashes, 14 were rear ends. 13 of those 14 crashes occurred in the eastbound direction. The existing signal at SR 700 is over-capacity, resulting in long queues and delays for EB drivers during the PM peak hours. Queuing from SR 700 does not appear to be a major factor in the crashes between SLM 12.3-12.6.


## Crash Rate:



## Recommendations:

The review of accident reports in this segment did not identify a consistent trend among crashes observed. The appearance of this location on the 2011 rural non-freeway priority list appears to be an anomaly. District will monitor the site.

A long-term recommendation is to work with the owner of the Iron Horse Saloon to consolidate access points.

## Countermeasures and Implementation Plan

No corrective action is recommended at this time. The appearance of this location on the 2011 Rural Non-Freeway priority list appears to be an anomaly. District will continue to monitor the site on future Safety Priority Lists.

To: Ohio Department of Transportation, District 12
From: HNTB Ohio, Inc.
Re: GEA 422/700 Intersection Capacity Analysis
Date: June 2007

At the request of District 12 of the Ohio Department of Transportation, HNTB has conducted an Intersection Capacity Analysis for the intersection US 422 and SR 700 in Geauga County, Ohio. The purpose of this study is to identify possible capacity improvements at the US 422/SR 700 intersection and suggest actions that can be taken to improve operation. A location map of the site and surrounding area is included as Page 2.

## Existing Conditions

On March 29, 2007 a field visit was performed, the existing conditions were observed and photographs were taken of each approach and are included in Attachment A.
US 422 is a rural principle arterial and SR 700 is a rural collector roadway. They both are two lane roadways (one lane in each direction) with a posted speed limit of 45 mph within the study area. The intersection is currently signalized with two-phase operation. A school zone is located on SR 700 just to the south of the intersection.

There is a high volume of trucks on US 422 passing through the intersection, approximately 15\% throughout the day. All four corners of the intersection show evidence of truck tire tracks leaving the paved surface while attempting to negotiate right turns. There is a structure on the southwest corner of the intersection located close to the right of way.

## Future Traffic

ODOT's Office of Technical Services certified 2010 and 2030 traffic for the intersection which is included as Attachment B. Design year traffic (2030) was used for the capacity analysis for this study. Figure 2 below shows the AM and PM peak period traffic volumes.

Figure 2 - Design Year Traffic Volumes - AM (PM)


FIGURE 1: STUDY AREA


## GEAUGA COUNTY




## Alternatives

Two alternatives with multiple signal phasing options and the no build condition were examined at this intersection. Table 1 below describes the geometry and signal operation of each of the alternatives. Alternatives 2 and 3 were run with the existing 2 -phase signal operation as well as protected/permitted left turn schemes. Schematic figures of each alternative are included as Attachment C. Capacity (Attachment D), storage lane lengths (Attachment E), right of way impacts, and construction cost magnitude were examined for each alternative. These are summarized in the evaluation matrix included as

## Attachment F .

Table 1: Alternatives

|  | Description | Signal Operation |
| :--- | :--- | :--- |
| Alternative 1 | Existing geometry | $\bullet$ 2-phase |
| Alternative 2 | Add EB, WB left turn lanes | $\bullet$ 2-phase <br> $\bullet$ Lead EB movement |
| Alternative 3 | Add left turn lanes all approaches | $\bullet$ 2-phase <br> $\bullet$ Lead EB and Lead NB movements |

## Alternative 1

Alternative 1 is the current condition. With existing geometry and 2 -phase signal operation, the overall intersection currently operates at LOS $D$ in the AM peak period and LOS D in the PM peak period. During the PM peak period, both the northbound and eastbound movements operate at LOS E. Safety is likely declining due to the lack of left turn lanes. Since this alternative is the no build condition, there would be no right of way costs and construction involvement is none.

## Alternative 2

Alternative 2 widens the pavement on US 422 to include left turn lanes on both the eastbound and westbound approaches. When run with 2-phase signal operation, the LOS is improved slightly (LOS D-AM peak period, LOS D - PM peak period) when compared to the existing condition. If phased with a leading eastbound movement the LOS declines for the AM peak period to LOS E with westbound thru-right movement and northbound movement operating at LOS E, but improves for the PM peak period to LOS C. With this alternative, safety is improved along US 422 since the left turn lanes along US 422 allow the turning vehicles to line up with opposing turning vehicles and they are removed from the thru lanes. Also, proper turning radii are provided at the corners to accommodate trucks. However, with this improvement, two structure or total takes are required and another two partial right of way takes would be required. Construction involvement for this alternative is mid-range.

## Alternative 3

Alternative 3 widens the pavement on both US 422 and SR 700 to include left turn lanes on all approaches. When run with 2-phase signal operation, the LOS is improved (LOS C - AM peak period, LOS C - PM peak period) when compared to the existing condition. If phased with a leading eastbound movement and leading northbound movement, the LOS is similar to the existing with LOS D in both AM and PM peak periods. With this alternative, safety is improved along both roadways since the left turn lanes along US 422 and SR 700 allow the turning vehicles to line up with opposing turning vehicles and they are removed from the thru lanes. Also, proper turning radii are provided at the corners to accommodate trucks. However, with this improvement, three structure or total takes are required and another two partial right of way takes would be required. Construction involvement for this alternative is high.



MEMO

| To: | Brian Blayney |
| :--- | :--- |
| From: | Beth Sliemers. Scott Knebel |
| Date: | October 10, 2014 |
| Subject: | Preliminary analysis and recommendations for US-422 and Rapids Road |
| Project \#: | $0107585 A .13$ |

The following serves as a summary of preliminary findings and recommendations for the intersection of US-422 and Rapids Road. LJB has prepared preliminary analyses including signal warrants and intersection capacity analysis. These results and recommendations will be included as part of a formal report for GEA-422-10.93/13.31.

## Existing Conditions

The US-422/Rapids Road intersection is a two-way, stop controlled intersection with Rapids Road as the stop controlled approaches. There is a single lane on all approaches. The posted speed limit on US-422 is 45 miles per hour. Turn count data was supplied by ODOT using Miovision technology. Field observations from October 1, 2014 indicate that the longest queue on Rapids Road was four vehicles with the queue duration of three minutes.

## Crash Evaluation

A total of 20 crashes were reported at the US-422/Rapids Road intersection during a three-year analysis period between January 1, 2011 and December 31, 2013. Of the total crashes, 30 percent resulted in injury. The most prevalent patterns are seven eastbound rear end crashes involving through vehicles stopped behind left turning vehicles and four right angle crashes involving vehicles entering US-422 from Rapids Road. A crash diagram for the US-422/Rapids Road intersection is attached to this memo.

## Traffic Signal Warrants

Traffic signal warrants were evaluated at the US-422/Rapids Road intersection to determine if signalization is warranted with current traffic volumes. Counted traffic volumes were evaluated against the warrants described below, as outlined in Section 4C of the Ohio Manual of Uniform Traffic Control Devices (OMUTCD). The warrants for US-422/Rapids Road were evaluated with the $70 \%$ factor applicable for roadways with posted speed limits greater than 40 MPH. Both US-422 and Rapids Road were evaluated as single-lane approaches. A reduction in right turning volume from the side street was not applied since the existing lane geometry consists of a single, shared lane. Detailed signal warrant worksheets are attached to this memo.

Warrant 1, Eight-Hour Vehicular Volume: The eight-hour warrant requires that for each of any 8 hours of an average day, volumes on both the major and minor street exceed minimum thresholds. The Rapids Road intersection does not satisfy requirements to meet the eight-hour warrant.

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Warrant 2, Four-Hour Vehicular Volume: The four-hour warrant requires that for each of any 4 hours of an average day, volumes on both the major and minor street fall above the applicable curve in Figure 4C-1 (for speeds less than 40 MPH ) or 4C-2 (for speeds greater than 40 MPH ). As shown below in Graph 1, the minimum volume for a one-lane, minor street approach is 60 vehicles per hour. Rapids Road approach volumes exceed the 60 vph threshold during the 6AM hour ( 75 vph ), the 7AM hour ( 73 vph ) and the 4:30 PM hour ( 68 vph ). The 3:30 PM hour approach volume of 59 vph is only 1 vehicle shy of the threshold. Based on these findings, it is concluded that the Rapids Road intersection satisfies four-hour signal warrant requirements.

## Graph 1: Four-Hour Signal Warrant Graph (4C-2)



Warrant 3, peak hour volume: The peak hour warrant requires that for any single hour of an average day, volumes on both the major and minor street fall above the applicable curve in Figure $4 \mathrm{C}-3$ (for speeds less than 40 MPH ) or 4C-4 (for speeds greater than 40 MPH ). As shown in Figure 2, the minimum volume for a one-lane, minor street approach is 75 vehicles per hour. The Rapids Road approach volume meets the 75 vph threshold during the 6AM hour ( 75 vph ). Based on this finding, it is concluded that the Rapids Road intersection satisfies peak hour signal warrant requirements.

Warrant 7, Crash Experience: The crash experience warrant requires that for any twelve month period, there must be five or more reported crashes involving personal injury or property damage that are susceptible to correction by signalization. In addition, for each of any eight hours of an average day, volumes on the major and minor street exceed minimum thresholds. The Rapids Road intersection does not satisfy requirements to meet the crash history warrant.

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Figure 2: Peak Hour Signal Warrant Graph


## Capacity Analysis

Field observations noted high vehicular delay on Rapids Road during peak hours, attributed to infrequent gaps in mainline traffic. Intersection capacity was evaluated with the assistance of Synchro traffic simulation software using counted traffic volumes. The northbound and southbound stop-controlled approaches operate at level of service F during the afternoon peak hour with average vehicle delays of 208 seconds for the northbound approach and 107 seconds for the southbound approach.

The following conditions were evaluated assuming signalization of the Rapids Road intersection:

- 2-phase signal operation (no left turn lanes on US-422): This condition represents the addition of a 2-phase traffic signal with no other changes to the existing condition.
- 3-phase signal operation (leading EB phase, no left turn lanes on US-422: During the PM peak hour, the demand volume for the eastbound approach is 1,008 vehicles per hour, compared to 461 vph for the westbound approach, 17 for the northbound approach and 57 for the southbound approach. Given the high eastbound demand volume coupled with an eastbound left turn demand of 145 vph , a leading eastbound left turn phase was modeled to more efficiently clear eastbound queues that could form at the signalized intersection.
- 2-phase signal operation with left turn lanes on US-422: The addition of left turn lanes on US-422 was evaluated to determine the level of benefit provided by dedicated left turn storage.

Capacity analysis results for the PM peak hour are summarized below in Table 1. Note that results reflect Synchro optimized green time splits. The critical approach delay balancing method was not used. Output reports reflective of HCM 2010 algorithms and Synchro reports with phasing/timing information are attached to this memo.

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Table 1: Capacity analysis results


Note: Letter/Number - Level of Service/Average Delay per Vehicle
As supported by field observation, the existing condition capacity analysis shows long delay on Rapids Road during peak hours. Analysis shows that a traffic signal will mitigate this delay.

Eastbound left turn volumes are high during the PM peak hour (145 vehicles). Without dedicated storage for left turning vehicles, even one left turning vehicle stopped in the single approach lane waiting for a gap in approaching traffic will block through traffic from traversing the intersection. This condition will increase delay and vehicle queue lengths. A leading eastbound phase is recommended to provide protected green time to service all eastbound traffic which may reduce queuing on the eastbound approach. For this reason, three phase signal operation is recommended if left turn lanes are not constructed on US-422.

If left turn lanes are installed at the intersection, a two phase signal is sufficient for both the AM and PM peak hours. This configuration yields the lowest overall delay and all movements operate at a level of service of C or better.

## Queue Analysis

In the existing stop controlled condition, the expected $95^{\text {th }}$ percentile queue length is 290 feet for the eastbound approach. An evaluation of vehicle queue lengths was conducted for the three variations of traffic signal control described in the capacity analysis section. Introducing a stop condition on US-422 which is inherent to the traffic signal operation may increase queue lengths of US-422. Queue length results are summarized below in Table 2.

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Table 2: $95^{\text {th }}$ percentile queue length results

|  | AM PEAK HOUR |  |  |  | PM PEAK HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { T } \\ & \frac{1}{6} \\ & 0 \\ & \frac{1 \pi}{4} \\ & \frac{1}{4} \\ & \text { H } \end{aligned}$ | 7 0 0 0 0 6 $\frac{1}{4}$ 0 8 | $\begin{aligned} & \frac{1}{0} \\ & \frac{1}{0} \\ & \frac{4}{4} \\ & \frac{1}{4} \\ & \frac{0}{2} \end{aligned}$ |  | $T$ 0 0 0 0 6 6 0 0 | 7 0 0 0 4 $\frac{1}{4}$ 0 3 3 | $\begin{aligned} & \frac{1}{0} \\ & \frac{1}{0} \\ & \frac{4}{4} \\ & \frac{1}{4} \\ & \frac{m}{2} \end{aligned}$ | $\begin{aligned} & \text { T } \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \frac{1}{4} \\ & \frac{1}{4} \\ & 0 \\ & 0 \end{aligned}$ |
| US-422 \& Rapids Rd |  |  |  |  |  |  |  |  |
| Existing Condition (Stop Control) | 115 | 20 | 50 | 60 | 290 | 180 | 60 | 80 |
| Two-Phase Signal | 190 | 210 | 65 | 75 | 410 | 210 | 35 | 100 |
| Three-Phase Signal | 165 | 420 | 75 | 100 | 445 | 285 | 40 | 90 |
| Two-Phase Signal w/ Left Turn Storage | 100 | 210 | 60 | 80 | 205 | 235 | 30 | 85 |

Note: Values given reflect 95th percentile queues measured in feet

Expected queue lengths are greatest during the PM peak hour when demand volumes on US-422 are the highest. With a 2-phase signal and no left turn lanes, the eastbound queue length exceeds 400 feet. While the simulation model with the leading eastbound phase indicates no significant change in the eastbound queue length compared to a 2-phase operation, experiences with similar sites suggests that the model output may be underestimating the effect of left turn blocking conditions. For this reason, a 3-phase signal operation is recommended. The addition of left turn lanes on US-422 is expected to reduce the eastbound queue length to less than the existing condition (with 2-phase operation).

## Recommendations

A traffic signal is recommended at the US-422/Rapids Road intersection to decrease vehicle delay and mitigate rear end and angle crashes within the intersection. In the absence of left turn lanes on US-422, a three-phase signal operation is recommended to provide a leading eastbound phase to better accommodate the eastbound left turn demand and reduce queueing potential. If dedicated left turn lanes are constructed on US-422, then a two-phase signal operation is sufficient.

Please feel free to contract me with questions or for further discussion. I can be reached at (937) 2595165 or by email at bsliemers@ljbinc.com.


Ohio Department of Transportation 1980 West Broad Street

Columbus, Ohio, United States 43223
16147528099 Stephanie.Marik@dot.state.oh.us

| Start Time | Turning Movement Data |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Westbound Approach |  |  |  | Northbound Approach |  |  |  | Eastbound Approach |  |  |  | Int. Total |
|  | Thru | Left | U-Turn | App. Total | Right | Left | U-Turn | App. Total | Right | Thru | U-Turn | App. Total |  |
| 6:00 AM | 191 | 18 | 0 | 209 | 30 | 5 | 0 | 35 | 5 | 55 | 0 | 60 | 304 |
| 6:15 AM | 220 | 22 | 0 | 242 | 3 | 1 | 0 | 4 | 8 | 56 | 0 | 64 | 310 |
| 6:30 AM | 233 | 51 | 0 | 284 | 4 | 3 | 0 | 7 | 16 | 62 | 0 | 78 | 369 |
| 6:45 AM | 221 | 34 | 0 | 255 | 11 | 2 | 0 | 13 | 15 | 85 | 0 | 100 | 368 |
| Hourly Total | 865 | 125 | 0 | 990 | 48 | 11 | 0 | 59 | 44 | 258 | 0 | 302 | 1351 |
| 7:00 AM | 233 | 8 | 0 | 241 | 79 | 4 | 0 | 83 | 5 | 74 | 0 | 79 | 403 |
| 7:15 AM | 218 | 11 | 0 | 229 | 4 | 1 | 0 | 5 | 16 | 86 | 0 | 102 | 336 |
| 7:30 AM | 228 | 11 | 0 | 239 | 3 | 1 | 0 | 4 | 12 | 107 | 0 | 119 | 362 |
| 7:45 AM | 185 | 12 | 0 | 197 | 1 | 2 | 0 | 3 | 23 | 97 | 0 | 120 | 320 |
| Hourly Total | 864 | 42 | 0 | 906 | 87 | 8 | 0 | 95 | 56 | 364 | 0 | 420 | 1421 |
| 8:00 AM | 192 | 11 | 0 | 203 | 0 | 0 | 0 | 0 | 11 | 80 | 0 | 91 | 294 |
| 8:15 AM | 147 | 8 | 0 | 155 | 2 | 9 | 0 | 11 | 18 | 97 | 0 | 115 | 281 |
| 8:30 AM | 153 | 3 | 0 | 156 | 1 | 6 | 0 | 7 | 10 | 87 | 0 | 97 | 260 |
| 8:45 AM | 114 | 6 | 0 | 120 | 2 | 4 | 0 | 6 | 11 | 79 | 0 | 90 | 216 |
| Hourly Total | 606 | 28 | 0 | 634 | 5 | 19 | 0 | 24 | 50 | 343 | 0 | 393 | 1051 |
| 9:00 AM | 129 | 2 | 0 | 131 | 2 | 5 | 0 | 7 | 7 | 76 | 0 | 83 | 221 |
| 9:15 AM | 106 | 6 | 0 | 112 | 3 | 4 | 0 | 7 | 7 | 96 | 0 | 103 | 222 |
| 9:30 AM | 102 | 3 | 0 | 105 | 3 | 4 | 0 | 7 | 6 | 92 | 0 | 98 | 210 |
| 9:45 AM | 78 | 0 | 0 | 78 | 1 | 7 | 0 | 8 | 3 | 69 | 0 | 72 | 158 |
| Hourly Total | 415 | 11 | 0 | 426 | 9 | 20 | 0 | 29 | 23 | 333 | 0 | 356 | 811 |
| 10:00 AM | 68 | 3 | 0 | 71 | 1 | 7 | 0 | 8 | 6 | 93 | 0 | 99 | 178 |
| 10:15 AM | 103 | 3 | 0 | 106 | 3 | 2 | 0 | 5 | 2 | 78 | 0 | 80 | 191 |
| 10:30 AM | 95 | 3 | 0 | 98 | 4 | 8 | 0 | 12 | 10 | 110 | 0 | 120 | 230 |
| 10:45 AM | 76 | 5 | 0 | 81 | 4 | 11 | 1 | 16 | 6 | 65 | 0 | 71 | 168 |
| Hourly Total | 342 | 14 | 0 | 356 | 12 | 28 | 1 | 41 | 24 | 346 | 0 | 370 | 767 |
| 11:00 AM | 83 | 1 | 0 | 84 | 6 | 3 | 0 | 9 | 3 | 79 | 0 | 82 | 175 |
| 11:15 AM | 68 | 2 | 0 | 70 | 7 | 9 | 0 | 16 | 3 | 92 | 0 | 95 | 181 |
| 11:30 AM | 83 | 6 | 0 | 89 | 3 | 4 | 0 | 7 | 3 | 84 | 0 | 87 | 183 |
| 11:45 AM | 83 | 5 | 0 | 88 | 3 | 7 | 0 | 10 | 8 | 91 | 0 | 99 | 197 |
| Hourly Total | 317 | 14 | 0 | 331 | 19 | 23 | 0 | 42 | 17 | 346 | 0 | 363 | 736 |
| 12:00 PM | 98 | 5 | 0 | 103 | 9 | 15 | 0 | 24 | 5 | 95 | 0 | 100 | 227 |
| 12:15 PM | 87 | 7 | 0 | 94 | 4 | 7 | 0 | 11 | 11 | 85 | 0 | 96 | 201 |
| 12:30 PM | 90 | 5 | 0 | 95 | 8 | 4 | 0 | 12 | 6 | 113 | 0 | 119 | 226 |
| 12:45 PM | 81 | 12 | 0 | 93 | 2 | 4 | 0 | 6 | 11 | 98 | 0 | 109 | 208 |
| Hourly Total | 356 | 29 | 0 | 385 | 23 | 30 | 0 | 53 | 33 | 391 | 0 | 424 | 862 |
| 1:00 PM | 81 | 14 | 0 | 95 | 4 | 3 | 0 | 7 | 5 | 101 | 0 | 106 | 208 |
| 1:15 PM | 97 | 14 | 0 | 111 | 7 | 4 | 0 | 11 | 10 | 106 | 0 | 116 | 238 |


| 1:30 PM | 86 | 13 | 0 | 99 | 3 | 3 | 0 | 6 | 10 | 94 | 0 | 104 | 209 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1:45 PM | 102 | 19 | 0 | 121 | 11 | 12 | 0 | 23 | 6 | 101 | 0 | 107 | 251 |
| Hourly Total | 366 | 60 | 0 | 426 | 25 | 22 | 0 | 47 | 31 | 402 | 0 | 433 | 906 |
| 2:00 PM | 91 | 19 | 0 | 110 | 28 | 11 | 0 | 39 | 7 | 106 | 0 | 113 | 262 |
| 2:15 PM | 112 | 28 | 0 | 140 | 12 | 4 | 0 | 16 | 8 | 127 | 0 | 135 | 291 |
| 2:30 PM | 97 | 28 | 0 | 125 | 13 | 11 | 0 | 24 | 8 | 128 | 0 | 136 | 285 |
| 2:45 PM | 101 | 15 | 0 | 116 | 11 | 10 | 0 | 21 | 2 | 147 | 0 | 149 | 286 |
| Hourly Total | 401 | 90 | 0 | 491 | 64 | 36 | 0 | 100 | 25 | 508 | 0 | 533 | 1124 |
| 3:00 PM | 87 | 2 | 0 | 89 | 80 | 20 | 0 | 100 | 2 | 154 | 0 | 156 | 345 |
| 3:15 PM | 98 | 4 | 0 | 102 | 22 | 7 | 0 | 29 | 6 | 193 | 0 | 199 | 330 |
| 3:30 PM | 116 | 3 | 0 | 119 | 30 | 17 | 0 | 47 | 4 | 199 | 0 | 203 | 369 |
| 3:45 PM | 93 | 0 | 0 | 93 | 4 | 10 | 0 | 14 | 0 | 218 | 0 | 218 | 325 |
| Hourly Total | 394 | 9 | 0 | 403 | 136 | 54 | 0 | 190 | 12 | 764 | 0 | 776 | 1369 |
| 4:00 PM | 116 | 3 | 0 | 119 | 11 | 8 | 0 | 19 | 2 | 262 | 0 | 264 | 402 |
| 4:15 PM | 103 | 0 | 0 | 103 | 11 | 8 | 0 | 19 | 0 | 255 | 0 | 255 | 377 |
| 4:30 PM | 91 | 1 | 0 | 92 | 17 | 17 | 0 | 34 | 2 | 238 | 0 | 240 | 366 |
| 4:45 PM | 107 | 3 | 0 | 110 | 7 | 9 | 0 | 16 | 1 | 222 | 0 | 223 | 349 |
| Hourly Total | 417 | 7 | 0 | 424 | 46 | 42 | 0 | 88 | 5 | 977 | 0 | 982 | 1494 |
| 5:00 PM | 124 | 0 | 0 | 124 | 34 | 31 | 0 | 65 | 2 | 236 | 0 | 238 | 427 |
| 5:15 PM | 133 | 1 | 0 | 134 | 7 | 24 | 0 | 31 | 3 | 240 | 0 | 243 | 408 |
| 5:30 PM | 123 | 1 | 0 | 124 | 2 | 9 | 0 | 11 | 1 | 313 | 0 | 314 | 449 |
| 5:45 PM | 102 | 0 | 0 | 102 | 2 | 6 | 0 | 8 | 3 | 204 | 0 | 207 | 317 |
| Hourly Total | 482 | 2 | 0 | 484 | 45 | 70 | 0 | 115 | 9 | 993 | 0 | 1002 | 1601 |
| 6:00 PM | 103 | 2 | 0 | 105 | 2 | 9 | 0 | 11 | 2 | 211 | 0 | 213 | 329 |
| 6:15 PM | 96 | 1 | 0 | 97 | 0 | 2 | 0 | 2 | 0 | 177 | 0 | 177 | 276 |
| 6:30 PM | 71 | 2 | 0 | 73 | 2 | 4 | 0 | 6 | 0 | 132 | 0 | 132 | 211 |
| 6:45 PM | 65 | 3 | 0 | 68 | 2 | 1 | 0 | 3 | 1 | 113 | 0 | 114 | 185 |
| Hourly Total | 335 | 8 | 0 | 343 | 6 | 16 | 0 | 22 | 3 | 633 | 0 | 636 | 1001 |
| Grand Total | 6160 | 439 | 0 | 6599 | 525 | 379 | 1 | 905 | 332 | 6658 | 0 | 6990 | 14494 |
| Approach \% | 93.3 | 6.7 | 0.0 | - | 58.0 | 41.9 | 0.1 | - | 4.7 | 95.3 | 0.0 | - | - |
| Total \% | 42.5 | 3.0 | 0.0 | 45.5 | 3.6 | 2.6 | 0.0 | 6.2 | 2.3 | 45.9 | 0.0 | 48.2 | - |
| Lights | 5364 | 377 | 0 | 5741 | 460 | 295 | 1 | 756 | 258 | 5862 | 0 | 6120 | 12617 |
| \% Lights | 87.1 | 85.9 | - | 87.0 | 87.6 | 77.8 | 100.0 | 83.5 | 77.7 | 88.0 | - | 87.6 | 87.0 |
| Mediums | 216 | 19 | 0 | 235 | 18 | 21 | 0 | 39 | 21 | 255 | 0 | 276 | 550 |
| \% Mediums | 3.5 | 4.3 | - | 3.6 | 3.4 | 5.5 | 0.0 | 4.3 | 6.3 | 3.8 | - | 3.9 | 3.8 |
| Articulated Trucks | 580 | 43 | 0 | 623 | 47 | 63 | 0 | 110 | 53 | 541 | 0 | 594 | 1327 |
| \% Articulated Trucks | 9.4 | 9.8 | - | 9.4 | 9.0 | 16.6 | 0.0 | 12.2 | 16.0 | 8.1 | - | 8.5 | 9.2 |

