

**OHIO DEPARTMENT OF TRANSPORTATION
2017 REHABILITATION FEASIBILITY STUDY
PID NO 99972**

**DETROIT-SUPERIOR BRIDGE OVER CUYAHOGA RIVER
BRIDGE NO. CUY-6-1456**

SFN: 1800930



REVISED MAY 2017

PREPARED BY:



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I. EXECUTIVE SUMMARY

The original feasibility study did not meet budget constraints for this project. The intent of the revised feasibility study is to summarize several additional Alternative No. 2's and their associated costs so that the District can make an informed decision for rehabilitation.

CUY-6-1456 (SFN 1800930), commonly known as the Detroit-Superior Bridge and later renamed the Veteran's Memorial Bridge, is a 1917 double-deck structure carrying vehicular and pedestrian traffic over the Cuyahoga River Valley (**Photos 1 & 2**). The bridge is approximately 2,880 feet long, including 1,673 feet of subway tunnel that is linked by the lower deck. In its original design, the upper deck carried vehicular and pedestrian traffic while the lower deck had four streetcar lines and capacity for two future tracks. The streetcar lines across the Detroit-Superior Bridge were discontinued in 1953. The Detroit-Superior Bridge is included on the National Register of Historic Places. With the bridge reaching it's 100th year of service, one of the goals is to provide a rehabilitation scheme that will allow the bridge to be of service for the next 50 years.

Pennoni was charged with the following tasks for the Feasibility Study:

1. Document the extent of the deterioration of the concrete on the approach spans.
2. Research the use Fiber Reinforced Polymer (FRP) to contain the concrete repairs and future deterioration over the public areas.
3. Identify the right-of-way needs for the rehabilitation.
4. Miscellaneous items such as, MOT, Navigation Lights, additional security for the Central Street Bridge Tenders Garage and vandal proofing the lower portions of the approach spans.
5. Provide alternates for the necessary repair.

In addition to the in-depth Inspections made in 2015 and in 2016, Pennoni documented the extensive concrete deterioration in the West Station, Spans 1A, 1B and 1 through 13 and the East Station. Several rehabilitation projects have been completed throughout the 100-year life span, including major rehabilitations in 1967-1970 and 1995-1997. The most recent rehabilitation from 2014-2016 was to repair concrete deterioration throughout the structure. Most of the deteriorated areas, including some repaired in the 1995-97 rehabilitation showed signs of reinforcing steel oxidation, or rusting. Several of those areas are in the West Station and lower deck area that get no salt. Therefore, non-chloride related concrete corrosion is likely present. Concrete corrosion is the chemical, colloidal or physicochemical deterioration and disintegration of solid concrete components and structures, due to attack by reactive liquids and gases. One type of concrete corrosion, carbonation, is a potential contributor of the ongoing deterioration. To verify this assumption, samples of the spalled concrete were tested for pH content (**Appendix C**). The concrete material of the samples show low alkalinity levels (< 12), suggesting that carbonation may be occurring. Carbonation is the result of CO₂ absorption into the concrete. In cities like Cleveland, carbonization can permeate concrete as

much as 0.04 inches per year, or 3 inches before the epoxy-urethane sealer was applied in 1997.

Several different FRP materials were investigated. Because the goal is to contain the deteriorated concrete and not to strengthen the members, it was determined that a low strength FRP wrap would be adequate for this application. The wrap would not alter the existing load paths. It should be noted that ODOT Central Office is studying FRP wrap for seismic containment on bridge columns. This assessment is outside the scope of our work and no consideration of seismic loading was taken into consideration.

Pennoni also looked at cathodic protection to stabilize the increasing concrete corrosion rate, and possibly to reverse it. Cathodic protection can be obtained with passive induction using anode pucks or active induction such as impressed current. Both have been used successfully over the past two decades. For this application, the active cathodic protection would provide the best results.

Primary construction tasks of the three alternates in this feasibility study are:

1. Maintenance Alternate: Replace upper deck wearing surface, Remove the deteriorated concrete but not patch the deteriorated concrete on the entire bridge.
2. FRP Alternate: Research the use of Fiber Reinforced Polymer (FRP) wraps to contain the concrete repairs and future deterioration over public areas. Replace upper deck wearing surface, Remove and patch the deteriorated concrete, Use of fiber wrap on the entire bridge.
3. Cathodic Protection Alternate. Replace upper deck wearing surface, patch deteriorated concrete, and apply active cathodic protection.

Alternate No. 1, at \$2.6 Million, does meet the purpose and need of the project, and will only provide a 5-year service life since further deterioration is not inhibited. Alternate No. 2, at \$26.0 Million, does meet the purpose and need of the project, and will provide 25 to 50-year service life and enhanced public safety. This alternate will not stop the current deterioration. Potentially, periodic small projects will be needed to secure loose or damaged FRP wrap. Both FRP suppliers that we spoke with cautioned us on the permeability of the FRP material. While both glass and carbon FRP wraps do have some permeability, it is not as great as exposed concrete. This may lead to further deterioration and higher rehabilitation cost in the future.

Alternate No. 2 has been broken down into smaller projects to meet the budget needs of the District. The recommended alternative is **Alternative No. 2C** based on addressing public safety, extending the service life of the bridge, and economic analysis.

Alternate No. 3 is at \$33.2 Million. While it may be the best solution for extending the life of the existing concrete for another 50 years, it does not meet our budget constraints.

All alternatives include the Maintenance Work Task 1 that were requested. A summary of Estimated Construction Costs is included in **Appendix A**. All estimates have been projected to construction in Year 2020.



Photo 1– North Elevation, Spans 4 through 6.



Photo 2– East Approach Spans Deck, Looking East.

II. PURPOSE & NEED

This project is being performed to restore the integrity of the bridge's concrete portions by arresting the deterioration of the concrete superstructure and substructure. On occasion, loose concrete has fallen, creating a hazard to the public safety below. In its most recent bridge inspection, the bridge, CUY-6-1456 (SFN 1800930) General Appraisal Rating was a **5** or **Fair** Condition. With this rehabilitation project, ODOT expects to maintaining the structure in good condition for a service life of 50 years.

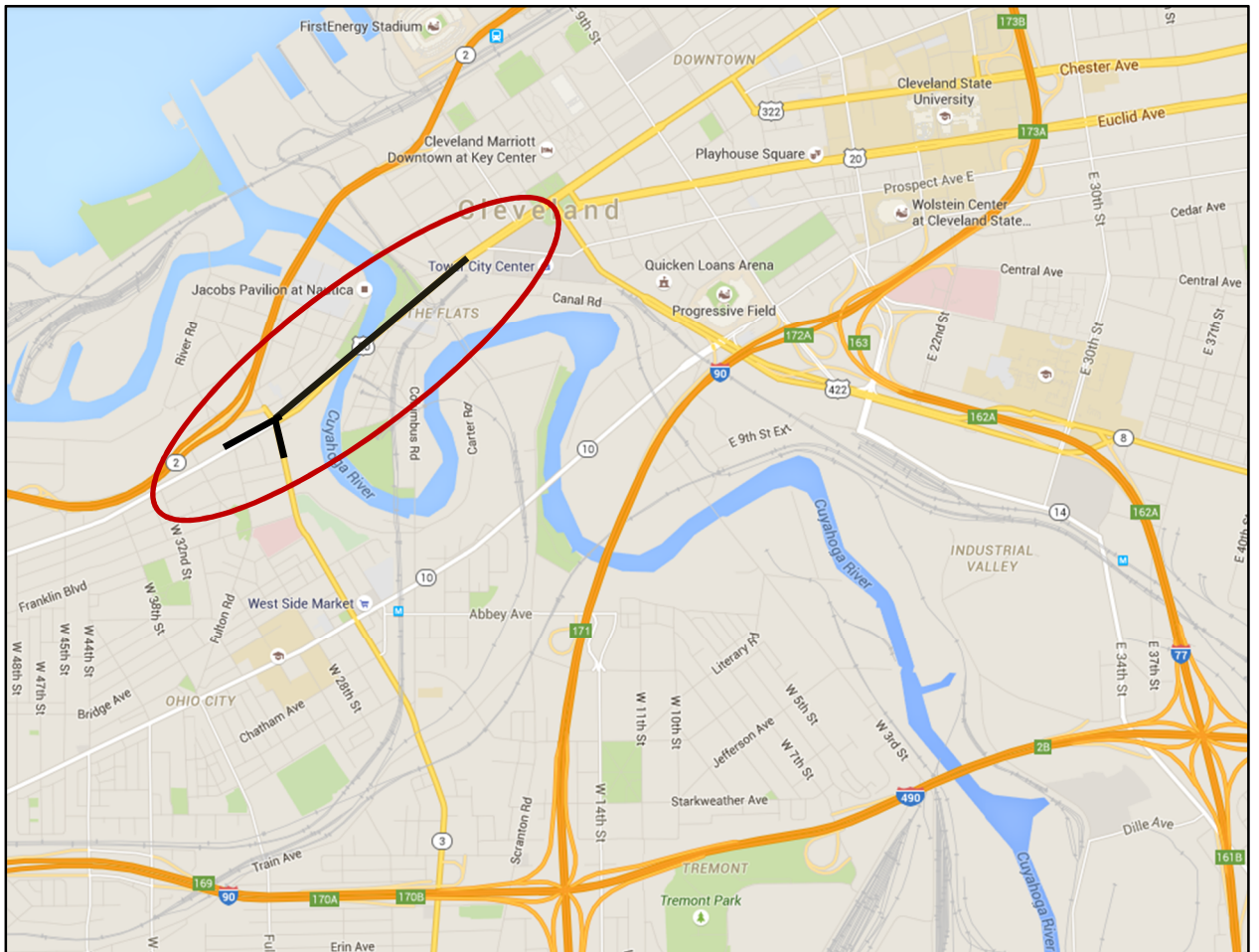


Figure 1 – Location of CUY-6-1456 (Circled).

Scope of Repairs

The repairs discussed in this feasibility study are as follows:

- Patching or replacement of the upper deck concrete wearing surface.
- Elimination of falling concrete over public areas.
- Investigation of FRP wrap on lower superstructure components.
- Continuation of repairs in the West Station, West 25th Street Tunnel and Detroit Avenue Tunnel.
- Placement of masonry block wall in Span 1A to prevent unauthorized access.
- Placement of a vandal resistant barrier to restrict unauthorized access from the Center Street Swing Bridge operator's car shelter to the Pier 4 pedestals.

Definition of Public Spaces

For this feasibility study, the defined public spaces below the structure are shown in **Appendix**

B. Areas designated as public space meet the following criteria:

1. Areas below or within 10 feet of concrete arch spans, and
2. Areas commonly occupied by vehicular and/or pedestrian traffic.

Following this guide, Span 1 and Span 4 are not considered public space. Following the recent announcement that the Cleveland Metroparks plan to create a new Irishtown Bend park, 75% of the area beneath Span 2 has been added to the public space inventory. ¹

¹ Cleveland Plain Dealer, *Port hires design team to envision transformation of Irishtown Bend*, February 9, 2017.

III. BRIDGE CONDITION

Bridge Description

CUY-6-1456 (SFN 1800930), commonly known as the Detroit-Superior Bridge and later renamed the Veteran's Memorial Bridge, is a 1917 double-deck structure carrying vehicular and pedestrian traffic over the Cuyahoga River Valley (**See Photos 1 & 2**). The bridge is approximately 2,880 feet long, including 1,673 feet of subway tunnel that is linked by the lower deck. In its original design, the upper deck carried vehicular and pedestrian traffic while the lower deck had four streetcar lines and capacity for two future tracks. The streetcar lines across the Detroit-Superior Bridge were discontinued in 1953. The Detroit-Superior Bridge is included on the National Register of Historic Places.

General plan and elevation views of the Detroit-Superior Bridge are included in **Figure 2**. **Figure 3** contains the typical nomenclature of the concrete elements of the main concrete spans.

The Detroit-Superior Bridge is composed of three distinct units. The first unit, the West Approach, is comprised of the West Station area spanning a total of 350 feet west of Tower A and two abandoned subway tunnels: the Detroit Avenue Tunnel (660 feet long) and the West 25th Street Tunnel (480 feet long). Several utilities are pass through the West Station and tunnels. Since the late 1980s, the West Station has been opened to the public for tours and festivals.

The main unit is Spans 1A, 1B and 1 through 13. Spans 1A and 1B are transition structures from the subterranean West Station to the double-deck approach and main spans. These two concrete cellular spans total 220 feet long and each has enclosed cellular construction below the lower deck.

The main spans, Span 1 through 13, are double-deck spans with vehicular and pedestrian traffic on the upper deck and utilities and maintenance access on the lower deck. Spans 1 through 3, 5 through 11 and Span 13 are concrete open spandrel arch spans, and Span 12 is a concrete encased steel half through arch. The main span, Span 4, is a 591-foot, three-hinged steel half-through arch truss in a Pratt configuration.

The third unit, the East Station, is a concrete cellular span that extends 165 feet past the East Abutment. A three panel long, cellular construction is present under the East Station lower deck immediately behind the East Abutment.

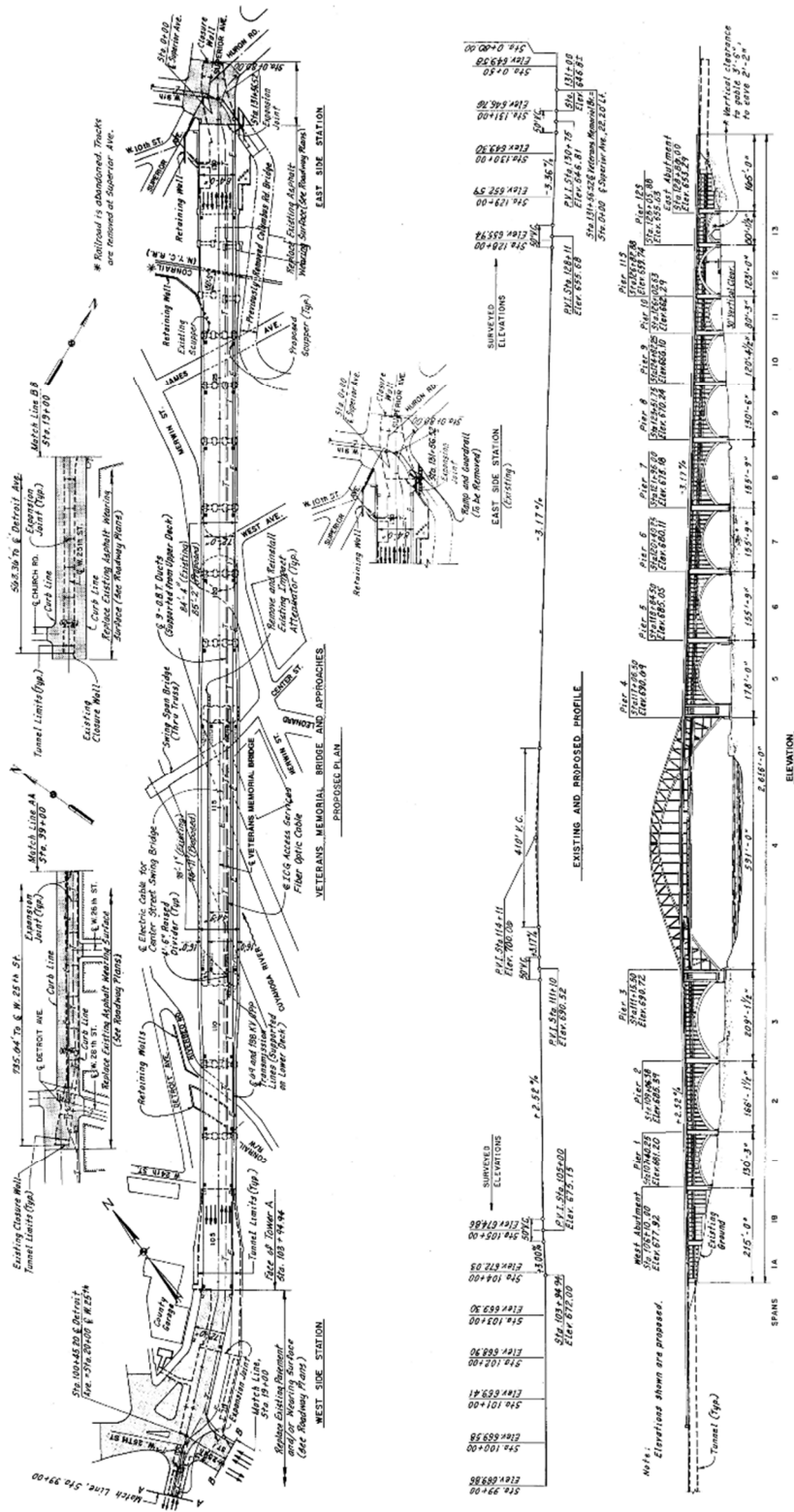


Figure 2 – CUY-6-1456 Plan & Elevation (Veterans Memorial Bridge Rehabilitation Plans, 1994).

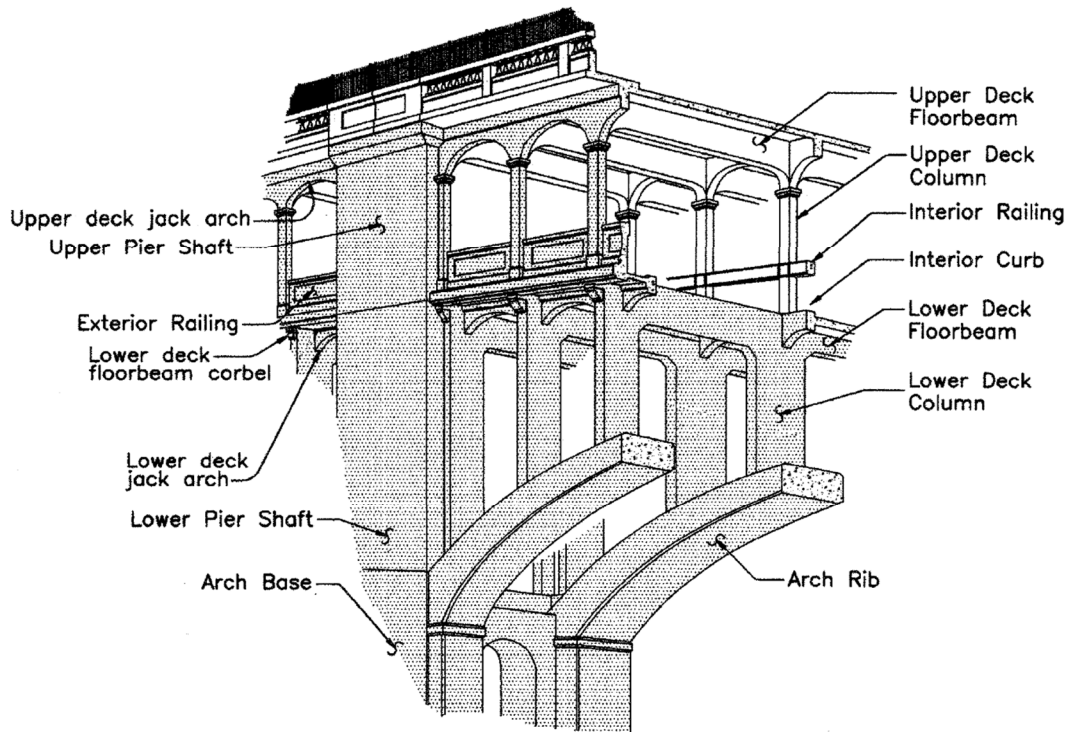


Figure 3 – Upper & Lower Deck Element Nomenclature, Approach Spans.

Inspection Procedure

Pennoni performed an in-depth inspection of the concrete components included in the scope of this feasibility study in conjunction with the 2016 in-depth inspection previously included in Project No. PID 93400 during September 13 through 16, 2016. Additional inspection was performed December 6 through January 10. Personnel included William J. Vermes PE, Christian Lunt, PE, Dale Arnold PE, Matthew Paroda EI, and Elizabeth Trapp, EI, Jessica Sizemore, EI and Alisha Ruff, EI. Inspection access was achieved as follows:

Detroit Avenue & W. 25th Street Tunnels – Extension ladders and delamtech sounding tool.

West Station – 30-foot electric manlift.

Spans 1-3, 5-13 Upper Deck superstructure – 40-foot electric manlift.

Spans 3, 5-12 Lower Deck superstructure – 80-foot diesel manlift and snooper.

East Station & Subway - Extension ladders and delamtech sounding tool.

Lighting in the tunnels, West Station and East Station and Subway was provided by two LED light stands, medium duty extension cords and a portable gasoline generator. Between October 6 and November 8, vandals destroyed the electric conduits and lighting in the West Station.

The presence, or lack of, top and bottom reinforcing steel was investigated in Spans 1 - 3 and 5 - 9 using a commercial metal detector.

Construction & Rehabilitation History

The Detroit-Superior Bridge was constructed from 1914 through 1917 to provide a high level vehicular and streetcar crossing over the Cuyahoga River, connecting the Ohio City community and Downtown Cleveland. The bridge replaced the Superior Viaduct, opened in 1878. Construction of the foundation began in 1913. The steel arch truss, Span 4, was erected from July 24 to November 6, 1915. On October 8, 1915, the two halves of the main truss were connected². Construction of the arch ribs began in May 1915 in Span 6 and proceeded eastward. The bridge opened to traffic on December 24, 1917.

By the mid-1930s, spalled concrete was occurring due to improper drainage. Repairs were discussed but postponed due to the needs of World War II, and ultimately not performed until the 1960s.

The Detroit-Superior Bridge has received a series of various major and minor rehabilitations as follows³:

1. 1967-70 Major Rehabilitation
 - a. Removal of the original upper deck consisting of four vehicular lanes and two 15-foot wide sidewalks.
 - b. Strengthening or replacement of all upper deck concrete floorbeams.
 - c. Span 4: Erection of new steel floorbeam cantilevers.
 - d. Construction of the new upper deck with six vehicular lanes and two five-foot wide sidewalks.
2. 1995-97 Major Rehabilitation
 - a. Replacement of the upper and lower deck floors.
 - b. Replacement of select upper and lower concrete floorbeams, columns, jack arches and pier shafts (**Table 1**).
 - c. Patching over 70,000 SF of concrete superstructure.
 - d. Application of epoxy-urethane or non-epoxy sealer to most exposed concrete surfaces.
 - e. Span 4: Replacement of all steel hangers, Panel Points 6 through 6'.
 - f. Replacement of Upper Deck and Lower Deck Floor Beams 5 and 5' and stringers.
 - g. Painting of all steel superstructure components.

² Beyer, William E, The History of the Veterans Memorial Bridge, 90th Anniversary Edition, Bookmasters, Inc, Ashland, Ohio.

³ Vermes, William J., Gasparini, Dario A. & Conley, Natalie, *Cleveland's Historic Bridges: Architectural & Engineering Masterpieces*, Publication of the 7th Historic Bridge Conference, Cleveland, Ohio, 2001.

- h. Installation of new drainage system.
 - i. Installation of architectural lighting.
3. 2003 North Sidewalk Linear Park Conversion.
- a. Conversion of vehicular traffic to two westbound and one eastbound lane between the steel trusses and on eastbound lane on the Span 4 south cantilever.
 - b. Widening of the north sidewalk. With longitudinal trench drainage.
 - c. Installation of public art and benches along the modified north sidewalk.

| Member | Total Members | Members Replaced | Total Percent Replaced |
|----------------------------|---------------|------------------|------------------------|
| Upper Deck Floor Beams | 686 | 316 | 38% |
| Upper Deck Columns | 693 | 179 | 26% |
| Upper Deck Jack Arches | 564 | 260 | 45% |
| Lower Deck Floor Beams | 548 | 50.5 | 11% |
| Lower Deck Corbels | 279 | 79 | 28% |
| Lower Deck Jack Arches | 520 | 176 | 34% |
| Lower Deck Columns | 488 | 8 | 2% |
| Upper Exterior Pier Shafts | 32 | 17.5 | 55% |
| Lower Exterior Pier Shafts | 28 | 5.5 | 20% |

Table 1 – 1995-97 Detroit-Superior Bridge Rehabilitation Concrete Superstructure Member Replacement Summary, Spans 1 to 3, 5 to 13 & East Station.⁴

4. 2014-16 Rehabilitation Work Summary

In 2014, a minor rehabilitation project began to address deteriorating concrete surfaces. Local patching was performed of the upper deck wearing surface. Significant and minor patching was performed on the lower deck superstructure and piers in Span 2 and from Span 7 to the East Abutment. In the West Station, four columns, C13, C14, C20 and C21, were replaced in kind along with patching from

⁴ Vermes, William J., *Rehabilitation of The Detroit-Superior Bridge*, Proceedings of an International Conference on Historic Bridges to Celebrate the 150th Anniversary of the Wheeling Suspension Bridge, West Virginia University Press, 1999, pp. 117-132.

column lines 25 to 31. Painting of the Span 4 superstructure between the upper and lower deck was also performed.

Work for this rehabilitation was suspended in early 2016 to reassess the repair needs of the structure and address safety concerns in public areas below the bridge. For the remainder of this report, the 1995-97 and 2014-16 rehabilitations will be referred to as the 1995 rehabilitation and the 2014 rehabilitation, respectively.

IV. STRUCTURE REPAIR NEEDS

Discussion of repair needs begins with maintenance repairs of Alternate No. 1. The work tasks associated with the deterioration of the concrete superstructure and public safety below the bridge is discussed as each repair need is approached, west to east and top to bottom.

Upper Deck Wearing Surface

The upper deck wearing surface was poured in 1995 and placed into service January 1997. Records show the wearing surface began exhibiting significant deterioration after 2010. Following patching in 2014, the wearing surface continued to deteriorate at increasing rates, especially in Spans 7 through 10 (**Table 2**). Soundings showed that the delamination patterns generally follow the wheel paths. Further observations show that the deck is subjected to impact loads as commercial trucks cross the bridge, especially east bound traffic, at speeds greater than the posted speed limit. At 20 years, the overlay is nearing the end of the expected service of 25 years. Because the rehabilitation project is scheduled for start in 2019, removal of the deficient wearing surface via hydro-demolition and placement of a micro-silica wearing surface is the recommended repair for the wearing surface. Since few signs of distress are present on the upper deck underside are present, no deck cores are recommended.

| Span | Wearing Surface Deterioration (SF) | | WB Area of Deck (SF) | EB Area of Deck (SF) | Concrete Repair (%) | | |
|--------------|------------------------------------|------|----------------------|----------------------|---------------------|-------------|-------------|
| | WB | EB | | | WB | EB | Total |
| Span 1A | 36 | 128 | 2890 | 2890 | 1.2 | 4.4 | 2.8 |
| Span 1B | 81 | 162 | 3607 | 3607 | 2.2 | 4.5 | 3.4 |
| Span 1 | 450 | 627 | 3718 | 3718 | 12.1 | 16.9 | 14.5 |
| Span 2 | 0 | 0 | 4685 | 4685 | 0.0 | 0.0 | 0.0 |
| Span 3 | 56 | 59 | 6368 | 6368 | 0.9 | 0.9 | 0.9 |
| Span 4 | 1495 | 2441 | 17228 | 17228 | 8.7 | 14.2 | 11.4 |
| Span 5 | 0 | 19 | 5186 | 5186 | 0.0 | 0.4 | 0.2 |
| Span 6 | 259 | 8 | 4191 | 4191 | 6.2 | 0.2 | 3.2 |
| Span 7 | 1367 | 664 | 4117 | 4117 | 33.2 | 16.1 | 24.7 |
| Span 8 | 1724 | 1792 | 4170 | 4170 | 41.3 | 43.0 | 42.2 |
| Span 9 | 814 | 354 | 3698 | 3698 | 22.0 | 9.6 | 15.8 |
| Span 10 | 642 | 754 | 3688 | 3688 | 17.4 | 20.4 | 18.9 |
| Span 11 | 76 | 360 | 2864 | 2864 | 2.7 | 12.6 | 7.6 |
| Span 12 | 108 | 229 | 3444 | 6642 | 3.1 | 3.4 | 3.3 |
| Span 13 | 28 | 0 | 2245 | 4331 | 1.2 | 0.0 | 0.4 |
| East Station | 44 | 0 | 8904 | 17172 | 0.5 | 0.0 | 0.2 |

Direction Subtotals: **7,180** **7,597** **81,003** **94,555**

Total: **14,777** SF

Total % Deteriorated = **8.42%**

Table 2 – Upper Deck Wearing Surface Deterioration Summary



W. 25th Street & Detroit Avenue Tunnels

The tunnels have received little rehabilitation during their service. Intermittent spalls present along the wall bases have changed little since the late 1980s, and may be caused by acidic ballast used for the street car lines but now removed since the 1950s. Wall deterioration is primarily located at the wall panel joints. The roof of the West 25th Street Tunnel exhibits little delamination. The original roof of the Detroit Avenue Tunnel is heavily spalled, however a new structural slab was placed above this slab during the 1995 rehabilitation. Since this is not a public area when the West Station is open to the public, no repair to the Detroit Avenue Tunnel is recommended.

West Station Columns & Jack Arches

Due to budgetary reasons, only essential repairs were performed in the West Station and tunnels during the 1995 rehabilitation. Since then, deterioration of the West Station columns and longitudinal beams (jack arches) has steadily increased despite repair of the roof slab and placement of a Type 2 waterproofing membrane.

Most West Station deterioration is present on the jack arches and columns of Lines A, B, C and D, roughly centered on the expansion joint and sag point between Columns 20 and 21. Location of deterioration is included in **Appendix F**. As shown in **Appendix G**, the deterioration has been steadily migrating east and west from this centroid of corrosion.

Along the north face of the Line A jack arches, a longitudinal construction joint has allowed water and salt infiltration, resulting in accelerated deterioration of the jack arches and columns below (**Figure 4**). This construction joint is part of the West Station original construction to facilitate a new rail line and expansion of the station northward.

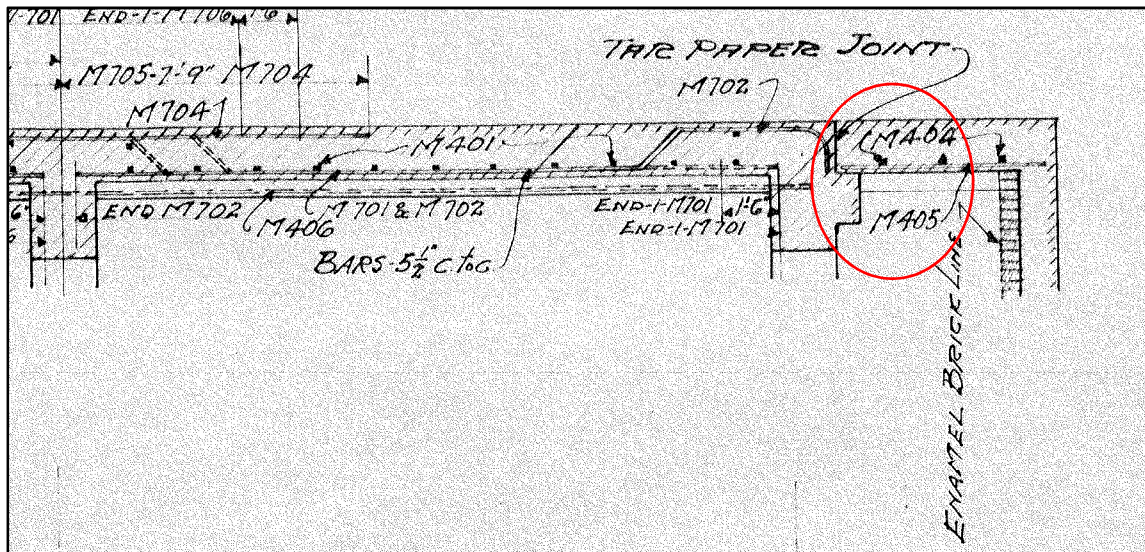


Figure 4 – Longitudinal Construction Joint (Circled, referenced as Tar Paper Joint), Above Line A North Face, Original Construction Drawing No. A2246.

Lower Deck Columns

The cause and magnitude of deterioration present among the lower deck columns is based on the column location. Away from the piers, spandrel columns have isolated delaminations and spalls commonly due to corrosion of the 1/2-inch square horizontal square bars. Several exterior columns have larger deterioration areas due to corrosion of the main steel reinforcement with 3-inch cover. On several exterior columns, lower deck corbel deterioration has propagated to the adjoining column surfaces below.

For the lower deck columns adjacent to piers, several columns have large delaminated surfaces likely due to the chloride contamination up through the beginning of the 1995 rehabilitation. The column surfaces facing the piers patched in 1995 are often delaminated now due either to continuing reinforcement corrosion or the insufficient space to perform proper shotcreting.

Estimated FRP lower column wrap quantities are based on the surface area from top of the arch pedestal up to the bottom of the lower floorbeam fillet. Following this delineation of the lower columns, any column less than two feet tall or non-existent at the center of the arch rib, are assumed to be too short to merit FRP wrapping and are not included in the quantities. Observation of the column pedestals showed no deficiencies, likely due to the increased reinforcement cover they provide. No FRP wrap of the pedestals is recommended due to durability and complexity of wrapping.

Lower Deck Floor Beams

During the 1995 rehabilitation, most lower deck floorbeam patching was for shallow (cover less than 1") over stirrup reinforcement. Now, new delaminations and spalls have occurred where stirrup cover is 1 1/4 to 1 1/2 inches, indicating that the corrosion mechanism has not stopped with the applied sealer (**Photo 3**). Elsewhere, ongoing corrosion of the bottom tensile reinforcement has resulted in 1995 several shotcrete patch failures, as the patches have been forced from the floorbeam bottoms (**Photo 4**). With the likelihood of eventual global concrete corrosion, it is recommended that FRP anchors be placed along the top of lower floorbeams to prevent a full-face failure of the wrap.

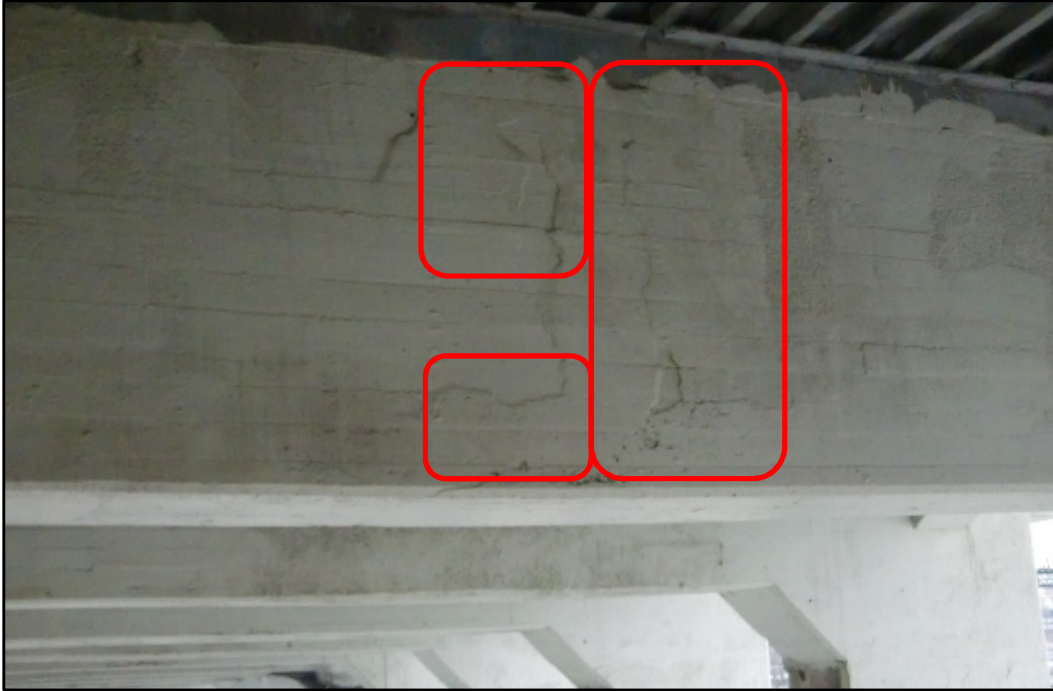


Photo 3 – Newly Developing Lower Deck Floor Beam Delaminations (Circled), South Bay, Span 8.



Photo 4 – Reinforcing Steel with Active Corrosion, Lower Deck Floorbeam 14, South Bay, Span 6.

Lower Deck Corbels

The lower deck corbels perform as part of a structural cantilever of the lower deck floor beams, supporting the upper deck columns and loads above. During the 1995 rehabilitation, 20% of the corbels were replaced. Currently, additional corbels have delaminated or spalled primarily due to the following causes:

1. Lack of Cover: One architectural feature of the corbels is that they are stepped down two inches on each side, thus providing significantly less cover for the slanted vertical anchorage reinforcement of the upper deck columns.
2. End Span Lower Deck Corbels: During the 1995 rehabilitation, construction of new corbel and/or lower deck exterior pier shafts used a thin felt bond breaker fabric between the adjoining surfaces (**Photo 5**). This bond breaker has not performed adequately, resulting in spalls in either the corbels, lightly reinforced pier shafts, or both. The first occurrences of this failure mode appeared by 2000 and have been steadily progressing since.

Replacement and/or patching of deficient corbels will be performed. Adjacent to the pier shafts, all corbel/pier shaft interface will be modified, regardless if repair is needed or not. A $3/8$ -inch paraffin bond breaker is recommended to be placed between the concrete surfaces.

Arch Ribs

The arch ribs exhibit spalls and isolated delaminations and spalls along the corners of the arch ribs (**Photo 5**). Additional delaminations are present on the intrados (underside) of the arches. Generally, no deterioration is present along the arch ribs side since no shear reinforcement is present throughout the arches. Furthermore, the field inspection verified that contrary to the original construction plans, top and bottom mat steel was placed continuously in the arches of Span 1 through 3, 5, and 7 through 9. In Span 6, however, no main reinforcement was detected in the North Exterior and Interior arch ribs between Columns 3 and 5, and Columns 11 and 13. Span 6 was the first concrete span constructed, and therefore likely the only span to have discontinuous reinforcement.

Lower Deck Pier Shafts

Most upper deck pier shaft and some lower deck pier shaft were replaced during the 1995 rehabilitation. Generally, the exterior lower deck pier shafts have little deterioration except for two occurrences. First, areas cast in concrete with the insufficient bond breaker have spalled due to thermal movement of the adjacent spandrel column (**Photo 6**). Next, on the Pier 6 South Exterior Lower Pier Shaft, a 140 SF spalled area exhibits an apparent deep scaling.

This is likely a due to failure of the original encased drain pipe within this shaft. It is anticipated sound concrete is not present until at least a depth of two feet.
(Photo 7 & Figure 5).



Photo 5 – Spalled Original Concrete & Secure 1996 Shotcrete Patch, Span 7 South Interior Arch Rib.



Photo 6 – Spalled & Loose Concrete Due to Ineffective Bond Breaker (Location denoted in yellow), Pier 5 Lower Deck Pier Shaft & South Lower Deck Corbel 1, Span 6.



Photo 7 – Deep Concrete Deterioration, Pier 6 South Lower Deck Pier Shaft.

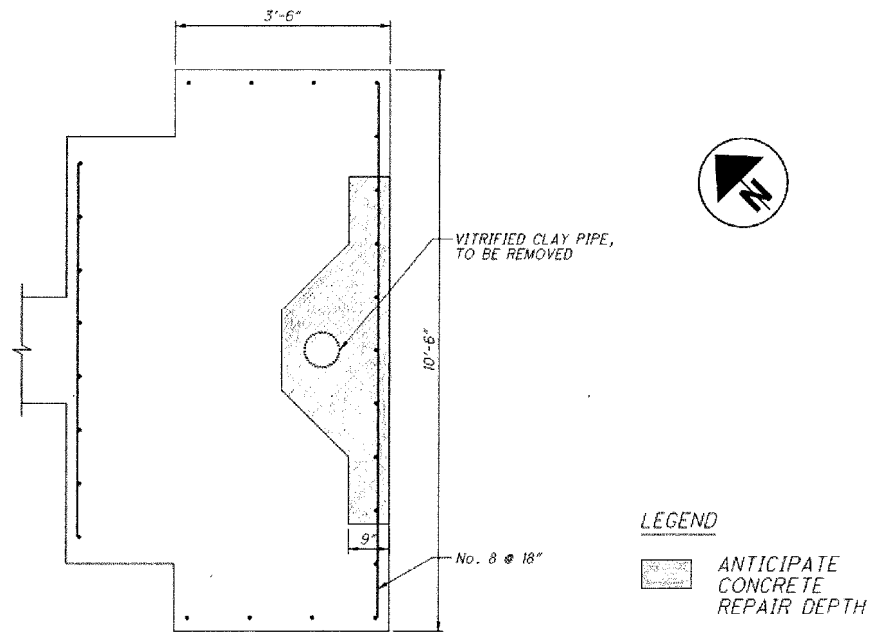


Figure 5 – Estimated Deterioration Depth, Pier 6 South Lower Deck Pier Shaft.

East Subway

Column M22, located along the north wall of the East Subway, adjacent to the compression seal deck joint between the East Station and the East Subway, has more than 60% section loss (**Photo 8**). Columns M27, East Subway, and South Exterior Column 20, also have advanced deterioration and require replacement. Approximately 30% of the north wall of the East Subway is spalled or delaminated, and requires patching.



Photo 8 – 60% Section Loss, Column M22, East Station.

Lower Deck Masonry Wall

Vandals have been accessing the lower deck and West Station increasingly the last several years along the southwest corner of Span 1A. Efforts to secure this area with chain link fencing and perforated steel plates have not been successful. More recently, vandals have set up step ladders at the northeast corner of Span 13 (**Photo 9**). The preferred method of securing the access to the lower deck via these points is placement of masonry block wall on top of the lower deck railing. The recommended location of the masonry block wall is shown in **Figure 6**.

Center Street Bridge Tender's Car Shelter

Within the last decade, a chain-link car shelter, measuring 17'-4" wide by 22'-6" deep with a roof, has been built adjacent to the west face of Pier 4. This shelter provides a secure parking area for the Center Street Swing Bridge operators. Vandals have accessed the interior of the shelter and pushed open a hole in the roof, gaining access to the south pedestal of Pier 4 and on up the Span 4 steel superstructure. Implementation of recent security measures on the Detroit-Superior and Lorain-Carnegie Bridges shows that construction of such features emboldens trespassers to damage and pass through these barriers. Therefore, it is recommended that instead constructing a vandal-proof fence atop of the shelter, the east half of the shelter be rebuilt, narrowing the shelter by four feet and removing trespasser access to the pedestal. This reduced shelter size is comparable to the bridge operator car shelter at the West 3rd Street Lift Bridge.



Photo 9 – Ladder Used by Vandals to Access Lower Deck, Span 13 at East Abutment.

