## OHIO DEPARTMENT OF TRANSPORTATION 2017 REHABILITATION FEASIBILITY STUDY PID NO 99972

# DETROIT-SUPERIOR BRIDGE OVER CUYAHOGA RIVER BRIDGE NO. CUY-6-1456

SFN: 1800930



REVISED MAY 2017

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## I. EXECUTIVE SUMMARY

The original feasibility study did not meet budget constraints for this project. The intent of the revised feasibility study is to summarize several additional Alternative No. 2's and their associated costs so that the District can make an informed decision for rehabilitation.

CUY-6-1456 (SFN 1800930), commonly known as the Detroit-Superior Bridge and later renamed the Veteran's Memorial Bridge, is a 1917 double-deck structure carrying vehicular and pedestrian traffic over the Cuyahoga River Valley (**Photos 1 & 2**). The bridge is approximately 2,880 feet long, including 1,673 feet of subway tunnel that is linked by the lower deck. In its original design, the upper deck carried vehicular and pedestrian traffic while the lower deck had four streetcar lines and capacity for two future tracks. The streetcar lines across the Detroit-Superior Bridge were discontinued in 1953. The Detroit-Superior Bridge is included on the National Register of Historic Places. With the bridge reaching it's 100th year of service, one of the goals is to provide a rehabilitation scheme that will allow the bridge to be of service for the next 50 years.

Pennoni was charged with the following tasks for the Feasibility Study:

- 1. Document the extent of the deterioration of the concrete on the approach spans.
- 2. Research the use Fiber Reinforced Polymer (FRP) to contain the concrete repairs and future deterioration over the public areas.
- 3. Identify the right-of-way needs for the rehabilitation.
- 4. Miscellaneous items such as, MOT, Navigation Lights, additional security for the Central Street Bridge Tenders Garage and vandal proofing the lower portions of the approach spans.
- 5. Provide alternates for the necessary repair.

In addition to the in-depth Inspections made in 2015 and in 2016, Pennoni documented the extensive concrete deterioration in the West Station, Spans 1A, 1B and 1 through 13 and the East Station. Several rehabilitation projects have been completed throughout the 100-year life span, including major rehabilitations in 1967-1970 and 1995-1997. The most recent rehabilitation from 2014-2016 was to repair concrete deterioration throughout the structure. Most of the deteriorated areas, including some repaired in the 1995-97 rehabilitation showed signs of reinforcing steel oxidation, or rusting. Several of those areas are in the West Station and lower deck area that get no salt. Therefore, non-chloride related concrete corrosion is likely present. Concrete corrosion is the chemical, colloidal or physicochemical deterioration and disintegration of solid concrete corrosion, carbonation, is a potential contributor of the ongoing deterioration. To verify this assumption, samples of the spalled concrete were tested for pH content (**Appendix C**). The concrete material of the samples show low alkalinity levels (< 12), suggesting that carbonation may be occurring. Carbonation is the result of CO<sub>2</sub> absorption into the concrete. In cities like Cleveland, carbonization can permeate concrete as



much as 0.04 inches per year, or 3 inches before the epoxy-urethane sealer was applied in 1997.

Several different FRP materials were investigated. Because the goal is to contain the deteriorated concrete and not to strengthen the members, it was determined that a low strength FRP wrap would be adequate for this application. The wrap would not alter the existing load paths. It should be noted that ODOT Central Office is studying FRP wrap for seismic containment on bridge columns. This assessment is outside the scope of our work and no consideration of seismic loading was taken into consideration.

Pennoni also looked at cathodic protection to stabilize the increasing concrete corrosion rate, and possibly to reverse it. Cathodic protection can be obtained with passive induction using anode pucks or active induction such as impressed current. Both have been used successfully over the past two decades. For this application, the active cathodic protection would provide the best results.

Primary construction tasks of the three alternates in this feasibility study are:

- 1. Maintenance Alternate: Replace upper deck wearing surface, Remove the deteriorated concrete but not patch the deteriorated concrete on the entire bridge.
- 2. FRP Alternate: Research the use of Fiber Reinforced Polymer (FRP) wraps to contain the concrete repairs and future deterioration over public areas. Replace upper deck wearing surface, Remove and patch the deteriorated concrete, Use of fiber wrap on the entire bridge.
- 3. Cathodic Protection Alternate. Replace upper deck wearing surface, patch deteriorated concrete, and apply active cathodic protection.

Alternate No. 1, at \$2.6 Million, does meet the purpose and need of the project, and will only provide a 5-year service life since further deterioration is not inhibited. Alternate No. 2, at \$26.0 Million, does meet the purpose and need of the project, and will provide 25 to 50-year service life and enhanced public safety. This alternate will not stop the current deterioration. Potentially, periodic small projects will be needed to secure loose or damaged FRP wrap. Both FRP suppliers that we spoke with cautioned us on the permeability of the FRP material. While both glass and carbon FRP wraps do have some permeability, it is not as great as exposed concrete. This may lead to further deterioration and higher rehabilitation cost in the future.

Alternate No. 2 has been broken down into smaller projects to meet the budget needs of the District. The recommended alternative is <u>Alternative No. 2C</u> based on addressing public safety, extending the service life of the bridge, and economic analysis.

Alternate No. 3 is at \$33.2 Million. While it may be the best solution for extending the life of the existing concrete for another 50 years, it does not meet our budget constraints.



All alternatives include the Maintenance Work Task 1 that were requested. A summary of Estimated Construction Costs is included in **Appendix A**. All estimates have been projected to construction in Year 2020.



Photo 1– North Elevation, Spans 4 through 6.



Photo 2– East Approach Spans Deck, Looking East.



## II. PURPOSE & NEED

This project is being performed to restore the integrity of the bridge's concrete portions by arresting the deterioration of the concrete superstructure and substructure. On occasion, loose concrete has fallen, creating a hazard to the public safety below. In its most recent bridge inspection, the bridge, CUY-6-1456 (SFN 1800930) General Appraisal Rating was a *5* or *Fair* Condition. With this rehabilitation project, ODOT expects to maintaining the structure in good condition for a service life of 50 years.



Figure 1 – Location of CUY-6-1456 (Circled).



#### Scope of Repairs

The repairs discussed in this feasibility study are as follows:

- Patching or replacement of the upper deck concrete wearing surface.
- Elimination of falling concrete over public areas.
- Investigation of FRP wrap on lower superstructure components.
- Continuation of repairs in the West Station, West 25<sup>th</sup> Street Tunnel and Detroit Avenue Tunnel.
- Placement of masonry block wall in Span 1A to prevent unauthorized access.
- Placement of a vandal resistant barrier to restrict unauthorized access from the Center Street Swing Bridge operator's car shelter to the Pier 4 pedestals.

#### **Definition of Public Spaces**

For this feasibility study, the defined public spaces below the structure are shown in **Appendix B**. Areas designated as public space meet the following criteria:

- 1. Areas below or within 10 feet of concrete arch spans, and
- 2. Areas commonly occupied by vehicular and/or pedestrian traffic.

Following this guide, Span 1 and Span 4 are not considered public space. Following the recent announcement that the Cleveland Metroparks plan to create a new Irishtown Bend park, 75% of the area beneath Span 2 has been added to the public space inventory. <sup>1</sup>



<sup>&</sup>lt;sup>1</sup> Cleveland Plain Dealer, Port hires design team to envision transformation of Irishtown Bend, February 9, 2017.

## III. BRIDGE CONDITION

#### Bridge Description

CUY-6-1456 (SFN 1800930), commonly known as the Detroit-Superior Bridge and later renamed the Veteran's Memorial Bridge, is a 1917 double-deck structure carrying vehicular and pedestrian traffic over the Cuyahoga River Valley (See Photos 1 & 2). The bridge is approximately 2,880 feet long, including 1,673 feet of subway tunnel that is linked by the lower deck. In its original design, the upper deck carried vehicular and pedestrian traffic while the lower deck had four streetcar lines and capacity for two future tracks. The streetcar lines across the Detroit-Superior Bridge were discontinued in 1953. The Detroit-Superior Bridge is included on the National Register of Historic Places.

General plan and elevation views of the Detroit-Superior Bridge are included in **Figure 2**. **Figure 3** contains the typical nomenclature of the concrete elements of the main concrete spans.

The Detroit-Superior Bridge is composed of three distinct units. The first unit, the West Approach, is comprised of the West Station area spanning a total of 350 feet west of Tower A and two abandoned subway tunnels: the Detroit Avenue Tunnel (660 feet long) and the West 25<sup>th</sup> Street Tunnel (480 feet long). Several utilities are pass through the West Station and tunnels. Since the late 1980s, the West Station has been opened to the public for tours and festivals.

The main unit is Spans 1A, 1B and 1 through 13. Spans 1A and 1B are transition structures from the subterranean West Station to the double-deck approach and main spans. These two concrete cellular spans total 220 feet long and each has enclosed cellular construction below the lower deck.

The main spans, Span 1 through 13, are double-deck spans with vehicular and pedestrian traffic on the upper deck and utilities and maintenance access on the lower deck. Spans 1 through 3, 5 through 11 and Span 13 are concrete open spandrel arch spans, and Span 12 is a concrete encased steel half through arch. The main span, Span 4, is a 591-foot, three-hinged steel half-through arch truss in a Pratt configuration.

The third unit, the East Station, is a concrete cellular span that extends 165 feet past the East Abutment. A three panel long, cellular construction is present under the East Station lower deck immediately behind the East Abutment.











Figure 3 – Upper & Lower Deck Element Nomenclature, Approach Spans.

#### **Inspection Procedure**

Pennoni performed an in-depth inspection of the concrete components included in the scope of this feasibility study in conjunction with the 2016 in-depth inspection previously included in Project No. PID 93400 during September 13 through 16, 2016. Additional inspection was performed December 6 through January 10. Personnel included William J. Vermes PE, Christian Lunt, PE, Dale Arnold PE, Matthew Paroda EI, and Elizabeth Trapp, EI, Jessica Sizemore, EI and Alisha Ruff, EI. Inspection access was achieved as follows:

Detroit Avenue & W. 25<sup>th</sup> Street Tunnels – Extension ladders and delamtech sounding tool.

West Station – 30-foot electric manlift.

Spans 1-3, 5-13 Upper Deck superstructure – 40-foot electric manlift.

Spans 3, 5-12 Lower Deck superstructure – 80-foot diesel manlift and snooper.

East Station & Subway - Extension ladders and delamtech sounding tool.

Lighting in the tunnels, West Station and East Station and Subway was provided by two LED light stands, medium duty extension cords and a portable gasoline generator. Between October 6 and November 8, vandals destroyed the electric conduits and lighting in the West Station.



The presence, or lack of, top and bottom reinforcing steel was investigated in Spans 1 - 3 and 5 - 9 using a commercial metal detector.

#### **Construction & Rehabilitation History**

The Detroit-Superior Bridge was constructed from 1914 through 1917 to provide a high level vehicular and streetcar crossing over the Cuyahoga River, connecting the Ohio City community and Downtown Cleveland. The bridge replaced the Superior Viaduct, opened in 1878. Construction of the foundation began in 1913. The steel arch truss, Span 4, was erected from July 24 to November 6, 1915. On October 8, 1915, the two halves of the main truss were connected<sup>2</sup>. Construction of the arch ribs began in May 1915 in Span 6 and proceeded eastward. The bridge opened to traffic on December 24, 1917.

By the mid-1930s, spalled concrete was occurring due to improper drainage. Repairs were discussed but postponed due to the needs of World War II, and ultimately not performed until the 1960s.

The Detroit-Superior Bridge has received a series of various major and minor rehabilitations as follows<sup>3</sup>:

- 1. 1967-70 Major Rehabilitation
  - a. Removal of the original upper deck consisting of four vehicular lanes and two 15-foot wide sidewalks.
  - b. Strengthening or replacement of all upper deck concrete floorbeams.
  - c. Span 4: Erection of new steel floorbeam cantilevers.
  - d. Construction of the new upper deck with six vehicular lanes and two five-foot wide sidewalks.
- 2. 1995-97 Major Rehabilitation
  - a. Replacement of the upper and lower deck floors.
  - b. Replacement of select upper and lower concrete floorbeams, columns, jack arches and pier shafts (**Table 1**).
  - c. Patching over 70,000 SF of concrete superstructure.
  - d. Application of epoxy-urethane or non-epoxy sealer to most exposed concrete surfaces.
  - e. Span 4: Replacement of all steel hangers, Panel Points 6 through 6'.
  - f. Replacement of Upper Deck and Lower Deck Floor Beams 5 and 5' and stringers.
  - g. Painting of all steel superstructure components.

<sup>&</sup>lt;sup>3</sup> Vermes, William J., Gasparini, Dario A. & Conley, Natalie, *Cleveland's Historic Bridges: Architectural & Engineering Masterpieces*, Publication of the 7<sup>th</sup> Historic Bridge Conference, Cleveland, Ohio, 2001.



<sup>&</sup>lt;sup>2</sup> Beyer, William E, The History of the Veterans Memorial Bridge, 90<sup>th</sup> Anniversary Edition, Bookmasters, Inc, Ashland, Ohio.

- h. Installation of new drainage system.
- i. Installation of architectural lighting.
- 3. 2003 North Sidewalk Linear Park Conversion.
  - a. Conversion of vehicular traffic to two westbound and one eastbound lane between the steel trusses and on eastbound lane on the Span 4 south cantilever.
  - b. Widening of the north sidewalk. With longitudinal trench drainage.
  - c. Installation of public art and benches along the modified north sidewalk.

Member	Total Members	Members Replaced	Total Percent Replaced
Upper Deck Floor Beams	686	316	38%
Upper Deck Columns	693	179	26%
Upper Deck Jack Arches	564	260	45%
Lower Deck Floor Beams	548	50.5	11%
Lower Deck Corbels	279	79	28%
Lower Deck Jack Arches	520	176	34%
Lower Deck Columns	488	8	2%
Upper Exterior Pier Shafts	32	17.5	55%
Lower Exterior Pier Shafts	28	5.5	20%

Table 1 – 1995-97 Detroit-Superior Bridge Rehabilitation Concrete SuperstructureMember Replacement Summary, Spans 1 to 3, 5 to 13 & East Station.4

4. 2014-16 Rehabilitation Work Summary

In 2014, a minor rehabilitation project began to address deteriorating concrete surfaces. Local patching was performed of the upper deck wearing surface. Significant and minor patching was performed on the lower deck superstructure and piers in Span 2 and from Span 7 to the East Abutment. In the West Station, four columns, C13, C14, C20 and C21, were replaced in kind along with patching from

<sup>&</sup>lt;sup>4</sup> Vermes, William J., *Rehabilitation of The Detroit-Superior Bridge*, Proceedings of an International Conference on Historic Bridges to Celebrate the 150th Anniversary of the Wheeling Suspension Bridge, West Virginia University Press, 1999, pp. 117-132.



column lines 25 to 31. Painting of the Span 4 superstructure between the upper and lower deck was also performed.

Work for this rehabilitation was suspended in early 2016 to reassess the repair needs of the structure and address safety concerns in public areas below the bridge. For the remainder of this report, the 1995-97 and 2014-16 rehabilitations will be referred to as the 1995 rehabilitation and the 2014 rehabilitation, respectively.

## IV. STRUCTURE REPAIR NEEDS

Discussion of repair needs begins with maintenance repairs of Alternate No. 1. The work tasks associated with the deterioration of the concrete superstructure and public safety below the bridge is discussed as each repair need is approached, west to east and top to bottom.

#### Upper Deck Wearing Surface

The upper deck wearing surface was poured in 1995 and placed into service January 1997. Records show the wearing surface began exhibiting significant deterioration after 2010. Following patching in 2014, the wearing surface continued to deteriorate at increasing rates, especially in Spans 7 through 10 (**Table 2**). Soundings showed that the delamination patterns generally follow the wheel paths. Further observations show that the deck is subjected to impact loads as commercial trucks cross the bridge, especially east bound traffic, at speeds greater than the posted speed limit. At 20 years, the overlay is nearing the end of the expected service of 25 years. Because the rehabilitation project is scheduled for start in 2019, removal of the deficient wearing surface via hydro-demolition and placement of a micro-silica wearing surface is the recommended repair for the wearing surface. Since few signs of distress are present on the upper deck underside are present, no deck cores are recommended.



Span	Wearing Surface Deterioration (SF)		WB Area of Deck	EB Area of Deck	Concrete Repair (%)		
	WB	EB	(37)	(37)	WB	EB	Total
Span 1A	36	128	2890	2890	1.2	4.4	2.8
Span 1B	81	162	3607	3607	2.2	4.5	3.4
Span 1	450	627	3718	3718	12.1	16.9	14.5
Span 2	0	0	4685	4685	0.0	0.0	0.0
Span 3	56	59	6368	6368	0.9	0.9	0.9
Span 4	1495	2441	17228	17228	8.7	14.2	11.4
Span 5	0	19	5186	5186	0.0	0.4	0.2
Span 6	259	8	4191	4191	6.2	0.2	3.2
Span 7	1367	664	4117	4117	33.2	16.1	24.7
Span 8	1724	1792	4170	4170	41.3	43.0	42.2
Span 9	814	354	3698	3698	22.0	9.6	15.8
Span 10	642	754	3688	3688	17.4	20.4	18.9
Span 11	76	360	2864	2864	2.7	12.6	7.6
Span 12	108	229	3444	6642	3.1	3.4	3.3
Span 13	28	0	2245	4331	1.2	0.0	0.4
East Station	44	0	8904	17172	0.5	0.0	0.2
Direction Subtotals:	7,180	7,597	81,003	94,555			

14,777 Total: SF

8.42% Total % Deteriorated =

Table 2 – Upper Deck Wearing Surface Deterioration Summary



#### W. 25<sup>th</sup> Street & Detroit Avenue Tunnels

The tunnels have received little rehabilitation during their service. Intermittent spalls present along the wall bases have changed little since the late 1980s, and may be caused by acidic ballast used for the street car lines but now removed since the 1950s. Wall deterioration is primarily located at the wall panel joints. The roof of the West 25<sup>th</sup> Street Tunnel exhibits little delamination. The original roof of the Detroit Avenue Tunnel is heavily spalled, however a new structural slab was placed above this slab during the 1995 rehabilitation. Since this is not a public area when the West Station is open to the public, no repair to the Detroit Avenue Tunnel is recommended.

#### West Station Columns & Jack Arches

Due to budgetary reasons, only essential repairs were performed in the West Station and tunnels during the 1995 rehabilitation. Since then, deterioration of the West Station columns and longitudinal beams (jack arches) has steadily increased despite repair of the roof slab and placement of a Type 2 waterproofing membrane.

Most West Station deterioration is present on the jack arches and columns of Lines A, B, C and D, roughly centered on the expansion joint and sag point between Columns 20 and 21. Location of deterioration is included in **Appendix F**. As shown in **Appendix G**, the deterioration has been steadily migrating east and west from this centroid of corrosion.

Along the north face of the Line A jack arches, a longitudinal construction joint has allowed water and salt infiltration, resulting in accelerated deterioration of the jack arches and columns below (**Figure 4**). This construction joint is part of the West Station original construction to facilitate a new rail line and expansion of the station northward.

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	ENO MT702 (11406 BARS 52 C tog)	END-1-17701
		Eraner C

Figure 4 – Longitudinal Construction Joint (Circled, referenced as Tar Paper Joint), Above Line A North Face, Original Construction Drawing No. A2246.



#### Lower Deck Columns

The cause and magnitude of deterioration present among the lower deck columns is based on the column location. Away from the piers, spandrel columns have isolated delaminations and spalls commonly due to corrosion of the 1/2-inch square horizontal square bars. Several exterior columns have larger deterioration areas due to corrosion of the main steel reinforcement with 3-inch cover. On several exterior columns, lower deck corbel deterioration has propagated to the adjoining column surfaces below.

For the lower deck columns adjacent to piers, several columns have large delaminated surfaces likely due to the chloride contamination up through the beginning of the 1995 rehabilitation. The column surfaces facing the piers patched in 1995 are often delaminated now due either to continuing reinforcement corrosion or the insufficient space to perform proper shotcreting.

Estimated FRP lower column wrap quantities are based on the surface area form top of the arch pedestal up to the bottom of the lower floorbeam fillet. Following this delineation of the lower columns, any column less than two feet tall or non-existent at the center of the arch rib, are assumed to be too short to merit FRP wrapping and are not included in the quantities. Observation of the column pedestals showed no deficiencies, likely due to the increased reinforcement cover they provide. No FRP wrap of the pedestals is recommended due to durability and complexity of wrapping.

#### Lower Deck Floor Beams

During the 1995 rehabilitation, most lower deck floorbeam patching was for shallow (cover less than 1") over stirrup reinforcement. Now, new delaminations and spalls have occurred where stirrup cover is  $1^{1}/_{4}$  to  $1^{1}/_{2}$  inches, indicating that the corrosion mechanism has not stopped with the applied sealer (**Photo 3**). Elsewhere, ongoing corrosion of the bottom tensile reinforcement has resulted in 1995 several shotcrete patch failures, as the patches have been forced from the floorbeam bottoms (**Photo 4**). With the likelihood of eventual global concrete corrosion, it is recommended that FRP anchors be placed along the top of lower floorbeams to prevent a full-face failure of the wrap.





Photo 3 – Newly Developing Lower Deck Floor Beam Delaminations (Circled), South Bay, Span 8.



Photo 4 – Reinforcing Steel with Active Corrosion, Lower Deck Floorbeam 14, South Bay, Span 6.



#### Lower Deck Corbels

The lower deck corbels perform as part of a structural cantilever of the lower deck floor beams, supporting the upper deck columns and loads above. During the 1995 rehabilitation, 20% of the corbels were replaced. Currently, additional corbels have delaminated or spalled primarily due to the following causes:

- 1. Lack of Cover: One architectural feature of the corbels is that they are stepped down two inches on each side, thus providing significantly less cover for the slanted vertical anchorage reinforcement of the upper deck columns.
- 2. End Span Lower Deck Corbels: During the 1995 rehabilitation, construction of new corbel and/or lower deck exterior pier shafts used a thin felt bond breaker fabric between the adjoining surfaces (Photo 5). This bond breaker has not performed adequately, resulting in spalls in either the corbels, lightly reinforced pier shafts, or both. The first occurrences of this failure mode appeared by 2000 and have been steadily progressing since.

Replacement and/or patching of deficient corbels will be performed. Adjacent to the pier shafts, all corbel/pier shaft interface will be modified, regardless if repair is needed or not. A  $^{3}/_{8}$ -inch paraffin bond breaker is recommended to be placed between the concrete surfaces.

#### Arch Ribs

The arch ribs exhibit spalls and isolated delaminations and spalls along the corners of the arch ribs (Photo 5). Additional delaminations are present on the intrados (underside) of the arches. Generally, no deterioration is present along the arch ribs side since no shear reinforcement is present throughout the arches. Furthermore, the field inspection verified that contrary to the original construction plans, top and bottom mat steel was placed continuously in the arches of Span 1 through 3, 5, and 7 through 9. In Span 6, however, no main reinforcement was detected in the North Exterior and Interior arch ribs between Columns 3 and 5, and Columns 11 and 13. Span 6 was the first concrete span constructed, and therefore likely the only span to have discontinuous reinforcement.

#### Lower Deck Pier Shafts

Most upper deck pier shaft and some lower deck pier shaft were replaced during the 1995 rehabilitation. Generally, the exterior lower deck pier shafts have little deterioration except for two occurrences. First, areas cast in concrete with the insufficient bond breaker have spalled due to thermal movement of the adjacent spandrel column (**Photo 6**). Next, on the Pier 6 South Exterior Lower Pier Shaft, a 140 SF spalled area exhibits an apparent deep scaling.





(Photo 7 & Figure 5).

Photo 5 – Spalled Original Concrete & Secure 1996 Shotcrete Patch, Span 7 South Interior Arch Rib.



This is likely a due to failure of the original encased drain pipe within this shaft. It is

anticipated sound concrete is not present until at least a depth of two feet.

Photo 6 – Spalled & Loose Concrete Due to Ineffective Bond Breaker (Location denoted in yellow), Pier 5 Lower Deck Pier Shaft & South Lower Deck Corbel 1, Span 6.





Photo 7 – Deep Concrete Deterioration, Pier 6 South Lower Deck Pier Shaft.



Figure 5 – Estimated Deterioration Depth, Pier 6 South Lower Deck Pier Shaft.



#### East Subway

Column M22, located along the north wall of the East Subway, adjacent to the compression seal deck joint between the East Station and the East Subway, has more than 60% section loss (**Photo 8**). Columns M27, East Subway, and South Exterior Column 20, also have advanced deterioration and require replacement. Approximately 30% of the north wall of the East Subway is spalled or delaminated, and requires patching.



Photo 8 – 60% Section Loss, Column M22, East Station.



#### Lower Deck Masonry Wall

Vandals have been accessing the lower deck and West Station increasingly the last several years along the southwest corner of Span 1A. Efforts to secure this area with chain link fencing and perforated steel plates have not been successful. More recently, vandals have set up step ladders at the northeast corner of Span 13 (Photo 9). The preferred method of securing the access to the lower deck via these points is placement of masonry block wall on top of the lower deck railing. The recommended location of the masonry block wall is shown in **Figure 6.** 

#### Center Street Bridge Tender's Car Shelter

Within the last decade, a chain-link car shelter, measuring 17'-4" wide by 22'-6" deep with a roof, has been built adjacent to the west face of Pier 4. This shelter provides a secure parking area for the Center Street Swing Bridge operators. Vandals have accessed the interior of the shelter and pushed open a hole in the roof, gaining access to the south pedestal of Pier 4 and on up the Span 4 steel superstructure. Implementation of recent security measures on the Detroit-Superior and Lorain-Carnegie Bridges shows that construction of such features emboldens trespassers to damage and pass through these barriers. Therefore, it is recommended that instead constructing a vandal-proof fence atop of the shelter, the east half of the shelter be rebuilt, narrowing the shelter by four feet and removing trespasser access to the pedestal. This reduced shelter size is comparable to the bridge operator car shelter at the West 3<sup>rd</sup> Street Lift Bridge.



Photo 9 – Ladder Used by Vandals to Access Lower Deck, Span 13 at East Abutment.







Figure 6 – Recommended Location of Security Wall.



## V. RECOMMENDED REPAIR STRATEGIES

#### General

The field inspection revealed that the delamination currently present does not follow the common opinion that concrete patches tend to fail. Throughout the lower superstructure, few examples of shotcrete patch failure due to debonding are present. In fact, several areas shotcrete failure are due the continued reinforcement corrosion or failure of the adjacent original concrete, also from reinforcement corrosion.

During the 1995 rehabilitation, the epoxy-urethane sealer placed on all lower superstructure exterior and upper superstructure components as well as piers as a barrier protection, is mostly intact after nearly 20 years of exposure. However, the sealer at best only slowed the rate of corrosion within these concrete elements, including those that have not been subjected to poor drainage and chlorides attack.

Thirteen concrete pH tests were performed on samples obtained from various delaminated lower superstructure elements (**Table 3 & Appendix C**). Several samples exhibited pH levels less than 12, suggesting that the passivation layer protecting the steel reinforcement has been broken due to hydroxide ion transfer, resulting in concrete corrosion. Due to the random nature of the pH results, it is not possible to conclusively determine if carbonation is the cause for the pH lower pH readings.