Ohio Department of Transportation
1980 West Broad Street
Mail Stop 5160
Columbus, Ohio, United States 43223 +16147528099 Stephanie.Marik@dot.state.oh.us

Office of Traffic Engineering

Turning Movement Data Plot


Count Name: GEA-422 @ Great Lakes Parkway TMC
Site Code: 0 Start Date: 09/09/2014
Page No: 3

Ohio Department of Transportation 1980 West Broad Street
Columbus, Ohio, United States 43223 +16147528099 Stephanie.Marik@dot.state.oh.us Office of Traffic Engineering

Count Name: GEA-422 @ Great Lakes Parkway TMC
Start Date: 09/09/2014
Page No: 4

Turning Movement Peak Hour Data (6:30 AM)

| Start Time | Westbound Approach Westbound |  |  |  | Northbound Approach Northbound |  |  |  | Eastbound Approach Eastbound |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thru | Left | U-Turn | App. Total | Right | Left | U-Turn | App. Total | Right | Thru | U-Turn | App. Total |  |
| 6:30 AM | 233 | 51 | 0 | 284 | 4 | 3 | 0 | 7 | 16 | 62 | 0 | 78 | 369 |
| 6:45 AM | 221 | 34 | 0 | 255 | 11 | 2 | 0 | 13 | 15 | 85 | 0 | 100 | 368 |
| 7:00 AM | 233 | 8 | 0 | 241 | 79 | 4 | 0 | 83 | 5 | 74 | 0 | 79 | 403 |
| 7:15 AM | 218 | 11 | 0 | 229 | 4 | 1 | 0 | 5 | 16 | 86 | 0 | 102 | 336 |
| Total | 905 | 104 | 0 | 1009 | 98 | 10 | 0 | 108 | 52 | 307 | 0 | 359 | 1476 |
| Approach \% | 89.7 | 10.3 | 0.0 | - | 90.7 | 9.3 | 0.0 | - | 14.5 | 85.5 | 0.0 | - | - |
| Total \% | 61.3 | 7.0 | 0.0 | 68.4 | 6.6 | 0.7 | 0.0 | 7.3 | 3.5 | 20.8 | 0.0 | 24.3 | - |
| PHF | 0.971 | 0.510 | 0.000 | 0.888 | 0.310 | 0.625 | 0.000 | 0.325 | 0.813 | 0.892 | 0.000 | 0.880 | 0.916 |
| Lights | 856 | 102 | 0 | 958 | 97 | 7 | 0 | 104 | 51 | 255 | 0 | 306 | 1368 |
| \% Lights | 94.6 | 98.1 | - | 94.9 | 99.0 | 70.0 | - | 96.3 | 98.1 | 83.1 | - | 85.2 | 92.7 |
| Mediums | 16 | 2 | 0 | 18 | 0 | 1 | 0 | 1 | 1 | 14 | 0 | 15 | 34 |
| \% Mediums | 1.8 | 1.9 | - | 1.8 | 0.0 | 10.0 | - | 0.9 | 1.9 | 4.6 | - | 4.2 | 2.3 |
| Articulated Trucks | 33 | 0 | 0 | 33 | 1 | 2 | 0 | 3 | 0 | 38 | 0 | 38 | 74 |
| \% Articulated Trucks | 3.6 | 0.0 | - | 3.3 | 1.0 | 20.0 | - | 2.8 | 0.0 | 12.4 | - | 10.6 | 5.0 |

Ohio Department of Transportation
1980 West Broad Street
Mail Stop 5160
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Office of Traffic Engineering

Turning Movement Peak Hour Data Plot (6:30 AM)


Count Name: GEA-422 @ Great Lakes Parkway TMC
Start Date: 09/09/2014
Start Date:

Ohio Department of Transportation 1980 West Broad Street

Columbus, Ohio, United States 43223 +16147528099 Stephanie.Marik@dot.state.oh.us Office of Traffic Engineering

Count Name: GEA-422 @ Great Lakes Parkway TMC
Start Date: 09/09/2014
Page No: 6

Turning Movement Peak Hour Data (4:45 PM)

| Start Time | Westbound Approach Westbound |  |  |  | Northbound Approach Northbound |  |  |  | Eastbound Approach Eastbound |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thru | Left | U-Turn | App. Total | Right | Left | U-Turn | App. Total | Right | Thru | U-Turn | App. Total |  |
| 4:45 PM | 107 | 3 | 0 | 110 | 7 | 9 | 0 | 16 | 1 | 222 | 0 | 223 | 349 |
| 5:00 PM | 124 | 0 | 0 | 124 | 34 | 31 | 0 | 65 | 2 | 236 | 0 | 238 | 427 |
| 5:15 PM | 133 | 1 | 0 | 134 | 7 | 24 | 0 | 31 | 3 | 240 | 0 | 243 | 408 |
| 5:30 PM | 123 | 1 | 0 | 124 | 2 | 9 | 0 | 11 | 1 | 313 | 0 | 314 | 449 |
| Total | 487 | 5 | 0 | 492 | 50 | 73 | 0 | 123 | 7 | 1011 | 0 | 1018 | 1633 |
| Approach \% | 99.0 | 1.0 | 0.0 | - | 40.7 | 59.3 | 0.0 | - | 0.7 | 99.3 | 0.0 | - | - |
| Total \% | 29.8 | 0.3 | 0.0 | 30.1 | 3.1 | 4.5 | 0.0 | 7.5 | 0.4 | 61.9 | 0.0 | 62.3 | - |
| PHF | 0.915 | 0.417 | 0.000 | 0.918 | 0.368 | 0.589 | 0.000 | 0.473 | 0.583 | 0.808 | 0.000 | 0.811 | 0.909 |
| Lights | 438 | 3 | 0 | 441 | 50 | 71 | 0 | 121 | 6 | 970 | 0 | 976 | 1538 |
| \% Lights | 89.9 | 60.0 | - | 89.6 | 100.0 | 97.3 | - | 98.4 | 85.7 | 95.9 | - | 95.9 | 94.2 |
| Mediums | 13 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 19 | 0 | 19 | 32 |
| \% Mediums | 2.7 | 0.0 | - | 2.6 | 0.0 | 0.0 | - | 0.0 | 0.0 | 1.9 | - | 1.9 | 2.0 |
| Articulated Trucks | 36 | 2 | 0 | 38 | 0 | 2 | 0 | 2 | 1 | 22 | 0 | 23 | 63 |
| \% Articulated Trucks | 7.4 | 40.0 | - | 7.7 | 0.0 | 2.7 | - | 1.6 | 14.3 | 2.2 | - | 2.3 | 3.9 |

Ohio Department of Transportation
1980 West Broad Street
Mail Stop 5160
Columbus, Ohio, United States 43223 +16147528099 Stephanie.Marik@dot.state.oh.us

Office of Traffic Engineering

Turning Movement Peak Hour Data Plot (4:45 PM)


Count Name: GEA-422 @ Great Lakes Parkway TMC
Site Code: 0 Start Date: 09/09/2014
Page No: 7

Ohio Department of Transportation 1980 West Broad Stree

Columbus, Ohio, United States 43223 +16147528099 ' Stephanie.Marik@dot.state.oh.us Site Code:
Start Date: 09/09/2014
Office of Traffic Engineering
Page No:

Turning Movement Data


| 1:30 PM | 6 | 0 | 0 | 0 | 6 | 0 | 105 | 1 | 0 | 106 | 1 | 1 | 1 | 0 | 3 | 3 | 77 | 12 | 0 | 92 | 207 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1:45 PM | 5 | 2 | 1 | 0 | 8 | 2 | 105 | 2 | 0 | 109 | 0 | 0 | 4 | 0 | 4 | 5 | 96 | 13 | 0 | 114 | 235 |
| Hourly Total | 25 | 8 | 2 | 0 | 35 | 2 | 402 | 5 | 0 | 409 | 1 | 6 | 8 | 0 | 15 | 19 | 357 | 49 | 0 | 425 | 884 |
| 2:00 PM | 7 | 2 | 1 | 0 | 10 | 0 | 111 | 5 | 0 | 116 | 3 | 2 | 3 | 0 | 8 | 5 | 125 | 7 | 0 | 137 | 271 |
| 2:15 PM | 15 | 1 | 1 | 0 | 17 | 2 | 124 | 0 | 0 | 126 | 1 | 1 | 2 | 0 | 4 | 3 | 126 | 12 | 0 | 141 | 288 |
| 2:30 PM | 6 | 1 | 1 | 0 | 8 | 0 | 115 | 3 | 0 | 118 | 1 | 3 | 2 | 0 | 6 | 1 | 116 | 19 | 0 | 136 | 268 |
| 2:45 PM | 7 | 4 | 1 | 0 | 12 | 1 | 94 | 2 | 0 | 97 | 1 | 1 | 1 | 0 | 3 | 3 | 151 | 15 | 0 | 169 | 281 |
| Hourly Total | 35 | 8 | 4 | 0 | 47 | 3 | 444 | 10 | 0 | 457 | 6 | 7 | 8 | 0 | 21 | 12 | 518 | 53 | 0 | 583 | 1108 |
| 3:00 PM | 11 | 2 | 2 | 0 | 15 | 3 | 81 | 0 | 0 | 84 | 0 | 3 | 1 | 0 | 4 | 10 | 193 | 28 | 0 | 231 | 334 |
| 3:15 PM | 10 | 2 | 0 | 0 | 12 | 0 | 86 | 0 | 0 | 86 | 3 | 0 | 2 | 0 | 5 | 13 | 192 | 16 | 0 | 221 | 324 |
| 3:30 PM | 14 | 0 | 2 | 0 | 16 | 3 | 108 | 0 | 0 | 111 | 1 | 1 | 0 | 0 | 2 | 12 | 185 | 30 | 0 | 227 | 356 |
| 3:45 PM | 10 | 2 | 1 | 0 | 13 | 0 | 70 | 0 | 0 | 70 | 1 | 1 | 2 | 0 | 4 | 10 | 199 | 24 | 0 | 233 | 320 |
| Hourly Total | 45 | 6 | 5 | 0 | 56 | 6 | 345 | 0 | 0 | 351 | 5 | 5 | 5 | 0 | 15 | 45 | 769 | 98 | 0 | 912 | 1334 |
| 4:00 PM | 11 | 4 | 2 | 0 | 17 | 4 | 108 | 5 | 0 | 117 | 3 | 2 | 6 | 0 | 11 | 14 | 210 | 39 | 0 | 263 | 408 |
| 4:15 PM | 7 | 5 | 1 | 0 | 13 | 1 | 97 | 4 | 0 | 102 | 1 | 2 | 0 | 0 | 3 | 14 | 211 | 33 | 0 | 258 | 376 |
| 4:30 PM | 16 | 3 | 4 | 0 | 23 | 5 | 84 | 7 | 0 | 96 | 0 | 1 | 1 | 0 | 2 | 19 | 210 | 33 | 0 | 262 | 383 |
| 4:45 PM | 12 | 0 | 0 | 0 | 12 | 0 | 96 | 4 | 0 | 100 | 1 | 1 | 0 | 0 | 2 | 15 | 185 | 26 | 0 | 226 | 340 |
| Hourly Total | 46 | 12 | 7 | 0 | 65 | 10 | 385 | 20 | 0 | 415 | 5 | 6 | 7 | 0 | 18 | 62 | 816 | 131 | 0 | 1009 | 1507 |
| 5:00 PM | 14 | 4 | 1 | 0 | 19 | 0 | 115 | 4 | 0 | 119 | 3 | 0 | 4 | 0 | 7 | 15 | 196 | 46 | 0 | 257 | 402 |
| 5:15 PM | 12 | 1 | 1 | 0 | 14 | 1 | 116 | 4 | 0 | 121 | 2 | 1 | 2 | 0 | 5 | 20 | 205 | 39 | 0 | 264 | 404 |
| 5:30 PM | 8 | 1 | 3 | 0 | 12 | 2 | 117 | 2 | 0 | 121 | 0 | 1 | 2 | 0 | 3 | 12 | 215 | 34 | 0 | 261 | 397 |
| 5:45 PM | 5 | 5 | 2 | 0 | 12 | 0 | 100 | 1 | 0 | 101 | 0 | 0 | 1 | 0 | 1 | 15 | 162 | 23 | 0 | 200 | 314 |
| Hourly Total | 39 | 11 | 7 | 0 | 57 | 3 | 448 | 11 | 0 | 462 | 5 | 2 | 9 | 0 | 16 | 62 | 778 | 142 | 0 | 982 | 1517 |
| 6:00 PM | 11 | 3 | 1 | 0 | 15 | 0 | 91 | 1 | 0 | 92 | 1 | 3 | 2 | 0 | 6 | 8 | 183 | 19 | 0 | 210 | 323 |
| 6:15 PM | 7 | 0 | 2 | 0 | 9 | 2 | 76 | 1 | 0 | 79 | 1 | 0 | 1 | 0 | 2 | 7 | 143 | 19 | 0 | 169 | 259 |
| 6:30 PM | 6 | 2 | 0 | 0 | 8 | 0 | 65 | 0 | 0 | 65 | 2 | 1 | 3 | 0 | 6 | 8 | 116 | 14 | 0 | 138 | 217 |
| 6:45 PM | 4 | 0 | 1 | 0 | 5 | 2 | 63 | 1 | 0 | 66 | 2 | 1 | 1 | 0 | 4 | 4 | 93 | 6 | 0 | 103 | 178 |
| Hourly Total | 28 | 5 | 4 | 0 | 37 | 4 | 295 | 3 | 0 | 302 | 6 | 5 | 7 | 0 | 18 | 27 | 535 | 58 | 0 | 620 | 977 |
| Grand Total | 478 | 82 | 54 | 0 | 614 | 74 | 5975 | 73 | 1 | 6123 | 66 | 87 | 128 | 0 | 281 | 283 | 6029 | 804 | 0 | 7116 | 14134 |
| Approach \% | 77.9 | 13.4 | 8.8 | 0.0 | - | 1.2 | 97.6 | 1.2 | 0.0 | - | 23.5 | 31.0 | 45.6 | 0.0 | - | 4.0 | 84.7 | 11.3 | 0.0 | - | - |
| Total \% | 3.4 | 0.6 | 0.4 | 0.0 | 4.3 | 0.5 | 42.3 | 0.5 | 0.0 | 43.3 | 0.5 | 0.6 | 0.9 | 0.0 | 2.0 | 2.0 | 42.7 | 5.7 | 0.0 | 50.3 | - |
| Lights | 453 | 82 | 51 | 0 | 586 | 69 | 5139 | 72 | 1 | 5281 | 62 | 82 | 126 | 0 | 270 | 279 | 5245 | 761 | 0 | 6285 | 12422 |
| \% Lights | 94.8 | 100.0 | 94.4 | - | 95.4 | 93.2 | 86.0 | 98.6 | 100.0 | 86.2 | 93.9 | 94.3 | 98.4 | - | 96.1 | 98.6 | 87.0 | 94.7 | - | 88.3 | 87.9 |
| Mediums | 20 | 0 | 2 | 0 | 22 | 4 | 233 | 1 | 0 | 238 | 4 | 5 | 2 | 0 | 11 | 4 | 247 | 32 | 0 | 283 | 554 |
| \% Mediums | 4.2 | 0.0 | 3.7 | - | 3.6 | 5.4 | 3.9 | 1.4 | 0.0 | 3.9 | 6.1 | 5.7 | 1.6 | - | 3.9 | 1.4 | 4.1 | 4.0 | - | 4.0 | 3.9 |
| Articulated Trucks | 5 | 0 | 1 | 0 | 6 | 1 | 603 | 0 | 0 | 604 | 0 | 0 | 0 | 0 | 0 | 0 | 537 | 11 | 0 | 548 | 1158 |
| \% Articulated Trucks | 1.0 | 0.0 | 1.9 | - | 1.0 | 1.4 | 10.1 | 0.0 | 0.0 | 9.9 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 8.9 | 1.4 | - | 7.7 | 8.2 |

Ohio Department of Transportation
1980 West Broad Street

Count Name: GEA-422 @ Rapids Rd TMC Site Code:
ate: 09/09/2014
Page No: 3


Turning Movement Data Plot

Ohio Department of Transportation 1980 West Broad Street

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Count Name: GEA-422 @ Rapids Rd TMC Site Code:
Start Date: 09/09/2014
Page No: 4

Turning Movement Peak Hour Data (6:15 AM)

| Start Time | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6:15 AM | 16 | 0 | 0 | 0 | 16 | 3 | 232 | 0 | 0 | 235 | 2 | 4 | 7 | 0 | 13 | 1 | 53 | 6 | 0 | 60 | 324 |
| 6:30 AM | 20 | 2 | 2 | 0 | 24 | 1 | 260 | 0 | 0 | 261 | 1 | 4 | 4 | 0 | 9 | 0 | 62 | 7 | 0 | 69 | 363 |
| 6:45 AM | 17 | 0 | 0 | 0 | 17 | 3 | 240 | 1 | 0 | 244 | 2 | 3 | 4 | 0 | 9 | 0 | 82 | 14 | 0 | 96 | 366 |
| 7:00 AM | 16 | 0 | 0 | 0 | 16 | 3 | 204 | 2 | 0 | 209 | 4 | 7 | 4 | 0 | 15 | 3 | 137 | 14 | 0 | 154 | 394 |
| Total | 69 | 2 | 2 | 0 | 73 | 10 | 936 | 3 | 0 | 949 | 9 | 18 | 19 | 0 | 46 | 4 | 334 | 41 | 0 | 379 | 1447 |
| Approach \% | 94.5 | 2.7 | 2.7 | 0.0 | - | 1.1 | 98.6 | 0.3 | 0.0 | - | 19.6 | 39.1 | 41.3 | 0.0 | - | 1.1 | 88.1 | 10.8 | 0.0 | - | - |
| Total \% | 4.8 | 0.1 | 0.1 | 0.0 | 5.0 | 0.7 | 64.7 | 0.2 | 0.0 | 65.6 | 0.6 | 1.2 | 1.3 | 0.0 | 3.2 | 0.3 | 23.1 | 2.8 | 0.0 | 26.2 | - |
| PHF | 0.863 | 0.250 | 0.250 | 0.000 | 0.760 | 0.833 | 0.900 | 0.375 | 0.000 | 0.909 | 0.563 | 0.643 | 0.679 | 0.000 | 0.767 | 0.333 | 0.609 | 0.732 | 0.000 | 0.615 | 0.918 |
| Lights | 67 | 2 | 2 | 0 | 71 | 10 | 888 | 3 | 0 | 901 | 7 | 17 | 19 | 0 | 43 | 3 | 274 | 39 | 0 | 316 | 1331 |
| \% Lights | 97.1 | 100.0 | 100.0 | - | 97.3 | 100.0 | 94.9 | 100.0 | - | 94.9 | 77.8 | 94.4 | 100.0 | - | 93.5 | 75.0 | 82.0 | 95.1 | - | 83.4 | 92.0 |
| Mediums | 2 | 0 | 0 | 0 | 2 | 0 | 15 | 0 | 0 | 15 | 2 | 1 | 0 | 0 | 3 | 1 | 19 | 2 | 0 | 22 | 42 |
| \% Mediums | 2.9 | 0.0 | 0.0 | - | 2.7 | 0.0 | 1.6 | 0.0 | - | 1.6 | 22.2 | 5.6 | 0.0 | - | 6.5 | 25.0 | 5.7 | 4.9 | - | 5.8 | 2.9 |
| Articulated Trucks | 0 | 0 | 0 | 0 | 0 | 0 | 33 | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 0 | 0 | 41 | 74 |
| \% Articulated Trucks | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 3.5 | 0.0 | - | 3.5 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 12.3 | 0.0 | - | 10.8 | 5.1 |

Ohio Department of Transportation
1980 West Broad Street

Count Name: GEA-422 @ Rapids Rd TMC Site Code:
ate: 09/09/2014
Page No: 5

Peak Hour Data

| O9/09/2014 6:15 AM |
| :--- |
| Ending At |
| 09/09/2014 7:15 AM |
| Lights |
| Mediums |
| Articulated Trucks |


| Mediums |
| :--- | :--- |
| Articulated Trucks |



Turning Movement Peak Hour Data Plot (6:15 AM)