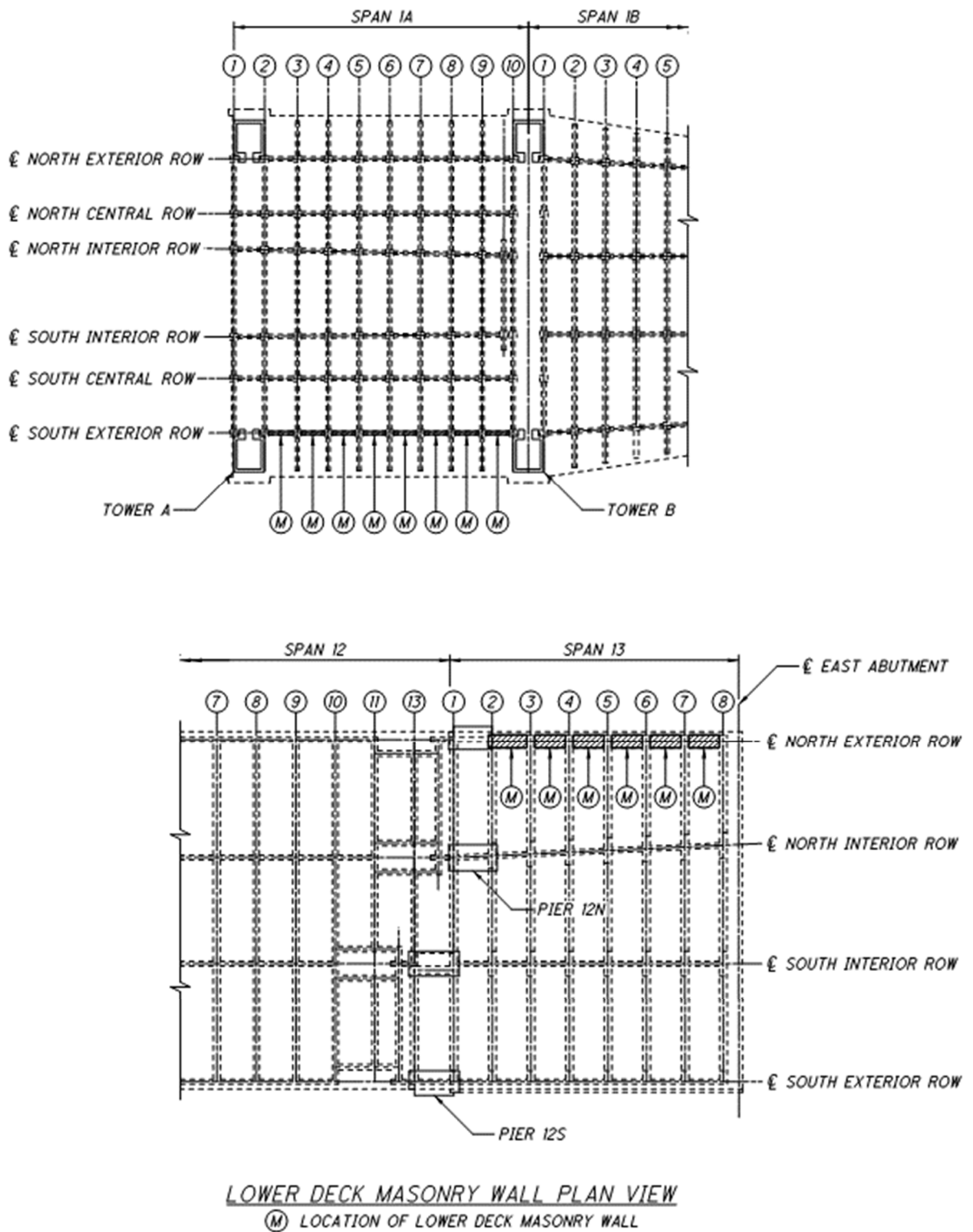


Figure 6 – Recommended Location of Security Wall.

V. RECOMMENDED REPAIR STRATEGIES

General

The field inspection revealed that the delamination currently present does not follow the common opinion that concrete patches tend to fail. Throughout the lower superstructure, few examples of shotcrete patch failure due to debonding are present. In fact, several areas shotcrete failure are due the continued reinforcement corrosion or failure of the adjacent original concrete, also from reinforcement corrosion.

During the 1995 rehabilitation, the epoxy-urethane sealer placed on all lower superstructure exterior and upper superstructure components as well as piers as a barrier protection, is mostly intact after nearly 20 years of exposure. However, the sealer at best only slowed the rate of corrosion within these concrete elements, including those that have not been subjected to poor drainage and chlorides attack.

Thirteen concrete pH tests were performed on samples obtained from various delaminated lower superstructure elements (**Table 3 & Appendix C**). Several samples exhibited pH levels less than 12, suggesting that the passivation layer protecting the steel reinforcement has been broken due to hydroxide ion transfer, resulting in concrete corrosion. Due to the random nature of the pH results, it is not possible to conclusively determine if carbonation is the cause for the pH lower pH readings.

| Sample No. | Span | Member | Location | Material | Predominant pH Level | | Comments |
|------------|------|-----------------------|----------------|-----------|---------------------------------------|--------|----------------------------------|
| | | | | | Near Surface | Int. | |
| 1A | 7 | Arch Rib | South Interior | Concrete | 9 - 10 | 9 - 10 | Bottom North Corner, near center |
| 1B | 7 | Arch Rib | South Interior | Shotcrete | 9 | 12 | Bottom North Corner, near center |
| 2 | 7 | LD Floor Beam | 4 North Bay | Shotcrete | 9 | 9, 12 | |
| 3 | 7 | LD Column | N. Int. 14 | Concrete | 9 | 12 | |
| 4 | 8 | Jack Arch | N. Int. 8-9 | Shotcrete | 9 | 9, 12 | |
| 5 | 8 | LD Floor Beam | 9 Center Bay | Concrete | 10 - 11 | 9 - 12 | 1 1/2" cover total |
| 6 | 8 | LD Floor Beam | 10 Center Bay | Concrete | 10 - 11 | 9, 12 | 2 1/2" cover total |
| 7 | 8 | LD Floor Beam | 11 Center Bay | Concrete | 10 - 11 | 9, 12 | 2 1/2" cover total |
| 8 | 8 | LD Floor Beam | 14 South Bay | Concrete | 9 - 10 | 12 | |
| 9 | 9 | LD Column | N. Int. 13 | Concrete | Aggregates: 10-11 Sand & Cement: 9 | | West Face |
| 10 | 10 | LD Floor Beam | 1 South Bay | Shotcrete | Mostly 12; Some aggregates, 9 | | |
| 11 | 10 | LD Floor Beam | 2 South Bay | Concrete | Aggregates: 10-11 Sand & Cement: 9 | | From above Sample No. 10 |
| 12 | 10 | LD S. Ext. Pier Shaft | West Face | Shotcrete | Mostly 12; Some aggregates, 9 | | West face, near corbel |

Table 3 – Concrete pH Tests Summary

Appendix D contains both a summary and estimated patching quantities calculations for superstructure and pier elements. **Appendix E** contains a summary of the estimated FRP wrap quantities and the associated calculations.

Discussion of the recommended structural repairs materials are divided among specific objectives: repair, protection and prevention. Each material is discussed as follows:

Concrete Patching/Replacement Materials (Repair)

Concrete patching shall be prepared, formed and finished in accordance with Item 519. Concrete members that are identified to require complete replacement including select columns, West Station beams and lower deck corbels shall be in accordance with Item 511. Recognizing the varying level of effort for patching or repairing concrete elements of the Detroit-Superior Bridge, the following repair/replacement items have been included in the

rehabilitation quantities. For cost estimating, concrete patching has been divided among the following items:

- Patching Concrete Structure: West Station, Tunnels and Upper Deck Superstructure
- Patching Concrete Structure: Lower Superstructure, Vertical Surfaces
- Patching Concrete Structure: Lower Superstructure, Bottom & Curved Surfaces
- Patching Concrete Structure: Deep Pier Shaft Deterioration
- Concrete, Misc.: West Station Concrete Beam Replacement
- Concrete, Misc.: Column Replacement
- Concrete, Misc.: Lower Deck Corbel Replacement

Fiber Reinforced Polymer Wrap (Protection)

Fiber reinforced polymer (FRP) wraps are composite systems made up of a glass fiber or carbon fiber material woven into sheets and saturated with a polymer bonding liquid (typically a two-part epoxy resin) and adhered to a concrete surface. Carbon fiber weaves generally have a higher unit tensile strength (100 ksi to over 200 ksi) with glass fiber weaves generally ranging from 30 ksi to 100 ksi. Due to their high tensile strength, FRP wraps are engineered to act as external reinforcement. Woven sheets may be engineered as unidirectional (designed to carry load in one direction) or bidirectional (designed to carry load in two or more directions). Containment is the primary consideration for FRP wrapping on this project to prevent future concrete delaminations from becoming dislodged and falling on public areas below the concrete arch spans. ODOT Central Office has a list of fiber wrap materials independently evaluated by ICC-ES.

Three options for applying the FRP wrap to the arch ribs over public areas have been developed (Figure 7). In each option, the FRP wrap must extend past a suspected future delamination area with a development length onto sound concrete. Generally, FRP wraps need a development length of one to two feet past concrete that will remain sound. If the FRP wrap is not developed correctly, a delamination could form and simply take the FRP wrap with it. As discussed previously, FRP wrap is not recommended on the lower deck column bases. Due to the structural nature and past corrosion history, placement of preformed shields over the lower deck corbels is recommended instead of application of an FRP wrap. Proposed areas of the FRP wraps on the lower pier shafts is shown in Figure 8.

Option No. 1 provides confinement of the arch intrados and extends upward on the sides with 1'-6" of adhesion development past potential corner spalls. This option provides containment for the areas of the arch ribs that would be most likely to fall.

Option No. 2 adds top corner FRP strip wraps as a means of containing edge spalls. This option does not cover the entire extrados because:

1. Inner extrados spalls are rare and when present, and are less likely to fall to the ground below, and

2. Greater surface preparation is required due to its very irregular surface.

Option No. 3 is a U-wrap of the arch ribs with development across two feet past the top corner. This option includes approximately 45,000 square feet of FRP wrap over Option No. 2.

Due to both coverage of the rib areas prone to spalling and overall economy, the quantities of Option No. 2 have been included in the development of the Alternative No. 2 cost estimate.

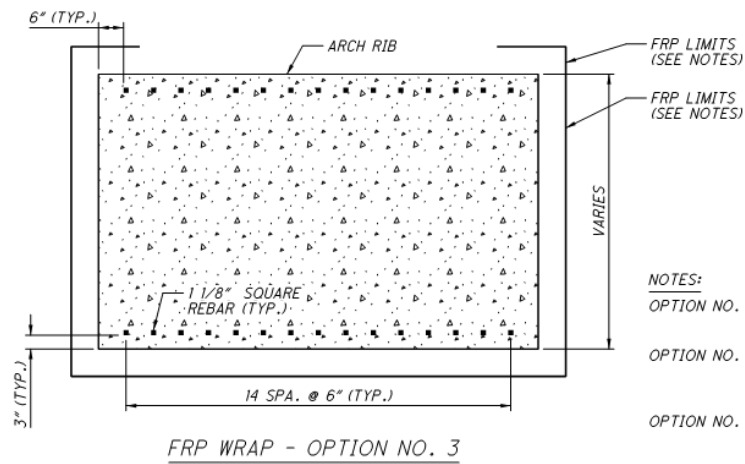
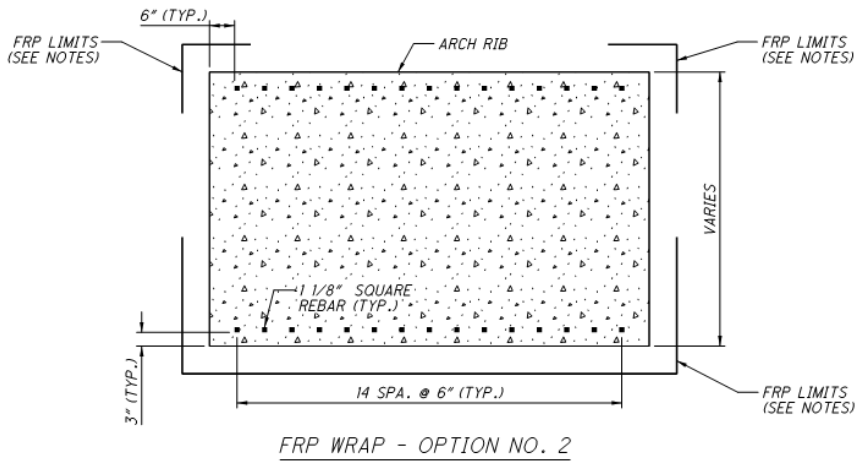
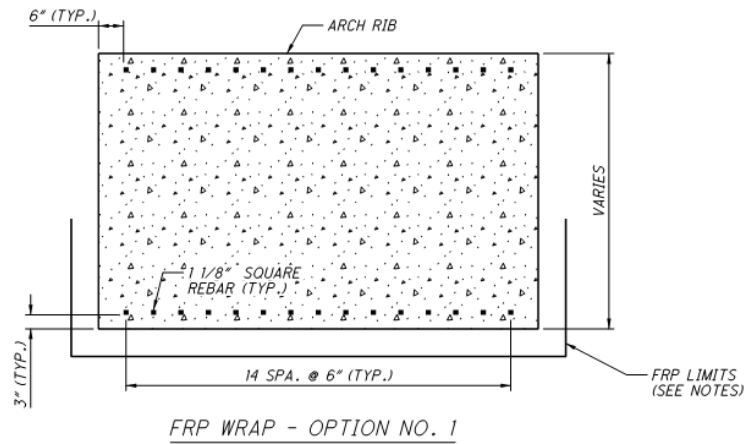
Surface preparation and installation of the FRP wrap systems vary from one manufacturer to another and among manufacturers' systems but some generalizations may apply. In the design of the FRP wrap system the bond between the existing concrete and the composite wrap is critical. Surface preparation of the existing concrete is important. Generally, the surfaces must be clean and free of contaminants and debris that would be detrimental to the bond between the wrap and the concrete. On this project, the existing epoxy-urethane sealer will need to be removed before the FRP wrap is installed. Another important issue is the profile or smoothness of the concrete surfaces. While some waviness, curvature or other unevenness of the concrete surface may be acceptable, sudden and abrupt changes in the surface profile and sharp corners greater than $1/16$ -inch are not acceptable. Sharp corners can tear the fabric during installation and surface profile irregularities can create air pockets under the FRP wrap.

The American Concrete Institute has surface profile specifications that some FRP wrap manufacturers reference. Generally abrupt surface profile changes or ridges larger than $1/16$ " are not acceptable. In the case of this project the arch rib sides are smooth but the top and bottom are generally not. The bottom surface of the arch ribs was formed using boards laid transversely. In some areas, the form boards did not butt up perfectly and the bottom surface of the concrete exhibits a stepped profile with ridges measuring up to $1/2$ -inch tall. These bottom surface irregularities will need to be remedied by some combination of grinding and or an epoxy paste applied to the ridges. The top surface of the arch ribs was roughly finished and has scattered debris embedded. The top surface irregularities will be addressed by some combination of mortar, grinding or epoxy paste. Finally, the corners between surfaces may require some grinding to provide a smoother corner. The existing concrete coating removal and surface profiling will take time and represents a significant portion of the final complete installed cost of the FRP wrap system.

Installation of the fiber sheets varies from one manufacturer to another and among manufacturers' systems but generally involves saturating the fiber sheets with resin either before or after applied to the concrete surface. Bubbles and voids under the fiber sheets are removed by rolling before the epoxy resin cures. After the FRP wrap is installed, epoxy-urethane sealer should be applied to provide UV protection for the fiber sheets and to the

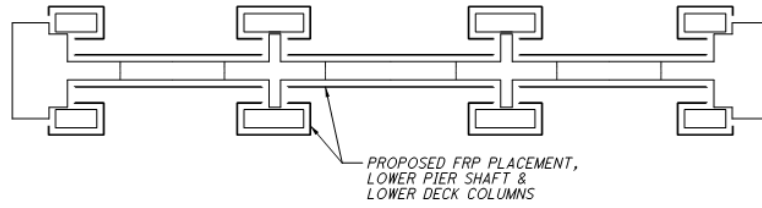
match the color of the existing sealer on adjacent unwrapped areas. The epoxy-urethane sealer may be applied to the FRP wrap areas as they are curing and still tacky. If the epoxy-urethane sealer is applied after the FRP wrap has cure, the surface of the FRP wrap may require a light sanding or roughening for the epoxy-urethane sealer to bond properly.

The FRP wrap will be relatively impervious and moisture becoming trapped in the wrapped concrete is a concern. Gaps up to 1" wide between the fiber sheets will be provided to give moisture inside the concrete a chance to escape.

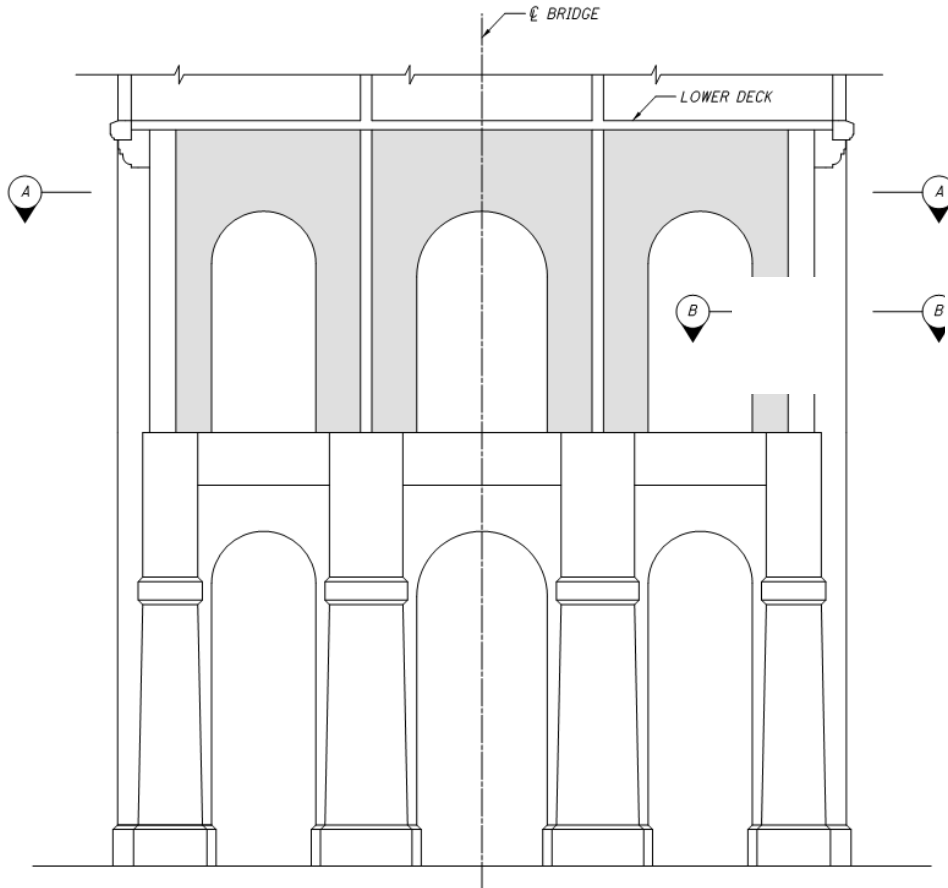


- NOTES:**
- OPTION NO. 1 - FRP Wrap INCLUDES FULL UNDERSIDE AND 2'-6" OF SIDES.
 - OPTION NO. 2 - FRP Wrap INCLUDES FULL UNDERSIDE AND 2'-6" OF SIDES AND 1'-6" OF TOP CORNERS.
 - OPTION NO. 3 - FRP Wrap INCLUDES FULL UNDERSIDE AND SIDES AND 1'-6" OF TOP CORNERS.

**Figure 7 – Feasible FRP Wrap Options on Arch Ribs
(Note: Arch height not to scale.)**



SECTION A
PIERS 5-10 SHOWN,
PIERS 3, 4, 11 & 12 SIMILAR



TYPICAL PIER ELEVATION
PIERS 5-10 SHOWN,
PIER 3, 4, 11 & 12 SIMILAR
(LOOKING EAST)

LEGEND
 FRP WRAP

Figure 8 – Proposed FRP Wrap Placement, Lower Pier Shafts.

Research published in 2002 and 2006 concluded that while FRP wraps slow the rate of reinforcement corrosion due to chloride attack, FRP wraps do not stop corrosion. An example of active concrete corrosion within a confining FRP application is present at the bridge carrying Fulton Road over I-71 (Photo 10). Furthermore, Section 1.2.1 – General of AASHTO’s *Guide Specifications for Design of Bonded FRP Systems for Repair and Strengthening of Concrete Bridge Elements* (First Edition, 2012) states the following:

The application of FRP systems will not stop the ongoing corrosion of existing steel reinforcement. The cause of corrosion to internal steel reinforcement should be addressed and corrosion-related deterioration should be repaired prior to application of any FRP system.

For the above reasons, a passive cathodic protection system following ODOT’s *Supplemental Specification 844 – Concrete Patching with Embedded Anode Protection* has been included in the Alternate 2 cost estimate.



Photo 10 – Active Concrete Corrosion Beneath FRP Wrap, Pier 1, CUY-71-1679 (Fulton Road over I-71).

Cathodic Protection – Impressed Current (Prevention)

A third means of concrete protection, active cathodic protection, is a technology that has been developing since the 1970s. Active cathodic protection systems include impressed current, chloride extraction, realkalization and thermally sprayed zinc coating. Each method of cathodic protection has its strengths and weaknesses.

Alternate 3 includes an estimated cost of an impressed current cathodic protection system in lieu of a FRP wrap and a passive galvanic anode form of cathodic protection. Of the active systems, impressed current is the most common. Impressed works by neutralizing the electric current flowing through the subject reinforcing steel that produces the corrosion mechanism. However, prescription of an appropriate active cathodic protection system can best be determined with additional and proper concrete testing.

VI. MISCELLANEOUS ASSESSMENTS

Right-of-Way Impacts

Properties that will require temporary right-of-way easements during construction, and are summarized in **Tables 4 and 5**. The costs associated with them do not include damages. Several of the properties impacted are parking lots. The temporary loss of parking revenue is not included in the costs but we have included a table summarizing the current cost to park along with the number of spaces that will be impacted.

| Property Owner | Parcel No. | Temporary Access (SF) | Temp. Access Cost (per SF) | COST |
|---|------------|-----------------------|----------------------------|----------|
| Stonebridge Waterfront, LLC | 003-20-008 | 5,653 | \$1.75 | \$9,900 |
| No Information (Newly created Parcel) | 003-20-009 | 656 | \$1.75 | \$1,150 |
| Board of Park Commissioners of the Cleveland Metropolitan Park District | 101-15-002 | 26,445 | \$1.75 | \$46,300 |
| City of Cleveland | 101-15-021 | 33,264 | \$1.75 | \$58,250 |
| Flats East Development LLC | 101-15-009 | 14,245 | \$1.75 | \$25,000 |
| Greater Cleveland Regional Transit Authority | 101-15-028 | 908 | \$1.75 | \$1,600 |
| United States of America | 101-15-011 | 4,348 | \$1.75 | \$7,600 |

Table 4 - Temporary Right-of-Way Impacts

| Span | Lot Owner | Estimated No. of Parking Spaces Impacted | Daily Rate | Notes |
|------|-------------------------|--|------------|--------------------|
| 3 | Stonebridge Properties | 30 - 35 | --- | |
| 5 | Cleveland Metroparks | 33 | \$3.00 | |
| 6 | Cleveland Metroparks | 15 | \$3.00 | |
| 8 | Canal Basin Parking Lot | 15 - 18 | \$2.00 | Open Monday-Friday |
| 9 | Canal Basin Parking Lot | 45 | \$2.00 | Open Monday-Friday |
| 12 | US Parking | 6 | \$4.00 | |
| 13 | US Parking | 34 | \$4.00 | |

Table 5 - Parking Lots Impacted

Maintenance of Traffic

Maintenance of Traffic (MOT) during repair work will be handled the same way regardless of the method of repair both for deck work and below deck work. Conceptual MOT drawings are included in **Appendix H**.

Deck: With the recommended wearing course replacement, MOT will be handled by closing one to two lanes at a time on the bridge, providing for part-width removal of the existing wearing surface and placement of the new. Given the proximity to the West 25th Street intersection and the West 9th/Superior/Huron intersection, the recommendation will be to position traffic for the lane closures prior to the intersections as shown in **Appendix B**.

Beneath the Bridge: Repair work on the piers and lower deck will be on Spans 2, 3, and 5 through 13 as indicated on the Public Areas Exhibit in **Appendix B**. Contractor access will be via manlift on the ground beneath the bridge. This will result in the following:

Span 2 – Riverbed Road will be closed for duration of work. Coordination with the Irishtown Bend Park development will be performed.

Span 3 –The closure of a portion of the parking lot for contractor access and equipment will be required. Work will be performed between the hours of 9:00 AM and 3:30 PM to minimize disruption to the residents.

Span 5 – Cleveland Metroparks Parking lot. Lot will be closed for duration of the work of the work above.

Span 6 - Cleveland Metroparks Parking lot. Lot will be closed for duration of the work of the work above.

Spans 6 and 7 – Public Roadways Merwin Avenue and West Avenue will be closed for the duration of work as shown in **Appendix B**. Pedestrian traffic will be maintained or detoured as needed.

Spans 8 and 9 – Portions of the parking lots will be closed for the duration of the work.

Span 10 – Pedestrian traffic will be detoured.

Span 11 – RTA Waterfront line – Coordination with GCRTA will take place to determine the best approach to maintaining rail traffic during repair work.

Span 12, Robert Lockwood Drive – There are several possibilities for maintaining traffic on Robert Lockwood Drive during construction. They include two way one lane traffic with flagger 9:00 AM to 3:30 PM, otherwise open to traffic, or utilizing weekend closures. Coordination with the City of Cleveland are necessary.

Span 13 - The closure of a portion of the parking lot will be required.

Navigation Lighting

There are six navigation lights mounted on the bridge which hang below the lower deck. Four are 180° red lights marking the channel edge and two are 360° green lights marking the channel center. Pennoni visited the site December 9, 2016 and inspected the navigation lighting. The lights were raised and the globes were removed, verifying that the fixtures have power (**Photo 11**). A night time visit later also verified the lights are on though with inadequate illumination (**Photo 12**). Further investigation by an electrician is warranted to determine the cause, whether it be the lights or the power service. An evaluation will then be done to determine the feasibility of repair or if replacement is warranted. We will coordinate with ODOT personnel and an electrician to perform a more thorough inspection of the lights and power service.



Photo 11 - Power Verification of Navigation Light (West Edge of Channel, South Face shown).



**Photo 12 – Typical Ineffective Illumination of Navigation Light
(East Edge of Channel, South Face circled).**

RTA Waterfront Line

The RTA Waterfront Line under Span 11 is constructed with concrete ties, has an overhead catenary system utilizing 600V DC, signal equipment on and around the track and a glass station north of the bridge. Once repair sites on finalized, coordination with the GCRTA is required. Conformance to RTA standards and specifications along with submitting proper request forms are required. Access within this area may be restricted to hours when the line is not in use, normally 11:00 PM to 6:00 AM although these hours would reduce during special events. A special event is defined as any event expected to draw 3,000 or more spectators to an area located within ¼ mile of an RTA Waterfront Rail Line.

VII. CONCEPTUAL ALTERNATIVES

Three alternates have been identified that would meet the purpose and need of the project. The criteria these alternatives should be judge by is the following:

1. Public Safety
2. Extend the life of the bridge for 50 years
3. Cost

Alternates No. 1 will maintain the structure in **Fair** condition. Alternates Nos. 2 and 3 will maintain the structure in **Satisfactory** condition or better.

Cost estimates have been extrapolated from current estimates to July 1, 2020 using ODOT's 2017-2021 Business Plan Inflation Calculator.

Alternative No. 1

This alternate project includes general maintenance work such as removal of loose overhead concrete in and around the defined public spaces, fixing the broken drain pipes at Pier 2 & 3. The upper deck that was replaced in the 1995-97 rehabilitation is showing signs of accelerating deterioration. It is recommended that the top 1 1/4" of the deck be removed by hydro demolition and a new micro silica wearing surface be placed. This will extend the life of the deck for another 25 years.

Currently, the Center Street Bridge tender has a fenced enclosure at Pier 4. This enclosure abuts Pier 4 and allows vandals to access the steel superstructure. It is proposed the enclosure be reduced in size and pulled away from the pier. This should prevent vandals from using the enclosure to access the pier. Additionally, the proximity of south face of Span 1A and the north face of Span 13 to the ground line allows vandals to enter the lower deck area with minimal effort. Currently, supplemental fencing has been unsuccessfully used to prevent entry onto the lower deck. These areas will be blocked up using concrete masonry units (CMU) to create a barrier. The CMU's will receive a mortar coat and a graffiti-resistant sealant.

The repair of the Navigation Lights will be further investigated. Although all are on during the night, the brightness of the lights is ineffective.

While Alternative No. 1 would provide a temporary solution to the falling concrete, it does not provide for future spalling and deterioration. This option does not extend the life of the structure.

This alternate is estimated to cost \$2,569,000.

Alternative No. 2

As with Alternative No. 1, all general maintenance items including the hydro-demolition and overlay of the upper deck will be included in Alternative No. 2. Alternative No. 2 introduces new major work items including concrete patching with localized passive cathodic protection, FRP wrapping the bottom surfaces of the lower concrete superstructure to protect the public access areas, and sealing these limits of concrete surfaces with an epoxy-urethane sealer. Work under the concrete patching includes patching all cracked, loose and spalled concrete on the bridge and installing passive cathodic protection to prevent advancing local concrete corrosion. Work under FRP wrapping includes preparing and wrapping the lower concrete superstructure to prevent concrete spalls from falling onto public access areas below. The preparation of the concrete for the FRP wrap will include removal of the existing epoxy-urethane sealant and smoothing the raised concrete form marks. Work under sealing the concrete surfaces includes sealing all areas that have been patched or FRP wrapped with an epoxy-urethane sealer. It is important to note that no epoxy-urethane sealing will be performed on the concrete patches in the Tunnels, West Station, Span 1A and 1B upper deck superstructure, and the East Station and subway.

Alternative No. 2 was originally estimated to cost \$25,984,000 and included FRP wrapping all concrete surfaces in the lower concrete superstructure. Since this cost was significantly over the original budget allotted for this project, Alternative No. 2 has been scaled back and further broken down into five (5) sub-alternatives to present the District with various options and their associated costs for rehabilitation. The following quantities were removed from Alternative No. 2 options due to limited effective and economy:

- Application of epoxy urethane sealer on patched surfaces of concrete components in the West Tunnel, West Station, upper deck approach spans, East Station and East Subway
- Arch patching and FRP wrapping in Spans 11, 12 and 13
- Lower Deck floorbeam patching and FRP wrapping in Spans 11 and 12
- Railroad coordination and flagging

Alternative No. 2A

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Sealing concrete patching limits with an epoxy-urethane sealer

Alternative No. 2B

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Fiber wrap bottom of arch ribs only over public access areas
- Sealing concrete patching and FRP limits with an epoxy-urethane sealer

Alternative No. 2C

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Fiber wrap bottom of arch ribs and lower deck floor beams over public access areas
- Sealing concrete patching and FRP limits with an epoxy-urethane sealer

Alternative No. 2D

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Fiber wrap bottom of arch ribs and lower deck floor beams over public access areas
- Fiber wrap end columns of piers
- Sealing concrete patching and FRP limits with an epoxy-urethane sealer

Alternative No. 2E

- Micro-silica modified concrete overlay using hydro-demolition
- Patching concrete surfaces with localized passive cathodic protection
- Fiber wrap bottom of arch ribs and lower deck floor beams over public access areas
- Fiber wrap end columns of piers and lower deck support columns

Each sub-alternative is described in further detail on the following pages. A breakdown of costs is also presented with each sub-alternative. Each sub-alternative includes all work items from the previous alternative and adds new work items.

The recommended alternative is **Alternative No. 2C** based on addressing public safety, extending the service life of the bridge, and economic analysis.

Alternative No. 2A

Alternative No. 2A includes all the general maintenance items presented in Alternative No. 1 and includes concrete patching with localized passive cathodic protection and sealing these concrete patching limits with an epoxy-urethane sealer (Note: all repair surfaces have been increased by 20% to account for future deterioration). Concrete patching with localized passive cathodic protection is the most feasible solution to repair the existing locations of failing concrete. Concrete patching will remove and replace all existing cracked, loose, and spalled concrete on the bridge. Localized passive cathodic protection will help to impede the concrete corrosion from advancing which will help prevent future spalling and deterioration in these areas only. It is important to note that this alternative repairs the existing problem areas only. It does not provide repairs or safety measures to address any concrete that may crack, spall, or fall to the ground in the future. Given the history and the patterns of concrete spalling on the bridge, we anticipate that there will be future locations where cracks and spalls develop which will result in additional repair work necessary to address these future locations. This alternate extends the service life of the bridge an estimated 20 years before future repair work is necessary.

This alternate is estimated to cost **\$6,660,000**.

| ALTERNATIVE No. 2A | | | | | | |
|--------------------|-------|-------|------|--|---|--------------------|
| ITEM | EXT | QTY | UNIT | DESCRIPTION | 2017 UNIT COST | 2017 COST |
| 511 | 81100 | 170 | FT | CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT | \$400.00 | \$68,000 |
| 511 | 81300 | 25 | EACH | CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT | \$3,000.00 | \$75,000 |
| 511 | 81300 | 7 | EACH | CONCRETE, MISC.: COLUMN REPLACEMENT | \$8,500.00 | \$59,500 |
| 512 | 10101 | 3780 | SY | SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | \$15.00 | \$56,700 |
| 512 | 10600 | 800 | FT | CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB) | \$70.00 | \$56,000 |
| 516 | 47000 | LUMP | - | JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | \$20,000.00 | \$20,000 |
| 519 | 11600 | 15300 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK) | \$90.00 | \$1,377,000 |
| 519 | 11600 | 9590 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES) | \$100.00 | \$959,000 |
| 519 | 11600 | 5560 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES) | \$125.00 | \$695,000 |
| 519 | 11900 | 6 | CY | SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION) | \$5,000.00 | \$30,000 |
| 530 | 00200 | LUMP | - | SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER | \$5,000.00 | \$5,000 |
| 530 | 00400 | 200 | EACH | SPECIAL - STRUCTURES CORBEL SHIELD | \$200.00 | \$40,000 |
| 530 | 00600 | 900 | SF | SPECIAL - STRUCTURES MASONRY BLOCK WALL | \$10.00 | \$9,000 |
| 625 | 98200 | LUMP | - | LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR | \$20,000.00 | \$20,000 |
| 844 | 10001 | 30450 | SF | CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN | \$20.00 | \$609,000 |
| 848 | 10000 | 17750 | SY | MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | \$25.00 | \$443,750 |
| 848 | 50320 | 17750 | SY | EXISTING CONCRETE OVERLAY REMOVED | \$10.00 | \$177,500 |
| 614 | 11000 | LUMP | - | MAINTAINING TRAFFIC | \$100,000.00 | \$100,000 |
| 619 | 16020 | 24 | MNTH | FIELD OFFICE, TYPE C | \$2,500.00 | \$60,000 |
| 624 | 10000 | LUMP | - | MOBILIZATION | \$100,000.00 | \$100,000 |
| | | | | | SUBTOTAL: | \$4,960,000 |
| | | | | | 20% CONTINGENCY: | \$992,000 |
| | | | | | 2017 TOTAL: | \$5,952,000 |
| | | | | | FUTURE WORTH (AT AN INFLATION RATE OF 11.9%) | \$6,660,000 |

Alternative No. 2B

Alternative No. 2B includes all the work items presented in Alternative No. 2A and includes FRP wrapping the bottom surfaces of the concrete arch ribs which will partially protect the public access below. In this alternative, FRP wrap will be used to contain future concrete delaminations from becoming dislodged and falling on public areas below the concrete arch spans. It is important to note that the lower deck floor beams are not protected in this alternative and therefore, the public areas between the concrete arch spans remain unprotected. Estimated quantities were calculated by assuming the FRP would cover the entire bottom of the arch intrados and the FRP would extend upward on the sides with a 1'-6" development length past potential corner spalls.

While the application of FRP will assist in confining the concrete members and protect the public from falling concrete, it's use will not stop the continual degradation of the concrete from reinforcement. Periodic repair work will be necessary to reapply the FRP in areas. This alternate extends the service life of the bridge an estimated 25 to 40 years before future repair work is necessary.

This alternate is estimated to cost **\$10,347,000.**

| ALTERNATIVE No. 2B | | | | | | |
|---|-------|-------|------|--|----------------|---------------------|
| ITEM | EXT | QTY | UNIT | DESCRIPTION | 2017 UNIT COST | 2017 COST |
| 511 | 81100 | 170 | FT | CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT | \$400.00 | \$68,000 |
| 511 | 81300 | 25 | EACH | CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT | \$3,000.00 | \$75,000 |
| 511 | 81300 | 7 | EACH | CONCRETE, MISC.: COLUMN REPLACEMENT | \$8,500.00 | \$59,500 |
| 512 | 10101 | 10590 | SY | SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | \$15.00 | \$158,850 |
| 512 | 10600 | 800 | FT | CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB) | \$70.00 | \$56,000 |
| 512 | 74000 | 6860 | SY | REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | \$20.00 | \$137,200 |
| 516 | 47000 | LUMP | - | JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | \$20,000.00 | \$20,000 |
| 519 | 00100 | 55693 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (ARCH RIBS) | \$45.00 | \$2,506,203 |
| 519 | 11600 | 15300 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK) | \$90.00 | \$1,377,000 |
| 519 | 11600 | 9590 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES) | \$100.00 | \$959,000 |
| 519 | 11600 | 5560 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES) | \$125.00 | \$695,000 |
| 519 | 11900 | 6 | CY | SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION) | \$5,000.00 | \$30,000 |
| 530 | 00200 | LUMP | - | SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER | \$5,000.00 | \$5,000 |
| 530 | 00400 | 200 | EACH | SPECIAL - STRUCTURES CORBEL SHIELD | \$200.00 | \$40,000 |
| 530 | 00600 | 900 | SF | SPECIAL - STRUCTURES MASONRY BLOCK WALL | \$10.00 | \$9,000 |
| 625 | 98200 | LUMP | - | LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR | \$20,000.00 | \$20,000 |
| 844 | 10001 | 30450 | SF | CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN | \$20.00 | \$609,000 |
| 848 | 10000 | 17750 | SY | MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | \$25.00 | \$443,750 |
| 848 | 50320 | 17750 | SY | EXISTING CONCRETE OVERLAY REMOVED | \$10.00 | \$177,500 |
| 614 | 11000 | LUMP | - | MAINTAINING TRAFFIC | \$100,000.00 | \$100,000 |
| 619 | 16020 | 24 | MNTH | FIELD OFFICE, TYPE C | \$2,500.00 | \$60,000 |
| 624 | 10000 | LUMP | - | MOBILIZATION | \$100,000.00 | \$100,000 |
| SUBTOTAL: | | | | | | \$7,706,000 |
| 20% CONTINGENCY: | | | | | | \$1,541,000 |
| 2017 TOTAL: | | | | | | \$9,247,000 |
| FUTURE WORTH (AT AN INFLATION RATE OF 11.9%) | | | | | | \$10,347,000 |

Alternative No. 2C

Alternative No. 2C includes all the work items presented in Alternative No. 2B and includes the additional FRP wrapping of the bottom surfaces of the concrete lower deck floor beams which will further protect the public access below. In this alternative, FRP wrap will be used to contain future concrete delaminations from becoming dislodged and falling onto public areas between the concrete arch spans. The lower deck floor beams are open to public access areas below and as a result, concrete would likely fall onto the public access areas below if it becomes dislodged. It is important to note that the bottom surfaces of most concrete members above public access areas are protected in this alternative. Estimated quantities were calculated by assuming the FRP would cover the entire bottom of the lower deck floor beams and the FRP would extend upward on the sides with a 1'-0" development length past potential corner spalls. This alternate extends the service life of the bridge an estimated 25 to 40 years before future repair work is necessary.

This alternate is estimated to cost **\$14,047,000**.

| ALTERNATIVE No. 2C | | | | | | |
|---|-------|-------|------|--|----------------|---------------------|
| ITEM | EXT | QTY | UNIT | DESCRIPTION | 2017 UNIT COST | 2017 COST |
| 511 | 81100 | 170 | FT | CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT | \$400.00 | \$68,000 |
| 511 | 81300 | 25 | EACH | CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT | \$3,000.00 | \$75,000 |
| 511 | 81300 | 7 | EACH | CONCRETE, MISC.: COLUMN REPLACEMENT | \$8,500.00 | \$59,500 |
| 512 | 10101 | 17430 | SY | SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | \$15.00 | \$261,450 |
| 512 | 10600 | 800 | FT | CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB) | \$70.00 | \$56,000 |
| 512 | 74000 | 13680 | SY | REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | \$20.00 | \$273,600 |
| 516 | 47000 | LUMP | - | JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | \$20,000.00 | \$20,000 |
| 519 | 00100 | 55693 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (ARCH RIBS) | \$45.00 | \$2,506,203 |
| 519 | 00100 | 55919 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (FLOOR BEAMS) | \$45.00 | \$2,516,355 |
| 519 | 11600 | 15300 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK) | \$90.00 | \$1,377,000 |
| 519 | 11600 | 9590 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES) | \$100.00 | \$959,000 |
| 519 | 11600 | 5560 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES) | \$125.00 | \$695,000 |
| 519 | 11900 | 6 | CY | SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION) | \$5,000.00 | \$30,000 |
| 530 | 00200 | LUMP | - | SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER | \$5,000.00 | \$5,000 |
| 530 | 00400 | 200 | EACH | SPECIAL - STRUCTURES CORBEL SHIELD | \$200.00 | \$40,000 |
| 530 | 00600 | 900 | SF | SPECIAL - STRUCTURES MASONRY BLOCK WALL | \$10.00 | \$9,000 |
| 625 | 98200 | LUMP | - | LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR | \$20,000.00 | \$20,000 |
| 844 | 10001 | 30450 | SF | CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN | \$20.00 | \$609,000 |
| 848 | 10000 | 17750 | SY | MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | \$25.00 | \$443,750 |
| 848 | 50320 | 17750 | SY | EXISTING CONCRETE OVERLAY REMOVED | \$10.00 | \$177,500 |
| 614 | 11000 | LUMP | - | MAINTAINING TRAFFIC | \$100,000.00 | \$100,000 |
| 619 | 16020 | 24 | MNTH | FIELD OFFICE, TYPE C | \$2,500.00 | \$60,000 |
| 624 | 10000 | LUMP | - | MOBILIZATION | \$100,000.00 | \$100,000 |
| SUBTOTAL: | | | | | | \$10,461,000 |
| 20% CONTINGENCY: | | | | | | \$2,092,000 |
| 2017 TOTAL: | | | | | | \$12,553,000 |
| FUTURE WORTH (AT AN INFLATION RATE OF 11.9%) | | | | | | \$14,047,000 |



Alternative No. 2D

Alternative No. 2D includes all the work items presented in Alternative No. 2C and includes additional protection of the public access areas by also wrapping the vertical surfaces of the end columns located at the piers. The location of the end columns on the piers are such that dislodged concrete has a high probability of falling onto the public access areas. These safety concerns, coupled with the fact that of all the vertical surfaces the end columns located at the piers are in the most critical shape, resulted in presenting this alternative to show the additional costs required to perform this work. This alternate extends the service life of the bridge an estimated 25 to 40 years before future repair work is necessary.