Sample	Span	Member	Location	Prec Material pl		ninant evel	
No.					Near Surface	Int.	Comments
1A	7	Arch Rib	South Interior	Concrete	9 - 10	9 - 10	Bottom North Corner, near center
1B	7	Arch Rib	South Interior	Shotcrete	9	12	Bottom North Corner, near center
2	7	LD Floor Beam	4 North Bay	Shotcrete	9	9, 12	
3	7	LD Column	N. Int. 14	Concrete	9	12	
4	8	Jack Arch	N. Int. 8-9	Shotcrete	9	9, 12	
5	8	LD Floor Beam	9 Center Bay	Concrete	10 - 11	9 - 12	$1 \frac{1}{2}$ " cover total
6	8	LD Floor Beam	10 Center Bay	Concrete	10 - 11	9, 12	$2 \frac{1}{2}$ " cover total
7	8	LD Floor Beam	11 Center Bay	Concrete	10 - 11 9, 12		$2^{1}/_{2}$ " cover total
8	8	LD Floor Beam	14 South Bay	Concrete	9 - 10	12	
9	9	LD Column	N. Int. 13	Concrete	Aggregates: 10-11 Sand & Cement: 9		West Face
10	10	LD Floor Beam	1 South Bay	Shotcrete	Mostly 12; Some aggregates, 9		
11	10	LD Floor Beam	2 South Bay	Concrete	Aggregates: 10-11 Sand & Cement: 9		From above Sample No. 10
12	10	LD S. Ext. Pier Shaft	West Face	Shotcrete	Mostly 12; Some aggregates, 9		West face, near corbel

Table 3 – Concrete pH Tests Summary

**Appendix D** contains both a summary and estimated patching quantities calculations for superstructure and pier elements. **Appendix E** contains a summary of the estimated FRP wrap quantities and the associated calculations.

Discussion of the recommended structural repairs materials are divided among specific objectives: repair, protection and prevention. Each material is discussed as follows:

#### Concrete Patching/Replacement Materials (Repair)

Concrete patching shall be prepared, formed and finished in accordance with Item 519. Concrete members that are identified to require complete replacement including select columns, West Station beams and lower deck corbels shall be in accordance with Item 511. Recognizing the varying level of effort for patching or repairing concrete elements of the Detroit-Superior Bridge, the following repair/replacement items have been included in the



rehabilitation quantities. For cost estimating, concrete patching has been divided among the following items:

- Patching Concrete Structure: West Station, Tunnels and Upper Deck Superstructure
- Patching Concrete Structure: Lower Superstructure, Vertical Surfaces
- Patching Concrete Structure: Lower Superstructure, Bottom & Curved Surfaces
- Patching Concrete Structure: Deep Pier Shaft Deterioration
- Concrete, Misc.: West Station Concrete Beam Replacement
- Concrete, Misc.: Column Replacement
- Concrete, Misc.: Lower Deck Corbel Replacement

#### Fiber Reinforced Polymer Wrap (Protection)

Fiber reinforced polymer (FRP) wraps are composite systems made up of a glass fiber or carbon fiber material woven into sheets and saturated with a polymer bonding liquid (typically a two-part epoxy resin) and adhered to a concrete surface. Carbon fiber weaves generally have a higher unit tensile strength (100 ksi to over 200 ksi) with glass fiber weaves generally ranging from 30 ksi to 100 ksi. Due to their high tensile strength, FRP wraps are engineered to act as external reinforcement. Woven sheets may be engineered as unidirectional (designed to carry load in one direction) or bidirectional (designed to carry load in two or more directions). Containment is the primary consideration for FRP wrapping on this project to prevent future concrete delaminations from becoming dislodged and falling on public areas below the concrete arch spans. ODOT Central Office has a list of fiber wrap materials independently evaluated by ICC-ES.

Three options for applying the FRP wrap to the arch ribs over public areas have been developed (Figure 7). In each option, the FRP wrap must extend past a suspected future delamination area with a development length onto sound concrete. Generally, FRP wraps need a development length of one to two feet past concrete that will remain sound. If the FRP wrap is not developed correctly, a delamination could form and simply take the FRP wrap with it. As discussed previously, FRP wrap is not recommended on the lower deck column bases. Due to the structural nature and past corrosion history, placement of preformed shields over the lower deck corbels is recommended instead of application of an FRP wrap. Proposed areas of the FRP wraps on the lower pier shafts is shown in Figure 8.

**Option No. 1** provides confinement of the arch intrados and extends upward on the sides with 1'-6'' of adhesion development past potential corner spalls. This option provides containment for the areas of the arch ribs that would be most likely to fall.

**Option No. 2** adds top corner FRP strip wraps as a means of containing edge spalls. This option does not cover the entire extrados because:

1. Inner extrados spalls are rare and when present, and are less likely to fall to the ground below, and



2. Greater surface preparation is required due to its very irregular surface.

**Option No. 3** is a U-wrap of the arch ribs with development across two feet past the top corner. This option includes approximately 45,000 square feet of FRP wrap over Option No. 2.

Due to both coverage of the rib areas prone to spalling and overall economy, the quantities of Option No. 2 have been included in the development of the Alternative No. 2 cost estimate.

Surface preparation and installation of the FRP wrap systems vary from one manufacturer to another and among manufacturers' systems but some generalizations may apply. In the design of the FRP wrap system the bond between the existing concrete and the composite wrap is critical. Surface preparation of the existing concrete is important. Generally, the surfaces must be clean and free of contaminates and debris that would be detrimental to the bond between the wrap and the concrete. On this project, the existing epoxy-urethane sealer will need to be removed before the FRP wrap is installed. Another important issue is the profile or smoothness of the concrete surfaces. While some waviness, curvature or other unevenness of the concrete surface may be acceptable, sudden and abrupt changes in the surface profile and sharp corners greater than  $1/_{16}$ -inch are not acceptable. Sharp corners can tear the fabric during installation and surface profile irregularities can create air pockets under the FRP wrap.

The American Concrete Institute has surface profile specifications that some FRP wrap manufacturers reference. Generally abrupt surface profile changes or ridges larger than  $1/_{16}$ " are not acceptable. In the case of this project the arch rib sides are smooth but the top and bottom are generally not. The bottom surface of the arch ribs was formed using boards laid transversely. In some areas, the form boards did not butt up perfectly and the bottom surface of the concrete exhibits a stepped profile with ridges measuring up to  $1/_{2}$ -inch tall. These bottom surface irregularities will need to be remedied by some combination of grinding and or an epoxy paste applied to the ridges. The top surface of the arch ribs was roughly finished and has scattered debris embedded. The top surface irregularities will be addressed by some combination of mortar, grinding or epoxy paste. Finally, the corners between surfaces may require some grinding to provide a smoother corner. The existing concrete coating removal and surface profiling will take time and represents a significant portion of the final complete installed cost of the FRP wrap system.

Installation of the fiber sheets varies from one manufacturer to another and among manufacturers' systems but generally involves saturating the fiber sheets with resin either before or after applied to the concrete surface. Bubbles and voids under the fiber sheets are removed by rolling before the epoxy resin cures. After the FRP wrap is installed, epoxy-urethane sealer should be applied to provide UV protection for the fiber sheets and to the



match the color of the existing sealer on adjacent unwrapped areas. The epoxy-urethane sealer may be applied to the FPR wrap areas as they are curing and still tacky. If the epoxy-urethane sealer is applied after the FPR wrap has cure, the surface of the FRP wrap may require a light sanding or roughening for the epoxy-urethane sealer to bond properly.

The FRP wrap will be relatively impervious and moisture becoming trapped in the wrapped concrete is a concern. Gaps up to 1" wide between the fiber sheets will be provided to give moisture inside the concrete a chance to escape.









Figure 7 – Feasible FRP Wrap Options on Arch Ribs (Note: Arch height not to scale.)









TYPICAL PIER ELEVATION PIERS 5-10 SHOWN, PIER 3, 4, 11 & 12 SIMILAR (LOOKING EAST)

LEGEND FRP WRAP





Research published in 2002 and 2006 concluded that while FRP warps slow the rate of reinforcement corrosion due to chloride attack, FRP wraps do not stop corrosion. An example of active concrete corrosion within a confining FRP application is present at the bridge carrying Fulton Road over I-71 (Photo 10). Furthermore, Section 1.2.1 – General of AASHTO's *Guide Specifications for Design of Bonded FRP Systems for Repair and Strengthening of Concrete Bridge Elements* (First Edition, 2012) states the following:

The application of FRP systems will not stop the ongoing corrosion of existing steel reinforcement. The cause of corrosion to internal steel reinforcement should be addressed and corrosion-related deterioration should be repaired prior to application of any FRP system.

For the above reasons, a passive cathodic protection system following ODOT's *Supplemental Specification 844 – Concrete Patching with Embedded Anode Protection* has been included in the Alternate 2 cost estimate.



Photo 10 – Active Concrete Corrosion Beneath FRP Wrap, Pier 1, CUY-71-1679 (Fulton Road over I-71).



#### Cathodic Protection – Impressed Current (Prevention)

A third means of concrete protection, active cathodic protection, is a technology that has been developing since the 1970s. Active cathodic protection systems include impressed current, chloride extraction, realkinization and thermally sprayed zinc coating. Each method of cathodic protection has its strengths and weaknesses.

Alternate 3 includes an estimated cost of an impressed current cathodic protection system in lieu of a FRP wrap and a passive galvanic anode form of cathodic protection. Of the active systems, impressed current is the most common. Impressed works by neutralizing the electric current flowing though the subject reinforcing steel that produces the corrosion mechanism. However, prescription of an appropriate active cathodic protection system can best be determined with additional and proper concrete testing.



## VI. MISCELLANEOUS ASSESSMENTS

#### Right-of-Way Impacts

Properties that will require temporary right-of-way easements during construction, and are summarized in **Tables 4 and 5**. The costs associated with them do not include damages. Several of the properties impacted are parking lots. The temporary loss of parking revenue is not included in the costs but we have included a table summarizing the current cost to park along with the number of spaces that will be impacted.

Property Owner	Parcel No.	Temporary Access (SF)	Temp. Access Cost (per SF)	COST
Stonebridge Waterfront, LLC	003-20-008	5,653	\$1.75	\$9,900
No Information (Newly created Parcel)	003-20-009	656	\$1.75	\$1,150
Board of Park Commissioners of the Cleveland Metropolitan Park District	101-15-002	26,445	\$1.75	\$46,300
City of Cleveland	101-15-021	33,264	\$1.75	\$58,250
Flats East Development LLC	101-15-009	14,245	\$1.75	\$25,000
Greater Cleveland Regional Transit Authority	101-15-028	908	\$1.75	\$1,600
United Stated of America	101-15-011	4,348	\$1.75	\$7,600

#### Table 4 - Temporary Right-of-Way Impacts

Span	Lot Owner	Estimated No. of Parking Spaces Impacted	Daily Rate	Notes
3	Stonebridge Properties	30 - 35		
5	Cleveland Metroparks	33	\$3.00	
6	Cleveland Metroparks	15	\$3.00	
8	Canal Basin Parking Lot	15 - 18	\$2.00	Open Monday-Friday
9	Canal Basin Parking Lot	45	\$2.00	Open Monday-Friday
12	US Parking	6	\$4.00	
13	US Parking	34	\$4.00	

#### Table 5 - Parking Lots Impacted



#### Maintenance of Traffic

Maintenance of Traffic (MOT) during repair work will be handled the same way regardless of the method of repair both for deck work and below deck work. Conceptual MOT drawings are in included in **Appendix H**.

Deck: With the recommended wearing course replacement, MOT will be handled by closing one to two lanes at a time on the bridge, providing for part-width removal of the existing wearing surface and placement of the new. Given the proximity to the West 25<sup>th</sup> Street intersection and the West 9<sup>th</sup>/Superior/Huron intersection, the recommendation will be to position traffic for the lane closures prior to the intersections as shown in **Appendix B**.

Beneath the Bridge: Repair work on the piers and lower deck will be on Spans 2, 3, and 5 through 13 as indicated on the Public Areas Exhibit in **Appendix B**. Contractor access will be via manlift on the ground beneath the bridge. This will result in the following:

Span 2 – Riverbed Road will be closed for duration of work. Coordination with the Irishtown Bend Park development will be performed.

Span 3 –The closure of a portion of the parking lot for contractor access and equipment will be required. Work will be performed between the hours of 9:00 AM and 3:30 PM to minimize disruption to the residents.

Span 5 – Cleveland Metroparks Parking lot. Lot will be closed for duration of the work of the work above.

Span 6 - Cleveland Metroparks Parking lot. Lot will be closed for duration of the work of the work above.

Spans 6 and 7 – Public Roadways Merwin Avenue and West Avenue will be closed for the duration of work as shown in **Appendix B**. Pedestrian traffic will be maintained or detoured as needed.

Spans 8 and 9 – Portions of the parking lots will be closed for the duration of the work.

Span 10 – Pedestrian traffic will be detoured.

Span 11 – RTA Waterfront line – Coordination with GCRTA will take place to determine the best approach to maintaining rail traffic during repair work.

Span 12, Robert Lockwood Drive – There are several possibilities for maintaining traffic on Robert Lockwood Drive during construction. They include two way one lane traffic with flagger 9:00 AM to 3:30 PM, otherwise open to traffic, or utilizing weekend closures. Coordination with the City of Cleveland are necessary.

Span 13 - The closure of a portion of the parking lot will be required.



#### Navigation Lighting

There are six navigation lights mounted on the bridge which hang below the lower deck. Four are 180° red lights marking the channel edge and two are 360° green lights marking the channel center. Pennoni visited the site December 9, 2016 and inspected the navigation lighting. The lights were raised and the globes were removed, verifying that the fixtures have power (**Photo 11**). A night time visit later also verified the lights are on though with inadequate illumination (**Photo 12**). Further investigation by an electrician is warranted to determine the cause, whether it be the lights or the power service. An evaluation will then be done to determine the feasibility of repair or if replacement is warranted. We will coordinate with ODOT personnel and an electrician to perform a more thorough inspection of the lights and power service.



Photo 11 - Power Verification of Navigation Light (West Edge of Channel, South Face shown).




Photo 12 – Typical Ineffective Illumination of Navigation Light (East Edge of Channel, South Face circled).

### **RTA Waterfront Line**

The RTA Waterfront Line under Span 11 is constructed with concrete ties, has an overhead catenary system utilizing 600V DC, signal equipment on and around the track and a glass station north of the bridge. Once repair sites on finalized, coordination with the GCRTA is required. Conformance to RTA standards and specifications along with submitting proper request forms are required. Access within this area may be restricted to hours when the line is not in use, normally 11:00 PM to 6:00 AM although these hours would reduce during special events. A special event is defined as any event expected to draw 3,000 or more spectators to an area located within ¼ mile of an RTA Waterfront Rail Line.



### VII. CONCEPTUAL ALTERNATIVES

Three alternates have been identified that would meet the purpose and need of the project. The criteria these alternatives should be judge by is the following:

- 1. Public Safety
- 2. Extend the life of the bridge for 50 years
- 3. Cost

Alternates No. 1 will maintain the structure in *Fair* condition. Alternates Nos. 2 and 3 will maintain the structure in *Satisfactory* condition or better.

Cost estimates have been extrapolated from current estimates to July 1, 2020 using ODOT's 2017-2021 Business Plan Inflation Calculator.

### Alternative No. 1

This alternate project includes general maintenance work such as removal of loose overhead concrete in and around the defined public spaces, fixing the broken drain pipes at Pier 2 & 3. The upper deck that was replaced in the 1995-97 rehabilitation is showing signs of accelerating deterioration. It is recommended that the top  $1 \frac{1}{4}$  of the deck be removed by hydro demolition and a new micro silica wearing surface be placed. This will extend the life of the deck for another 25 years.

Currently, the Center Street Bridge tender has a fenced enclosure at Pier 4. This enclosure abuts Pier 4 and allows vandals to access the steel superstructure. It is proposed the enclosure be reduced in size and pulled away from the pier. This should prevent vandals from using the enclosure to access the pier. Additionally, the proximity of south face of Span 1A and the north face of Span 13 to the ground line allows vandals to enter the lower deck area with minimal effort. Currently, supplemental fencing has been unsuccessfully used to prevent entry onto the lower deck. These areas will be blocked up using concrete masonry units (CMU) to create a barrier. The CMU's will receive a mortar coat and a graffiti-resistant sealant.

The repair of the Navigation Lights will be further investigated. Although all are on during the night, the brightness of the lights is ineffective.

While Alternative No. 1 would provide a temporary solution to the falling concrete, it does not provide for future spalling and deterioration. This option does not extend the life of the structure.

This alternate is estimated to cost \$2,569,000.



### Alternative No. 2

As with Alternative No. 1, all general maintenance items including the hydro-demolition and overlay of the upper deck will be included in Alternative No. 2. Alternative No. 2 introduces new major work items including concrete patching with localized passive cathodic protection, FRP wrapping the bottom surfaces of the lower concrete superstructure to protect the public access areas, and sealing these limits of concrete surfaces with an epoxy-urethane sealer. Work under the concrete patching includes patching all cracked, loose and spalled concrete on the bridge and installing passive cathodic protection to prevent advancing local concrete superstructure to prevent concrete spalls from falling onto public access areas below. The preparation of the concrete for the FRP wrap will include removal of the existing epoxy-urethane sealant and smoothing the raised concrete form marks. Work under sealing the concrete surfaces includes sealing all areas that have been patched or FRP wrapped with an epoxy-urethane sealer. It is important to note that no epoxy-urethane sealing will be performed on the concrete patches in the Tunnels, West Station, Span 1A and 1B upper deck superstructure, and the East Station and subway.

Alternative No. 2 was originally estimated to cost \$25,984,000 and included FRP wrapping all concrete surfaces in the lower concrete superstructure. Since this cost was significantly over the original budget allotted for this project, Alternative No. 2 has been scaled back and further broken down into five (5) sub-alternatives to present the District with various options and their associated costs for rehabilitation. The following quantities were removed from Alternative No. 2 options due to limited effective and economy:

- Application of epoxy urethane sealer on patched surfaces of concrete components in the West Tunnel, West Station, upper deck approach spans, East Station and East Subway
- Arch patching and FRP wrapping in Spans 11, 12 and 13
- Lower Deck floorbeam patching and FRP wrapping in Spans 11 and 12
- Railroad coordination and flagging

### Alternative No. 2A

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Sealing concrete patching limits with an epoxy-urethane sealer

### Alternative No. 2B

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Fiber wrap bottom of arch ribs only over public access areas
- Sealing concrete patching and FRP limits with an epoxy-urethane sealer



### <u>Alternative No. 2C</u>

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Fiber wrap bottom of arch ribs and lower deck floor beams over public access areas
- Sealing concrete patching and FRP limits with an epoxy-urethane sealer

### Alternative No. 2D

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Fiber wrap bottom of arch ribs and lower deck floor beams over public access areas
- Fiber wrap end columns of piers
- Sealing concrete patching and FRP limits with an epoxy-urethane sealer

### Alternative No. 2E

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Fiber wrap bottom of arch ribs and lower deck floor beams over public access areas
- Fiber wrap end columns of piers and lower deck support columns

Each sub-alternative is described in further detail on the following pages. A breakdown of costs is also presented with each sub-alternative. Each sub-alternative includes all work items from the previous alternative and adds new work items.

The recommended alternative is <u>Alternative No. 2C</u> based on addressing public safety, extending the service life of the bridge, and economic analysis.



#### Alternative No. 2A

Alternative No. 2A includes all the general maintenance items presented in Alternative No. 1 and includes concrete patching with localized passive cathodic protection and sealing these concrete patching limits with an epoxy-urethane sealer (Note: all repair surfaces have been increased by 20% to account for future deterioration). Concrete patching with localized passive cathodic protection is the most feasible solution to repair the existing locations of failing concrete. Concrete patching will remove and replace all existing cracked, loose, and spalled concrete on the bridge. Localized passive cathodic protection will help to impede the concrete corrosion from advancing which will help prevent future spalling and deterioration in these areas only. It is important to note that this alternative repairs the existing problem areas only. It does not provide repairs or safety measures to address any concrete that may crack, spall, or fall to the ground in the future. Given the history and the patterns of concrete spalling on the bridge, we anticipate that there will be future locations where cracks and spalls develop which will result in additional repair work necessary to address these future locations. This alternate extends the service life of the bridge an estimated 20 years before future repair work is necessary.

	ALTERNATIVE No. 2A								
ITEM	EXT	QTY	UNIT	DESCRIPTION	2017 UNIT COST	2017 COST			
511	81100	170	FT	CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT	\$400.00	\$68,000			
511	81300	25	EACH	CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT	\$3,000.00	\$75,000			
511	81300	7	EACH	CONCRETE, MISC.: COLUMN REPLACEMENT	\$8,500.00	\$59,500			
512	10101	3780	SY	SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN	\$15.00	\$56,700			
512	10600	800	FT	CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB)	\$70.00	\$56,000			
516	47000	LUMP	-	JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE	\$20,000.00	\$20,000			
519	11600	15300	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK)	\$90.00	\$1,377,000			
519	11600	9590	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES)	\$100.00	\$959,000			
519	11600	5560	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)	\$125.00	\$695,000			
519	11900	6	СҮ	SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION)	\$5,000.00	\$30,000			
530	00200	LUMP	-	SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER	\$5,000.00	\$5,000			
530	00400	200	EACH	SPECIAL - STRUCTURES CORBEL SHIELD	\$200.00	\$40,000			
530	00600	900	SF	SPECIAL - STRUCTURES MASONRY BLOCK WALL	\$10.00	\$9,000			
625	98200	LUMP	-	LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR	\$20,000.00	\$20,000			
844	10001	30450	SF	CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN	\$20.00	\$609,000			
848	10000	17750	SY	MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION	\$25.00	\$443,750			
848	50320	17750	SY	EXISTING CONCRETE OVERLAY REMOVED	\$10.00	\$177,500			
614	11000	LUMP	-	MAINTAINING TRAFFIC	\$100,000.00	\$100,000			
619	16020	24	MNTH	FIELD OFFICE, TYPE C	\$2,500.00	\$60,000			
624	10000	LUMP	-	MOBILIZATION	\$100,000.00	\$100,000			
SUBTOTAL:									
20% CONTINGENCY:						\$992,000			
2017 TOTAL:									
FUTURE WORTH (AT AN INFLATION RATE OF 11.9%)									

This alternate is estimated to cost **\$6,660,000**.



#### Alternative No. 2B

Alternative No. 2B includes all the work items presented in Alternative No. 2A and includes FRP wrapping the bottom surfaces of the concrete arch ribs which will partially protect the public access below. In this alternative, FRP wrap will be used to contain future concrete delaminations from becoming dislodged and falling on public areas <u>below</u> the concrete arch spans. It is important to note that the lower deck floor beams are not protected in this alternative and therefore, the public areas <u>between</u> the concrete arch spans remain unprotected. Estimated quantities were calculated by assuming the FRP would cover the entire bottom of the arch intrados and the FRP would extend upward on the sides with a 1'-6" development length past potential corner spalls.

While the application of FRP will assist in confining the concrete members and protect the public from falling concrete, it's use will not stop the continual degradation of the concrete from reinforcement. Periodic repair work will be necessary to reapply the FRP in areas. This alternate extends the service life of the bridge an estimated 25 to 40 years before future repair work is necessary.

	ALTERNATIVE No. 2B								
ITEM	EXT	QTY	UNIT	DESCRIPTION	2017 UNIT COST	2017 COST			
511	81100	170	FT	CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT	\$400.00	\$68,000			
511	81300	25	EACH	CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT	\$3,000.00	\$75,000			
511	81300	7	EACH	CONCRETE, MISC.: COLUMN REPLACEMENT	\$8,500.00	\$59,500			
512	10101	10590	SY	SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN	\$15.00	\$158,850			
512	10600	800	FT	CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB)	\$70.00	\$56,000			
512	74000	6860	SY	REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES	\$20.00	\$137,200			
516	47000	LUMP	-	JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE	\$20,000.00	\$20,000			
519	00100	55693	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (ARCH RIBS)	\$45.00	\$2,506,203			
519	11600	15300	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK)	\$90.00	\$1,377,000			
519	11600	9590	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES)	\$100.00	\$959,000			
519	11600	5560	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)	\$125.00	\$695,000			
519	11900	6	СҮ	SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION)	\$5,000.00	\$30,000			
530	00200	LUMP	-	SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER	\$5,000.00	\$5,000			
530	00400	200	EACH	SPECIAL - STRUCTURES CORBEL SHIELD	\$200.00	\$40,000			
530	00600	900	SF	SPECIAL - STRUCTURES MASONRY BLOCK WALL	\$10.00	\$9,000			
625	98200	LUMP	-	LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR	\$20,000.00	\$20,000			
844	10001	30450	SF	CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN	\$20.00	\$609,000			
848	10000	17750	SY	MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION	\$25.00	\$443,750			
848	50320	17750	SY	EXISTING CONCRETE OVERLAY REMOVED	\$10.00	\$177,500			
614	11000	LUMP	-	MAINTAINING TRAFFIC	\$100,000.00	\$100,000			
619	16020	24	MNTH	FIELD OFFICE, TYPE C	\$2,500.00	\$60,000			
624	10000	LUMP	-	MOBILIZATION	\$100,000.00	\$100,000			
					SUBTOTAL:	\$7,706,000			
20% CONTINGENCY:						\$1,541,000			
2017 TOTAL:									
FUTURE WORTH (AT AN INFLATION RATE OF 11.9%)									

This alternate is estimated to cost **\$10,347,000**.



#### Alternative No. 2C

Alternative No. 2C includes all the work items presented in Alternative No. 2B and includes the additional FRP wrapping of the bottom surfaces of the concrete lower deck floor beams which will further protect the public access below. In this alternative, FRP wrap will be used to contain future concrete delaminations from becoming dislodged and falling onto public areas between the concrete arch spans. The lower deck floor beams are open to public access areas below and as a result, concrete would likely fall onto the public access areas below if it becomes dislodged. It is important to note that the bottom surfaces of most concrete members above public access areas are protected in this alternative. Estimated quantities were calculated by assuming the FRP would cover the entire bottom of the lower deck floor beams and the FRP would extend upward on the sides with a 1'-0" development length past potential corner spalls. This alternate extends the service life of the bridge an estimated 25 to 40 years before future repair work is necessary.

ALTERNATIVE No. 2C								
ITEM	EXT	QTY	UNIT	DESCRIPTION	2017 UNIT COST	2017 COST		
511	81100	170	FT	CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT	\$400.00	\$68,000		
511	81300	25	EACH	CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT	\$3,000.00	\$75,000		
511	81300	7	EACH	CONCRETE, MISC.: COLUMN REPLACEMENT	\$8,500.00	\$59,500		
512	10101	17430	SY	SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN	\$15.00	\$261,450		
512	10600	800	FT	CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB)	\$70.00	\$56,000		
512	74000	13680	SY	REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES	\$20.00	\$273,600		
516	47000	LUMP	-	JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE	\$20,000.00	\$20,000		
519	00100	55693	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (ARCH RIBS)	\$45.00	\$2,506,203		
519	00100	55919	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (FLOOR BEAMS)	\$45.00	\$2,516,355		
519	11600	15300	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK)	\$90.00	\$1,377,000		
519	11600	9590	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES)	\$100.00	\$959,000		
519	11600	5560	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)	\$125.00	\$695,000		
519	11900	6	СҮ	SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION)	\$5,000.00	\$30,000		
530	00200	LUMP	-	SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER	\$5,000.00	\$5,000		
530	00400	200	EACH	SPECIAL - STRUCTURES CORBEL SHIELD	\$200.00	\$40,000		
530	00600	900	SF	SPECIAL - STRUCTURES MASONRY BLOCK WALL	\$10.00	\$9,000		
625	98200	LUMP	-	LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR	\$20,000.00	\$20,000		
844	10001	30450	SF	CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN	\$20.00	\$609,000		
848	10000	17750	SY	MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION	\$25.00	\$443,750		
848	50320	17750	SY	EXISTING CONCRETE OVERLAY REMOVED	\$10.00	\$177,500		
614	11000	LUMP	-	MAINTAINING TRAFFIC	\$100,000.00	\$100,000		
619	16020	24	MNTH	FIELD OFFICE, TYPE C	\$2,500.00	\$60,000		
624	10000	LUMP	-	MOBILIZATION	\$100,000.00	\$100,000		
SUBTOTAL:								
20% CONTINGENCY:								
2017 TOTAL:								
	FUTURE WORTH (AT AN INFLATION RATE OF 11.9%)							

This alternate is estimated to cost **\$14,047,000**.