Ohio Department of Transportation 1980 West Broad Stree

Columbus, Ohio, United States 43223 +16147528099 Stephanie.Marik@dot.state.oh.us

Count Name: GEA-422 @ Rapids Rd TMC Site Code:
Start Date: 09/09/2014
Page No: 6

Turning Movement Peak Hour Data (4:45 PM)

| Start Time | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Right | Thru | Left | U-Turn | App. Total | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4:45 PM | 12 | 0 | 0 | 0 | 12 | 0 | 96 | 4 | 0 | 100 | 1 | 1 | 0 | 0 | 2 | 15 | 185 | 26 | 0 | 226 | 340 |
| 5:00 PM | 14 | 4 | 1 | 0 | 19 | 0 | 115 | 4 | 0 | 119 | 3 | 0 | 4 | 0 | 7 | 15 | 196 | 46 | 0 | 257 | 402 |
| 5:15 PM | 12 | 1 | 1 | 0 | 14 | 1 | 116 | 4 | 0 | 121 | 2 | 1 | 2 | 0 | 5 | 20 | 205 | 39 | 0 | 264 | 404 |
| 5:30 PM | 8 | 1 | 3 | 0 | 12 | 2 | 117 | 2 | 0 | 121 | 0 | + | 2 | 0 | 3 | 12 | 215 | 34 | 0 | 261 | 397 |
| Total | 46 | 6 | 5 | 0 | 57 | 3 | 444 | 14 | 0 | 461 | 6 | 3 | 8 | 0 | 17 | 62 | 801 | 145 | 0 | 1008 | 1543 |
| Approach \% | 80.7 | 10.5 | 8.8 | 0.0 | - | 0.7 | 96.3 | 3.0 | 0.0 | - | 35.3 | 17.6 | 47.1 | 0.0 | - | 6.2 | 79.5 | 14.4 | 0.0 | - | - |
| Total \% | 3.0 | 0.4 | 0.3 | 0.0 | 3.7 | 0.2 | 28.8 | 0.9 | 0.0 | 29.9 | 0.4 | 0.2 | 0.5 | 0.0 | 1.1 | 4.0 | 51.9 | 9.4 | 0.0 | 65.3 | - |
| PHF | 0.821 | 0.375 | 0.417 | 0.000 | 0.750 | 0.375 | 0.949 | 0.875 | 0.000 | 0.952 | 0.500 | 0.750 | 0.500 | 0.000 | 0.607 | 0.775 | 0.931 | 0.788 | 0.000 | 0.955 | 0.955 |
| Lights | 44 | 6 | 5 | 0 | 55 | 3 | 395 | 14 | 0 | 412 | 5 | 3 | 8 | 0 | 16 | 62 | 763 | 141 | 0 | 966 | 1449 |
| \% Lights | 95.7 | 100.0 | 100.0 | - | 96.5 | 100.0 | 89.0 | 100.0 | - | 89.4 | 83.3 | 100.0 | 100.0 | - | 94.1 | 100.0 | 95.3 | 97.2 | - | 95.8 | 93.9 |
| Mediums | 1 | 0 | 0 | 0 | 1 | 0 | 15 | 0 | 0 | 15 | 1 | 0 | 0 | 0 | 1 | 0 | 15 | 3 | 0 | 18 | 35 |
| \% Mediums | 2.2 | 0.0 | 0.0 | - | 1.8 | 0.0 | 3.4 | 0.0 | - | 3.3 | 16.7 | 0.0 | 0.0 | - | 5.9 | 0.0 | 1.9 | 2.1 | - | 1.8 | 2.3 |
| Articulated Trucks | 1 | 0 | 0 | 0 | 1 | 0 | 34 | 0 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 1 | 0 | 24 | 59 |
| \% Articulated Trucks | 2.2 | 0.0 | 0.0 | - | 1.8 | 0.0 | 7.7 | 0.0 | - | 7.4 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 2.9 | 0.7 | - | 2.4 | 3.8 |

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Office of Traffic Engineering

Count Name: GEA-422 @ Rapids Rd TMC Site Code:
Start Date: 09/09/2014
Page No: 7

Peak Hour Data

| 09/09/2014 4:45 PM |
| :--- |
| Ending At |
| at/o9/2014 5:45 PM |
| Lights |
| Mediums |
| Articulated Trucks |

Mriums
Ariculated Trucks


Turning Movement Peak Hour Data Plot (4:45 PM)

Ohio Department of Transportation 1980 West Broad Stre

| Start Time | Southbound Approach Southbound |  |  |  |  |  | Westbound Approach Westbound |  |  |  |  |  | Northbound Approach Northbound |  |  |  |  |  | Eastbound Approach Eastbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | U-Turn | Peds | App. <br> Total | Right | Thru | Left | U-Turn | Peds | App. <br> Total | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. <br> Total |  |
| 6:00 AM | 16 | 5 | 0 | 0 | 0 | 21 | 2 | 158 | 4 | 0 | 0 | 164 | 6 | 13 | 21 | 0 | 0 | 40 | 3 | 65 | 10 | 0 | 0 | 78 | 303 |
| 6:15 AM | 22 | 8 | 0 | 0 | 0 | 30 | 4 | 188 | 5 | 0 | 0 | 197 | 3 | 10 | 29 | 0 | 0 | 42 | 2 | 34 | 11 | 0 | 0 | 47 | 316 |
| 6:30 AM | 26 | 9 | 0 | 0 | 0 | 35 | 1 | 212 | 5 | 0 | 0 | 218 | 4 | 15 | 28 | 0 | 0 | 47 | 4 | 54 | 6 | 0 | 0 | 64 | 364 |
| 6:45 AM | 30 | 14 | 0 | 0 | 0 | 44 | 2 | 184 | 2 | 0 | 0 | 188 | 3 | 16 | 23 | 0 | 0 | 42 | 7 | 66 | 18 | 0 | 0 | 91 | 365 |
| Hourly Total | 94 | 36 | 0 | 0 | 0 | 130 | 9 | 742 | 16 | 0 | 0 | 767 | 16 | 54 | 101 | 0 | 0 | 171 | 16 | 219 | 45 | 0 | 0 | 280 | 1348 |
| 7:00 AM | 21 | 10 | 2 | 0 | 0 | 33 | 6 | 165 | 7 | 0 | 0 | 178 | 8 | 18 | 25 | 0 | 0 | 51 | 8 | 105 | 15 | 0 | 0 | 128 | 390 |
| 7:15 AM | 20 | 12 | 3 | 0 | 0 | 35 | 4 | 155 | 5 | 0 | 0 | 164 | 13 | 17 | 21 | 0 | 0 | 51 | 8 | 62 | 18 | 0 | 0 | 88 | 338 |
| 7:30 AM | 22 | 7 | 4 | 0 | 0 | 33 | 0 | 163 | 6 | 0 | 0 | 169 | 5 | 22 | 33 | 0 | 0 | 60 | 9 | 77 | 16 | 0 | 0 | 102 | 364 |
| 7:45 AM | 19 | 18 | 5 | 0 | 0 | 42 | 6 | 130 | 11 | 0 | 0 | 147 | 8 | 18 | 26 | 0 | 0 | 52 | 13 | 48 | 22 | 0 | 0 | 83 | 324 |
| Hourly Total | 82 | 47 | 14 | 0 | 0 | 143 | 16 | 613 | 29 | 0 | 0 | 658 | 34 | 75 | 105 | 0 | 0 | 214 | 38 | 292 | 71 | 0 | 0 | 401 | 1416 |
| 8:00 AM | 12 | 11 | 1 | 0 | 0 | 24 | 2 | 127 | 6 | 0 | 0 | 135 | 9 | 22 | 31 | 0 | 0 | 62 | 7 | 62 | 13 | 0 | 0 | 82 | 303 |
| 8:15 AM | 15 | 10 | 0 | 0 | 0 | 25 | 5 | 131 | 8 | 0 | 0 | 144 | 5 | 19 | 20 | 0 | 0 | 44 | 7 | 60 | 13 | 0 | 0 | 80 | 293 |
| 8:30 AM | 16 | 9 | 2 | 0 | 0 | 27 | 5 | 105 | 3 | 0 | 0 | 113 | 6 | 20 | 14 | 0 | 0 | 40 | 3 | 67 | 15 | 0 | 0 | 85 | 265 |
| 8:45 AM | 20 | 13 | 1 | 0 | 0 | 34 | 1 | 77 | 3 | 0 | 0 | 81 | 3 | 18 | 8 | 0 | 0 | 29 | 10 | 41 | 10 | 0 | 0 | 61 | 205 |
| Hourly Total | 63 | 43 | 4 | 0 | 0 | 110 | 13 | 440 | 20 | 0 | 0 | 473 | 23 | 79 | 73 | 0 | 0 | 175 | 27 | 230 | 51 | 0 | 0 | 308 | 1066 |
| 9:00 AM | 13 | 8 | 3 | 0 | 0 | 24 | 5 | 92 | 7 | 0 | 0 | 104 | 5 | 8 | 10 | 0 | 0 | 23 | 11 | 46 | 15 | 0 | 0 | 72 | 223 |
| 9:15 AM | 9 | 5 | 1 | 0 | 0 | 15 | 4 | 84 | 0 | 0 | 0 | 88 | 0 | 10 | 6 | 0 | 0 | 16 | 9 | 63 | 9 | 0 | 0 | 81 | 200 |
| 9:30 AM | 3 | 11 | 4 | 0 | 0 | 18 | 5 | 90 | 4 | 0 | 0 | 99 | 6 | 5 | 10 | 0 | 0 | 21 | 9 | 66 | 17 | 0 | 0 | 92 | 230 |
| 9:45 AM | 6 | 7 | 3 | 0 | 0 | 16 | 2 | 53 | 7 | 0 | 0 | 62 | 10 | 13 | 6 | 0 | 0 | 29 | 7 | 54 | 13 | 0 | 0 | 74 | 181 |
| Hourly Total | 31 | 31 | 11 | 0 | 0 | 73 | 16 | 319 | 18 | 0 | 0 | 353 | 21 | 36 | 32 | 0 | 0 | 89 | 36 | 229 | 54 | 0 | 0 | 319 | 834 |
| 10:00 AM | 10 | 7 | 4 | 0 | 0 | 21 | 1 | 60 | 4 | 0 | 0 | 65 | 1 | 7 | 4 | 0 | 0 | 12 | 16 | 49 | 8 | 0 | 0 | 73 | 171 |
| 10:15 AM | 21 | 11 | 1 | 0 | 0 | 33 | 1 | 74 | 5 | 0 | 0 | 80 | 4 | 10 | 9 | 0 | 0 | 23 | 8 | 58 | 12 | 0 | 0 | 78 | 214 |
| 10:30 AM | 14 | 6 | 2 | 0 | 0 | 22 | 2 | 69 | 2 | 0 | 0 | 73 | 7 | 10 | 7 | 0 | 0 | 24 | 10 | 75 | 12 | 0 | 0 | 97 | 216 |
| 10:45 AM | 11 | 4 | 5 | 0 | 0 | 20 | 0 | 56 | 2 | 0 | 0 | 58 | 2 | 10 | 7 | 0 | 0 | 19 | 3 | 59 | 3 | 0 | 0 | 65 | 162 |
| Hourly Total | 56 | 28 | 12 | 0 | 0 | 96 | 4 | 259 | 13 | 0 | 0 | 276 | 14 | 37 | 27 | 0 | 0 | 78 | 37 | 241 | 35 | 0 | 0 | 313 | 763 |
| 11:00 AM | 9 | 10 | 2 | 0 | 0 | 21 | 4 | 59 | 5 | 0 | 0 | 68 | 4 | 16 | 6 | 0 | 0 | 26 | 7 | 53 | 15 | 0 | 0 | 75 | 190 |
| 11:15 AM | 9 | 14 | 3 | 0 | 0 | 26 | 3 | 61 | 5 | 0 | 0 | 69 | 8 | 6 | 9 | 0 | 0 | 23 | 9 | 72 | 15 | 0 | 0 | 96 | 214 |
| 11:30 AM | 9 | 4 | 3 | 0 | 0 | 16 | 7 | 71 | 3 | 0 | 0 | 81 | 3 | 8 | 8 | 0 | 0 | 19 | 12 | 55 | 16 | 0 | 0 | 83 | 199 |
| 11:45 AM | 12 | 8 | 4 | 0 | 0 | 24 | 4 | 58 | 4 | 0 | 0 | 66 | 4 | 14 | 4 | 0 | 0 | 22 | 5 | 52 | 14 | 0 | 0 | 71 | 183 |
| Hourly Total | 39 | 36 | 12 | 0 | 0 | 87 | 18 | 249 | 17 | 0 | 0 | 284 | 19 | 44 | 27 | 0 | 0 | 90 | 33 | 232 | 60 | 0 | 0 | 325 | 786 |
| 12:00 PM | 12 | 11 | 1 | 0 | 0 | 24 | 2 | 89 | 5 | 0 | 0 | 96 | 3 | 10 | 10 | 0 | 0 | 23 | 14 | 73 | 16 | 0 | 0 | 103 | 246 |
| 12:15 PM | 7 | 12 | 2 | 0 | 0 | 21 | 2 | 70 | 3 | 0 | 0 | 75 | 3 | 12 | 7 | 0 | 0 | 22 | 9 | 48 | 10 | 0 | 0 | 67 | 185 |
| 12:30 PM | 12 | 6 | 2 | 0 | 0 | 20 | 4 | 66 | 3 | 0 | 0 | 73 | 8 | 5 | 11 | 0 | 0 | 24 | 9 | 68 | 19 | 0 | 0 | 96 | 213 |
| 12:45 PM | 16 | 9 | 2 | 0 | 0 | 27 | 1 | 62 | 4 | 0 | 0 | 67 | 6 | 14 | 5 | 0 | 0 | 25 | 9 | 70 | 14 | 0 | 0 | 93 | 212 |
| Hourly Total | 47 | 38 | 7 | 0 | 0 | 92 | 9 | 287 | 15 | 0 | 0 | 311 | 20 | 41 | 33 | 0 | 0 | 94 | 41 | 259 | 59 | 0 | 0 | 359 | 856 |
| 1:00 PM | 11 | 10 | 4 | 0 | 0 | 25 | 3 | 72 | 2 | 0 | 0 | 77 | 6 | 6 | 10 | 0 | 0 | 22 | 5 | 59 | 17 | 0 | 0 | 81 | 205 |


| 1:15 PM | 11 | 8 | 3 | 0 | 0 | 22 | 3 | 78 | 3 | 0 | 0 | 84 | 3 | 13 | 7 | 0 | 0 | 23 | 12 | 76 | 12 | 0 | 0 | 100 | 229 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1:30 PM | 12 | 10 | 6 | 0 | 0 | 28 | 0 | 87 | 2 | 0 | 0 | 89 | 4 | 12 | 6 | 0 | 0 | 22 | 10 | 53 | 16 | 0 | 0 | 79 | 218 |
| 1:45 PM | 14 | 13 | 1 | 0 | 0 | 28 | 3 | 87 | 6 | 0 | 0 | 96 | 8 | 16 | 7 | 0 | 0 | 31 | 9 | 71 | 10 | 0 | 0 | 90 | 245 |
| Hourly Total | 48 | 41 | 14 | 0 | 0 | 103 | 9 | 324 | 13 | 0 | 0 | 346 | 21 | 47 | 30 | 0 | 0 | 98 | 36 | 259 | 55 | 0 | 0 | 350 | 897 |
| 2:00 PM | 16 | 12 | 4 | 0 | 0 | 32 | 2 | 83 | 2 | 0 | 0 | 87 | 6 | 7 | 15 | 0 | 0 | 28 | 11 | 107 | 15 | 0 | 0 | 133 | 280 |
| 2:15 PM | 22 | 8 | 0 | 0 | 0 | 30 | 3 | 96 | 6 | 0 | 0 | 105 | 6 | 2 | 11 | 0 | 0 | 19 | 15 | 88 | 15 | 0 | 0 | 118 | 272 |
| 2:30 PM | 15 | 12 | 4 | 0 | 0 | 31 | 2 | 86 | 5 | 0 | 0 | 93 | 4 | 18 | 13 | 0 | 0 | 35 | 11 | 104 | 11 | 0 | 0 | 126 | 285 |
| 2:45 PM | 15 | 10 | 3 | 0 | 0 | 28 | 4 | 73 | 11 | 0 | 0 | 88 | 0 | 6 | 5 | 0 | 0 | 11 | 26 | 82 | 23 | 0 | 0 | 131 | 258 |
| Hourly Total | 68 | 42 | 11 | 0 | 0 | 121 | 11 | 338 | 24 | 0 | 0 | 373 | 16 | 33 | 44 | 0 | 0 | 93 | 63 | 381 | 64 | 0 | 0 | 508 | 1095 |
| 3:00 PM | 13 | 11 | 0 | 0 | 0 | 24 | 3 | 61 | 10 | 0 | 0 | 74 | 17 | 10 | 11 | 0 | 0 | 38 | 17 | 148 | 29 | 0 | 0 | 194 | 330 |
| 3:15 PM | 23 | 19 | 6 | 0 | 0 | 48 | 2 | 64 | 6 | 0 | 0 | 72 | 5 | 16 | 7 | 0 | 0 | 28 | 20 | 137 | 29 | 0 | 0 | 186 | 334 |
| 3:30 PM | 18 | 17 | 3 | 0 | 0 | 38 | 4 | 76 | 7 | 0 | 0 | 87 | 7 | 16 | 10 | 0 | 0 | 33 | 14 | 160 | 15 | 0 | 0 | 189 | 347 |
| 3:45 PM | 13 | 18 | 2 | 0 | 0 | 33 | 2 | 50 | 5 | 0 | 0 | 57 | 6 | 24 | 9 | 0 | 0 | 39 | 16 | 154 | 15 | 0 | 0 | 185 | 314 |
| Hourly Total | 67 | 65 | 11 | 0 | 0 | 143 | 11 | 251 | 28 | 0 | 0 | 290 | 35 | 66 | 37 | 0 | 0 | 138 | 67 | 599 | 88 | 0 | 0 | 754 | 1325 |
| 4:00 PM | 18 | 16 | 5 | 0 | 0 | 39 | 4 | 87 | 7 | 0 | 0 | 98 | 7 | 12 | 11 | 0 | 0 | 30 | 19 | 143 | 21 | 0 | 0 | 183 | 350 |
| 4:15 PM | 14 | 21 | 8 | 0 | 0 | 43 | 2 | 73 | 6 | 0 | 0 | 81 | 7 | 17 | 12 | 0 | 0 | 36 | 21 | 150 | 24 | 0 | 0 | 195 | 355 |
| 4:30 PM | 17 | 16 | 10 | 0 | 0 | 43 | 5 | 62 | 2 | 0 | 0 | 69 | 9 | 16 | 9 | 0 | 0 | 34 | 23 | 166 | 24 | 0 | 0 | 213 | 359 |
| 4:45 PM | 14 | 18 | 4 | 0 | 0 | 36 | 3 | 78 | 5 | 0 | 0 | 86 | 7 | 13 | 10 | 0 | 0 | 30 | 21 | 161 | 18 | 0 | 0 | 200 | 352 |
| Hourly Total | 63 | 71 | 27 | 0 | 0 | 161 | 14 | 300 | 20 | 0 | 0 | 334 | 30 | 58 | 42 | 0 | 0 | 130 | 84 | 620 | 87 | 0 | 0 | 791 | 1416 |
| 5:00 PM | 26 | 22 | 1 | 0 | 0 | 49 | 1 | 89 | 5 | 0 | 0 | 95 | 6 | 12 | 4 | 0 | 0 | 22 | 28 | 165 | 20 | 0 | 0 | 213 | 379 |
| 5:15 PM | 29 | 23 | 1 | 0 | 0 | 53 | 2 | 73 | 6 | 0 | 0 | 81 | 4 | 16 | 10 | 0 | 0 | 30 | 29 | 157 | 30 | 0 | 0 | 216 | 380 |
| 5:30 PM | 23 | 12 | 4 | 0 | 0 | 39 | 3 | 88 | 4 | 0 | 0 | 95 | 4 | 14 | 10 | 0 | 0 | 28 | 27 | 165 | 22 | 0 | 0 | 214 | 376 |
| 5:45 PM | 23 | 19 | 5 | 0 | 0 | 47 | 5 | 64 | 5 | 0 | 0 | 74 | 4 | 12 | 12 | 0 | 0 | 28 | 22 | 152 | 17 | 0 | 0 | 191 | 340 |
| Hourly Total | 101 | 76 | 11 | 0 | 0 | 188 | 11 | 314 | 20 | 0 | 0 | 345 | 18 | 54 | 36 | 0 | 0 | 108 | 106 | 639 | 89 | 0 | 0 | 834 | 1475 |
| 6:00 PM | 12 | 17 | 2 | 0 | 0 | 31 | 4 | 60 | 0 | 0 | 0 | 64 | 6 | 13 | 15 | 0 | 0 | 34 | 24 | 121 | 22 | 0 | 0 | 167 | 296 |
| 6:15 PM | 12 | 11 | 6 | 0 | 0 | 29 | 0 | 62 | 4 | 0 | 0 | 66 | 2 | 14 | 8 | 0 | 0 | 24 | 16 | 132 | 17 | 0 | 0 | 165 | 284 |
| 6:30 PM | 5 | 7 | 5 | 0 | 0 | 17 | 2 | 54 | 7 | 0 | 0 | 63 | 6 | 11 | 7 | 0 | 0 | 24 | 23 | 88 | 11 | 0 | 0 | 122 | 226 |
| 6:45 PM | 13 | 6 | 3 | 0 | 0 | 22 | 5 | 58 | 4 | 0 | 0 | 67 | 4 | 8 | 4 | 0 | 0 | 16 | 15 | 81 | 15 | 0 | 0 | 111 | 216 |
| Hourly Total | 42 | 41 | 16 | 0 | 0 | 99 | 11 | 234 | 15 | 0 | 0 | 260 | 18 | 46 | 34 | 0 | 0 | 98 | 78 | 422 | 65 | 0 | 0 | 565 | 1022 |
| Grand Total | 801 | 595 | 150 | 0 | 0 | 1546 | 152 | 4670 | 248 | 0 | 0 | 5070 | 285 | 670 | 621 | 0 | 0 | 1576 | 662 | 4622 | 823 | 0 | 0 | 6107 | 14299 |
| Approach \% | 51.8 | 38.5 | 9.7 | 0.0 | - | - | 3.0 | 92.1 | 4.9 | 0.0 | - | - | 18.1 | 42.5 | 39.4 | 0.0 | - | - | 10.8 | 75.7 | 13.5 | 0.0 | $\checkmark$ | - | - |
| Total \% | 5.6 | 4.2 | 1.0 | 0.0 | - | 10.8 | 1.1 | 32.7 | 1.7 | 0.0 | - | 35.5 | 2.0 | 4.7 | 4.3 | 0.0 | - | 11.0 | 4.6 | 32.3 | 5.8 | 0.0 | - | 42.7 | - |
| Lights | 741 | 554 | 130 | 0 | - | 1425 | 134 | 3941 | 209 | 0 | - | 4284 | 235 | 618 | 586 | 0 | - | 1439 | 620 | 3922 | 745 | 0 | - | 5287 | 12435 |
| \% Lights | 92.5 | 93.1 | 86.7 | - | - | 92.2 | 88.2 | 84.4 | 84.3 | - | - | 84.5 | 82.5 | 92.2 | 94.4 | - | - | 91.3 | 93.7 | 84.9 | 90.5 | - | $\checkmark$ | 86.6 | 87.0 |
| Mediums | 39 | 29 | 15 | 0 | - | 83 | 16 | 165 | 21 | 0 | - | 202 | 24 | 31 | 26 | 0 | - | 81 | 27 | 164 | 42 | 0 | - | 233 | 599 |
| \% Mediums | 4.9 | 4.9 | 10.0 | - | - | 5.4 | 10.5 | 3.5 | 8.5 | - | - | 4.0 | 8.4 | 4.6 | 4.2 | - | - | 5.1 | 4.1 | 3.5 | 5.1 | - | - | 3.8 | 4.2 |
| Articulated Trucks | 21 | 12 | 5 | 0 | - | 38 | 2 | 564 | 17 | 0 | - | 583 | 25 | 21 | 9 | 0 | - | 55 | 15 | 536 | 36 | 0 | - | 587 | 1263 |
| \% Articulated Trucks | 2.6 | 2.0 | 3.3 | - | - | 2.5 | 1.3 | 12.1 | 6.9 | - | - | 11.5 | 8.8 | 3.1 | 1.4 | - | - | 3.5 | 2.3 | 11.6 | 4.4 | - | - | 9.6 | 8.8 |
| Horse and Buggy | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | $\cdots$ | 1 | 1 | 0 | 0 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 2 |
| $\begin{gathered} \text { \% Horse and } \\ \text { Buggy } \end{gathered}$ | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 | 0.0 | 0.4 | - | - | 0.0 | 0.4 | 0.0 | 0.0 | - | - | 0.1 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

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Office of Traffic Engineering