This alternate is estimated to cost **\$15,409,000**.

| ALTERNATIVE No. 2D | | | | | | |
|---|-------|-------|------|--|----------------|---------------------|
| ITEM | EXT | QTY | UNIT | DESCRIPTION | 2017 UNIT COST | 2017 COST |
| 511 | 81100 | 170 | FT | CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT | \$400.00 | \$68,000 |
| 511 | 81300 | 25 | EACH | CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT | \$3,000.00 | \$75,000 |
| 511 | 81300 | 7 | EACH | CONCRETE, MISC.: COLUMN REPLACEMENT | \$8,500.00 | \$59,500 |
| 512 | 10101 | 19910 | SY | SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | \$15.00 | \$298,650 |
| 512 | 10600 | 800 | FT | CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB) | \$70.00 | \$56,000 |
| 512 | 74000 | 16210 | SY | REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | \$20.00 | \$324,200 |
| 516 | 47000 | LUMP | - | JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | \$20,000.00 | \$20,000 |
| 519 | 00100 | 55693 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (ARCH RIBS) | \$45.00 | \$2,506,203 |
| 519 | 00100 | 20568 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (END COLUMNS) | \$45.00 | \$925,560 |
| 519 | 00100 | 55919 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (FLOOR BEAMS) | \$45.00 | \$2,516,355 |
| 519 | 11600 | 15300 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK) | \$90.00 | \$1,377,000 |
| 519 | 11600 | 9590 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES) | \$100.00 | \$959,000 |
| 519 | 11600 | 5560 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES) | \$125.00 | \$695,000 |
| 519 | 11900 | 6 | CY | SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION) | \$5,000.00 | \$30,000 |
| 530 | 00200 | LUMP | - | SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER | \$5,000.00 | \$5,000 |
| 530 | 00400 | 200 | EACH | SPECIAL - STRUCTURES CORBEL SHIELD | \$200.00 | \$40,000 |
| 530 | 00600 | 900 | SF | SPECIAL - STRUCTURES MASONRY BLOCK WALL | \$10.00 | \$9,000 |
| 625 | 98200 | LUMP | - | LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR | \$20,000.00 | \$20,000 |
| 844 | 10001 | 30450 | SF | CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN | \$20.00 | \$609,000 |
| 848 | 10000 | 17750 | SY | MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | \$25.00 | \$443,750 |
| 848 | 50320 | 17750 | SY | EXISTING CONCRETE OVERLAY REMOVED | \$10.00 | \$177,500 |
| 614 | 11000 | LUMP | - | MAINTAINING TRAFFIC | \$100,000.00 | \$100,000 |
| 619 | 16020 | 24 | MNTH | FIELD OFFICE, TYPE C | \$2,500.00 | \$60,000 |
| 624 | 10000 | LUMP | - | MOBILIZATION | \$100,000.00 | \$100,000 |
| SUBTOTAL: | | | | | | \$11,475,000 |
| 20% CONTINGENCY: | | | | | | \$2,295,000 |
| 2017 TOTAL: | | | | | | \$13,770,000 |
| FUTURE WORTH (AT AN INFLATION RATE OF 11.9%) | | | | | | \$15,409,000 |

Alternative No. 2E

Alternative No. 2E includes all the work items presented in Alternative No. 2D and includes additional protection of the public access areas by also wrapping the vertical surfaces of the lower deck support columns. The lower deck support columns are located over public access areas and dislodged concrete may potentially fall on to the public access areas below if it does not land on the concrete arch ribs below. This additional work would result in containing all the concrete with a high probability of falling on the public access areas below. Since all the existing problematic areas are addressed by concrete patching with cathodic protection and future areas are addressed by containment with FRP wrapping, this alternate extends the service life of the bridge an estimated 25 to 50 years before future repair work is necessary.

This alternate is estimated to cost **\$19,515,000**.

| ALTERNATIVE No. 2E | | | | | | |
|--------------------|-------|-------|------|--|---|---------------------|
| ITEM | EXT | QTY | UNIT | DESCRIPTION | 2017 UNIT COST | 2017 COST |
| 511 | 81100 | 170 | FT | CONCRETE, MISC.: WEST STATION CONCRETE BEAM REPLACEMENT | \$400.00 | \$68,000 |
| 511 | 81300 | 25 | EACH | CONCRETE, MISC.: LOWER DECK CORBEL REPLACEMENT | \$3,000.00 | \$75,000 |
| 511 | 81300 | 7 | EACH | CONCRETE, MISC.: COLUMN REPLACEMENT | \$8,500.00 | \$59,500 |
| 512 | 10101 | 27480 | SY | SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | \$15.00 | \$412,200 |
| 512 | 10600 | 800 | FT | CONCRETE REPAIR BY EPOXY INJECTION (ARCH RIB) | \$70.00 | \$56,000 |
| 512 | 74000 | 23790 | SY | REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | \$20.00 | \$475,800 |
| 516 | 47000 | LUMP | - | JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | \$20,000.00 | \$20,000 |
| 519 | 00100 | 55693 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (ARCH RIBS) | \$45.00 | \$2,506,203 |
| 519 | 00100 | 62060 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (LOWER DECK SUPPORT COLUMNS) | \$45.00 | \$2,792,700 |
| 519 | 00100 | 20568 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (END COLUMNS) | \$45.00 | \$925,560 |
| 519 | 00100 | 55919 | SF | SPECIAL - COMPOSITE FIBER WRAP SYSTEM (FLOOR BEAMS) | \$45.00 | \$2,516,355 |
| 519 | 11600 | 15300 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (WEST STATION, TUNNELS AND UPPER DECK) | \$90.00 | \$1,377,000 |
| 519 | 11600 | 9590 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, VERTICAL SURFACES) | \$100.00 | \$959,000 |
| 519 | 11600 | 5560 | SF | SPECIAL - PATCHING CONCRETE STRUCTURE (LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES) | \$125.00 | \$695,000 |
| 519 | 11900 | 6 | CY | SPECIAL - PATCHING CONCRETE STRUCTURE (DEEP PIER SHAFT DETERIORATION) | \$5,000.00 | \$30,000 |
| 530 | 00200 | LUMP | - | SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER | \$5,000.00 | \$5,000 |
| 530 | 00400 | 200 | EACH | SPECIAL - STRUCTURES CORBEL SHIELD | \$200.00 | \$40,000 |
| 530 | 00600 | 900 | SF | SPECIAL - STRUCTURES MASONRY BLOCK WALL | \$10.00 | \$9,000 |
| 625 | 98200 | LUMP | - | LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR | \$20,000.00 | \$20,000 |
| 844 | 10001 | 30450 | SF | CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN | \$20.00 | \$609,000 |
| 848 | 10000 | 17750 | SY | MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | \$25.00 | \$443,750 |
| 848 | 50320 | 17750 | SY | EXISTING CONCRETE OVERLAY REMOVED | \$10.00 | \$177,500 |
| 614 | 11000 | LUMP | - | MAINTAINING TRAFFIC | \$100,000.00 | \$100,000 |
| 619 | 16020 | 24 | MNTH | FIELD OFFICE, TYPE C | \$2,500.00 | \$60,000 |
| 624 | 10000 | LUMP | - | MOBILIZATION | \$100,000.00 | \$100,000 |
| | | | | | SUBTOTAL: | \$14,533,000 |
| | | | | | 20% CONTINGENCY: | \$2,907,000 |
| | | | | | 2017 TOTAL: | \$17,440,000 |
| | | | | | FUTURE WORTH (AT AN INFLATION RATE OF 11.9%) | \$19,515,000 |

Alternative No. 3

As with Alternate No. 1 and 2, all general maintenance items including the hydro- demolition and overlay of the upper deck will be included. In Spans 2 through 13, excluding Span 4, all cracked, loose and deteriorated concrete will be patched. The areas in the West Station will be patched and/or replaced. As opposed to Alternate 2, in lieu of wrap, active impressed cathodic protection be employed to counteract and stabilize the corrosion. Once in place, this system can restore the concrete to its original composition and halt the ongoing concrete corrosion.

If installed and maintained properly, it is estimated that the service life would be greater than 50 years. Several bridges throughout the United States have this system in place and appear to be functioning as designed.

This alternate is estimated to cost \$33,226,000. This estimated cost does not include maintenance of the active cathodic protection system.

The estimated costs for all alternates have been projected to the 2020 construction year.

**OHIO DEPARTMENT OF TRANSPORTATION
2017 REHABILITATION FEASIBILITY STUDY
APPENDICES
PID NO 99972**

**DETROIT-SUPERIOR BRIDGE OVER CUYAHOGA RIVER
BRIDGE NO. CUY-6-1456**

SFN: 1800930



FEBRUARY 2017

PREPARED BY:



1655 W. Market Street, Suite 355 | Akron, OH 44313

BRIDGE NO. CUY-6-1456
DETROIT-SUPERIOR BRIDGE OVER CUYAHOGA RIVER
2017 REHABILITATION FEASIBILITY STUDY

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- Appendix G – West Station Deterioration History**
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APPENDIX A

SUMMARY OF ESTIMATED COST

Summary of Estimated Cost

| Alternative | Description | February 15, 2015 Estimate | Construction Mid-Point | July 1, 2020 Estimate |
|-------------|---|----------------------------|------------------------|-----------------------|
| 1 | Maintenance Only | \$2,282,400 | 41 Month | \$2,569,000 |
| 2 | Rehabilitation w/Patching and FRP Wrap | \$22,907,400 | 41 Month | \$25,984,000 |
| 3 | Rehabilitation w/Patching Cathodic Protection | \$29,519,400 | 41 Month | \$33,226,000 |

| | | | | |
|----|-------------------------------|--------------|-----------|--------------|
| 2A | Maintenance plus patching | \$5,952,000 | 38 Months | \$6,660,000 |
| 2B | 2A plus FRP Wrap Arch Ribs | \$9,247,000 | 38 Months | \$10,347,000 |
| 2C | 2B plus FRP Wrap Floor Beams | \$12,553,000 | 38 Months | \$14,047,000 |
| 2D | 2C plus FRP Wrap End Columns | \$13,770,000 | 38 Months | \$15,409,000 |
| 2E | 2D plus FRP Wrap L.D. Columns | \$17,440,000 | 38 Months | \$19,515,000 |



CY 2017-2021 Business Plan Inflation Calculator:

[Not sure if you have the latest calculator? Click here.](#)

Last Modified: 1/19/2017

Today's Date:
February 15, 2017

Please Enter Values in the Yellow Areas Only:

Estimation Start Date:

Less than or Equal to Today's Date
(mm/dd/yyyy)

2/15/2017

Start Date:

Enter Construction Mid-Point Date:

(cannot exceed 02/15/2042)
(mm/dd/yyyy)

7/1/2020

Construction Mid-Point Date:

Present-Day Estimated Cost:

\$2,282,400.00

Estimated Dollar Amount:

Estimate Start Date to Construction Mid-Point Date:

41

Months

Inflation - Start to Mid-Point of Construction:

(compounded growth rate)

Inflated Dollar Amount:

Business Plan

12.6%

\$2,568,995.13

Estimator's Name:

County - Route - Section:

CUY-6-1456

PID:

99972

Estimator's Notes:

Alternate 1 - Maintenance Only

Estimate ODOT1602

Estimated Cost:\$1,902,000.00

Contingency: 20.00%

Estimated Total: \$2,282,400.00

ALTERNATE 1 - MAINTENANCE ONLY

Base Date: 02/13/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type:

Season:

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by DEA on 02/13/17

Checked by WJV on 02/14/17

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|---------------------------------|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |

Group 0001: STRUCTURE

| | | | | | |
|---|-----------|------------|----|----------------|----------------|
| 0005 | 530E00200 | 1.000 | LS | \$5,000.00000 | \$5,000.00 |
| SPECIAL - STRUCTURES BRIDGE OPERATOR'S CAR SHELTER | | | | | |
| 0006 | 530E00600 | 900.000 | SF | \$10.00000 | \$9,000.00 |
| SPECIAL - STRUCTURES MASONRY BLOCK WALL | | | | | |
| 0007 | 530E00600 | 15,000.000 | SF | \$22.00000 | \$330,000.00 |
| SPECIAL - STRUCTURES REMOVE LOOSE AND DELAMINATED CONCRETE | | | | | |
| 0008 | 625E98200 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR | | | | | |
| 0009 | 848E10000 | 19,400.000 | SY | \$60.00000 | \$1,164,000.00 |
| MICRO SILICA MODIFIED CONCRETE OVELAY USING HYDRODEMOLITION | | | | | |
| 0010 | 848E50320 | 19,400.000 | SY | \$10.00000 | \$194,000.00 |
| EXISTING CONCRETE OVERLAY REMOVED | | | | | |

Total for Group 0001:\$1,722,000.00

Group 0002: INCIDENTAL

| | | | | | |
|----------------------|-----------|--------|------|-----------------|--------------|
| 0011 | 614E11000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MAINTAINING TRAFFIC | | | | | |
| 0012 | 619E16020 | 12.000 | MNTH | \$2,500.00000 | \$30,000.00 |
| FIELD OFFICE, TYPE C | | | | | |
| 0013 | 624E10000 | 1.000 | LS | \$50,000.00000 | \$50,000.00 |
| MOBILIZATION | | | | | |

Total for Group 0002:\$180,000.00

CY 2017-2021 Business Plan Inflation Calculator:

[Not sure if you have the latest calculator? Click here.](#)

Last Modified: 1/19/2017

Today's Date:
February 15, 2017

Please Enter Values in the Yellow Areas Only:

Estimation Start Date:

Less than or Equal to Today's Date
(mm/dd/yyyy)

2/15/2017

Start Date:

Enter Construction Mid-Point Date:

(cannot exceed 02/15/2042)
(mm/dd/yyyy)

7/1/2020

Construction Mid-Point Date:

Present-Day Estimated Cost:

\$22,907,400.00

Estimated Dollar Amount:

Estimate Start Date to Construction Mid-Point Date:

41

Months

Inflation - Start to Mid-Point of Construction:

(compounded growth rate)

Inflated Dollar Amount:

Business Plan

12.6%

\$25,783,823.60

Estimator's Name:

County - Route - Section:

CUY-6-1456

PID:

99972

Estimator's Notes:

Alternate 2 - Rehab w/ Patching and Fiber Wrap

Estimate ODOT1602

Estimated Cost:\$19,089,500.00

Contingency: 20.00%

Estimated Total: \$22,907,400.00

ALTERNATE 2 - REHAB W/ PATCHING AND FIBER WRAP

Base Date: 02/13/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type:

Season:

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by DEA on 02/13/17

Checked by WJV on 02/14/17

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|-----------------------|---|-----------------|--------------|-------------------|------------------|
| | Description <u>Supplemental Description</u> | | | | |
| Group 0001: STRUCTURE | | | | | |
| 0005 | 511E81100 | 150.000 | FT | \$400.00000 | \$60,000.00 |
| | CONCRETE, MISC.: <i>WEST STATION CONCRETE BEAM REPLACEMENT</i> | | | | |
| 0006 | 511E81300 | 25.000 | EACH | \$3,000.00000 | \$75,000.00 |
| | CONCRETE, MISC.: <i>LOWER DECK CORBEL REPLACEMENT</i> | | | | |
| 0007 | 511E81300 | 4.000 | EACH | \$8,500.00000 | \$34,000.00 |
| | CONCRETE, MISC.: <i>COLUMN REPLACEMENT</i> | | | | |
| 0008 | 512E10101 | 31,000.000 | SY | \$15.00000 | \$465,000.00 |
| | SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | | | | |
| 0009 | 512E10600 | 800.000 | FT | \$70.00000 | \$56,000.00 |
| | CONCRETE REPAIR BY EPOXY INJECTION <i>ARCH RIB</i> | | | | |
| 0010 | 512E74000 | 31,000.000 | SY | \$20.00000 | \$620,000.00 |
| | REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | | | | |
| 0011 | 516E47000 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| | JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | | | | |
| 0012 | 519E00100 | 275,000.000 | SF | \$45.00000 | \$12,375,000.00 |
| | SPECIAL - COMPOSITE FIBER WRAP SYSTEM | | | | |
| 0013 | 519E11600 | 15,000.000 | SF | \$90.00000 | \$1,350,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>WEST STATION, TUNNELS AND UPPER DECK</i> | | | | |
| 0014 | 519E11600 | 9,500.000 | SF | \$100.00000 | \$950,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>LOWER SUPERSTRUCTURE, VERTICAL SURFACES</i> | | | | |
| 0015 | 519E11600 | 5,500.000 | SF | \$125.00000 | \$687,500.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>LOWER SUPERSTRUCTURE - BOTTOM AND CURVED SURFACES</i> | | | | |
| 0016 | 519E11900 | 6.000 | CY | \$5,000.00000 | \$30,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>DEEP PIER SHAFT DETERIORATION</i> | | | | |
| 0017 | 530E00200 | 1.000 | LS | \$5,000.00000 | \$5,000.00 |
| | SPECIAL - STRUCTURES <i>BRIDGE OPERATOR'S CAR SHELTER</i> | | | | |
| 0018 | 530E00400 | 200.000 | EACH | \$200.00000 | \$40,000.00 |
| | SPECIAL - STRUCTURES <i>CORBEL SHIELD</i> | | | | |
| 0019 | 530E00600 | 900.000 | SF | \$10.00000 | \$9,000.00 |
| | SPECIAL - STRUCTURES <i>MASONRY BLOCK WALL</i> | | | | |
| 0020 | 625E98200 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| | LIGHTING, MISC.: <i>NAVIGATION LIGHTING REPAIR</i> | | | | |
| 0021 | 844E10001 | 30,000.000 | SF | \$20.00000 | \$600,000.00 |
| | CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLA N | | | | |

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|---------------|--|-----------------|--------------|-------------------|------------------|
| | <u>Description</u> <u>Supplemental Description</u> | | | | |
| 0022 | 848E10000 | 19,400.000 | SY | \$60.00000 | \$1,164,000.00 |
| | <i>MICRO SILICA MODIFIED CONCRETE OVELAY USING HYDRODEMOLITION</i> | | | | |
| 0023 | 848E50320 | 19,400.000 | SY | \$10.00000 | \$194,000.00 |
| | EXISTING CONCRETE OVERLAY REMOVED | | | | |

Total for Group 0001:\$18,754,500.00

Group 0002: INCIDENTAL

| | | | | | |
|------|---|--------|------|-----------------|--------------|
| 0024 | 614E11000 MAINTAINING TRAFFIC | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| 0025 | 614E18002 MAINTAINING TRAFFIC, MISC.: RAILROAD FLAGGER | 1.000 | LS | \$50,000.00000 | \$50,000.00 |
| 0026 | 614E18002 MAINTAINING TRAFFIC, MISC.: RAILROAD COORDINATION | 1.000 | LS | \$25,000.00000 | \$25,000.00 |
| 0027 | 619E16020 FIELD OFFICE, TYPE C | 24.000 | MNTH | \$2,500.00000 | \$60,000.00 |
| 0028 | 624E10000 MOBILIZATION | 1.000 | LS | \$100,000.00000 | \$100,000.00 |

Total for Group 0002:\$335,000.00

CY 2017-2021 Business Plan Inflation Calculator:

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Last Modified: 1/19/2017

Today's Date:
May 17, 2017

Please Enter Values in the Yellow Areas Only:

Estimation Start Date:

Less than or Equal to Today's Date
(mm/dd/yyyy)

5/17/2017

Start Date:

Enter Construction Mid-Point Date:

(cannot exceed 05/17/2042)
(mm/dd/yyyy)

7/1/2020

Construction Mid-Point Date:

Present-Day Estimated Cost:

\$5,952,000.00

Estimated Dollar Amount:

Estimate Start Date to Construction Mid-Point Date:

38

Months

Inflation - Start to Mid-Point of Construction:

(compounded growth rate)

Inflated Dollar Amount:

Business Plan

11.9%

\$6,658,148.51

Estimator's Name:

County - Route - Section:

CUY-6-14.56

PID:

99972

Estimator's Notes:

Alternative No. 2A

Estimate ODOT1602

Estimated Cost:\$4,960,450.00

Contingency: 20.00%

Estimated Total: \$5,952,540.00

Alternative No. 2A

Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17

Checked by WJV on 05/17/17

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|--|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |
| Group 0001: STRUCTURE | | | | | |
| 0001 | 511E81100 | 170.000 | FT | \$400.00000 | \$68,000.00 |
| CONCRETE, MISC.: <i>WEST STATION CONCRETE BEAM REPLACEMENT</i> | | | | | |
| 0002 | 511E81300 | 25.000 | EACH | \$3,000.00000 | \$75,000.00 |
| CONCRETE, MISC.: <i>LOWER DECK CORBEL REPLACEMENT</i> | | | | | |
| 0003 | 511E81300 | 7.000 | EACH | \$8,500.00000 | \$59,500.00 |
| CONCRETE, MISC.: <i>COLUMN REPLACEMENT</i> | | | | | |
| 0004 | 512E10101 | 3,780.000 | SY | \$15.00000 | \$56,700.00 |
| SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | | | | | |
| 0005 | 512E10600 | 800.000 | FT | \$70.00000 | \$56,000.00 |
| CONCRETE REPAIR BY EPOXY INJECTION <i>(ARCH RIB)</i> | | | | | |
| 0006 | 516E47000 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | | | | | |
| 0007 | 519E11600 | 15,300.000 | SF | \$90.00000 | \$1,377,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(WEST STATION, TUNNELS, AND UPPER DECK)</i> | | | | | |
| 0008 | 519E11600 | 9,590.000 | SF | \$100.00000 | \$959,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, VERTICAL SURFACES)</i> | | | | | |
| 0009 | 519E11600 | 5,560.000 | SF | \$125.00000 | \$695,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)</i> | | | | | |
| 0010 | 519E11900 | 6.000 | CY | \$5,000.00000 | \$30,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(DEEP PIER SHAFT DETERIORATION)</i> | | | | | |
| 0011 | 530E00200 | 1.000 | LS | \$5,000.00000 | \$5,000.00 |
| SPECIAL - STRUCTURES <i>BRIDGE OPERATOR'S CAR SHELTER</i> | | | | | |
| 0012 | 530E00400 | 200.000 | EACH | \$200.00000 | \$40,000.00 |
| SPECIAL - STRUCTURES <i>CORBEL SHIELD</i> | | | | | |
| 0013 | 530E00600 | 900.000 | SF | \$10.00000 | \$9,000.00 |
| SPECIAL - STRUCTURES <i>MASONRY BLOCK WALL</i> | | | | | |
| 0014 | 625E98200 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| LIGHTING, MISC.: <i>NAVIGATION LIGHTING REPAIR</i> | | | | | |
| 0015 | 844E10001 | 30,450.000 | SF | \$20.00000 | \$609,000.00 |
| CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN | | | | | |
| 0016 | 848E10000 | 17,750.000 | SY | \$25.00000 | \$443,750.00 |
| MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | | | | | |
| 0017 | 848E50320 | 17,750.000 | SY | \$10.00000 | \$177,500.00 |
| EXISTING CONCRETE OVERLAY REMOVED | | | | | |
| 0018 | 614E11000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MAINTAINING TRAFFIC | | | | | |

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|---------------------------------|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |
| 0019 | 619E16020 | 24.000 | MNTH | \$2,500.00000 | \$60,000.00 |
| FIELD OFFICE, TYPE C | | | | | |
| 0020 | 624E10000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MOBILIZATION | | | | | |

Total for Group 0001:\$4,960,450.00

CY 2017-2021 Business Plan Inflation Calculator:

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Last Modified: 1/19/2017

Today's Date:
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Less than or Equal to Today's Date
(mm/dd/yyyy)

5/17/2017

Start Date:

Enter Construction Mid-Point Date:

(cannot exceed 05/17/2042)
(mm/dd/yyyy)

7/1/2020

Construction Mid-Point Date:

Present-Day Estimated Cost:

\$9,247,000.00

Estimated Dollar Amount:

Estimate Start Date to Construction Mid-Point Date:

38

Months

Inflation - Start to Mid-Point of Construction:

(compounded growth rate)

Inflated Dollar Amount:

Business Plan

11.9%

\$10,344,069.10

Estimator's Name:

County - Route - Section:

CUY-6-14.56

PID:

99972

Estimator's Notes:

Alternative No. 2B

Estimate ODOT1602

Estimated Cost:\$7,705,985.00

Contingency: 20.00%

Estimated Total: \$9,247,182.00

Alternative No. 2B

Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17

Checked by WJV on 05/17/17

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|--|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |
| Group 0001: STRUCTURE | | | | | |
| 0001 | 511E81100 | 170.000 | FT | \$400.00000 | \$68,000.00 |
| CONCRETE, MISC.: <i>WEST STATION CONCRETE BEAM REPLACEMENT</i> | | | | | |
| 0002 | 511E81300 | 25.000 | EACH | \$3,000.00000 | \$75,000.00 |
| CONCRETE, MISC.: <i>LOWER DECK CORBEL REPLACEMENT</i> | | | | | |
| 0003 | 511E81300 | 7.000 | EACH | \$8,500.00000 | \$59,500.00 |
| CONCRETE, MISC.: <i>COLUMN REPLACEMENT</i> | | | | | |
| 0004 | 512E10101 | 10,590.000 | SY | \$15.00000 | \$158,850.00 |
| SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | | | | | |
| 0005 | 512E10600 | 800.000 | FT | \$70.00000 | \$56,000.00 |
| CONCRETE REPAIR BY EPOXY INJECTION <i>(ARCH RIB)</i> | | | | | |
| 0006 | 512E74000 | 6,860.000 | SY | \$20.00000 | \$137,200.00 |
| REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | | | | | |
| 0007 | 516E47000 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | | | | | |
| 0008 | 519E00100 | 55,693.000 | SF | \$45.00000 | \$2,506,185.00 |
| SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(ARCH RIBS)</i> | | | | | |
| 0009 | 519E11600 | 15,300.000 | SF | \$90.00000 | \$1,377,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(WEST STATION, TUNNELS, AND UPPER DECK)</i> | | | | | |
| 0010 | 519E11600 | 9,590.000 | SF | \$100.00000 | \$959,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, VERTICAL SURFACES)</i> | | | | | |
| 0011 | 519E11600 | 5,560.000 | SF | \$125.00000 | \$695,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)</i> | | | | | |
| 0012 | 519E11900 | 6.000 | CY | \$5,000.00000 | \$30,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(DEEP PIER SHAFT DETERIORATION)</i> | | | | | |
| 0013 | 530E00200 | 1.000 | LS | \$5,000.00000 | \$5,000.00 |
| SPECIAL - STRUCTURES <i>BRIDGE OPERATOR'S CAR SHELTER</i> | | | | | |
| 0014 | 530E00400 | 200.000 | EACH | \$200.00000 | \$40,000.00 |
| SPECIAL - STRUCTURES <i>CORBEL SHIELD</i> | | | | | |
| 0015 | 530E00600 | 900.000 | SF | \$10.00000 | \$9,000.00 |
| SPECIAL - STRUCTURES <i>MASONRY BLOCK WALL</i> | | | | | |
| 0016 | 625E98200 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| LIGHTING, MISC.: <i>NAVIGATION LIGHTING REPAIR</i> | | | | | |
| 0017 | 844E10001 | 30,450.000 | SF | \$20.00000 | \$609,000.00 |
| CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN | | | | | |
| 0018 | 848E10000 | 17,750.000 | SY | \$25.00000 | \$443,750.00 |
| MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | | | | | |

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|-----------------------------------|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |
| 0019 | 848E50320 | 17,750.000 | SY | \$10.00000 | \$177,500.00 |
| EXISTING CONCRETE OVERLAY REMOVED | | | | | |
| 0020 | 614E11000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MAINTAINING TRAFFIC | | | | | |
| 0021 | 619E16020 | 24.000 | MNTH | \$2,500.00000 | \$60,000.00 |
| FIELD OFFICE, TYPE C | | | | | |
| 0022 | 624E10000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MOBILIZATION | | | | | |

Total for Group 0001:\$7,705,985.00

CY 2017-2021 Business Plan Inflation Calculator:

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Last Modified: 1/19/2017

Today's Date:
May 17, 2017

Please Enter Values in the Yellow Areas Only:

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(mm/dd/yyyy)

5/17/2017

Start Date:

Enter Construction Mid-Point Date:

(cannot exceed 05/17/2042)
(mm/dd/yyyy)

7/1/2020

Construction Mid-Point Date:

Present-Day Estimated Cost:

\$12,553,000.00

Estimated Dollar Amount:

Estimate Start Date to Construction Mid-Point Date:

38

Months

Inflation - Start to Mid-Point of Construction:

(compounded growth rate)

Inflated Dollar Amount:

Business Plan

11.9%

\$14,042,294.74

Estimator's Name:

County - Route - Section:

CUY-6-14.56

PID:

99972

Estimator's Notes:

Alternative No. 2C

Estimate ODOT1602

Estimated Cost:\$10,461,340.00

Contingency: 20.00%

Estimated Total: \$12,553,608.00

Alternative No. 2C

Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17

Checked by WJV on 05/17/17

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|--|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |
| Group 0001: STRUCTURE | | | | | |
| 0001 | 511E81100 | 170.000 | FT | \$400.00000 | \$68,000.00 |
| CONCRETE, MISC.: <i>WEST STATION CONCRETE BEAM REPLACEMENT</i> | | | | | |
| 0002 | 511E81300 | 25.000 | EACH | \$3,000.00000 | \$75,000.00 |
| CONCRETE, MISC.: <i>LOWER DECK CORBEL REPLACEMENT</i> | | | | | |
| 0003 | 511E81300 | 7.000 | EACH | \$8,500.00000 | \$59,500.00 |
| CONCRETE, MISC.: <i>COLUMN REPLACEMENT</i> | | | | | |
| 0004 | 512E10101 | 17,430.000 | SY | \$15.00000 | \$261,450.00 |
| SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | | | | | |
| 0005 | 512E10600 | 800.000 | FT | \$70.00000 | \$56,000.00 |
| CONCRETE REPAIR BY EPOXY INJECTION <i>(ARCH RIB)</i> | | | | | |
| 0006 | 512E74000 | 13,680.000 | SY | \$20.00000 | \$273,600.00 |
| REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | | | | | |
| 0007 | 516E47000 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | | | | | |
| 0008 | 519E00100 | 55,693.000 | SF | \$45.00000 | \$2,506,185.00 |
| SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(ARCH RIBS)</i> | | | | | |
| 0009 | 519E00100 | 55,919.000 | SF | \$45.00000 | \$2,516,355.00 |
| SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(FLOOR BEAMS)</i> | | | | | |
| 0010 | 519E11600 | 15,300.000 | SF | \$90.00000 | \$1,377,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(WEST STATION, TUNNELS, AND UPPER DECK)</i> | | | | | |
| 0011 | 519E11600 | 9,590.000 | SF | \$100.00000 | \$959,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, VERTICAL SURFACES)</i> | | | | | |
| 0012 | 519E11600 | 5,560.000 | SF | \$125.00000 | \$695,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)</i> | | | | | |
| 0013 | 519E11900 | 6.000 | CY | \$5,000.00000 | \$30,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>(DEEP PIER SHAFT DETERIORATION)</i> | | | | | |
| 0014 | 530E00200 | 1.000 | LS | \$5,000.00000 | \$5,000.00 |
| SPECIAL - STRUCTURES <i>BRIDGE OPERATOR'S CAR SHELTER</i> | | | | | |
| 0015 | 530E00400 | 200.000 | EACH | \$200.00000 | \$40,000.00 |
| SPECIAL - STRUCTURES <i>CORBEL SHIELD</i> | | | | | |
| 0016 | 530E00600 | 900.000 | SF | \$10.00000 | \$9,000.00 |
| SPECIAL - STRUCTURES <i>MASONRY BLOCK WALL</i> | | | | | |
| 0017 | 625E98200 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| LIGHTING, MISC.: <i>NAVIGATION LIGHTING REPAIR</i> | | | | | |
| 0018 | 844E10001 | 30,450.000 | SF | \$20.00000 | \$609,000.00 |
| CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLAN | | | | | |

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|--|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |
| 0019 | 848E10000 | 17,750.000 | SY | \$25.00000 | \$443,750.00 |
| MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | | | | | |
| 0020 | 848E50320 | 17,750.000 | SY | \$10.00000 | \$177,500.00 |
| EXISTING CONCRETE OVERLAY REMOVED | | | | | |
| 0021 | 614E11000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MAINTAINING TRAFFIC | | | | | |
| 0022 | 619E16020 | 24.000 | MNTH | \$2,500.00000 | \$60,000.00 |
| FIELD OFFICE, TYPE C | | | | | |
| 0023 | 624E10000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MOBILIZATION | | | | | |

Total for Group 0001:\$10,461,340.00

CY 2017-2021 Business Plan Inflation Calculator:

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Last Modified: 1/19/2017

Today's Date:
May 17, 2017

Please Enter Values in the Yellow Areas Only:

Estimation Start Date:

Less than or Equal to Today's Date
(mm/dd/yyyy)

5/17/2017

Start Date:

Enter Construction Mid-Point Date:

(cannot exceed 05/17/2042)
(mm/dd/yyyy)

7/1/2020

Construction Mid-Point Date:

Present-Day Estimated Cost:

\$13,770,000.00

Estimated Dollar Amount:

Estimate Start Date to Construction Mid-Point Date:

38

Months

Inflation - Start to Mid-Point of Construction:

(compounded growth rate)

Inflated Dollar Amount:

Business Plan

11.9%

\$15,403,680.28

Estimator's Name:

County - Route - Section:

CUY-6-14.56

PID:

99972

Estimator's Notes:

Alternative No. 2D

Estimate ODOT1602

Estimated Cost:\$11,474,700.00

Contingency: 20.00%

Estimated Total: \$13,769,640.00

Alternative No. 2D

Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17

Checked by WJV on 05/17/17

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|-----------------------|--|-----------------|--------------|-------------------|------------------|
| | Description <u>Supplemental Description</u> | | | | |
| Group 0001: STRUCTURE | | | | | |
| 0001 | 511E81100 | 170.000 | FT | \$400.00000 | \$68,000.00 |
| | CONCRETE, MISC.: <i>WEST STATION CONCRETE BEAM REPLACEMENT</i> | | | | |
| 0002 | 511E81300 | 25.000 | EACH | \$3,000.00000 | \$75,000.00 |
| | CONCRETE, MISC.: <i>LOWER DECK CORBEL REPLACEMENT</i> | | | | |
| 0003 | 511E81300 | 7.000 | EACH | \$8,500.00000 | \$59,500.00 |
| | CONCRETE, MISC.: <i>COLUMN REPLACEMENT</i> | | | | |
| 0004 | 512E10101 | 19,910.000 | SY | \$15.00000 | \$298,650.00 |
| | SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | | | | |
| 0005 | 512E10600 | 800.000 | FT | \$70.00000 | \$56,000.00 |
| | CONCRETE REPAIR BY EPOXY INJECTION <i>(ARCH RIB)</i> | | | | |
| 0006 | 512E74000 | 16,210.000 | SY | \$20.00000 | \$324,200.00 |
| | REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | | | | |
| 0007 | 516E47000 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| | JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | | | | |
| 0008 | 519E00100 | 55,693.000 | SF | \$45.00000 | \$2,506,185.00 |
| | SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(ARCH RIBS)</i> | | | | |
| 0009 | 519E00100 | 20,568.000 | SF | \$45.00000 | \$925,560.00 |
| | SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(END COLUMNS)</i> | | | | |
| 0010 | 519E00100 | 55,919.000 | SF | \$45.00000 | \$2,516,355.00 |
| | SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(FLOOR BEAMS)</i> | | | | |
| 0011 | 519E11600 | 15,300.000 | SF | \$90.00000 | \$1,377,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>(WEST STATION, TUNNELS, AND UPPER DECK)</i> | | | | |
| 0012 | 519E11600 | 9,590.000 | SF | \$100.00000 | \$959,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, VERTICAL SURFACES)</i> | | | | |
| 0013 | 519E11600 | 5,560.000 | SF | \$125.00000 | \$695,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)</i> | | | | |
| 0014 | 519E11900 | 6.000 | CY | \$5,000.00000 | \$30,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>(DEEP PIER SHAFT DETERIORATION)</i> | | | | |
| 0015 | 530E00200 | 1.000 | LS | \$5,000.00000 | \$5,000.00 |
| | SPECIAL - STRUCTURES <i>BRIDGE OPERATOR'S CAR SHELTER</i> | | | | |
| 0016 | 530E00400 | 200.000 | EACH | \$200.00000 | \$40,000.00 |
| | SPECIAL - STRUCTURES <i>CORBEL SHIELD</i> | | | | |
| 0017 | 530E00600 | 900.000 | SF | \$10.00000 | \$9,000.00 |
| | SPECIAL - STRUCTURES <i>MASONRY BLOCK WALL</i> | | | | |
| 0018 | 625E98200 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| | LIGHTING, MISC.: | | | | |

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|--|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |
| <i>NAVIGATION LIGHTING REPAIR</i> | | | | | |
| 0019 | 844E10001 | 30,450.000 | SF | \$20.00000 | \$609,000.00 |
| CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLA N | | | | | |
| 0020 | 848E10000 | 17,750.000 | SY | \$25.00000 | \$443,750.00 |
| MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | | | | | |
| 0021 | 848E50320 | 17,750.000 | SY | \$10.00000 | \$177,500.00 |
| EXISTING CONCRETE OVERLAY REMOVED | | | | | |
| 0022 | 614E11000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MAINTAINING TRAFFIC | | | | | |
| 0023 | 619E16020 | 24.000 | MNTH | \$2,500.00000 | \$60,000.00 |
| FIELD OFFICE, TYPE C | | | | | |
| 0024 | 624E10000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| MOBILIZATION | | | | | |

Total for Group 0001:\$11,474,700.00

CY 2017-2021 Business Plan Inflation Calculator:

[Not sure if you have the latest calculator? Click here.](#)

Last Modified: 1/19/2017

Today's Date:
May 17, 2017

Please Enter Values in the Yellow Areas Only:

Estimation Start Date:

Less than or Equal to Today's Date
(mm/dd/yyyy)

5/17/2017

Start Date:

Enter Construction Mid-Point Date:

(cannot exceed 05/17/2042)
(mm/dd/yyyy)

7/1/2020

Construction Mid-Point Date:

Present-Day Estimated Cost:

\$17,440,000.00

Estimated Dollar Amount:

Estimate Start Date to Construction Mid-Point Date:

38

Months

Inflation - Start to Mid-Point of Construction:

(compounded growth rate)

Inflated Dollar Amount:

Business Plan

11.9%

\$19,509,091.07

Estimator's Name:

County - Route - Section:

CUY-6-14.56

PID:

99972

Estimator's Notes:

Alternative No. 2E

Estimate ODOT1602

Estimated Cost:\$14,532,550.00

Contingency: 20.00%

Estimated Total: \$17,439,060.00

Alternative No. 2E

Base Date: 05/17/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type: URBAN CLASS

Season: SUMMER

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number: 99972

Prepared by BPS on 05/17/17

Checked by WJV on 05/17/17

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|---------------|---------------------------------|-----------------|--------------|-------------------|------------------|
| | <u>Description</u> | | | | |
| | <u>Supplemental Description</u> | | | | |

Group 0001: STRUCTURE

| | | | | | |
|------|--|------------|------|----------------|----------------|
| 0001 | 511E81100 | 170.000 | FT | \$400.00000 | \$68,000.00 |
| | CONCRETE, MISC.: <i>WEST STATION CONCRETE BEAM REPLACEMENT</i> | | | | |
| 0002 | 511E81300 | 25.000 | EACH | \$3,000.00000 | \$75,000.00 |
| | CONCRETE, MISC.: <i>LOWER DECK CORBEL REPLACEMENT</i> | | | | |
| 0003 | 511E81300 | 7.000 | EACH | \$8,500.00000 | \$59,500.00 |
| | CONCRETE, MISC.: <i>COLUMN REPLACEMENT</i> | | | | |
| 0004 | 512E10101 | 27,480.000 | SY | \$15.00000 | \$412,200.00 |
| | SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | | | | |
| 0005 | 512E10600 | 800.000 | FT | \$70.00000 | \$56,000.00 |
| | CONCRETE REPAIR BY EPOXY INJECTION <i>(ARCH RIB)</i> | | | | |
| 0006 | 512E74000 | 23,790.000 | SY | \$20.00000 | \$475,800.00 |
| | REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | | | | |
| 0007 | 516E47000 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| | JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | | | | |
| 0008 | 519E00100 | 55,693.000 | SF | \$45.00000 | \$2,506,185.00 |
| | SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(ARCH RIBS)</i> | | | | |
| 0009 | 519E00100 | 62,060.000 | SF | \$45.00000 | \$2,792,700.00 |
| | SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(LOWER DECK SUPPORT COLUMNS)</i> | | | | |
| 0010 | 519E00100 | 20,568.000 | SF | \$45.00000 | \$925,560.00 |
| | SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(END COLUMNS)</i> | | | | |
| 0011 | 519E00100 | 55,919.000 | SF | \$45.00000 | \$2,516,355.00 |
| | SPECIAL - COMPOSITE FIBER WRAP SYSTEM <i>(FLOOR BEAMS)</i> | | | | |
| 0012 | 519E11600 | 15,300.000 | SF | \$90.00000 | \$1,377,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>(WEST STATION, TUNNELS, AND UPPER DECK)</i> | | | | |
| 0013 | 519E11600 | 9,590.000 | SF | \$100.00000 | \$959,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, VERTICAL SURFACES)</i> | | | | |
| 0014 | 519E11600 | 5,560.000 | SF | \$125.00000 | \$695,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>(LOWER SUPERSTRUCTURE, BOTTOM AND CURVED SURFACES)</i> | | | | |
| 0015 | 519E11900 | 6.000 | CY | \$5,000.00000 | \$30,000.00 |
| | SPECIAL - PATCHING CONCRETE STRUCTURE <i>(DEEP PIER SHAFT DETERIORATION)</i> | | | | |
| 0016 | 530E00200 | 1.000 | LS | \$5,000.00000 | \$5,000.00 |
| | SPECIAL - STRUCTURES <i>BRIDGE OPERATOR'S CAR SHELTER</i> | | | | |
| 0017 | 530E00400 | 200.000 | EACH | \$200.00000 | \$40,000.00 |
| | SPECIAL - STRUCTURES <i>CORBEL SHIELD</i> | | | | |
| 0018 | 530E00600 | 900.000 | SF | \$10.00000 | \$9,000.00 |
| | SPECIAL - STRUCTURES | | | | |

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|---------------|--|-----------------|--------------|-------------------|------------------|
| | Description <u>Supplemental Description</u> | | | | |
| | MASONRY BLOCK WALL | | | | |
| 0019 | 625E98200 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| | LIGHTING, MISC.: NAVIGATION LIGHTING REPAIR | | | | |
| 0020 | 844E10001 | 30,450.000 | SF | \$20.00000 | \$609,000.00 |
| | CONCRETE PATCHING WITH GALVANIC ANODE PROTECTION, AS PER PLA N | | | | |
| 0021 | 848E10000 | 17,750.000 | SY | \$25.00000 | \$443,750.00 |
| | MICRO SILICA MODIFIED CONCRETE OVERLAY USING HYDRODEMOLITION | | | | |
| 0022 | 848E50320 | 17,750.000 | SY | \$10.00000 | \$177,500.00 |
| | EXISTING CONCRETE OVERLAY REMOVED | | | | |
| 0023 | 614E11000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| | MAINTAINING TRAFFIC | | | | |
| 0024 | 619E16020 | 24.000 | MNTH | \$2,500.00000 | \$60,000.00 |
| | FIELD OFFICE, TYPE C | | | | |
| 0025 | 624E10000 | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| | MOBILIZATION | | | | |

Total for Group 0001:\$14,532,550.00

CY 2017-2021 Business Plan Inflation Calculator:

[Not sure if you have the latest calculator? Click here.](#)

Last Modified: 1/19/2017

Today's Date:
February 15, 2017

Please Enter Values in the Yellow Areas Only:

Estimation Start Date:

Less than or Equal to Today's Date
(mm/dd/yyyy)

2/15/2017

Start Date:

Enter Construction Mid-Point Date:

(cannot exceed 02/15/2042)
(mm/dd/yyyy)

7/1/2020

Construction Mid-Point Date:

Present-Day Estimated Cost:

\$29,519,400.00

Estimated Dollar Amount:

Estimate Start Date to Construction Mid-Point Date:

41

Months

Inflation - Start to Mid-Point of Construction:

(compounded growth rate)

Inflated Dollar Amount:

Business Plan

12.6%

\$33,226,075.52

Estimator's Name:

County - Route - Section:

CUY-6-1456

PID:

99972

Estimator's Notes:

Alternate 3 - Rehab w/ Patching and Cathodic Protection

Estimate ODOT1602

Estimated Cost:\$24,599,500.00

Contingency: 20.00%

Estimated Total: \$29,519,400.00

ALTERNATE 3 - REHAB W/ PATCHING AND ACTIVE CATHODIC PROTECTION

Base Date: 02/13/17

Spec Year: 16

Unit System: E

Work Type: BRIDGE REHABILITATION

Highway Type:

Urban/Rural Type:

Season:

County: CUYAHOGA

Latitude of Midpoint: 412929

Longitude of Midpoint: -814242

District: 12

Federal/State Project Number:

Prepared by DEA on 02/13/17

Checked by WJV on 02/14/17

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|---|--------------------|-----------------|--------------|-------------------|------------------|
| <u>Description</u> | | | | | |
| <u>Supplemental Description</u> | | | | | |
| Group 0001: STRUCTURE | | | | | |
| 0005 | 511E81100 | 150.000 | FT | \$400.00000 | \$60,000.00 |
| CONCRETE, MISC.: <i>WEST STATION CONCRETE BEAM REPLACEMENT</i> | | | | | |
| 0006 | 511E81300 | 25.000 | EACH | \$3,000.00000 | \$75,000.00 |
| CONCRETE, MISC.: <i>LOWER DECK CORBEL REPLACEMENT</i> | | | | | |
| 0007 | 511E81300 | 4.000 | EACH | \$8,500.00000 | \$34,000.00 |
| CONCRETE, MISC.: <i>COLUMN REPLACEMENT</i> | | | | | |
| 0008 | 512E10101 | 2,000.000 | SY | \$15.00000 | \$30,000.00 |
| SEALING OF CONCRETE SURFACES (EPOXY-URETHANE), AS PER PLAN | | | | | |
| 0009 | 512E10600 | 800.000 | FT | \$70.00000 | \$56,000.00 |
| CONCRETE REPAIR BY EPOXY INJECTION <i>ARCH RIB</i> | | | | | |
| 0010 | 512E74000 | 2,000.000 | SY | \$20.00000 | \$40,000.00 |
| REMOVAL OF EXISTING COATINGS FROM CONCRETE SURFACES | | | | | |
| 0011 | 516E47000 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| JACKING AND TEMPORARY SUPPORT OF SUPERSTRUCTURE | | | | | |
| 0013 | 519E11600 | 15,000.000 | SF | \$90.00000 | \$1,350,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>WEST STATION, TUNNELS AND UPPER DECK</i> | | | | | |
| 0014 | 519E11600 | 9,500.000 | SF | \$100.00000 | \$950,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>LOWER SUPERSTRUCTURE, VERTICAL SURFACES</i> | | | | | |
| 0015 | 519E11600 | 5,500.000 | SF | \$125.00000 | \$687,500.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>LOWER SUPERSTRUCTURE - BOTTOM AND CURVED SURFACES</i> | | | | | |
| 0016 | 519E11900 | 6.000 | CY | \$5,000.00000 | \$30,000.00 |
| SPECIAL - PATCHING CONCRETE STRUCTURE <i>DEEP PIER SHAFT DETERIORATION</i> | | | | | |
| 0017 | 530E00200 | 1.000 | LS | \$5,000.00000 | \$5,000.00 |
| SPECIAL - STRUCTURES <i>BRIDGE OPERATOR'S CAR SHELTER</i> | | | | | |
| 0018 | 530E00400 | 200.000 | EACH | \$200.00000 | \$40,000.00 |
| SPECIAL - STRUCTURES <i>CORBEL SHIELD</i> | | | | | |
| 0019 | 530E00600 | 900.000 | SF | \$10.00000 | \$9,000.00 |
| SPECIAL - STRUCTURES <i>MASONRY BLOCK WALL</i> | | | | | |
| 0020 | 530E00600 | 325,000.000 | SF | \$60.00000 | \$19,500,000.00 |
| SPECIAL - STRUCTURES <i>CATHODIC PROTECTION WITH IMPRESSED CURRENT</i> | | | | | |
| 0021 | 625E98200 | 1.000 | LS | \$20,000.00000 | \$20,000.00 |
| LIGHTING, MISC.: <i>NAVIGATION LIGHTING REPAIR</i> | | | | | |
| 0023 | 848E10000 | 19,400.000 | SY | \$60.00000 | \$1,164,000.00 |
| <i>MICRO SILICA MODIFIED CONCRETE OVELAY USING HYDRODEMOLITION</i> | | | | | |

| <u>Line #</u> | <u>Item Number</u> | <u>Quantity</u> | <u>Units</u> | <u>Unit Price</u> | <u>Extension</u> |
|---------------|---|-----------------|--------------|-------------------|------------------|
| | <u>Description</u> <u>Supplemental Description</u> | | | | |
| 0024 | 848E50320 EXISTING CONCRETE OVERLAY REMOVED | 19,400.000 | SY | \$10.00000 | \$194,000.00 |

Total for Group 0001:\$24,264,500.00

Group 0002: INCIDENTAL

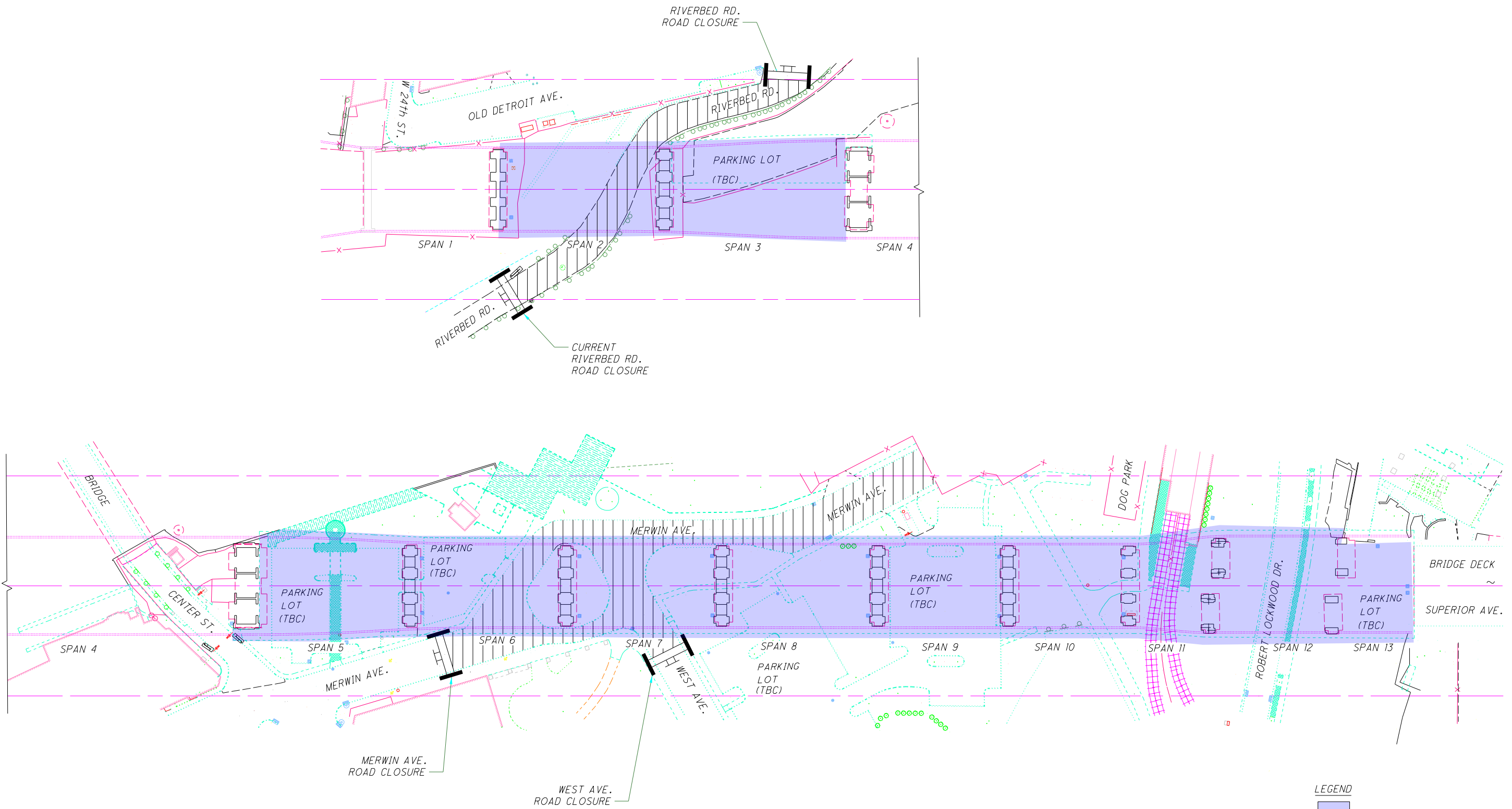
| | | | | | |
|------|---|--------|------|-----------------|--------------|
| 0025 | 614E11000 MAINTAINING TRAFFIC | 1.000 | LS | \$100,000.00000 | \$100,000.00 |
| 0026 | 614E18002 MAINTAINING TRAFFIC, MISC.: RAILROAD FLAGGER | 1.000 | LS | \$50,000.00000 | \$50,000.00 |
| 0027 | 614E18002 MAINTAINING TRAFFIC, MISC.: RAILROAD COORDINATION | 1.000 | LS | \$25,000.00000 | \$25,000.00 |
| 0028 | 619E16020 FIELD OFFICE, TYPE C | 24.000 | MNTH | \$2,500.00000 | \$60,000.00 |
| 0029 | 624E10000 MOBILIZATION | 1.000 | LS | \$100,000.00000 | \$100,000.00 |

Total for Group 0002:\$335,000.00





APPENDIX B

PUBLIC AREA BELOW STRUCTURE

P:\Projects\000T1602-CUY-6-1456\DESIGN\CT\ProjectData\99972\Design\M01\Sheets\99972MP004.dgn Model 2/14/2017 3:01:07 PM SDudek



LEGEND

-  - PUBLIC AREAS
-  - ROAD CLOSED
-  - ROAD CLOSURE BARRIER AND ROAD CLOSED SIGN
-  (TBC) - TO BE CLOSED, WHEN REQUIRED

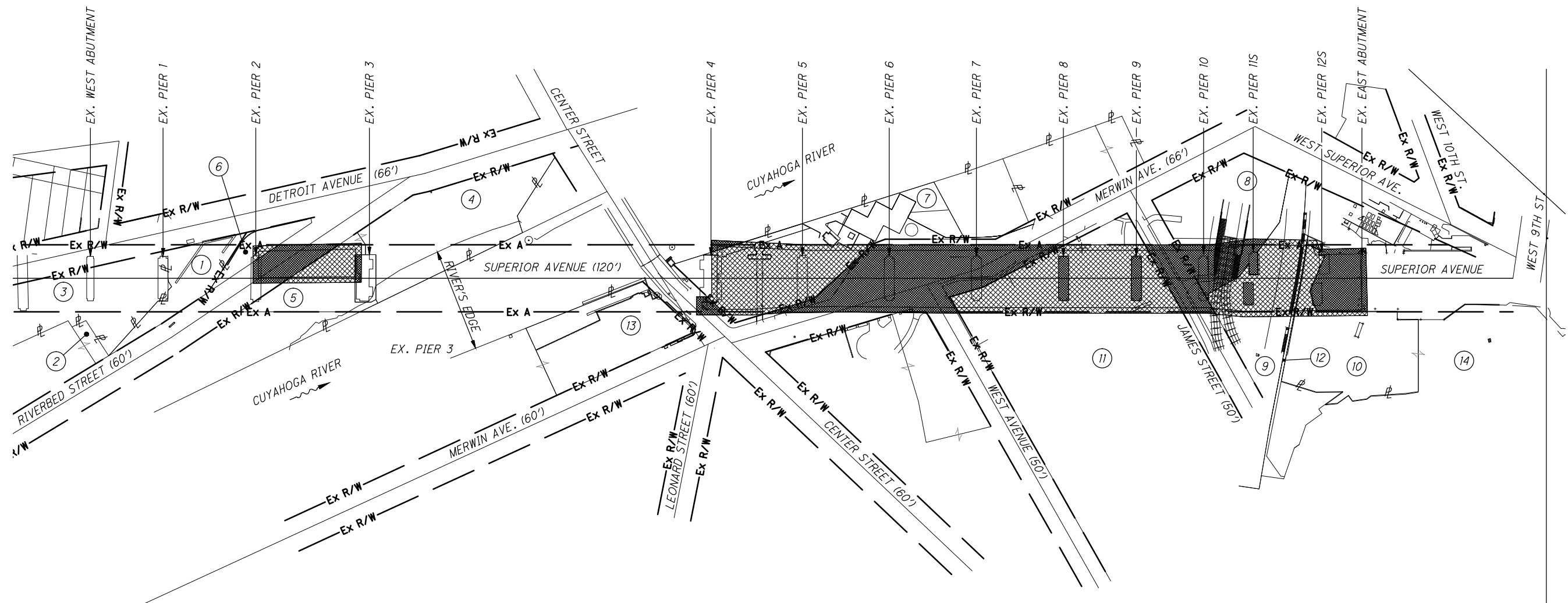


MAINTENANCE OF TRAFFIC PUBLIC AREAS AND CLOSURES

CUY-6-14.56



**CUY-006-14.56
CITY OF CLEVELAND
CUYAHOGA COUNTY**



- | | | |
|--|--|--|
| ① 003-20-002 L.A.N.D. STUDIO INC. | ⑥ 003-20-009 NO INFORMATION (NEWLY CREATED PARCEL) | ⑪ 101-15-021 CITY OF CLEVELAND |
| ② 003-20-003 CLEVELAND METRO HOUSING AUTHORITY | ⑦ 101-15-002 BOARD OF PARK COMMISSIONERS OF CLEVELAND METROPOLITAN PARK DISTRICT | ⑫ 101-15-028 R.T.A. |
| ③ 003-20-004 CUYAHOGA COUNTY BOARD OF COMMISSIONERS | ⑧ 101-15-008 THE GREATER CLEVELAND REGIONAL TRANSIT AUTHORITY | ⑬ 101-16-001 MARLIN INVESTMENT GROUP, LLC |
| ④ 003-20-006 STONEBRIDGE WATERFRONT, LLC | ⑨ 101-15-009 FLATS EAST DEVELOPMENT, LLC | ⑭ 101-20-013 UNITED STATES OF AMERICA |
| ⑤ 003-20-008 STONEBRIDGE WATERFRONT, LLC | ⑩ 101-15-011 UNITED STATES OF AMERICA | |

F:\Jobs\997 - CUY-6 Survey and RW\Right of Way\997-PROPMAP.dwg 16-May-17 8:21 AM

0 100 200
50
HORIZONTAL
SCALE IN FEET

CALCULATED
VMB
CHECKED
APP

PROPERTY MAP EXHIBIT

CUY-006-14.56



APPENDIX C

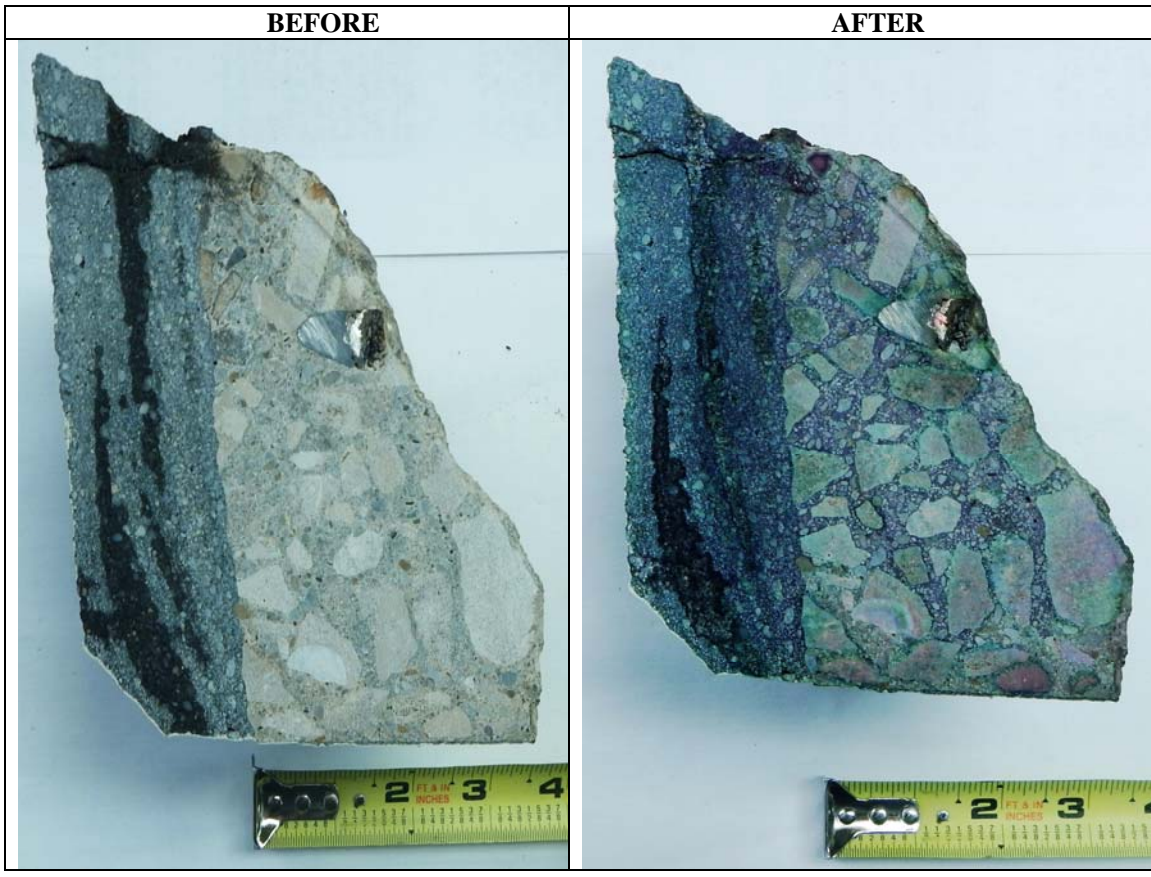
CONCRETE PH RESULTS

pH TEST
per
GERMANN INSTRUMENTS Manual



| | | | |
|----------------------|--|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 1A | Date. | 1/30/2017 |
| Core Location | Span 7, Arch Rib, South Interior Concrete (Bottom North Corner, Near Center) | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The aggregates in the concrete in between depths of 0 to 3.5 inches have dominant green color with less purple color indicating a pH of 9 to 10.

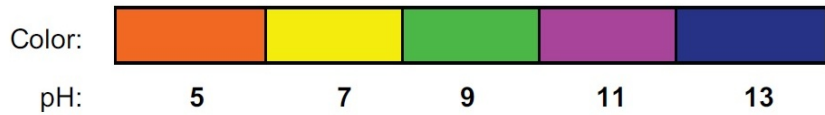
In surrounding area of the aggregates have a dark purple color indicating a pH of 11.

pH TEST
per
GERMANN INSTRUMENTS Manual



| | | | |
|----------------------|---|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 1B | Date. | 1/30/2017 |
| Core Location | Span 7, Arch Rib, South Interior Shotcrete (Bottom North Corner, Near Center) | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The upper depth of shotcrete from 0.0 to 0.25 inches has dominant green color indicating a pH of 9.

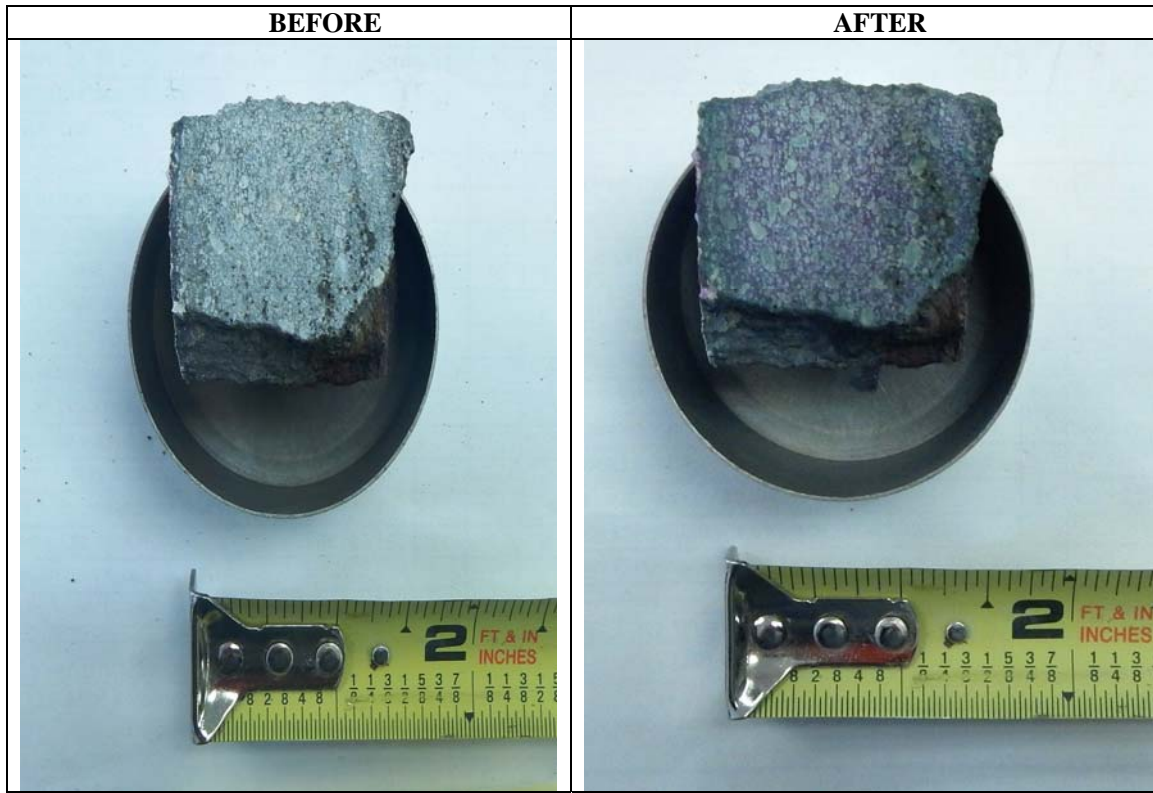
The inner part of shotcrete from 0.25 to 1.5 inches has a dominant dark purple color indicating a pH of 12.

pH TEST
per
GERMANN INSTRUMENTS Manual



| | | | |
|----------------------|--|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Pennoni | Project No. | G17005T |
| Sample No. | 2 | Date. | 1/30/2017 |
| Core Location | Span 7, LD Floor Beam, 4 North Bay Shotcrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The upper depth of shotcrete from 0.0 to 0.25 inches has a green color indicating a pH of 9.

The inner part of shotcrete from 0.25 to 1.5 inches has a dominant dark purple color indicating a pH of 12.

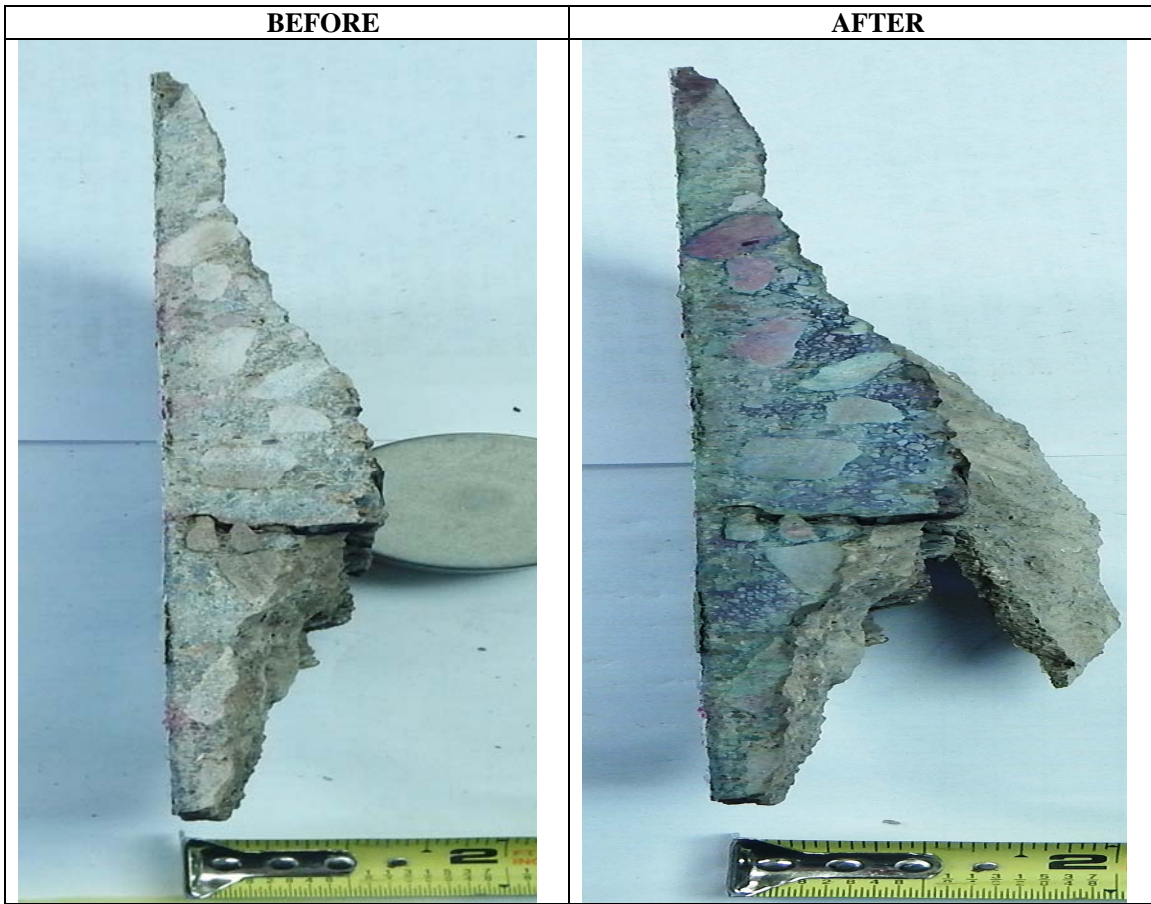
Also note that the aggregates in between depths of 0.25 and 1.5 inches have a green color indicating a pH of 9.

pH TEST
per
GERMANN INSTRUMENTS Manual



| | | | |
|----------------------|---|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 3 | Date. | 1/30/2017 |
| Core Location | Span 7, LD Column, North Interior 14 Concrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The upper depth of the concrete from 0.0 to 0.5 inches has a dominant green color indicating a pH of 9.

The lower depth of the concrete from 0.5 to 1.25 inches has a dominant dark purple color indicating a pH of 12.

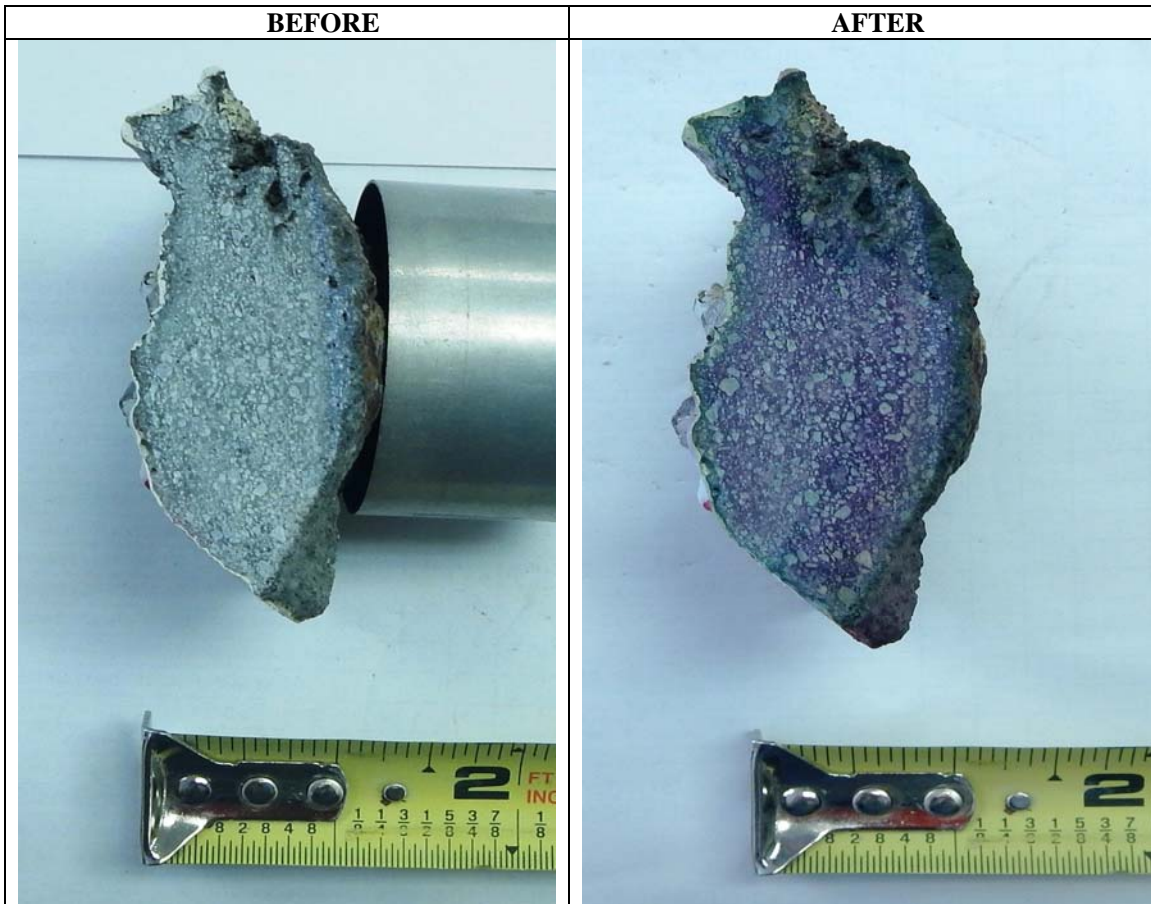
The aggregates in concrete between depths of 0 to 1.25 inches have green and purple colors indicating a pH of 9 to 10.

pH TEST
per
GERMANN INSTRUMENTS Manual



| | | | |
|----------------------|---|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 4 | Date. | 1/30/2017 |
| Core Location | Span 8, Jack Arch, North Interior Shotcrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The upper depth of shotcrete from 0.0 to 0.15 inches has a dominant green color indicating a pH of 9.

The inner part of shotcrete from 0.15 to 1.0 inches has a dominant dark purple color indicating a pH of 12.

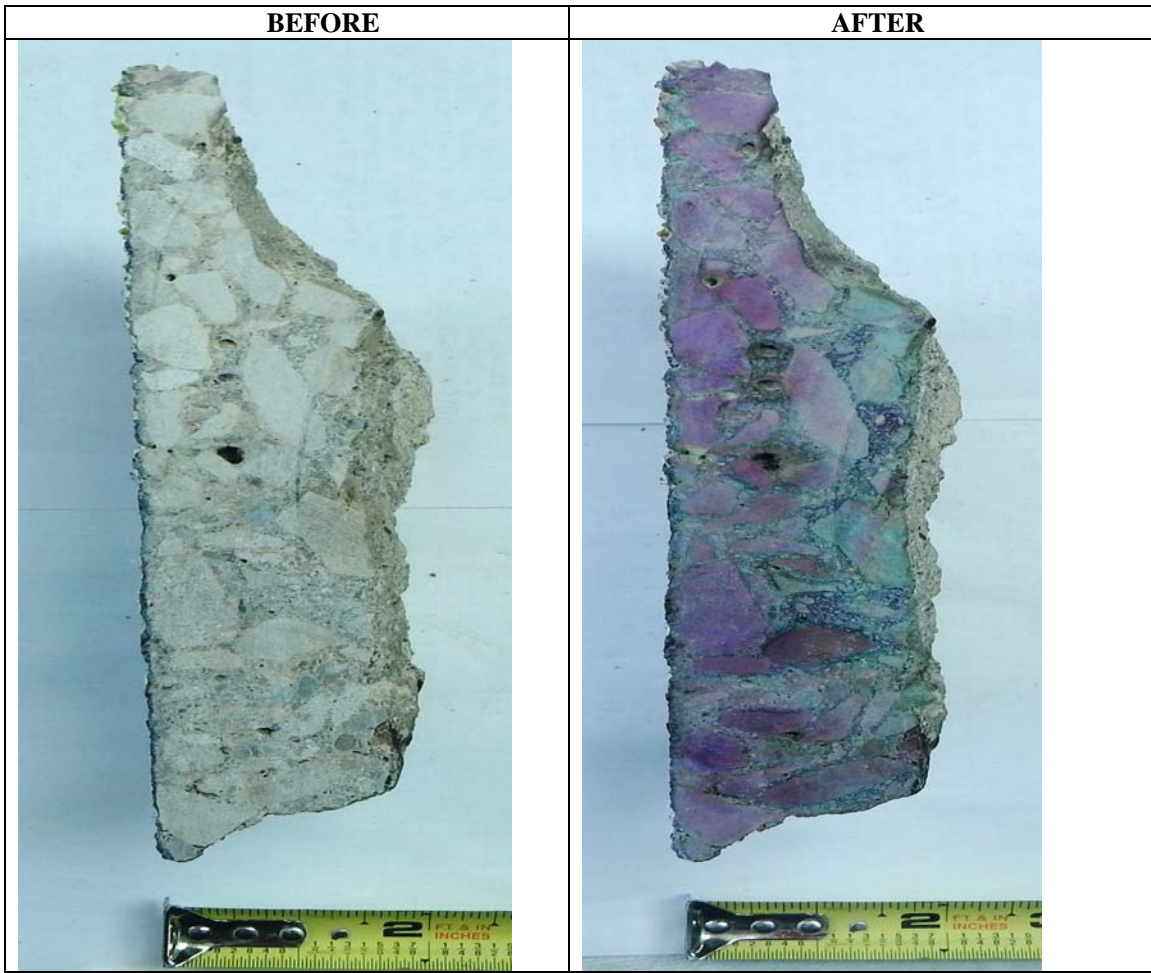
Also note that the aggregates in between depths of 0.15 to 1.0 inches have green color indicating a pH of 9.

pH TEST
per
GERMANN INSTRUMENTS Manual



| | | | |
|----------------------|--|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 5 | Date. | 1/30/2017 |
| Core Location | Span 8, LD Floor Beam, 9 Center Bay Concrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

Most of the aggregates between depths of 0 to 1.0 inches have a dominant purple color with less green color in the surrounding area indicating a pH of 10 to 11.

Some of the aggregates in between depths of 1.0 to 2.0 inches have a green color indicating a pH of 9.

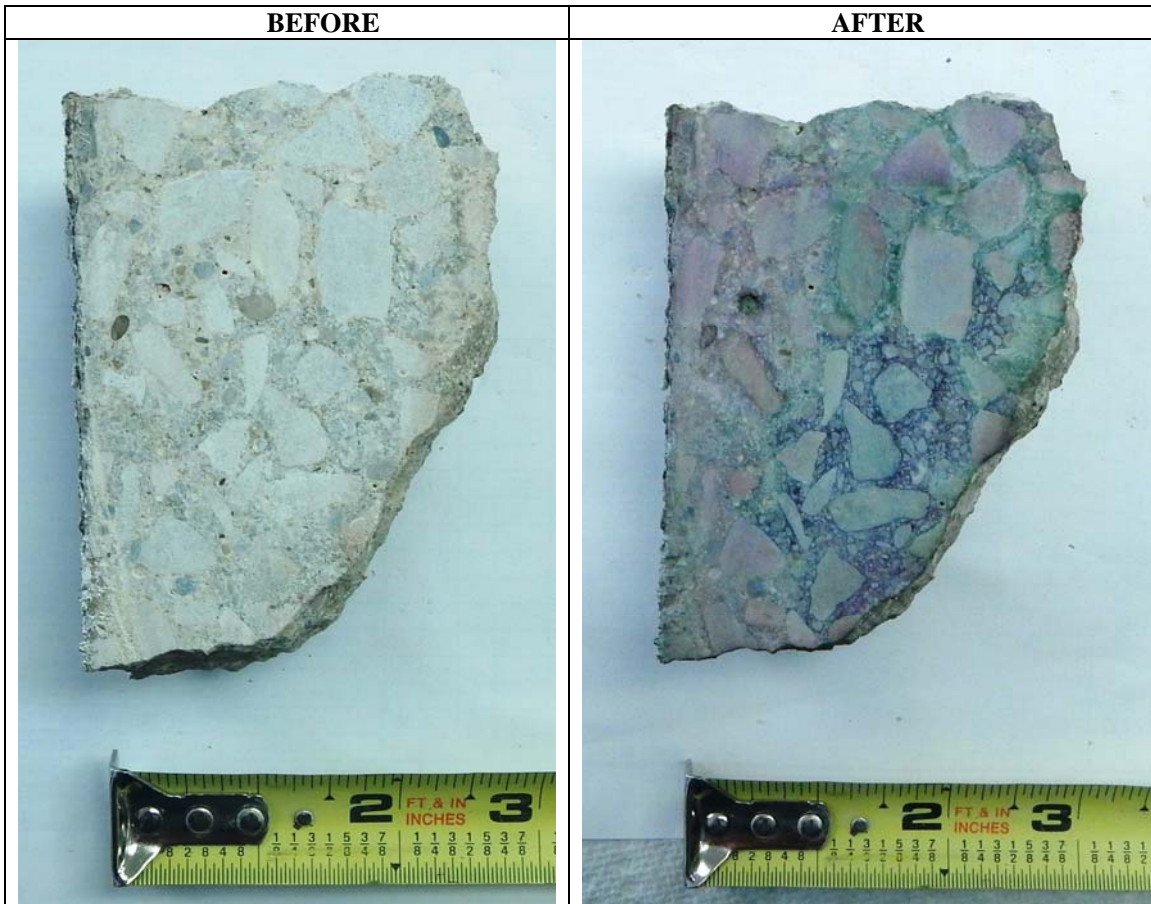
The dark purple color corresponding to a pH of 12 is dominant between depths of 1.0 to 2.0 inches.

pH TEST
per
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| | | | |
|----------------------|---|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 6 | Date. | 1/30/2017 |
| Core Location | Span 8, LD Floor Beam, 10 Center Bay Concrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

Most of the aggregates between depths of 0 to 1.0 inches have a dominant purple color with less green color in the surrounding area indicating a pH of 10 to 11.

The dark purple color, corresponding to a pH of 12, is dominant between depths of 1.0 to 3.0 inches.

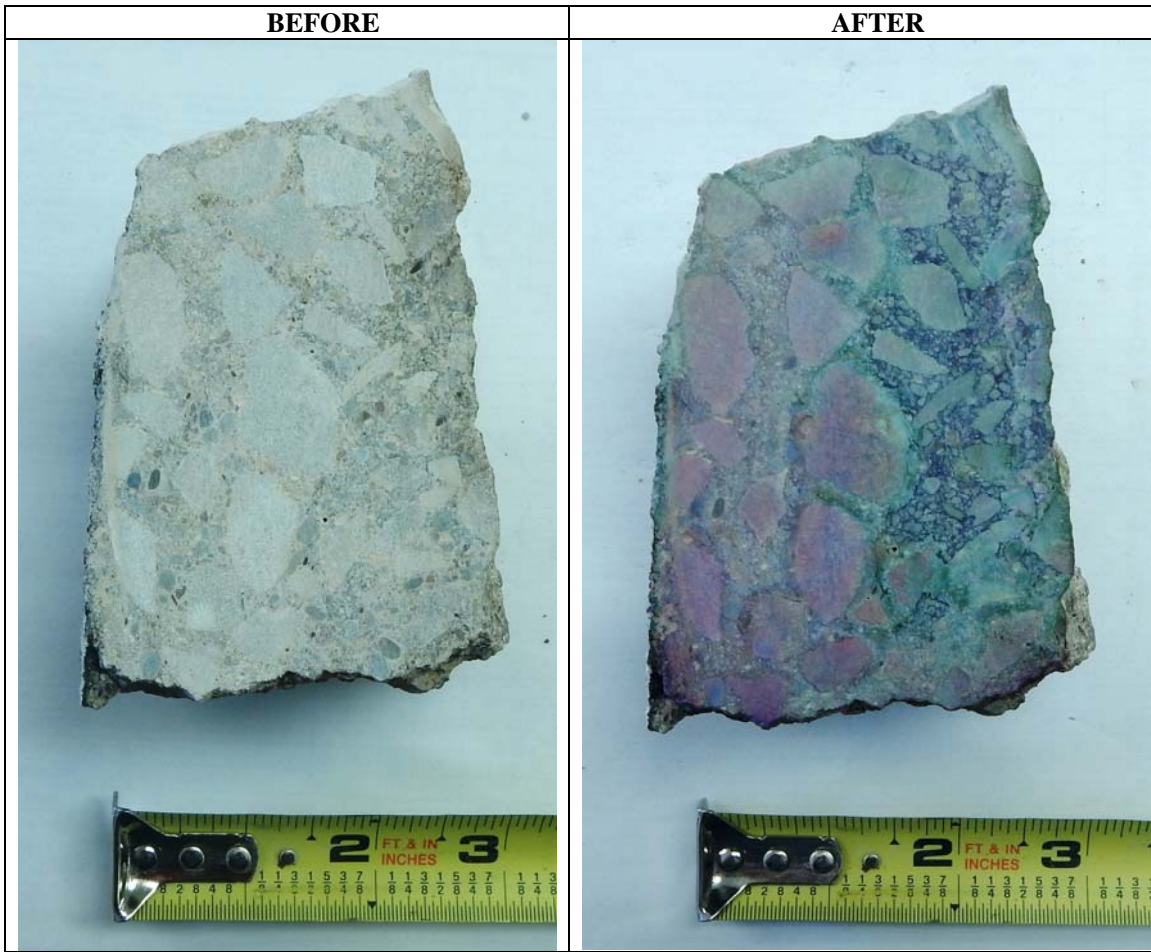
Also note that some of the aggregates in between depths of 2 to 3.5 inches have a green color indicating a pH of 9.

pH TEST
per
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| | | | |
|----------------------|---|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 7 | Date. | 1/30/2017 |
| Core Location | Span 8, LD Floor Beam, 11 Center Bay Concrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

Most of the aggregates between depths of 0 to 2 inches have a dominant purple color with less green color in the surrounding area indicating a pH of 10 to 11.

The dark purple color, corresponding to a pH of 12, is dominant between depths of 2 to 3.0 inches.

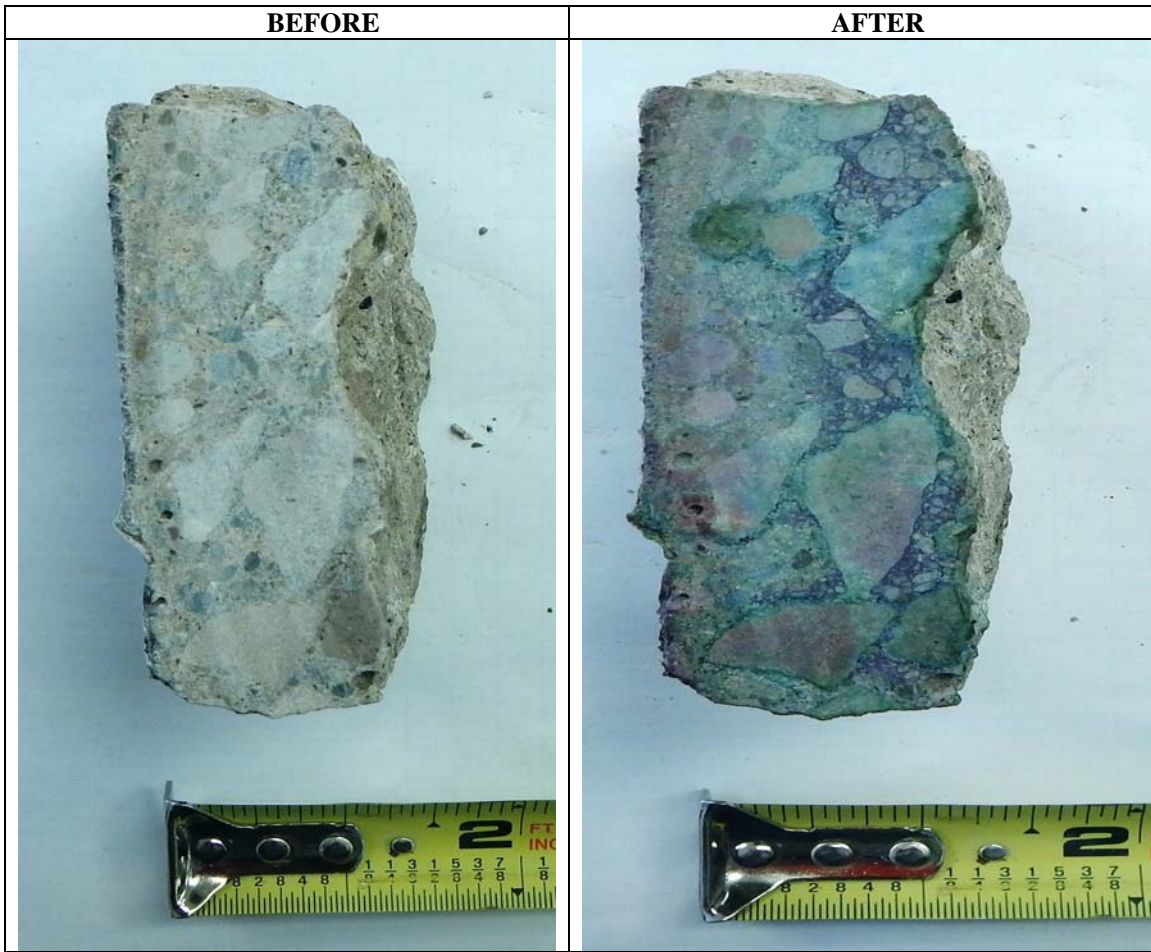
Also note that some of the aggregates in between depths of 2 to 3.0 inches have a green color indicating a pH of 9.

pH TEST
per
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| | | | |
|----------------------|--|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 8 | Date. | 1/30/2017 |
| Core Location | Span 8, LD Floor Beam, 14 South Bay Concrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The depth between 0 and 0.75 inches have green and purple colors indicating a pH of 9 to 10.