### Alternative No. 2D

Alternative No. 2D includes all the work items presented in Alternative No. 2C and includes additional protection of the public access areas by also wrapping the vertical surfaces of the end columns located at the piers. The location of the end columns on the piers are such that dislodged concrete has a high probability of falling onto the public access areas. These safety concerns, coupled with the fact that of all the vertical surfaces the end columns located at the piers are in the most critical shape, resulted in presenting this alternative to show the additional costs required to perform this work. This alternate extends the service life of the bridge an estimated 25 to 40 years before future repair work is necessary.

This alternate is estimated to cost **\$15,409,000**.

	ALTERNATIVE No. 2D							
ITEM	EXT	QTY	UNIT	DESCRIPTION	2017 UNIT COST	2017 COST		
511	81100	170	FT	CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT	\$400.00	\$68,000		
511	81300	25	EACH	CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT	\$3,000.00	\$75,000		
511	81300	7	EACH	CONCRETE, MISC.: COLUMN REPLACEMENT	\$8,500.00	\$59,500		
512	10101	19910	SY	SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN	\$15.00	\$298,650		
512	10600	800	FT	CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB)	\$70.00	\$56,000		
512	74000	16210	SY	REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES	\$20.00	\$324,200		
516	47000	LUMP	-	JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE	\$20,000.00	\$20,000		
519	00100	55693	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (ARCH RIBS)	\$45.00	\$2,506,203		
519	00100	20568	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (END COLUMNS)	\$45.00	\$925,560		
519	00100	55919	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (FLOOR BEAMS)	\$45.00	\$2,516,355		
519	11600	15300	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK)	\$90.00	\$1,377,000		
519	11600	9590	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES)	\$100.00	\$959,000		
519	11600	5560	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)	\$125.00	\$695,000		
519	11900	6	СҮ	SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION)	\$5,000.00	\$30,000		
530	00200	LUMP	-	SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER	\$5,000.00	\$5,000		
530	00400	200	EACH	SPECIAL - STRUCTURES CORBEL SHIELD	\$200.00	\$40,000		
530	00600	900	SF	SPECIAL - STRUCTURES MASONRY BLOCK WALL	\$10.00	\$9,000		
625	98200	LUMP	-	LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR	\$20,000.00	\$20,000		
844	10001	30450	SF	CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN	\$20.00	\$609,000		
848	10000	17750	SY	MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION	\$25.00	\$443,750		
848	50320	17750	SY	EXISTING CONCRETE OVERLAY REMOVED	\$10.00	\$177,500		
614	11000	LUMP	-	MAINTAINING TRAFFIC	\$100,000.00	\$100,000		
619	16020	24	MNTH	FIELD OFFICE, TYPE C	\$2,500.00	\$60,000		
624	10000	LUMP	-	MOBILIZATION	\$100,000.00	\$100,000		
					SUBTOTAL:	\$11,475,000		
20% CONTINGENCY:								
2017 TOTAL:								
				FUTURE WORTH (AT AN INFLATION R	ATE OF 11.9%)	\$15,409,000		



### Alternative No. 2E

Alternative No. 2E includes all the work items presented in Alternative No. 2D and includes additional protection of the public access areas by also wrapping the vertical surfaces of the lower deck support columns. The lower deck support columns are located over public access areas and dislodged concrete may potentially fall on to the public access areas below if it does not land on the concrete arch ribs below. This additional work would result in containing all the concrete with a high probability of falling on the public access areas below. Since all the existing problematic areas are addressed by concrete patching with cathodic protection and future areas are addressed by containment with FRP wrapping, this alternate extends the service life of the bridge an estimated 25 to 50 years before future repair work is necessary.

	ALTERNATIVE No. 2E							
ITEM	EXT	QTY	UNIT	DESCRIPTION	2017 UNIT COST	2017 COST		
511	81100	170	FT	CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT	\$400.00	\$68,000		
511	81300	25	EACH	CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT	\$3,000.00	\$75,000		
511	81300	7	EACH	CONCRETE, MISC.: COLUMN REPLACEMENT	\$8,500.00	\$59,500		
512	10101	27480	SY	SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN	\$15.00	\$412,200		
512	10600	800	FT	CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB)	\$70.00	\$56,000		
512	74000	23790	SY	REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES	\$20.00	\$475,800		
516	47000	LUMP	-	JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE	\$20,000.00	\$20,000		
519	00100	55693	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (ARCH RIBS)	\$45.00	\$2,506,203		
519	00100	62060	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (LOWER DECK SUPPORT COLUMNS)	\$45.00	\$2,792,700		
519	00100	20568	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (END COLUMNS)	\$45.00	\$925,560		
519	00100	55919	SF	SPECIAL - COMPOSITE FIBER WRAP SYSTEM (FLOOR BEAMS)	\$45.00	\$2,516,355		
519	11600	15300	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK)	\$90.00	\$1,377,000		
519	11600	9590	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES)	\$100.00	\$959,000		
519	11600	5560	SF	SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, ROTTOM AND CURVED SUBFACES)	\$125.00	\$695,000		
519	11900	6	СҮ	SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION)	\$5,000.00	\$30,000		
530	00200	LUMP	-	SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER	\$5,000.00	\$5,000		
530	00400	200	EACH	SPECIAL - STRUCTURES CORBEL SHIELD	\$200.00	\$40,000		
530	00600	900	SF	SPECIAL - STRUCTURES MASONRY BLOCK WALL	\$10.00	\$9,000		
625	98200	LUMP	-	LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR	\$20,000.00	\$20,000		
844	10001	30450	SF	CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN	\$20.00	\$609,000		
848	10000	17750	SY	MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION	\$25.00	\$443,750		
848	50320	17750	SY	EXISTING CONCRETE OVERLAY REMOVED	\$10.00	\$177,500		
614	11000	LUMP	-	MAINTAINING TRAFFIC	\$100,000.00	\$100,000		
619	16020	24	MNTH	FIELD OFFICE, TYPE C	\$2,500.00	\$60,000		
624	10000	LUMP	-	MOBILIZATION	\$100,000.00	\$100,000		
					SUBTOTAL:	\$14,533,000		
				20% C	ONTINGENCY:	\$2,907,000		
2017 TOTAL:								
				FUTURE WORTH (AT AN INFLATION R	ATE OF 11.9%)	\$19,515,000		

This alternate is estimated to cost **\$19,515,000**.



### Alternative No. 3

As with Alternate No. 1 and 2, all general maintenance items including the hydro- demolition and overlay of the upper deck will be included. In Spans 2 through 13, excluding Span 4, all cracked, loose and deteriorated concrete will be patched. The areas in the West Station will be patched and/or replaced. As opposed to Alternate 2, in lieu of wrap, active impressed cathodic protection be employed to counteract and stabilize the corrosion. Once in place, this system can restore the concrete to its original composition and halt the ongoing concrete corrosion.

If installed and maintained properly, it is estimated that the service life would be greater than 50 years. Several bridges throughout the United States have this system in place and appear to be functioning as designed.

This alternate is estimated to cost \$33,226,000. This estimated cost does not include maintenance of the active cathodic protection system.

The estimated costs for all alternates have been projected to the 2020 construction year.



# OHIO DEPARTMENT OF TRANSPORTATION 2017 REHABILITATION FEASIBILITY STUDY APPENDICES PID NO 99972

## DETROIT-SUPERIOR BRIDGE OVER CUYAHOGA RIVER BRIDGE NO. CUY-6-1456

SFN: 1800930



FEBRUARY 2017

PREPARED BY:



1655 W. Market Street, Suite 355 | Akron, OH 44313

# BRIDGE NO. CUY-6-1456 DETROIT-SUPERIOR BRIDGE OVER CUYAHOGA RIVER 2017 REHABILITATION FEASIBILITY STUDY

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- Appendix B Public Area Below Structure and Property Map
- **Appendix C Concrete pH Test Results**
- **Appendix D Estimated Concrete Patching Quantities**
- **Appendix E Estimated FRP Wrap Quantities**
- Appendix F West Station Deterioration Drawings
- **Appendix G West Station Deterioration History**
- **Appendix H Maintenance of Traffic**



# APPENDIX A

SUMMARY OF ESTIMATED COST



CUY-6-1456 over Cuyahoga River Rehabilitation Feasibility Study Ohio Department of Transportation

\$6,660,000	\$10,347,000	\$14,047,000	\$15,409,000	\$19,515,000
38 Months	38 Months	38 Months	38 Months	38 Months
\$5,952,000	\$9,247,000	\$12,553,000	\$13,770,000	\$17,440,000
Maintenance plus patching	2A plus FRP Wrap Arch Ribs	2B plus FRP Wrap Floor Beams	2C plus FRP Wrap End Columns	2D plus FRP Wrap L.D. Columns
2A	2B	2C	2D	2E

CUY-6-1456 over Cuyahoga River Rehabilitation Feasibility Study Ohio Department of Transportation



CY 2017-2021 Business Plan Inflation Calculator:								
Not sure if you have the latest calculator? Click here.								
Last Modified: 1/19/2017		Today's Date:						
Please Enter Values in the Yellow	Areas Only:	February 15, 2017						
Estimation Start Date: Less than or Equal to Today's D (mm/dd/yyyy)	ate	Enter Construction Mid-Point Date: (cannot exceed 02/15/2042) (mm/dd/yyyy)						
2/15/2017 Start Date:		7/1/2020 Construction Mid-Point Date:						
Present-Day Estimated Cost \$2,282,400.00 Estimated Dollar Amount:								
Estimate Start Date to Cons Inflation - Start to Mid-Poir	Estimate Start Date to Construction Mid-Point Date: 41 Months Inflation - Start to Mid-Point of Construction:							
(compounded growth r	rate)	Inflated Dollar Amount:						
Business Plan	12.6%	\$2,568,995.13						
Estimator's Name:								
County - Route - Section:	CUY-6-1456							
PID:	99972							
Estimator's Notes:	Alternate 1 - Mainte	enance Only						

Estimated Cost:\$1,902,000.00

Contingency: 20.00%

### Estimated Total: \$2,282,400.00

ALTERNATE 1 - MAINTENANCE ONLY

### Base Date: 02/13/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type:

### Season:

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by DEA on 02/13/17 Checked by WJV on 02/14/17

Line # Item Number	<u>Quantity</u>	<u>Units</u>	Unit Price	Extension
Description Supplemental Description				
<u></u>				

### Group 0001: STRUCTURE

0005	530E00200	1.000	LS	\$5,000.00000	\$5,000.00		
SPE BRI	ECIAL - STRUCTURES DGE OPERATOR'S CAR SHELTER	2					
0006	530E00600	900.000	SF	\$10.00000	\$9,000.00		
SPE MAS	ECIAL - STRUCTURES SONRY BLOCK WALL						
0007	530E00600	15,000.000	SF	\$22.00000	\$330,000.00		
SPE	ECIAL - STRUCTURES						
REI	MOVE LOOSE AND DELAMINATEL	D CONCRETE					
8000	625E98200	1.000	LS	\$20,000.00000	\$20,000.00		
LIG	HTING, MISC.:						
NA۱	/IGATION LIGHTING REPAIR						
0009	848E10000	19,400.000	SY	\$60.00000	\$1,164,000.00		
IVIIC	RU SILICA MUDIFIED CUNCRET	E UVELAT US		RODEWOLITION			
0010	848E50320	19,400.000	SY	\$10.00000	\$194,000.00		
EXI	STING CONCRETE OVERLAY REMOVE	D					

### Total for Group 0001:\$1,722,000.00

Group 0002: INCIDENTAL

0011 614E11000 MAINTAINING TRAFFIC	1.000	LS	\$100,000.00000	\$100,000.00
0012 619E16020 FIELD OFFICE, TYPE C	12.000	MNTH	\$2,500.00000	\$30,000.00
0013 624E10000 MOBILIZATION	1.000	LS	\$50,000.00000	\$50,000.00

## Total for Group 0002:\$180,000.00

CY 2017-2021 Business Plan Inflation Calculator:						
<u>Not sure if ye</u>	Not sure if you have the latest calculator? Click here.					
Last Modified: 1/19/2017		Today's Date				
Please Enter Values in the Yellow	Areas Only:	February 15, 2017				
Estimation Start Date: Less than or Equal to Today's D (mm/dd/yyyy)	ate	Enter Construction Mid-Point Date: (cannot exceed 02/15/2042) (mm/dd/yyyy)				
2/15/2017		7/1/2020				
Start Date:		Construction Mid-Point Date:				
Present-Day Estimated Cost \$22,907,400.00 Estimated Dollar Amount:	:					
Estimate Start Date to Const	truction Mid-Po	bint Date: 41 Months				
Inflation - Start to Mid-Poir	nt of Constructio	on:				
(compounded growth r	ate)	Inflated Dollar Amount:				
Business Plan	12.6%	\$25,783,823.60				
Estimator's Name:						
County - Route - Section:	CUY-6-1456					
PID <sup>.</sup>	99972					
Estimator's Notos:	Alternate 2 - Debak	h w/ Dataking and Fiber Wran				
Estimator s notes.	Allemale 2 - Kenal	b w/ Patching and Fiber Wrap				

Estimated Cost:\$19,089,500.00

Contingency: 20.00%

### Estimated Total: \$22,907,400.00

ALTERNATE 2 - REHAB W/ PATCHING AND FIBER WRAP

#### Base Date: 02/13/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type:

### Season:

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by DEA on 02/13/17 Checked by WJV on 02/14/17

Line # Item Number	Quantity U	<u>Inits</u>	Unit Price	<u>E</u>	Extension
Description Supplemental Description					
<u>Supplemental Description</u>					

### Group 0001: STRUCTURE

0005 511E81100	150.000	FT	\$400.00000	\$60,000.00
CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLA	ACEMEN	Т		
0006 511E81300	25.000	EACH	\$3,000.00000	\$75,000.00
CONCRETE, MISC.:				
LOWER DECK CORBEL REPLACEMENT	4 000	EACH	\$8 500 00000	\$34,000,00
	4.000	LAGIT	\$8,300.00000	φ34,000.00
COLUMN REPLACEMENT				
0008 512E10101 31,0	000.000	SY	\$15.00000	\$465,000.00
SEALING OF CONCRETE SURFACES (EPOXY-U	RETHANE	), AS PER	PLAN	
0009 512E10600	800.000	FT	\$70.00000	\$56,000.00
CONCRETE REPAIR BY EPOXY INJECTION ARCH RIB				
0010 512E74000 31,0	000.000	SY	\$20.00000	\$620,000.00
REMOVAL OF EXISTING COATINGS FROM CON	CRETE SL	IRFACES		
0011 516E47000	1.000	LS	\$20,000.00000	\$20,000.00
JACKING AND TEMPORARY SUPPORT OF SUPP	ERSTRUC	FURE		
0012 519E00100 275,0	000.000	SF	\$45.00000	\$12,375,000.00
SPECIAL - COMPOSITE FIBER WRAP SYSTEM				
0013 519E11600 15,0	000.000	SF	\$90.00000	\$1,350,000.00
SPECIAL - PATCHING CONCRETE STRUCTURE WEST STATION, TUNNELS AND UPPER D	ECK			
0014 519E11600 9,4	500.000	SF	\$100.00000	\$950,000.00
SPECIAL - PATCHING CONCRETE STRUCTURE		-0		
0015 519E11600 54	50RFACE	SF	\$125,00000	\$687 500 00
SPECIAL - PATCHING CONCRETE STRUCTURE	000.000	01	¢120.00000	<i>\\\</i> 001,000.00
LOWER SUPERSTRUCTURE - BOTTOM A	ND CUR	VED SUI	RFACES	
0016 519E11900	6.000	CY	\$5,000.00000	\$30,000.00
SPECIAL - PATCHING CONCRETE STRUCTURE DEEP PIER SHAFT DETERIORATION				
0017 530E00200	1.000	LS	\$5,000.00000	\$5,000.00
SPECIAL - STRUCTURES				
0018 530E00400	200.000	EACH	\$200.00000	\$40,000.00
SPECIAL - STRUCTURES CORBEL SHIELD				
0019 530E00600 9	900.000	SF	\$10.00000	\$9,000.00
SPECIAL - STRUCTURES MASONRY BLOCK WALL				
0020 625E98200	1.000	LS	\$20,000.00000	\$20,000.00
LIGHTING, MISC.:				
NAVIGATION LIGHTING REPAIR		SE	00000	¢600.000.00
				φουυ,υυυ.υυ
	PROTEC	HON, AS	PER PLA N	

Estimate:	ODOT1602				
<u>Line #</u> Dese Sup	<u>Item Number</u> <u>cription</u> plemental Description	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
0022	848E10000	19,400.000	SY	\$60.00000	\$1,164,000.00
MIC	RU SILICA MODIFIED CONCRETE	= OVELAY US	SING HYL	¢10,0000	¢104.000.00
EXIS	646E50320 STING CONCRETE OVERLAY REMOVE	19,400.000 D	51	\$10.00000	\$194,000.00
				Total for Group 0	001:\$18,754,500.00
Group	0002: INCIDENTAL 614E11000	1.000	LS	\$100,000.00000	\$100,000.00
MAIN	ITAINING TRAFFIC				
0025 MAII RAII	614E18002 NTAINING TRAFFIC, MISC.: LROAD FLAGGER	1.000	LS	\$50,000.00000	\$50,000.00
0026 MAII RAII	614E18002 NTAINING TRAFFIC, MISC.: LROAD COORDINATION	1.000	LS	\$25,000.00000	\$25,000.00
0027 FIELI	619E16020 D OFFICE, TYPE C	24.000	MNTH	\$2,500.00000	\$60,000.00
0028 MOB	624E10000 ILIZATION	1.000	LS	\$100,000.00000	\$100,000.00

Total for Group 0002:\$335,000.00

CY 2017-2021 Business Plan Inflation Calculator:							
<u>Not sure if y</u>	Not sure if you have the latest calculator? Click here.						
Last Modified: 1/19/2017		Today's Date:					
Please Enter Values in the Yellow	v Areas Only:	May 17, 2017					
<b>Estimation Start Date:</b> Less than or Equal to Today's E (mm/dd/yyyy)	Date	Enter Construction Mid-Point Date: (cannot exceed 05/17/2042) (mm/dd/yyyy)					
5/17/2017		7/1/2020					
Start Date:		Construction Mid-Point Date:					
Present-Day Estimated Cos \$5,952,000.00 Estimated Dollar Amount:	t:						
Estimate Start Date to Cons	struction Mid-Poin	t Date: <u>38</u> Months					
Inflation - Start to Mid-Poi	nt of Construction						
(compounded growth	rate)	Inflated Dollar Amount:					
Business Plan	11.9%	\$6,658,148.51					
Estimator's Name:							
County - Route - Section:	CUY-6-14.56						
PID:	99972						
Estimator's Notes:	Alternative No. 2A						

Estimated Cost:\$4,960,450.00 Contingency: 20.00%

### Estimated Total: \$5,952,540.00

Alternative No. 2A

### Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17 Checked by WJV on 05/17/17

<u>Line #</u> <u>Item Number</u> <u>Description</u> <u>Supplemental Description</u>	<u>Quantity</u>	<u>Units</u>	Unit Price	<u>Extension</u>
Group 0001: STRUCTURE				

0001	511E81100	170.000	FT	\$400.00000	\$68,000.00
W	EST STATION CONCRETE BEAM REF	PLACEMEN	Т		
0002	511E81300	25.000	EACH	\$3,000.00000	\$75,000.00
C	DNCRETE, MISC.:				
LC	WER DECK CORBEL REPLACEMEN	T			
0003	511E81300	7.000	EACH	\$8,500.00000	\$59,500.00
C	DNCRETE, MISC.:				
0004	512E10101	3 780 000	ev.	\$15,00000	\$56,700,00
0004		3,700.000			\$30,700.00
50	EALING OF CONCRETE SURFACES (EPOX)	I-URETHANE	I), AS PER	PLAN	
0005	512E10600	800 000	FT	\$70,00000	\$56,000,00
C		000.000	• •	\$10.00000	\$00,000.00
(A	RCH RIB)				
0006	516E47000	1.000	LS	\$20,000.00000	\$20,000.00
JA	CKING AND TEMPORARY SUPPORT OF SI	UPERSTRUC	TURE		
0007	519E11600 1	5,300.000	SF	\$90.00000	\$1,377,000.00
SF	PECIAL - PATCHING CONCRETE STRUCTU	RE			
(W)	EST STATION, TUNNELS, AND UPPE	:R DECK)	<u>e</u> e	£100.00000	¢050.000.00
0000		9,090.000	ЗГ	\$100.00000	\$959,000.00
5F // (	OWER SUPERSTRUCTURE VERTICA	RE AL SURFAC	ES)		
0009	519E11600	5.560.000	SF	\$125.00000	\$695.000.00
SF	PECIAL - PATCHING CONCRETE STRUCTU	RE			. ,
(L0	OWER SUPERSTRUCTURE, BOTTOM	AND CUR	VED SUI	RFACES)	
0010	519E11900	6.000	CY	\$5,000.00000	\$30,000.00
SF	PECIAL - PATCHING CONCRETE STRUCTU	RE			
(D)	EEP PIER SHAFT DETERIORATION)	4 000		¢C 000 00000	<b>۴</b> ۲ 000 00
0011	530E00200	1.000	LS	\$5,000.00000	\$5,000.00
SH	PECIAL - STRUCTURES				
0012	530E00400	200.000	EACH	\$200.00000	\$40.000.00
SF	PECIAL - STRUCTURES				+ ,
CC	ORBEL SHIELD				
0013	530E00600	900.000	SF	\$10.00000	\$9,000.00
SF	PECIAL - STRUCTURES				
MA	ASONRY BLOCK WALL	4 000		<b>#00.000.0000</b>	<b>#00.000.00</b>
0014	625E98200	1.000	LS	\$20,000.00000	\$20,000.00
	GHTING, MISC.:				
0015	844F10001 3	30 450 000	SF	\$20,00000	\$609,000,00
C	NCRETE PATCHING WITH GAI VANIC AND		TION AS	PER PLAN	\$000,000.00
0.		DETROTEC	, , , , , , , , , , , , , , , , , , , ,		
0016	848E10000 1	7,750.000	SY	\$25.00000	\$443,750.00
M	CRO SILICA MODIFIED CONCRETE OVERL	AY USING H	YDRODE	NOLITION	
0017	848E50320 1	7,750.000	SY	\$10.00000	\$177,500.00
Ε>	STING CONCRETE OVERLAY REMOVED				
0018	614E11000	1.000	LS	\$100,000.00000	\$100,000.00
M	AINTAINING TRAFFIC				
1:57:36	PM day, May 17, 2017				
vveunes	uay, Way 17, 2017				Page 2 01 3

Estimate: ODOT1602				
Line # Item Number Description Supplemental Description	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
0019 619E16020 FIELD OFFICE, TYPE C	24.000	MNTH	\$2,500.00000	\$60,000.00
0020 624E10000 MOBILIZATION	1.000	LS	\$100,000.00000	\$100,000.00
			Total for Group 0001:\$4,960,	450.00

CY 2017-2021 Business Plan Inflation Calculator:							
<u>Not sure if y</u>	Not sure if you have the latest calculator? Click here.						
Last Modified: 1/19/2017		Today's Date:					
Please Enter Values in the Yellow	Areas Only:	May 17, 2017					
<b>Estimation Start Date:</b> Less than or Equal to Today's D (mm/dd/yyyy)	Date	Enter Construction Mid-Point Date: (cannot exceed 05/17/2042) (mm/dd/yyyy)					
5/17/2017		7/1/2020					
Start Date:		Construction Mid-Point Date:					
Present-Day Estimated Cost \$9,247,000.00 Estimated Dollar Amount:	t: 						
Estimate Start Date to Cons	truction Mid Doin	t Date: 29 Months					
Inflation - Start to Mid-Poin	nt of Construction	<b>:</b>					
(compounded growth i	rate)	Inflated Dollar Amount:					
Business Plan	11.9%	\$10,344,069.10					
Estimator's Name:							
County - Route - Section:	CUY-6-14.56						
PTD.	99972						
Estimator's Notos							
Estimator's Notes:	Alternative No. 2B						

Estimated Cost:\$7,705,985.00 Contingency: 20.00%

### Estimated Total: \$9,247,182.00

Alternative No. 2B

#### Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17 Checked by WJV on 05/17/17

Line # Item Number Description Supplemental Description	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
Group 0001: STRUCTURE				

0001 CC WI	511E81100 DNCRETE, MISC.: EST STATION CONCRETE BEAM RE	170.000 PLACEMEN	FT <i>T</i>	\$400.00000	\$68,000.00
0002 CC LC	511E81300 DNCRETE, MISC.: DWER DECK CORBEL REPLACEMEN	25.000	EACH	\$3,000.00000	\$75,000.00
0003 CC CC	511E81300 DNCRETE, MISC.: DLUMN REPLACEMENT	7.000	EACH	\$8,500.00000	\$59,500.00
0004 Se	512E10101 EALING OF CONCRETE SURFACES (EPOX	10,590.000 Y-URETHANE	SY E), AS PER	\$15.00000 PLAN	\$158,850.00
0005 CC (Al	512E10600 DNCRETE REPAIR BY EPOXY INJECTION RCH RIB)	800.000	FT	\$70.00000	\$56,000.00
0006 RE	512E74000 EMOVAL OF EXISTING COATINGS FROM C	6,860.000 CONCRETE SU	SY JRFACES	\$20.00000	\$137,200.00
0007 JA	516E47000 CKING AND TEMPORARY SUPPORT OF S	1.000 UPERSTRUC	LS TURE	\$20,000.00000	\$20,000.00
0008 SF <i>(Al</i>	519E00100 PECIAL - COMPOSITE FIBER WRAP SYSTE RCH RIBS)	55,693.000 M	SF	\$45.00000	\$2,506,185.00
0009 SF <i>(W</i>	519E11600 PECIAL - PATCHING CONCRETE STRUCTL /EST STATION, TUNNELS, AND UPPI	15,300.000 JRE <b>ER DECK</b> )	SF	\$90.00000	\$1,377,000.00
0010 SF <i>(L</i> C	519E11600 PECIAL - PATCHING CONCRETE STRUCTL OWER SUPERSTRUCTURE, VERTIC	9,590.000 JRE <i>AL SURFAC</i>	SF ES)	\$100.00000	\$959,000.00
0011 SF <i>(L</i> 0	519E11600 PECIAL - PATCHING CONCRETE STRUCTU OWER SUPERSTRUCTURE, BOTTO	5,560.000 JRE <i>M AND CUR</i>	SF VED SUI	\$125.00000 RFACES)	\$695,000.00
0012 SF (D	519E11900 PECIAL - PATCHING CONCRETE STRUCTL EEP PIER SHAFT DETERIORATION)	6.000 JRE	CY	\$5,000.00000	\$30,000.00
0013 SF BF	530E00200 PECIAL - STRUCTURES RIDGE OPERATOR'S CAR SHELTER	1.000	LS	\$5,000.00000	\$5,000.00
0014 SF CC	530E00400 PECIAL - STRUCTURES DRBEL SHIELD	200.000	EACH	\$200.00000	\$40,000.00
0015 SF <i>MA</i>	530E00600 PECIAL - STRUCTURES ASONRY BLOCK WALL	900.000	SF	\$10.00000	\$9,000.00
0016 LIC NA	625E98200 GHTING, MISC.: IVIGATION LIGHTING REPAIR	1.000	LS	\$20,000.00000	\$20,000.00
0017 CC	844E10001 DNCRETE PATCHING WITH GALVANIC AN	30,450.000 ODE PROTEC	SF TION, AS	\$20.00000 PER PLA N	\$609,000.00
0018 MI 2:10:20	848E10000 CRO SILICA MODIFIED CONCRETE OVER	17,750.000 LAY USING H	SY YDRODEN	\$25.00000 IOLITION	\$443,750.00
Wednes	day, May 17, 2017				Page 2 of 3