Count Name: GEA-422 @ SR-700 TMC Site Code:
ate: 09/09/2014
Page No: 3


Turning Movement Data Plot

Ohio Department of Transportation

Columbus, Ohio, United States 43223 16147528099 Stephanie.Marik@dot.state.oh.us

Count Name: GEA-422 @ SR-700 TMC Site Code:
te: 09/09/2014

Turning Movement Peak Hour Data (6:30 AM)

| Start Time | Southbound Approach Southbound |  |  |  |  |  | Westbound Approach Westbound |  |  |  |  |  | Northbound Approach Northbound |  |  |  |  |  | Eastbound Approach Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. Total | Right | Thru | Left | U-Turn | Peds | App. Total | Int. Total |
| 6:30 AM | 26 | 9 | 0 | 0 | 0 | 35 | 1 | 212 | 5 | 0 | 0 | 218 | 4 | 15 | 28 | 0 | 0 | 47 | 4 | 54 | 6 | 0 | 0 | 64 | 364 |
| 6:45 AM | 30 | 14 | 0 | 0 | 0 | 44 | 2 | 184 | 2 | 0 | 0 | 188 | 3 | 16 | 23 | 0 | 0 | 42 | 7 | 66 | 18 | 0 | 0 | 91 | 365 |
| 7:00 AM | 21 | 10 | 2 | 0 | 0 | 33 | 6 | 165 | 7 | 0 | 0 | 178 | 8 | 18 | 25 | 0 | 0 | 51 | 8 | 105 | 15 | 0 | 0 | 128 | 390 |
| 7:15 AM | 20 | 12 | 3 | 0 | 0 | 35 | 4 | 155 | 5 | 0 | 0 | 164 | 13 | 17 | 21 | 0 | 0 | 51 | 8 | 62 | 18 | 0 | 0 | 88 | 338 |
| Total | 97 | 45 | 5 | 0 | 0 | 147 | 13 | 716 | 19 | 0 | 0 | 748 | 28 | 66 | 97 | 0 | 0 | 191 | 27 | 287 | 57 | 0 | 0 | 371 | 1457 |
| Approach \% | 66.0 | 30.6 | 3.4 | 0.0 | - | - | 1.7 | 95.7 | 2.5 | 0.0 | - | - | 14.7 | 34.6 | 50.8 | 0.0 | - | - | 7.3 | 77.4 | 15.4 | 0.0 | - | - | - |
| Total \% | 6.7 | 3.1 | 0.3 | 0.0 | - | 10.1 | 0.9 | 49.1 | 1.3 | 0.0 | - | 51.3 | 1.9 | 4.5 | 6.7 | 0.0 | - | 13.1 | 1.9 | 19.7 | 3.9 | 0.0 | - | 25.5 | - |
| PHF | 0.808 | 0.804 | 0.417 | 0.000 | - | 0.835 | 0.542 | 0.844 | 0.679 | 0.000 | - | 0.858 | 0.538 | 0.917 | 0.866 | 0.000 | - | 0.936 | 0.844 | 0.683 | 0.792 | 0.000 | - | 0.725 | 0.934 |
| Lights | 91 | 44 | 4 | 0 | - | 139 | 11 | 673 | 19 | 0 | - | 703 | 24 | 62 | 97 | 0 | - | 183 | 25 | 235 | 54 | 0 | - | 314 | 1339 |
| \% Lights | 93.8 | 97.8 | 80.0 | - | - | 94.6 | 84.6 | 94.0 | 100.0 | - | - | 94.0 | 85.7 | 93.9 | 100.0 | - | - | 95.8 | 92.6 | 81.9 | 94.7 | - | - | 84.6 | 91.9 |
| Mediums | 5 | 1 | 1 | 0 | - | 7 | 2 | 10 | 0 | 0 | - | 12 | 3 | 2 | 0 | 0 | - | 5 | 1 | 13 | 2 | 0 | $-$ | 16 | 40 |
| \% Mediums | 5.2 | 2.2 | 20.0 | - | - | 4.8 | 15.4 | 1.4 | 0.0 | - | - | 1.6 | 10.7 | 3.0 | 0.0 | - | - | 2.6 | 3.7 | 4.5 | 3.5 | - | - | 4.3 | 2.7 |
| Articulated Trucks | 1 | 0 | 0 | 0 | - | 1 | 0 | 33 | 0 | 0 | - | 33 | 1 | 2 | 0 | 0 | - | 3 | 1 | 39 | 1 | 0 | - | 41 | 78 |
| \% Articulated Trucks | 1.0 | 0.0 | 0.0 | . | - | 0.7 | 0.0 | 4.6 | 0.0 | - | - | 4.4 | 3.6 | 3.0 | 0.0 | . | - | 1.6 | 3.7 | 13.6 | 1.8 | - | - | 11.1 | 5.4 |
| Horse and Buggy | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | $\checkmark$ | 0 | 0 |
| \% Horse and Buggy | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

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Office of Traffic Engineering

Count Name: GEA-422 @ SR-700 TMC Site Code:
Start Date: 09/09/2014
Page No: 5


Turning Movement Peak Hour Data Plot (6:30 AM)

Ohio Department of Transportation

Columbus, Ohio, United States 43223 16147528099 Stephanie.Marik@dot.state.oh.us

Count Name: GEA-422 @ SR-700 TMC Site Code:
ate: 09/09/2014
Page No: 6

Turning Movement Peak Hour Data (4:45 PM)

| Start Time | Southbound Approach Southbound |  |  |  |  |  | Westbound Approach Westbound |  |  |  |  |  | Northbound Approach Northbound |  |  |  |  |  | Eastbound Approach Eastbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | U-Turn | Peds | App. | Right | Thru | Left | U-Turn | Peds | App. | Right | Thru | Left | U-Turn | Peds | App. | Right | Thru | Left | U-Turn | Peds | App. | Int. Total |
| 4:45 PM | 14 | 18 | 4 | 0 | 0 | 36 | 3 | 78 | 5 | 0 | 0 | 86 | 7 | 13 | 10 | 0 | 0 | 30 | 21 | 161 | 18 | 0 | 0 | 200 | 352 |
| 5:00 PM | 26 | 22 | 1 | 0 | 0 | 49 | 1 | 89 | 5 | 0 | 0 | 95 | 6 | 12 | 4 | 0 | 0 | 22 | 28 | 165 | 20 | 0 | 0 | 213 | 379 |
| 5:15 PM | 29 | 23 | 1 | 0 | 0 | 53 | 2 | 73 | 6 | 0 | 0 | 81 | 4 | 16 | 10 | 0 | 0 | 30 | 29 | 157 | 30 | 0 | 0 | 216 | 380 |
| 5:30 PM | 23 | 12 | 4 | 0 | 0 | 39 | 3 | 88 | 4 | 0 | 0 | 95 | 4 | 14 | 10 | 0 | 0 | 28 | 27 | 165 | 22 | 0 | 0 | 214 | 376 |
| Total | 92 | 75 | 10 | 0 | 0 | 177 | 9 | 328 | 20 | 0 | 0 | 357 | 21 | 55 | 34 | 0 | 0 | 110 | 105 | 648 | 90 | 0 | 0 | 843 | 1487 |
| Approach \% | 52.0 | 42.4 | 5.6 | 0.0 | - | - | 2.5 | 91.9 | 5.6 | 0.0 | - | - | 19.1 | 50.0 | 30.9 | 0.0 | - | - | 12.5 | 76.9 | 10.7 | 0.0 | - | - | - |
| Total \% | 6.2 | 5.0 | 0.7 | 0.0 | - | 11.9 | 0.6 | 22.1 | 1.3 | 0.0 | - | 24.0 | 1.4 | 3.7 | 2.3 | 0.0 | - | 7.4 | 7.1 | 43.6 | 6.1 | 0.0 | - | 56.7 | - |
| PHF | 0.793 | 0.815 | 0.625 | 0.000 | - | 0.835 | 0.750 | 0.921 | 0.833 | 0.000 | - | 0.939 | 0.750 | 0.859 | 0.850 | 0.000 | - | 0.917 | 0.905 | 0.982 | 0.750 | 0.000 | - | 0.976 | 0.978 |
| Lights | 91 | 74 | 10 | 0 | - | 175 | 9 | 284 | 17 | 0 | - | 310 | 20 | 52 | 33 | 0 | - | 105 | 102 | 618 | 85 | 0 | - | 805 | 1395 |
| \% Lights | 98.9 | 98.7 | 100.0 | - | - | 98.9 | 100.0 | 86.6 | 85.0 | - | - | 86.8 | 95.2 | 94.5 | 97.1 | - | - | 95.5 | 97.1 | 95.4 | 94.4 | - | - | 95.5 | 93.8 |
| Mediums | 0 | 0 | 0 | 0 | - | 0 | 0 | 12 | 2 | 0 | - | 14 | 0 | 3 | 1 | 0 | - | 4 | 3 | 7 | 3 | 0 | - | 13 | 31 |
| \% Mediums | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 | 3.7 | 10.0 | - | - | 3.9 | 0.0 | 5.5 | 2.9 | - | - | 3.6 | 2.9 | 1.1 | 3.3 | - | - | 1.5 | 2.1 |
| Articulated Trucks | 1 | 1 | 0 | 0 | - | 2 | 0 | 32 | 1 | 0 | - | 33 | 1 | 0 | 0 | 0 | - | 1 | 0 | 23 | 2 | 0 | - | 25 | 61 |
| $\begin{gathered} \hline \text { \% Articulated } \\ \text { Trucks } \\ \hline \end{gathered}$ | 1.1 | 1.3 | 0.0 | - | - | 1.1 | 0.0 | 9.8 | 5.0 | - | - | 9.2 | 4.8 | 0.0 | 0.0 | - | - | 0.9 | 0.0 | 3.5 | 2.2 | . | - | 3.0 | 4.1 |
| Horse and Buggy | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 |
| $\begin{gathered} \text { \% Horse and } \\ \text { Buggy } \end{gathered}$ | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | $\checkmark$ | - | - | $\checkmark$ | - | $\checkmark$ | $\checkmark$ | $\cdot$ | $\checkmark$ | $\checkmark$ | - | $\cdot$ | $\checkmark$ | - | - | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | - | - | - |

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Office of Traffic Engineering

Count Name: GEA-422 @ SR-700 TMC Site Code:
Start Date: 09/09/2014
Page No: 7


Turning Movement Peak Hour Data Plot (4:45 PM)


## CLEARANCE INTERVALS

The National Cooperative Highway Research Program (NCHRP) Report 731: Guidelines for Timing Yellow and All-Red Intervals at Signalized Intersections was published July 2012. A number of conclusions were reached as a result of the comprehensive study that is important to the safety performance of signalized intersections.
> The Institute of Transportation Engineers (ITE) Proposed Recommended Practice for the calculation of yellow change intervals and all-red clearance intervals is the methodology used by the highest percentage of state and local agencies.
$>$ Drivers were documented to decelerate when turning at an intersection. The NCHRP Report 731 recommended using a design speed of 20 mile per hour for the calculation of all red timing. Research conducted by the North Carolina Department of Transportation published by the ITE Journal determined that the average operating speed for left turning traffic is 17 miles per hour.
> Using the current ITE guidelines to calculate the duration of yellow change and red clearance intervals has been shown to reduce total crashes between 8 and 14 percent while reducing injury crashes by approximately 12 percent.
$>$ Using the current ITE guidelines to calculate the duration of yellow change and red clearance intervals has been shown to reduce red light running occurrences between 36 and 50 percent.

Vehicular clearance times were calculated for each study area intersection based on guidelines published in the Ohio Manual of Uniform Traffic Control Devices and the ITE Proposed Recommended Practice. The following posted speeds were used to calculate clearance intervals for through phases:

- U.S. Hwy 422 and S.R. 70: 45 MPH
- Rapids Road: 55 MPH (unposted speed limit per Ohio Revised Code)
- Great Lakes Parkway: 25 MPH
- A 25 MPH speed was used to calculate clearance intervals for all leading left turn phases.

Calculated clearance intervals were included in the Synchro models for the proposed conditions, as described in the following section. A summary of the existing and calculated clearance intervals for the three signalized intersections is listed below in Table C1 and the calculations are appended at the end of this section.

TABLE C1: PROPOSED CLEARANCE INTERVALS

| Phase | Existing Yellow/ All Red [sec] | Existing TOTAL [sec] | Calculated Yellowl All Red [sec] | Calculated TOTAL [sec] |
| :---: | :---: | :---: | :---: | :---: |
| US-422 and Great Lakes Pkwy |  |  |  |  |
| Phase 1: WB Left | 4.0 / 2.0 | 6.0 | 3.0 / 2.9 | 5.9 |
| Phase 2: EB Through | 4.0 / 2.0 | 6.0 | 4.3 / 1.4 | 5.7 |
| Phase 6: WB Through | 4.0 / 2.0 | 6.0 | 4.3 / 1.4 | 5.7 |
| Phase 8: NB All | 4.0 / 2.0 | 6.0 | 3.0 / 2.6 | 5.9 |
| US-422 and Rapids Rd |  |  |  |  |
| Phase 2: EB Through | N/A <br> (Stop Control) |  | 4.3 / 1.0 | 5.3 |
| Phase 4: SB Through |  |  | 5.0 / 1.0 | 6.0 |
| Phase 5: EB Left |  |  | 3.0 / 1.3 | 4.3 |
| Phase 6: WB Through |  |  | 4.3 / 1.0 | 5.3 |
| Phase 8: NB Through |  |  | 5.0 / 1.0 | 6.0 |
| US-422 and SR-700 |  |  |  |  |
| Phase 2: EB Through | 4.0 / 2.0 | 6.0 | 4.9 / 1.2 | 6.1 |
| Phase 4: SB Through | 4.0 / 2.0 | 6.0 | 4.8 / 1.4 | 6.2 |
| Phase 5: EB Left | 4.0 / 2.0 | 6.0 | 3.0 / 2.0 | 5.0 |
| Phase 6: WB Through | 4.0 / 2.0 | 6.0 | 4.9 / 1.2 | 6.1 |
| Phase 8: NB Through | 4.0 / 2.0 | 6.0 | 4.8 / 1.4 | 6.2 |

Note: The maximum all-red clearance time set at 3 seconds. Calculated values may be longer than 3 seconds.

Recommended intervals exceed the existing timings at SR-700 on the southbound and westbound approaches. This is attributed to the approach grades at the intersection. The downward grades are approximated at $-4 \%$ in the southbound direction and $-5 \%$ in the westbound direction.

| INTERSECTION: | US-422 | AND | Great Lakes Parkway |
| ---: | :--- | :--- | :--- |
| LOCATION: | ODOT District 12 |  |  |
| BY: | MLS |  |  |
| DATE: | $9 / 30 / 2014$ |  |  |


| PEDESTRIAN CLEARANCE <br> CALCULATIONS <br> OMUTCD 4E.06-07 | Great Lakes Parkway <br> Nb FDW <br> (East XWalk) | Great Lakes Parkway <br> Sb FDW <br> (West Xwalk) | US-422 <br> Eb FDW <br> (South Xwalk) | US-422 <br> Wb FDW <br> (North Xwalk) |
| :--- | :---: | :---: | :---: | :---: |
| Curb to Curb or Edge Line to Edge Line Distance (ft) | 43 | 43 | 85 |  |
| Walking Rate (ft/sec)* | 3.5 | 3.5 | 3.5 |  |
| Calculated Ped Clearance Time (sec) <br> (includes buffer) | 12.3 | 12.3 | 3.5 |  |

*4.0 ft-per-sec walk rate may be used if an extended pushbutton feature is available for slower moving pedestrians to have longer pedestrian clearance time.
PEDESTRIAN WALK CALCULATIONS

| Ped Detector to Curb Distance (ft) (6' if none) | 10 | 10 | 10 | 10 |
| :---: | :---: | :---: | :---: | :---: |
| Crossing Distance (ft) (from above) | 43 | 43 | 85 | 0 |
| Total Crossing Distance (ft) <br> (Detector + Crossing) | 53 | 53 | 95 | 10 |
| Walking Rate (ft/sec) | 3.0 | 3.0 | 3.0 | 3.0 |
| $\begin{aligned} & \hline \text { Total Pedestrian Phase (sec) } \\ & \text { (Walk + Ped Clearance Time) } \\ & \hline \end{aligned}$ | 17.7 | 17.7 | 31.7 | 3.3 |
| Minimum Walk Time (sec)** | 7.0 | 7.0 | 7.0 | 7.0 |
| Calculated Walk Interval (sec) | 5.4 | 5.4 | 7.4 | 3.3 |
| Recommended Walk Interval (sec) | 7 | 7 | 8 | 0 |

**4 sec walk interval may be used if pedestrian volumes and characteristics do not require 7 -second Walk
FLASHING DON'T WALK CALCULATION

| OMUTCD 4E.06-04 |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Programmed Ped Change Interval (sec.) (FDW) <br> (Ped Clear -Yellow - All-Red) | $\mathbf{1 3}$ |  |  |
| Ped Change Interval (sec.) (FDW) <br> (Through Yellow***) | $\mathbf{1 3}$ | $\mathbf{1 9}$ |  |

Note: Pedestrian calculation methods from the federal MUTCD 2009 edition.
***May not conform to OMTUCD requirements for 3 sec buffer

| YELLOW CHANGE INTERVAL | Great Lakes Parkway |  | Great Lakes Parkway |  | US-422 |  | US-422 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Nb | Nb Lt | Sb | Sb Lt | Eb | Eb Lt | Wb | Wb Lt |
| Signal Design Speed (mph) | 25 | 25 | 45 | 25 | 45 | 25 | 45 | 25 |
| Approximate Grade (\%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Calculated Yellow Int. | 2.8 | 2.8 | 4.3 | 2.8 | 4.3 | 2.8 | 4.3 | 2.8 |
| Yellow Interval Limit Check (sec) | 3.0 | 3.0 | 4.3 | 3.0 | 4.3 | 3.0 | 4.3 | 3.0 |
| Recommended Yellow Interval (sec) |  | 3.0 |  |  | 4.3 |  | 4.3 | 3.0 |

Note: TCDH recommends yellow intervals lengths greater than 3 sec and no longer than 5 sec. OMUTCD recommends interval lengths between $3-6$ sec
This table will recommend yellow intervals as calculated by the ITE Proposed Recommended Practice (1985) except where calculated intervals exceed 5 sec
and extreme speed and grade conditions do not exist.

| RED CLEARANCE INTERVAL | Great Lakes Parkway |  | Great Lakes Parkway |  | US-422 |  | US-422 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Nb | Nb Lt | Sb | Sb Lt | Eb | Eb Lt | Wb | Wb Lt |
| Signal Design Speed (mph) | 25 | 25 | 45 | 25 | 45 | 25 | 45 | 25 |
| Width of Intersection (ft) | 0 | 97 | 0 | 0 | 91 | 0 | 83 | 106 |
| Length of Vehicle (ft) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Calculated Red Int. | 0.0 | 2.6 | 0.0 | 0.0 | 1.4 | 0.0 | 1.3 | 2.9 |
| Red Interval Limit Check (sec) | 1.0 | 2.6 | 1.0 | 1.0 | 1.4 | 1.0 | 1.3 | 2.9 |
| Recommended Red Interval (sec) |  | 2.6 |  |  | 1.4 |  | 1.4 | 2.9 |

Note: This table will recommend all-red intervals as calculated by the ITE Proposed Recommended Practice except where calculated intervals are greater
than 3 sec. Red Clearance Interval based on $(w+L) / v$ equation where $L=0 \mathrm{ft}$.


| PEDESTRIAN CLEARANCE <br> CALCULATIONS <br> OMUTCD 4E.06-07 | Rapids Rd <br> Nb FDW <br> (East XWalk) | Rapids Rd <br> Sb FDW <br> (West Xwalk) | US-422 <br> Eb FDW <br> (South Xwalk) | US-422 <br> Wb FDW <br> (North Xwalk) |
| :--- | :---: | :---: | :---: | :---: |
| Curb to Curb or Edge Line to Edge Line Distance (ft) | 37 | 39 | 40 |  |
| Walking Rate (ft/sec)* | 3.5 | 3.5 | 3.5 | 4. |
| Calculated Ped Clearance Time (sec) <br> (includes buffer) | 10.6 | 11.1 | 11.4 |  |

*4.0 ft-per-sec walk rate may be used if an extended pushbutton feature is available for slower moving pedestrians to have longer pedestrian clearance time.

## PEDESTRIAN WALK CALCULATIONS

| MUTCD 4E.06-14 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Ped Detector to Curb Distance (ft) (6' if none) | 10 | 10 | 10 | 10 |
| Crossing Distance (ft) (from above) | 37 | 39 | 40 | 41 |
| Total Crossing Distance (ft) <br> (Detector + Crossing) | 47 | 49 | 50 | 51 |
| Walking Rate (ft/sec) | 3.0 | 3.0 | 3.0 | 3.0 |
| $\begin{aligned} & \text { Total Pedestrian Phase (sec) } \\ & \text { (Walk }+ \text { Ped Clearance Time }) \\ & \hline \end{aligned}$ | 15.7 | 16.3 | 16.7 | 17.0 |
| Minimum Walk Time (sec)** | 7.0 | 7.0 | 7.0 | 7.0 |
| Calculated Walk Interval (sec) | 5.1 | 5.2 | 5.2 | 5.3 |
| Recommended Walk Interval (sec) | 7 | 7 | 7 | 7 |

**4 sec walk interval may be used if pedestrian volumes and characteristics do not require 7-second Walk

## FLASHING DON'T WALK CALCULATION

| OMUTCD 4E.06-04 |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Programmed Ped Change Interval (sec.) (FDW) <br> (Ped Clear -Yellow - All-Red) | $\mathbf{5}$ |  |  |
| Ped Change Interval (sec.) (FDW) <br> (Through Yellow***) | $\mathbf{6}$ |  |  |

Note: Pedestrian calculation methods from the federal MUTCD 2009 edition.
***May not conform to OMTUCD requirements for 3 sec buffer

| YELLOW CHANGE INTERVAL | Rapids Rd |  | Rapids Rd |  | US-422 |  | US-422 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Nb | Nb Lt | Sb | Sb Lt | Eb | Eb Lt | Wb | Wb Lt |
| Signal Design Speed (mph) | 55 | 25 | 55 | 25 | 45 | 25 | 45 | 25 |
| Approximate Grade (\%) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Calculated Yellow Int. | 5.0 | 2.8 | 5.0 | 2.8 | 4.3 | 2.8 | 4.3 | 2.8 |
| Yellow Interval Limit Check (sec) | 5.0 | 3.0 | 5.0 | 3.0 | 4.3 | 3.0 | 4.3 | 3.0 |
| Recommended Yellow Interval (sec) | 5.0 | 3.0 | 5.0 | 3.0 | 4.3 | 3.0 | 4.3 | 3.0 |

Note: TCDH recommends yellow intervals lengths greater than 3 sec and no longer than 5 sec. OMUTCD recommends interval lengths between $3-6$ sec
This table will recommend yellow intervals as calculated by the ITE Proposed Recommended Practice (1985) except where calculated intervals exceed 5 sec
and extreme speed and grade conditions do not exist.

| RED CLEARANCE INTERVAL | Rapids Rd |  | Rapids Rd |  | US-422 |  | US-422 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Nb | Nb Lt | Sb | Sb Lt | Eb | Eb Lt | Wb | Wb Lt |
| Signal Design Speed (mph) | 55 | 25 | 55 | 25 | 45 | 25 | 45 | 25 |
| Width of Intersection (ft) | 43 | 41 | 43 | 41 | 48 | 46 | 48 | 46 |
| Length of Vehicle (ft) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Calculated Red Int. | 0.5 | 1.1 | 0.5 | 1.1 | 0.7 | 1.3 | 0.7 | 1.3 |
| Red Interval Limit Check (sec) | 1.0 | 1.1 | 1.0 | 1.1 | 1.0 | 1.3 | 1.0 | 1.3 |
| Recommended Red Interval (sec) | 1.0 | 1.1 | 1.0 | 1.1 | 1.0 | 1.3 | 1.0 | 1.3 |

Note: This table will recommend all-red intervals as calculated by the ITE Proposed Recommended Practice except where calculated intervals are greater than 3 sec. Red Clearance Interval based on $(w+L) / v$ equation where $L=0 \mathrm{ft}$.

| REQUIRED SPLIT CHECK | Nb |  | Sb |  | Eb | Wb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Green time to accommodate Pedestrians |  |  |  |  |  |  |
| ( sec) |  |  |  |  | 13.1 | 13.4 |
| LJB Inc. | Legend: | Input Field | Referenced | Calculated | Recommended |  |