The dark purple color, corresponding to a pH of 12, is dominant at depth 0.75 to 1.5 inches.

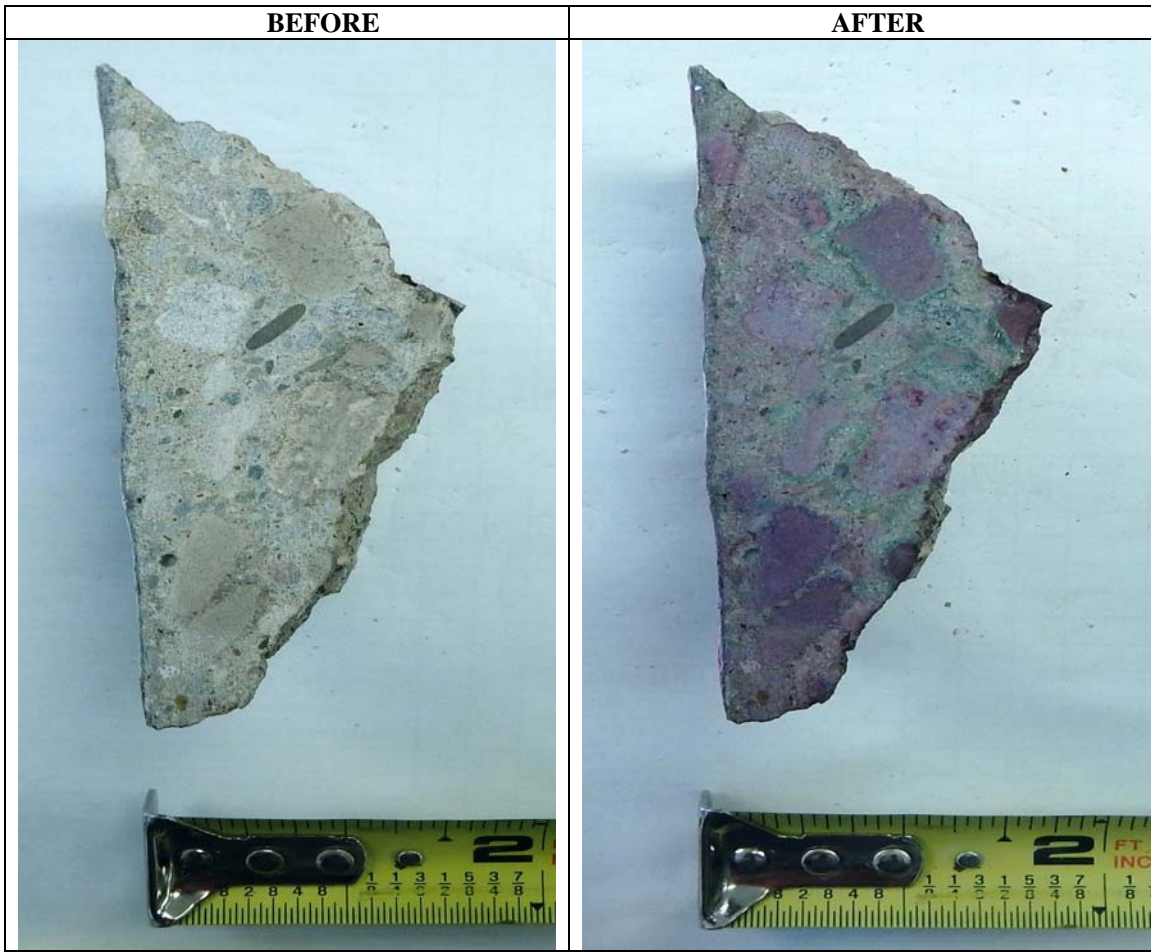
Also note that the aggregates in between depths of 0 to 1.5 inches have green and purple colors indicating a pH of 9 to 10.

pH TEST
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| | | | |
|----------------------|---|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 9 | Date. | 1/30/2017 |
| Core Location | Span 9, LD Column, North Interior 13 Concrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

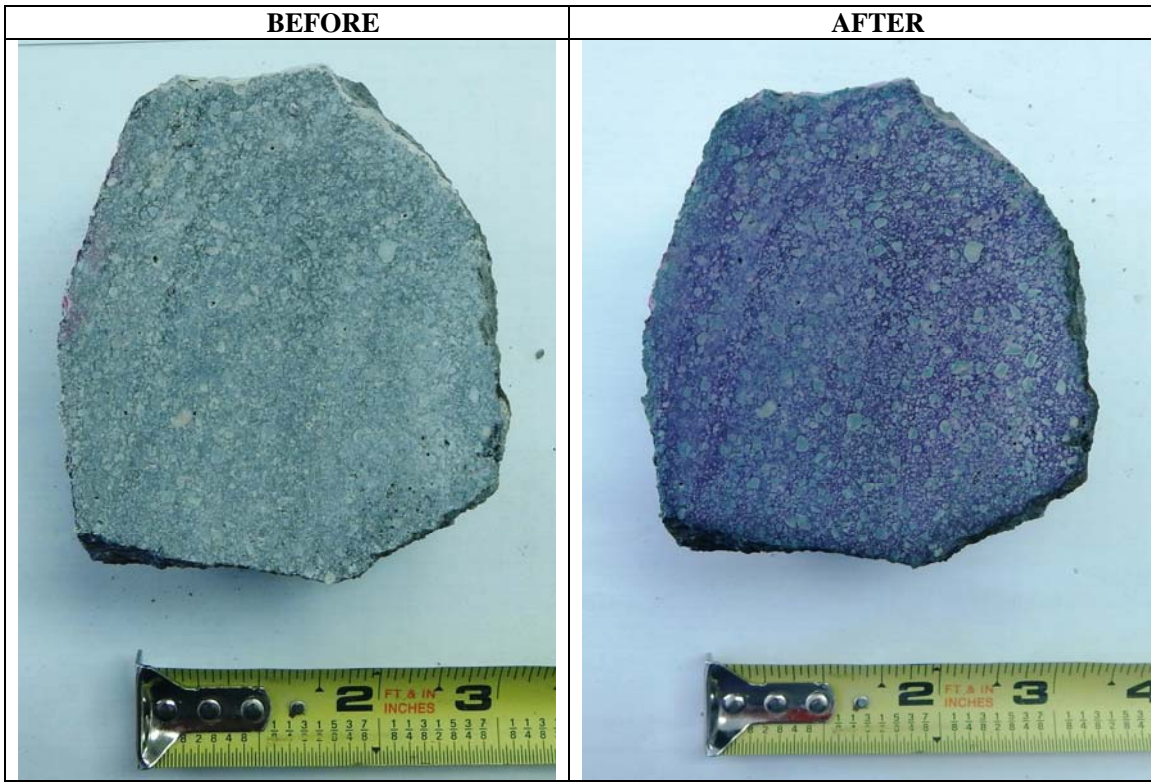
Most of the aggregates between depths of 0 to 1.5 inches have dominant purple color indicating a pH of 10 to 11 with surrounding area having green color indicating a pH of 9.

pH TEST
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| | | | |
|----------------------|---|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 10 | Date. | 1/30/2017 |
| Core Location | Span 10, LD Floor Beam, 1 South Bay Shotcrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The entire depth from 0.0 to 3.5 inches has a dominant dark purple color indicating a pH of 12.

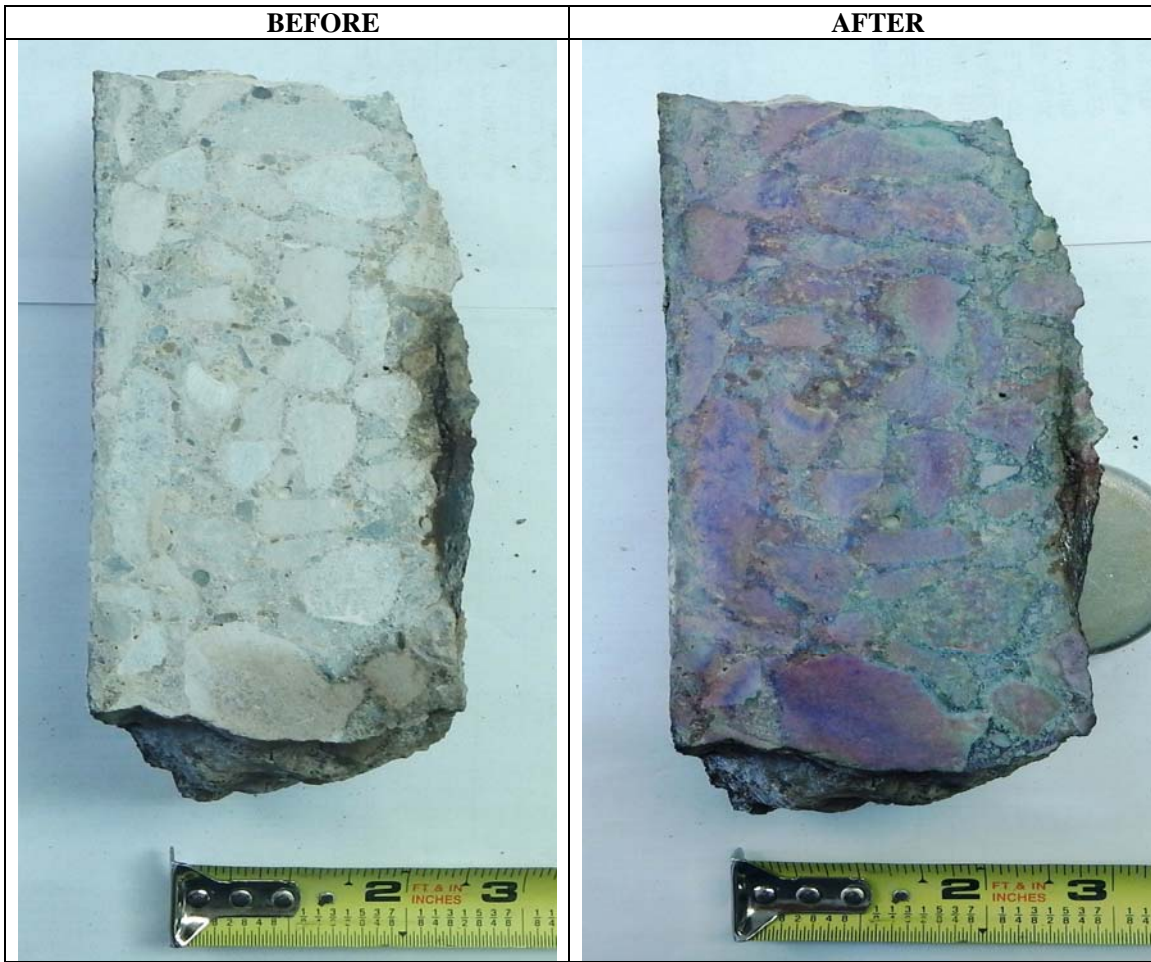
Also note that some of the aggregates have a green color indicating a pH of 9.

pH TEST
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| | | | |
|----------------------|--|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 11 | Date. | 1/30/2017 |
| Core Location | Span 10, LD Floor Beam, 2 South Bay Concrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the concrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

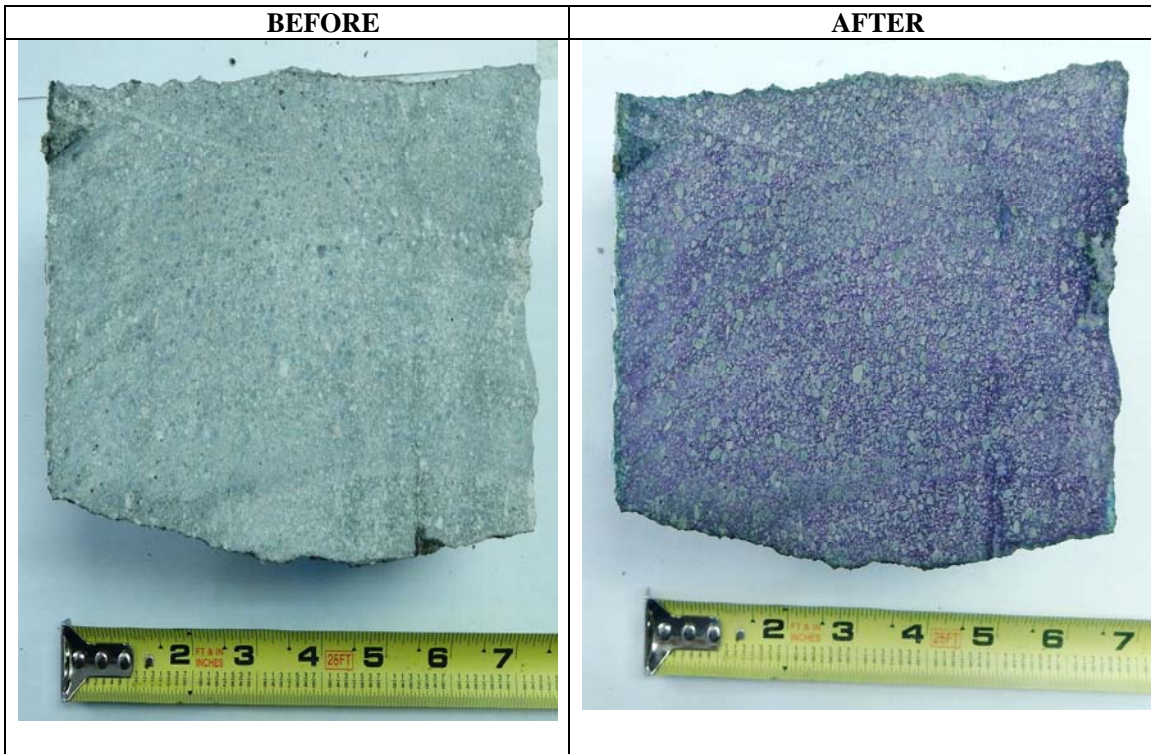
Most of the aggregates between depths of 0 to 3.0 inches have dominant purple color indicating a pH of 10 to 11 with the surrounding area having green color indicating a pH of 9.

pH TEST
per
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| | | | |
|----------------------|---------------------------------------|--------------------|---------------------|
| Project | Superior Avenue Bridge Rehabilitation | Location | Cuyahoga County, OH |
| Client | Jones Stuckey | Project No. | G17005T |
| Sample No. | 12 | Date. | 1/30/2017 |
| Core Location | Span 10, LD Pier Shaft Shotcrete | | |

Rainbow Indicator



Shown in the photo to the right, the pH profile was evaluated by the **Rainbow Indicator** on a newly cut area of the shotcrete sample provided by the client. Top surface is indicated by zero on measuring Tape.

The entire depth from 0.0 to 7.0 inches has dominant dark purple color indicating a pH of 12.

Also note that the aggregates have a green color indicating a pH of 9.

APPENDIX D

***ESTIMATED CONCRETE
PATCHING QUANTITIES***

CUY-6-1456 ARCH REPAIR

| Span | Location | Total (SF) | North Exterior Bay | North Interior Bay | South Interior Bay | South Exterior Bay |
|------|----------|------------|--------------------|--------------------|--------------------|--------------------|
| 1 | Vertical | 672 | 206 | 106 | 140 | 220 |
| | Bottom | 537 | 165 | 100 | 104 | 168 |
| 2 | Vertical | 22 | 22 | 0 | 0 | 0 |
| | Bottom | 44 | 44 | 0 | 0 | 0 |
| 3 | Vertical | 10 | 0 | 10 | | |
| | Bottom | 25 | 25 | 0 | | |
| 5 | Vertical | 123 | 16 | 39 | 68 | 0 |
| | Bottom | 136 | 16 | 17 | 25 | 78 |
| 6 | Vertical | 246 | 130 | 42 | 74 | 0 |
| | Bottom | 303 | 84 | 97 | 20 | 102 |
| 7 | Vertical | 0 | 0 | 0 | 0 | 0 |
| | Bottom | 432 | 86 | 16 | 198 | 132 |
| 8 | Vertical | 0 | 0 | 0 | 0 | 0 |
| | Bottom | 579 | 162 | 163 | 92 | 162 |
| 9 | Vertical | 26 | 0 | 0 | 26 | 0 |
| | Bottom | 116 | 0 | 70 | 26 | 20 |
| 10 | Vertical | 0 | 0 | 0 | 0 | 0 |
| | Bottom | 445 | 0 | 0 | 271 | 174 |
| 11 | Vertical | 27 | 18 | 0 | 0 | 9 |
| | Bottom | 0 | 0 | 0 | 0 | 0 |
| 12 | Vertical | 71 | 10 | 0 | 26 | 35 |
| | Bottom | 374 | 144 | 16 | 90 | 124 |
| 13 | Vertical | 81 | | 24 | 14 | 43 |
| | Bottom | 308 | | 119 | 62 | 127 |

Vertical Patches Total = 1278 SF
 Bottom Patches Total = 3299 SF
 Total = 4577 SF

Span 3 South & Exterior Arches
 are Difficult to Access, Span 13
 North Exterior Arch Rib Does
 Not Exist

CUY-6-1456 Lower Deck Column Patching

Total Deterioration: 2,143 SF

| Span | Col. No. | North Exterior | | | | | | | | | | Col. No. | North Interior | | | | | | | | | | Col. No. | South Interior | | | | | | | | | | Col. No. | South Exterior | | | | | | | | | | Span |
|------------|----------|----------------|-------------|-------------|-------------|---------------|---------|---------|---------|---------|----------|----------|----------------|-------------|-------------|-------------|---------------|---------|---------|---------|---------|----------|----------|----------------|-------------|-------------|-------------|---------------|---------|---------|----------|----------|---------|----------|----------------|----|----|----|--|--|--|--|--|--|------|
| | | Surface Total | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Deterioration | | | | | | | Surface Total | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Deterioration | | | | | | | Surface Total | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Deterioration | | | | | | | | | | | | | | | | | |
| | | | | | | H (in.) | W (in.) | H (in.) | W (in.) | H (in.) | W (in.) | | | | | | H (in.) | W (in.) | H (in.) | W (in.) | H (in.) | W (in.) | | | | | | H (in.) | W (in.) | H (in.) | W (in.) | H (in.) | W (in.) | | | | | | | | | | | | |
| Span 3 | 1 | 0 | 0 | 0 | 0 | | | | | | | 1 | 16 | 4 | 12 | 0 | 48 | 12 | 112 | 16 | | | 1 | 0 | 0 | 0 | 0 | | | | | 1 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 2 | 206 | 27 | 13 | 166 | 160 | 24 | 161 | 12 | 155 | 155 | 2 | 13 | 1 | 4 | 8 | 16 | 13 | 36 | 16 | 48 | 24 | 2 | 0 | 0 | 0 | 0 | | | | | 2 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 3 | 21 | 12 | 9 | 0 | 70 | 24 | 113 | 12 | | | 3 | 0 | 0 | 0 | 0 | | | | | | | 3 | 0 | 0 | 0 | 0 | | | | | 3 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 4 | 5 | 5 | 0 | 0 | 30 | 24 | | | | | 4 | 0 | 0 | 0 | 0 | | | | | | | 4 | 0 | 0 | 0 | 0 | | | | | 4 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 5 | 0 | 0 | 0 | 0 | | | | | | | 5 | 0 | 0 | 0 | 0 | | | | | | | 5 | 0 | 0 | 0 | 0 | | | | | 5 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 6 | 0 | 0 | 0 | 0 | | | | | | | 6 | 0 | 0 | 0 | 0 | | | | | | | 6 | 0 | 0 | 0 | 0 | | | | | 6 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 7 | 0 | 0 | 0 | 0 | | | | | | | 7 | 0 | 0 | 0 | 0 | | | | | | | 7 | 0 | 0 | 0 | 0 | | | | | 7 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 8 | 0 | 0 | 0 | 0 | | | | | | | 8 | 0 | 0 | 0 | 0 | | | | | | | 8 | 0 | 0 | 0 | 0 | | | | | 8 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 9 | 0 | 0 | 0 | 0 | | | | | | | 9 | 0 | 0 | 0 | 0 | | | | | | | 9 | 0 | 0 | 0 | 0 | | | | | 9 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 10 | 0 | 0 | 0 | 0 | | | | | | | 10 | 0 | 0 | 0 | 0 | | | | | | | 10 | 0 | 0 | 0 | 0 | | | | | 10 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 11 | 0 | 0 | 0 | 0 | | | | | | | 11 | 0 | 0 | 0 | 0 | | | | | | | 11 | 0 | 0 | 0 | 0 | | | | | 11 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 12 | 0 | 0 | 0 | 0 | | | | | | | 12 | 0 | 0 | 0 | 0 | | | | | | | 12 | 0 | 0 | 0 | 0 | | | | | 12 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 13 | 0 | 0 | 0 | 0 | | | | | | | 13 | 0 | 0 | 0 | 0 | | | | | | | 13 | 0 | 0 | 0 | 0 | | | | | 13 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 14 | 0 | 0 | 0 | 0 | | | | | | | 14 | 0 | 0 | 0 | 0 | | | | | | | 14 | 0 | 0 | 0 | 0 | | | | | 14 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 15 | 0 | 0 | 0 | 0 | | | | | | | 15 | 4 | 2 | 2 | 0 | 12 | 24 | 12 | 24 | | | | 15 | 0 | 0 | 0 | 0 | | | | | 15 | 0 | 0 | 0 | 0 | | | | | | | | |
| | 16 | 0 | 0 | 0 | 0 | | | | | | | 16 | 2 | 2 | 0 | 0 | 18 | 18 | | | | | | 16 | 0 | 0 | 0 | 0 | | | | | 16 | 0 | 0 | 0 | 0 | | | | | | | | |
| | 17 | 0 | 0 | 0 | 0 | | | | | | | 17 | 0 | 0 | 0 | 0 | | | | | | | | 17 | 0 | 0 | 0 | 0 | | | | | 17 | 0 | 0 | 0 | 0 | | | | | | | | |
| | 18 | 12 | 12 | 0 | 0 | 70 | 24 | | | | | 18 | 0 | 0 | 0 | 0 | | | | | | | 18 | 0 | 0 | 0 | 0 | | | | | 18 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | Subtotal | | 244 | | | | | | | | | Subtotal | 36 | | | | | | | | | | Subtotal | 0 | | | | | | | | Subtotal | 0 | | | | | | | | | | | | |
| Span Total | | 280 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Span 5 | 1 | 0 | 0 | 0 | 0 | | | | | | 1 | 0 | 0 | 0 | 0 | | | | | | | 1 | 10 | 6 | 4 | 0 | 24 | 36 | 24 | 24 | | | | | | | | | | | | | | | |
| | 2 | 0 | 0 | 0 | 0 | | | | | | 2 | 0 | 0 | 0 | 0 | | | | | | | 2 | 0 | 0 | 0 | 0 | | | | | 2 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 3 | 0 | 0 | 0 | 0 | | | | | | 3 | 0 | 0 | 0 | 0 | | | | | | | 3 | 12 | 12 | 0 | 0 | 42 | 42 | | | | | | | | | | | | | | | | | |
| | 4 | 0 | 0 | 0 | 0 | | | | | | 4 | 0 | 0 | 0 | 0 | | | | | | | 4 | 19 | 15 | 4 | 0 | 36 | 60 | 24 | 24 | | | | | | | | | | | | | | | |
| | 5 | 0 | 0 | 0 | 0 | | | | | | 5 | 0 | 0 | 0 | 0 | | | | | | | 5 | 0 | 0 | 0 | 0 | | | | | 5 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 6 | 0 | 0 | 0 | 0 | | | | | | 6 | 0 | 0 | 0 | 0 | | | | | | | 6 | 0 | 0 | 0 | 0 | | | | | 6 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 7 | 0 | 0 | 0 | 0 | | | | | | 7 | 0 | 0 | 0 | 0 | | | | | | | 7 | 0 | 0 | 0 | 0 | | | | | 7 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 8 | 0 | 0 | 0 | 0 | | | | | | 8 | 0 | 0 | 0 | 0 | | | | | | | 8 | 1 | 1 | 0 | 0 | 12 | 12 | | | | | | | | | | | | | | | | | |
| | 9 | 0 | 0 | 0 | 0 | | | | | | 9 | 0 | 0 | 0 | 0 | | | | | | | 9 | 8 | 8 | 0 | 0 | 36 | 33 | | | | | | | | | | | | | | | | | |
| | 10 | 0 | 0 | 0 | 0 | | | | | | 10 | 0 | 0 | 0 | 0 | | | | | | | 10 | 0 | 0 | 0 | 0 | | | | | 10 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 11 | 0 | 0 | 0 | 0 | | | | | | 11 | 0 | 0 | 0 | 0 | | | | | | | 11 | 0 | 0 | 0 | 0 | | | | | 11 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 12 | 0 | 0 | 0 | 0 | | | | | | 12 | 0 | 0 | 0 | 0 | | | | | | | 12 | 0 | 0 | 0 | 0 | | | | | 12 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 13 | 0 | 0 | 0 | 0 | | | | | | 13 | 0 | 0 | 0 | 0 | | | | | | | 13 | 0 | 0 | 0 | 0 | | | | | 13 | 7 | 7 | 0 | 0 | 42 | 24 | | | | | | | | |
| | 14 | 0 | 0 | 0 | 0 | | | | | | 14 | 0 | 0 | 0 | 0 | | | | | | | 14 | 0 | 0 | 0 | 0 | | | | | 14 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 15 | 0 | 0 | 0 | 0 | | | | | | 15 | 0 | 0 | 0 | 0 | | | | | | | 15 | 0 | 0 | 0 | 0 | | | | | 15 | 5 | 5 | 0 | 0 | 36 | 18 | | | | | | | | |
| | Subtotal | | 0 | | | | | | | | Subtotal | 0 | | | | | | | | | | Subtotal | 0 | | | | | | | | Subtotal | 62 | | | | | | | | | | | | | |
| Span Total | | 62 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Span 6 | 1 | 180 | 13 | 2 | 165 | 70 | 26 | 24 | 12 | 331 | 72 | 1 | 2 | 2 | 0 | 0 | 24 | 12 | | | | 1 | 0 | 0 | 0 | 0 | 72 | 24 | 60 | 24 | | | | | | | | | | | | | | | |
| | 2 | 0 | 0 | 0 | 0 | | | | | | | 2 | 0 | 0 | 0 | 0 | | | | | | 2 | 0 | 0 | 0 | 0 | | | | | 2 | 0 | 0 | 0 | 0 | | | | | | | | | | |
| | 3 | 0 | 0 | 0 | 0 | | | | | | | 3 | 0 | 0 | 0 | 0 | | | | | | 3 | 0 | 0 | 0 | 0 | 42 | 48 | | | | | | | | | | | | | | | | | |
| | 4 | 0 | 0 | 0 | 0 | | | | | | | 4 | 2 | 1 | 1 | 0 | 12 | 12 | 12 | 12 | | | 4 | 0 | 0 | 0 | 0 | 24 | 24 | | | | | | | | | | | | | | | | |
| | 5 | 0 | 0 | 0 | 0 | | | | | | | 5 | 12 | 12 | 0 | 0 | 76 | 22 | | | | | 5 | 0 | 0 | 0 | 0 | | | | | 5 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 6 | 0 | 0 | 0 | 0 | | | | | | | 6 | 0 | 0 | 0 | 0 | | | | | | | 6 | 0 | 0 | 0 | 0 | | | | | 6 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 7 | 0 | 0 | 0 | 0 | | | | | | | 7 | 0 | 0 | 0 | 0 | | | | | | | 7 | 0 | 0 | 0 | 0 | | | | | 7 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 8 | 0 | 0 | 0 | 0 | | | | | | | 8 | 0 | 0 | 0 | 0 | | | | | | | 8 | 0 | 0 | 0 | 0 | | | | | 8 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 9 | 0 | 0 | 0 | 0 | | | | | | | 9 | 0 | 0 | 0 | 0 | | | | | | | 9 | 0 | 0 | 0 | 0 | | | | | 9 | 1 | 1 | 0 | 0 | 12 | 12 | | | | | | | |
| | 10 | 0 | 0 | 0 | 0 | | | | | | | 10 | 0 | 0 | 0 | 0 | | | | | | | 10 | 0 | 0 | 0 | 0 | | | | | 10 | 0 | 0 | 0 | 0 | | | | | | | | | |
| | 11 | 0 | 0 | 0 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

CUY-6-1456 Pier Patching Quantities

| Pier | Total (SF) | N. Exterior Shaft | S. Exterior Shaft | E. Face | | | | W. Face | | | |
|---------|------------|-------------------|-------------------|-----------|------------|-----------|----------|-----------|------------|-----------|----------|
| | | | | North Bay | Center Bay | South Bay | Subtotal | North Bay | Center Bay | South Bay | Subtotal |
| Pier 1 | 0 | | | | | | 0 | | | | 0 |
| Pier 2 | 0 | | | | | | 0 | | | | 0 |
| Pier 3 | 26 | | 13 | | | | 0 | 13 | | | 13 |
| Pier 4 | 49 | | 49 | | | | 0 | | | | 0 |
| Pier 5 | 180 | | 138 | | | | 0 | 36 | | 6 | 42 |
| Pier 6 | 166 | | 139 | | | 23 | 23 | 4 | | | 4 |
| Pier 7 | 275 | | 28 | | | | 0 | | | 246 | 246 |
| Pier 8 | 312 | 14 | 166 | | | | 0 | | | 132 | 132 |
| Pier 9 | 101 | 15 | 69 | | | 17 | 17 | | | | 0 |
| Pier 10 | 18 | | 18 | | | | 0 | | | | 0 |
| Pier 11 | 0 | | | | | | 0 | | | | 0 |
| Pier 12 | 0 | | | | | | 0 | | | | 0 |
| Pier 13 | 0 | | | | | | 0 | | | | 0 |

Total 1,127 SF

CUY-6-1456

Wearing Surface Survey

| Span | Concrete Repairs (SF) | | WB Area of Deck (SF) | EB Area of Deck (SF) | Concrete Repair (%) | | |
|--------------|-----------------------|------|----------------------|----------------------|---------------------|------|-------|
| | WB | EB | | | WB | EB | Total |
| Span 1A | 36 | 128 | 2890 | 2890 | 1.2 | 4.4 | 2.8 |
| Span 1B | 81 | 162 | 3607 | 3607 | 2.2 | 4.5 | 3.4 |
| Span 1 | 450 | 627 | 3718 | 3718 | 12.1 | 16.9 | 14.5 |
| Span 2 | 0 | 0 | 4685 | 4685 | 0.0 | 0.0 | 0.0 |
| Span 3 | 56 | 59 | 6368 | 6368 | 0.9 | 0.9 | 0.9 |
| Span 4 | 1495 | 2441 | 17228 | 17228 | 8.7 | 14.2 | 11.4 |
| Span 5 | 0 | 19 | 5186 | 5186 | 0.0 | 0.4 | 0.2 |
| Span 6 | 259 | 8 | 4191 | 4191 | 6.2 | 0.2 | 3.2 |
| Span 7 | 1367 | 664 | 4117 | 4117 | 33.2 | 16.1 | 24.7 |
| Span 8 | 1724 | 1792 | 4170 | 4170 | 41.3 | 43.0 | 42.2 |
| Span 9 | 814 | 354 | 3698 | 3698 | 22.0 | 9.6 | 15.8 |
| Span 10 | 642 | 754 | 3688 | 3688 | 17.4 | 20.4 | 18.9 |
| Span 11 | 76 | 360 | 2864 | 2864 | 2.7 | 12.6 | 7.6 |
| Span 12 | 108 | 229 | 3444 | 6642 | 3.1 | 3.4 | 3.3 |
| Span 13 | 28 | 0 | 2245 | 4331 | 1.2 | 0.0 | 0.4 |
| East Station | 44 | 0 | 8904 | 17172 | 0.5 | 0.0 | 0.2 |

Direction Subtotals: **7,180** **7,597** **81,003** **94,555**

Total: 14,777 SF

Total % Deteriorated = 8.42%

APPENDIX E

ESTIMATED FRP WRAP QUANTITIES

CUY-6-1456 Arch Rib
Estimated FRP Wrap Quantities

Side Wrap Ht.

Future Spall Ht. 1.00 Ft.
 FRP Development 1.50 Ft.
 2.50 Ft.

Rough Form Length Factor:
 50% Form board length

| Span | Intrados Length (ft) | Arch Side Surface Area (ft ²) | Exterior Arch Ribs | | Interior Arch Ribs | | FRP Wrap - Alternate No. 1 | | FRP Wrap - Alternate No. 2 | | | FRP Wrap - Alternate No. 3 | | Estimated Board Form Length (ft.) | Estimated Rough Form Length (ft.) |
|------|----------------------|---|--------------------|----------------------|--------------------|----------------------|----------------------------|------------------------------|-----------------------------------|---------------------------------|------------------------------|-------------------------------|------------------------------|-----------------------------------|-----------------------------------|
| | | | No. of Ribs | Arch Rib Width (ft.) | No. of Ribs | Arch Rib Width (ft.) | Side Wrap Height (ft.) | Wrap Area (ft ²) | Top Corners - Horiz Width (ft.) * | Top Corners - Side Height (ft.) | Wrap Area (ft ²) | Full Side Wrap Height (ft.) * | Wrap Area (ft ²) | | |
| 1 | 138.9 | 744.4 | 0 | 6.75 | | 9.00 | | | | | | | | 0 | 0 |
| 2 | 180.0 | 1061.0 | 1.5 | 6.75 | 1.5 | 9.00 | 2.50 | 6952.5 | 1.50 | 2.50 | 7672.5 | 7986.0 | 12238.5 | 17010 | 8505 |
| 3 | 201.2 | 1379.4 | 1 | 6.75 | 1 | 9.00 | 2.50 | 5180.9 | 1.50 | 2.50 | 5985.7 | 6724.8 | 9893.7 | 12676 | 6338 |
| 5 | 178.3 | 1020.2 | 2 | 6.00 | 2 | 8.00 | 2.50 | 8558.4 | 1.50 | 2.50 | 9271.6 | 10301.2 | 15293.6 | 19970 | 9985 |
| 6 ** | 172.1 | 996.1 | 2 | 6.00 | 2 | 8.00 | 2.50 | 6340.8 | 1.50 | 2.50 | 7029.2 | 10034.0 | 14852.8 | 19275 | 9638 |
| 7 | 170.3 | 1051.9 | 2 | 6.00 | 2 | 8.00 | 2.50 | 8174.4 | 1.50 | 2.50 | 8855.6 | 10458.8 | 15227.2 | 19074 | 9537 |
| 8 | 165.4 | 964.3 | 2 | 6.00 | 2 | 8.00 | 2.50 | 7939.2 | 1.50 | 2.50 | 8600.8 | 9699.2 | 14330.4 | 18525 | 9262 |
| 9 | 137.5 | 728.7 | 2 | 6.00 | 2 | 8.00 | 2.50 | 6600.0 | 1.50 | 2.50 | 7150.0 | 7479.6 | 11329.6 | 15400 | 7700 |
| 10 | 123.9 | 618.2 | 2 | 6.00 | 2 | 8.00 | 2.50 | 5947.2 | 1.50 | 2.50 | 6442.8 | 6432.4 | 9901.6 | 13877 | 6938 |
| 11 | 84.9 | 318.1 | 2 | 5.63 | 2 | 6.63 | 2.50 | 3778.1 | 1.50 | 2.50 | 4117.7 | 3563.6 | 5643.7 | 8320 | 4160 |
| 12 | 67.0 | 382.4 | 2 | 5.50 | 2 | 5.50 | 2.50 | 2814.0 | 1.50 | 2.50 | 3082.0 | 3863.4 | 5337.4 | 5896 | 2948 |
| 13 | 81.7 | 338.0 | 1 | 5.50 | 2 | 6.75 | 2.50 | 2777.8 | 1.50 | 2.50 | 3104.6 | 2763.3 | 4315.6 | 6209 | 3105 |

* Includes top corner overlap of 1.5 ft.

Alt. 1 Total = 65,063 ft²

Alt. 2 Total = 71,312 ft²

Total = 78,116 ft²

** FRP Wrap calculations do not include areas between Columns 3 to 5 and 11 to 13 since no steel reinforcement is present at these locations.

Alt 3. Total = 118,364 ft²

**CUY-6-1456 Lower Deck Column
FRP Wrap Quantities**

* & **Red Text** : No FRP wrap is recommended for column heights less than 2.0 feet. Several lower deck columns do not exist either.

| Span | Col. No. | Column Height. (ft.) | Column Width (ft.) | No. of Exterior Columns | Exterior Column Width (ft.) | No. of Interior Columns | Interior Column Width (ft.) | FRP Wrap Area (ft ²) |
|---------------|----------|----------------------|--------------------|-------------------------|-----------------------------|-------------------------|-----------------------------|----------------------------------|
| Span 2 | 1 | 26.75 | 2.00 | 1 | 4.50 | 1 | 6.00 | 776 |
| | 2 | 18.69 | 2.00 | 1 | 4.50 | 1 | 6.00 | 542 |
| | 3 | 12.37 | 2.00 | 1 | 4.50 | 1 | 6.00 | 359 |
| | 4 | 7.40 | 2.00 | 1 | 4.50 | 1 | 6.00 | 215 |
| | 5 | 3.64 | 2.00 | 1 | 4.50 | 1 | 6.00 | 106 |
| | 6* | 0.92 | 2.00 | 1 | 4.50 | 2 | 6.00 | 0 |
| | 7* | -0.67 | 2.00 | 1 | 4.50 | 2 | 6.00 | 0 |
| | 8* | -1.30 | 2.00 | 2 | 4.50 | 2 | 6.00 | 0 |
| | 9* | -1.04 | 2.00 | 2 | 4.50 | 2 | 6.00 | 0 |
| | 10* | 0.11 | 2.00 | 2 | 4.50 | 2 | 6.00 | 0 |
| | 11 | 2.21 | 2.00 | 2 | 4.50 | 2 | 6.00 | 128 |
| | 12 | 5.45 | 2.00 | 2 | 4.50 | 2 | 6.00 | 316 |
| | 13 | 9.73 | 2.00 | 2 | 4.50 | 2 | 6.00 | 565 |
| | 14 | 15.22 | 2.00 | 2 | 4.50 | 2 | 6.00 | 883 |
| | 15 | 22.06 | 2.00 | 2 | 4.50 | 2 | 6.00 | 1280 |
| | 16 | 30.64 | 2.00 | 2 | 4.50 | 2 | 6.00 | 1777 |
| Span 3 | 1 | 35.86 | 2.00 | 0 | 4.5 | 1 | 6.0 | 538 |
| | 2 | 26.74 | 2.00 | 1 | 4.5 | 1 | 6.0 | 775 |
| | 3 | 19.44 | 2.00 | 1 | 4.5 | 1 | 6.0 | 564 |
| | 4 | 13.30 | 2.00 | 1 | 4.5 | 1 | 6.0 | 386 |
| | 5 | 8.49 | 2.00 | 1 | 4.5 | 1 | 6.0 | 246 |
| | 6 | 4.77 | 2.00 | 1 | 4.5 | 1 | 6.0 | 138 |
| | 7 | 2.13 | 2.00 | 1 | 4.5 | 1 | 6.0 | 62 |
| | 8* | 0.48 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 9* | -0.10 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 10* | 0.09 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 11* | 1.06 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 12 | 3.10 | 2.00 | 1 | 4.5 | 1 | 6.0 | 90 |
| | 13 | 6.12 | 2.00 | 1 | 4.5 | 1 | 6.0 | 177 |
| | 14 | 10.23 | 2.00 | 1 | 4.5 | 1 | 6.0 | 297 |
| | 15 | 15.43 | 2.00 | 1 | 4.5 | 1 | 6.0 | 447 |
| | 16 | 21.95 | 2.00 | 1 | 4.5 | 1 | 6.0 | 636 |
| | 17 | 29.64 | 2.00 | 1 | 4.5 | 1 | 6.0 | 860 |
| | 18 | 39.15 | 2.00 | 0 | 4.5 | 0 | 6.0 | 0 |

CUY-6-1456 Lower Deck Column FRP Wrap Quantities

* & **Red Text** : No FRP wrap is recommended for column heights less than 2.0 feet. Several lower deck columns do not exist either.

| Span | Col. No. | Column Height. (ft.) | Column Width (ft.) | No. of Exterior Columns | Exterior Column Width (ft.) | No. of Interior Columns | Interior Column Width (ft.) | FRP Wrap Area (ft ²) |
|---------------|----------|----------------------|--------------------|-------------------------|-----------------------------|-------------------------|-----------------------------|----------------------------------|
| Span 5 | 1 | 35.02 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1786 |
| | 2 | 28.30 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1641 |
| | 3 | 20.80 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1206 |
| | 4 | 14.92 | 2.00 | 2 | 4.5 | 2 | 6.0 | 865 |
| | 5 | 10.46 | 2.00 | 2 | 4.5 | 2 | 6.0 | 607 |
| | 6 | 7.26 | 2.00 | 2 | 4.5 | 2 | 6.0 | 421 |
| | 7 | 5.34 | 2.00 | 2 | 4.5 | 2 | 6.0 | 310 |
| | 8 | 4.51 | 2.00 | 2 | 4.5 | 2 | 6.0 | 262 |
| | 9 | 4.85 | 2.00 | 2 | 4.5 | 2 | 6.0 | 281 |
| | 10 | 6.27 | 2.00 | 2 | 4.5 | 2 | 6.0 | 363 |
| | 11 | 8.97 | 2.00 | 2 | 4.5 | 2 | 6.0 | 520 |
| | 12 | 12.93 | 2.00 | 2 | 4.5 | 2 | 6.0 | 750 |
| | 13 | 18.31 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1062 |
| | 14 | 25.31 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1468 |
| | 15 | 31.54 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1609 |
| Span 6 | 1 | 34.23 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1403 |
| | 2 | 24.40 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1415 |
| | 3 | 16.82 | 2.00 | 2 | 4.5 | 2 | 6.0 | 976 |
| | 4 | 10.86 | 2.00 | 2 | 4.5 | 2 | 6.0 | 630 |
| | 5 | 6.32 | 2.00 | 2 | 4.5 | 2 | 6.0 | 367 |
| | 6 | 3.04 | 2.00 | 2 | 4.5 | 2 | 6.0 | 177 |
| | 7* | 1.05 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 8* | 0.14 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 9* | 0.39 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 10 | 2.52 | 2.00 | 2 | 4.5 | 2 | 6.0 | 146 |
| | 11 | 4.35 | 2.00 | 2 | 4.5 | 2 | 6.0 | 252 |
| | 12 | 8.23 | 2.00 | 2 | 4.5 | 2 | 6.0 | 477 |
| | 13 | 13.53 | 2.00 | 2 | 4.5 | 2 | 6.0 | 785 |
| | 14 | 20.96 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1215 |
| | 15 | 29.63 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1511 |

CUY-6-1456 Lower Deck Column FRP Wrap Quantities

* & **Red Text** : No FRP wrap is recommended for column heights less than 2.0 feet. Several lower deck columns do not exist either.

| Span | Col. No. | Column Height. (ft.) | Column Width (ft.) | No. of Exterior Columns | Exterior Column Width (ft.) | No. of Interior Columns | Interior Column Width (ft.) | FRP Wrap Area (ft ²) |
|---------------|----------|----------------------|--------------------|-------------------------|-----------------------------|-------------------------|-----------------------------|----------------------------------|
| Span 7 | 1 | 31.67 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1299 |
| | 2 | 22.70 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1316 |
| | 3 | 15.48 | 2.00 | 2 | 4.5 | 2 | 6.0 | 898 |
| | 4 | 9.81 | 2.00 | 2 | 4.5 | 2 | 6.0 | 569 |
| | 5 | 5.42 | 2.00 | 2 | 4.5 | 2 | 6.0 | 314 |
| | 6 | 2.27 | 2.00 | 2 | 4.5 | 2 | 6.0 | 132 |
| | 7* | 0.32 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 8* | -0.56 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 9* | -0.34 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 10* | 0.95 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 11 | 3.44 | 2.00 | 2 | 4.5 | 2 | 6.0 | 200 |
| | 12 | 7.18 | 2.00 | 2 | 4.5 | 2 | 6.0 | 416 |
| | 13 | 12.18 | 2.00 | 2 | 4.5 | 2 | 6.0 | 707 |
| | 14 | 18.75 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1087 |
| | 15 | 27.07 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1381 |
| Span 8 | 1 | 30.26 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1240 |
| | 2 | 21.76 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1262 |
| | 3 | 14.94 | 2.00 | 2 | 4.5 | 2 | 6.0 | 866 |
| | 4 | 9.49 | 2.00 | 2 | 4.5 | 2 | 6.0 | 550 |
| | 5 | 5.28 | 2.00 | 2 | 4.5 | 2 | 6.0 | 306 |
| | 6 | 2.23 | 2.00 | 2 | 4.5 | 2 | 6.0 | 129 |
| | 7* | 0.38 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 8* | -0.50 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 9* | -0.28 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 10* | 0.91 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 11 | 3.31 | 2.00 | 2 | 4.5 | 2 | 6.0 | 192 |
| | 12 | 6.86 | 2.00 | 2 | 4.5 | 2 | 6.0 | 398 |
| | 13 | 11.65 | 2.00 | 2 | 4.5 | 2 | 6.0 | 676 |
| | 14 | 17.81 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1033 |
| | 15 | 25.65 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1308 |

CUY-6-1456 Lower Deck Column FRP Wrap Quantities

* & **Red Text** : No FRP wrap is recommended for column heights less than 2.0 feet. Several lower deck columns do not exist either.

| Span | Col. No. | Column Height. (ft.) | Column Width (ft.) | No. of Exterior Columns | Exterior Column Width (ft.) | No. of Interior Columns | Interior Column Width (ft.) | FRP Wrap Area (ft ²) |
|----------------------------|----------|----------------------|--------------------|-------------------------|-----------------------------|-------------------------|-----------------------------|----------------------------------|
| Span 9 | 1 | 25.89 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1061 |
| | 2 | 17.91 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1039 |
| | 3 | 11.80 | 2.00 | 2 | 4.5 | 2 | 6.0 | 684 |
| | 4 | 7.04 | 2.00 | 2 | 4.5 | 2 | 6.0 | 408 |
| | 5 | 3.65 | 2.00 | 2 | 4.5 | 2 | 6.0 | 212 |
| | 6* | 1.60 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 7* | 0.64 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 8* | 0.97 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 9 | 2.38 | 2.00 | 2 | 4.5 | 2 | 6.0 | 138 |
| | 10 | 5.14 | 2.00 | 2 | 4.5 | 2 | 6.0 | 298 |
| | 11 | 9.26 | 2.00 | 2 | 4.5 | 2 | 6.0 | 537 |
| | 12 | 14.74 | 2.00 | 2 | 4.5 | 2 | 6.0 | 855 |
| | 13 | 22.62 | 2.00 | 2 | 4.5 | 2 | 6.0 | 1154 |
| Span 10 | 1 | 22.16 | 2.00 | 2 | 4.5 | 2 | 6.0 | 909 |
| | 2 | 14.73 | 2.00 | 2 | 4.5 | 2 | 6.0 | 854 |
| | 3 | 8.90 | 2.00 | 2 | 4.5 | 2 | 6.0 | 516 |
| | 4 | 4.41 | 2.00 | 2 | 4.5 | 2 | 6.0 | 256 |
| | 5* | 1.35 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 6* | -0.19 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 7* | -0.51 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 8* | 0.40 | 2.00 | 2 | 4.5 | 2 | 6.0 | 0 |
| | 9 | 2.83 | 2.00 | 2 | 4.5 | 2 | 6.0 | 164 |
| | 10 | 6.68 | 2.00 | 2 | 4.5 | 2 | 6.0 | 387 |
| | 11 | 11.87 | 2.00 | 2 | 4.5 | 2 | 6.0 | 689 |
| | 12 | 18.68 | 2.00 | 2 | 4.5 | 2 | 6.0 | 952 |
| Span 11 NE & NI | 1 | 16.20 | 2.00 | 1 | 4.5 | 1 | 6.0 | 332 |
| | 2 | 8.96 | 2.00 | 1 | 4.5 | 1 | 6.0 | 260 |
| | 3 | 3.97 | 2.00 | 1 | 4.5 | 1 | 6.0 | 115 |
| | 4* | 0.89 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 5* | -0.36 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 6* | -0.02 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 7 | 2.19 | 2.00 | 1 | 4.5 | 1 | 6.0 | 63 |
| | 8 | 6.14 | 2.00 | 1 | 4.5 | 1 | 6.0 | 178 |
| | 9 | 12.38 | 2.00 | 1 | 4.5 | 1 | 6.0 | 316 |
| Span 11 SE & SI | 1 | 16.20 | 2.00 | 1 | 4.5 | 1 | 6.0 | 332 |
| | 2 | 8.63 | 2.00 | 1 | 4.5 | 1 | 6.0 | 250 |
| | 3 | 4.14 | 2.00 | 1 | 4.5 | 1 | 6.0 | 120 |
| | 4* | 1.75 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 5* | 1.34 | 2.00 | 1 | 4.5 | 1 | 6.0 | 0 |
| | 6 | 2.81 | 2.00 | 1 | 4.5 | 1 | 6.0 | 82 |
| | 7 | 6.32 | 2.00 | 1 | 4.5 | 1 | 6.0 | 183 |
| | 8 | 12.70 | 2.00 | 1 | 4.5 | 1 | 6.0 | 324 |

Note: No lower deck columns are present in Spans 12 & 13.