Estimate: (	ODOT1602
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Line # <u>Item Number</u> <u>Description</u> Supplemental Desc	<u>Quantity</u> cription	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
0019 848E50320 EXISTING CONCRETE	17,750.000 E OVERLAY REMOVED	SY	\$10.00000	\$177,500.00
0020 614E11000 MAINTAINING TRAFF	1.000 C	LS	\$100,000.00000	\$100,000.00
0021 619E16020 FIELD OFFICE, TYPE	24.000 C	MNTH	\$2,500.00000	\$60,000.00
0022 624E10000 MOBILIZATION	1.000	LS	\$100,000.00000	\$100,000.00

Total for Group 0001:\$7,705,985.00

CY 2017-2021 Business Plan Inflation Calculator:						
Not sure if you have the latest calculator? Click here.						
Last Modified: 1/19/2017		Today's Date:				
Please Enter Values in the Yellow	Areas Only:	May 17, 2017				
<b>Estimation Start Date:</b> Less than or Equal to Today's D (mm/dd/yyyy)	Date	Enter Construction Mid-Point Date: (cannot exceed 05/17/2042) (mm/dd/yyyy)				
5/17/2017		7/1/2020				
Start Date:		Construction Mid-Point Date:				
Present-Day Estimated Cost \$12,553,000.00 Estimated Dollar Amount:	:: 					
Estimate Start Date to Cons	truction Mid-Poir	t Date: 38 Months				
Inflation - Start to Mid-Poin	nt of Constructior					
(compounded growth i	rate)	Inflated Dollar Amount:				
<b>Business Plan</b>	11.9%	\$14,042,294.74				
Estimator's Name:						
County - Route - Section:	CUY-6-14.56					
PID:	99972					
Estimator's Notes	Altornativo No. 20					
Estimator 5 Notes.	Alternative No. 20					

Estimated Cost:\$10,461,340.00 Contingency: 20.00%

Contangonoy. 20.0070

### Estimated Total: \$12,553,608.00

Alternative No. 2C

#### Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17 Checked by WJV on 05/17/17

<u>Line #</u> <u>Item Number</u> <u>Description</u> <u>Supplemental Description</u>	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
Group 0001: STRUCTURE				

0001	511E81100	170.000	FT	\$400.00000	\$68,000.00
CO WE	NCRETE, MISC.: ST STATION CONCRETE BEAM RE	PLACEMEN	т		
0002	511E81300	25.000	EACH	\$3,000.00000	\$75,000.00
LOI	NCRETE, MISC.: NER DECK CORBEL REPLACEMEN	NT.			
0003	511E81300	7.000	EACH	\$8,500.00000	\$59,500.00
со СО	NCRETE, MISC.: LUMN REPLACEMENT				
0004	512E10101	17,430.000	SY	\$15.00000	\$261,450.00
SE	ALING OF CONCRETE SURFACES (EPO)	Y-URETHANE	:), AS PEF	PLAN	
0005	512E10600	800.000	FT	\$70.00000	\$56,000.00
CO (AR	NCRETE REPAIR BY EPOXY INJECTION				
0006	512E74000	13,680.000	SY	\$20.00000	\$273,600.00
RE	MOVAL OF EXISTING COATINGS FROM	CONCRETE SU	JRFACES		
0007	540547000	4 000	1.0	<b>#00.000.0000</b>	<b>\$00,000,00</b>
0007			LS	\$20,000.00000	\$20,000.00
JAC	CRING AND TEMPORART SUPPORT OF S	DUPERSTRUC	IURE		
8000	519E00100	55,693.000	SF	\$45.00000	\$2,506,185.00
SPI	ECIAL - COMPOSITE FIBER WRAP SYSTE	ΞM			
0009 (AR	519E00100	55,919,000	SF	\$45,00000	\$2,516,355,00
SPI	ECIAL - COMPOSITE FIBER WRAP SYSTE	EM		•••••••••	<i> </i>
(FL	OOR BEAMS)	45 000 000	05	<b>A</b> AA AAAAA	<b>*</b> 4 077 000 00
0010		15,300.000	SF	\$90.00000	\$1,377,000.00
(WE	EST STATION, TUNNELS, AND UPP	ER DECK)			
0011	519E11600	9,590.000	SF	\$100.00000	\$959,000.00
SPI	ECIAL - PATCHING CONCRETE STRUCT	JRE			
0012	519E11600	5.560.000	SF	\$125.00000	\$695.000.00
SPI	ECIAL - PATCHING CONCRETE STRUCT	JRE			, ,
(LO	WER SUPERSTRUCTURE, BOTTO	MAND CUR	VED SU	RFACES)	¢20.000.00
0013		0.000	Cr	\$5,000.00000	\$30,000.00
(DE	EP PIER SHAFT DETERIORATION)				
0014	530E00200	1.000	LS	\$5,000.00000	\$5,000.00
SPI RD	ECIAL - STRUCTURES				
0015	530E00400	200.000	EACH	\$200.00000	\$40,000.00
SPI	ECIAL - STRUCTURES				
CO	RBEL SHIELD	000 000	05	¢10,00000	¢0,000,00
		900.000	ЪГ	\$10.00000	\$9,000.00
MA	SONRY BLOCK WALL				
0017	625E98200	1.000	LS	\$20,000.00000	\$20,000.00
	HTING, MISC.: /IGATION LIGHTING REPAIR				
0018	844E10001	30,450.000	SF	\$20.00000	\$609,000.00
со	NCRETE PATCHING WITH GALVANIC AN	IODE PROTEC	TION, AS	PER PLA N	
2:22:13F	PM				

Wednesday, May 17, 2017

MOBILIZATION

<u>Line #</u> Des <u>Sup</u>	<u>Item Number</u> <u>cription</u> plemental Description	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
0019	848E10000	17,750.000	SY	\$25.00000	\$443,750.00
MIC	RO SILICA MODIFIED CONCRETE OVER	LAY USING H	YDRODE	MOLITION	
0020	848E50320	17,750.000	SY	\$10.00000	\$177,500.00
EXI	STING CONCRETE OVERLAY REMOVED				
0021	614E11000	1.000	LS	\$100,000.00000	\$100,000.00
MAI	NTAINING TRAFFIC				
0022	619E16020	24.000	MNTH	\$2,500.00000	\$60,000.00
FIEI	LD OFFICE, TYPE C				
0023	624E10000	1.000	LS	\$100,000.00000	\$100,000.00

Total for Group 0001:\$10,461,340.00

CY 2017-2021 Business Plan Inflation Calculator:						
Not sure if you have the latest calculator? Click here.						
Last Modified: 1/19/2017		Today's Date:				
Please Enter Values in the Yellow	Areas Only:	May 17, 2017				
<b>Estimation Start Date:</b> Less than or Equal to Today's D (mm/dd/yyyy)	Pate	Enter Construction Mid-Point Date: (cannot exceed 05/17/2042) (mm/dd/yyyy)				
5/17/2017		7/1/2020				
Start Date:		Construction Mid-Point Date:				
Present-Day Estimated Cost \$13,770,000.00 Estimated Dollar Amount:	:: 					
Estimate Start Date to Cons	truction Mid-Poin	at Date: 38 Months				
Inflation - Start to Mid-Poin	nt of Construction	1:				
(compounded growth i	rate)	Inflated Dollar Amount:				
Business Plan	11.9%	\$15,403,680.28				
Estimator's Name:						
County - Route - Section:	CUY-6-14.56					
PID:	99972					
Estimator's Notes:	Alternative No. 2D					

Estimated Cost:\$11,474,700.00 Contingency: 20.00%

Estimated Total: \$13,769,640.00

Alternative No. 2D

#### Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17 Checked by WJV on 05/17/17

Line # <u>Item Number</u> <u>Description</u> <u>Supplemental Description</u>	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
Group 0001: STRUCTURE				

0001	511E81100	170.000	FT	\$400.00000	\$68,000.00
CO WE	NCRETE, MISC.: ST STATION CONCRETE BEAM RI	EPLACEMEN	т		
0002	511E81300	25.000	EACH	\$3,000.00000	\$75,000.00
LO	NCRETE, MISC.: WER DECK CORBEL REPLACEME	NT			
0003	511E81300	7.000	EACH	\$8,500.00000	\$59,500.00
со СО	NCRETE, MISC.: LUMN REPLACEMENT				
0004	512E10101	19,910.000	SY	\$15.00000	\$298,650.00
SE	ALING OF CONCRETE SURFACES (EPO	XY-URETHANE	E), AS PEF	{ PLAN	
0005	512E10600	. 800.000	FT	\$70.00000	\$56,000.00
(AF	NCRETE REPAIR BY EPOXY INJECTION RCH RIB)	1			
0006	512E74000	16,210.000	SY	\$20.00000	\$324,200.00
RE	MOVAL OF EXISTING COATINGS FROM	CONCRETE S	JRFACES		
0007	516E47000	1.000	LS	\$20,000.00000	\$20,000.00
JAC	CKING AND TEMPORARY SUPPORT OF	SUPERSTRUC	TURE		
0008	519E00100	55,693.000	SF	\$45.00000	\$2,506,185.00
SPI (AF	ECIAL - COMPOSITE FIBER WRAP SYST	EM			
0009	519E00100	20,568.000	SF	\$45.00000	\$925,560.00
SPI <i>(EN</i>	ECIAL - COMPOSITE FIBER WRAP SYST ID COLUMNS)	EM			
0010	519E00100	55,919.000	SF	\$45.00000	\$2,516,355.00
SPI (FL	ECIAL - COMPOSITE FIBER WRAP SYST OOR BEAMS)	EM			
0011	519E11600	15,300.000	SF	\$90.00000	\$1,377,000.00
SPI (WE	ECIAL - PATCHING CONCRETE STRUCT EST STATION, TUNNELS, AND UPP	URE PER DECK)			
0012	519E11600	9,590.000	SF	\$100.00000	\$959,000.00
SPI (LO	ECIAL - PATCHING CONCRETE STRUCT WER SUPERSTRUCTURE, VERTIN	<sup>-</sup> URE CAL SURFAC	ES)		
0013	519E11600	5,560.000	SF	\$125.00000	\$695,000.00
SPI	ECIAL - PATCHING CONCRETE STRUCT				
0014	519E11900	6.000	CY	\$5.000.00000	\$30,000,00
SPI (DE	ECIAL - PATCHING CONCRETE STRUCT	URE	•	<i><b>4</b>-,</i>	<i> </i>
0015	530E00200	1.000	LS	\$5,000.00000	\$5,000.00
SP	ECIAL - STRUCTURES				
0016	530E00400	200.000	FACH	\$200.00000	\$40,000,00
SPI	ECIAL - STRUCTURES	200.000	E/ (OII	¢200.00000	\$10,000.00
0017	530E00600	900.000	SF	\$10.00000	\$9,000.00
SPI MA	ECIAL - STRUCTURES SONRY BLOCK WALL				
0018	625E98200	1.000	LS	\$20,000.00000	\$20,000.00
LIG	HTING, MISC.:				
2:26:32F	PM				
Estimate:	ODOT1602				
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<u>Line #</u> Des Sup	<u>Item Number</u> <u>cription</u> plemental Description	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
NAV	IGATION LIGHTING REPAIR				
0019	844E10001	30,450.000	SF	\$20.00000	\$609,000.00
COI	NCRETE PATCHING WITH GALVANIC AN	NODE PROTEC	CTION, AS	PER PLA N	
0020	848E10000	17,750.000	SY	\$25.00000	\$443,750.00
MIC	RO SILICA MODIFIED CONCRETE OVEF	RLAY USING H	YDRODE	MOLITION	
0021	848E50320	17,750.000	SY	\$10.00000	\$177,500.00
EXI	STING CONCRETE OVERLAY REMOVED	)			
0022	614E11000	1.000	LS	\$100,000.00000	\$100,000.00
MAI	NTAINING TRAFFIC				
0023	619E16020	24.000	MNTH	\$2,500.00000	\$60,000.00
FIE	LD OFFICE, TYPE C				
0024	624E10000	1.000	LS	\$100,000.00000	\$100,000.00
MO	BILIZATION				

Total for Group 0001:\$11,474,700.00

CY 2017-2021 Business Plan Inflation Calculator:								
Not sure if you have the latest calculator? Click here.								
Last Modified: 1/19/2017		Today's Date:						
Please Enter Values in the Yellow	Areas Only:	May 17, 2017						
<b>Estimation Start Date:</b> Less than or Equal to Today's D (mm/dd/yyyy)	ate	Enter Construction Mid-Point Date: (cannot exceed 05/17/2042) (mm/dd/yyyy)						
5/17/2017 Start Date:		7/1/2020 Construction Mid-Point Date:						
Present-Day Estimated Cost \$17,440,000.00 Estimated Dollar Amount:	: _							
Estimate Start Date to Cons Inflation - Start to Mid-Poin	truction Mid-Poir	nt Date: <u>38</u> Months						
(compounded growth r	rate)	Inflated Dollar Amount:						
Business Plan	11.9%	\$19,509,091.07						
Estimator's Name:								
County - Route - Section:	CUY-6-14.56							
PID:	99972							
Estimator's Notes:	Alternative No. 2E							

### Estimate ODOT1602

Estimated Cost:\$14,532,550.00 Contingency: 20.00%

#### Estimated Total: \$17,439,060.00

Alternative No. 2E

#### Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17 Checked by WJV on 05/17/17

Line # Item Number Description Supplemental Description	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
Group 0001: STRUCTURE				

0001	511E81100	170.000	FT	\$400.00000	\$68,000.00
CC WE	ONCRETE, MISC.: EST STATION CONCRETE BEAM RE	PLACEMEN	т		
0002	511E81300	25.000	EACH	\$3,000.00000	\$75,000.00
CC	NCRETE, MISC.:	IT.			
0003	511E81300	7.000	EACH	\$8,500,00000	\$59.500.00
CC	DNCRETE, MISC.:			<i>+-,</i>	<i> </i>
CC	LUMN REPLACEMENT				
0004	512E10101	27,480.000	SY	\$15.00000	\$412,200.00
SE	ALING OF CONCRETE SURFACES (EPOX	Y-URE I HANE	:), AS PEF	( PLAN	
0005	512E10600	800.000	FT	\$70.00000	\$56,000.00
	ONCRETE REPAIR BY EPOXY INJECTION				
0006	512E74000	23,790.000	SY	\$20.00000	\$475,800.00
RE	MOVAL OF EXISTING COATINGS FROM	CONCRETE SU	JRFACES		
0007	516E47000	1.000	LS	\$20,000.00000	\$20,000.00
JA	CKING AND TEMPORARY SUPPORT OF S	OPERSTRUC	TURE		
8000	519E00100	55,693.000	SF	\$45.00000	\$2,506,185.00
SF	ECIAL - COMPOSITE FIBER WRAP SYSTE	EM			
(AF	RCH RIBS)	62 060 000	<u>ог</u>	¢45,00000	¢0,700,700,00
0009		02,000.000	3F	\$45.00000	\$2,792,700.00
(LC	WER DECK SUPPORT COLUMNS)	_1VI			
0010	519E00100	20,568.000	SF	\$45.00000	\$925,560.00
SF	ECIAL - COMPOSITE FIBER WRAP SYSTE	EM			
0011	519E00100	55.919.000	SF	\$45.00000	\$2.516.355.00
SF	ECIAL - COMPOSITE FIBER WRAP SYSTE	EM			<i>,</i> ,
(FL	OOR BEAMS)		~-		
0012		15,300.000	SF	\$90.00000	\$1,377,000.00
SF (W	EST STATION. TUNNELS. AND UPP	ER DECK)			
0013	519E11600	9,590.000	SF	\$100.00000	\$959,000.00
SF	ECIAL - PATCHING CONCRETE STRUCTU	JRE			
(LC	WER SUPERSTRUCTURE, VERTIC	AL SURFAC	SES)	\$125,00000	\$605,000,00
SF	ECIAL - PATCHING CONCRETE STRUCT	JRF	01	\$123.00000	ψ033,000.00
(LC	WER SUPERSTRUCTURE, BOTTO	MAND CUR	VED SU	RFACES)	
0015	519E11900	6.000	CY	\$5,000.00000	\$30,000.00
SF	ECIAL - PATCHING CONCRETE STRUCTU	JRE			
0016	530E00200	1.000	LS	\$5,000.00000	\$5,000.00
SF	ECIAL - STRUCTURES				
BR	IDGE OPERATOR'S CAR SHELTER		-	4000 0000	<b>*</b> 40,000,00
0017		200.000	EACH	\$200.00000	\$40,000.00
SP	BEL STRUCTURES				
0018	530E00600	900.000	SF	\$10.00000	\$9,000.00
SF	ECIAL - STRUCTURES				
2:25:56	PM				
					<b>B A I I</b>

Wednesday, May 17, 2017

Estimate:	ODOT1602
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.sumate.	00011002				
<u>Line #</u> Des Sup	l <u>tem Number</u> cription plemental Description	<u>Quantity</u>	<u>Units</u>	Unit Price	<u>Extension</u>
MAS	SONRY BLOCK WALL				
0019 LIGI NAV	625E98200 HTING, MISC.: <i>'IGATION LIGHTING REPAIR</i>	1.000	LS	\$20,000.00000	\$20,000.00
0020	844E10001	30,450.000	SF	\$20.00000	\$609,000.00
CON	NCRETE PATCHING WITH GALVANIC A	NODE PROTEC	TION, AS	PER PLA N	
0021	848E10000	17,750.000	SY	\$25.00000	\$443,750.00
MIC	RO SILICA MODIFIED CONCRETE OVE	RLAY USING H	YDRODE	MOLITION	
0022	848E50320	17,750.000	SY	\$10.00000	\$177,500.00
EXI	STING CONCRETE OVERLAY REMOVE	D			
0023	614E11000	1.000	LS	\$100,000.00000	\$100,000.00
MAI	NTAINING TRAFFIC				
0024	619E16020	24.000	MNTH	\$2,500.00000	\$60,000.00
FIEL	LD OFFICE, TYPE C				
0025	624E10000	1.000	LS	\$100,000.00000	\$100,000.00
MOI	BILIZATION				

Total for Group 0001:\$14,532,550.00

CY 2017-2021 Business Plan Inflation Calculator:						
<u>Not sure if ye</u>	ou have the late	est calculator?	Click here	<u>.</u>		
Last Modified: 1/19/2017			Toda	av's Date:		
Please Enter Values in the Yellow	Areas Only:		Februa	ary 15, 2017		
Estimation Start Date: Less than or Equal to Today's Da (mm/dd/yyyy)	ate	Enter Construct (cannot exceed 02 (mm/dd/yyyy)	<b>ion Mid-Poin</b> 2/15/2042)	t Date:		
2/15/2017 Start Date:		Construction Mid-Poin	<b>1/2020</b> nt Date:			
Present-Day Estimated Cost \$29,519,400.00 Estimated Dollar Amount:	:					
Estimate Start Date to Const Inflation - Start to Mid-Poin	truction Mid-Point	t Date:	41	Months		
(compounded growth r	ate)	Inflated Dollar	Amount:			
Business Plan	12.6%	\$33,226,0	075.52	[		
Estimator's Name:						
County - Route - Section:	CUY-6-1456					
PID:	99972					
Estimator's Notes:	Alternate 3 - Rehab w	/ Patching and Cathodic	c Protection			

### Estimate ODOT1602

Estimated Cost:\$24,599,500.00

Contingency: 20.00%

#### Estimated Total: \$29,519,400.00

ALTERNATE 3 - REHAB W/ PATCHING AND ACTIVE CATHODIC PROTECTION

#### Base Date: 02/13/17

Spec Year: 16

Unit System: E

#### Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type:

#### Season:

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number:

Prepared by DEA on 02/13/17 Checked by WJV on 02/14/17

Line # Item Number	<u>Quantity</u>	<u>Units</u>	Unit Price	Extensior
Description Supplemental Description				
<b>o</b>				

#### Group 0001: STRUCTURE

0005	511E81100	150.000	FT	\$400.00000	\$60,000.00
COI WE	NCRETE, MISC.: ST STATION CONCRETE BEAM REI	PLACEMEN	Т		
0006	511E81300	25.000	EACH	\$3,000.00000	\$75,000.00
CO	NCRETE, MISC.:	_			
LOV	VER DECK CORBEL REPLACEMEN	T 4 000			¢04.000.00
0007	511E81300	4.000	EACH	\$8,500.00000	\$34,000.00
	NCRETE, MISC.: LIMNEREDIACEMENT				
0008	512E10101	2.000.000	SY	\$15.00000	\$30.000.00
SEA	ALING OF CONCRETE SURFACES (EPOX	Y-URETHANE	). AS PER	PLAN	¥ )
	X		,,		
0009	512E10600	800.000	FT	\$70.00000	\$56,000.00
COI ARC	NCRETE REPAIR BY EPOXY INJECTION				
0010	512E74000	2,000.000	SY	\$20.00000	\$40,000.00
RE	MOVAL OF EXISTING COATINGS FROM C	ONCRETE SU	JRFACES		
0011	516E47000	1.000	LS	\$20,000.00000	\$20,000.00
JAC	KING AND TEMPORARY SUPPORT OF S	UPERSTRUC	TURE		
0013	519E11600	15,000.000	SF	\$90.00000	\$1,350,000.00
SPE	ECIAL - PATCHING CONCRETE STRUCTU				
0014	519E11600	9 500 000	SE	\$100,0000	\$950 000 00
SPE	-CIAL - PATCHING CONCRETE STRUCTU	18F	01	\$100.00000	φ300,000.00
LOV	VER SUPERSTRUCTURE, VERTICA	AL SURFACI	ES		
0015	519E11600	5,500.000	SF	\$125.00000	\$687,500.00
SPE	ECIAL - PATCHING CONCRETE STRUCTU	IRE			
LOV	VER SUPERSTRUCTURE - BOTTO	MAND CUR	VED SUI	RFACES	¢20,000,00
0016		6.000	CY	\$5,000.00000	\$30,000.00
DEF	ECIAL - PATCHING CONCRETE STRUCTU EP PIER SHAFT DETERIORATION	IRE			
0017	530E00200	1.000	LS	\$5,000.00000	\$5,000.00
SPE	ECIAL - STRUCTURES				. ,
BRI	DGE OPERATOR'S CAR SHELTER				
0018	530E00400	200.000	EACH	\$200.00000	\$40,000.00
SPE COI	ECIAL - STRUCTURES RBEL SHIELD				
0019	530E00600	900.000	SF	\$10.00000	\$9,000.00
SPE MAS	ECIAL - STRUCTURES SONRY BLOCK WALL				
0020	530E00600 32	25,000.000	SF	\$60.00000	\$19,500,000.00
SPE	ECIAL - STRUCTURES				
CA1	625E98200	SSED CUR	RENT	\$20,000,00000	\$20,000,00
1100		1.000	L0	ψ20,000.00000	φ20,000.00
NAL	/IGATION LIGHTING REPAIR				
0023	848E10000	19,400.000	SY	\$60.00000	\$1,164,000.00
MIC				PODEMOLITION	
IVIIC	RU SILICA MODIFIED CONCRETE	OVELAY US	ING HYL	RODEWOLITION	

Estimate:	ODOT1602				
<u>Line #</u> Dese <u>Sup</u>	<u>Item Number</u> cription plemental Description	<u>Quantity</u>	<u>Units</u>	<u>Unit Price</u>	<u>Extension</u>
0024 EXIS	848E50320 STING CONCRETE OVERLAY REMOVED	19,400.000	SY	\$10.00000	\$194,000.00
				Total for Group 0001:\$24,26	64,500.00
Group	0002: INCIDENTAL				
0025 MAIN	614E11000 ITAINING TRAFFIC	1.000	LS	\$100,000.00000	\$100,000.00
0026 MAII RAII	614E18002 NTAINING TRAFFIC, MISC.: .ROAD FLAGGER	1.000	LS	\$50,000.00000	\$50,000.00
0027 MAII RAII	614E18002 NTAINING TRAFFIC, MISC.: .ROAD COORDINATION	1.000	LS	\$25,000.00000	\$25,000.00
0028 FIELI	619E16020 D OFFICE, TYPE C	24.000	MNTH	\$2,500.00000	\$60,000.00

1.000 LS \$100,000.00000 \$100,000.00

Total for Group 0002:\$335,000.00

0029

624E10000

MOBILIZATION

## APPENDIX B

**PUBLIC AREA BELOW STRUCTURE** 



CUY-6-1456 over Cuyahoga River Rehabilitation Feasibility Study Ohio Department of Transportation



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## APPENDIX C

**CONCRETE PH RESULTS** 



CUY-6-1456 over Cuyahoga River Rehabilitation Feasibility Study Ohio Department of Transportation

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH					
Client	Jones Stuckey	Project No.	G17005T					
Sample No.	1A	Date.	1/30/2017					
Core Location	Span 7, Arch Rib, South Interior Concrete (Bottom North Corner, Near Center)							

#### **Rainbow Indicator**





Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The aggregates in the concrete in between depths of 0 to 3.5 inches have dominant green color with less purple color indicating a pH of 9 to 10.

In surrounding area of the aggregates have a dark purple color indicating a pH of 11.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH	
Client	Jones Stuckey	Project No.	G17005T	
Sample No.	1B	Date.	1/30/2017	
Core Location	Span 7, Arch Rib, South Interior Shotcrete (Bottom North Corner, Near Center)			

#### **Rainbow Indicator**





Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The upper depth of shotcrete from 0.0 to 0.25 inches has dominant green color indicating a pH of 9.

The inner part of shotcrete from 0.25 to 1.5 inches has a dominant dark purple color indicating a pH of 12.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue B	ridge Rehabili	tation	Location	Cuyahoga Co	ounty, OH
Client	Pennoni			Project No.	G17005T	
Sample No.	2		Date.	1/30/2017		
<b>Core Location</b>	Span 7, LD Floor B	eam, 4 North	Bay Sho	otcrete		
Rainbow Indica	tor Color: pH:	5	7	9	11	13
	BEFORE				AFTER	
		T         T				Image: Second system         Image: Second system

Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The upper depth of shotcrete from 0.0 to 0.25 inches has a green color indicating a pH of 9.

The inner part of shotcrete from 0.25 to 1.5 inches has a dominant dark purple color indicating a pH of 12.

Also note that the aggregates in between depths of 0.25 and 1.5 inches have a green color indicating a pH of 9.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH
Client	Jones Stuckey	Project No.	G17005T
Sample No.	3	Date.	1/30/2017
Core Location	Span 7, LD Column, North Interior 14 Concrete		

# Rainbow IndicatorColor:pH:5791113



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The upper depth of the concrete from 0.0 to 0.5 inches has a dominant green color indicating a pH of 9.

The lower depth of the concrete from 0.5 to 1.25 inches has a dominant dark purple color indicating a pH of 12.

The aggregates in concrete between depths of 0 to 1.25 inches have green and purple colors indicating a pH of 9 to 10.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH			
Client	Jones Stuckey	Project No.	G17005T			
Sample No.	4	<b>Date.</b> 1/30/2017				
Core Location	Span 8, Jack Arch, North Interior Shotcrete					





Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The upper depth of shotcrete from 0.0 to 0.15 inches has a dominant green color indicating a pH of 9.

The inner part of shotcrete from 0.15 to 1.0 inches has a dominant dark purple color indicating a pH of 12.

Also note that the aggregates in between depths of 0.15 to 1.0 inches have green color indicating a pH of 9.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH			
Client	Jones Stuckey	Project No.	G17005T			
Sample No.	5	<b>Date.</b> 1/30/2017				
Core Location	Span 8, LD Floor Beam, 9 Center Bay Concrete					

#### **Rainbow Indicator**





Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

Most of the aggregates between depths of 0 to 1.0 inches have a dominant purple color with less green color in the surrounding area indicating a pH of 10 to 11.

Some of the aggregates in between depths of 1.0 to 2.0 inches have a green color indicating a pH of 9.

The dark purple color corresponding to a pH of 12 is dominant between depths of 1.0 to 2.0 inches.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH	
Client	Jones Stuckey	Project No.	G17005T	
Sample No.	6	Date.	1/30/2017	
Core Location	Span 8. LD Floor Beam. 10 Center Bay Concrete			

#### **Rainbow Indicator**





Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

Most of the aggregates between depths of 0 to 1.0 inches have a dominant purple color with less green color in the surrounding area indicating a pH of 10 to 11.