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INTERSECTION
BY: MLS
DATE: 9/30/2014
```

| PEDESTRIAN CLEARANCE <br> CALCULATIONS <br> OMUTCD 4E.06-07 | SR-700 <br> Nb FDW <br> (East XWalk) | SR-700 <br> Sb FDW <br> (West Xwalk) | US-422 <br> Eb FDW <br> (South Xwalk) | US-422 <br> Wb FDW <br> (North Xwalk) |
| :--- | :---: | :---: | :---: | :---: |
| Curb to Curb or Edge Line to Edge Line Distance (ft) | 40 | 42 | 34 |  |
| Walking Rate (ft/sec)* | 3.5 | 3.5 | 3.5 |  |
| Calculated Ped Clearance Time (sec) <br> (includes buffer) | 11.4 | 12.0 | 3.5 |  |

*4.0 ft-per-sec walk rate may be used if an extended pushbutton feature is available for slower moving pedestrians to have longer pedestrian clearance time.

## PEDESTRIAN WALK CALCULATIONS

| Ped Detector to Curb Distance (ft) (6' if none) | 10 | 10 | 10 | 10 |
| :---: | :---: | :---: | :---: | :---: |
| Crossing Distance (ft) (from above) | 40 | 42 | 34 | 50 |
| Total Crossing Distance (ft) <br> (Detector + Crossing) | 50 | 52 | 44 | 60 |
| Walking Rate (ft/sec) | 3.0 | 3.0 | 3.0 | 3.0 |
| Total Pedestrian Phase (sec) <br> (Walk + Ped Clearance Time) | 16.7 | 17.3 | 14.7 | 20.0 |
| Minimum Walk Time (sec)** | 7.0 | 7.0 | 7.0 | 7.0 |
| Calculated Walk Interval (sec) | 5.2 | 5.3 | 5.0 | 5.7 |
| Recommended Walk Interval (sec) | 7 | 7 | 7 | 7 |

**4 sec walk interval may be used if pedestrian volumes and characteristics do not require 7 -second Walk

## FLASHING DON'T WALK CALCULATION

| OMUTCD 4E.06-04 |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Programmed Ped Change Interval (sec.) (FDW) <br> (Ped Clear -Yellow - All-Red) | $\mathbf{6}$ |  |  |
| Ped Change Interval (sec.) (FDW) <br> (Through Yellow***) | $\mathbf{6}$ |  |  |

Note: Pedestrian calculation methods from the federal MUTCD 2009 edition.
***May not conform to OMTUCD requirements for 3 sec buffer

| YELLOW CHANGE INTERVAL | SR-700 |  | SR-700 |  | US-422 |  | US-422 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Nb | Nb Lt | Sb | Sb Lt | Eb | Eb Lt | Wb | Wb Lt |
| Signal Design Speed (mph) | 45 | 25 | 45 | 25 | 45 | 25 | 45 | 25 |
| Approximate Grade (\%) | 2.5 | 2.5 | -4 | -4 | 7 | 7 | -5 | -5 |
| Calculated Yellow Int. | 4.1 | 2.7 | 4.8 | 3.1 | 3.7 | 2.5 | 4.9 | 3.2 |
| Yellow Interval Limit Check (sec) | 4.1 | 3.0 | 4.8 | 3.1 | 3.7 | 3.0 | 4.9 | 3.2 |
| Recommended Yellow Interval (sec) | 4.8 | 3.1 | 4.8 | 3.1 | 4.9 | 3.2 | 4.9 | 3.2 |

Note: TCDH recommends yellow intervals lengths greater than 3 sec and no longer than 5 sec. OMUTCD recommends interval lengths between $3-6$ sec
This table will recommend yellow intervals as calculated by the ITE Proposed Recommended Practice (1985) except where calculated intervals exceed 5 sec
and extreme speed and grade conditions do not exist.

| RED CLEARANCE INTERVAL | SR-700 |  | SR-700 |  | US-422 |  | US-422 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Nb | Nb Lt | Sb | Sb Lt | Eb | Eb Lt | Wb | Wb Lt |
| Signal Design Speed (mph) | 45 | 25 | 45 | 25 | 45 | 25 | 45 | 25 |
| Width of Intersection (ft) | 82 | 80 | 95 | 84 | 78 | 66 | 78 | 75 |
| Length of Vehicle (ft) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Calculated Red Int. | 1.2 | 2.2 | 1.4 | 2.3 | 1.2 | 1.8 | 1.2 | 2.0 |
| Red Interval Limit Check (sec) | 1.2 | 2.2 | 1.4 | 2.3 | 1.2 | 1.8 | 1.2 | 2.0 |
| Recommended Red Interval (sec) | 1.4 | 2.3 | 1.4 | 2.3 | 1.2 | 2.0 | 1.2 | 2.0 |

Note: This table will recommend all-red intervals as calculated by the ITE Proposed Recommended Practice except where calculated intervals are greater than 3 sec. Red Clearance Interval based on $(w+L) / v$ equation where $L=0 \mathrm{ft}$.

| REQUIRED SPLIT CHECK | Nb |  | Sb |  | Eb | Wb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Green time to accommodate Pedestrians |  |  |  |  |  |  |
| ( sec) |  |  |  |  | 10.6 | 15.2 |
| LJB Inc. | Legend: | Input Field | Referenced | Calculated | Recommended |  |



## CAPACITY ANALYSIS

Capacity analysis was conducted for existing and Build conditions at the three study intersections. Signalized intersection analysis was performed with the assistance of Synchro traffic simulation software (version 8) with output reflective of HCS 2010 algorithms.

The following existing and build analysis scenarios were evaluated. Traffic volumes for all scenarios reflect 2014 counts. Capacity analysis results are summarized in Table D2 with Synchro output reports appended to this section.
$>$ Existing Conditions - AM and PM peak hours

- Existing lane use
- Existing signal timing and signal phasing
$>$ Build Conditions
- U.S. Hwy 422/Great Lakes Parkway
- Optimized splits with an eastbound right turn overlap and calculated vehicle clearance times
- U.S. Hwy 422/Rapids Road
- Traffic signal control with a two-phase operation
- Traffic signal control with a three-phase operation
- Traffic signal control with eastbound and westbound left turn storage lanes
- U.S. Hwy 422/S.R. 700
- Optimized splits and calculated vehicle clearance times
- Widen eastbound and westbound approaches to add left turn storage lanes, two phase signal operation
- Widen eastbound and westbound approaches to add left turn storage lanes, three phase signal operation

Intersections are graded using a level of service (LOS) designation expressed in terms of letter grades. Level of service is a quality measure describing operational conditions with a traffic stream with LOS A representing the highest quality traffic flow and minimal delay, and LOS F representing poor traffic operations, significant delay, and substantial queuing. Level of service is defined in terms of vehicle delay, as published in the Highway Capacity Manual (Transportation Research Board, 2010). Levels of service thresholds for signalized intersections have been summarized in Table D1.

Modifications to the existing model were made to replicate the observed delay and queues at the U.S. Hwy 422 / S.R. 700 intersection as observed on site. Field observations noted high vehicular delay on and extensive eastbound queues forming during peak hours, attributed to infrequent gaps in mainline traffic. Vehicles were also observed to accelerate slowly from a stop when approaching the intersection. This is attributable to a high approach grade (7\%) and heavy vehicles (4\%). The following adjustments were made in synchro to reproduce these results in the capacity analysis model.

To account for eastbound left turn vehicles blocking the through and right turn movements while waiting for acceptable gaps in opposing traffic, the eastbound saturation flow rate was adjusted from

1,900 vehicles per hour to 1,450 . This adjustment was applied to all models where left turn vehicles blocked through movements from entering the intersection.

To account for startup lost time, the standard value of 0 seconds was adjusted to 3 seconds for eastbound vehicles at the intersection. This adjustment was applied to all models since the approach grade is not affected by any recommended countermeasures.

TABLE D1 - LEVELS OF SERVICE THRESHOLDS FOR SIGNALIZED/UNSIGNALIZED INTERSECTIONS

| Level of Service | Signalized Intersections <br> Control Delay <br> (sec/veh) | Unsignalized Intersections <br> Control Delay <br> (sec/veh) |
| :---: | :---: | :---: |
| A | $\leq 10$ | $\leq 10$ |
| B | $>10$ and $\leq 20$ | $>10$ and $\leq 15$ |
| C | $>20$ and $\leq 35$ | $>15$ and $\leq 25$ |
| D | $>35$ and $\leq 55$ | $>25$ and $\leq 35$ |
| E | $>55$ and $\leq 80$ | $>35$ and $\leq 50$ |
| F | $>80$ | $>50$ |

Results indicate that under current conditions, there are capacity deficiencies at the US-422/Rapids Road intersection on the northbound and southbound approaches during the morning and afternoon peak hours. Deficiencies are also present at the US-422/SR-700 intersection during the afternoon peak hour, especially in the eastbound direction. The volume to capacity ratio of the EB approach is 1.10 during the PM peak, which is $10 \%$ over capacity.

TABLE D2: CAPACITY ANALYSIS RESULTS

|  | AM PEAK HOUR |  |  |  |  | PM PEAK HOUR |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 은 曾 总 Z |  |  |  |  |  |
| US-422 \& Great Lakes Parkway |  |  |  |  |  |  |  |  |  |  |
| Existing Condition | B/14.2 | B/19.2 | D/38.2 | - | C/21.4 | D/45.3 | A/5.2 | D/36.4 | - | C/33.5 |
| Optimized Signal | A/5.9 | B/19.1 | D/43.4 | - | C/20.5 | C/25.7 | A/3.9 | E/64.3 | - | C/24.7 |

## US-422 \& Rapid Road

| Existing Condition (2-Way Stop) | $\mathrm{A} / 1.0$ | $\mathrm{~A} / 0.1$ | $\mathrm{~F} / 261.2$ | $\mathrm{~F} / 52.4$ | $\mathrm{~B} / 13.3$ | $\mathrm{~A} / 1.4$ | $\mathrm{~A} / 0.3$ | $\mathrm{~F} / \mathbf{2 0 8 . 2}$ | $\mathrm{F} / \mathbf{1 0 7 . 0}$ | $\mathrm{A} / 9.7$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Two-Phase Signal | $\mathrm{A} / 4.2$ | $\mathrm{~A} / 7.8$ | $\mathrm{C} / 24.1$ | $\mathrm{C} / 25.1$ | $\mathrm{~A} / 8.1$ | $\mathrm{~B} / 14.9$ | $\mathrm{~A} / 3.2$ | $\mathrm{C} / 33.7$ | $\mathrm{D} / 36.6$ | $\mathrm{~B} / 12.9$ |
| Three-Phase Signal | $\mathrm{A} / 3.7$ | $\mathrm{~B} / 20.0$ | $\mathrm{D} / 35.5$ | $\mathrm{D} / 38.0$ | $\mathrm{~B} / 16.1$ | $\mathrm{~B} / 10.6$ | $\mathrm{~A} / 6.7$ | $\mathrm{D} / 35.5$ | $\mathrm{D} / 38.6$ | $\mathrm{~B} / 11.2$ |
| Two-Phase Signal w/ Left Turn Storage | $\mathrm{A} / 4.8$ | $\mathrm{~A} / 7.6$ | $\mathrm{C} / 25.5$ | $\mathrm{C} / 26.7$ | $\mathrm{~A} / 8.4$ | $\mathrm{~A} / 9.9$ | $\mathrm{~A} / 4.5$ | $\mathrm{C} / 20.7$ | $\mathrm{C} / 22.1$ | $\mathrm{~A} / 9.1$ |

US-422 \& SR-700 *

| Existing Condition | $\mathrm{D} / 47.5$ | $\mathrm{D} / 46.2$ | $\mathrm{D} / 41.7$ | $\mathrm{C} / 27.4$ | $\mathrm{D} / 44.1$ | $\mathrm{~F} / 289.5$ | $\mathrm{~B} / 11.4$ | $\mathrm{E} / 77.7$ | $\mathrm{E} / 77.2$ | $\mathrm{~F} / 190.9$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Optimized Signal | $\mathrm{C} / 34.3$ | $\mathrm{C} / 33.5$ | $\mathrm{E} / 63.9$ | $\mathrm{C} / 31.4$ | $\mathrm{D} / 37.4$ | $\mathrm{~F} / 222.9$ | $\mathrm{~A} / 8.6$ | $\mathrm{~F} / 356.7$ | $\mathrm{~F} / \mathbf{1 8 9 . 4}$ | $\mathrm{F} / 183.2$ |
| Two-Phase Signal w/ Left Turn Storage | $\mathrm{B} / 13.0$ | $\mathrm{C} / 28.8$ | $\mathrm{D} / 49.9$ | $\mathrm{C} / 30.0$ | $\mathrm{C} / 27.1$ | $\mathrm{D} / 38.7$ | $\mathrm{~A} / 5.9$ | $\mathrm{D} / 44.1$ | $\mathrm{D} / 48.3$ | $\mathrm{C} / 33.3$ |
| Three-Phase Signal w/ Left Turn Storage | $\mathrm{B} / 10.4$ | $\mathrm{E} / 61.5$ | $\mathrm{E} / 79.1$ | $\mathrm{D} / 36.9$ | $\mathrm{D} / 46.8$ | $\mathrm{D} / 38.7$ | $\mathrm{~B} / 11.2$ | $\mathrm{D} / 44.1$ | $\mathrm{D} / 48.3$ | $\mathrm{C} / 34.4$ |

[^1]As supported by field observation, the existing condition capacity analysis shows long delay on Rapids Road during peak hours. Analysis shows that a traffic signal will mitigate this delay. Existing conditions analysis also shows high delay at the US-422/SR-700 intersection on multiple approaches, particularly the eastbound approach. Analysis shows that the addition of eastbound and westbound left turn lanes will mitigate this delay.

## US-422/Rapids Road Intersection Queue Analysis

In the existing stop controlled condition, the expected $95^{\text {th }}$ percentile queue length is 290 feet for the eastbound approach. An evaluation of vehicle queue lengths was conducted for the three variations of traffic signal control described in the capacity analysis section. Introducing a stop condition on US422 which is inherent to the traffic signal operation may increase queue lengths of US-422. Queue length results are summarized below in Table D3.

Table D3: $\mathbf{9 5}^{\text {th }}$ percentile queue length results

|  | AM PEAK HOUR |  |  |  | PM PEAK HOUR |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 픙 0 0 0 0 0. 0.1 0 3 |  |  | EB APPROACH | I 0 0 0 0 0 0 0 0 3 |  |  |
| US-422 \& Rapids Rd |  |  |  |  |  |  |  |  |
| Existing Condition (Stop Control) | 115 | 20 | 50 | 60 | 290 | 180 | 60 | 80 |
| Two-Phase Signal | 190 | 210 | 65 | 75 | 410 | 210 | 35 | 100 |
| Three-Phase Signal | 165 | 420 | 75 | 100 | 445 | 285 | 40 | 90 |
| Two-Phase Signal w/ Left Turn Storage | 100 | 210 | 60 | 80 | 205 | 235 | 30 | 85 |

Note: Values given reflect 95th percentile queues measured in feet

Expected queue lengths are greatest during the PM peak hour when demand volumes on US-422 are the highest. With a 2-phase signal and no left turn lanes, the eastbound queue length exceeds 400 feet. While the simulation model with the leading eastbound phase indicates no significant change in the eastbound queue length compared to a 2-phase operation, experiences with similar sites suggests that the model output may be underestimating the effect of left turn blocking conditions. For this reason, a 3-phase signal operation is recommended. The addition of left turn lanes on US-422 is expected to reduce the eastbound queue length to less than the existing condition (with 2-phase operation).

3: Great Lakes Pkwy \& US-422
AM Existing Condition

|  | $\rightarrow$ | $\checkmark$ | 7 | $\Perp$ | 4 | $p$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 4 | 「 | * | 4 | ${ }^{1}$ | 「 |
| Volume (veh/h) | 307 | 52 | 104 | 905 | 10 | 98 |
| Number | 2 | 12 | 1 | 6 | 3 | 18 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow veh/h/ln | 169.6 | 190.0 | 190.0 | 182.7 | 158.3 | 188.1 |
| Lanes | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h | 834 | 794 | 593 | 1157 | 341 | 362 |
| Arrive On Green | 0.49 | 0.49 | 0.08 | 0.63 | 0.23 | 0.23 |
| Sat Flow, veh/h | 1696 | 1615 | 1810 | 1827 | 1508 | 1599 |
| Grp Volume(v), veh/h | 345 | 64 | 204 | 1006 | 16 | 316 |
| Grp Sat Flow(s),veh/h/ln | 1696 | 1615 | 1810 | 1827 | 1508 | 1599 |
| Q Serve(g_s), s | 10.6 | 1.7 | 4.2 | 36.8 | 0.7 | 15.6 |
| Cycle Q Clear(g_c), s | 10.6 | 1.7 | 4.2 | 36.8 | 0.7 | 15.6 |
| Prop In Lane |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 834 | 794 | 593 | 1157 | 341 | 362 |
| V/C Ratio(X) | 0.41 | 0.08 | 0.34 | 0.87 | 0.05 | 0.87 |
| Avail Cap(c_a), veh/h | 1036 | 987 | 999 | 1786 | 553 | 586 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 13.3 | 11.0 | 8.7 | 12.2 | 24.8 | 30.5 |
| Incr Delay (d2), s/veh | 1.5 | 0.2 | 0.3 | 9.0 | 0.1 | 8.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q (50\%), veh/ln | 4.3 | 0.6 | 1.6 | 16.3 | 0.3 | 6.9 |
| Lane Grp Delay (d), s/veh | 14.8 | 11.2 | 9.1 | 21.2 | 24.8 | 38.9 |
| Lane Grp LOS | B | B | A | C | C | D |
| Approach Vol, veh/h | 409 |  |  | 1210 | 332 |  |
| Approach Delay, s/veh | 14.2 |  |  | 19.2 | 38.2 |  |
| Approach LOS | B |  |  | B | D |  |
| Timer |  |  |  |  |  |  |
| Assigned Phs | 2 |  | 1 | 6 |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 46.2 |  | 11.6 | 57.8 |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , $s$ | 6.0 |  | 5.0 | 6.0 |  |  |
| Max Green Setting (Gmax), s | 50.0 |  | 25.0 | 80.0 |  |  |
| Max Q Clear Time (g_c+11), s | 12.6 |  | 6.2 | 38.8 |  |  |
| Green Ext Time (p_c), s | 12.7 |  | 0.5 | 13.1 |  |  |
| Intersection Summary |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 21.4 |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |
| Notes |  |  |  |  |  |  |

2: Rapids Rd \& US-422
AM Existing Condition

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 13.3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Vol, veh/h | 41 | 334 | 4 | 3 | 936 | 10 | 19 | 18 | 9 | 2 | 2 | 69 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 73 | 61 | 33 | 38 | 90 | 83 | 68 | 64 | 56 | 25 | 25 | 86 |
| Heavy Vehicles, \% | 0 | 12 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 56 | 548 | 12 | 8 | 1040 | 12 | 28 | 28 | 16 | 8 | 8 | 80 |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  | Minor2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1052 | 0 | 0 | 560 | 0 | 0 | 1772 | 1734 | 554 | 1750 | 1734 | 1046 |
| Stage 1 | - | - | - | - | - | - | 666 | 666 | - | 1062 | 1062 | - |
| Stage 2 | - | - | - | - | - | - | 1106 | 1068 | - | 688 | 672 | - |
| Follow-up Headway | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Capacity-1 Maneuver | 669 | - | - | 1021 | - | - | 65 | 89 | 536 | 68 | 89 | 280 |
| Stage 1 | - | - | - | - | - | - | 452 | 460 | - | 273 | 303 | - |
| Stage 2 | - | - | - | - | - | - | 258 | 301 | - | 440 | 458 | - |


| Time blocked-Platoon, \% |  | - | - | - | - |  |  |  |  |  |  |  |
| :--- | ---: | :--- | :--- | ---: | :--- | :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Mov Capacity-1 Maneuver | 669 | - | - | 1021 | - | - | 38 | 77 | 536 | 43 | 77 | 280 |
| Mov Capacity-2 Maneuver | - | - | - | - | - | - | 38 | 77 | - | 43 | 77 | - |
| Stage 1 | - | - | - | - | - | - | 397 | 404 | - | 240 | 297 | - |
| Stage 2 | - | - | - | - | - | - | 176 | 295 | - | 349 | 402 | - |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | ---: | ---: |
| HCM Control Delay, s | 1 | 0.1 | 261.2 | 52.4 |
| HCM LOS |  | $F$ | $F$ |  |


| Minor Lane / Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 64 | 669 | - | - | 1021 | - | - | 167 |
| HCM Lane V/C Ratio | 1.127 | 0.084 | - | - | 0.008 | - | - | 0.576 |
| HCM Control Delay (s) | 261.2 | 10.874 | 0 | - | 8.553 | 0 | - | 52.4 |
| HCM Lane LOS | F | B | A |  | A | A | F |  |
| HCM 95th \%tile Q(veh) | 5.735 | 0.274 | - | - | 0.023 | - | - | 3.037 |

Notes
~ : Volume Exceeds Capacity; \$ : Delay Exceeds 300 Seconds; Error : Computation Not Defined

9: SR-700 \& US-422
AM Existing Condition

|  | * | $\rightarrow$ | $\checkmark$ | 1 |  | 4 | 4 | 4 | \% |  | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | \& |  |  | \& |  |  | \$ |  |
| Volume (vph) | 57 | 287 | 27 | 19 | 716 | 13 | 97 | 66 | 28 | 5 | 45 | 97 |
| Ideal Flow (vphpl) | 1450 | 1450 | 1450 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (\%) |  | 7\% |  |  | -5\% |  |  | 2\% |  |  | -4\% |  |
| Total Lost time (s) |  | 9.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Frt |  | 0.99 |  |  | 1.00 |  |  | 0.97 |  |  | 0.91 |  |
| Flt Protected |  | 0.99 |  |  | 1.00 |  |  | 0.98 |  |  | 1.00 |  |
| Satd. Flow (prot) |  | 1161 |  |  | 1488 |  |  | 1779 |  |  | 1749 |  |
| Flt Permitted |  | 0.80 |  |  | 0.98 |  |  | 0.71 |  |  | 0.97 |  |
| Satd. Flow (perm) |  | 932 |  |  | 1455 |  |  | 1301 |  |  | 1707 |  |
| Peak-hour factor, PHF | 0.79 | 0.68 | 0.84 | 0.68 | 0.84 | 0.54 | 0.87 | 0.90 | 0.54 | 0.42 | 0.80 | 0.81 |
| Adj. Flow (vph) | 72 | 422 | 32 | 28 | 852 | 24 | 111 | 73 | 52 | 12 | 56 | 120 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 526 | 0 | 0 | 904 | 0 | 0 | 236 | 0 | 0 | 188 | 0 |