Total = **64,616** ft²

**CUY-6-1456 Lower Deck Floor Beam
FRP Wrap Quantities**

* No FRP Wrap, 1995 Floorbeam

Rough Form Length Factor:
25% of form board length

| Span | Floor Beam No. | Interior Floor Beam Length (ft.) | Exterior Floor Beam Length (ft.) | Floor Beam Width (ft.) | Floor Beam Height (ft.) | Fillet Area (ft ²) | FRP Wrap Area (ft ²) | Rough Surface Length (ft.) | Rough Surface Length (ft.) |
|--------|----------------|----------------------------------|----------------------------------|------------------------|-------------------------|--------------------------------|----------------------------------|----------------------------|----------------------------|
| Span 2 | 1* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 561 | 2243 | 561 |
| | 2* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 561 | 2243 | 561 |
| | 3 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 4 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 5 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 6* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 561 | 2243 | 561 |
| | 7* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 561 | 2243 | 561 |
| | 8 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 9 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 10 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 11* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 561 | 2243 | 561 |
| | 12 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 13 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 14 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 15 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 16 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| Span 3 | 1* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 0 | 0 | 0 |
| | 2 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 3 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 4 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 5 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 6 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 7 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 8 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 9 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 10 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 11 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 12 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 13 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 14 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 15 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 16 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 17* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 0 | 0 | 0 |
| | 18* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 0 | 0 | 0 |
| Span 5 | 1* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 0 | 0 | 0 |
| | 2* | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 561 | 2243 | 561 |
| | 3 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 4 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 5 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 6 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 7 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 8 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 9 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 10 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 11 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 12 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 13 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 14 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 15 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| Span 6 | 1 | 25.25 | 26.63 | 2.00 | 3.67 | 38.3 | 771 | 3084 | 771 |
| | 2 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 3 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 4 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 5 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 6 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 7 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 8 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 9 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 10 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 11 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 12 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 13 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 14 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 15 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| Span 7 | 1 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 2 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 3 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 4 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 5 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 6 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 7 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 8 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 9 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 10 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 11 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 12 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 13 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 14 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 15 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |

**CUY-6-1456 Lower Deck Floor Beam
FRP Wrap Quantities**

* No FRP Wrap, 1995 Floorbeam

Rough Form Length Factor:
25% of form board length

| Span | Floor Beam No. | Interior Floor Beam Length (ft.) | Exterior Floor Beam Length (ft.) | Floor Beam Width (ft.) | Floor Beam Height (ft.) | Fillet Area (ft ²) | FRP Wrap Area (ft ²) | Rough Surface Length (ft.) | Rough Surface Length (ft.) |
|---------|----------------|----------------------------------|----------------------------------|------------------------|-------------------------|--------------------------------|----------------------------------|----------------------------|----------------------------|
| Span 8 | 1 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 2 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 3 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 4 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 5 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 6 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 7 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 8 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 9 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 10 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 11 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 12 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 13 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 14 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 15 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| Span 9 | 1 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 2 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 3 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 4 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 5 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 6 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 7 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 8 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 9 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 10 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 11 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 12 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 13 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| Span 10 | 1 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 2 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 3 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 4 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 5 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 6 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 7 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 8 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 9 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 10 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 11 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| | 12 | 25.25 | 26.63 | 2.00 | 3.67 | 76.5 | 809 | 3237 | 809 |
| Span 11 | 1 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 2 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 3 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 4 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 5 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 6 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 7 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 8 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 9 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| | 10 | 26.38 | 33.60 | 2.00 | 3.67 | 76.5 | 950 | 3799 | 950 |
| Span 12 | 1* | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 0 | 0 | 0 |
| | 2* | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 570 | 2279 | 570 |
| | 3 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 4 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 5 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 6 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 7 | 26.38 | 33.60 | 1.83 | 4.00 | 0 | 920 | 3680 | 920 |
| | 8 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 9 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 10 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 11 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 12 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 13 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| | 14 | 26.38 | 33.60 | 1.50 | 4.00 | 0 | 889 | 3556 | 889 |
| Span 13 | 1 | 26.38 | 30.75 | 2.58 | 3.67 | 0 | 741 | 2963 | 741 |
| | 2 | 26.38 | 30.75 | 2.58 | 3.67 | 0 | 566 | 2266 | 566 |
| | 3 | 26.38 | 30.75 | 2.58 | 3.67 | 0 | 566 | 2266 | 566 |
| | 4 | 26.38 | 30.75 | 2.58 | 3.67 | 0 | 566 | 2266 | 566 |
| | 5 | 26.38 | 30.75 | 2.58 | 3.67 | 0 | 566 | 2266 | 566 |
| | 6 | 26.38 | 30.75 | 2.58 | 3.67 | 0 | 566 | 2266 | 566 |
| | 7 | 26.38 | 30.75 | 2.58 | 3.67 | 0 | 566 | 2266 | 566 |
| | 8 | 26.38 | 30.75 | 2.58 | 3.67 | 0 | 871 | 3486 | 871 |

Totals = 117,303 469,213 117,303 ft.

CUY-6-1456 PIERS

FRP Wrap Quantities

| Location | North Exterior Bay (ft ²) | Interior Bay | South Exterior Bay |
|------------|---------------------------------------|--------------|--------------------|
| West Abut. | 0 | 0 | 0 |
| Pier 1 | 0 | 0 | 0 |
| Pier 2 | 0 | 0 | 0 |
| Pier 3 | 0 | 0 | 0 |
| Pier 4 | 200 | 200 | 200 |
| Pier 5 | 1098 | 1133 | 1098 |
| Pier 6 | 1098 | 1133 | 1098 |
| Pier 7 | 1098 | 1133 | 1098 |
| Pier 8 | 1098 | 1133 | 1098 |
| Pier 9 | 1098 | 1133 | 1098 |
| Pier 10 | 1098 | 1133 | 1098 |
| Pier 11 | 0 | 0 | 0 |
| Pier 12 | 0 | 0 | 0 |
| East Abut. | 0 | 0 | 0 |
| | 6,785 | 6,998 | 6,785 |

Total 20,569 SF

CUY-6-1456 FRP Wrap Totals

| Element | Estimated FRP Wrap Area | | | Rough Surface Length (ft) |
|-------------------|---|---|---|---------------------------|
| | With Arch Rib Alt. No. 1 (ft ²) | With Arch Rib Alt. No. 2 (ft ²) | With Arch Rib Alt. No. 3 (ft ²) | |
| Arch Ribs | 65,063 | 71,312 | 118,364 | 78,116 |
| Columns | 64,616 | 64,616 | 64,616 | 20,000 |
| Floor Beams | 117,303 | 117,303 | 117,303 | 117,303 |
| Lower Pier Shafts | | | | 5,000 |
| Total | 246,983 | 253,232 | 300,284 | 215,419 |

APPENDIX F

**WEST STATION
DETERIORATION DRAWINGS**

CUY-6-1456

2016 West Station Patching

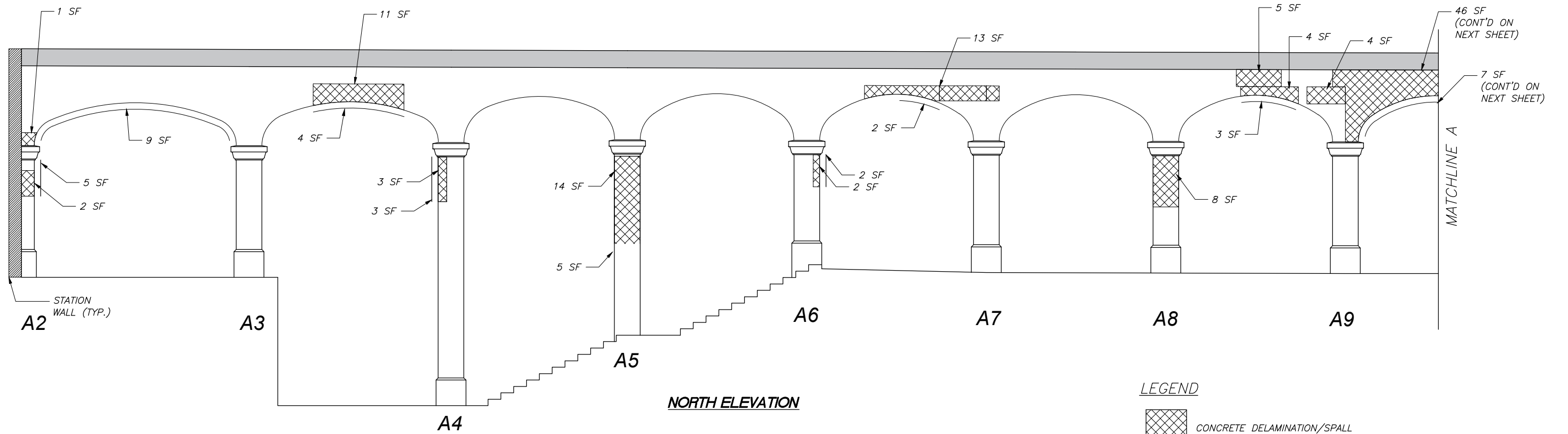
| Detroit Tunnel | | | |
|----------------|-----------------------|---------|------------|
| Bay | Concrete Repairs (SF) | | |
| | North Wall | Ceiling | South Wall |
| 1 | 407 | 16 | 279 |
| 2 | 347 | 150 | 353 |
| 3 | 225 | 220.5 | 204 |
| 4 | 203.25 | 36 | 410 |
| 5 | 171.25 | 98 | 343.5 |
| 6 | 260.75 | 108 | 371.5 |
| 7 | 350.5 | 294 | 422.25 |
| 8 | 153 | 588 | 224 |
| 9 | 184 | 844.5 | 131 |
| 10 | 300 | 171.5 | 614 |

Sub-Totals 2,602 2,527 3,352

Totals 11,329 SF



| W. 25th Tunnel | | | |
|----------------|-----------------------|---------|-----------|
| Bay | Concrete Repairs (SF) | | |
| | West Wall | Ceiling | East Wall |
| 11 | 136 | 32 | 386 |
| 12 | 133 | 0 | 131 |
| 13 | 65 | 16 | 292.5 |
| 14 | 182 | 0 | 163 |
| 15 | 81 | 0 | 92 |
| 16 | 166 | 16 | 159 |
| 17 | 363 | 280 | 155 |

Sub-Totals 1,126 344 1,379

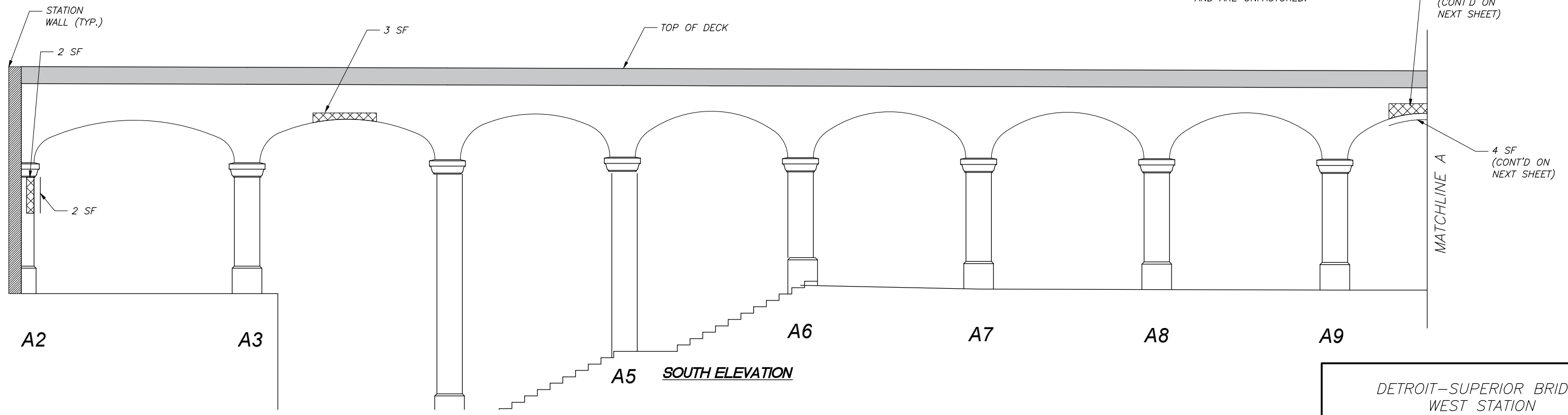


NORTH ELEVATION

LEGEND

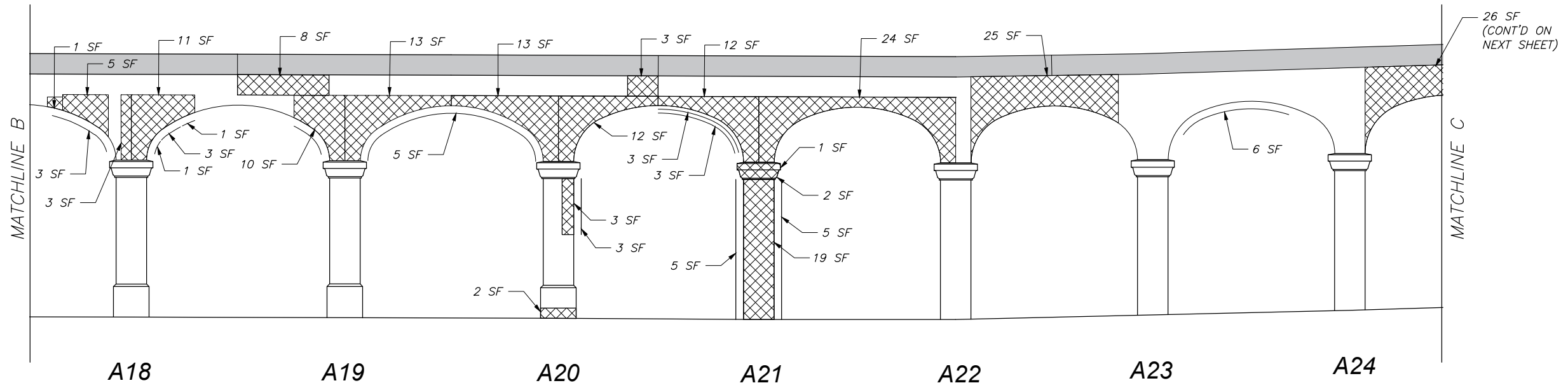
-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.





SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE A, COLUMNS A2 TO A9
1

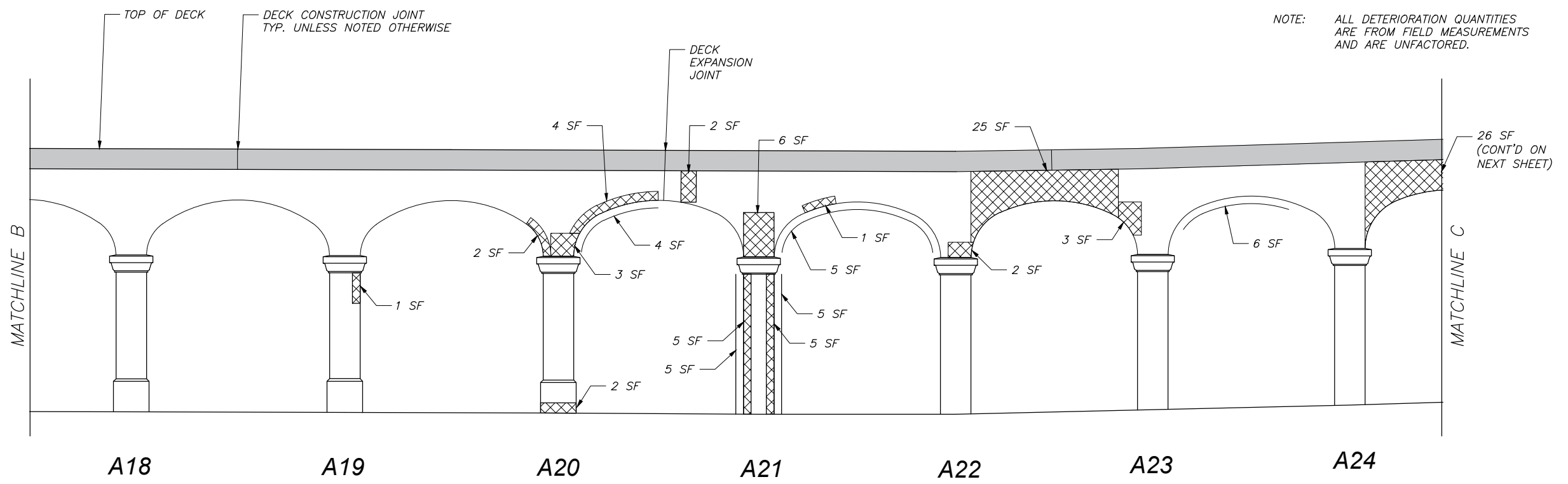


NORTH ELEVATION

LEGEND

-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

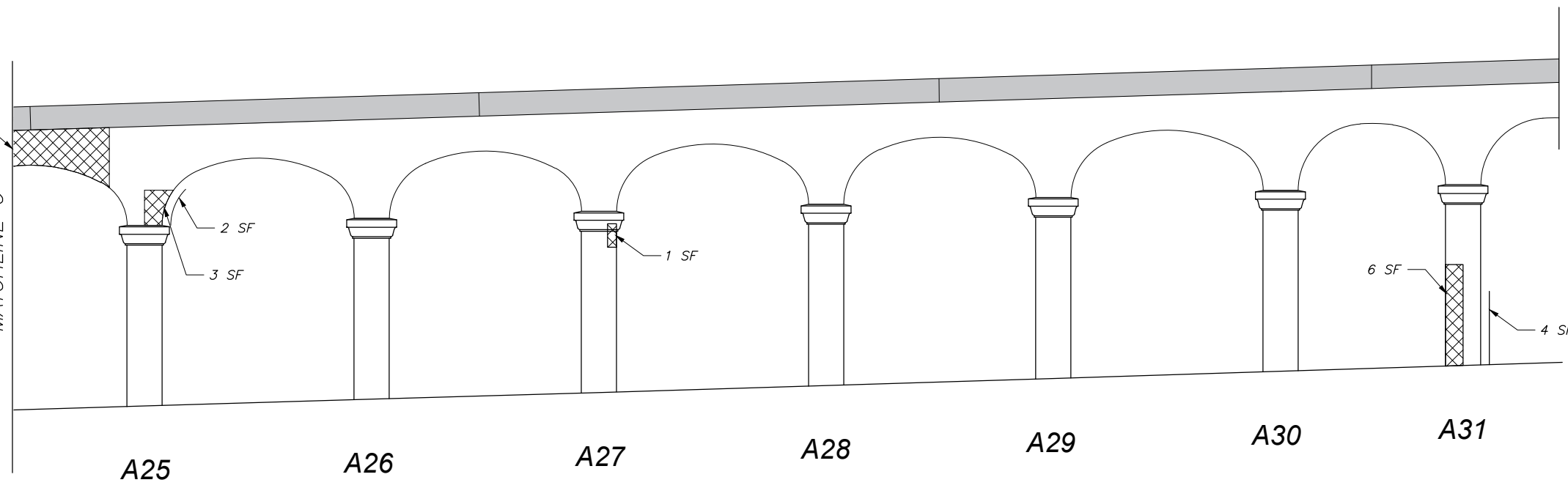


SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE A, COLUMNS A18 TO A24
3



26 SF
(CONT'D FROM
PREVIOUS SHEET)

MATCHLINE C



NORTH ELEVATION

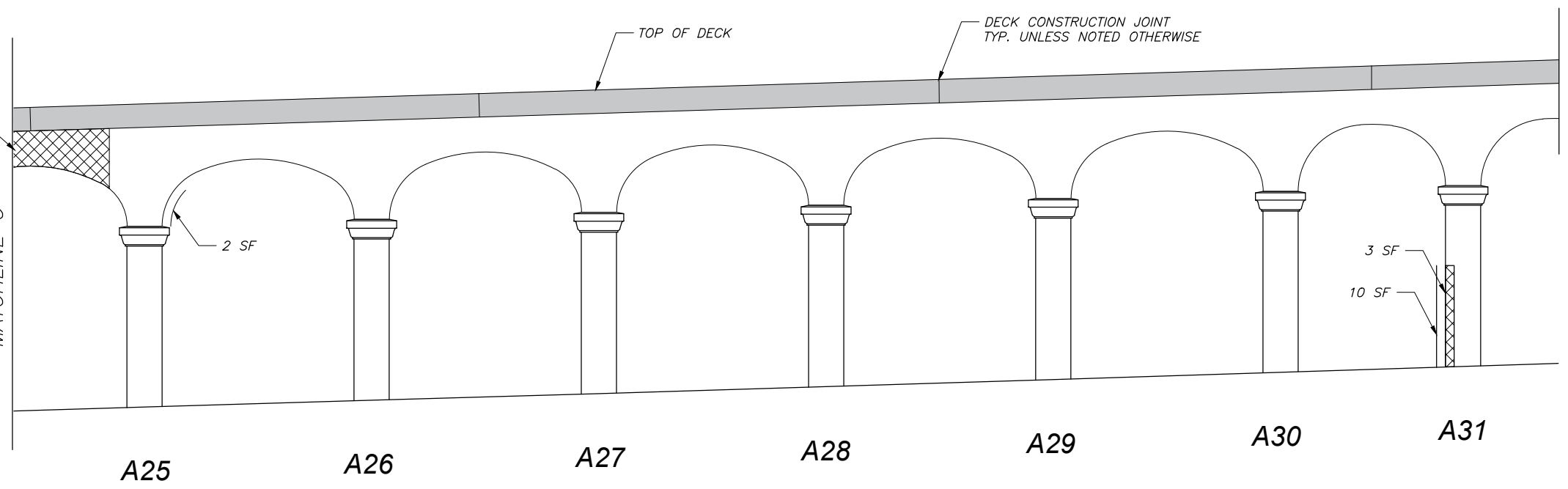
LEGEND

-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

26 SF
(CONT'D FROM
PREVIOUS SHEET)

MATCHLINE C

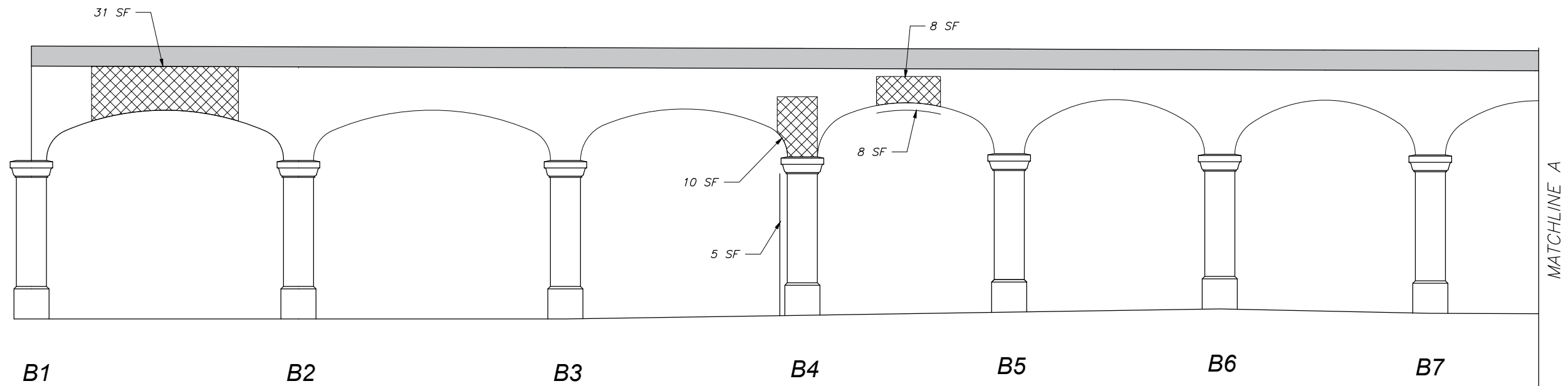


SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION

LINE A, COLUMNS A25 TO A31



4



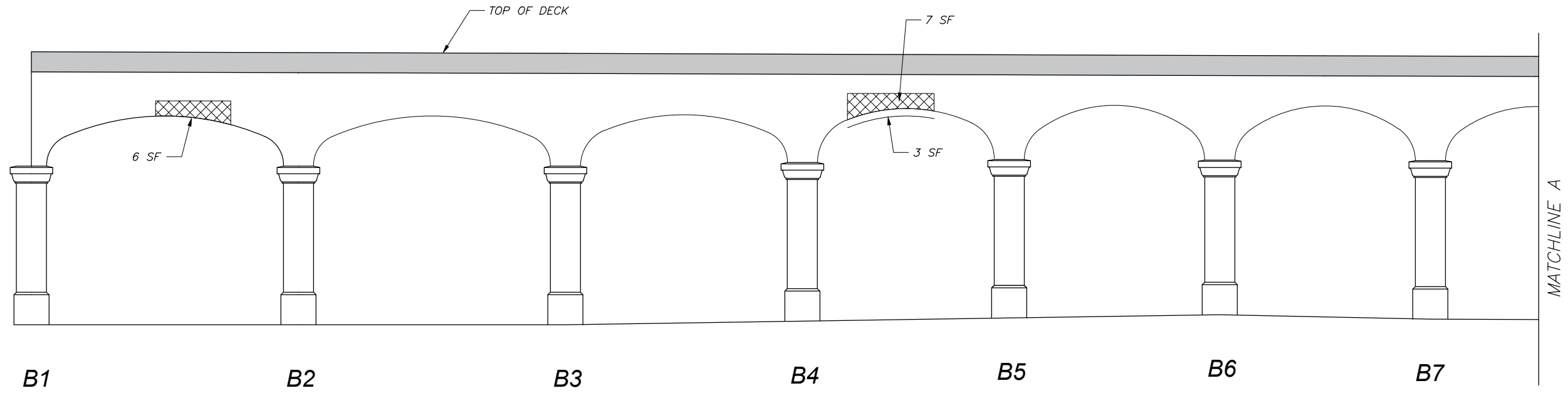
B1 B2 B3 B4 B5 B6 B7

NORTH ELEVATION

LEGEND

-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

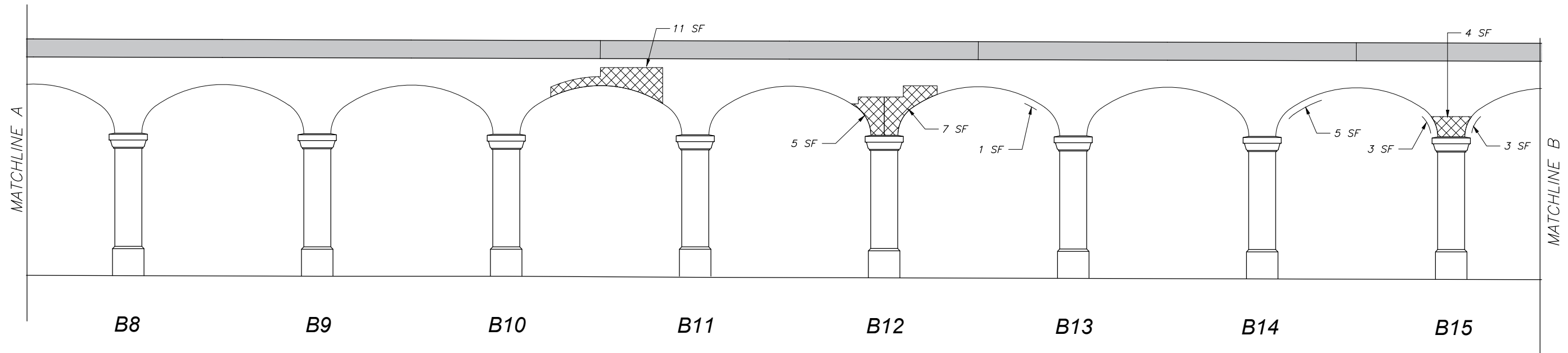
NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.



B1 B2 B3 B4 B5 B6 B7

SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE B, COLUMNS B1 TO B7
5

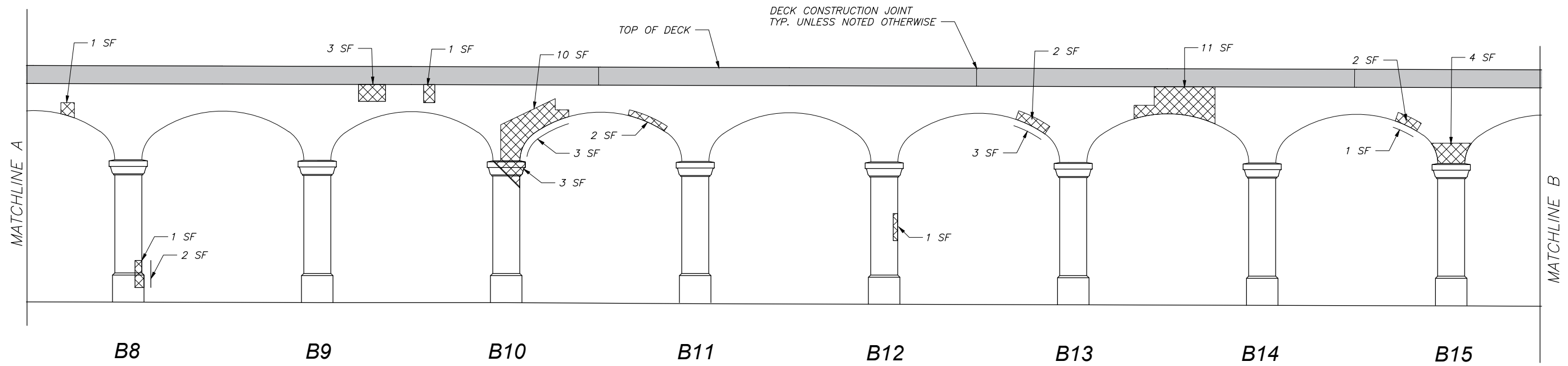


NORTH ELEVATION

LEGEND

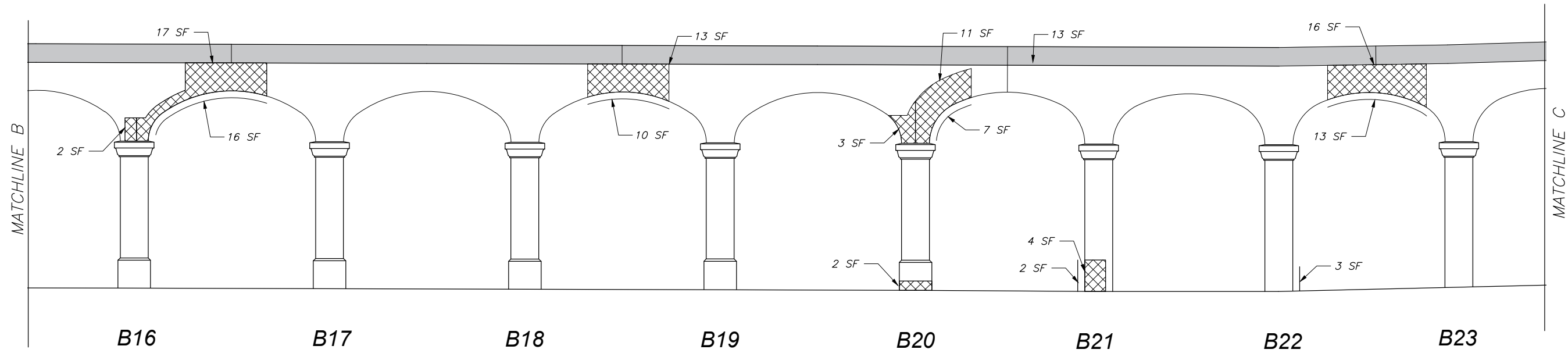
-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.



SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE B, COLUMNS B8 TO B15



NORTH ELEVATION

LEGEND

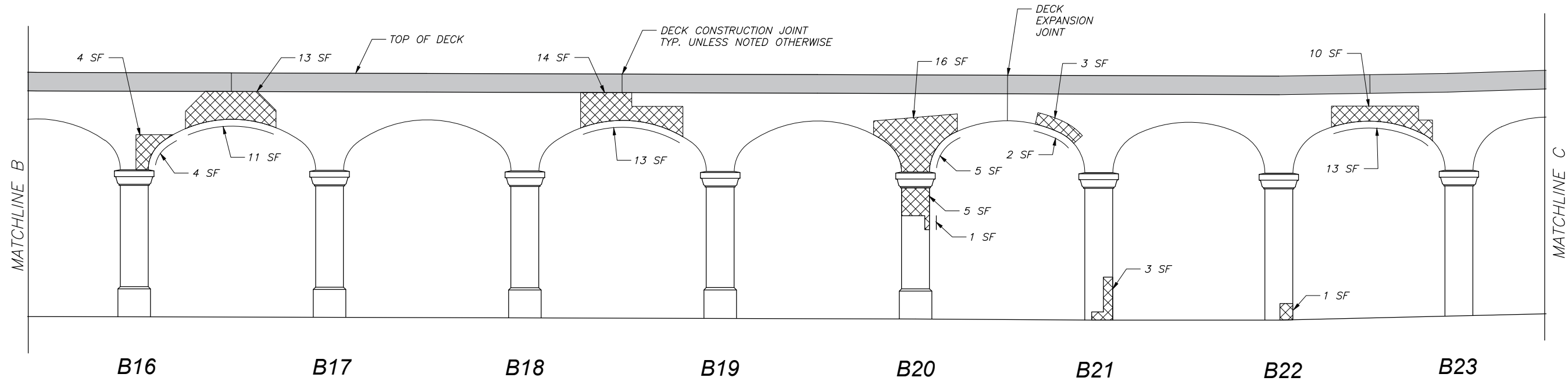


CONCRETE DELAMINATION/SPALL



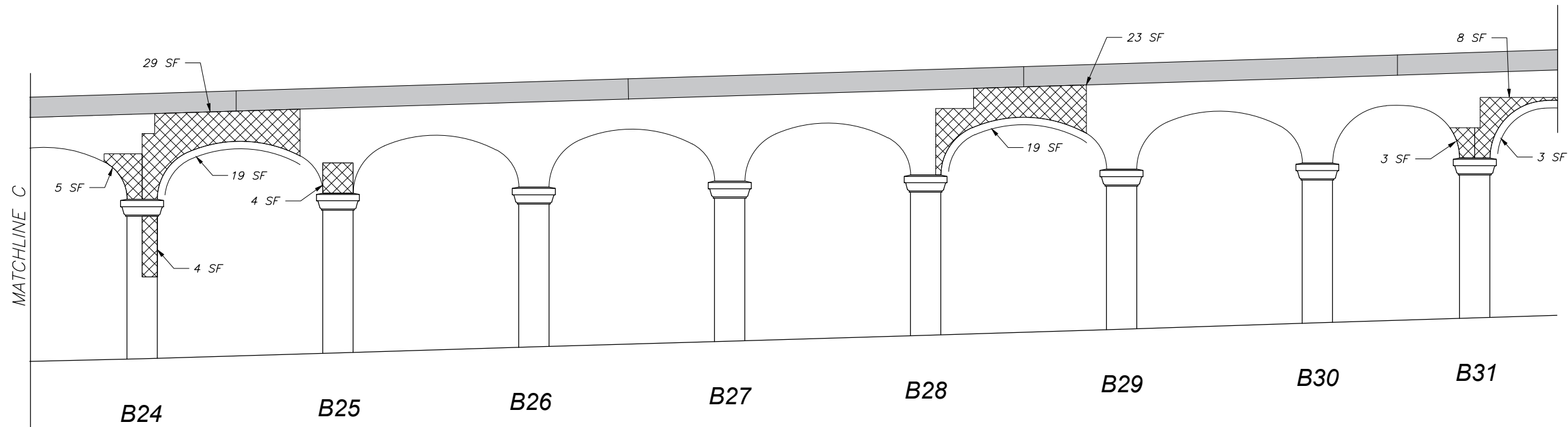
CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.



SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE B, COLUMNS B16 TO B23
7



NORTH ELEVATION

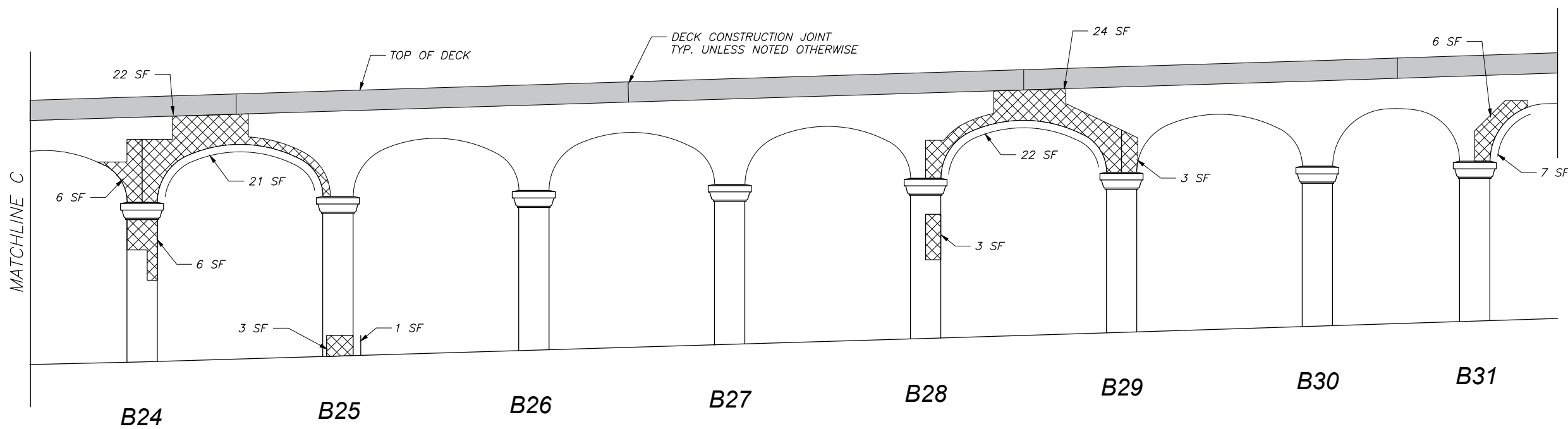
LEGEND



CONCRETE DELAMINATION/SPALL

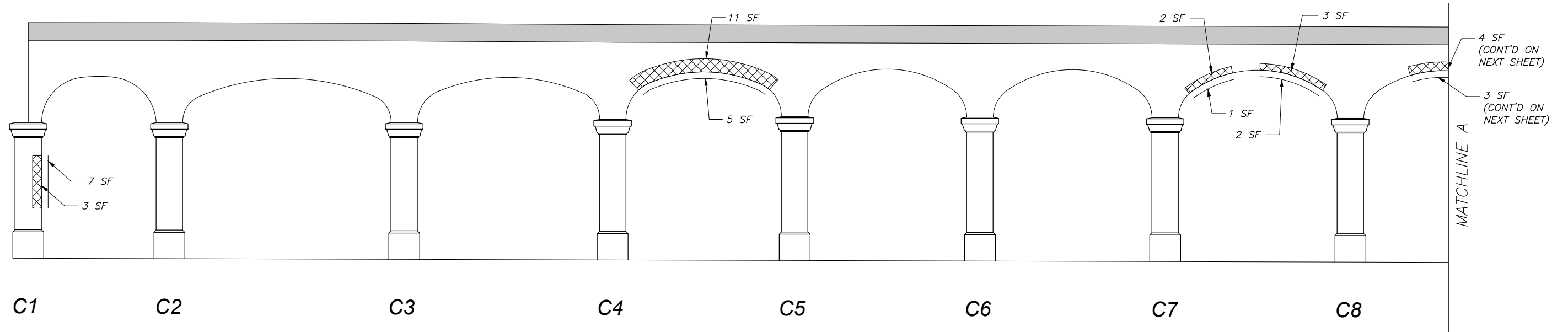
CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.