The dark purple color, corresponding to a pH of 12, is dominant between depths of 1.0 to 3.0 inches.

Also note that some of the aggregates in between depths of 2 to 3.5 inches have a green color indicating a pH of 9.



GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH	
Client	Jones Stuckey	Project No.	G17005T	
Sample No.	7	Date.	1/30/2017	
Core Location	Span 8, LD Floor Beam, 11 Center Bay Concrete			

# Rainbow Indicator Color: PH: 5 7 9 11 13



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

Most of the aggregates between depths of 0 to 2 inches have a dominant purple color with less green color in the surrounding area indicating a pH of 10 to 11.

The dark purple color, corresponding to a pH of 12, is dominant between depths of 2 to 3.0 inches.

Also note that some of the aggregates in between depths of 2 to 3.0 inches have a green color indicating a pH of 9.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH
Client	Jones Stuckey	Project No.	G17005T
Sample No.	8	Date.	1/30/2017
Core Location	Span 8, LD Floor Beam, 14 South Bay Concrete		

# Rainbow Indicator Color: 9 11 13



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The depth between 0 and 0.75 inches have green and purple colors indicating a pH of 9 to 10.

The dark purple color, corresponding to a pH of 12, is dominant at depth 0.75 to 1.5 inches.

Also note that the aggregates in between depths of 0 to 1.5 inches have green and purple colors indicating a pH of 9 to 10.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH
Client	Jones Stuckey	Project No.	G17005T
Sample No.	9	Date.	1/30/2017
Core Location	Span 9, LD Column, North Interior 13 Concrete		





Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

Most of the aggregates between depths of 0 to 1.5 inches have dominant purple color indicating a pH of 10 to 11 with surrounding area having green color indicating a pH of 9.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH	
Client	Jones Stuckey	Project No.	G17005T	
Sample No.	10	Date.	1/30/2017	
<b>Core Location</b>	Span 10, LD Floor Beam, 1 South Bay Shotcrete			
Core Location	Span 10, ED 1 1001 Deann, 1 South Day S	noterete		





Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The entire depth from 0.0 to 3.5 inches has a dominant dark purple color indicating a pH of 12.

Also note that some of the aggregates have a green color indicating a pH of 9.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Bridge Rehabilitation	Location	Cuyahoga County, OH
Client	Jones Stuckey	Project No.	G17005T
Sample No.	11	Date.	1/30/2017
Core Location	Span 10, LD Floor Beam, 2 South Bay Concrete		

#### **Rainbow Indicator**





Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

Most of the aggregates between depths of 0 to 3.0 inches have dominant purple color indicating a pH of 10 to 11 with the surrounding area having green color indicating a pH of 9.

per GERMANN INSTRUMENTS Manual



Project	Superior Avenue Br	idge Rehabili	tation	Loca	ation	Cuyahoga C	County, OH	
Client	Jones Stuckey			Proj	ject No.	<b>.</b> G17005T		
Sample No.	12 <b>Date.</b> 1/30/2017							
<b>Core Location</b>	Span 10, LD Pier Sh	aft Shotcrete						
Rainbow Indica	tor Color: pH:	5	7	7	9	11	13	
	BEFORE					AFTER		
						3 4		

Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The entire depth from 0.0 to 7.0 inches has dominant dark purple color indicating a pH of 12.

Also note that the aggregates have a green color indicating a pH of 9.

## APPENDIX D

ESTIMATED CONCRETE PATCHING QUANTITIES



CUY-6-1456 over Cuyahoga River Rehabilitation Feasibility Study Ohio Department of Transportation

## CUY-6-1456 ARCH REPAIR

Snan	Location	Total	North Exterior	North Interior	South Interior	South Exterior
Span	Location	(SF)	Вау	Вау	Вау	Вау
1	Vertical	672	206	106	140	220
L	Bottom	537	165	100	104	168
2	Vertical	22	22	0	0	0
2	Bottom	44	44	0	0	0
2	Vertical	10	0	10		
5	Bottom	25	25	0		
F	Vertical	123	16	39	68	0
5	Bottom	136	16	17	25	78
6	Vertical	246	130	42	74	0
0	Bottom	303	84	97	20	102
7	Vertical	0	0	0	0	0
7	Bottom	432	86	16	198	132
0	Vertical	0	0	0	0	0
0	Bottom	579	162	163	92	162
0	Vertical	26	0	0	26	0
9	Bottom	116	0	70	26	20
10	Vertical	0	0	0	0	0
10	Bottom	445	0	0	271	174
11	Vertical	27	18	0	0	9
11	Bottom	0	0	0	0	0
12	Vertical	71	10	0	26	35
12	Bottom	374	144	16	90	124
12	Vertical	81		24	14	43
13	Bottom	308		119	62	127
Vertical	Patches Total =	1278	SE	Snan 3 South &	Exterior Arches	]

Vertical Patches Total =	1278 SF	Span 3 South & Exterior Arches
Bottom Patches Total =	3299 SF	are Difficult to Access, Span 13
		North Exterior Arch Rib Does
Total =	<b>4577</b> SF	Not Exist

#### CUY-6-1456 Lower Deck Column Patching

Total Deterioration: 2,143 SF

			North Exterior														North In	terior											Sout	th Inter	rior										9	South Ext	erior								
Span	Col. No.	Surface Total	Area 1	1 (SF)	Area 2 (SF)	Area 3 (SF)	H (in.)	W (in.)	Det H (in.)	terioratio W (in.	on ,	H (in.)	W (in.)	Col. No.	Surface Total	Area 1 (	SF) Ar	ea 2 SF)	Area 3 (SF)	H (in.)	W (in.)	Deter H (in.)	rioration W (in.)	H (in.)	W (in	v	Col. No.	Surface Total	Area 1 (	SF) Area (SF	a 2 Are ;) (Si	a 3 F) H	4	W (in.)	Deterior H (in.)	w (in.)	H (in.)	W (in.)	Col. No.	Surface Total	Area 1	(SF) Ar	rea 2 A (SF)	Area 3 (SF)	H (in.)	W (in.)	Deterio H (in.)	w (in.)	H (in.)	W (in.)	Span
Span 3	1 2 3 4 5 6 7 7 8 9 10 11 11 12 13 14 15 16 17 17 18 Subtotal Span Total	0 206 21 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 77 12 12 5 0 0 0 0 0 0 0 0 0 0 0 0 0	0 13 9 0 0 0 0 0 0 0 0 0 0 0 0 0	0 166 0 0 0 0 0 0 0 0 0 0 0 0 0	160 70 30 70	24 24 24 24 24 24 24 24 24 24 24 24 24 2						1 2 3 4 5 6 7 8 9 10 11 11 12 13 14 15 16 17 18 5 Subtotal	16 13 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		12 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	48 16 12 12 18	(III.) 12 13 13 24 18	112 36 12 12	24	48	24	4	1 2 3 4 5 6 7 7 8 9 9 10 11 12 13 13 14 15 16 16 17 17 18 btotal	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0											1 2 3 4 5 6 7 8 9 10 11 11 12 13 14 15 16 16 17 18 Subtotal				0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0							Span 3
Span 5	1 2 3 4 5 6 7 7 8 9 10 11 11 12 13 14 15 Subtotal Span Total	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0									1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15 5 5ubtotal				0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0							Sub	1 2 3 4 5 6 7 8 9 9 10 11 12 13 13 14 15 5 5 5 5 5 5 5 5 5 5	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0											1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15 5 5 9 5 0 10 11 12 13 14 5 5 5 5 6 7 7 8 9 9 10 9 10 9 10 9 10 9 10 9 10 9 10	10 0 12 9 0 0 0 1 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6 0 122 15 0 0 0 1 1 8 8 0 0 0 0 7 7 0 0 5		4 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	24 42 36 12 36 42 42 36	36 42 60 12 33 24 18	24	24			Span 5
Span 6	1 2 3 4 5 6 7 7 8 9 10 11 11 12 13 14 15 Subtotal Span Total	180 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	165 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	70	26	24	12		331	72	1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15 Subtotal	2 0 2 12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 0 0 1 1 12 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	24 12 76 54 210	12 12 22 42 24	12	12			Sub	1 2 3 4 5 6 7 7 8 9 9 10 11 12 13 13 14 15 5 5 5 5 5 5 5 6 7 7 8 9 9 9 10 11 11 12 13 14 15 5 5 7 7 8 9 9 10 9 10 9 10 9 10 9 10 9 10 10 10 10 10 10 10 10 10 10 10 10 10	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0											1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 Subtotal	22 0 14 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	12 0 14 4 0 0 0 0 0 0 1 1 0 0 0 0 1 1 0 0 0 0		10 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	72           42           24           12           48           21           60           24	24 48 24 12 12 24 24 24 24 24	60	24	36	54	Span 6
2 bau 2	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 Subtotal Span Total	28 2 7 0 0 0 0 0 0 0 0 2 0 0 2 2 0 145 188 373	14	3           1           4           0           0           0           0           0           0           0           0           0           0           0           0           0           0           0           5           0           15	6 1 3 0 0 0 0 0 0 0 0 0 0 0 0 0	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	72 12 24 41 18 145	25 12 24 16 18 145	58 12 30	16 12 12		80		1 2 3 4 5 6 7 7 8 9 10 11 12 13 14 15 Subtotal	30 4 7 0 0 0 0 0 0 0 0 1 1 0 0 13 0 55	23 2 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		7 2 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	84 12 20 12 12 16	40 24 50 12 32	60 12 45	16 24 31			Sub	1 2 3 4 5 6 7 7 8 9 9 10 11 12 13 14 15 5 5 5 5 5 5 5 5 5 6 6 7 7 7 8 9 9 10 11 11 12 5 5 5 6 6 7 7 7 8 9 9 5 5 6 6 7 7 8 9 9 10 9 10 9 10 9 10 9 10 10 10 10 10 10 10 10 10 10 10 10 10	32 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 33	32 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				2	24					1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 Subtotal	11 8 0 0 0 0 0 0 0 0 0 0 0 0 0	4 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	48 48 60 21 21 64 64	12 24 48 21 16 60	48	12 54 15	36	12	Span 7

					North Exterior												North In	terior									South Int	erior									South Ex	terior					
SI	pan	Col. No.	Surface Total	Area 1 (SF	Area 2 (SF)	Area 3 (SF)	Area 3 (SF) H W H W H \ (in.) (in.) (in.) (in.) (in.) (in.)			W (in.)	Col. No.	Surface Total	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)	H (in.)	W (in.)	Deteriorat H (in.)	tion W (in.) (i	H W n.) (in.)	Col. No.	Surface Total	e Area	a 1 (SF) Area 2 (SF)	2 Area 3 (SF)	H (in.)	W (in.)	Deterio H (in.)	ration W (in.)	H W (in.) (in.)	Col. No.	Surface Total	Area 1 (SF	) Area 2 (SF)	Area 3 (SF)	H (in.)	W (in.)	Deteriorat H (in.) (	ion W in.) (	H W in.) (in	Span		
	Subti	1 2 3 4 5 6 7 7 8 9 9 10 11 11 12 13 13 14 15 otal	0 19 0 0 0 0 0 0 0 0 0 0 0 0 0	0 18 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		112 112 72 66 84	23 40 32 25	8	18			1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 5 Subtotal	33 0 0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	13 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	36	24	58	34 9	20	1 2 3 4 5 6 7 8 8 9 10 11 12 13 3 14 15 5 Subtotal	191 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 226		9         182           0         0		112	12	162	162		1 2 3 4 5 6 7 8 9 10 0 11 11 12 13 3 14 15 5 Subtotal	11 1 0 0 0 0 0 0 0 0 0 0 0 0 0	11 1 0 0 0 0 0 0 0 0 0 0 0 0 0			132 12 18 18 66 180	12 12 18 18 18	20	42	68 51	Span 8
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	Span 10	1 2 3 4 5 5 6 7 8 9 10 11 11 12 12 0 tal	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0										1 2 3 4 5 6 7 7 8 9 10 10 11 11 12 Subtotal	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0						1 2 3 4 5 6 6 7 8 9 9 10 11 12 5 Subtotal	75 0 0 0 0 0 0 0 0 0 0 0 0 0 75		34         19           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0           0         0	22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	144	34	80	34	57 57	1 2 3 4 5 6 7 7 8 9 10 0 11 11 12 Subtotal	57 0 0 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	23 0 0 0 1 0 0 0 0 0 0 0 0 0 0 0 18		14 0 0 0 0 0 0 0 0 0 0 0 0 0 0	84 12 108	40	24	27		
	Span 11 NE & NI	1 2 3 4 5 6 7 8 9 9 0tal	0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0									1 2 3 4 5 6 7 7 8 9 9 Subtotal	0 0 0 0 0 0 0 0 0		0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0						1 2 3 4 5 6 7 8 9 9 Subtotal			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0							1 2 3 4 5 6 7 8 9 9 Subtotal	0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0		0 0 0 0 0 0 0 0 0						Span 11 NE & NI
	Span 11 SE & SI	1 2 3 4 5 6 7 8 0 tal pan 0 tal	0	0	0	0							1 2 3 4 5 6 7 8 8 Subtotal	0	0	0	0						1 2 3 4 5 6 7 7 8 Subtotal	0		0 0	0						1 2 3 4 5 6 7 8 Subtotal	0	0	0	0						Span 11 NE & NI

Vertical Face Deterioration: 3200 SF Total Estimated Lower Deck Floor Bottom Face Deterioration: 1138 SF Beam Deterioration: 4338 SF															•	Floor beam	replaced duri	ng 1995 reha ed average d	bilition eficiency																		
Span	Floor Beam No.	Surface	Surface Total	Area 1	Area 2	Area 3	н (in.)	W (in.)	No H (in.)	rth Bay W (in.)	Н (in.)	W (in.)	Floor Beam No.	Surface	Surface Total	Area 1	Area 2	Area 3	H (in.)	W (in.)	Center H (in.)	r Bay w (in.)	H (in.)	W (in.)	Floor Beam No.	Surface	Surface Total	Area 1	Area 2	Area 3	Н (in.)	W (in.)	Sout H (in.)	th Bay W (in.)	H (in.)	W (in.)	Span
Span 1	1 <sup>4</sup> 2 <sup>4</sup> 5 6 6 7 8 9 9 10 11 12 13	s s Subtot al Span Total	10 10 10 10 10 10 10 10 70 250		Vert. Total	167							1* 2* 3 4 5 5 6 7 7 8 9 10 11 11 12 2 13	* Subtot al	10 10 10 10 10 10 10 10 10 10 90										1* 2* 3 4 5 6 7 8 8 7 8 9* 10' 11 11 12 13	Subtot	10 10 10 10 10 10 10 10 10 10 10 10 90										Span 1
Span 2	1* 2* 3 4 5 6 7 7 8 9 0 10 11 12 13 3 14 15 16	Subtot al Span Total	10 10 10 10 10 10 10 10 10 10 10 10 10 1		Vert. Total	273							1 2 3 4 5 6 7 7 8 9 10 11 11 12 13 3 14 15 16	Subtot	10 10 10 10 10 10 10 10 10 10										1* 2* 3 6* 6* 7* 8 8 9 10 10 11 11 12 13 13 14 15 5 16	Subtot	10 10 10 10 10 10 10 10 10 10 10 10 10 1										Span 2

										Vertic	al Face	Deteri	ioration:	3200	SF										•	Floor beam r	eplaced duri	ng 1995 reha	abilition								
	Total Es	timated L	ower Dec	ck Floor						Botto	m Face	Deteri	ioration:	1138	SF										##	Green Quant	ity - Estimate	ed average d	eficiency								
	В	eam Dete	rioration	:	4338	SF																			##	Red quantiu	ty - Visually e	stimated dif	iciency								
	Floor	l I			r				Nor	h Bay			Floor	T		T	1	1	1		Cente	r Bay			Floor	1			r		1		South	n Bay			
Span	Beam	Surface	Surface	Area 1	Area 2	Area 3		w		w		w	Beam	Surface	Surface	Area 1	Area 2	Area 3		w	u	w			Beam	Surface	Surface	Area 1	Area 2	Area 3		w		w			Span
	No.		Iotai				(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	No.		Iotai				п (in.)	(in.)	п (in.)	(in.)	п (in.)	(in.)	No.		Iotai				(in.)	(in.)	(in.)	(in.)	(in.) (i	n.)	
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	1	Bottom	0	0	0	0					ļ		1	Bottom	0	0	0	0							1	Bottom	0	0	0	0							
		West	13	7	2	5	42	24	16	16	18	36		West	0	0	0	0								West	0	0	0	0				-			
	2	Bottom	13	13	0	0	78	24				1	2	Bottom	0	0	0	0		<u> </u>	1				2	Bottom	0	0	0	0							
		East	6	2	2	2	12	24	12	24	32	24		East	0	0	0	0								East	0	0	0	0						_	
	3	Bottom	Ő	0	0	0	~~			10			3	Bottom	0	0	0	ő		·					3	Bottom	0	ō	0	0 0							
		East	7	2	2	3	12	24	12	24	18	24		East	0	0	0	0								East	0	0	0	0							
	4	Bottom	7	7	0	0	42	24			+		4	Bottom	0	0	0	0							4	Bottom	0	0	0	0							
		East	0	0	0	0								East	0	0	0	0								East	0	0	0	0							
	5	West	0	0	0	0	36	8			+		5	West	0	0	0	0							5	West Bottom	0	0	0	0							
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		West	6	2	2	2	24	12	12	24	18	18		West	0	0	0	0	ļ							West	0	0	0	0							
		East	9	9	0	0	102	6		ļ	+		•	East	0	0	0	0	+	<u> </u>					0	East	0	0	0	0							
	_	West	1	1	0	0	12	17					_	West	0	0	0	0	L						_	West	0	0	0	0							
	7	Bottom	0	0	0	0	26	12	15	19	12	20	7	Bottom	0	0	0	0		<u> </u>					7	Bottom	0	0	0	0							
		West	1	1	0	0	12	12	15	10	12	50		West	0	0	0	0								West	0	0	0	0						_	
	8	Bottom	0	0	0	0					ļ		8	Bottom	0	0	0	0	ļ	ļ					8	Bottom	0	0	0	0							
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	9	Bottom	0	0	0	0					1		9	Bottom	0	0	0	0	İ						9	Bottom	0	0	0	0							
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~	10	Bottom	4	4	0	ů ů	24	24			1		10	Bottom	0	0	0	ŏ		<u> </u>					10	Bottom	0 0	0	0	ō							
a		East	2	2	0	0	12	24						East	0	0	0	0								East	0	0	0	0		ļ					an
Sp	11	Bottom	0	0	0	0	10	16			+		11	Bottom	0	0	0	0	+						11	Bottom	0	0	0	0							s
		East	0	0	0	0							1	East	0	0	0	0								East	0	0	0	0							
	12	Bottom	2	2	0	0	18	18			+		12	West Bottom	0	0	0	0	+						12	West Bottom	0	0	0	0							
		East	0	0	0	0								East	0	0	0	0								East	0	0	0	0							
	13	West	0	0	0	0	42	24					13	West	0	0	0	0							13	West	0	0	0	0							
		East	2	2	0	0	12	24			1		-	East	0	0	0	ů 0	1							East	0 0	0	0	ō							
		West	6	6	0	0	36	24						West	0	0	0	0								West	0	0	0	0							
	14	Bottom East	0	0	0	0					+		14	Bottom East	0	0	0	0	+						14	Bottom East	0	0	0	0							
		West	9	5	3	2	42	16	24	16	12	24		West	0	0	0	0	L							West	0	0	0	0							
	15	Bottom	0	0	0	0	12	12					15	Bottom	0	0	0	0					·		15	Bottom	0	0	0	0							
		West	5	5	Ő	0	28	28						West	Ő	0	0	0								West	0	Ő	Ő	Ő							
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		West	9	0	8	0	18	12	30	36				West	0	0	0	0								West	0	0	0	0							
	17	Bottom	0	0	0	0				1	1	ļ	17	Bottom	0	0	0	0	1	<u>.</u>					17	Bottom	0	0	0	0							
		East West	0	0	0	0	-	-	-					East	0	0	0	0								East West	0	0	0	0		-	-			_	
	18	Bottom	ō	ő	ō	Ő				<u> </u>	1	1	18	Bottom	o	0	o	ő	1	<u>†</u>					18	Bottom	ō	ō	o	Ő							
		East	0	0	0	0	_	-						East	0	0	0	0								East	0	0	0	0	1						
1		al	146		Vert. Total	105				1	1	1		al	0											al	0										
						1					1																										
		Span Total	146		Bot Total	42																															
			•																																		

		Vertical Bottom	Face I Face I	Deterio Deterio	oration: oration:	3200 1138	SF SF										• ##	Floor beam r Green Quant Red quantiut	replaced dur tity - Estimat ty - Visually	ing 1995 reh ed average c estimated di	abilition deficiency ficiency																
	Nort	h Bay			Floor		Curdona						Cente	r Bay			Floor		Surface						Sout	h Bay											
Span	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in)	W (in.)	H (in)	W (in)	H (in )	w (in)	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in)	W (in)	H (in)	W (in)	H (in)	W (in)	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in)	W (in )	H (in.)	W (in)	H (in)	W (in)	Span
		West	0	0	0	0	(,	(,	()	(,	(,	()		West	0	0	0	0	(,	()	(,	()	()	(,		West	0	0	0	0	()	()	()	(,	(,	()	
	1	Bottom East	0	0	0	0		······					1	Bottom East	0	0	0	0	-	+					1	Bottom East	0	0	0	0							r.
	2	West	0	0	0	0		·····					2	West	51 41	41	10	0	30 30	195 195	60	24			2	West	7	7	0	0	44 84	24 24					ı
		East	0	0	0	0		•••••						East	41	41	0	0	30	195						East	18	4	11	4	24	24	54	28	30	18	r.
	3	West Bottom	10	0	0	0		<b>.</b>					3	West Bottom	11 0	11 0	0	0	55	30					3	West Bottom	10	0	0	0							r.
		East West		0	0	0								East West	0	0	0	0	-	-						East West		0	0	0							r.
	4	Bottom	10	0	0	0		·····					4	Bottom	10	0	0	0	-	-					4	Bottom	10	0	0	0							r.
	-	West		0	0	0								West		0	0	0	1						_	West		0	0	0							ı
	5	Bottom East	10	0	0	0		·····•			<u> </u>		5	Bottom East	10	0	0	0	-						5	Bottom East	10	0	0	0							r.
	6	West Bottom	10	0	0	0							6	West Bottom	10	0	0	0							6	West Bottom	10	0	0	0							ı
		East		0	0	0								East		0	0	0								East		0	0	0							ı
	7	Bottom	10	0	0	0		······					7	Bottom	10	0	0	0	1						7	Bottom	10	0	0	0							ı
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	8	Bottom Fast	10	0	0	0					Ĭ		8	Bottom	10	0	0	0	-	1					8	Bottom	10	0	0	0							r.
n 5		West	10	0	0	0								West	10	0	0	0								West	10	0	0	0							115
Spa	9	East	10	0	0	0		·····					3	East	10	0	0	0							9	East	10	0	0	0							Spa
	10	West Bottom	10	0	0	0		······					10	West Bottom	10	0	0	0	-	+					10	West Bottom	10	0	0	0							r.
		East	•	0	0	0								East		0	0	0		-						East		0	0	0					—		r.
	11	Bottom	10	10	0	0	38	38					11	Bottom	10	0	0	0	1	1					11	Bottom	10	0	0	0							ı
		East West	0	0	0	0								East West		0	0	0								East West		0	0	0							n.
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	13	West	10	0	0	0							13	West	10	0	0	0							13	West	10	0	0	0							ı
		East		0	0	0							17	East		0	0	0								East		0	0	0							n.
	14	West Bottom	2	2	0	0	15	15					14	West Bottom	10	0	0	0	+						14	West Bottom	10	0	0	0							ı
		East West	0	0	0	0	24	30						East West	0	0	0	0								East West	0	0	0	0							ı
	15	Bottom	3	3	0	0	47	10	47	45	ļ		15	Bottom	0	0	0	0	1	1					15	Bottom	0	0	0	0	[						
		Subtot	137	-			12	24	47	43				Subtot	253		0									Subtot	160	0									ı
		al			vert. Iotal	3/2								al												al											
		Span Total	549		Bot Total	177																															i i

	Total Es B	timated L eam Dete			Vertica Bottor	al Face n Face	Deteri Deteri	oration: oration:	3200 1138	SF SF									• ##	Floor beam i Green Quan Red quantiu	replaced dur tity - Estimat ity - Visually (	ing 1995 reh ed average c estimated di	abilition leficiency ficiency													
Floor North													Floor		Surface						Center Ba	У		Floor		Eurface						Sout	h Bay			
Span         Beam         Surface         Surface         Area 1         Area 2         Area 3         H         W           No.         No.         (in.)         (in.)											H (in.)	W (in.)	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in.)	W (in.)	H W	н ) (in.	W ) (in.)	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in.)	w (in.)	H (in.)	W (in.)	H (in.)	W (in.)	Span
		West	10	10	0	0	24	60	()	(,	()	()		West	0	0	0	0	(,	()	(, (	., (	, (,		West	0	0	0	0	()	(,	()	()	(,	()	
	1	Bottom East	11 11	11 5	0	0 2	64 32	24 24	24	18	18	18	1	Bottom East	0	0	0	0							Bottom East	0	0	0	0							ı
	2	West Bottom	0	0	0	0							2	West Bottom	10	0	0	0						2	West Bottom	10	0	0	0							
		East West	0	0	0	0								East		0	0	0							East West		0	0	0							
	3	Bottom	0	0	0	0		-					3	Bottom	10	0	0	0	-	ļ			<u> </u>	3	Bottom	10	0	0	0							
		West	7	7	0	0	48	21						West	0	0	0	0							West		0	0	0		<u> </u>					
	4	Bottom East	0	0	0	0							4	Bottom East	0 12	0 12	0	0	36	48					Bottom East	10	0	0	0							ı
	5	West Bottom	0	0	0	0							5	West Bottom	1	1	0	0	2	72				5	West Bottom	10	0	0	0		·					
		East West	2	2	0	0	12 12	24 12						East West	0	0	0	0							East West		0	0	0					-+		
	6	Bottom	0	0	0	0						ļ	6	Bottom	10	0	0	0	-	<u>.</u>			<u> </u>	6	Bottom	10	0	0	0							
	7	West	10	0	0	0							7	West	10	0	0	0							West	10	0	0	0							
		East		0	0	0							,	East		0	0	0							East		0	0	0							
	8	West Bottom	2	2 0	0	0	12	24					8	West Bottom	10	0	0	0	-						West Bottom	10	0	0	0							
و		East West	2	2	0	0	12	24						East West		0	0	0					-		East West	0	0	0	0							9
Span	9	Bottom East	8	8 0	0	0	45	24					9	Bottom East	10	0	0	0						9	Bottom East	0 6	0 6	0	0	29	29					Span
	10	West	7	7	0	0	48	20					10	West	10	0	0	0						10	West	0	0	0	0							
		East	0	0	0	0								East		0	0	0							East	6	6	0	0	29	29					
	11	West Bottom	0 51	0 51	0	0	24	303					11	West Bottom	10	0	0	0	-					11	West Bottom	10	0	0	0							
		East West	0	0	0	0								East West		0	0	0							East West		0	0	0							
	12	Bottom East	10	0	0	0							12	Bottom East	10	0	0	0							Bottom East	10	0	0	0							
	13	West Bottom	10	0	0	0							13	West Bottom	10	0	0	0						13	West Bottom	10	0	0	0		ļ					
		East	0	0	0	0								East	0	0	0	0							East		0	0	0							
	14	Bottom	0	0	0	0							14	Bottom	0	0	0	0		~ .				14	Bottom	51	51	0	0	24	303					
		West	5	5	4	0	30	<u>32</u> 6	24	24				East West	0	0	0	0	30	24					East West	25	25	0	0	12	303					
	15	Bottom East	20 17	20 5	0	0	122 122	24 6	42	42			15	Bottom East	0	0	0	0						15	Bottom East	51 25	51 25	0	0	24 12	303 303					
		Subtot al	199		Vert. Total	308								Subtot al	118										Subtot al	264										ı.
		Span Total	580		Bot Total	272																														1