| Heavy Vehicles (\%) | 2\% | 23\% | 0\% | 1\% | 32\% | 0\% | 0\% | 0\% | 1\% | 0\% | 1\% | 1\% |
| Turn Type | Perm | NA |  | Perm | NA |  | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |  |
| Actuated Green, G (s) |  | 49.2 |  |  | 49.2 |  |  | 18.3 |  |  | 18.3 |  |
| Effective Green, g (s) |  | 46.2 |  |  | 49.2 |  |  | 18.3 |  |  | 18.3 |  |
| Actuated g/C Ratio |  | 0.58 |  |  | 0.62 |  |  | 0.23 |  |  | 0.23 |  |
| Clearance Time (s) |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  | 6.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  |  | 3.0 |  |  | 3.0 |  |
| Lane Grp Cap (vph) |  | 541 |  |  | 900 |  |  | 299 |  |  | 392 |  |
| v/s Ratio Prot |  |  |  |  |  |  |  |  |  |  |  |  |
| v/s Ratio Perm |  | 0.56 |  |  | c0.62 |  |  | c0.18 |  |  | 0.11 |  |
| v/c Ratio |  | 0.97 |  |  | 1.00 |  |  | 0.79 |  |  | 0.48 |  |
| Uniform Delay, d1 |  | 16.0 |  |  | 15.1 |  |  | 28.8 |  |  | 26.5 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  | 1.00 |  |
| Incremental Delay, d2 |  | 31.5 |  |  | 31.1 |  |  | 12.9 |  |  | 0.9 |  |
| Delay (s) |  | 47.5 |  |  | 46.2 |  |  | 41.7 |  |  | 27.4 |  |
| Level of Service |  | D |  |  | D |  |  | D |  |  | C |  |
| Approach Delay (s) |  | 47.5 |  |  | 46.2 |  |  | 41.7 |  |  | 27.4 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 44.1 |  | HCM 2000 | evel of | ervice |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.99 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 79.5 |  | Sum of los | ime (s) |  |  | 15.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 97.3\% |  | CU Level | Service |  |  | F |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

## 3: Great Lakes Pkwy \& US-422

 PM Existing Condition|  | $\rightarrow$ | 7 | $\%$ |  | 4 | $p$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 4 | 7 | ${ }^{4}$ | 4 | ${ }^{*}$ | F |
| Volume (veh/h) | 1011 | 7 | 5 | 487 | 73 | 50 |
| Number | 2 | 12 | 1 | 6 | 3 | 18 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow veh/h/ln | 186.3 | 166.7 | 135.7 | 177.6 | 184.5 | 190.0 |
| Lanes | 1 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h | 1217 | 926 | 113 | 1303 | 204 | 188 |
| Arrive On Green | 0.65 | 0.65 | 0.01 | 0.73 | 0.12 | 0.12 |
| Sat Flow, veh/h | 1863 | 1417 | 1293 | 1776 | 1757 | 1615 |
| Grp Volume(v), veh/h | 1248 | 12 | 12 | 541 | 124 | 135 |
| Grp Sat Flow(s),veh/h/ln | 1863 | 1417 | 1293 | 1776 | 1757 | 1615 |
| Q Serve(g_s), s | 50.0 | 0.2 | 0.2 | 8.9 | 5.1 | 6.2 |
| Cycle Q Clear(g_c), s | 50.0 | 0.2 | 0.2 | 8.9 | 5.1 | 6.2 |
| Prop In Lane |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 1217 | 926 | 113 | 1303 | 204 | 188 |
| V/C Ratio(X) | 1.03 | 0.01 | 0.11 | 0.42 | 0.61 | 0.72 |
| Avail Cap(c_a), veh/h | 1217 | 926 | 516 | 1857 | 689 | 633 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 13.3 | 4.6 | 21.3 | 3.9 | 32.2 | 32.6 |
| Incr Delay (d2), s/veh | 32.4 | 0.0 | 0.4 | 1.0 | 2.9 | 5.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q (50\%), veh/ln | 28.2 | 0.1 | 0.2 | 2.9 | 2.4 | 2.7 |
| Lane Grp Delay (d), s/veh | 45.7 | 4.7 | 21.7 | 4.9 | 35.1 | 37.7 |
| Lane Grp LOS | F | A | C | A | D | D |
| Approach Vol, veh/h | 1260 |  |  | 553 | 259 |  |
| Approach Delay, s/veh | 45.3 |  |  | 5.2 | 36.4 |  |
| Approach LOS | D |  |  | A | D |  |
| Timer |  |  |  |  |  |  |
| Assigned Phs | 2 |  | 1 | 6 |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 56.0 |  | 6.1 | 62.1 |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s | 6.0 |  | 5.0 | 6.0 |  |  |
| Max Green Setting (Gmax), s | 50.0 |  | 25.0 | 80.0 |  |  |
| Max Q Clear Time (g_c+11), s | 52.0 |  | 2.2 | 10.9 |  |  |
| Green Ext Time (p_c), s | 0.0 |  | 0.0 | 26.5 |  |  |
| Intersection Summary |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 33.5 |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |
| Notes |  |  |  |  |  |  |

2: Rapids Rd \& US-422
PM Existing Condition

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Intersection Delay, s/veh | 9.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Vol, veh/h | 145 | 801 | 62 | 14 | 444 | 3 | 8 | 3 | 6 | 5 | 6 | 46 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 79 | 90 | 78 | 88 | 90 | 38 | 50 | 75 | 50 | 42 | 38 | 82 |
| Heavy Vehicles, \% | 1 | 3 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Mvmt Flow | 184 | 890 | 79 | 16 | 493 | 8 | 16 | 4 | 12 | 12 | 16 | 56 |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  |  |  |  |  |
| :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 501 | 0 | 0 | 969 | 0 | 0 | 1862 | 1830 | 930 | 1834 | 1866 | 497 |
| Stage 1 | - | - | - | - | - | - | 1297 | 1297 | - | 529 | 529 | - |
| Stage 2 | - | - | - | - | - | - | 565 | 533 | - | 1305 | 1337 | - |
| Follow-up Headway | 2.209 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.318 |
| Pot Capacity-1 Maneuver | 1068 | - | - | 719 | - | - | 57 | 77 | 327 | 59 | 73 | 573 |
| Stage 1 | - | - | - | - | - | - | 201 | 234 | - | 537 | 530 | - |
| Stage 2 | - | - | - | - | - | - | 513 | 528 | - | 199 | 224 | - |

Time blocked-Platoon, \%

| Mov Capacity-1 Maneuver | 1068 | - | - | 719 | - | - | 26 | 46 | 327 | 37 | 44 | 573 |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Mov Capacity-2 Maneuver | - | - | - | - | - | - | 26 | 46 | - | 37 | 44 | - |
| Stage 1 | - | - | - | - | - | - | 124 | 145 | - | 332 | 514 | - |
| Stage 2 | - | - | - | - | - | - | 435 | 512 | - | 115 | 139 | - |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | ---: | :---: |
| HCM Control Delay, s | 1.4 | 0.3 | 208.2 | 107 |
| HCM LOS |  | $F$ | $F$ |  |


| Minor Lane / Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 43 | 1068 | - | - | 719 | - | - | 108 |
| HCM Lane V/C Ratio | 0.744 | 0.172 | - | - | 0.022 | - | - | 0.776 |
| HCM Control Delay (s) | 208.2 | 9.069 | 0 | - | 10.12 | 0 | - | 107 |
| HCM Lane LOS | F | A | A |  | B | A | F |  |
| HCM 95th \%tile Q(veh) | 2.844 | 0.619 | - | - | 0.068 | - | - | 4.293 |

Notes
~ : Volume Exceeds Capacity; \$ : Delay Exceeds 300 Seconds; Error : Computation Not Defined

9: SR-700 \& US-422
PM Existing Condition


3: Great Lakes Pkwy \& US-422
AM w Optimized Timing


9: SR-700 \& US-422
AM w Optimized Timing


3: Great Lakes Pkwy \& US-422
AM w Optimized Timing

|  | $\rightarrow$ |  | 4 |
| :---: | :---: | :---: | :---: |
| Phase Number | 2 | 6 | 8 |
| Movement | EBT | WBTL | NBL |
| Lead/Lag |  |  |  |
| Lead-Lag Optimize |  |  |  |
| Recall Mode | Min | Min | None |
| Maximum Split (s) | 52 | 52 | 23 |
| Maximum Split (\%) | 69.3\% | 69.3\% | 30.7\% |
| Minimum Split (s) | 31 | 30 | 15.5 |
| Yellow Time (s) | 4 | 4 | 4 |
| All-Red Time (s) | 2 | 2 | 1.5 |
| Minimum Initial (s) | 6 | 6 | 6 |
| Vehicle Extension (s) | 3 | 3 | 3 |
| Minimum Gap (s) | 3 | 3 | 3 |
| Time Before Reduce (s) | 0 | 0 | 0 |
| Time To Reduce (s) | 0 | 0 | 0 |
| Walk Time (s) |  |  |  |
| Flash Dont Walk (s) |  |  |  |
| Dual Entry | Yes | Yes | Yes |
| Inhibit Max | Yes | Yes | Yes |
| Start Time (s) | 0 | 0 | 52 |
| End Time (s) | 52 | 52 | 0 |
| Yield/Force Off (s) | 46 | 46 | 69.5 |
| Yield/Force Off 170(s) | 46 | 46 | 69.5 |
| Local Start Time (s) | 29 | 29 | 6 |
| Local Yield (s) | 0 | 0 | 23.5 |
| Local Yield 170(s) | 0 | 0 | 23.5 |
| Intersection Summary |  |  |  |
| Cycle Length |  |  | 75 |
| Control Type | Actuate | d-Uncoor | dinated |
| Natural Cycle |  |  | 75 |

Splits and Phases: 3: Great Lakes Pkwy \& US-422


9: SR-700 \& US-422
AM w Optimized Timing


Splits and Phases: 9: SR-700 \& US-422


## 3: Great Lakes Pkwy \& US-422

PM w Optimized Timing


## Notes

* HCM 2010 computational engine requires equal clearance times for the phases crossing the barrier.

9: SR-700 \& US-422
PM w Optimized Timing


3: Great Lakes Pkwy \& US-422
PM w Optimized Timing


Splits and Phases: 3: Great Lakes Pkwy \& US-422


9: SR-700 \& US-422
PM w Optimized Timing


Splits and Phases: 9: SR-700 \& US-422


2: Rapids Rd \& US-422
AM 2-Phase

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | 4 | \% | $t$ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | * |  |  | $\ddagger$ |  |  | \$ |  |
| Volume (veh/h) | 41 | 334 | 4 | 3 | 936 | 10 | 19 | 18 | 9 | 2 | 2 | 69 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow veh/h/ln | 190.0 | 171.7 | 190.0 | 190.0 | 182.8 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Cap, veh/h | 124 | 997 | 21 | 68 | 1263 | 14 | 140 | 85 | 39 | 78 | 20 | 136 |
| Arrive On Green | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.70 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| Sat Flow, veh/h | 76 | 1418 | 30 | 4 | 1796 | 21 | 505 | 848 | 387 | 76 | 196 | 1360 |
| Grp Volume(v), veh/h | 616 | 0 | 0 | 1060 | 0 | 0 | 72 | 0 | 0 | 96 | 0 | 0 |
| Grp Sat Flow(s), veh/h/ln | 1524 | 0 | 0 | 1820 | 0 | 0 | 1740 | 0 | 0 | 1632 | 0 | 0 |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 9.3 | 0.0 | 0.0 | 22.9 | 0.0 | 0.0 | 2.0 | 0.0 | 0.0 | 3.1 | 0.0 | 0.0 |
| Prop In Lane | 0.09 |  | 0.02 | 0.01 |  | 0.01 | 0.39 |  | 0.22 | 0.08 |  | 0.83 |
| Lane Grp Cap(c), veh/h | 1141 | 0 | 0 | 1345 | 0 | 0 | 263 | 0 | 0 | 233 | 0 | 0 |
| V/C Ratio(X) | 0.54 | 0.00 | 0.00 | 0.79 | 0.00 | 0.00 | 0.27 | 0.00 | 0.00 | 0.41 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 1448 | 0 | 0 | 1742 | 0 | 0 | 321 | 0 | 0 | 292 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 3.8 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | 23.5 | 0.0 | 0.0 | 24.0 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.4 | 0.0 | 0.0 | 1.9 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.2 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q (50\%), veh/ln | 2.2 | 0.0 | 0.0 | 6.3 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 | 1.2 | 0.0 | 0.0 |
| Lane Grp Delay (d), s/veh | 4.2 | 0.0 | 0.0 | 7.8 | 0.0 | 0.0 | 24.1 | 0.0 | 0.0 | 25.1 | 0.0 | 0.0 |
| Lane Grp LOS | A |  |  | A |  |  | C |  |  | C |  |  |
| Approach Vol, veh/h |  | 616 |  |  | 1060 |  |  | 72 |  |  | 96 |  |
| Approach Delay, s/veh |  | 4.2 |  |  | 7.8 |  |  | 24.1 |  |  | 25.1 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | C |  |
| Timer |  |  |  |  |  |  |  |  |  |  |  |  |
| Assigned Phs |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 44.8 |  |  | 44.8 |  |  | 11.0 |  |  | 11.0 |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , $s$ |  | 5.6 |  |  | 5.6 |  |  | 5.4 |  |  | 5.4 |  |
| Max Green Setting (Gmax), s |  | 51.4 |  |  | 51.4 |  |  | 7.6 |  |  | 7.6 |  |
| Max Q Clear Time (g_c+l1), s |  | 11.3 |  |  | 24.9 |  |  | 4.0 |  |  | 5.1 |  |
| Green Ext Time (p_c), s |  | 17.3 |  |  | 14.2 |  |  | 0.2 |  |  | 0.2 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 8.1 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |



Splits and Phases: 2: Rapids Rd \& US-422


Queuing and Blocking Report
AM 2-Phase
Intersection: 2: Rapids Rd \& US-422

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 232 | 234 | 68 | 78 |
| Average Queue (ft) | 89 | 119 | 28 | 39 |
| 95th Queue (ft) | 192 | 208 | 64 | 77 |
| Link Distance (ft) | 2241 | 7768 | 1454 | 1274 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

2: Rapids Rd \& US-422
AM 3-Phase

|  | 4 | $\rightarrow$ |  | 4 |  | 4 | $4$ | 4 | \% | $t$ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | \$ |  |  | $\ddagger$ |  |  | \$ |  |
| Volume (veh/h) | 41 | 334 | 4 | 3 | 936 | 10 | 19 | 18 | 9 | 2 | 2 | 69 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow veh/h/ln | 190.0 | 171.7 | 190.0 | 190.0 | 182.8 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Cap, veh/h | 104 | 916 | 19 | 49 | 1134 | 13 | 102 | 60 | 28 | 56 | 15 | 107 |
| Arrive On Green | 0.78 | 0.78 | 0.78 | 0.63 | 0.63 | 0.63 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 | 0.08 |
| Sat Flow, veh/h | 68 | 1172 | 25 | 4 | 1795 | 21 | 490 | 776 | 362 | 81 | 197 | 1387 |
| Grp Volume(v), veh/h | 616 | 0 | 0 | 1060 | 0 | 0 | 72 | 0 | 0 | 96 | 0 | 0 |
| Grp Sat Flow(s), veh/h/ln | 1265 | 0 | 0 | 1820 | 0 | 0 | 1628 | 0 | 0 | 1665 | 0 | 0 |
| Q Serve(g_s), s | 6.0 | 0.0 | 0.0 | 4.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 9.6 | 0.0 | 0.0 | 39.8 | 0.0 | 0.0 | 3.2 | 0.0 | 0.0 | 4.3 | 0.0 | 0.0 |
| Prop In Lane | 0.09 |  | 0.02 | 0.01 |  | 0.01 | 0.39 |  | 0.22 | 0.08 |  | 0.83 |
| Lane Grp Cap(c), veh/h | 1040 | 0 | 0 | 1196 | 0 | 0 | 190 | 0 | 0 | 179 | 0 | 0 |
| V/C Ratio(X) | 0.59 | 0.00 | 0.00 | 0.89 | 0.00 | 0.00 | 0.38 | 0.00 | 0.00 | 0.54 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 1083 | 0 | 0 | 1256 | 0 | 0 | 190 | 0 | 0 | 179 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 2.9 | 0.0 | 0.0 | 12.6 | 0.0 | 0.0 | 34.5 | 0.0 | 0.0 | 35.1 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.8 | 0.0 | 0.0 | 7.7 | 0.0 | 0.0 | 1.2 | 0.0 | 0.0 | 3.1 | 0.0 | 0.0 |
| Initial Q Delay( ${ }^{\text {d }}$ ), s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q (50\%), veh/ln | 2.3 | 0.0 | 0.0 | 16.4 | 0.0 | 0.0 | 1.4 | 0.0 | 0.0 | 1.9 | 0.0 | 0.0 |
| Lane Grp Delay (d), s/veh | 3.7 | 0.0 | 0.0 | 20.3 | 0.0 | 0.0 | 35.7 | 0.0 | 0.0 | 38.2 | 0.0 | 0.0 |
| Lane Grp LOS | A |  |  | C |  |  | D |  |  | D |  |  |
| Approach Vol, veh/h |  | 616 |  |  | 1060 |  |  | 72 |  |  | 96 |  |
| Approach Delay, s/veh |  | 3.7 |  |  | 20.3 |  |  | 35.7 |  |  | 38.2 |  |
| Approach LOS |  | A |  |  | C |  |  | D |  |  | D |  |
| Timer |  |  |  |  |  |  |  |  |  |  |  |  |
| Assigned Phs | 5 | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 11.6 | 66.2 |  |  | 54.6 |  |  | 11.4 |  |  | 11.4 |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s | 5.6 | 5.6 |  |  | 5.6 |  |  | 5.4 |  |  | 5.4 |  |
| Max Green Setting (Gmax), s | 6.0 | 63.0 |  |  | 51.6 |  |  | 6.0 |  |  | 6.0 |  |
| Max Q Clear Time (g_c+l1), s | 0.0 | 11.6 |  |  | 41.8 |  |  | 5.2 |  |  | 6.3 |  |
| Green Ext Time (p_c), s | 0.0 | 20.1 |  |  | 7.3 |  |  | 0.1 |  |  | 0.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 16.3 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | B |  |  |  |  |  |  |  |  |  |



Splits and Phases: 2: Rapids Rd \& US-422


Intersection: 2: Rapids Rd \& US-422

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 217 | 458 | 78 | 97 |
| Average Queue (ft) | 67 | 242 | 34 | 52 |
| 95th Queue (ft) | 164 | 419 | 74 | 97 |
| Link Distance (ft) | 2241 | 7768 | 1454 | 1274 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

2: Rapids Rd \& US-422
AM w Turn Lane

|  | 4 | $\rightarrow$ |  | 4 |  | 4 | 4 | 4 | $p$ | $t$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  |  | * |  |  | \$ |  |  | \$ |  |
| Volume (veh/h) | 41 | 334 | 4 | 3 | 936 | 10 | 19 | 18 | 9 | 2 | 2 | 69 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow veh/h/ln | 190.0 | 170.0 | 190.0 | 190.0 | 182.8 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 |
| Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Cap, veh/h | 299 | 1188 | 26 | 64 | 1287 | 15 | 134 | 81 | 37 | 74 | 19 | 130 |
| Arrive On Green | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.72 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| Sat Flow, veh/h | 545 | 1658 | 36 | 4 | 1796 | 21 | 513 | 847 | 389 | 76 | 195 | 1360 |
| Grp Volume(v), veh/h | 56 | 0 | 560 | 1060 | 0 | 0 | 72 | 0 | 0 | 96 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 545 | 0 | 1694 | 1820 | 0 | 0 | 1749 | 0 | 0 | 1632 | 0 | 0 |
| Q Serve(g_s), s | 4.5 | 0.0 | 8.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 27.6 | 0.0 | 8.2 | 23.0 | 0.0 | 0.0 | 2.1 | 0.0 | 0.0 | 3.3 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.02 | 0.01 |  | 0.01 | 0.39 |  | 0.22 | 0.08 |  | 0.83 |
| Lane Grp Cap(c), veh/h | 299 | 0 | 1214 | 1366 | 0 | 0 | 253 | 0 | 0 | 223 | 0 | 0 |
| V/C Ratio(X) | 0.19 | 0.00 | 0.46 | 0.78 | 0.00 | 0.00 | 0.28 | 0.00 | 0.00 | 0.43 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 387 | 0 | 1486 | 1657 | 0 | 0 | 306 | 0 | 0 | 278 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 14.9 | 0.0 | 3.5 | 5.6 | 0.0 | 0.0 | 24.9 | 0.0 | 0.0 | 25.4 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.3 | 0.0 | 0.3 | 1.9 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q (50\%), veh/ln | 0.6 | 0.0 | 1.8 | 6.3 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 | 1.3 | 0.0 | 0.0 |
| Lane Grp Delay (d), s/veh | 15.2 | 0.0 | 3.8 | 7.6 | 0.0 | 0.0 | 25.5 | 0.0 | 0.0 | 26.7 | 0.0 | 0.0 |
| Lane Grp LOS | B |  | A | A |  |  | C |  |  | C |  |  |
| Approach Vol, veh/h |  | 616 |  |  | 1060 |  |  | 72 |  |  | 96 |  |
| Approach Delay, s/veh |  | 4.8 |  |  | 7.6 |  |  | 25.5 |  |  | 26.7 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | C |  |
| Timer |  |  |  |  |  |  |  |  |  |  |  |  |
| Assigned Phs |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 47.6 |  |  | 47.6 |  |  | 11.0 |  |  | 11.0 |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s |  | 5.6 |  |  | 5.6 |  |  | 5.4 |  |  | 5.4 |  |
| Max Green Setting (Gmax), s |  | 51.4 |  |  | 51.4 |  |  | 7.6 |  |  | 7.6 |  |
| Max Q Clear Time (g_c+l1), s |  | 29.6 |  |  | 25.0 |  |  | 4.1 |  |  | 5.3 |  |
| Green Ext Time (p_c), s |  | 12.4 |  |  | 13.8 |  |  | 0.2 |  |  | 0.2 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 8.4 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

AM w Turn Lane


Splits and Phases: 2: Rapids Rd \& US-422


Intersection: 2: Rapids Rd \& US-422

| Movement | EB | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | LTR | LTR | LTR |
| Maximum Queue (ft) | 65 | 96 | 222 | 60 | 87 |
| Average Queue (ft) | 27 | 41 | 124 | 26 | 38 |
| 95th Queue (ft) | 60 | 97 | 209 | 58 | 77 |
| Link Distance (ft) |  | 2241 | 7768 | 1448 | 1268 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (ft) | 245 |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |


|  | 4 |  |  |  | $\leftarrow$ |  | 4 | 4 | $p$ | + | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Volume (veh/h) | 145 | 801 | 62 | 14 | 444 | 3 | 8 | , | 6 | 5 | 6 | 46 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow veh/h/ln | 190.0 | 185.4 | 190.0 | 190.0 | 176.5 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 187.5 | 190.0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Cap, veh/h | 232 | 987 | 86 | 64 | 1311 | 21 | 114 | 34 | 46 | 65 | 28 | 78 |
| Arrive On Green | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| Sat Flow, veh/h | 226 | 1261 | 109 | 20 | 1675 | 27 | 598 | 464 | 638 | 154 | 390 | 1087 |
| Grp Volume(v), veh/h | 1153 | 0 | 0 | 517 | 0 | 0 | 32 | 0 | 0 | 84 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1596 | 0 | 0 | 1721 | 0 | 0 | 1700 | 0 | 0 | 1631 | 0 | 0 |