SOUTH ELEVATION



DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE B, COLUMNS B24 TO B31



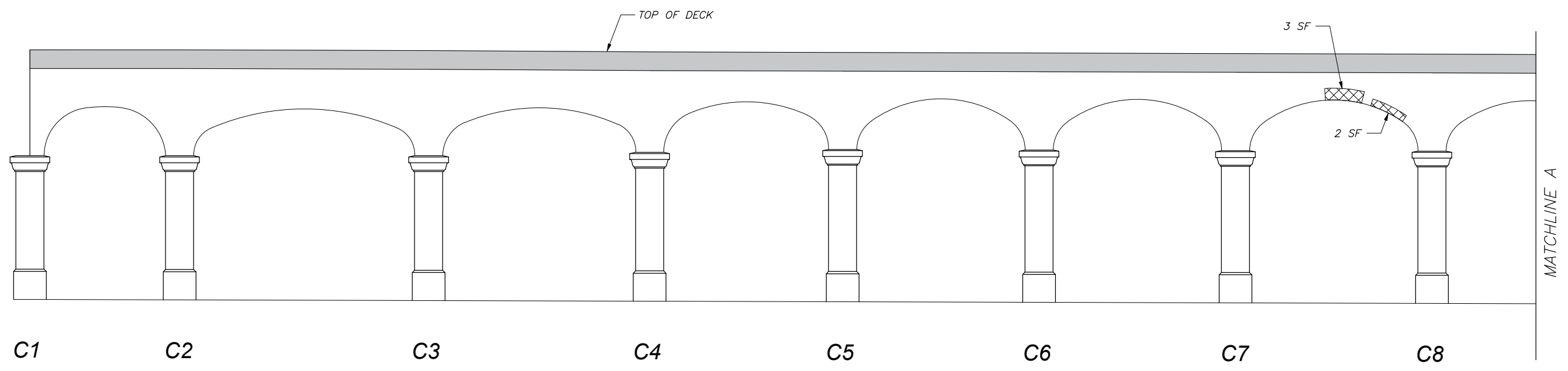
C1 C2 C3 C4 C5 C6 C7 C8

NORTH ELEVATION

LEGEND

-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

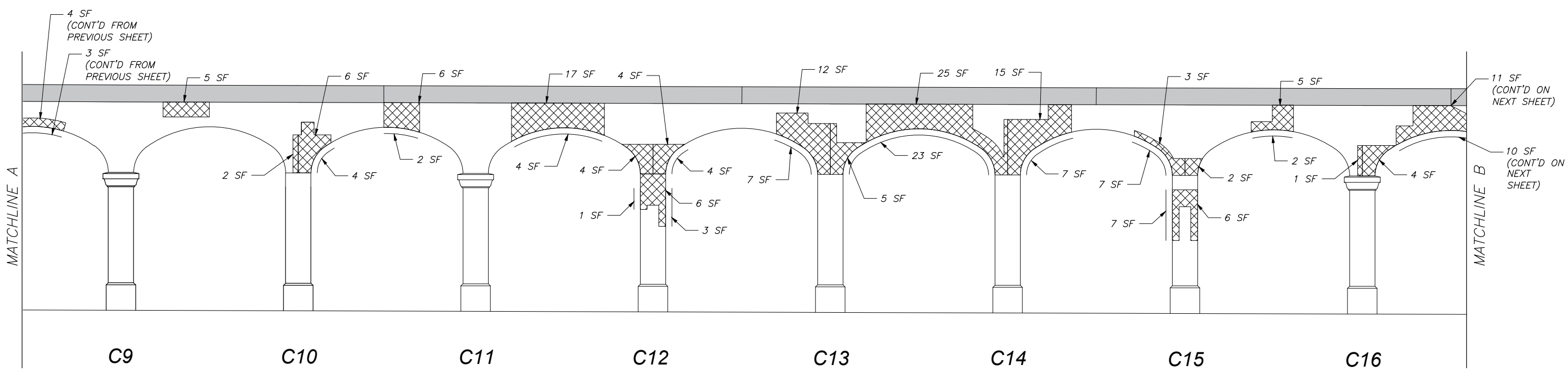
NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.



C1 C2 C3 C4 C5 C6 C7 C8

SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE C, COLUMNS C1 TO C8
9



NORTH ELEVATION

LEGEND

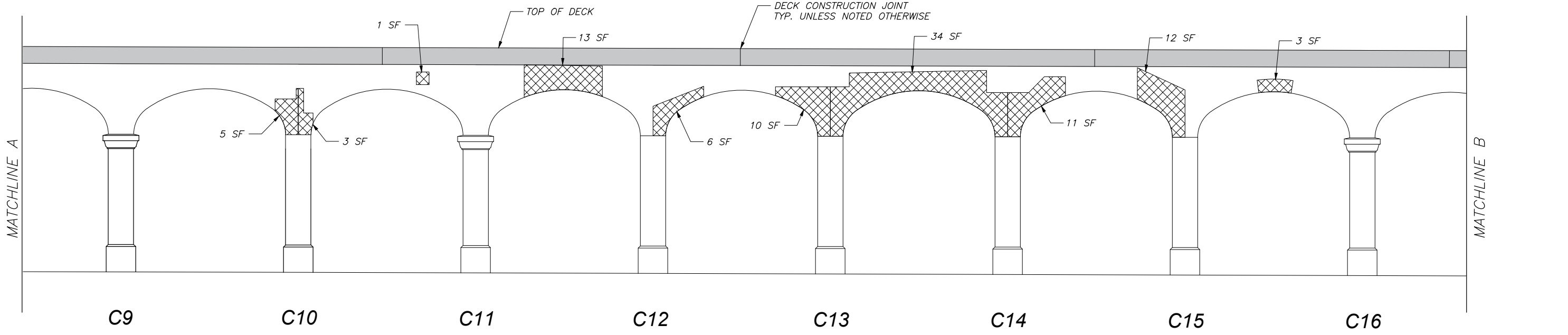


CONCRETE DELAMINATION/SPALL



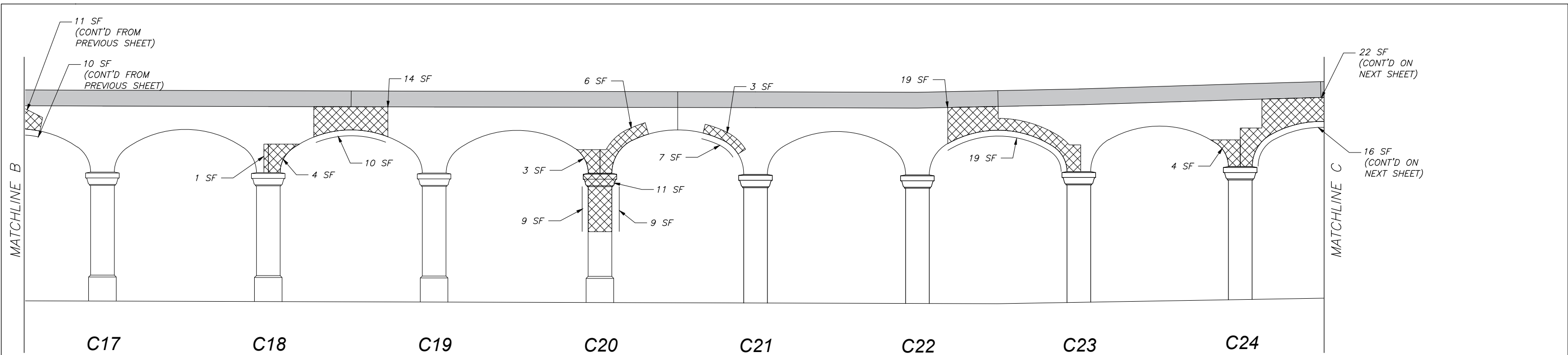
CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.





SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE C, COLUMNS C9-C16
10

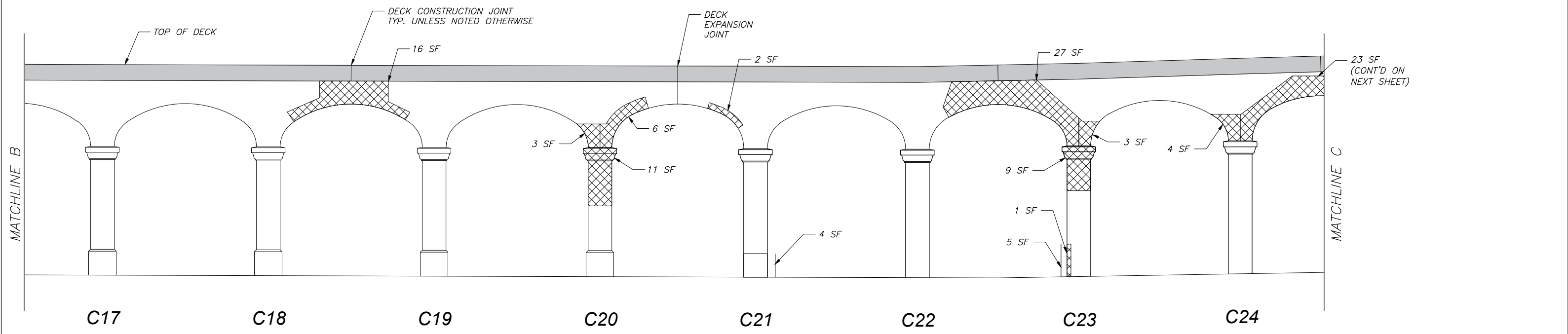


NORTH ELEVATION

LEGEND

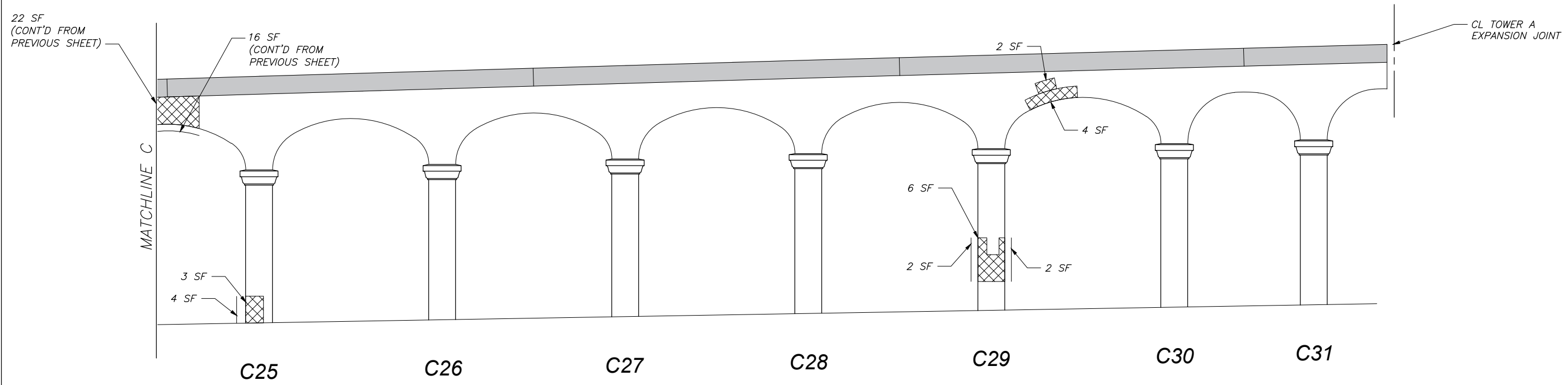
-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.





SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE C, COLUMNS C17 TO C24
11

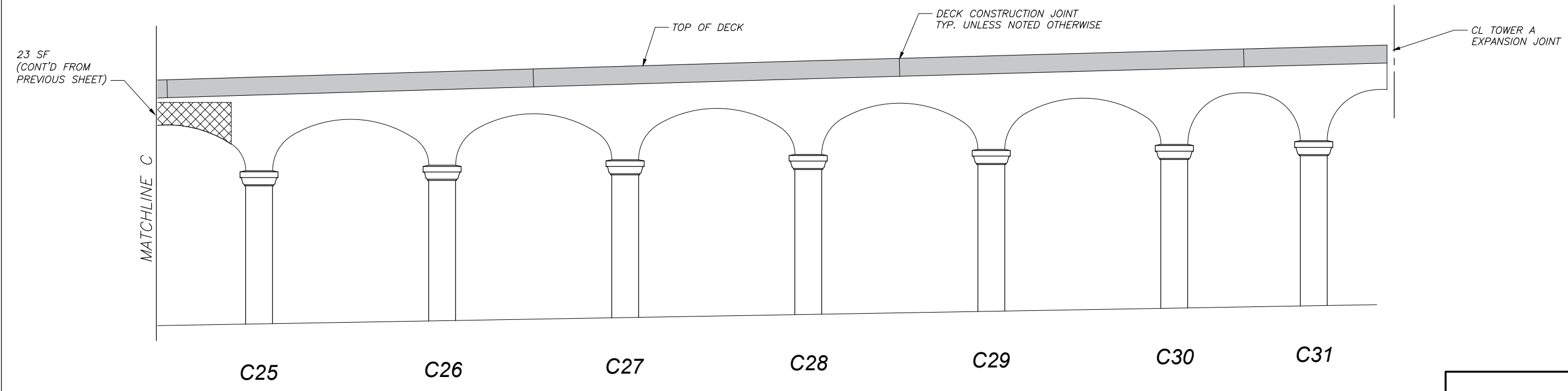


NORTH ELEVATION

LEGEND

-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

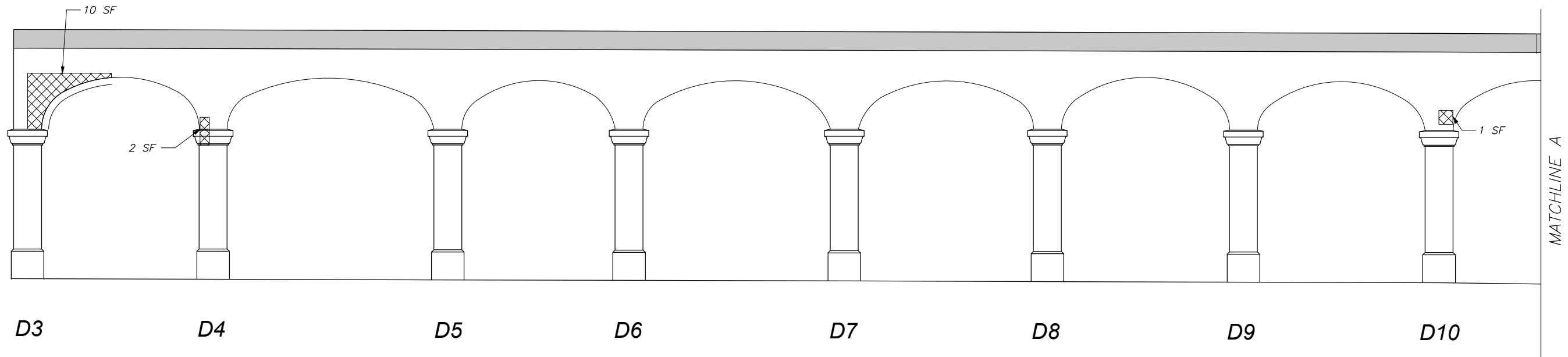


SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION

LINE C, COLUMNS C25-C31



12



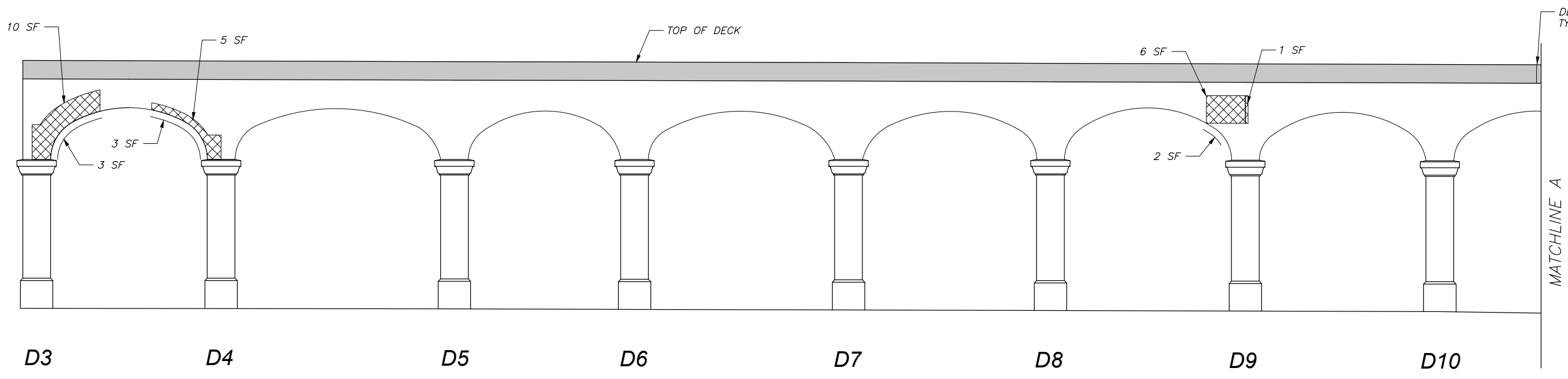
D3 D4 D5 D6 D7 D8 D9 D10

NORTH ELEVATION

LEGEND

-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.



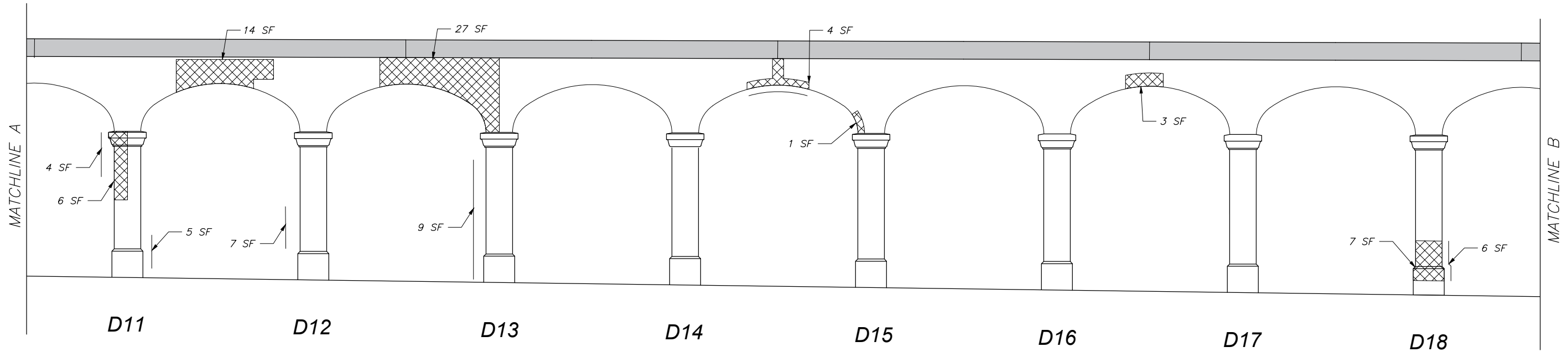
D3 D4 D5 D6 D7 D8 D9 D10

SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION



LINE D, COLUMNS D3 TO D10

13

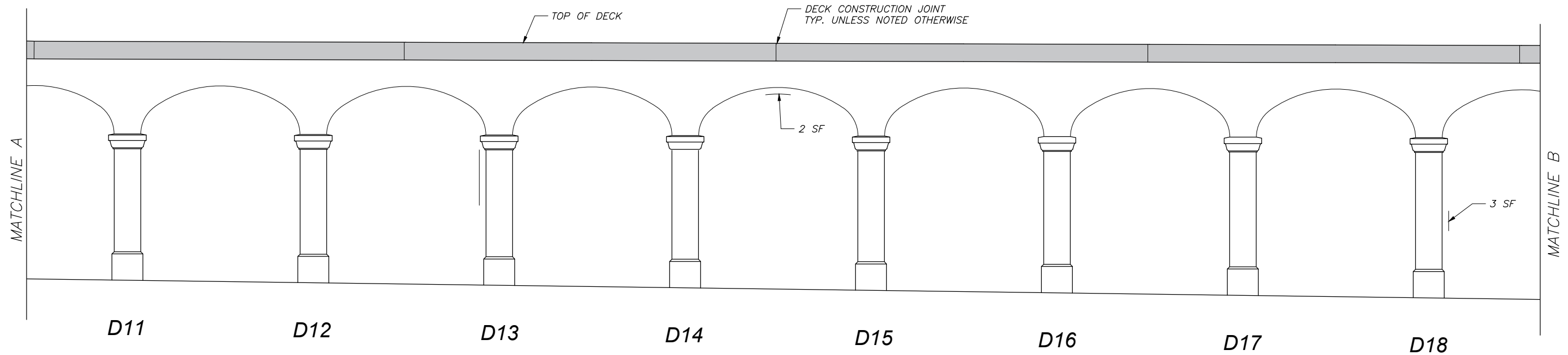


NORTH ELEVATION

LEGEND

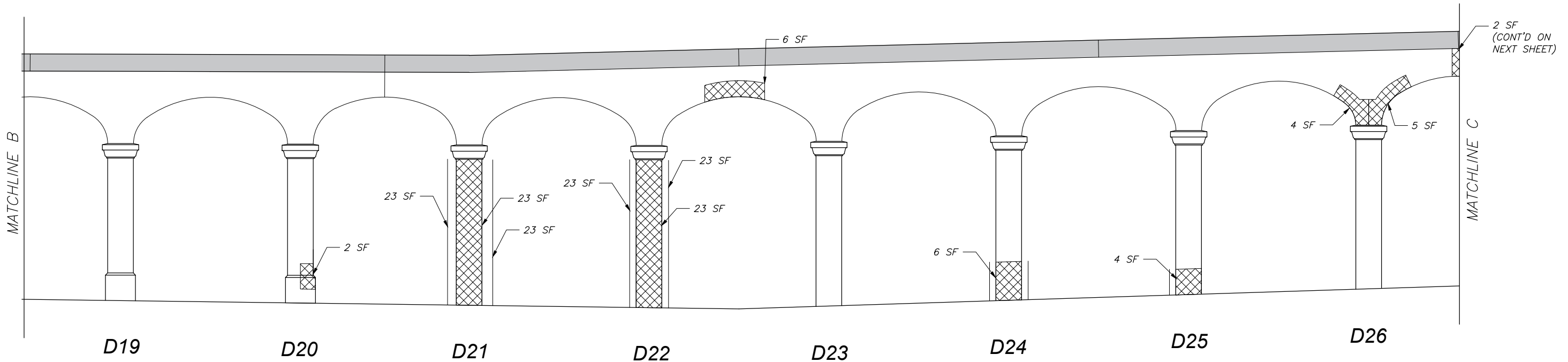
-  CONCRETE DELAMINATION/SPALL
-  CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.



SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE D, COLUMNS D11 TO D18

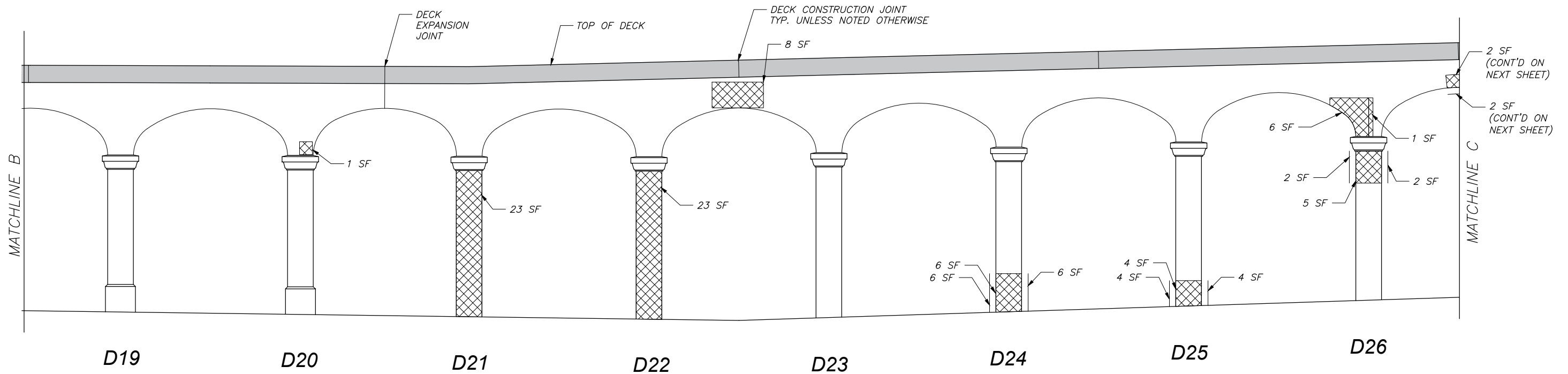


LEGEND

- CONCRETE DELAMINATION/SPALL
- CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

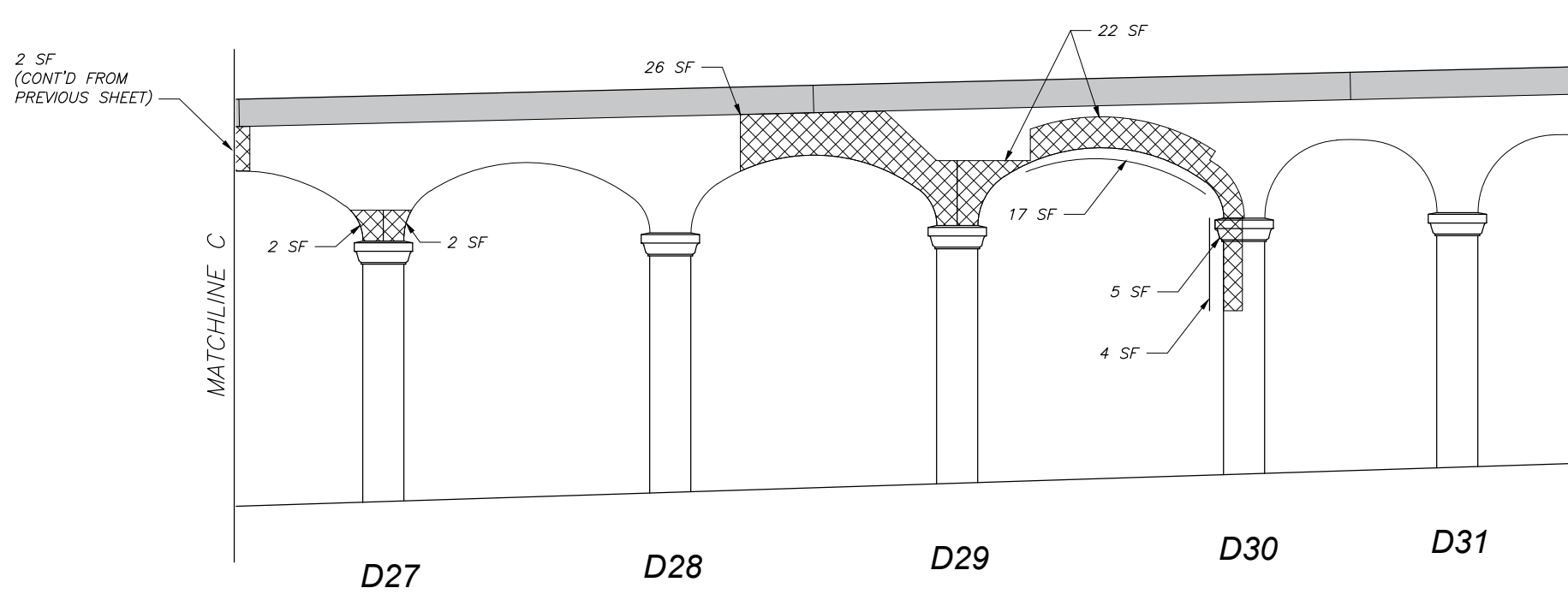
NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.

NORTH ELEVATION



SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION
LINE D, COLUMNS D19 TO D26
15



NORTH ELEVATION

LEGEND

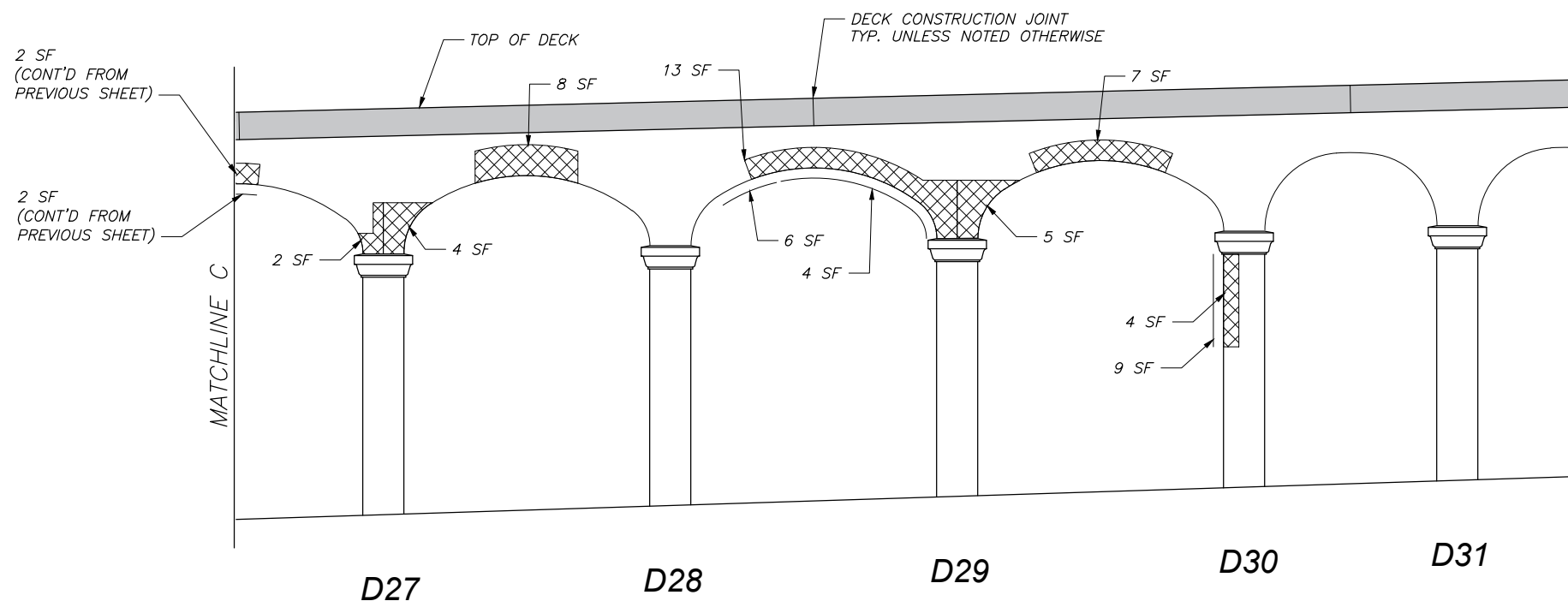


CONCRETE DELAMINATION/SPALL



CONCRETE DELAMINATION/SPALL ON VERTICAL FACE

NOTE: ALL DETERIORATION QUANTITIES ARE FROM FIELD MEASUREMENTS AND ARE UNFACTORED.



SOUTH ELEVATION

DETROIT-SUPERIOR BRIDGE
WEST STATION

LINE D, COLUMNS D27 TO D31

16

APPENDIX G

**WEST STATION
DETERIORATION HISTORY**

CUY-6-1456 West Station
2016 Column Repair Summary

Replacement Recommended

| Column No. | Total Deficiency (SF) | Surface | Subtotal (SF) | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Column No. | Total Deficiency (SF) | Surface | Subtotal (SF) | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Column No. | Total Deficiency (SF) | Surface | Subtotal (SF) | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Column No. | Total Deficiency (SF) | Surface | Subtotal (SF) | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | | |
|------------|-----------------------|-------------------------|---------------------|--------------------|-------------|-------------|------------|-----------------------|-------------------------|-------------------|-------------------|-------------|-------------|------------|-----------------------|-------------------------|----------------------|-------------|-------------|-------------|------------|-----------------------|-------------------------|-------------------------|----------------------|--------------|-------------|--|--|
| | | | | | | | B1 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C1 | 9 | North Sides South | 2.7 6.7 0.0 | 2.7 6.7 | | | | | | | | | | | |
| A2 | 8 | North Sides South | 2.0 4.7 1.7 | 2.0 4.7 1.7 | | | B2 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C2 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | | | | | | | | |
| A3 | 0 | North Sides South | 0.0 0.0 0.0 | 0.0 0.0 0.0 | | | B3 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C3 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D3 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A4 | 5 | North Sides South | 2.3 2.3 0.0 | 2.3 2.3 | | | B4 | 5 | North Sides South | 0.0 4.7 0.0 | 4.7 | | | C4 | 0 | North Sides South | 0.0 4.7 0.0 | | | | D4 | 1 | North Sides South | 0.8 0.0 0.0 | 0.8 | | | | |
| A5 | 19 | North Sides South | 18.7 0.0 0.0 | 18.7 | | | B5 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C5 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D5 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A6 | 3 | North Sides South | 1.3 1.9 0.0 | 1.3 1.9 | | | B6 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C6 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D6 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A7 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B7 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C7 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D7 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A8 | 8 | North Sides South | 8.0 0.0 0.0 | 8.0 | | | B8 | 3 | North Sides South | 0.0 1.5 1.2 | 1.5 1.2 | | | C8 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D8 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A9 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B9 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C9 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D9 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A10 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B10 | 2 | North Sides South | 0.0 0.0 2.3 | 2.3 | | | C10 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D10 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A11 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B11 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C11 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D11 | 14 | North Sides South | 5.5 8.3 0.0 | 5.5 3.3 | 5.0 | | | |
| A12 | 14 | North Sides South | 3.5 6.7 3.9 | 3.5 6.7 1.6 | 2.3 | | B12 | 1 | North Sides South | 0.0 0.0 0.7 | 0.7 | | | C12 | 9 | North Sides South | 6.0 3.0 0.0 | 6.0 0.8 | 2.2 | | | D12 | 6 | North Sides South | 0.0 6.3 0.0 | 6.3 | | | |
| A13 | 4 | North Sides South | 1.6 2.1 0.0 | 1.6 2.1 | | | B13 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C13 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D13 | 9 | North Sides South | 0.0 9.0 0.0 | 9.0 | | | | |
| A14 | 44 | North Sides South | 15.7 23.3 5.3 | 15.7 5.1 5.3 | 15.3 2.9 | | B14 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C14 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D14 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A15 | 22 | North Sides South | 13.7 4.3 3.5 | 13.7 4.3 3.5 | | | B15 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C15 | 12 | North Sides South | 5.6 6.7 0.0 | 5.6 6.7 | | | | D15 | 0 | North Sides South | 0.0 0.0 0.0 | | | | |
| A16 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B16 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C16 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D16 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A17 | 11 | North Sides South | 4.4 4.1 2.3 | 1.3 1.3 2.8 | 3.2 2.8 | | B17 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C17 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D17 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A18 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B18 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C18 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D18 | 15 | North Sides South | 6.3 9.0 0.0 | 6.3 3.0 | 6.0 | | | |
| A19 | 1 | North Sides South | 0.0 0.0 1.0 | 1.0 | | | B19 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C19 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D19 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A20 | 9 | North Sides South | 4.3 2.8 1.6 | 1.6 2.8 1.6 | 2.8 | | B20 | 6 | North Sides South | 1.6 0.3 4.3 | 1.6 0.3 4.3 | | | C20 | 37 | North Sides South | 10.5 16.4 10.5 | 10.5 8.2 | 8.2 | | | D20 | 2 | North Sides South | 2.2 0.0 0.0 | 2.2 | | | |
| A21 | 46 | North Sides South | 18.4 18.4 9.2 | 18.4 9.2 4.6 | 4.6 4.6 | | B21 | 8 | North Sides South | 3.4 1.7 2.5 | 3.4 1.7 2.5 | | | C21 | 7 | North Sides South | 0.0 3.3 4.0 | 3.3 4.0 | | | | D21 | 91 | North Sides South | 22.7 45.4 22.7 | 22.7 22.7 | 22.7 | | |
| A22 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B22 | 4 | North Sides South | 0.0 2.6 1.1 | 2.6 1.1 | | | C22 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D22 | 92 | North Sides South | 23.0 46.0 23.0 | 23.0 23.0 | 23.0 | | | |
| A23 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B23 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C23 | 14 | North Sides South | 0.0 4.6 9.2 | 4.6 8.3 | 0.9 | | | D23 | 0 | North Sides South | 0.0 0.0 0.0 | | | | |
| A24 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B24 | 9 | North Sides South | 4.0 0.0 5.3 | 4.0 0.0 5.3 | | | C24 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D24 | 24 | North Sides South | 6.0 12.0 6.0 | 6.0 6.0 | 6.0 | | | |
| A25 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B25 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C25 | 6 | North Sides South | 2.7 3.3 0.0 | 2.7 3.3 | | | | D25 | 16 | North Sides South | 4.0 8.0 4.0 | 4.0 4.0 | 4.0 | | |
| A26 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B26 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C26 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D26 | 9 | North Sides South | 0.0 3.5 5.0 | 1.9 5.0 | 1.7 | | | |
| A27 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B27 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C27 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D27 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A28 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B28 | 3 | North Sides South | 0.0 0.0 3.0 | 3.0 | | | C28 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D28 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| A29 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B29 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C29 | 8 | North Sides South | 5.4 3.0 0.0 | 5.4 1.6 | 1.4 | | | D29 | 0 | North Sides South | 0.0 0.0 0.0 | | | | |
| A30 | 0 | North Sides South | 0.0 0.0 0.0 | | | | B30 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C30 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D30 | 21 | North Sides South | 4.5 13.1 3.4 | 4.5 9.0 | 4.1 | | | |
| A31 | 22 | North Sides South | 5.7 13.1 2.9 | 5.7 9.6 2.9 | 3.5 | | B31 | 0 | North Sides South | 0.0 0.0 0.0 | | | | C31 | 0 | North Sides South | 0.0 0.0 0.0 | | | | D31 | 0 | North Sides South | 0.0 0.0 0.0 | | | | | |
| Totals | 214 | | | | | | | 40 | | | | | | 103 | | | | | | | 300 | | | | | | | | |