Total Estimated Lower Deck Floor Beam Deterioration: 4338 SF											al Face m Face	Deteri Deteri	ioration: ioration:	3200 1138	SF SF										• ##	Floor beam r Green Quant Red quantiut	replaced duri tity - Estimate ty - Visually e	ng 1995 reho ed average d estimated dif	abilition leficiency liciency								
	th Bay			Floor		Surface						Cente	r Bay			Floor		Eurface						Sou	uth Bay												
Span	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in.)	W (in.)	H (in.)	W (in.)	H (in.)	W (in.)	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in.)	W (in.)	H (in.)	W (in.)	H (in.)	W (in.)	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in.)	W (in.)	H (in.)	W (in.)	H (in.)	W (in.)	Span
	1	West Bottom	32 0	8 0	19 0	4	48	24	32	87	30	21	1	West Bottom	0 0	0 0	0	0 0							1	West Bottom	22 3	16 3	6 0	0 0	60 48	38 8	36	24			
	2	East West Bottom	4 2 0	4 2 0	0 0	0 0	24 18	24 15					2	East West Bottom	0	0 0	0 0	0		<u> </u>					2	East West Bottom	13 32 0	3 32 0	10 0 0	0 0	48 133	8 35	45	32			I
		East West	2 28	2	0 21	0	24 36	10 30	68	44				East West		0	0	0								East West	0	0	0	0							ı
	3	Bottom East West	0 0 24	0 0 24	0	0 0 0	34	102					3	East West	10	0 0 0	0	0							3	Bottom East West	10	0	0	0 0 0		<u> </u>					ı
	4	Bottom East	21 0	21 0	0	0	24	128					4	Bottom East	10	0	0	0	20	40					4	Bottom East	10	0	0	0							ı
	5	Bottom East	6 1 0	6 1 0	0	0	12	12					5	Bottom East	4	4	0	0	12	40 48					5	Bottom East	10	0	0	0							ı
	6	West Bottom East	0	0 0	0	0						-	6	West Bottom East	10	0	0	0							6	West Bottom East	10	0 0	0	0 0							ı
	7	West Bottom	16 0	16 0	0	0	24	96					7	West Bottom	10	0	0	0							7	West Bottom	20 0	20 0	0	0	54	54					ı
	8	West Bottom	6 30	6 30	0	0	12 24	72 180					8	West Bottom	10	0	0	0							8	West Bottom	10	0	0	0							ı
an 7	9	East West Bottom	0 0 51	0 0 51	0	0 0	24	303					9	East West Bottom	10	0	0	0							9	East West Bottom	10	0	0	0							an 7
Sp	10	East West Bottom	4 8	4 5 3	0 3	0	24 48	24 16 8	12	36			10	East West Bottom	0	0	0	0		<u> </u>					10	East West Bottom	10	0	0	0		<u> </u>					ds
	10	East West	0	0	0	0	40	0						East West	6 0	6 0	0	0	22	38					10	East West	10	0	0	0		<u> </u>					ı
	11	Bottom East West	10	0 0	0 0	0 0							11	Bottom East West	0 0 33	0 0 4	0 0 17	0 0 12	24	22	75	32	56	32	11	Bottom East West	10	0 0	0 0	0 0		<u> </u>					ı
	12	Bottom East Wort	10	0	0	0							12	Bottom East Wort	1 3	1 3	0	0	30 30	6 12 24	12	24			12	Bottom East Wort	10	0	0	0							ı
	13	Bottom East	10	0	0	0							13	Bottom East	0 0	0	0	0	12	24		24			13	Bottom East	10	0	0	0							ı
	14	West Bottom East	10	0	0 0 0	0 0 0							14	West Bottom East	10	0	0 0 0	0 0 0							14	West Bottom East	10	0 0 0	0	0 0 0							ı
	15	West Bottom East	0 0 43	0 0 20	0 0 5	0 0 18	36	80	21	34	44	60	15	West Bottom East	0 0 0	0 0 0	0 0 0	0 0 0							15	West Bottom East	0 12 0	0 12 0	0 0 0	0 0 0	42	42					I
		Subtot al	321		Vert. Total	472								Subtot al	142											Subtot	211			-							I
		Span Total	675		Bot Total	203																															I

										Vertice	al Face	Deteri	ioration:	3200	SF										•	Floor beam	replaced duri	ng 1995 reh	abilition								
Total Estimated Lower Deck Floor										Bottor	n Face	Deteri	ioration:	1138	SF										##	Green Quan	tity - Estimate	ed average d	leficiency								
	В	eam Dete	rioration	1:	4338	SF																				Red quantiu	tv - Visuallv e	stimated dif	ficiency								
	-					•																															
	Floor								Nor	th Bay			Floor								Cente	r Bay			Floor								Sr	outh Bay			
Span	Beam	Surface	Surface	Area 1	Area 2	Area 3			1	1	1		Beam	Surface	Surface	Area 1	Area 2	Area 3			I I		1		Beam	Surface	Surface	Area 1	Area 2	Area 3					1		Span
	Span Beam Surface Total Area 1 Area 2 Area 3 H W H											(in)	No.		Total				H (in)	(in)	H (in)	(in)	(in)	(in)	No.		Total				(in)	(in	) (in	(in)	(in)	(in)	
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	1	Bottom	4	4	0	0	6	90					1	Bottom	0	0	0	0							1	Bottom	7	7	0	0	84	12					
		East	0	0	0	0					1			East	0	0	0	0	1		1	•••••	·····†·			East	0	0	0	0						-	
		West	2	2	0	0	48	7						West	0	0	0	0								West	20	20	0	0	48	60	-				-
	2	Bottom	5	5	0	0	48	16					2	Bottom	0	0	0	0							2	Bottom	5	5	0	0	12	60					
		East	0	0	0	0		40						East	0	0	0	0								East	0	0	0	0	_		_	_			-
	3	Rottom	1/	4	14	0	44	12	54	36			3	West	0	0	0	0	+			·····			3	Rottom	0	0	0	0							
	-	East	0	0	0	0		-			1		-	East	0	0	0	0	+							East	0	0	0	0		-			-		
		West	0	0	0	0								West	0	0	0	0								West	0	0	0	0		-				-	-
	4	Bottom	0	0	0	0					[		4	Bottom	0	0	0	0	1		l l				4	Bottom	0	0	0	0							
		East	0	0	0	0				_				East	0	0	0	0								East	0	0	0	0							_
		West	0	0	0	0								West	0	0	0	0					·····			West	0	0	0	0							
	2	Fast	0	0	0	0		-						Bottom	0	0	0	0	+							Bottom	0	0	0	0							
		West	0	ő	ů ů	ů ů		-		1				West	0	0	0	ů ů					-			West	ů ů	ů ů	ő	ů ů		+					-
	6	Bottom	0	0	0	0		-			1		6	Bottom	0	0	0	0	1			•••••			6	Bottom	0	0	0	0		-			-		
		East	0	0	0	0								East	0	0	0	0	Ī							East	0	0	0	0							
		West	3	3	0	0	30	12						West	0	0	0	0							-	West	0	0	0	0							
	'	Bottom	0	0	0	0		-						Bottom	0	0	0	0	+						'	Bottom	0	0	0	0							
		EdSt	0	0	0	0	-	+		+				EdSL	0	0	0	0	-							EdSt	0	0	0	0							-
	8	Bottom	0	ŏ	0	õ		-					8	Bottom	0	0	ō	ů 0	-						8	Bottom	0	ő	ō	0							
		East	8	8	0	0	48	24						East	2	2	0	0	24	12		•				East	0	0	0	0							
38		West	39	39	0	0	116	48						West	7	7	0	0	44	24						West	0	0	0	0							18
bai	9	Bottom	0	0	0	0							9	Bottom	0	0	0	0					Ļ.		9	Bottom	0	0	0	0							ba
s		East	0	0	0	0	_	_	_					East	0	0	0	0	_							East	0	0	0	0	-	<u> </u>		_	_		~ ~
	10	Bottom	0	0	0	0							10	Bottom	0	0	0	0					·····		10	Bottom	0	0	0	0							
		East	0	0	0	0		-			1			East	0	0	0	0	1			•••••	t in the second se			East	0	0	0	0		-			-		
		West	0	0	0	0								West	0	0	0	0	1							West	0	0	0	0							_
	11	Bottom	0	0	0	0							11	Bottom	0	0	0	0					Ļ.		11	Bottom	0	0	0	0						ļ	
		East	0	0	0	0		-		_				East	0	0	0	0								East	0	0	0	0							-
	12	Bottom	1	1	0	0	24	ь					12	Bottom	0	0	0	0	+						12	Bottom	0	0	0	0							
		East	0	ŏ	ő	ő					•			East	0	0	ő	ő	+		<del>-</del>	•••••	·····			East	0	ŏ	ŏ	0							
		West	8	8	0	0	38	30						West	0	0	0	0			1		1			West	0	0	0	0		1	-				-
	13	Bottom	0	0	0	0							13	Bottom	0	0	0	0	I						13	Bottom	0	0	0	0							
		East	0	0	0	0								East	0	0	0	0								East	0	0	0	0							_
	14	West	10	10	0	0	36	39					14	West	0	0	0	0							14	West	16	16	0	0	43	54					
	14	Fast	0	0	0	0		-					14	Bottom	0	0	0	0	+						14	Bottom	0	3	0	0	36	12					
		West	1	1	0	0	12	6						West	0	0	0	0								West	28	23	5	0	44	74	21	34			-
1	15	Bottom	2	2	0	0	36	6			1		15	Bottom	0	0	0	0	1				t		15	Bottom	5	5	0	0	30	24					
		East	0	0	0	0								East	0	0	0	0								East	8	8	0	0	48	24					
1		Subtot	102		Ver. 7									Subtot	9	1			1							Subtot	95			1	1						1
1		aı		1	vert. rota	176	1							aı		1	1		1				1			aı		1	1		1				1		1
			207											1																							
		Span Total			Bot Total	31	1												1												1						
										Vertic	cal Face	Deteri	ioration:	3200	SF										•	Floor beam	replaced duri	ng 1995 reha	bilition								
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	Total Es	timated L	ower De	ck Floor						Botto	om Face	Deteri	ioration:	1138	SF										**	Green Quant	tity - Estimat	ed average d	eficiency								
	В	eam Dete	rioration	:	4338	SF																			##	Red quantiu	ty - Visually e	stimated dif	iciency								
		r 1		r	<u> </u>	1	1							1		1	1	r –	r –			-				1	r –	r		-	r –						<del></del>
<b>C</b>	Floor	6 . f	Surface						Nor	th Bay			Floor		Surface						Cent	er Bay			Floor	c	Surface						Sou	ith Bay			
Span	Beam	Surrace	Total	Area 1	Area 2	Area 3	н	w	н	w	н	w	Beam	Surface	Total	Area 1	Area 2	Area 3	н	w	н	w	н	w	Beam	Surface	Total	Area 1	Area 2	Area 3	н	w	н	w	н	w	Span
	NO.						(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	NO.						(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	NO.						(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	<u> </u>
	1	West	4	4	0	0	24	24					1	West	47	29	18	0	94	44	59	44			1	West	22	19	3	0	72	38	12	36			4
	-	East	5	5	ő	0	28	24			-	+	-	East	10	8	3	ő	36	30	69	6		-	-	East	26	5	18	3	24	30	58	44	18	24	1
		West	18	1	2	15	12	12	18	18	180	12		West	2	1	1	0	24	6	12	6				West	7	5	2	0	27	28	15	15	-		
	2	Bottom	6	6	0	0	72	12				1	2	Bottom	3	2	1	0	24	12	12	12		1	2	Bottom	1	1	0	0	15	12					
		East	0	0	0	0	10	6						East	2	2	0	0	24	12						East	0	0	0	0							1
	2	West	11	2	4	6	18	18	20	26	15	*****		West	2	2	0	0	24	12		ļ		Ļ	,	West	2	2	0	0	42	6				ļļ	1
	3	Fact	14	5	4	5	36	18	24	24	12	60		Bottom Fast	5	4	1	0	18	30	12	12		-		Fast	3	3	0	0	42	9			ļ	ļ	
		West	24	24	0	0	72	48	24	24	12	00		West	26	2	22	3	15	15	134	24	12	30		West	5	5	0	0	36	18					1
	4	Bottom	0	0	0	0			-			1	4	Bottom	3	3	0	0	60	6		•			4	Bottom	0	0	0	0					1		
		East	5	3	2	0	24	18	24	12				East	6	2	3	2	15	15	60	6	14	21		East	0	0	0	0							
		West	12	3	1	8	16	24	12	17	12	95	_	West	0	0	0	0							_	West	9	3	4	2	80	6	24	24	15	15	
	5	Bottom	0	0	0	0						+	5	Bottom	0	0	0	0	+					<u> </u>	5	Bottom	3	3	0	0	80	6			ļ	ļ	
		EdSL	0	0	0	0								EdSL	2	2	0	0	15	15						EdSt	2	2	0	0	15	15					
	6	Bottom	0	ő	ő	ő						+	6	Bottom	0	0	o o	ő				<u> </u>		<u>+</u>	6	Bottom	0	ő	0	ő							
		East	4	2	2	0	16	16	12	24		1		East	0	0	0	0	1	1		1		t		East	0	0	0	0		1			1		
		West	3	2	1	0	24	12	12	12				West	2	2	0	0	16	18						West	1	1	0	0	12	12					
	7	Bottom	7	6	1	0	92	10	12	12		Ļ	7	Bottom	0	0	0	0				ļ		Ļ	7	Bottom	0	0	0	0					ļ	Ļ	
•		East	3	1	2	0	12	12	28	12				East	0	0	0	0	10							East	6	1	2	3	12	12	15	18	12	36	
u.	8	Bottom	20	20	0	0	64	46			-	+	8	Bottom	2	2	0	0	12	24					8	Bottom	3	3	0	0	21	21			ļ	ļ	
Spc		East	ů 0	ő	0 0	ŏ						+		East	. ŭ	ō	0	o o	+	+		†		<u>†</u>		East	0	ő	ő	0							Spc
		West	0	0	0	0						1		West	0	0	0	0								West	4	2	2	0	18	12	12	24			
	9	Bottom	0	0	0	0						1	9	Bottom	0	0	0	0	1	1		1		<u> </u>	9	Bottom	0	0	0	0	1				1	I	1
		East	0	0	0	0		_						East	0	0	0	0								East	0	0	0	0						L'	1
	10	West	0	0	0	0						ļ	10	West	5	5	0	0	6	108				<u> </u>	10	West	2	2	0	0	16	16			ļ	ļ	
	10	Fort	0	0	0	0						+	10	Fort	· /	, ,	0	0	9	100		ł		<u> </u>	10	Fort	0	0	0	0						ļ	
		West	0	0	0	0		_			-			West	4	4	0	0	94	6						West	12	6	4	2	24	36	12	44	18	18	
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		West	0	0	0	0								West	0	0	0	0	1							West	11	7	4	0	42	24	24	24			1
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	12	West	0	0	0	0	24					+	12	West	0	0	0	0	+						12	West	38	24	14	0	80	43	42	48		ł	
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										Vertice	al Face	Deteri	ioration:	3200	SF										•	Floor beam r	eplaced duri	ng 1995 reh	abilition								
	Total Es	timated L	ower De	ck Floor						Bottor	n Face	Deteri	ioration:	1138	SF										##	Green Quant	ity - Estimat	ed average o	deficiency								
	В	eam Dete	rioratio	ı:	4338	SF																			##	Red quantiu	ty - Visually e	stimated di	ficiency								
	Floor		Surface						Nort	h Bay			Floor		Surface						Cente	er Bay			Floor		Surface						Sout	h Bay			
Span	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in)	W (in)	H (in)	W (in)	H (in)	W (in)	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in)	W (in)	H (in)	W (in)	H (in)	W (in)	Beam No.	Surface	Total	Area 1	Area 2	Area 3	H (in)	W (in)	H (in)	W (in)	H (in )	w	Span
		Wort	E	2	2	•	24	16	29	14	()	()		Wort	12	٩	2	0	20	(11.)	26	12	()	()		Wort	٥	0	0	0	26	26	()	()	()	()	
	1	Bottom	2	2	0	0	24	8	20	14			1	Bottom	12	0	0	0	50	42	30	12	·		1	Bottom	9 17	9 17	0	0	102	24					
		East	4	1	3	0	12	15	12	30	1	1		East	3	2	1	0	15	15	12	12	·	t	-	East	20	20	0	0	53	53					
		West	2	1	1	0	12	17	12	12				West	7	2	4	1	15	15	24	24	12	12		West	2	2	0	0	10	32					
	2	Bottom	0	0	0	0	1	1			1	1	2	Bottom	0	0	0	0	1	1		1		Ť	2	Bottom	0	0	0	0							
		East	0	0	0	0							]	East	0	0	0	0								East	5	5	0	0	15	48					
		West	4	4	0	0	18	30			ļ			West	1	1	0	0	12	12				L		West	4	4	0	0	24	24		ļļ			
	3	Bottom	0	0	0	0					ļ	Ļ	3	Bottom	0	0	0	0				ļ		Ļ	3	Bottom	0	0	0	0				ļ			
		East	0	0	0	0								East	0	0	0	0					10			East	2	2	0	0	16	16		⊨+			
	4	west	0	0	0	0					<b> </b>		4	West	10	4	4		24	24	20	32	12	24		west	1/	1/	0	0	44	55					
	-	Fact	0	0	0	0								Fast	0	0	0	0	+				·	+		Fact	1	1	0	0	10	16		-			
		West	0	0	0	ő		1						West	ő	0	0	ő		1						West	0	Ô	0	0		10					
	5	Bottom	0	0	0	0					1	÷	5	Bottom	0	0	0	0	+				·		5	Bottom	0	0	0	0							
		East	0	0	0	0					1		1	East	4	4	0	0	32	16				Ī	-	East	6	6	0	0	16	52					
		West	0	0	0	0								West	8	8	0	0	35	35						West	10	10	0	0	24	58					
	6	Bottom	0	0	0	0					1		6	Bottom	9	9	0	0	53	24				I	6	Bottom	0	0	0	0							
		East	0	0	0	0								East	14	12	2	0	30	58	24	12				East	18	18	0	0	44	60					
	_	West	0	0	0	0					ļ	ļ	_	West	22	15	3	4	36	60	10	48	32	18	_	West	46	9	37	0	44	30	44	120			
10	7	Bottom	0	0	0	0					ļ	Ļ	7	Bottom	13	13	0	0	80	24		ļ		Ļ	7	Bottom	0	0	0	0				ļ			10
5		East	0	0	0	0								East	33	7	26	0	30	34	44	84				East	12	12	0	0	44	38		⊢			5
Ş,	8	west	26	20	ь	0	44	65	32	27	<b> </b>			West	3	3			26	18						west	· · · ·	· .	0	0	44	24					2 Z
	Ű	East	4	4	0	0	24	24			l	+	Ŭ	East	• •	0	4	0	24	24	24	24		<u> </u>	Ŭ	East	0	0	0	0							-
		West	0	0	0	0		-				-		West	11	11	0	0	44	35	24	24				West	29	29	0	0	44	96					
	9	Bottom	0	0	0	ů ů					<u> </u>		9	Bottom	0	0	0	0							9	Bottom	0	0	0	0		50					
	-	East	0	0	0	0					1			East	7	4	3	0	44	12	30	16	·•····	1	-	East	70	22	26	22	44	72	86	44	56	56	
		West	8	3	5	0	36	12	24	30				West	26	26	0	0	85	44						West	47	16	1	31	62	36	18	9 1	.00 4	44	
	10	Bottom	16	16	0	0	96	24			1		10	Bottom	0	0	0	0	T					Ī	10	Bottom	0	0	0	0							
		East	0	0	0	0							]	East	11	2	6	3	12	24	34	24	24	20		East	0	0	0	0							
		West	0	0	0	0					<u> </u>			West	2	2	0	0	15	15				L		West	0	0	0	0							
	11	Bottom	10	10	0	0	58	24			ļ	ļ	11	Bottom	0	0	0	0						L	11	Bottom	0	0	0	0							
		East	0	0	0	0		-						East	6	3	3	0	36	12	36	12				East	2	2	0	0	10	32		$ \longrightarrow $			
		West	0	0	0	0					ļ			West	0	0	0	0				ļ		ļ		West	39	21	18	0	36	84	38	70			
	12	Bottom	26	26	0	0	24	158					12	Bottom	0	0	0	0						<u> </u>	- 12	Bottom	9	9	0	0	53	24		-			
		Subtot	U	U	U	U								Subtot	20	20	U	U	44	90						Subtot	2	2	U	U	24	12					
		al	107		Vert. Total	612								al	237						]					al	376										
		Span Total	719		Bot Total	107																															

Tot	al Esti	mated I a	wer Der	k Floor						Bottor	m Face	Deterio	oration:	1138	SF											Green Quant	ity - Estimate	d average d	leficiency								
	Re	nm Deter	ioration		4338	SE																				Red augustiut	Vicually o	etimotod dil	Fictoria								
	Dei	in Delei	ioration	•	4330	Jr Jr																				Red quantitut	ty - visually e	stimated di	liciency								
EL	oor								Nort	th Bay		1	Floor								Conto	r Bav			Floor					1			South	Ray			
Span Be	aam	Surface	Surface	Area 1	Area 2	Area 3			1	in Day	1 .		Ream	Surface	Surface	Area 1	Area 2	Area 3			center	Day			Ream	Surface	Surface	Area 1	Area 2	Area 3			5000	i Day			Snan
Span De	No	Junace	Total	AICU I	Alcur	Alcus	н	w	н	w	н.	w	No	Junace	Total	Alcui	Alcuz	Alcus	н	w	н	w	H (I)	w	No	Junace	Total	AICU I	Alcur	Aicu 5	н	w	н	w	H V	w	pan
	•0.						(in.)	(in.)	(in.)	(in.)	(in.)	(in.)							(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	140.						(in.)	(in.)	(in.)	(in.) (	in.) (ir	in.)	
		West	0	0	0	0								West	0	0	0	0								West	0	0	0	0							
	±	Bottom	0	0	0	0					++		1	Bottom	0	0	0	0							1	Bottom	0	0	0	0							
		West	8	8	0	0	48	24						West	0	0	0	0								West	0	0	0	0							
	2	Bottom	0	0	0	0					1	••••••	2	Bottom	0	0	0	0							2	Bottom	0	0	0	0	-						
		East	0	0	0	0				1	1			East	0	0	0	0			1		1			East	0	0	0	0							
		West	26	16	10	0	48	48	12	120				West	0	0	0	0								West	0	0	0	0							
	3	Bottom	0	0	0	0							3	Bottom	0	0	0	0							3	Bottom	0	0	0	0							
		East	0	0	0	0		_						East	0	0	0	0								East	0	0	0	0							
		West	8	8	0	0	48	24						West	0	0	0	0							4	West	0	0	0	0							
	•	Bottom	0	0	0	0							-	Bottom	0	0	0	0					·····+			Bottom	0	0	0	0							
		West	0	0	0	0		-						West	0	0	0	0								West	0	0	0	0							
	5	Bottom	0	0	0	0		•			1		5	Bottom	0	0	0	0							5	Bottom	0	0	0	0							
		East	0	0	0	0				1	Ī			East	0	0	0	0	İ		Ī		1			East	0	0	0	0							
		West	0	0	0	0								West	0	0	0	0								West	0	0	0	0							
	6	Bottom	0	0	0	0							6	Bottom	0	0	0	0							6	Bottom	0	0	0	0							
		East	0	0	0	0		1						East	0	0	0	0								East	0	0	0	0							-
7	7	West	7	4	4	0	42	12	42	12			7	West	0	0	0	0							7	West	0	0	0	0							
au	· -	Fast	0	0	0	0					-			Fast	0	0	0	0							,	Fast	0	0	0	0	-						Jan
15		West	4	4	ů ů	0	42	12		1				West	0	0	ů ů	ů ů								West	0	ů ů	ő	0							s
	8	Bottom	0	0	0	0					1		8	Bottom	0	0	0	0	1						8	Bottom	0	0	0	0							
		East	4	4	0	0	42	12			Ī			East	0	0	0	0	İ		1		1			East	0	0	0	0							
		West	0	0	0	0								West	0	0	0	0								West	0	0	0	0							
	9	Bottom	0	0	0	0					ļļ		9	Bottom	0	0	0	0							9	Bottom	0	0	0	0							
		East	0	0	0	0								East	0	0	0	0								East	0	0	0	0							
	10	Rottom	0	0	0	0							10	West	0	0	0	0							10	Rottom	0	0	0	0							
		Fact	0	0	0	0					+			Fact	0	0	0	0								Fact	0	0	0	0							
		West	0	0	0	0								West	0	0	0	0								West	0	0	0	0							
	11	Bottom	0	0	0	0				1	1 T		11	Bottom	0	0	0	0	1		1				11	Bottom	0	0	0	0					1		
	Ë	East	0	0	0	0								East	0	0	0	0	Ι							East	0	0	0	0							
		Subtot	56											Subtot	0											Subtot	0										
		al			vert. Total	56	1		1	1				al	-	1	1	1								al	-			1	1				1		
						1	1		1	1						1	1	1												1	1						
		nan Total	56		Rot Total																																
		i oldi			bot Total	0				1																											