| Q Serve(g_s), s | 34.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 41.7 | 0.0 | 0.0 | 6.9 | 0.0 | 0.0 | 1.3 | 0.0 | 0.0 | 3.8 | 0.0 | 0.0 |
| Prop In Lane | 0.16 |  | 0.07 | 0.03 |  | 0.02 | 0.50 |  | 0.37 | 0.14 |  | 0.67 |
| Lane Grp Cap (c), veh/h | 1304 | 0 | 0 | 1397 | 0 | 0 | 194 | 0 | 0 | 172 | 0 | 0 |
| V/C Ratio(X) | 0.88 | 0.00 | 0.00 | 0.37 | 0.00 | 0.00 | 0.17 | 0.00 | 0.00 | 0.49 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 1583 | 0 | 0 | 1690 | 0 | 0 | 204 | 0 | 0 | 183 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 0.00 | 0.94 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 5.9 | 0.0 | 0.0 | 2.5 | 0.0 | 0.0 | 33.3 | 0.0 | 0.0 | 34.4 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 9.0 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 | 2.1 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q (50\%), veh/ln | 11.3 | 0.0 | 0.0 | 1.9 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.6 | 0.0 | 0.0 |
| Lane Grp Delay (d), s/veh | 14.9 | 0.0 | 0.0 | 3.2 | 0.0 | 0.0 | 33.7 | 0.0 | 0.0 | 36.6 | 0.0 | 0.0 |
| Lane Grp LOS | B |  |  | A |  |  | C |  |  | D |  |  |
| Approach Vol, veh/h |  | 1153 |  |  | 517 |  |  | 32 |  |  | 84 |  |
| Approach Delay, s/veh |  | 14.9 |  |  | 3.2 |  |  | 33.7 |  |  | 36.6 |  |
| Approach LOS |  | B |  |  | A |  |  | C |  |  | D |  |
| Timer |  |  |  |  |  |  |  |  |  |  |  |  |
| Assigned Phs |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s |  | 65.1 |  |  | 65.1 |  |  | 10.9 |  |  | 10.9 |  |
| Change Period ( $Y+R \mathrm{R}$ ), $s$ |  | 5.6 |  |  | 5.6 |  |  | 5.4 |  |  | 5.4 |  |
| Max Green Setting (Gmax), s |  | 73.0 |  |  | 73.0 |  |  | 6.0 |  |  | 6.0 |  |
| Max Q Clear Time (g_c+11), s |  | 43.7 |  |  | 8.9 |  |  | 3.3 |  |  | 5.8 |  |
| Green Ext Time (p_c), s |  | 15.8 |  |  | 21.6 |  |  | 0.1 |  |  | 0.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 12.9 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

## 2: Rapids Rd \& US-422

PM 2-Phase


Splits and Phases: 2: Rapids Rd \& US-422


Intersection: 2: Rapids Rd \& US-422

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 422 | 276 | 38 | 107 |
| Average Queue (ft) | 221 | 82 | 12 | 48 |
| 95th Queue (ft) | 411 | 212 | 37 | 96 |
| Link Distance (ft) | 2241 | 7767 | 1454 | 1274 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |


|  | 4 |  |  |  |  |  | 4 | $\uparrow$ | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | \$ |  |  | \$ |  |  | ¢ |  |
| Volume (veh/h) | 145 | 801 | 62 | 14 | 444 | 3 | 8 | , | 6 | 5 | 6 | 46 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow veh/h/ln | 190.0 | 185.4 | 190.0 | 190.0 | 176.5 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 187.5 | 190.0 |
| Lanes | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Cap, veh/h | 227 | 983 | 85 | 60 | 1109 | 18 | 109 | 32 | 44 | 63 | 27 | 76 |
| Arrive On Green | 0.79 | 0.79 | 0.79 | 0.66 | 0.66 | 0.66 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 | 0.07 |
| Sat Flow, veh/h | 220 | 1242 | 108 | 20 | 1674 | 27 | 590 | 458 | 629 | 154 | 389 | 1087 |
| Grp Volume(v), veh/h | 1153 | 0 | 0 | 517 | 0 | 0 | 32 | 0 | 0 | 84 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 1569 | 0 | 0 | 1721 | 0 | 0 | 1676 | 0 | 0 | 1631 | 0 | 0 |
| Q Serve(g_s), s | 6.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.2 | 0.0 | 0.0 |
| Cycle Q Clear (g_c), s | 45.6 | 0.0 | 0.0 | 11.2 | 0.0 | 0.0 | 1.4 | 0.0 | 0.0 | 4.0 | 0.0 | 0.0 |
| Prop In Lane | 0.16 |  | 0.07 | 0.03 |  | 0.02 | 0.50 |  | 0.37 | 0.14 |  | 0.67 |
| Lane Grp Cap (c), veh/h | 1297 | 0 | 0 | 1187 | 0 | 0 | 185 | 0 | 0 | 165 | 0 | 0 |
| VIC Ratio(X) | 0.89 | 0.00 | 0.00 | 0.44 | 0.00 | 0.00 | 0.17 | 0.00 | 0.00 | 0.51 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 1495 | 0 | 0 | 1381 | 0 | 0 | 193 | 0 | 0 | 175 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 4.3 | 0.0 | 0.0 | 6.4 | 0.0 | 0.0 | 35.0 | 0.0 | 0.0 | 36.2 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 6.3 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 | 2.4 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q (50\%), veh/ln | 5.4 | 0.0 | 0.0 | 3.7 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.7 | 0.0 | 0.0 |
| Lane Grp Delay (d), s/veh | 10.6 | 0.0 | 0.0 | 6.7 | 0.0 | 0.0 | 35.5 | 0.0 | 0.0 | 38.6 | 0.0 | 0.0 |
| Lane Grp LOS | B |  |  | A |  |  | D |  |  | D |  |  |
| Approach Vol, veh/h |  | 1153 |  |  | 517 |  |  | 32 |  |  | 84 |  |
| Approach Delay, s/veh |  | 10.6 |  |  | 6.7 |  |  | 35.5 |  |  | 38.6 |  |
| Approach LOS |  | B |  |  | A |  |  | D |  |  | D |  |
| Timer |  |  |  |  |  |  |  |  |  |  |  |  |
| Assigned Phs | 5 | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Phs Duration ( $\mathrm{G}+\mathrm{Y}+\mathrm{Rc}$ ), s | 10.3 | 68.5 |  |  | 58.2 |  |  | 10.9 |  |  | 10.9 |  |
| Change Period ( $Y+R \mathrm{Rc}$ ), $s$ | 4.3 | 5.6 |  |  | 5.6 |  |  | 5.4 |  |  | 5.4 |  |
| Max Green Setting (Gmax), s | 6.7 | 73.0 |  |  | 62.0 |  |  | 6.0 |  |  | 6.0 |  |
| Max Q Clear Time (g_c+11), s | 0.0 | 47.6 |  |  | 13.2 |  |  | 3.4 |  |  | 6.0 |  |
| Green Ext Time (p_c), s | 0.0 | 15.3 |  |  | 21.5 |  |  | 0.1 |  |  | 0.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 11.2 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | B |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

## 2: Rapids Rd \& US-422

PM 3-Phase

|  | $\rightarrow$ |  | 4 | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Phase Number | 2 | 4 | 5 | 6 | 8 |
| Movement | EBTL | SBTL | EBL | WBTL | NBTL |
| Lead/Lag |  |  | Lead | Lag |  |
| Lead-Lag Optimize |  |  | Yes | Yes |  |
| Recall Mode | Min | None | Min | Min | None |
| Maximum Split (s) | 78.6 | 11.4 | 11 | 67.6 | 11.4 |
| Maximum Split (\%) | 87.3\% | 12.7\% | 12.2\% | 75.1\% | 12.7\% |
| Minimum Split (s) | 30 | 11.4 | 11 | 30 | 11.4 |
| Yellow Time (s) | 4.3 | 4.3 | 3 | 4.3 | 4.3 |
| All-Red Time (s) | 1.3 | 1.1 | 1.3 | 1.3 | 1.1 |
| Minimum Initial (s) | 6 | 6 | 6 | 6 | 6 |
| Vehicle Extension (s) | 3 | 3 | 3 | 3 | 3 |
| Minimum Gap (s) | 3 | 3 | 3 | 3 | 3 |
| Time Before Reduce (s) | 0 | 0 | 0 | 0 | 0 |
| Time To Reduce (s) | 0 | 0 | 0 | 0 | 0 |
| Walk Time (s) |  |  |  |  |  |
| Flash Dont Walk (s) |  |  |  |  |  |
| Dual Entry | Yes | Yes | No | Yes | Yes |
| Inhibit Max | Yes | Yes | Yes | Yes | Yes |
| Start Time (s) | 0 | 78.6 | 0 | 11 | 78.6 |
| End Time (s) | 78.6 | 0 | 11 | 78.6 | 0 |
| Yield/Force Off (s) | 73 | 84.6 | 6.7 | 73 | 84.6 |
| Yield/Force Off 170(s) | 73 | 84.6 | 6.7 | 73 | 84.6 |
| Local Start Time (s) | 17 | 5.6 | 17 | 28 | 5.6 |
| Local Yield (s) | 0 | 11.6 | 23.7 | 0 | 11.6 |
| Local Yield 170(s) | 0 | 11.6 | 23.7 | 0 | 11.6 |
| Intersection Summary |  |  |  |  |  |
| Cycle Length |  |  | 90 |  |  |
| Control Type Actuated-Uncoo |  |  | Actuated-Uncoordinated |  |  |
| Natural Cycle | 90 |  |  |  |  |

Splits and Phases: 2: Rapids Rd \& US-422


Intersection: 2: Rapids Rd \& US-422

| Movement | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| Directions Served | LTR | LTR | LTR | LTR |
| Maximum Queue (ft) | 473 | 336 | 37 | 98 |
| Average Queue (ft) | 220 | 119 | 13 | 48 |
| 95th Queue (ft) | 445 | 283 | 38 | 91 |
| Link Distance (ft) | 2241 | 7767 | 1454 | 1274 |
| Upstream Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |

2: Rapids Rd \& US-422
PM w Turn Lane

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | 4 | 7 | $t$ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  |  | \& |  |  | \& |  |  | \& |  |
| Volume (veh/h) | 145 | 801 | 62 | 14 | 444 | 3 | 8 | 3 | 6 | 5 | 6 | 46 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow veh/h/ln | 188.1 | 184.9 | 190.0 | 190.0 | 176.5 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 187.5 | 190.0 |
| Lanes | 1 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Cap, veh/h | 640 | 1139 | 101 | 87 | 1142 | 18 | 164 | 46 | 60 | 98 | 38 | 105 |
| Arrive On Green | 0.68 | 0.68 | 0.68 | 0.68 | 0.68 | 0.68 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 | 0.10 |
| Sat Flow, veh/h | 902 | 1674 | 149 | 17 | 1678 | 27 | 564 | 475 | 623 | 152 | 392 | 1088 |
| Grp Volume(v), veh/h | 184 | 0 | 969 | 517 | 0 | 0 | 32 | 0 | 0 | 84 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 902 | 0 | 1823 | 1722 | 0 | 0 | 1662 | 0 | 0 | 1632 | 0 | 0 |
| Q Serve(g_s), s | 5.7 | 0.0 | 17.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 12.3 | 0.0 | 17.9 | 6.6 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 | 2.4 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.08 | 0.03 |  | 0.02 | 0.50 |  | 0.37 | 0.14 |  | 0.67 |
| Lane Grp Cap(c), veh/h | 640 | 0 | 1241 | 1247 | 0 | 0 | 270 | 0 | 0 | 241 | 0 | 0 |
| V/C Ratio(X) | 0.29 | 0.00 | 0.78 | 0.41 | 0.00 | 0.00 | 0.12 | 0.00 | 0.00 | 0.35 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 965 | 0 | 1897 | 1840 | 0 | 0 | 356 | 0 | 0 | 333 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 0.00 | 1.00 | 0.94 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 6.3 | 0.0 | 5.4 | 3.6 | 0.0 | 0.0 | 20.5 | 0.0 | 0.0 | 21.2 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 1.1 | 0.0 | 4.9 | 1.0 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile Back of Q (50\%), veh/ln | 1.1 | 0.0 | 5.5 | 1.6 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | 0.9 | 0.0 | 0.0 |
| Lane Grp Delay (d), s/veh | 7.5 | 0.0 | 10.3 | 4.5 | 0.0 | 0.0 | 20.7 | 0.0 | 0.0 | 22.1 | 0.0 | 0.0 |
| Lane Grp LOS | A |  | B | A |  |  | C |  |  | C |  |  |
| Approach Vol, veh/h |  | 1153 |  |  | 517 |  |  | 32 |  |  | 84 |  |
| Approach Delay, s/veh |  | 9.9 |  |  | 4.5 |  |  | 20.7 |  |  | 22.1 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | C |  |
| Timer |  |  |  |  |  |  |  |  |  |  |  |  |
| Assigned Phs |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 39.2 |  |  | 39.2 |  |  | 10.2 |  |  | 10.2 |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s |  | 5.6 |  |  | 5.6 |  |  | 5.4 |  |  | 5.4 |  |
| Max Green Setting (Gmax), s |  | 51.4 |  |  | 51.4 |  |  | 7.6 |  |  | 7.6 |  |
| Max Q Clear Time (g_c+l1), s |  | 19.9 |  |  | 8.6 |  |  | 2.8 |  |  | 4.4 |  |
| Green Ext Time (p_c), s |  | 13.7 |  |  | 15.3 |  |  | 0.2 |  |  | 0.1 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 9.1 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |
| Notes |  |  |  |  |  |  |  |  |  |  |  |  |

## 2: Rapids Rd \& US-422

PM w Turn Lane


Splits and Phases: 2: Rapids Rd \& US-422


Intersection: 2: Rapids Rd \& US-422

| Movement | EB | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | LTR | LTR | LTR |
| Maximum Queue (ft) | 87 | 220 | 278 | 27 | 94 |
| Average Queue (ft) | 43 | 103 | 89 | 11 | 43 |
| 95th Queue (ft) | 83 | 204 | 233 | 32 | 85 |
| Link Distance (ft) |  | 2241 | 7768 | 1448 | 1268 |
| Upstream Blk Time (\%) |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |
| Storage Bay Dist (ft) | 245 |  |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |

9: SR-700 \& US-422
AM 2-Phase w Turn Lanes


9: SR-700 \& US-422
AM 2-Phase w Turn Lanes


Splits and Phases: 9: SR-700 \& US-422


9: SR-700 \& US-422
AM 3-Phase w Turn Lanes

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

9: SR-700 \& US-422
AM 3-Phase w Turn Lanes


Splits and Phases: 9: SR-700 \& US-422


## 9: SR-700 \& US-422

PM 2-Phase w Turn Lanes


9: SR-700 \& US-422
PM 2-Phase w Turn Lanes


Splits and Phases: 9: SR-700 \& US-422


## 9: SR-700 \& US-422

PM 3-Phase w Turn Lanes


9: SR-700 \& US-422
PM 3-Phase w Turn Lanes

|  | $\rightarrow$ |  | 4 | 4 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Phase Number | 2 | 4 | 5 | 6 | 8 |
| Movement | EBTL | SBTL | EBL | WBTL | NBTL |
| Lead/Lag |  |  | Lead | Lag |  |
| Lead-Lag Optimize |  |  |  |  |  |
| Recall Mode | Min | Min | None | Min | Min |
| Maximum Split (s) | 73.9 | 26.1 | 11 | 62.9 | 26.1 |
| Maximum Split (\%) | 73.9\% | 26.1\% | 11.0\% | 62.9\% | 26.1\% |
| Minimum Split (s) | 23 | 26.1 | 11 | 28.2 | 25.5 |
| Yellow Time (s) | 4.9 | 4.8 | 3 | 4.9 | 4.8 |
| All-Red Time (s) | 1.2 | 1.4 | 2 | 1.2 | 1.4 |
| Minimum Initial (s) | 6 | 6 | 6 | 6 | 6 |
| Vehicle Extension (s) | 3 | 3 | 3 | 3 | 3 |
| Minimum Gap (s) | 3 | 3 | 3 | 3 | 3 |
| Time Before Reduce (s) | 0 | 0 | 0 | 0 | 0 |
| Time To Reduce (s) | 0 | 0 | 0 | 0 | 0 |
| Walk Time (s) | 7 | 7 |  | 7 | 7 |
| Flash Dont Walk (s) | 9.7 | 12 |  | 14.3 | 11.4 |
| Dual Entry | Yes | Yes | No | Yes | Yes |
| Inhibit Max | Yes | Yes | Yes | Yes | Yes |
| Start Time (s) | 0 | 73.9 | 0 | 11 | 73.9 |
| End Time (s) | 73.9 | 0 | 11 | 73.9 | 0 |
| Yield/Force Off (s) | 67.8 | 93.8 | 6 | 67.8 | 93.8 |
| Yield/Force Off 170(s) | 67.8 | 93.8 | 6 | 67.8 | 93.8 |
| Local Start Time (s) | 32.2 | 6.1 | 32.2 | 43.2 | 6.1 |
| Local Yield (s) | 0 | 26 | 38.2 | 0 | 26 |
| Local Yield 170(s) | 0 | 26 | 38.2 | 0 | 26 |
| Intersection Summary |  |  |  |  |  |
| Cycle Length |  |  | 100 |  |  |
| Control Type Actuated-Uncoo |  |  | Actuated-Uncoordinated |  |  |
| Natural Cycle | 100 |  |  |  |  |

Splits and Phases: 9: SR-700 \& US-422




NUMBER OF CRASHES
7 PROPERTY DAMAGE ONLY
$\xlongequal{1}$ INUURY OR FATAL TOTAL CRASHES

|  | SYMBOLS | TYPES OF COLLISIONS | SHOW FOR EACH CRASH |
| :---: | :---: | :---: | :---: |
|  | MOVING VEHICLE | $\cdots$ REAR END |  |
| $\because>$ | BACKING VEHICLE | RIGHT ANGLE | 1. TIME, DAY, DATE |
|  | NON-INVOLVED VEH. | $\because$ SIDE SWIPE | 2. WEATHER AND ROAD |
| $\square$ | PARKED VEHICLE | OUTOFCONTROL | SURFACE IF UNUSUAL CONDITION EXISTED |
| $\square$ | FIXED OBJECT | $\bigcirc$ left turn |  |
| $\bigcirc$ | FATAL CRASH INJURY CRASH | HEAD ON | DUSK AND DAWN |




NUMBER OF CRASHES
3 PROPERTY DAMAGE ONLY
1 INJURY OR FATAL
TOTAL CRASHES

| SYMBOLS | TYPES OF COLLISIONS | SHOW FOR EACH CRASH |
| :---: | :---: | :---: |
|  |  | 1. TIME, DAY, DATE <br> 2. WEATHER AND ROAD SURFACE IF UNUSUAL CONDITION EXISTED <br> 3. NITE - IF BETWEEN DUSK AND DAWN |

COLLISION DIAGRAM

| LOG POINT No. | 11.03 |  |  | то | 11.15 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PERIOD |  | FROM | 2011 |  | TO | 2013 |
| COUNTY | Geauga |  | ROUTE | NUMBER |  | 422 |




NUMBER OF CRASHES
3 PROPERTY DAMAGE ONLY
1 INJURY OR FATAL TOTAL CRASHES


| SHOW FOR |
| :---: |
| EACH CRASH |
| 1. TIME, DAY, DATE |
| 2. WEATHER AND ROAD |
| SURACE IF UNUSUAL |
| CONDITION EXISTED |
| 3. NITE - IF BETWEEN |
| DUSK AND DAWN |

COLLISION DIAGRAM

| LOG POINT No. | 11.30 |  |  | то | 11.42 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PERIOD | 3 Years | FROM | 2011 |  | TO | 2013 |
| COUNTY | Geauga |  | ROUTE | NUM |  | 422 |




NUMBER OF CRASHES
2 PROPERTY DAMAGE ONLY
0 INJURY OR FATAL
total crashes

|  | SYMBOLS |  |  | TYPES OF COLLISIONS |
| :---: | :---: | :---: | :---: | :---: |
| SHOW FOR |  |  |  |  |
| EACH CRASH |  |  |  |  |


| LOG POINT No. | COLLISION DIAGRAM |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 11.59 |  | TO | 11.71 |  |
| PERIOD 3 Years | FROM | 2011 |  | то | 2013 |
| COUNTY Geauga |  | ROUTE | NUMBER |  | 422 |



NUMBER OF CRASHES
2 PROPERTY DAMAGE ONLY
$\underline{\underline{0}}$ injury or Fatal
total crashes


COLLISION DIAGRAM





NUMBER OF CRASHES
1 PROPERTY DAMAGE ONLY
$\xlongequal{0}$ INJURY OR FATAL total crashes



| DATE: $10 / 8 / 2014$ |
| :--- |
| PAGE: 10 of 16 |





NUMBER OF CRASHES
5 PROPERTY DAMAGE ONLY
1 INJURY OR FATAL
6 total crashes






## SIGNAL WARRANT ANALYSIS

Traffic signals should be installed only if an intersection meets at least one of the criteria specified in the Ohio Manual of Uniform Traffic Control Devices, Section 4C.02.
> Warrant 1, Eight-Hour Vehicular Volume: This warrant requires traffic volumes on both the major and minor street approaches to satisfy minimum criteria for eight hours of an average day.
> Warrant \#2: Four Hour Volume. This warrant requires that for a minimum of four hours of an average day traffic volumes on both the major and minor street fall above the applicable curve in the attached figures. The Four-Hour signal warrant conditions are intended to be applied where the volume of intersecting traffic is the principal reason to consider installing a traffic signal.
> Warrant 3, Peak Hour: This warrant requires that for a minimum of one hour of an average day traffic volumes on both the major and minor street fall above the applicable curve in the attached figures. The minimum side street volume is 75 vehicles in the peak hour. Warrant 3 is intended for use where traffic conditions are such that for a minimum of one hour of an average day, minor street traffic experiences undue delay when entering or crossing the major street.

Existing traffic volumes were evaluated against eight-hour, four-hour and peak-hour signal warrant criteria at the three study intersections.

Warrants were evaluated based on high-speed criteria applicable for roadways with posted speed limits exceeding 40 miles per hour. U.S. Hwy 422 is defined as major street for signal warrant analysis purposes, and respective cross street as minor street approach. No reduction of right-turning vehicles was applied to side street traffic volumes.

Results indicate that all three intersections justify installation of traffic signal, as summarized in Table F1. Detailed signal warrant worksheets are appended.

TABLE F1: SIGNAL WARRANT SUMMARY

| SIGNAL WARRANT | U.S. HWY 422/ <br> GREAT LAKES PKWY | U.S. HWY 422/ <br> RAPIDS RD | U.S. HWY 422/ <br> S.R. 700 |
| :--- | :---: | :---: | :---: |
| Warrant 1: <br> 8 -Hour Vehicular Volume | Warrant Not Met | Warrant Not Met | Warrant Met |
| Warrant 2: <br> 4-Hour Vehicular Volume | Warrant Met | Warrant Not Met | Warrant Met |
| Warrant 3: <br> Peak Hour Volume | Warrant Met | Warrant Met | Warrant Met |

## U.S. HWY 422 AT S.R. 700

The intersection of U.S. Hwy 422 at S.R. 700 meets the criteria for all three warrants.

## U.S. HWY 422 AT GREAT LAKES PARKWAY

The intersection of U.S. Hwy 422 at Great Lakes Parkway justifies installation of traffic signal control based on warrants 2 and 3.
U.S. HWY 422 AT RAPIDS ROAD

The intersection of U.S. Hwy 422/Rapids Road meets warrant 3, peak hour volume.

The four-hour warrant requires that for each of any 4 hours of an average day, volumes on both the major and minor street fall above the applicable curve in Figure 4C-1 (for speeds less than 40 MPH ) or 4C-2 (for speeds greater than 40 MPH ). As shown below in Graph F1, the minimum volume for a one-lane, minor street approach is 60 vehicles per hour. Rapids Road approach volumes exceed the 60 vph threshold during the 6AM hour ( 75 vph ), the 7AM hour ( 73 vph ) and the $4: 30 \mathrm{PM}$ hour ( 68 vph ). The 3:30 PM hour approach volume of 59 vph is only 1 vehicle shy of the threshold. Based on these findings, it is concluded that the Rapids Road intersection satisfies four-hour signal warrant requirements.