										Vertico	al Face	Deteri	oration:	3200	SF										•	Floor beam	replaced duri	ing 1995 reh	abilition								
	Total Es	timated L	ower De	ck Floor						Botton	n Face	Deteri	oration:	1138	SF										##	Green Quant	tity - Estimat	ed average d	eficiency								
	В	eam Dete	rioration	n:	4338	SF																			##	Red quantiu	ty - Visually e	estimated dif	iciency								
	Floor					1			Nort	h Bay			Floor			1					Cent	er Bay			Floor			1					So	uth Bay			Т
Span	Beam	Surface	Surface Total	Area 1	Area 2	Area 3	н	w	н	w	н	w	Beam	Surface	Surface Total	Area 1	Area 2	Area 3	н	w	н	w	н	w	Beam	Surface	Surface Total	Area 1	Area 2	Area 3	н	w	н	w	н	w	Span
	NO.						(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	NO.						(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	NO.						(in.)	(in.)	(in.)	(in.)	(in.)	(in.)	
	1	West Bottom	0	0	0	0							1	West Bottom	0	0	0	0							1	West	0	0	0	0							
		East	0	0	0	0						1		East	0	0	0	0	1			1		1		East	0	0	0	0					-	1	-
		West	0	0	0	0								West	17	17	0	0	40	60						West	0	0	0	0					_		.]
	2	Bottom	0	0	0	0						ļ	2	Bottom	5	5	0	0	12	60				Ļ	2	Bottom	0	0	0	0							
		East	0	0	0	0	12	12						East	17	17	0	0	40	60 12						East	0	0	0	0		—	_				-
	3	Bottom	ō	ō	0	ů ů						1	3	Bottom	2	2	0	ŏ	12	24		1		÷	3	Bottom	0	ō	0	ů 0					-		
		East	0	0	0	0								East	3	3	0	0	40	12						East	0	0	0	0							
		West	0	0	0	0								West	9	4	1	3	32	20	12	17	26	15		West	16	3	14	0	26	15	26	75			.]
	4	Bottom	0	0	0	0					<u>.</u>	ļ	4	Bottom	0	0	0	0						Ļ	4	Bottom	0	0	0	0							
		East	0	0	0	0								East	0	0	0	0	1	-						East	6	6	0	0	16	50	<u> </u>			+	-
	5	Bottom	0	ŏ	0	ů ů							5	Bottom	ō	0	0	ŏ	+			•			5	Bottom	0	0	0	ů 0		50			-		
		East	0	0	0	0			•					East	4	2	2	0	26	9	18	18		İ		East	9	5	4	0	9	72	32	18			
		West	0	0	0	0						<u> </u>		West	0	0	0	0	1					Ļ		West	0	0	0	0	ļ						
	6	Bottom	0	0	0	0					<u>.</u>	ļ	6	Bottom	1	1	0	0	12	12				Ļ	6	Bottom	0	0	0	0							
		East	16	16	0	0	32	188						East	2	2	0	0	24	12						East	0	0	0	0		<u> </u>	<u> </u>	——		+	-
	7	Bottom	0	0	0	ů ů		100					7	Bottom	0	0	0	ŏ				•			7	Bottom	0	0	0	ů 0					-		
		East	37	18	4	15	30	87	27	22	26	82		East	4	4	0	0	30	20		1				East	0	0	0	0			-				
12		West	0	0	0	0						ļ		West	16	4	2	10	32	20	20	12	38	38		West	0	0	0	0	ļ						12
a	8	Bottom	0	0	0	0						ļ	8	Bottom	0	0	0	0		-		. <b>ļ</b>		Ļ	8	Bottom	0	0	0	0		ļ					
s,		East	4	4	0	0	24	24						East	10	10	0	0	24	35						East	13	3	0	9	9	48	10	12	40	34	- s
	9	Bottom	0	0	0	ů ů							9	Bottom	o	0	0	ŏ				•			9	Bottom	0	ō	ō	ō							
		East	4	4	0	0	24	24				1		East	3	3	0	0	24	18		1		†		East	7	7	0	0	40	26					
		West	1	1	0	0	12	12						West	0	0	0	0	1							West	3	1	2	0	12	12	12	24			.]
	10	Bottom	0	0	0	0						Ļ	10	Bottom	0	0	0	0				.ļ		Ļ	10	Bottom	0	0	0	0		ļ					
		East	0	0	0	0	40	72						East	0	0	0	0		_						East	0	0	0	0		<u> </u>	<u> </u>	——		<u> </u>	-
	11	Bottom	20	20	0	0	40	72				ł	11	Bottom	0	0	0	0	+			+		ł	11	Bottom	0	0	0	0							
		East	20	20	0	0	40	72				†		East	0	0	0	0	1	1		1		†		East	0	0	0	0					-	-	-
1		West	0	0	0	0								West	0	0	0	0								West	0	0	0	0						1	]
1	12	Bottom	0	0	0	0		ļ		ļ	ļ	ļ	12	Bottom	0	0	0	0	<b> </b>	.ļ		ļ		Ļ	12	Bottom	0	0	0	0		ļ		ļ		ļ	
		East	0	0	0	0			1	-				East	0	0	0	0		-	_					East	0	0	0	0		<u> </u>	+-			+	-
	13	Bottom	0	0	0	0							13	Bottom	0	0	0	0	+						13	Bottom	0	0	0	0							
		East	0	0	0	0								East	0	0	0	0	1	1		1				East	0	0	0	0					-	1	-
		Subtot	114											Subtot	100											Subtot	54									1	1
		al			Vert. Total	254								al	100											al											
		Span Total	268		Bot Total	14																															

## CUY-6-1456 Pier Patching Quantities

	Total	N. Exterior	S. Exterior		E. F	ace			W. F	ace	
Pier	(SF)	Shaft	Shaft	North Bay	Center Bay	South Bay	Subtotal	North Bay	Center Bay	South Bay	Subtotal
Pier 1	0						0				0
Pier 2	0						0				0
Pier 3	26		13				0	13			13
Pier 4	49		49				0				0
Pier 5	180		138				0	36		6	42
Pier 6	166		139			23	23	4			4
Pier 7	275		28				0			246	246
Pier 8	312	14	166				0			132	132
Pier 9	101	15	69			17	17				0
Pier 10	18		18				0				0
Pier 11	0						0				0
Pier 12	0						0				0
Pier 13	0						0				0

Total 1,127 SF

## CUY-6-1456

## Wearing Surface Survey

Span	Concrete R	Repairs (SF)	WB Area	EB Area of Deck	Con	crete Repair	(%)
opun	WB	EB	(SF)	(SF)	WB	EB	Total
Span 1A	36	128	2890	2890	1.2	4.4	2.8
Span 1B	81	162	3607	3607	2.2	4.5	3.4
Span 1	450	627	3718	3718	12.1	16.9	14.5
Span 2	0	0	4685	4685	0.0	0.0	0.0
Span 3	56	59	6368	6368	0.9	0.9	0.9
Span 4	1495	2441	17228	17228	8.7	14.2	11.4
Span 5	0	19	5186	5186	0.0	0.4	0.2
Span 6	259	8	4191	4191	6.2	0.2	3.2
Span 7	1367	664	4117	4117	33.2	16.1	24.7
Span 8	1724	1792	4170	4170	41.3	43.0	42.2
Span 9	814	354	3698	3698	22.0	9.6	15.8
Span 10	642	754	3688	3688	17.4	20.4	18.9
Span 11	76	360	2864	2864	2.7	12.6	7.6
Span 12	108	229	3444	6642	3.1	3.4	3.3
Span 13	28	0	2245	4331	1.2	0.0	0.4
East Station	44	0	8904	17172	0.5	0.0	0.2

Direction Subtotals:	7,180	7,597	81,003	94,555
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Total: 14,777 SF

Total % Deteriorated = 8.42%

## APPENDIX E

ESTIMATED FRP WRAP QUANTITIES



CUY-6-1456 over Cuyahoga River Rehabilitation Feasibility Study Ohio Department of Transportation

#### CUY-6-1456 Arch Rib Estimated FRP Wrap Quantities

Side Wrap Ht.

Future Spall Ht.	1.00	Ft.

FRP Development 1.50 Ft.

2.50 Ft.

Alt. 1 Total =

Rough Form Length Factor: 50% Form board length

		0 metr	Exterio	or Arch Ribs	Interio	r Arch Ribs	FRP Altern	Wrap - ate No. 1		FRP Wrap - Alternate No	. 2	FRP V Alterna	Vrap - te No. 3		
Span	Intrados Length (ft)	Arch Side Surface Area (ft <sup>2</sup> )	No. of Ribs	Arch Rib Width (ft.)	No. of Ribs	Arch Rib Width (ft.)	Side Wrap Height (ft.)	Wrap Area (ft <sup>2</sup> )	Top Corners - Horiz Width (ft.) *	Top Corners - Side Height (ft.)	Wrap Area (ft <sup>2</sup> )	Full Side Wrap Height (ft.) *	Wrap Area (ft <sup>2</sup> )	Estmated Board Form Length (ft.)	Estimated Rough Form Length (ft.)
1	138.9	744.4	0	6.75		9.00								0	0
2	180.0	1061.0	1.5	6.75	1.5	9.00	2.50	6952.5	1.50	2.50	7672.5	7986.0	12238.5	17010	8505
3	201.2	1379.4	1	6.75	1	9.00	2.50	5180.9	1.50	2.50	5985.7	6724.8	9893.7	12676	6338
5	178.3	1020.2	2	6.00	2	8.00	2.50	8558.4	1.50	2.50	9271.6	10301.2	15293.6	19970	9985
6 **	172.1	996.1	2	6.00	2	8.00	2.50	6340.8	1.50	2.50	7029.2	10034.0	14852.8	19275	9638
7	170.3	1051.9	2	6.00	2	8.00	2.50	8174.4	1.50	2.50	8855.6	10458.8	15227.2	19074	9537
8	165.4	964.3	2	6.00	2	8.00	2.50	7939.2	1.50	2.50	8600.8	9699.2	14330.4	18525	9262
9	137.5	728.7	2	6.00	2	8.00	2.50	6600.0	1.50	2.50	7150.0	7479.6	11329.6	15400	7700
10	123.9	618.2	2	6.00	2	8.00	2.50	5947.2	1.50	2.50	6442.8	6432.4	9901.6	13877	6938
11	84.9	318.1	2	5.63	2	6.63	2.50	3778.1	1.50	2.50	4117.7	3563.6	5643.7	8320	4160
12	67.0	382.4	2	5.50	2	5.50	2.50	2814.0	1.50	2.50	3082.0	3863.4	5337.4	5896	2948
13	81.7	338.0	1	5.50	2	6.75	2.50	2777.8	1.50	2.50	3104.6	2763.3	4315.6	6209	3105

\* Includes top corner overlap of 1.5 ft.

\*\* FRP Wrap calculations do not includes areas between

\lt. 2 Total =

65,063 ft<sup>2</sup>

Alt 3. Total = 118,364 ft<sup>2</sup>

ft²

Total = 78,116

71,312 ft<sup>2</sup>

Columns 3 to 5 and 11 to 13 since no steel reinforcement

is present at these locations.

Span	Col. No.	Column Height.	Column Width	No. of Exterior	Exterior Column Width	No. of Interior	Interior Column Width	FRP Wrap
		(ft.)	(ft.)	Columns	(ft.)	Columns	(ft.)	Alea (It )
	1	26.75	2.00	1	4.50	1	6.00	776
	2	18.69	2.00	1	4.50	1	6.00	542
	3	12.37	2.00	1	4.50	1	6.00	359
	4	7.40	2.00	1	4.50	1	6.00	215
	5	3.64	2.00	1	4.50	1	6.00	106
	6*	0.92	2.00	1	4.50	2	6.00	0
~	7*	-0.67	2.00	1	4.50	2	6.00	0
u .	8*	-1.30	2.00	2	4.50	2	6.00	0
pa	9*	-1.04	2.00	2	4.50	2	6.00	0
S	10*	0.11	2.00	2	4.50	2	6.00	0
	11	2.21	2.00	2	4.50	2	6.00	128
	12	5.45	2.00	2	4.50	2	6.00	316
	13	9.73	2.00	2	4.50	2	6.00	565
	14	15.22	2.00	2	4.50	2	6.00	883
	15	22.06	2.00	2	4.50	2	6.00	1280
	16	30.64	2.00	2	4.50	2	6.00	1777
	1	35.86	2.00	0	4.5	1	6.0	538
	2	26.74	2.00	1	4.5	1	6.0	775
	3	19.44	2.00	1	4.5	1	6.0	564
	4	13.30	2.00	1	4.5	1	6.0	386
	5	8.49	2.00	1	4.5	1	6.0	246
	6	4.77	2.00	1	4.5	1	6.0	138
	7	2.13	2.00	1	4.5	1	6.0	62
	8*	0.48	2.00	1	4.5	1	6.0	0
n 3	9*	-0.10	2.00	1	4.5	1	6.0	0
ba	10*	0.09	2.00	1	4.5	1	6.0	0
S	11*	1.06	2.00	1	4.5	1	6.0	0
	12	3.10	2.00	1	4.5	1	6.0	90
	13	6.12	2.00	1	4.5	1	6.0	177
	14	10.23	2.00	1	4.5	1	6.0	297
	15	15.43	2.00	1	4.5	1	6.0	447
	16	21.95	2.00	1	4.5	1	6.0	636
	17	29.64	2.00	1	4.5	1	6.0	860
	18	39.15	2.00	0	4.5	0	6.0	0

\* & Red Text : No FRP wrap is recommended for column heights less than 2.0 feet. Several lower deck columns do not exist either.

Span	Col. No.	Column Height. (ft.)	Column Width (ft.)	No. of Exterior Columns	Exterior Column Width (ft.)	No. of Interior Columns	Interior Column Width (ft.)	FRP Wrap Area (ft <sup>2</sup> )
	1	35.02	2.00	2	4.5	2	6.0	1786
	2	28.30	2.00	2	4.5	2	6.0	1641
	3	20.80	2.00	2	4.5	2	6.0	1206
	4	14.92	2.00	2	4.5	2	6.0	865
	5	10.46	2.00	2	4.5	2	6.0	607
	6	7.26	2.00	2	4.5	2	6.0	421
5	7	5.34	2.00	2	4.5	2	6.0	310
an	8	4.51	2.00	2	4.5	2	6.0	262
Sp	9	4.85	2.00	2	4.5	2	6.0	281
	10	6.27	2.00	2	4.5	2	6.0	363
	11	8.97	2.00	2	4.5	2	6.0	520
	12	12.93	2.00	2	4.5	2	6.0	750
	13	18.31	2.00	2	4.5	2	6.0	1062
	14	25.31	2.00	2	4.5	2	6.0	1468
	15	31.54	2.00	2	4.5	2	6.0	1609
	1	34.23	2.00	2	4.5	2	6.0	1403
	2	24.40	2.00	2	4.5	2	6.0	1415
	3	16.82	2.00	2	4.5	2	6.0	976
	4	10.86	2.00	2	4.5	2	6.0	630
	5	6.32	2.00	2	4.5	2	6.0	367
	6	3.04	2.00	2	4.5	2	6.0	177
9	7*	1.05	2.00	2	4.5	2	6.0	0
an	8*	0.14	2.00	2	4.5	2	6.0	0
Sp	9*	0.39	2.00	2	4.5	2	6.0	0
	10	2.52	2.00	2	4.5	2	6.0	146
	11	4.35	2.00	2	4.5	2	6.0	252
	12	8.23	2.00	2	4.5	2	6.0	477
	13	13.53	2.00	2	4.5	2	6.0	785
	14	20.96	2.00	2	4.5	2	6.0	1215
	15	29.63	2.00	2	4.5	2	6.0	1511

\* & Red Text : No FRP wrap is recommended for column heights less than 2.0 feet. Several lower deck columns do not exist either.

Span	Col. No.	Column Height. (ft.)	Column Width (ft.)	No. of Exterior Columns	Exterior Column Width (ft.)	No. of Interior Columns	Interior Column Width (ft.)	FRP Wrap Area (ft <sup>2</sup> )
	1	31.67	2.00	2	4.5	2	6.0	1299
	2	22.70	2.00	2	4.5	2	6.0	1316
	3	15.48	2.00	2	4.5	2	6.0	898
	4	9.81	2.00	2	4.5	2	6.0	569
	5	5.42	2.00	2	4.5	2	6.0	314
	6	2.27	2.00	2	4.5	2	6.0	132
N	7*	0.32	2.00	2	4.5	2	6.0	0
an	8*	-0.56	2.00	2	4.5	2	6.0	0
Sp	9*	-0.34	2.00	2	4.5	2	6.0	0
	10*	0.95	2.00	2	4.5	2	6.0	0
	11	3.44	2.00	2	4.5	2	6.0	200
	12	7.18	2.00	2	4.5	2	6.0	416
	13	12.18	2.00	2	4.5	2	6.0	707
	14	18.75	2.00	2	4.5	2	6.0	1087
	15	27.07	2.00	2	4.5	2	6.0	1381
	1	30.26	2.00	2	4.5	2	6.0	1240
	2	21.76	2.00	2	4.5	2	6.0	1262
	3	14.94	2.00	2	4.5	2	6.0	866
	4	9.49	2.00	2	4.5	2	6.0	550
	5	5.28	2.00	2	4.5	2	6.0	306
	6	2.23	2.00	2	4.5	2	6.0	129
8	7*	0.38	2.00	2	4.5	2	6.0	0
an	8*	-0.50	2.00	2	4.5	2	6.0	0
Sp	9*	-0.28	2.00	2	4.5	2	6.0	0
	10*	0.91	2.00	2	4.5	2	6.0	0
	11	3.31	2.00	2	4.5	2	6.0	192
	12	6.86	2.00	2	4.5	2	6.0	398
	13	11.65	2.00	2	4.5	2	6.0	676
	14	17.81	2.00	2	4.5	2	6.0	1033
	15	25.65	2.00	2	4.5	2	6.0	1308

\* & Red Text : No FRP wrap is recommended for column heights less than 2.0 feet. Several lower deck columns do not exist either.

Span	Col. No.	Column Height. (ft.)	Column Width (ft.)	No. of Exterior Columns	Exterior Column Width (ft.)	No. of Interior Columns	Interior Column Width (ft.)	FRP Wrap Area (ft <sup>2</sup> )	
	1	25.89	2.00	2	4.5	2	6.0	1061	
	2	17.91	2.00	2	4.5	2	6.0	1039	
	3	11.80	2.00	2	4.5	2	6.0	684	
	4	7.04	2.00	2	4.5	2	6.0	408	
	5	3.65	2.00	2	4.5	2	6.0	212	
6	6*	1.60	2.00	2	4.5	2	6.0	0	
an	7*	0.64	2.00	2	4.5	2	6.0	0	
Sp	8*	0.97	2.00	2	4.5	2	6.0	0	
	9	2.38	2.00	2	4.5	2	6.0	138	
	10	5.14	2.00	2	4.5	2	6.0	298	
	11	9.26	2.00	2	4.5	2	6.0	537	
	12	14.74	2.00	2	4.5	2	6.0	855	
	13	22.62	2.00	2	4.5	2	6.0	1154	
	1	22.16	2.00	2	4.5	2	6.0	909	
	2	14.73	2.00	2	4.5	2	6.0	854	
	3	8.90	2.00	2	4.5	2	6.0	516	
	4	4.41	2.00	2	4.5	2	6.0	256	
0	5*	1.35	2.00	2	4.5	2	6.0	0	
11	6*	-0.19	2.00	2	4.5	2	6.0	0	
oai	7*	-0.51	2.00	2	4.5	4.5 2		0	
SI	8*	0.40	2.00	2	4.5 2		6.0	0	
	9	2.83	2.00	2	4.5 2		6.0	164	
	10	6.68	2.00	2	4.5	2	6.0	387	
	11	11.87	2.00	2	4.5	2	6.0	689	
	12	18.68	2.00	2	4.5	2	6.0	952	
	1	16.20	2.00	1	4.5	1	6.0	332	
5	2	8.96	2.00	1	4.5	1	6.0	260	
& I	3	3.97	2.00	1	4.5	1	6.0	115	
IE .	4*	0.89	2.00	1	4.5	1	6.0	0	
1 V	5*	-0.36	2.00	1	4.5	1	6.0	0	
11	6*	-0.02	2.00	1	4.5	1	6.0	0	
) aı	7	2.19	2.00	1	4.5	1	6.0	63	
st	8	6.14	2.00	1	4.5	1	6.0	178	
	9	12.38	2.00	1	4.5	1	6.0	316	
	1	16.20	2.00	1	4.5	1	6.0	332	
: SI	2	8.63	2.00	1	4.5	1	6.0	250	
<b>%</b>	3	4.14	2.00	1	4.5	1	6.0	120	
St	4*	1.75	2.00	1	4.5	1	6.0	0	
11	5*	1.34	2.00	1	4.5	1	6.0	0	
an	6	2.81	2.00	1	4.5	1	6.0	82	
Sp	7	6.32	2.00	1	4.5	1	6.0	183	
	8	12.70	2.00	1	4.5	1	6.0	324	

\* & Red Text : No FRP wrap is recommended for column heights less than 2.0 feet. Several lower deck columns do not exist either.

Note: No lower deck columns are present in Spans 12 & 13.

\* No FRP Wrap, 1995 Floorbeam

Rough Form Length Factor: 25% of form board length

r	-	1	1		1	1			1	
	Floor	Interior	Exterior	Floor Beam	Floor Beam					
Span	Beam	Floor Beam	Floor Beam	Width	Height	Fillet Area	FRP Wrap	Rough Surface	Rough Surface	
	No.	Length	Length	(ft.)	(ft.)	(ft²)	Area (ft <sup>2</sup> )	Length (ft.)	Length (ft.)	
		(ft.)	(ft.)							
	1*	25.25	26.63	2.00	3.67	76.5	561	2243	561	
	2*	25.25	26.63	2.00	3.67	76.5	561	2243	561	
	3	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	4	25.25	20.03	2.00	3.67	76.5	809	3237	809	
	5 C*	25.25	20.05	2.00	3.07	70.5	609 E61	3237	809	
	7*	25.25	20.05	2.00	3.07	70.5	561	2243	561	
N	0	25.25	20.05	2.00	3.07	70.5	800	2243	561	
au	9	25.25	26.63	2.00	3.67	76.5	809	3237	809	
Sp	10	25.25	26.63	2.00	3.67	76.5	809	2227	809	
	11*	25.25	26.63	2.00	3.67	76.5	561	2243	561	
	12	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	13	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	14	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	15	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	16	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	1*	25.25	26.63	2.00	3.67	76.5	0	0	0	
	2	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	3	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	4	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	5	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	6	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	7	25.25	26.63	2.00	3.67	76.5	809	3237	809	
~	8	25.25	26.63	2.00	3.67	76.5	809	3237	809	
5	9	25.25	26.63	2.00	3.67	76.5	809	3237	809	
Spc	10	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l - '	11	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	12	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	13	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	14	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	15	25.25	26.63	2.00	3.6/	76.5	800	3237	809	
l	10	25.25	20.03	2.00	3.6/	70.5	0	3237	809	
l	1/*	25.25	20.03	2.00	3.0/	76.5	0	0	U	
	10	25.25	20.05	2.00	3.67	76.5	0	0	0	
	2*	25.25	26.63	2.00	3.67	76.5	561	22/3	561	
	3	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	4	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	5	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	6	25.25	26.63	2.00	3.67	76.5	809	3237	809	
Ś	7	25.25	26.63	2.00	3.67	76.5	809	3237	809	
a	8	25.25	26.63	2.00	3.67	76.5	809	3237	809	
Sp	9	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	10	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	11	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	12	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	13	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	14	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	15	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	1	25.25	26.63	2.00	3.67	38.3	//1	3084	771	
l	2	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	3	25.25	20.03	2.00	3.6/	70.5	800	3237	809	
l	5	25.25	20.03	2.00	3.07	76.5	809	3237	800	
	6	25.25	26.63	2,00	3,67	76.5	809	3237	809	
9	7	25.25	26.63	2.00	3.67	76.5	809	3237	809	
5	8	25.25	26.63	2.00	3.67	76.5	809	3237	809	
Spi	9	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l .	10	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	11	25.25	26.63	2.00	3.67	76.5	809	3237	809	
1	12	25.25	26.63	2.00	3.67	76.5	809	3237	809	
1	13	25.25	26.63	2.00	3.67	76.5	809	3237	809	
l	14	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	15	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	1	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	2	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	3	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	4	25.25	26.63	2.00	3.6/	76.5	800	3237	809	
	5	25.25	20.03	2.00	3.6/	70.5	800	3237	809	
	7	25.25	20.03	2.00	3.6/	70.5	800	3237	809	
5	8	25.25	20.03	2.00	3.07	76.5	809	3237	809	
pds	9	25.25	26.63	2.00	3.67	76.5	809	3257	809	
~	10	25.25	26.63	2,00	3,67	76.5	809	3237	809	
	11	25.25	26.63	2,00	3,67	76.5	809	3237	809	
	12	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	13	25.25	26.63	2.00	3.67	76.5	809	3237	809	
1	14	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	15	25.25	26.63	2.00	3.67	76.5	809	3237	809	

\* No FRP Wrap, 1995 Floorbeam

Rough Form Length Factor: 25% of form board length

	I	Interior	Exterior							
	Floor	Interior Floor Beam	Exterior Floor Beam	Floor Beam	Floor Beam	Fillet Area	FRP Wrap	Rough Surface	Rough Surface	
Span	Beam	Length	Length	Width	Height	(ft <sup>2</sup> )	Area (ft <sup>2</sup> )	Length (ft.)	Length (ft.)	
	NO.	(ft.)	(ft.)	(π.)	(π.)					
	1	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	2	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	3	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	4	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	6	25.25	26.63	2.00	3.67	76.5	809	3237	809	
~	7	25.25	26.63	2.00	3.67	76.5	809	3237	809	
Span	8	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	9	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	10	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	11	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	13	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	14	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	15	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	1	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	2	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	4	25.25	26.63	2.00	3,67	76.5	809	3237	809	
	5	25.25	26.63	2.00	3.67	76.5	809	3237	809	
9	6	25.25	26.63	2.00	3.67	76.5	809	3237	809	
an	7	25.25	26.63	2.00	3.67	76.5	809	3237	809	
s	8	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	9	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	10	25.25	20.03	2.00	3.67	76.5	809	3237	809	
	12	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	13	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	1	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	2	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	3	25.25	26.63	2.00	3.67	76.5	809	3237	809	
-	4	25.25	26.63	2.00	3.67	76.5	809	3237	809	
10	6	25.25	26.63	2.00	3.67	76.5	809	3237	809	
an	7	25.25	26.63	2.00	3.67	76.5	809	3237	809	
1s	8	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	9	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	10	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	11	25.25	26.63	2.00	3.67	76.5	809	3237	809	
	1	26.38	33.60	2.00	3.67	76.5 950		3799	950	
	2	26.38	33.60	2.00	3.67	76.5	950	3799	950	
	3	26.38	33.60	2.00	3.67	76.5	950	3799	950	
11	4	26.38	33.60	2.00	3.67	76.5	950	3799	950	
5	5	26.38	33.60	2.00	3.67	76.5	950	3799	950	
Spc	7	26.38	33.60	2.00	3,67	76.5	950	3799	950	
	8	26.38	33.60	2.00	3.67	76.5	950	3799	950	
	9	26.38	33.60	2.00	3.67	76.5	950	3799	950	
	10	26.38	33.60	2.00	3.67	76.5	950	3799	950	
	1*	26.38	33.60	1.50	4.00	0	0	0	0	
	2*	26.38	33.60	1.50	4.00	0	889	3556	570	
	4	26.38	33.60	1.50	4.00	0	889	3556	889	
	5	26.38	33.60	1.50	4.00	0	889	3556	889	
12	6	26.38	33.60	1.50	4.00	0	889	3556	889	
B	/ 8	26.38	33.60	1.83	4.00	0	920	3680	920	
Spi	9	26.38	33.60	1.50	4.00	0	889	3556	889	
	10	26.38	33.60	1.50	4.00	0	889	3556	889	
	11	26.38	33.60	1.50	4.00	0	889	3556	889	
	12	26.38	33.60	1.50	4.00	0	889	3556	889	
	15	26.38	33.60	1.50	4.00	0	889	3556	889	
	1	26.38	30.75	2.58	3.67	0	741	2963	741	
	2	26.38	30.75	2.58	3.67	0	566	2266	566	
3	3	26.38	30.75	2.58	3.67	0	566	2266	566	
, u	4	26.38	30.75	2.58	3.67	0	566	2266	566	
Spa	5	26.38	30.75	2.58	3.67	0	566	2266	566	
	7	26.38	30.75	2.58	3,67	0	566	2200	566	
	- ·		20.75	2.50	2.07		071	2200	074	

Totals = 117,303 469,213 117,303 ft.

## CUY-6-1456 PIERS FRP Wrap Quantities

Location	North Exterior Bay (ft <sup>2</sup> )	Interior Bay	South Exterior Bay			
West Abut.	0	0	0			
Pier 1	0	0	0			
Pier 2	0	0	0			
Pier 3	0	0	0			
Pier 4	200	200	200			
Pier 5	1098	1133	1098			
Pier 6	1098	1133	1098			
Pier 7	1098	1133	1098			
Pier 8	1098	1133	1098			
Pier 9	1098	1133	1098			
Pier 10	1098	1133	1098			
Pier 11	0	0	0			
Pier 12	0	0	0			
East Abut.	0	0	0			
	6,785	6,998	6,785			

Total 20,5

20,569 SF

## CUY-6-1456 FRP Wrap Totals

	Esti	Rough				
Element	With Arch Rib Alt. No. 1 (ft <sup>2</sup> )	With Arch Rib Alt. No. 2 (ft <sup>2</sup> )	With Arch Rib Alt. No. 3 (ft <sup>2</sup> )	Surface Length (ft)		
Arch Ribs	65,063	71,312	118,364	78,116		
Columns	64,616	64,616	64,616	20,000		
Floor Beams	117,303	117,303	117,303	117,303		
Lower Pier Shafts				5,000		
Total	246,983	253,232	300,284	215,419		

## APPENDIX F

# West Station Deterioration Drawings



## CUY-6-1456 2016 West Station Patching

Detroit Tunnel										
Bay	Concrete Repairs (SF)									
20,	North Wall	Ceiling	South Wall							
1	407	16	279							
2	347	150	353							
3	225	220.5	204							
4	203.25	36	410							
5	171.25	98	343.5							
6	260.75	108	371.5							
7	350.5	294	422.25							
8	153	588	224							
9	184	844.5	131							
10	300	171.5	614							
Sub-Totals	2,602	2,527	3,352							

W. 25th Tunnel											
Bay	Concrete Repairs (SF)										
2017	West Wall	Ceiling	East Wall								
11	136	32	386								
12	133	0	131								
13	65	16	292.5								
14	182	0	163								
15	81	0	92								
16	166	16	159								
17	363	280	155								
Sub-Totals	1,126	344	1,379								

11,329 Totals

SF









DETROIT-SUPERIOR BRIDGE WEST STATION

LINE A, COLUMNS A18 TO A24



— 4 SF

CONCRETE DELAMINATION/SPALL

CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

DETROIT-SUPERIOR BRIDGE WEST STATION

LINE A, COLUMNS A25 TO A31









SOUTH ELEVATION

CONCRETE DELAMINATION/SPALL

CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

DETROIT-SUPERIOR BRIDGE WEST STATION LINE B, COLUMNS B1 TO B7

5





SOUTH ELEVATION





CONCRETE DELAMINATION/SPALL

CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

> DETROIT-SUPERIOR BRIDGE WEST STATION LINE B, COLUMNS B8 TO B15 6





SOUTH ELEVATION





CONCRETE DELAMINATION/SPALL

CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

> DETROIT-SUPERIOR BRIDGE WEST STATION LINE B, COLUMNS B16 TO B23 7





SOUTH ELEVATION





CONCRETE DELAMINATION/SPALL

CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

DETROIT-SUPERIOR BRIDGE WEST STATION LINE B, COLUMNS B24 TO B31 8





SOUTH ELEVATION







SOUTH ELEVATION









SOUTH ELEVATION

- CL TOWER A EXPANSION JOINT

#### <u>LEGEND</u>



CONCRETE DELAMINATION/SPALL



CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

DETROIT-SUPERIOR BRIDGE WEST STATION LINE C, COLUMNS C25-C31





SOUTH ELEVATION







SOUTH ELEVATION

LINE D, COLUMNS D11 TO D18





SOUTH ELEVATION







SOUTH ELEVATION



CONCRETE DELAMINATION/SPALL

CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

DETROIT-SUPERIOR BRIDGE WEST STATION

LINE D, COLUMNS D27 TO D31

## APPENDIX G

# West Station Deterioration History



CUY-6-1456 over Cuyahoga River Rehabilitation Feasibility Study Ohio Department of Transportation

### CUY-6-1456 West Station

#### Jack Arch Deterioration Summary, 1995-2016

#### Part. Rep. - Partial Replacement

R - Replacement

Jack Arch	1995	2012	2016	Jack Arch	1995	2012	2016	Jack Arch	1995	2012	2016	Jack Arch	1995	2012	2016	Jack Arch	1995	2012	2016	Jack Arch	1995	2012	2016
NO.				NO.				NO.				NO.				NO.				NO.			
				<b>P12</b>	15		+	C1 2	DD														
A 2-2	14	20	10	B 2-2	12			C 1-2	5														
Δ 3-4	17	5	10	B 3-4			5	C 2-5				D 3-4		2	29								
A 4-5	4		<i>1</i> /	B 4-5	Д		25	C 4-5	6			D 4-5											
A 5-6	3			B 5-6	·			C 5-6	Ŭ			D 5-6	2										
A 6-7	4	10	16	B 6-7			1	C 6-7				D 6-7	_			E 6-7	2						
A 7-8			1	B 7-8			1	C 7-8	4		11	D 7-8				E 7-8	- 5						
A 8-9	2		15	B 8-9	Part. Rep.			C 8-9	5		6	D 8-9	Part, Rep.		8	E 8-9	R						
A 9-10	14		58	B 9-10	3	4	4	C 9-10	5	4	10	D 9-10	3			E 9-10	8						
A 10-11	R			B 10-11	Part. Rep.	10	24	C 10-11	Part. Rep.		21	D 10-11	Part. Rep.		1	E 10-11	2						
A 11-12	14	50	55	B 11-12	8		4	C 11-12	6	20	36	D 11-12			14	E 11-12	6						
A 12-13	R		21	B 12-13	Part. Rep.	33	11	C 12-13	Part. Rep.	11	41	D 12-13	15	10	27	E 12-13	5						
A 13-14	R		9	B 13-14			11	C 13-14	10	72	85	D 13-14	3			E 13-14	3						
A 14-15	R		20	B 14-15	Part. Rep.		13	C 14-15	Part. Rep.		53	D 14-15	6		6	E 14-15	3						L
A 15-16	16		42	B 15-16		14	7	C 15-16		2	12	D 15-16				E 15-16	3			F 15-16			L
A 16-17	22		61	B 16-17	15	31	47	C 16-17	12	43	24	D 16-17	6		3	E 16-17	5			F 16-17			
A 17-18	3	62	37	B 17-18				C 17-18			1	D 17-18				E 17-18	3			F 17-18			Ļ
A 18-19	Part. Rep.	12	32	B 18-19	12	56	38	C 18-19	14	69	43	D 18-19	6			E 18-19	3			F 18-19			
A 19-20	12	24	32	B 19-20			11	C 19-20			5	D 19-20	2			E 19-20	3			F 19-20			
A 20-21	Part. Rep.		46	B 20-21	Part. Rep.	23	28	C 20-21	Part. Rep.	62	23	D 20-21	Part. Rep.		1	E 20-21	Part. Rep.			F 20-21	4		
A 21-22	4		32	B 21-22				C 21-22				D 21-22				E 21-22				F 21-22			
A 22-23	9	11	76	B 22-23	6	35	39	C 22-23	15	64	64	D 22-23	8		14	E 22-23				F 22-23			
A 23-24	5		6	B 23-24	3		10	C 23-24	2		9	D 23-24				E 23-24				F 23-24			
A 24-25	5		75	B 24-25	12	40	73	C 24-25	5	30	60	D 24-25	3			E 24-25	4			F 24-25			
A 25-26	4		4	B 25-26	2		2	C 25-26				D 25-26	5		10	E 25-26				F 25-26	5	6	r
A 26-27	4			B 26-27	16	33		C 26-27	18	32		D 26-27	9	4	16	E 26-27	6			F 26-27	6		r
A 27-28				B 27-28				C 27-28	4			D 27-28	8		13	E 27-28	6			F 27-28	R		
A 28-29	8			B 28-29	12	35	68	C 28-29	21	55		D 28-29	16	36	49	E 28-29				F 28-29	R		
A 29-30	8	1/		B 29-30			3	C 29-30	2	10	4	D 29-30	8	5	50	E 29-30				F 29-30	ĸ		
A 30-31	10			B 30-31		10	2	C 30-31	3	19		D 30-31				E 30-31	ĸ			F 30-31	ĸ		
A 31-Jt.	10	/		B 31-Jt.		10	20	C 31-JT.	12	20		D 31-Jt.	5			E 31-Jt.	к			F 31-Jt.	ĸ		
Totals	182	218	665		119	324	446		149	503	524		105	58	241		67	0	0		15	6	0
												1										-	
West							1																
Station	637	1109	1876																				1
Totals																							1
							1			[													
## CUY-6-1456 West Station 2016 Column Repair Summary

Replacement Recommended

Column No.	Total Deficiency (SF)	Surface	Subtotal (SF)	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)	Column No.	Total Deficiency (SF)	Surface	Subtotal (SF)	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)	Column No.	Total Deficiency (SF)	Surface	Subtotal (SF)	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)	Column No.	Total Deficiency (SF)	Surface	Subtotal (SF)	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)
								0	North	0.0				n	٩	North	2.7	2.7									
		North	2.0	2.0				Ů	South	0.0						South	0.0	0.7									
A2	8	Sides	4.7	4.7			B2	0	Sides	0.0				C2	0	Sides	0.0										
A2	0	North	0.0	0.0		<b>.</b>	82	0	North	0.0				6	0	North	0.0				D2	0	North	0.0			
AS	Ŭ	South	0.0	0.0				Ů	South	0.0				3	Ů	South	0.0				5	Ů	Sides	0.0			
A4	5	Sides	2.3	2.3			В4	5	Sides	4.7	4.7			C4	0	Sides	0.0				D4	1	Sides	0.8	0.8		
		North	0.0	18.7					North	0.0						North	0.0						North	0.0			
A5	19	Sides	0.0				В5	U	Sides South	0.0				LS .	U	Sides South	0.0				D2	U	Sides South	0.0			
A6	3	North Sides	1.3 1.9	1.3 1.9		<u> </u>	B6	0	North Sides	0.0				C6	0	North Sides	0.0				D6	0	North Sides	0.0			
		South North	0.0 0.0						South North	0.0						South North	0.0						South North	0.0			
A7	0	Sides South	0.0	<u> </u>			B7	0	Sides South	0.0				C7	0	Sides South	0.0				D7	0	Sides South	0.0			
A8	8	North Sides	8.0 0.0	8.0			B8	3	North Sides	0.0 1.5	1.5			C8	0	North Sides	0.0				D8	0	North Sides	0.0			
		South North	0.0	<u> </u>					South North	1.2 0.0	1.2					South North	0.0						South North	0.0			
A9	0	Sides South	0.0				B9	0	Sides South	0.0				C9	0	Sides South	0.0				D9	0	Sides South	0.0			
A10	0	North Sides	0.0				B10	2	North Sides	0.0				C10	0	North Sides	0.0				D10	0	North Sides	0.0			
		South North	0.0	<u> </u>					South North	2.3 0.0	2.3					South North	0.0						South North	0.0	5.5		
A11	0	Sides	0.0	f			B11	0	Sides	0.0				C11	0	Sides	0.0				D11	14	Sides	8.3	3.3	5.0	
A12	14	North Sides	3.5 6.7	3.5 6.7			B12	1	North Sides	0.0				C12	9	North Sides	6.0 3.0	6.0 0.8	2.2		D12	6	North Sides	0.0	6.3		
		South	3.9	1.6	2.3				South	0.7	0.7					South	0.0	0.0					South	0.0	0.0		
A13	4	Sides	2.1	2.1		<b> </b>	B13	0	Sides	0.0				C13	0	Sides	0.0				D13	9	Sides	9.0	9.0		
Δ14	44	North	15.7	15.7	15.2	2.0	B14	0	North	0.0				C14	0	North	0.0				D14	0	North	0.0			
		South	5.3	5.3	13.3	2.5		-	South	0.0				014		South	0.0	5.6			514	-	South	0.0			
A15	22	Sides	4.3	4.3			B15	0	Sides	0.0				C15	12	Sides	6.7	6.7			D15	0	Sides	0.0			
A16	0	North	0.0	3.5			B16	0	North	0.0				C16	0	North	0.0				D16	0	North	0.0			
A10	Ů	South	0.0					Ů	South	0.0				010	Ů	South	0.0				510	Ů	South	0.0			
A17	11	Sides	4.4	1.3	2.8	<b> </b>	B17	0	Sides	0.0				C17	0	Sides	0.0				D17	0	Sides	0.0			
410	_	North	2.3	2.3			<b>P10</b>	_	North	0.0				<b>C19</b>		North	0.0				D19	15	North	6.3	6.3		
AIS	U	Sides	0.0				- D19	0	Sides	0.0				C18	0	Sides	0.0				D19	15	Sides	9.0	3.0	6.0	
A19	1	Sides	0.0			<b> </b>	B19	0	Sides	0.0				C19	0	Sides	0.0				D19	0	Sides	0.0			
		North	4.3	1.0	2.8				North	0.0	1.6			620		North	0.0	10.5					North	2.2	2.2		
AZU	y	Sides	2.8	2.8			B20	6	Sides	0.3 4.3	0.3 4.3			C20	37	Sides	16.4 10.5	8.2 10.5	8.2		D20	2	Sides South	0.0			
A21	46	North Sides	18.4 18.4	18.4 9.2	4.6	4.6	B21	8	North Sides	3.4 1.7	3.4 1.7			C21	7	North Sides	0.0 3.3	3.3			D21	91	North Sides	22.7 45.4	22.7 22.7	22.7	
		South North	9.2 0.0	4.6	4.6				South North	2.5 0.0	2.5					South North	4.0 0.0	4.0					South North	22.7 23.0	22.7 23.0		
A22	0	Sides South	0.0 0.0	<sup> </sup>			822	4	Sides South	2.6 1.1	2.6 1.1			C22	0	Sides South	0.0				DZZ	92	Sides South	46.0 23.0	23.0 23.0	23.0	
A23	0	North Sides	0.0 0.0	ļ		<u> </u>	B23	0	North Sides	0.0				C23	14	North Sides	0.0 4.6	4.6			D23	0	North Sides	0.0			
<u> </u>		South North	0.0		 	<b> </b>			South North	0.0	4.0					South North	9.2 0.0	8.3	0.9				South North	0.0	6.0		
A24	0	Sides South	0.0	<u> </u>			B24	9	Sides South	0.0 5.3	5.3			C24	0	Sides South	0.0				D24	24	Sides South	12.0 6.0	6.0 6.0	6.0	
A25	0	North Sides	0.0	ļ	<u> </u>		B25	0	North Sides	0.0	<u> </u>			C25	6	North Sides	2.7 3.3	2.7 3.3			D25	16	North Sides	4.0 8.0	4.0 4.0	4.0	
		South North	0.0 0.0				<u> </u>		South North	0.0						South North	0.0						South North	4.0 0.0	4.0		
A26	0	Sides South	0.0 0.0				B26	0	Sides South	0.0				C26	0	Sides South	0.0 0.0				D26	9	Sides South	3.5 5.0	1.9 5.0	1.7	
A27	0	North Sides	0.0	<u> </u>			B27	0	North Sides	0.0				C27	0	North Sides	0.0				D27	0	North Sides	0.0			
<u> </u>		South North	0.0						South North	0.0						South North	0.0						South North	0.0			
A28	0	Sides South	0.0	<u> </u>			B28	3	Sides South	0.0	3.0			C28	0	Sides South	0.0				D28	0	Sides South	0.0			
A29	0	North Sides	0.0				B29	0	North Sides	0.0				C29	8	North Sides	5.4 3.0	5.4 1.6	1.4		D29	0	North Sides	0.0			
		South North	0.0				]		South North	0.0						South North	0.0						South North	0.0	4.5		
A30	0	Sides South	0.0		<b> </b>		B30	0	Sides South	0.0				C30	0	Sides South	0.0				D30	21	Sides South	13.1 3.4	9.0 3.4	4.1	
A31	22	North Sides	5.7 13.1	5.7 9.6	3.5		B31	0	North Sides	0.0				C31	0	North Sides	0.0				D31	0	North Sides	0.0			
		South	2.9	2.9			1		South	0.0						South	0.0						South	0.0			
Totals	214							40							103							300					

R -	Replaced	Replace

Column No.	1995	2012	2016	Column No.	1995	2012	2016	Column No.	1995	2012	2016	Column No.	1995	2012	2016	Column No.	1995	2012	2016	Column No.	1995	2012	2016
				P1				<u></u>		6	0												
Δ2			8	B1 B2		+				0	5												
A3				B3		+		C2 C3															
A4	8		5	B4		5	5	C4				D4	2		1								
A5	3		19	B5	3			C5				D5	3										
A6			3	B6	6	1		C6	1			D6				E6							
A7				B7		1		C7				D7				E7							
A8			8	B8		1	3	C8	2			D8	16			E8	R						
A9				B9		2		C9				D9				E9	R						
A10	R			B10		1	2	C10	4	20		D10	R			E10							
A11				B11		]		C11	2			D11	15	2	14	E11	12	12					
A12	14	65	14	B12	4		1	C12	7	13	9	D12			6	E12	3						
A13			4	B13				C13	18	R		D13		15	9	E13							
A14	10	50	44	B14		4		C14	11	R		D14				E14							
A15	11	60	22	B15				C15		10	12	D15				E15				F15			
A16	4	R		B16				C16		2		D16				E16				F16			
A17	2		11	B17				C17				D17				E17	2			F17			
A18				B18				C18	3	8		D18	17	6	15	E18				F18			
A19			1	B19			~	C19	45		~~	D19				E19				F19			
A20	2	2	9	B20			6	C20	15		3/	D20	4.0	2	2	E20				F20			
A21	4	100	46	B21	4		8	(21	4		/	D21	16	12	91	E21				F21	г	4	
A22	۷			B22	4	+	4	C22	4		14	D22	10	10	92	E22		2		F22		4	
A23				B23	10	+	٩	C23	2	R	14	D23	6	18	24	F24	3	5		F23	8	1	
Δ25				B25	2	+		C25	2	N.	6	D24	10	10	16	F25	J			F25	0		
A26				B26	2	+		C26		7		D26	26	12	9	F26	8	24	24	F26			
A27	3			B27		+		C27		13		D27	6	9		E27		9	~ ·	F27		19	20
A28	3			B28		3	3	C28				D28	-	9		E28	R			F28	R		
A29	5	6		B29	4	7		C29			8	D29	R			E29	R			F29	R		
A30				B30	12	10		C30		2		D30	R		21	E30	R			F30	R		
A31	4		22	B31	10	1		C31		36		D31				E31	R			F31	R		
						1																	
	75	283	216		55	31	41		76	117	102		127	115	300		36	52	24		13	27	20
West																							
Station	382	625	703																				
Totals						+																	

## CUY-6-1456 West Station Jack Arch Repair Summary

## REPLACEMENT RECOMMENDED

Jack Arch No.	Total Deficiency (SF)	Surface	Subtotal (SF)	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)	Jack Arch No.	Total Deficiency (SF)	Surface	Subtotal (SF)	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)	Jack Arch No.	Total Deficiency (SF)	Surface	Subtotal (SF)	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)	Jack Arch No.	Total Deficiency (SF)	Surface	Subtotal (SF)	Area 1 (SF)	Area 2 (SF)	Area 3 (SF)
							B 1-2	0	North Bottom	30.7 0.0	30.7			C 1-2	0	North Bottom	0.0 0.0										
A 2-3	10	North Bottom	1.1 8.5	1.1 8.5			B 2-3	0	South North Bottom	5.8 0.0 0.0	5.8			C 2-3	0	South North Bottom	0.0 0.0 0.0										
A 3-4	17	South North Bottom	0.0 11.0 3.6	11.0 3.6			в 3-4	5	South North Bottom	0.0 5.0 0.0	5.0			C 3-4	0	South North Bottom	0.0 0.0 0.0				D 3-4	29	North Bottom	10.2 4.9	9.6 2.4	0.6 2.5	
A 4-5	0	South North Bottom	2.9 0.0 0.0	2.9			B 4-5	25	South North Bottom	0.0 7.7 10.3	7.7 2.8	7.5		C 4-5	16	South North Bottom	0.0 11.1 4.8	11.1 4.8			D 4-5	0	South North Bottom	14.3 0.0 0.0	10.1	4.3	
A 5-6	0	South North Bottom	0.0 0.0 0.0				B 5-6	0	South North Bottom	6.8 0.0 0.0	6.8			C 5-6	0	South North Bottom	0.0 0.0 0.0				D 5-6	0	South North Bottom	0.0 0.0 0.0			
A 6-7	16	South North Bottom	0.0 14.6 1.5	4.9 1.5	9.7		B 6-7	0	South North Bottom	0.0 0.0 0.0				C 6-7	0	South North Bottom	0.0 0.0 0.0				D 6-7	0	South North Bottom	0.0 0.0 0.0			
A 7-8	1	South North Bottom	0.0 1.2 0.0	1.2			B 7-8	1	South North Bottom	0.0 0.0 0.0				C 7-8	11	South North Bottom	0.0 4.5 2.8	1.9 1.1	2.6 1.8		D 7-8	0	South North Bottom	0.0 0.0 0.0			
A 8-9	15	South North Bottom	0.0 12.4 2.3	4.7 2.3	3.8	4.0	B 8-9	0	South North Bottom	1.0 0.0 0.0	1.0			C 8-9	6	South North Bottom	3.6 3.5 2.4	2.3 3.5 2.4	1.3		D 8-9	8	South North Bottom	0.0 0.0 2.0	2.0		
A 9-10	58	South North Bottom	0.0 45.5 7.0	45.5 7.0			в 9-10	4	South North Bottom	0.0 0.0 0.0				C 9-10	10	South North Bottom	0.0 5.5 0.0	4.3	1.3		D 9-10	0	South North Bottom	5.6 0.0 0.0	5.6		
A 10-11	0	South North Bottom	5.6 0.0 0.0	5.6			B 10-11	24	South North Bottom	3.6 10.7 2.3	2.5 10.7 2.3	1.1		C 10-11	21	South North Bottom	4.3 12.0 5.5	4.3 6.1 4.2	5.9 1.4		D 10-11	1	South North Bottom	0.4 1.0 0.0	0.4		
A 11-12	55	South North Bottom	0.0 44.8 9.3	44.8 9.3			B 11-12	4	South North Bottom	11.2 4.3 0.0	9.9 4.3	1.3		C 11-12	36	South North Bottom	3.7 19.8 3.6	2.7 16.4 3.6	1.0 3.3		D 11-12	14	South North Bottom	0.0 13.9 0.0	13.9		
A 12-13	21	South North Bottom	0.8 13.9 1.9	0.8 13.9 1.9			B 12-13	11	South North Bottom	0.0 6.9 2.7	6.9 2.7			C 12-13	41	South North Bottom	13.0 15.1 11.1	13.0 3.4 4.0	11.7 7.1		D 12-13	27	South North Bottom	0.0 26.5 0.0	26.5		
A 13-14	9	North Bottom	5.4 9.2 0.0	5.4 9.2			B 13-14	11	South North Bottom	1.7 0.0 0.0	1.7			C 13-14	85	South North Bottom	15.2 29.1 22.9	5.9 4.6 22.9	9.3 24.5		D 13-14	0	South North Bottom	0.0 0.0 0.0			
A 14-15	20	South North Bottom	0.0 12.8 4.3	2.7 4.3	10.1		B 14-15	13	South North Bottom	11.1 1.8 8.1	11.1 1.8 0.6	5.0	2.5	C 14-15	53	South North Bottom	33.4 17.3 13.3	33.4 14.3 6.7	3.0 6.7		D 14-15	6	South North Bottom	0.0 4.4 1.3	3.6 1.3	0.8	
A 15-16	42	North Bottom	3.0 26.1 6.5	3.0 26.1 6.5			B 15-16	7	South North Bottom	3.0 3.1 2.5	1.2 1.8 2.5	1.8		C 15-16	12	South North Bottom	22.0 6.9 1.9	10.5 1.5 1.9	4.5	0.9	D 15-16	0	South North Bottom	0.0 0.0 0.0			
A 16-17	61	North Bottom	9.6 42.1 4.5	26.1 2.3	2.0 16.0 2.3	26	B 16-17	47	North Bottom	1.8 16.4 14.4	1.8 16.4 4.0	10.5		C 16-17	24	North Bottom	2.7 14.3 9.9	2.7 3.5 9.9	10.8		D 16-17	3	North Bottom	2.9 0.0	2.9		
A 17-18	37	North Bottom	14.8 20.5 11.3	3.9 11.8 8.3	8.3 5.9 0.5	2.6 2.9 2.5	B 17-18	0	North Bottom	0.0	3.5	12.4		C 17-18	1	North Bottom	0.0	0.9			D 17-18	0	North Bottom	0.0			
A 18-19	32	North Bottom	5.7 0.0 3.3	1.0	2.3		B 18-19	38	North Bottom	0.0 12.7 12.5	12.7 12.5			C 18-19	43	North Bottom	0.0 16.9 10.0	3.5 10.0	13.4		D 18-19	0	North Bottom	0.0			
A 19-20	32	North Bottom	1.4 4.6	10.8 1.4 4.6	9.0	8.0	B 19-20	11	North Bottom	2.9	2.9			C 19-20	5	North Bottom	2.6	2.6			D 19-20	0	North Bottom	0.0			
A 20-21	46	North Bottom	26.0 9.3	11.7 3.3 6.1	11.7 3.0 2.1	2.7 3.0	B 20-21	28	North Bottom	10.7 6.6	10.7 5.0	1.6		C 20-21	23	North Bottom	8.8 6.7	5.9 6.7	2.9		D 20-21	1	North Bottom	0.0	10		
A 21-22	32	North Bottom	23.7 4.6	23.7 4.6	1.1	2.5	B 21-22	0	North Bottom	0.0	1.1	2.0		C 21-22	0	North Bottom	0.0		1.7		D 21-22	0	North Bottom	0.0	1.0		
A 22-23	76	North Bottom South	24.7	24.7 23.0	24.6	2.6	B 22-23	38	North Bottom	16.1 12.5	16.1 12.5			C 22-23	64	North Bottom	19.1 18.7	19.1 18.7 26.2			D 22-23	14	North Bottom	5.9 0.0	5.9		
A 23-24	6	North Bottom	0.0	6.0	24.0	2.0	B 23-24	10	North Bottom	4.9 0.0	4.9			C 23-24	9	North Bottom	3.2 0.0	3.2	2.2		D 23-24	0	North Bottom	0.0	8.0		
A 24-25	75	North Bottom	25.5 24.0	25.5 24.0			B 24-25	73	North Bottom	30.5 20.8	28.5	2.0		C 24-25	60	North Bottom	22.1 15.5	22.0 22.1 15.5	5.2		D 24-25	0	North Bottom	0.0			
A 25-26	4	North Bottom	25.5	25.5 2.4 1.6			B 25-26	2	North Bottom	21.7 2.0 0.0	2.0			C 25-26	o	North Bottom	0.0				D 25-26	10	North Bottom	0.0 4.0 0.0	4.0		
A 26-27	0	North Bottom	0.0				B 26-27	0	North Bottom	0.0				C 26-27	0	North Bottom	0.0				D 26-27	16	North Bottom	8.8 2.0	4.9 2.0	2.2	1.8
A 27-28	0	North Bottom	0.0				B 27-28	0	South North Bottom	0.0				C 27-28	0	South North Bottom	0.0				D 27-28	13	South North Bottom	4.7 1.7 0.0	1.0	1.9	1.8
A 28-29	0	South North Bottom	0.0				B 28-29	68	South North Bottom	0.0 23.2 21.7	23.2 21.7			C 28-29	0	South North Bottom	0.0				D 28-29	49	South North Bottom	11.1 25.6 10.0	3.5 25.6 6.0	4.0	
A 29-30	o	North Bottom	0.0				B 29-30	3	South North Bottom	23.3 0.0 0.0	23.3			C 29-30	4	North Bottom	0.0 4.4 0.0	1.2	3.2		D 29-30	50	North Bottom	12.9 22.0 17.0	12.9 22.0 17.0	6.0	
A 30-31	0	South North Bottom	0.0				B 30-31	2	South North Bottom	2.7 2.4 0.0	2.7			C 30-31	0	South North Bottom	0.0				D 30-31	o	South North Bottom	11.2 0.0 0.0	4.4	6.8	
A 31-Jt.	o	North Bottom	0.0				B 31-Jt.	20	South North Bottom	0.0 7.3 6.7	7.3 6.7			C 31-Jt.	0	North Bottom	0.0				D 31-Jt.	o	North Bottom	0.0			
Totals	667	South 0	0.0					445	SOUCH	5.5	5.5				525	south	0.0					239	south	0.0			
<b>}</b>	<u> </u>	+		+	+	+	<b>†</b>	ł	<u> </u>	<u> </u>	+	·†	t	<b> </b>	t	<u>+</u>	L	+		+	<u> </u>	<b> </b>			<u> </u>	<u> </u>	

Lines A-D: Total Deterioration = 1875.4 SF

## APPENDIX H

**MAINTENANCE OF TRAFFIC** 



CUY-6-1456 over Cuyahoga River Rehabilitation Feasibility Study Ohio Department of Transportation









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---- MAKE INSIDE RIGHT TURN ONLY TO W. SUPERIOR



OVERHEAD SIGN DETAIL W. 9TH ST.



MOT DETAIL LANE CLOSURES

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MAKE LEFT ONLY TO W. SUPERIOR

MOT DETAIL LANE CLOSURES

MARIA

AGAA.

A DA

Shaheen Modern

& Contemporary

STILL I

LUIS .

W Superior Ave

CLOSE LEFT TURN LANE

4







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