## Graph F1: Four-Hour Signal Warrant Graph (4C-2)



Date:
Jurisdiction:
Intersection:
Number of APPROACH Lanes:
Major Street = $\quad 1$
Minor Street =
Speed Limit $=\quad 45 \quad(\mathrm{mph})$
Population above 10,000? $\qquad$
70\% Warrant Apply? $\square$

|  | Warrant 1 - Condition A |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 100\% | 80\% | 70\% | 56\% |
| Major Approach: | 500 | 400 | 350 | 280 |
| Minor Approach: | 150 | 120 | 105 | 84 |
| Mid - 1 AM |  |  |  |  |
| 1AM - 2 AM |  |  |  |  |
| 2:00 AM |  |  |  |  |
| 3:00 AM |  |  |  |  |
| 4:00 AM |  |  |  |  |
| 5:00 AM |  |  |  |  |
| 6:00 AM |  |  |  |  |
| 7:00 AM |  |  |  | + |
| 8:00 AM |  |  |  |  |
| 9:00 AM |  |  |  |  |
| 10:00 AM |  |  |  |  |
| 11:00 AM |  |  |  |  |
| Noon - 1PM |  |  |  |  |
| 1PM - 2PM |  |  |  |  |
| 2:00 PM |  |  |  | + |
| 3:00 PM | + | + | + | + |
| 4:00 PM |  |  |  | + |
| 5:00 PM |  |  | + | + |
| 6:00 PM |  |  |  |  |
| 7:00 PM |  |  |  |  |
| 8:00 PM |  |  |  |  |
| 9:00 PM |  |  |  |  |
| 10:00 PM |  |  |  |  |
| 11:00 PM |  |  |  |  |
| Hours M | 1 | 1 | 2 | 5 |

Warrant 1-Condition A:

| $100 \%$ | Warrant Met? | No |
| :---: | :--- | :--- |
| $70 \%$ | Warrant Met? | No |

Tuesday, September 09, 2014
Geauga County, OHIO
US 422 at Great Lakes Pkwy

Traffic Signal Warrant (OMUTCD - 2012)


| Data: | Major St: |  | TOTAL | Mino |  | > OF TWO |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mid - 1AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 1AM-2AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 AM | 990 | 302 | 1292 | 0 | 59 | 59 |
| 7:00 AM | 906 | 420 | 1326 | 0 | 95 | 95 |
| 8:00 AM | 634 | 393 | 1027 | 0 | 24 | 24 |
| 9:00 AM | 426 | 356 | 782 | 0 | 29 | 29 |
| 10:00 AM | 356 | 370 | 726 | 0 | 40 | 40 |
| 11:00 AM | 331 | 363 | 694 | 0 | 42 | 42 |
| Noon - 1PM | 385 | 424 | 809 | 0 | 53 | 53 |
| 1PM - 2PM | 426 | 433 | 859 | 0 | 47 | 47 |
| 2:00 PM | 491 | 533 | 1024 | 0 | 100 | 100 |
| 3:00 PM | 403 | 776 | 1179 | 0 | 190 | 190 |
| 4:00 PM | 424 | 982 | 1406 | 0 | 88 | 88 |
| 5:00 PM | 484 | 1002 | 1486 | 0 | 115 | 115 |
| 6:00 PM | 343 | 636 | 979 | 0 | 22 | 22 |
| 7:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |

Combination of Warrant 1 - Conditions A \& B:

| $80 \%$ | Warrant Met? | No |
| :---: | :---: | :---: |
| $56 \%(70 \%)$ | Warrant Met? | No |

Warrant 1-Condition B:

| $100 \%$ | Warrant Met? | No |
| :---: | :--- | :--- |
| $70 \%$ | Warrant Met? | No |

US 422 at Great Lakes Pkwy



70\% Warrant Apply?
Yes

## US 422 at Great Lakes Pkwy

## Warrant 3, Peak-Hour Vehicular Volume



Warrant 3, Peak-Hour Vehicular Volume (70\% Factor)


Date:
Jurisdiction:
Intersection:
Number of APPROACH Lanes:
Major Street =
Minor Street =
Speed Limit 1
Population above 10,000 ?
(mph)
70\% Warrant Apply? $\square$

|  | Warrant 1 - Condition A |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 100\% | 80\% | 70\% | 56\% |
| Major Approach: | 500 | 400 | 350 | 280 |
| Minor Approach: | 150 | 120 | 105 | 84 |
| Mid - 1AM |  |  |  |  |
| 1AM - 2AM |  |  |  |  |
| 2:00 AM |  |  |  |  |
| 3:00 AM |  |  |  |  |
| 4:00 AM |  |  |  |  |
| 5:00 AM |  |  |  |  |
| 6:00 AM |  |  |  |  |
| 7:00 AM |  |  |  |  |
| 8:00 AM |  |  |  |  |
| 9:00 AM |  |  |  |  |
| 10:00 AM |  |  |  |  |
| 11:00 AM |  |  |  |  |
| Noon - 1PM |  |  |  |  |
| 1PM - 2PM |  |  |  |  |
| 2:00 PM |  |  |  |  |
| 3:00 PM |  |  |  |  |
| 4:00 PM |  |  |  |  |
| 5:00 PM |  |  |  |  |
| 6:00 PM |  |  |  |  |
| 7:00 PM |  |  |  |  |
| 8:00 PM |  |  |  |  |
| 9:00 PM |  |  |  |  |
| 10:00 PM |  |  |  |  |
| 11:00 PM |  |  |  |  |
| Hours M | 0 | 0 | 0 | 0 |

Warrant 1-Condition A:

| $100 \%$ | Warrant Met? | No |
| :---: | :--- | :--- |
| $70 \%$ | Warrant Met? | No |

Tuesday, September 09, 2014
Geauga County, OHIO
US 422 at Rapids Road


| Data: | Major St: |  | TOTAL | Minc |  | > OF TWO |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mid - 1AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 1AM-2AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 AM | 937 | 308 | 1245 | 75 | 37 | 75 |
| 7:00 AM | 812 | 452 | 1264 | 73 | 46 | 73 |
| 8:00 AM | 574 | 350 | 924 | 49 | 29 | 49 |
| 9:00 AM | 384 | 334 | 718 | 32 | 20 | 32 |
| 10:00 AM | 339 | 364 | 703 | 25 | 12 | 25 |
| 11:00 AM | 313 | 363 | 676 | 27 | 13 | 27 |
| Noon - 1PM | 367 | 414 | 781 | 36 | 21 | 36 |
| 1PM - 2PM | 409 | 425 | 834 | 35 | 15 | 35 |
| 2:00 PM | 457 | 583 | 1040 | 47 | 21 | 47 |
| 3:00 PM | 351 | 912 | 1263 | 56 | 15 | 56 |
| 4:00 PM | 415 | 1009 | 1424 | 65 | 18 | 65 |
| 5:00 PM | 462 | 982 | 1444 | 57 | 16 | 57 |
| 6:00 PM | 302 | 620 | 922 | 37 | 18 | 37 |
| 7:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |

Combination of Warrant 1 - Conditions A \& B:

| $80 \%$ | Warrant Met? | No |
| :---: | :---: | :---: |
| $56 \%(70 \%)$ | Warrant Met? | No |

Warrant 1 - Condition B:

| $100 \%$ | Warrant Met? | No |
| :---: | :--- | :--- |
| $70 \%$ | Warrant Met? | No |

Date:
Jurisdiction:
Intersection:
Number of APPROACH Lanes:
Major Street =
Minor Street =
Speed Limit $=\quad 45 \quad(\mathrm{mph})$
Population above 10,000?
70\% Warrant Apply? Yes

Tuesday, September 09, 2014
Geauga County, OHIO
US 422 at Rapids Road
Traffic Signal Warrant (OMUTCD - 2012)

| Data: | Major St: |  | TOTAL | Mino |  | > OF TWO |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6:00 AM | 937 | 308 | 1245 | 75 | 37 | 75 |
| 7:00 AM | 812 | 452 | 1264 | 73 | 46 | 73 |
| 3:30 PM | 392 | 981 | 1373 | 59 | 20 | 59 |
| 4:30 PM | 430 | 1009 | 1439 | 68 | 16 | 68 |
| 5:30 PM | 461 | 840 | 1301 | 48 | 12 | 48 |
|  | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 |

US 422 at Rapids Road



70\% Warrant Apply?
Yes

## US 422 at Rapids Road

## Warrant 3, Peak-Hour Vehicular Volume



Warrant 3, Peak-Hour Vehicular Volume (70\% Factor)


Date:
Jurisdiction:
Intersection:
Number of APPROACH Lanes:
Major Street =
Minor Street =
Speed Litit 1
45 (mph)
70\% Warrant Apply? Yes

|  | Warrant 1 - Condition A |  |  |  |
| :---: | :---: | :---: | ---: | ---: |
|  | $100 \%$ | $80 \%$ |  | $70 \%$ |
|  | $56 \%$ |  |  |  |
| Major Approach: | 500 | 400 | 350 | 280 |
| Minor Approach: | 150 | 120 | 105 | 84 |
| Mid - 1AM |  |  |  |  |
| 1AM - 2AM |  |  |  |  |
| 2:00 AM |  |  |  |  |
| 3:00 AM |  |  |  |  |
| 4:00 AM |  |  |  |  |
| 5:00 AM |  |  |  |  |
| 6:00 AM | + | + | + | + |
| 7:0 AM | + | + | + | + |
| 8:00 AM | + | + | + | + |
| 9:00 AM |  |  |  | + |
| 10:00 AM |  |  |  | + |
| 11:00 AM |  |  |  | + |
| Noon - 1PM |  |  |  | + |
| 1PM - 2PM |  |  |  | + |
| 2:00 PM |  | + | + | + |
| 3:00 PM |  | + | + | + |
| 4:00 PM | + | + | + | + |
| 5:00 PM | + | + | + | + |
| 6:00 PM |  |  |  | + |
| 7:00 PM |  |  |  |  |
| 8:00 PM |  |  |  |  |
| 9:00 PM |  |  |  |  |
| 10:00 PM |  |  |  |  |
| 11:00 PM |  |  |  |  |
| Hours Met | 5 | 7 | 7 | 13 |

Warrant 1-Condition A:

| $100 \%$ | Warrant Met? | No |
| :---: | :--- | :--- |
| $70 \%$ | Warrant Met? | No |

Tuesday, September 09, 2014
Geauga County, OHIO
US 422 at SR 700

## 151

| Data: | Major St: |  | TOTAL | Minc |  | > OF TWO |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mid - 1AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 1AM-2AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 AM | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:00 AM | 767 | 280 | 1047 | 130 | 171 | 171 |
| 7:00 AM | 658 | 401 | 1059 | 143 | 214 | 214 |
| 8:00 AM | 473 | 308 | 781 | 110 | 175 | 175 |
| 9:00 AM | 353 | 319 | 672 | 73 | 88 | 88 |
| 10:00 AM | 276 | 313 | 589 | 96 | 78 | 96 |
| 11:00 AM | 284 | 325 | 609 | 87 | 90 | 90 |
| Noon - 1PM | 311 | 359 | 670 | 92 | 94 | 94 |
| 1PM - 2PM | 346 | 350 | 696 | 103 | 98 | 103 |
| 2:00 PM | 373 | 508 | 881 | 121 | 93 | 121 |
| 3:00 PM | 289 | 754 | 1043 | 143 | 138 | 143 |
| 4:00 PM | 334 | 791 | 1125 | 161 | 130 | 161 |
| 5:00 PM | 345 | 834 | 1179 | 188 | 108 | 188 |
| 6:00 PM | 260 | 565 | 825 | 99 | 98 | 99 |
| 7:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 PM | 0 | 0 | 0 | 0 | 0 | 0 |


| Combination of Warrant 1 - Conditions A \& B: |
| :--- |
| $80 \%$ |
| $50 \%$ |


| $80 \%$ | Warrant Met? | No |
| :---: | :---: | :---: |
| $56 \%$ (70\%) | Warrant Met? | Yes |

## Traffic Signal Warrant (OMUTCD - 2012)



## Warrant 1 - Condition B:

| $100 \%$ | Warrant Met? | Yes |
| :---: | :---: | :---: |
| $70 \%$ | Warrant Met? | Yes |

US 422 at SR 700



70\% Warrant Apply?
Yes

## Warrant 3, Peak-Hour Vehicular Volume



Warrant 3, Peak-Hour Vehicular Volume (70\% Factor)



## STORAGE LANE LENGTHS

Turn lane lengths were calculated for proposed turn lanes at the U.S. Hwy 422 and Rapids Road intersection and the U.S. Hwy 422 and S.R. 700 intersection. Lane lengths were calculated using guidelines specified in the Location and Design Manual Section 401 (Ohio Department of Transportation). Lane lengths based on ODOT standard criteria assume posted speed limits and include vehicle storage and a 125 foot diverging taper. The calculated lengths were compared to the 95th percentile queue lengths generated by SimTraffic modeling software. A recommended length is provided based on the above calculations and engineering judgment. A summary of the lane sizing comparison is shown in Table G1 with lane sizing calculations appended to this section.

Turn lane lengths were calculated using the following parameters:
$>2014$ AM \& PM peak hour traffic volumes
$>45$ MPH design speed for U.S. Hwy 422
> 100 second cycle length
TABLE G1: STORAGE LENGTH SUMMARY -U.S. Hwy 422 Intersections

| Movement | Existing <br> Storage <br> Length (with taper) | Turn Lane Sizing (feet) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ODOT <br> Calculated* | No Block Turn Lane Length | Synchro 95 ${ }^{\text {th }}$ Percentile Queue | Recommended Length* |
| U.S. Hwy 422/Rapids Road |  |  |  |  |  |
| EB Left Turn | 0 | 300 | 800 | 205 | 300 |
| WB Left Turn | 0 | 175 | 460 | 235 | 175 |
| U.S. Hwy 422/S.R. 700 |  |  |  |  |  |
| EB Left Turn | 0 | 275 | 830 | 260 | 275 |
| WB Left Turn | 0 | 175 | 360 | 65 | 175 |

[^2]| MOVEMENT:EB Left <br> PM Unsignalized Through |  |  |
| :--- | :---: | :--- |
| Movement | EBLT |  |
| Design Speed | 45 | mph |
| Cycle Length | 60 | seconds |
| Control (Stop or Signal) | Stop |  |
| Through Volume | 863 | vph |
| Number of Through Lanes | 1 |  |
| Turning Volume | 145 | vph |
| Number of Turning Lanes | 1 |  |
| Design Condition | C | A, B, or C |
| Turning Percentage | $14 \%$ |  |
| Vehicles Per Cycle | 2.4 |  |
| Storage Length | 120 | feet |
| Deceleration/Taper | 125 | feet |
| Calculated Turn Lane Length | 245 | feet |
| No Block Distance | N.A. | feet |
| No Block Turn Lane Length | N.A. | feet |


| MOVEMENT:WB <br> PM Unsignalized Through |  |  |
| :--- | :---: | :--- |
| Movement | WBLT |  |
| Design Speed | 45 | mph |
| Cycle Length | 60 | seconds |
| Control (Stop or Signal) | Stop |  |
| Through Volume | 447 | vph |
| Number of Through Lanes | 1 |  |
| Turning Volume | 14 | vph |
| Number of Turning Lanes | 1 |  |
| Design Condition | B | A, B, or C |
| Turning Percentage | $3 \%$ |  |
| Vehicles Per Cycle | 0.2 |  |
| Storage Length | 50 | feet |
| Deceleration/Taper | 175 | feet |
| Calculated Turn Lane Length | 175 | feet |
| No Block Distance | N.A. | feet |
| No Block Turn Lane Length | N.A. | feet |


| MOVEMENT:EB Left Turn <br> PM Signalized |  |  |
| :--- | :---: | :--- |
| Movement | EBLT |  |
| Design Speed | 45 | mph |
| Cycle Length | 100 | seconds |
| Control (Stop or Signal) | Signal |  |
| Through Volume | 863 | vph |
| Number of Through Lanes | 1 |  |
| Turning Volume | 145 | vph |
| Number of Turning Lanes | 1 |  |
| Design Condition | C | A, B, or C |
| Turning Percentage | $14 \%$ |  |
| Vehicles Per Cycle | 4.0 |  |
| Storage Length | 175 | feet |
| Deceleration/Taper | 125 | feet |
| Calculated Turn Lane Length | 300 | feet |
| No Block Distance | 798 | feet |
| No Block Turn Lane Length | 798 | feet |


| MOVEMENT:WB Left Turn <br> PM Signalized |  |  |
| :--- | :---: | :--- |
| Movement | WBLT |  |
| Design Speed | 45 | mph |
| Cycle Length | 100 | seconds |
| Control (Stop or Signal) | Signal |  |
| Through Volume | 447 | vph |
| Number of Through Lanes | 1 |  |
| Turning Volume | 14 | vph |
| Number of Turning Lanes | 1 |  |
| Design Condition | B | A, B, or C |
| Turning Percentage | $3 \%$ |  |
| Vehicles Per Cycle | 0.4 |  |
| Storage Length | 50 | feet |
| Deceleration/Taper | 175 | feet |
| Calculated Turn Lane Length | 175 | feet |
| No Block Distance | 460 | feet |
| No Block Turn Lane Length | 460 | feet |


| MOVEMENT:EB Left Turn <br> PM Peak hour volumes |  |  |
| :--- | :---: | :--- |
| Movement | EBLT |  |
| Design Speed | 45 | mph |
| Cycle Length | 100 | seconds |
| Control (Stop or Signal) | Signal |  |
| Through Volume | 904 | vph |
| Number of Through Lanes | 1 |  |
| Turning Volume | 108 | vph |
| Number of Turning Lanes | 1 |  |
| Design Condition | C | A, B, or C |
| Turning Percentage | $11 \%$ |  |
| Vehicles Per Cycle | 3.0 |  |
| Storage Length | 150 | feet |
| Deceleration/Taper | 125 | feet |
| Calculated Turn Lane Length | 275 | feet |
| No Block Distance | 828 | feet |
| No Block Turn Lane Length | 828 | feet |


| MOVEMENT:WB Left Turn <br> PM Peak hour volumes |  |  |
| :--- | :---: | :--- |
| Movement | WBLT |  |
| Design Speed | 45 | mph |
| Cycle Length | 100 | seconds |
| Control (Stop or Signal) | Signal |  |
| Through Volume | 337 | vph |
| Number of Through Lanes | 1 |  |
| Turning Volume | 20 | vph |
| Number of Turning Lanes | 1 |  |
| Design Condition | C | A, B, or C |
| Turning Percentage | $6 \%$ |  |
| Vehicles Per Cycle | 0.6 |  |
| Storage Length | 50 | feet |
| Deceleration/Taper | 125 | feet |
| Calculated Turn Lane Length | 175 | feet |
| No Block Distance | 358 | feet |
| No Block Turn Lane Length | 358 | feet |



| ITEM | GEA-422-10.93-13.31 <br> MAIN MARKET ROAD (US 422) AT CLARIDON ROAD (SR 700) PRELIMINARY CONSTRUCTION ESTIMATE - OCTOBER 14, 2014 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DESCRIPTION | QUANTITY | UNIT COST |  | TOTAL COST |  |
| 201 | CLEARING AND GRUBBING | 1 LS | \$ | 10,000.00 | \$ | 10,000.00 |
| 202 | PAVEMENT REMOVED, ASPHALT | 180 SY | \$ | 12.00 | \$ | 2,160.00 |
| 202 | WALK REMOVED | SF | \$ | 1.50 | \$ |  |
| 202 | MEDIAN REMOVED | SY | \$ | 5.00 | \$ | - |
| 202 | CURB REMOVED | 900 LF | \$ | 5.00 | \$ | 4,500.00 |
| 202 | CATCH BASIN OR INLET REMOVED | 3 EA | \$ | 500.00 | \$ | 1,500.00 |
| 203 | EXCAVATION | 850 CY | \$ | 15.00 | \$ | 12,750.00 |
| 203 | EMBANKMENT | 50 CY | \$ | 12.00 | \$ | 600.00 |
| 204 | SUBGRADE COMPACTION | 1700 SY | \$ | 2.00 | \$ | 3,400.00 |
| 206 | CEMENT STABILIZED SUBGRADE, 16" DEEP | SY | \$ | 5.50 | \$ | - |
| 252 | PAVEMENT SAWING | 1550 LF | \$ | 3.00 | \$ | 4,650.00 |
| 254 | PAVEMENT PLANING, ASPHALT CONCRETE | 4000 SY | \$ | 3.00 | \$ | 12,000.00 |
| 301 | ASPHALT CONCRETE BASE 6" | 300 CY | \$ | 125.00 | \$ | 37,500.00 |
| 304 | AGGREGATE BASE 10" | 500 CY | \$ | 60.00 | \$ | 30,000.00 |
| 407 | TACK COAT | 800 GAL | \$ | 3.00 | \$ | 2,400.00 |
| 448 | ASPHALT CONCRETE INTERMEDIATE COURSE 1.5" | 100 CY | \$ | 150.00 | \$ | 15,000.00 |
| 448 | ASPHALT CONCRETE SURFACE COURSE 1.5" | 270 CY | \$ | 175.00 | \$ | 47,250.00 |
| 451 | CONCRETE PAVEMENT | SY | \$ | 75.00 | \$ | - |
| 603 | 15" CONDUIT | 100 LF | \$ | 75.00 | \$ | 7,500.00 |
| 604 | CATCH BASIN | 3 EA | \$ | 2,500.00 | \$ | 7,500.00 |
| 604 | MANHOLE, NO. 3 | 1 EA | \$ | 3,000.00 | \$ | 3,000.00 |
| 605 | 6" BASE PIPE UNDERDRAIN | 1600 LF | \$ | 8.00 | \$ | 12,800.00 |
| 606 | GUARD RAIL | 200 LF | \$ | 20.00 | \$ | 4,000.00 |
| 608 | 4" CONCRETE WALK | SF | \$ | 5.00 | \$ | - |
| 608 | CURB RAMPS | EA | \$ | 450.00 | \$ | - |
| 609 | CURB | 900 LF | \$ | 18.00 | \$ | 16,200.00 |
| 609 | CONCRETE DRIVE APPROACH | 200 SY | \$ | 75.00 | \$ | 15,000.00 |
| 609 | 6" CONCRETE TRAFFIC ISLAND | SY | \$ | 50.00 | \$ | - |
| 625 | RED LIGHT CAMERAS RELOCATED | EA | \$ | 7,500.00 | \$ | - |
| 630 | SIGNAGE | 1 LS | \$ | 3,500.00 | \$ | 3,500.00 |
| SPECIAL | LANDSCAPING MOUND | LS | \$ | 15,000.00 | \$ | - |
| 632 | TRAFFIC SIGNAL INSTALLATION | 1 EA | \$ | 150,000.00 | \$ | 150,000.00 |
| 644 | PAVEMENT MARKINGS | 1 LS | \$ | 7,500.00 | \$ | 7,500.00 |
| 659 | TOPSOIL | 100 CY | \$ | 25.00 | \$ | 2,500.00 |
| 659 | SEEDING AND MULCHING | 2000 SY | \$ | 3.00 | \$ | 6,000.00 |
| 832 | SWPPP | 1 LS | \$ | 10,000.00 | \$ | 10,000.00 |
| 832 | EROSION CONTROL | 3500 EA | \$ | 1.00 | \$ | 3,500.00 |
| Subtotal \$ 433,000.00 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| 614 | MAINTAINING TRAFFIC | 1 LS | \$ | 20,000.00 | \$ | 20,000.00 |
| 619 | FIELD OFFICE, TYPE B | 6 MN | \$ | 2,000.00 | \$ | 12,000.00 |
| 623 | CONSTRUCTION LAYOUT STAKES | 1 LS | \$ | 6,500.00 | \$ | 6,500.00 |
| 624 | MOBILIZATION | 1 LS | \$ | 20,000.00 | \$ | 20,000.00 |
|  |  |  |  |  |  |  |
|  |  |  |  | Subtotal | \$ | 492,000.00 |
|  |  |  |  |  |  |  |
| Design Risk (35\%) \$ 173,000.00 |  |  |  |  |  |  |
| Subtotal \$ 665,000.00 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Inflation Cost (10\%) \$ 67,000.00 |  |  |  |  |  |  |
| Total \$ 732,000.00 |  |  |  |  |  |  |

[^3]
# MAIN MARKET ROAD AT CLARIDON ROAD 

PRELIMINARY RIGHT OF WAY ESTIMATE - OCTOBER 14, 2014


Notes:
1 Existing R/W estimated using GIS parcel lines, where available
2 Where R/W cannot be easily estimated from GIS parcels, existing R/W is assumed to be 1 ' behind walk
3 Property value based upon auditor's records


[^0]:    Note:Letter/Number - Level of Service/Average Delay per Vehicle

[^1]:    Note: Letter/Number - Level of Service/Average Delay per Vehicle

    * Intersection w as analyzed according to HCM 2000 methodology w hich more closely resembles the existing condition

[^2]:    * Length includes decceleration, rounded to nearest 5 ft .

[^3]:    1 Right of way is estimated separately
    2 Existing pavement is assumed to be full depth asphalt
    3 Pavement widening is assumed to be full depth asphalt
    4 Utility relocation not included
    5 Construction estimated to occur in mid 2017