CUY-6-1456 West Station
Jack Arch Repair Summary

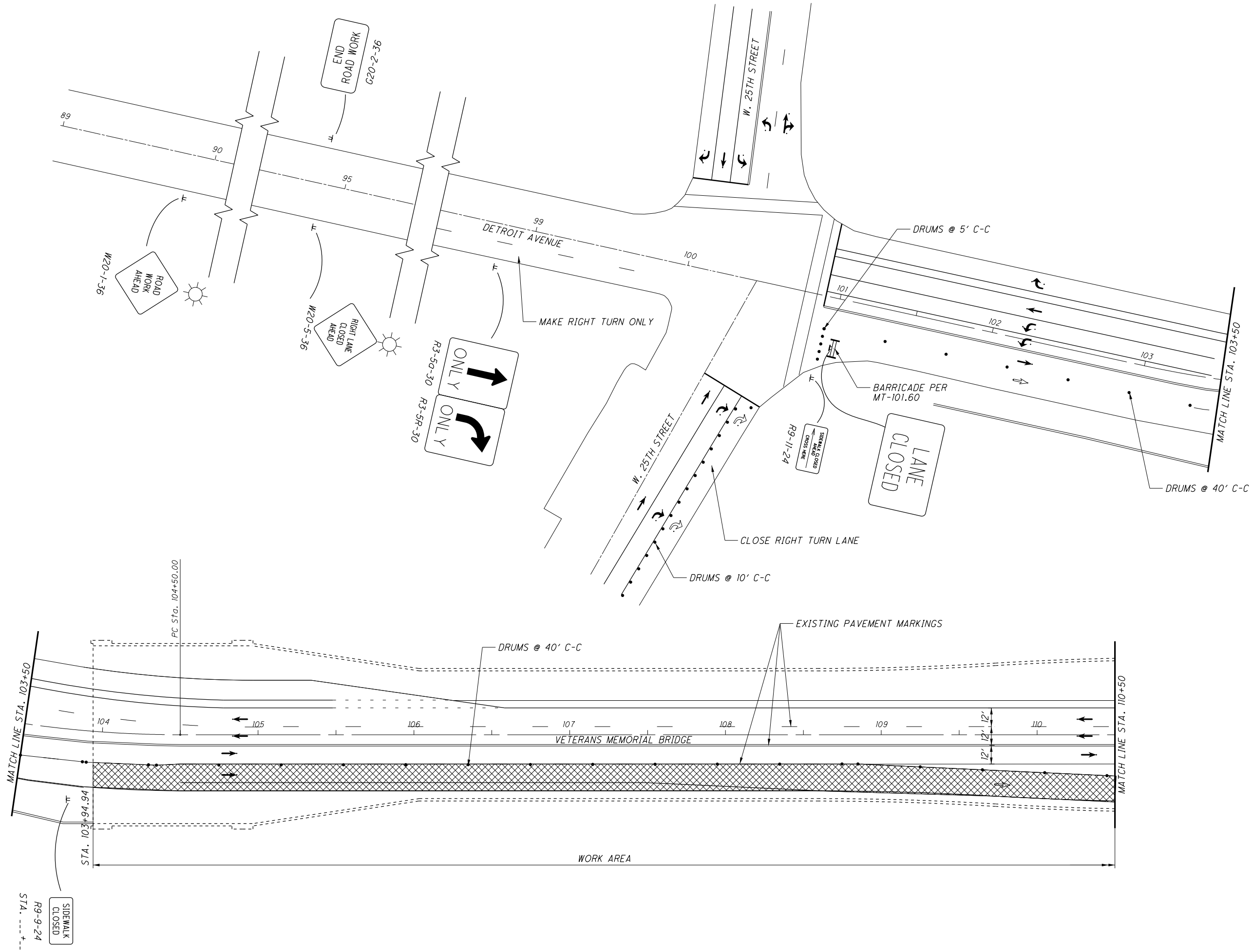
REPLACEMENT RECOMMENDED

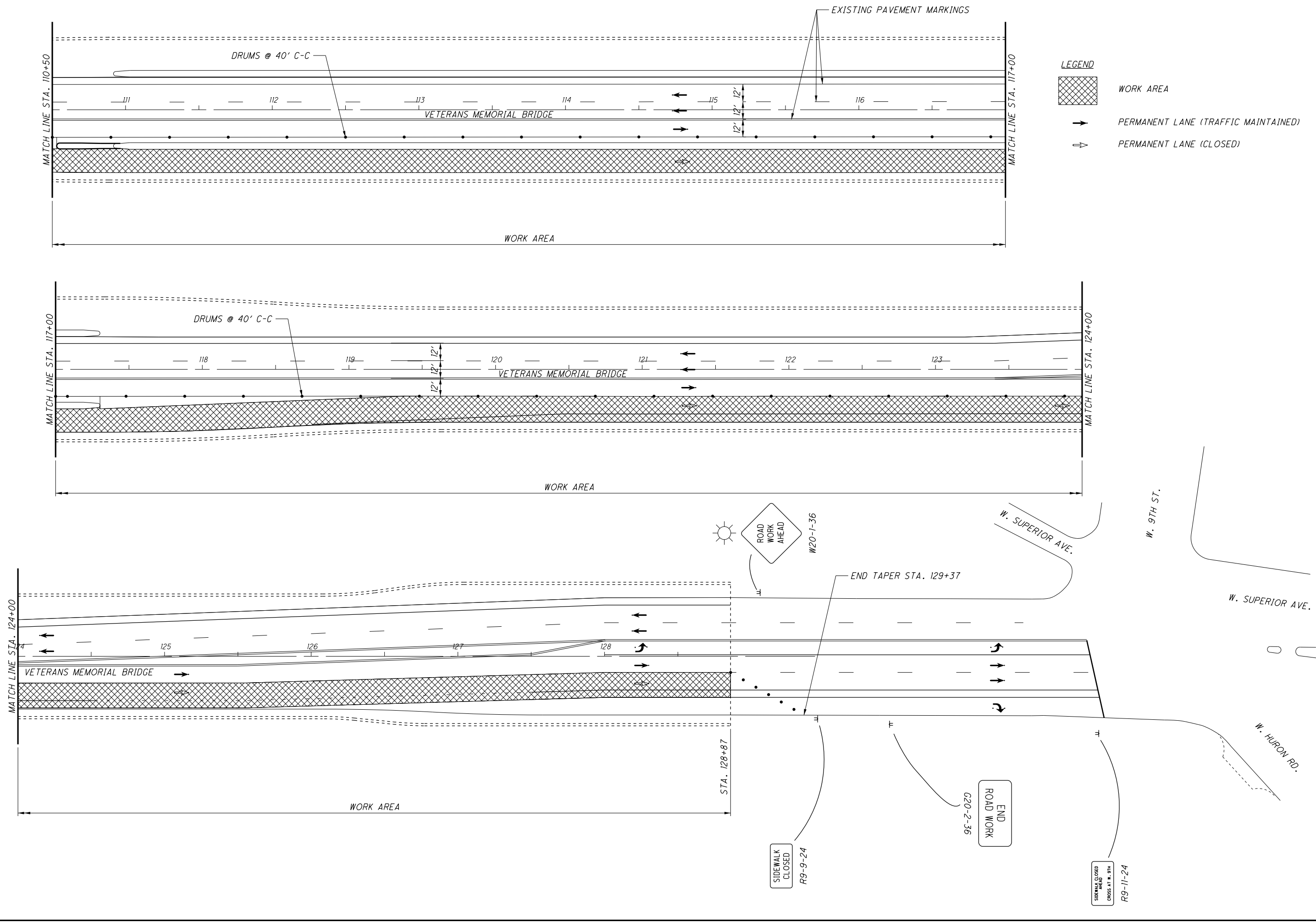
| Jack Arch No. | Total Deficiency (SF) | Surface | Subtotal (SF) | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Jack Arch No. | Total Deficiency (SF) | Surface | Subtotal (SF) | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Jack Arch No. | Total Deficiency (SF) | Surface | Subtotal (SF) | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | Jack Arch No. | Total Deficiency (SF) | Surface | Subtotal (SF) | Area 1 (SF) | Area 2 (SF) | Area 3 (SF) | |
|---------------|-----------------------|--------------------------|----------------------|---------------------|--------------------|-------------------|---------------|-----------------------|--------------------------|----------------------|----------------------|--------------|-------------|---------------|-----------------------|--------------------------|----------------------|----------------------|--------------------|-------------|---------------|-----------------------|--------------------------|--------------------------|----------------------|---------------------|-------------|--|
| | | | | | | | B 1-2 | 0 | North Bottom South | 30.7 0.0 5.8 | 30.7 | | | C 1-2 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | | | | | | | | |
| A 2-3 | 10 | North Bottom South | 1.1 8.5 0.0 | 1.1 8.5 | | | B 2-3 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | C 2-3 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | | | | | | | | |
| A 3-4 | 17 | North Bottom South | 11.0 3.6 2.9 | 11.0 3.6 2.9 | | | B 3-4 | 5 | North Bottom South | 5.0 0.0 0.0 | 5.0 | | | C 3-4 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 3-4 | 29 | North Bottom South | 10.2 4.9 14.3 | 9.6 2.4 10.1 | 0.6 2.5 4.3 | | |
| A 4-5 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 4-5 | 25 | North Bottom South | 7.7 10.3 6.8 | 7.7 2.8 6.8 | | 7.5 | C 4-5 | 16 | North Bottom South | 11.1 4.8 0.0 | 11.1 4.8 | | | | D 4-5 | 0 | North Bottom South | 0.0 0.0 0.0 | | | |
| A 5-6 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 5-6 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | C 5-6 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 5-6 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | |
| A 6-7 | 16 | North Bottom South | 14.6 1.5 0.0 | 4.9 1.5 | 9.7 | | B 6-7 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | C 6-7 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 6-7 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | |
| A 7-8 | 1 | North Bottom South | 1.2 0.0 0.0 | 1.2 | | | B 7-8 | 1 | North Bottom South | 0.0 0.0 1.0 | | 1.0 | | C 7-8 | 11 | North Bottom South | 4.5 2.8 3.6 | 1.9 1.1 2.3 | 2.6 1.8 1.3 | | | D 7-8 | 0 | North Bottom South | 0.0 0.0 0.0 | | | |
| A 8-9 | 15 | North Bottom South | 12.4 2.3 0.0 | 4.7 2.3 | 3.8 4.0 | | B 8-9 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | C 8-9 | 6 | North Bottom South | 3.5 2.4 0.0 | 3.5 2.4 | | | | D 8-9 | 8 | North Bottom South | 0.0 2.0 5.6 | | 2.0 5.6 | |
| A 9-10 | 58 | North Bottom South | 45.5 7.0 5.6 | 45.5 7.0 5.6 | | | B 9-10 | 4 | North Bottom South | 0.0 0.0 3.6 | | 2.5 1.1 | | C 9-10 | 10 | North Bottom South | 5.5 0.0 4.3 | 4.3 4.3 | 1.3 | | | D 9-10 | 0 | North Bottom South | 0.0 0.0 0.4 | | 0.4 | |
| A 10-11 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 10-11 | 24 | North Bottom South | 10.7 2.3 11.2 | 10.7 2.3 9.9 | | 1.3 | C 10-11 | 21 | North Bottom South | 12.0 5.5 3.7 | 6.1 4.2 2.7 | 5.9 1.4 1.0 | | | D 10-11 | 1 | North Bottom South | 1.0 0.0 0.0 | 1.0 | | |
| A 11-12 | 55 | North Bottom South | 44.8 9.3 0.8 | 44.8 9.3 0.8 | | | B 11-12 | 4 | North Bottom South | 4.3 0.0 0.0 | 4.3 | | | C 11-12 | 36 | North Bottom South | 19.8 3.6 13.0 | 16.4 3.6 13.0 | 3.3 | | | D 11-12 | 14 | North Bottom South | 13.9 0.0 0.0 | 13.9 | | |
| A 12-13 | 21 | North Bottom South | 13.9 1.9 5.4 | 13.9 1.9 5.4 | | | B 12-13 | 11 | North Bottom South | 6.9 2.7 1.7 | 6.9 2.7 1.7 | | | C 12-13 | 41 | North Bottom South | 15.1 11.1 15.2 | 3.4 4.0 5.9 | 11.7 7.1 9.3 | | | D 12-13 | 27 | North Bottom South | 26.5 0.0 0.0 | 26.5 | | |
| A 13-14 | 9 | North Bottom South | 9.2 0.0 0.0 | 9.2 | | | B 13-14 | 11 | North Bottom South | 0.0 0.0 11.1 | | 11.1 | | C 13-14 | 85 | North Bottom South | 29.1 22.9 33.4 | 4.6 22.9 33.4 | 24.5 | | | D 13-14 | 0 | North Bottom South | 0.0 0.0 0.0 | | | |
| A 14-15 | 20 | North Bottom South | 12.8 4.3 3.0 | 2.7 4.3 3.0 | 10.1 | | B 14-15 | 13 | North Bottom South | 1.8 8.1 3.0 | 1.8 0.6 1.2 | 5.0 2.5 | | C 14-15 | 53 | North Bottom South | 17.3 13.3 22.0 | 14.3 6.7 10.5 | 3.0 6.7 11.5 | | | D 14-15 | 6 | North Bottom South | 4.4 1.3 0.0 | 3.6 1.3 | 0.8 | |
| A 15-16 | 42 | North Bottom South | 26.1 6.5 9.6 | 26.1 6.5 7.6 | | | B 15-16 | 7 | North Bottom South | 3.1 2.5 1.8 | 1.8 2.5 | 1.4 | | C 15-16 | 12 | North Bottom South | 6.9 1.9 2.7 | 1.5 1.9 2.7 | 4.5 0.9 | | | D 15-16 | 0 | North Bottom South | 0.0 0.0 0.0 | | | |
| A 16-17 | 61 | North Bottom South | 42.1 4.5 14.8 | 26.1 2.3 3.9 | 16.0 2.3 8.3 | 2.6 | B 16-17 | 47 | North Bottom South | 16.4 14.4 15.9 | 16.4 4.0 3.5 | 10.5 12.4 | | C 16-17 | 24 | North Bottom South | 14.3 9.9 0.0 | 3.5 9.9 | 10.8 | | | D 16-17 | 3 | North Bottom South | 2.9 0.0 0.0 | 2.9 | | |
| A 17-18 | 37 | North Bottom South | 20.5 11.3 5.7 | 11.8 8.3 2.6 | 5.9 0.5 3.1 | 2.9 2.5 | B 17-18 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | C 17-18 | 1 | North Bottom South | 0.9 0.0 0.0 | 0.9 | | | D 17-18 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | |
| A 18-19 | 32 | North Bottom South | 3.3 28.4 1.4 | 1.0 10.8 1.4 | 2.3 9.6 13.1 | 8.0 | B 18-19 | 38 | North Bottom South | 12.7 12.5 13.2 | 12.7 12.5 13.2 | | | C 18-19 | 43 | North Bottom South | 16.9 10.0 16.0 | 3.5 10.0 16.0 | 13.4 | | | D 18-19 | 0 | North Bottom South | 0.0 0.0 0.0 | | | |
| A 19-20 | 32 | North Bottom South | 1.4 4.6 26.1 | 1.4 4.6 13.1 | | | B 19-20 | 11 | North Bottom South | 2.9 0.0 7.7 | 2.9 | | | C 19-20 | 5 | North Bottom South | 2.6 0.0 2.6 | 2.6 | | | D 19-20 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | |
| A 20-21 | 46 | North Bottom South | 26.0 9.3 11.1 | 11.7 3.3 6.1 | 11.7 3.0 2.1 | 2.7 3.0 2.9 | B 20-21 | 28 | North Bottom South | 10.7 6.6 10.5 | 10.7 5.0 7.7 | 1.6 2.8 | | C 20-21 | 23 | North Bottom South | 8.8 6.7 7.6 | 5.9 6.7 5.9 | 2.9 1.7 | | | D 20-21 | 1 | North Bottom South | 0.0 0.0 1.0 | 1.0 | | |
| A 21-22 | 32 | North Bottom South | 23.7 4.6 4.0 | 23.7 4.6 2.9 | 1.1 | | B 21-22 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | C 21-22 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 21-22 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | |
| A 22-23 | 76 | North Bottom South | 24.7 23.0 28.8 | 24.7 23.0 1.6 | 24.6 2.6 | | B 22-23 | 38 | North Bottom South | 16.1 12.5 9.2 | 16.1 12.5 9.2 | | | C 22-23 | 64 | North Bottom South | 19.1 18.7 26.3 | 19.1 18.7 26.3 | | | | D 22-23 | 14 | North Bottom South | 5.9 0.0 8.0 | 5.9 | | |
| A 23-24 | 6 | North Bottom South | 0.0 6.0 0.0 | 6.0 | | | B 23-24 | 10 | North Bottom South | 4.9 0.0 5.6 | 4.9 0.0 5.6 | | | C 23-24 | 9 | North Bottom South | 3.2 0.0 5.8 | 3.2 0.0 2.6 | 3.2 | | | D 23-24 | 0 | North Bottom South | 0.0 0.0 0.0 | | | |
| A 24-25 | 75 | North Bottom South | 25.5 24.0 25.5 | 25.5 24.0 2.4 | | | B 24-25 | 73 | North Bottom South | 30.5 20.8 21.7 | 28.5 20.8 21.7 | 2.0 | | C 24-25 | 60 | North Bottom South | 22.1 15.5 22.5 | 22.1 15.5 22.5 | | | | D 24-25 | 0 | North Bottom South | 0.0 0.0 0.0 | | | |
| A 25-26 | 4 | North Bottom South | 2.4 1.6 0.0 | 1.6 | | | B 25-26 | 2 | North Bottom South | 2.0 0.0 0.0 | 2.0 | | | C 25-26 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 25-26 | 10 | North Bottom South | 4.0 0.0 5.6 | 4.0 | | | |
| A 26-27 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 26-27 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | C 26-27 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 26-27 | 16 | North Bottom South | 8.8 2.0 4.7 | 4.9 2.0 1.0 | 2.2 1.9 | 1.8 1.8 | |
| A 27-28 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 27-28 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | C 27-28 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 27-28 | 13 | North Bottom South | 1.7 0.0 11.1 | 1.7 | 3.5 7.6 | | |
| A 28-29 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 28-29 | 68 | North Bottom South | 23.2 21.7 23.3 | 23.2 21.7 23.3 | | | C 28-29 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 28-29 | 49 | North Bottom South | 25.6 10.0 12.9 | 25.6 6.0 12.9 | 4.0 | | |
| A 29-30 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 29-30 | 3 | North Bottom South | 0.0 0.0 2.7 | 2.7 | | | C 29-30 | 4 | North Bottom South | 4.4 0.0 0.0 | 1.2 0.0 | 3.2 | | | D 29-30 | 50 | North Bottom South | 22.0 17.0 11.2 | 22.0 17.0 4.4 | 6.8 | |
| A 30-31 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 30-31 | 2 | North Bottom South | 2.4 0.0 0.0 | 2.4 | | | C 30-31 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 30-31 | 0 | North Bottom South | 0.0 0.0 0.0 | | | | |
| A 31-Jt. | 0 | North Bottom South | 0.0 0.0 0.0 | | | | B 31-Jt. | 20 | North Bottom South | 7.3 6.7 5.5 | 7.3 6.7 5.5 | | | C 31-Jt. | 0 | North Bottom South | 0.0 0.0 0.0 | | | | D 31-Jt. | 0 | North Bottom South | 0.0 0.0 0.0 | | | | |
| Totals | 667 | 0 | | | | | | 445 | | | | | | 525 | | | | | | | | 239 | | | | | | |

Lines A-D: Total Deterioration = 1875.4 SF

APPENDIX H

MAINTENANCE OF TRAFFIC



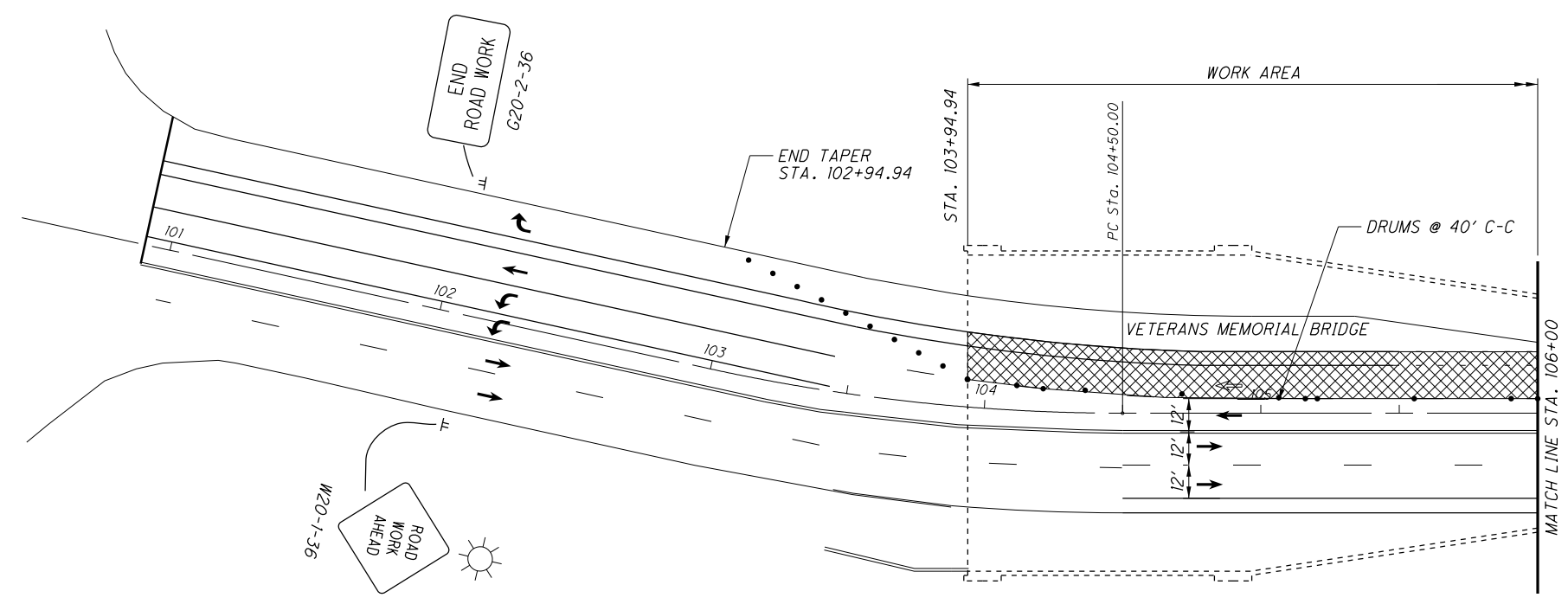
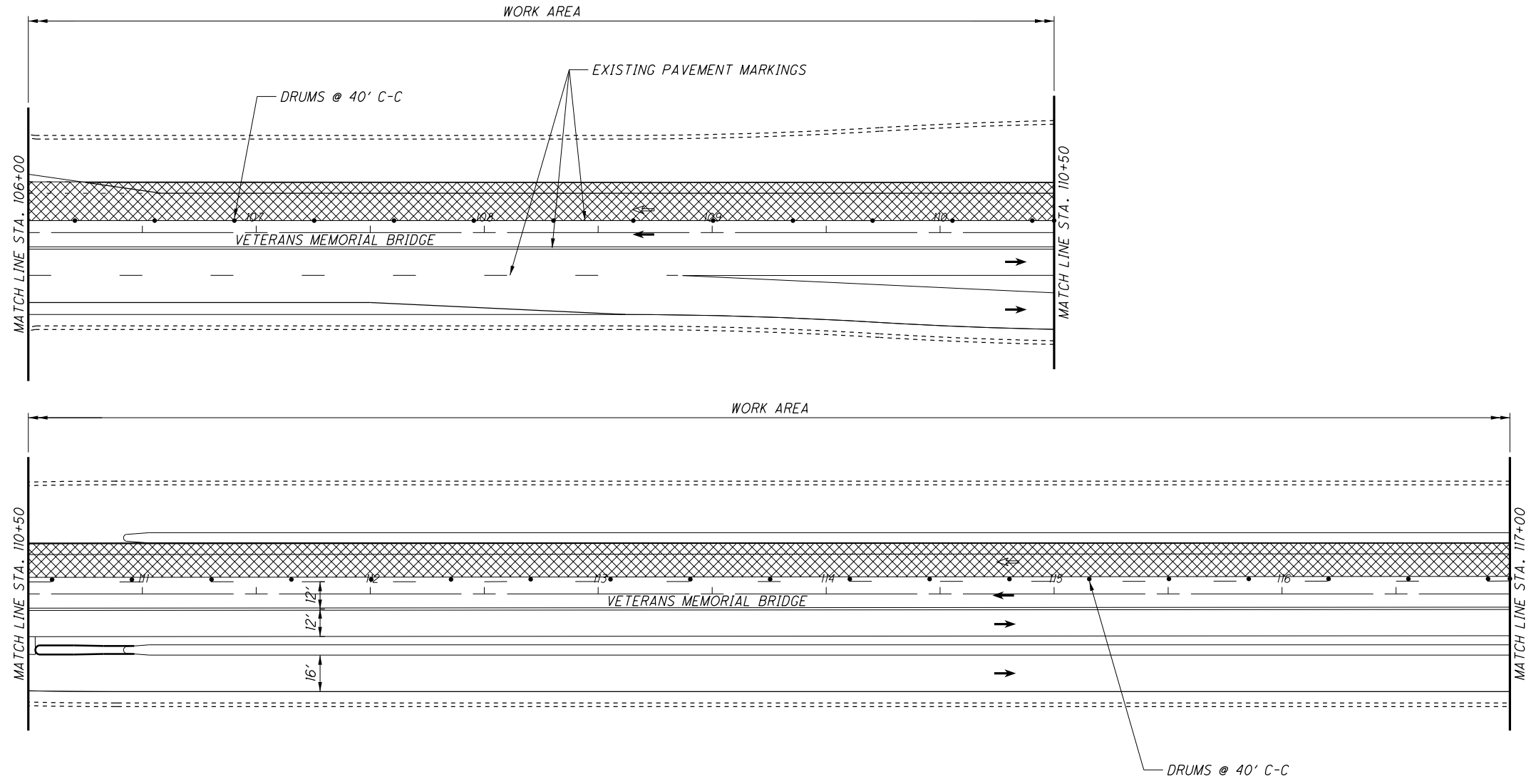


CALCULATED SJD CHECKED JMZ

0 30 60
15
HORIZONTAL SCALE IN FEET

**MAINTENANCE OF TRAFFIC
PHASE 1**

CUY-6-14.56



CALCULATED
SJD
CHECKED
JMZ

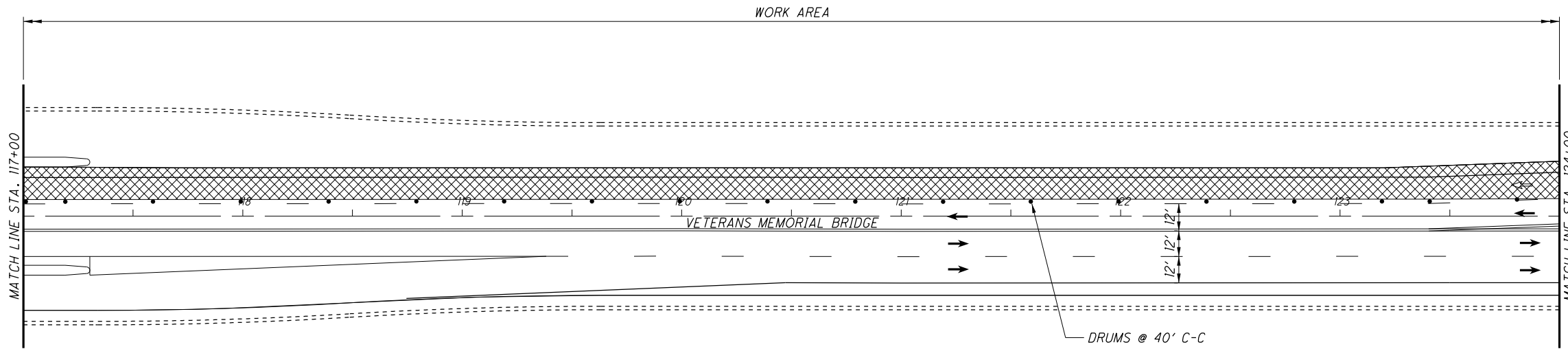
0 15 30 60
HORIZONTAL
SCALE IN FEET

**MAINTENANCE OF TRAFFIC
PHASE 2**

CUY -6 -14.56



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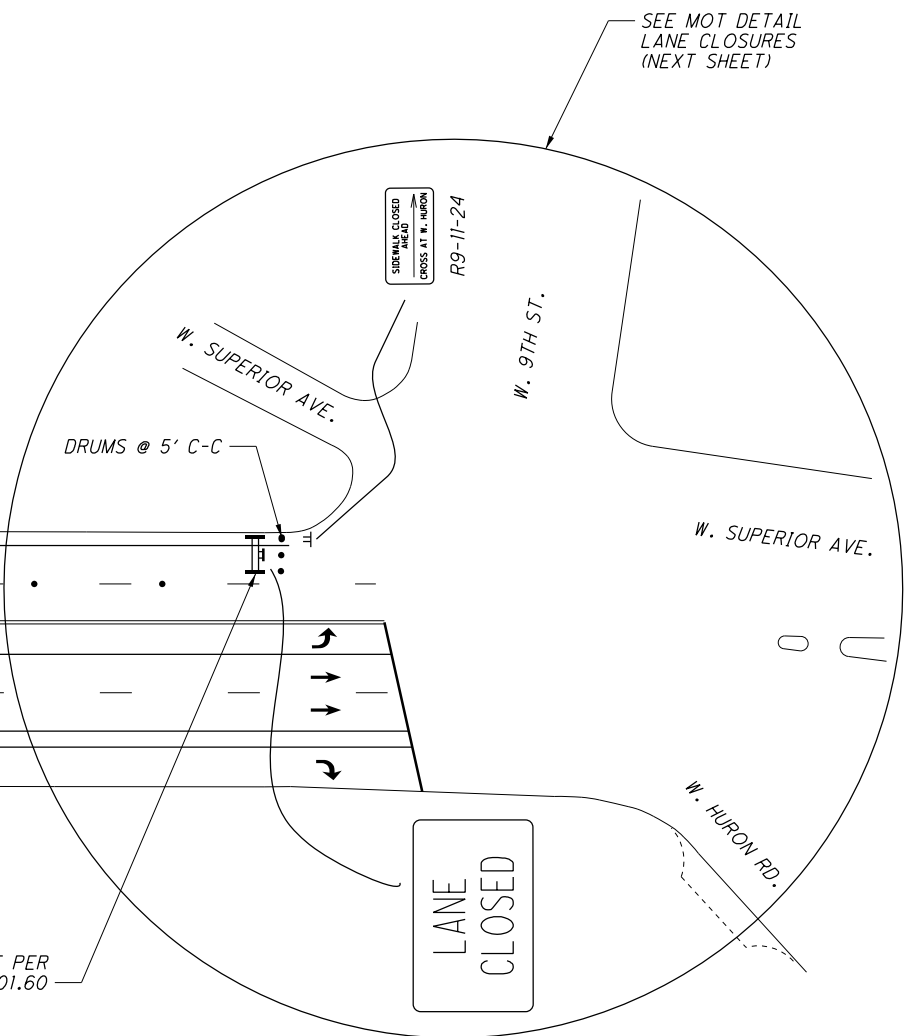
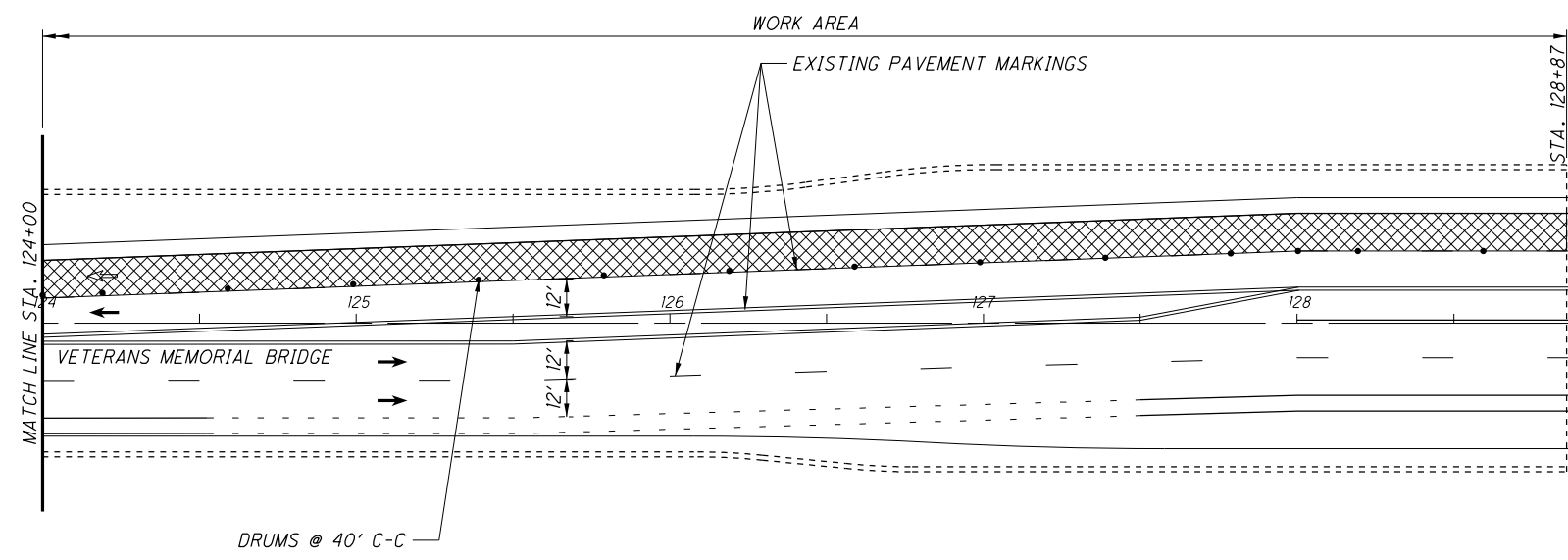


LEGEND

- WORK AREA
- PERMANENT LANE (TRAFFIC MAINTAINED)
- PERMANENT LANE (CLOSED)

CALCULATED SJD CHECKED JMZ

HORIZONTAL SCALE IN FEET



MAINTENANCE OF TRAFFIC PHASE 2

CUY -6 -14.56





MAKE INSIDE RIGHT TURN ONLY TO W. SUPERIOR

OVERHEAD SIGN DETAIL
W. 9TH ST.



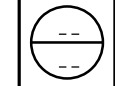
MOT DETAIL LANE CLOSURES

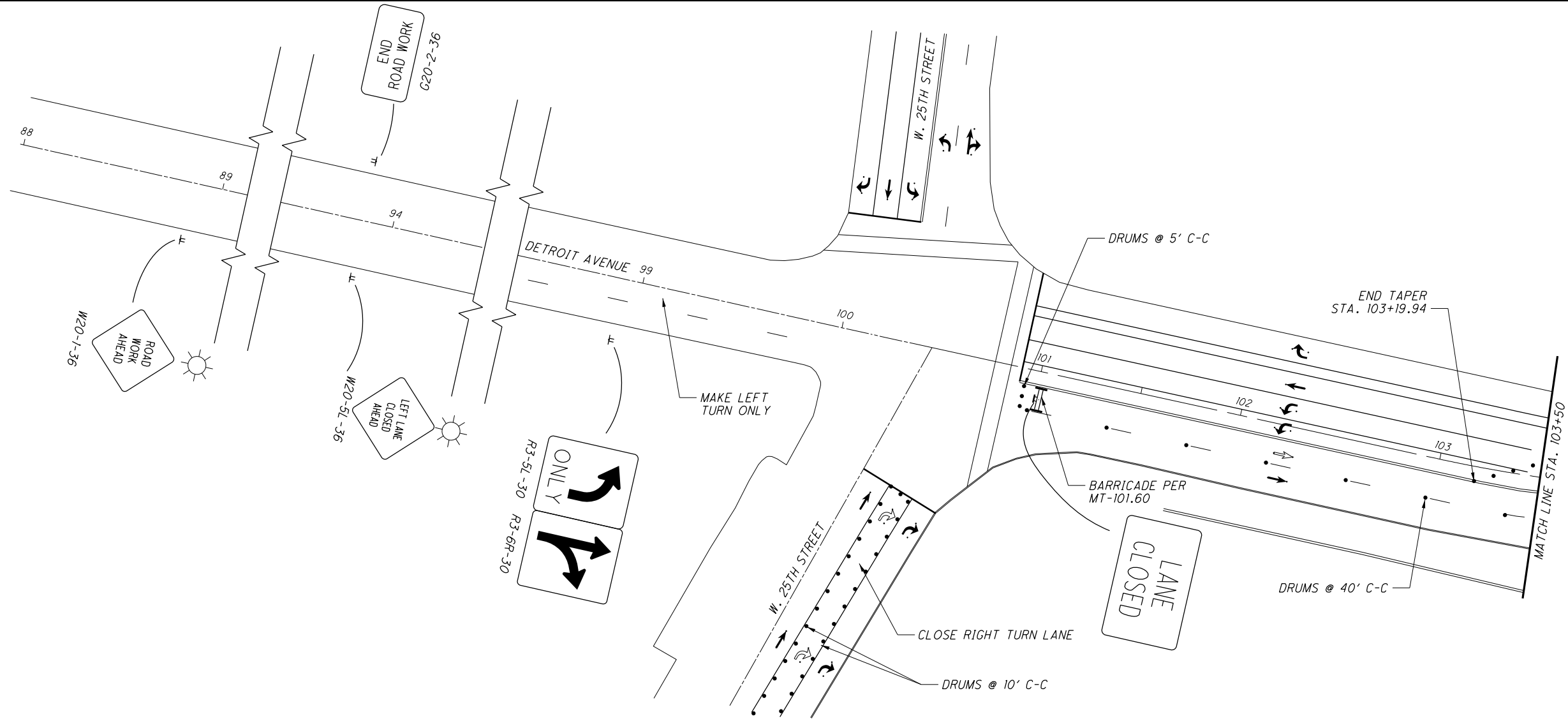
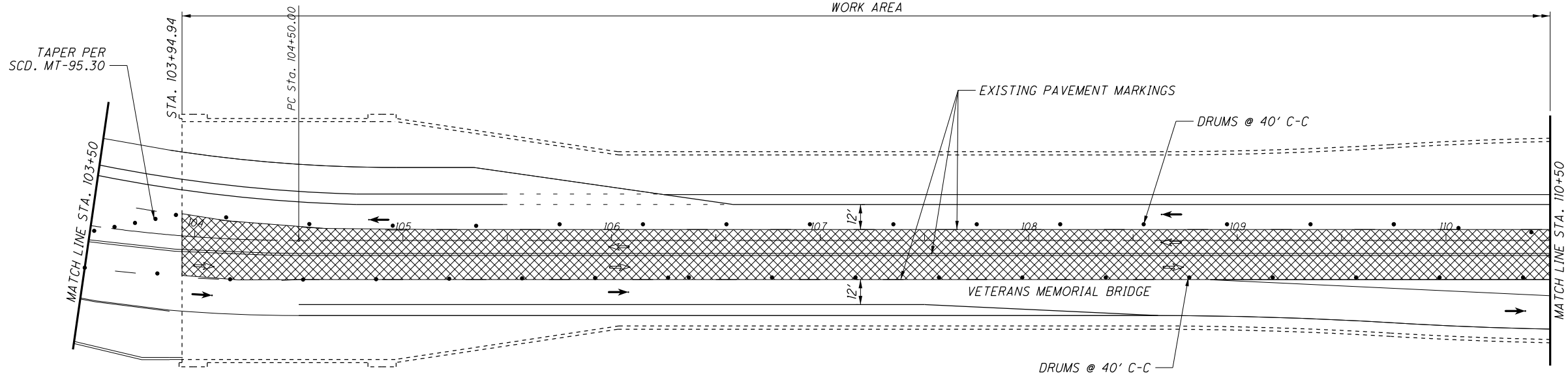
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HORIZONTAL SCALE IN FEET

**MAINTENANCE OF TRAFFIC
PHASE 2**

CUY-6-14.56





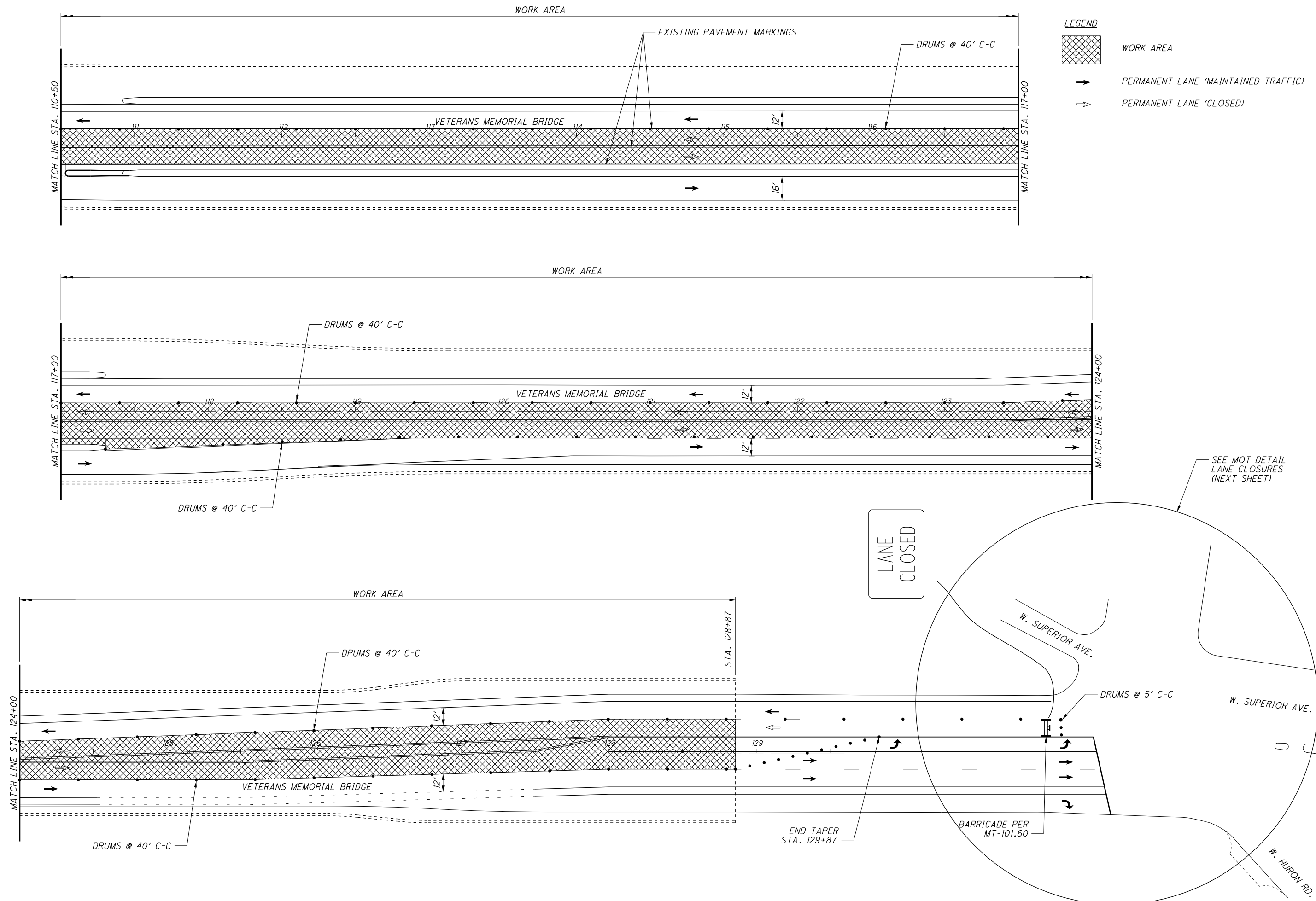
| | | | |
|------------|-----|---------|-----|
| CALCULATED | SJD | CHECKED | JMZ |
| | | | |

0 30 60
15
HORIZONTAL
SCALE IN FEET

**MAINTENANCE OF TRAFFIC
PHASE 3**

CUY-6-14.56

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CALCULATED SJD CHECKED JMZ

0 15 30 60

HORIZONTAL SCALE IN FEET

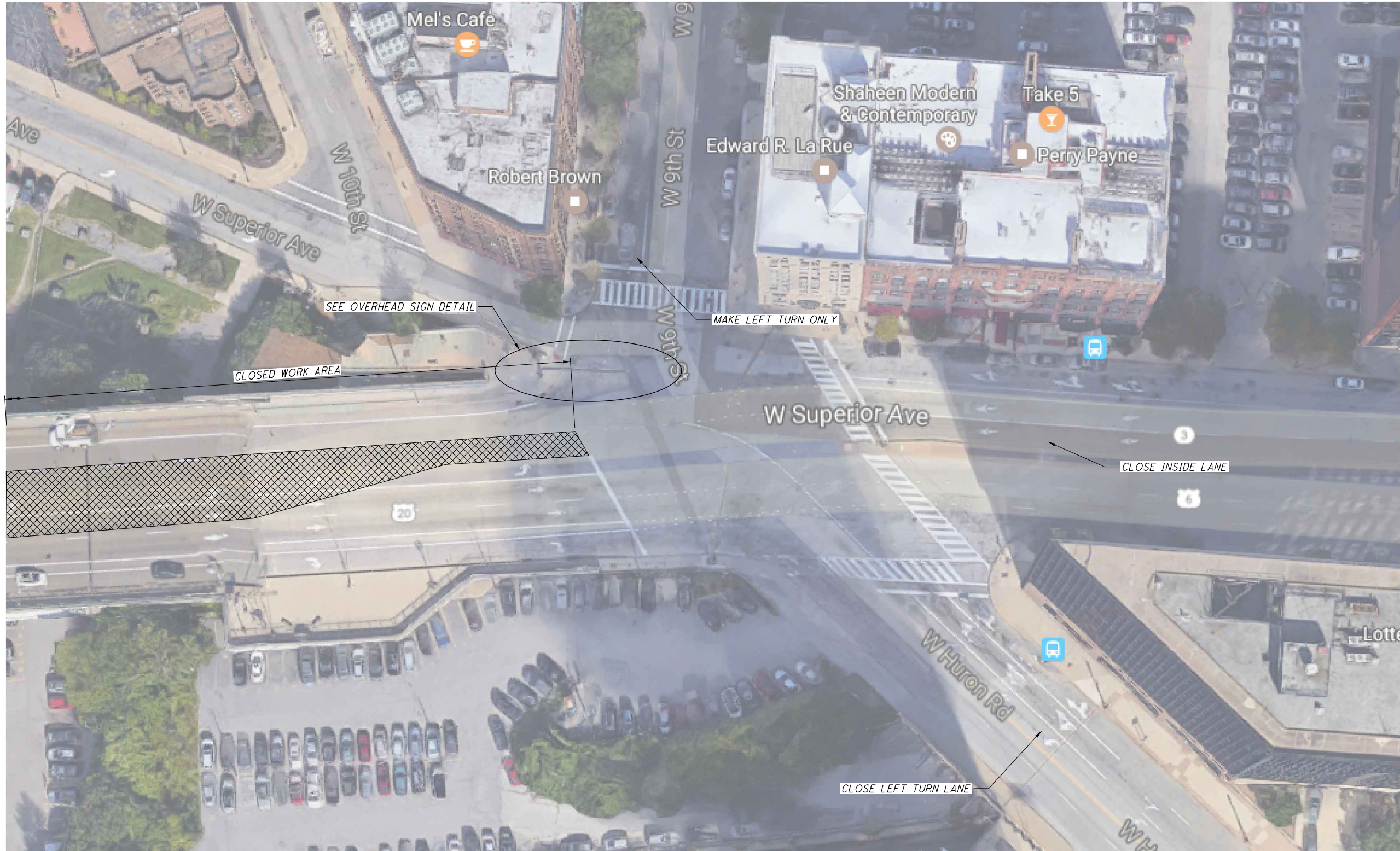
MAINTENANCE OF TRAFFIC PHASE 3

CUY-6-14.56





OVERHEAD SIGN DETAIL



MOT DETAIL LANE CLOSURES



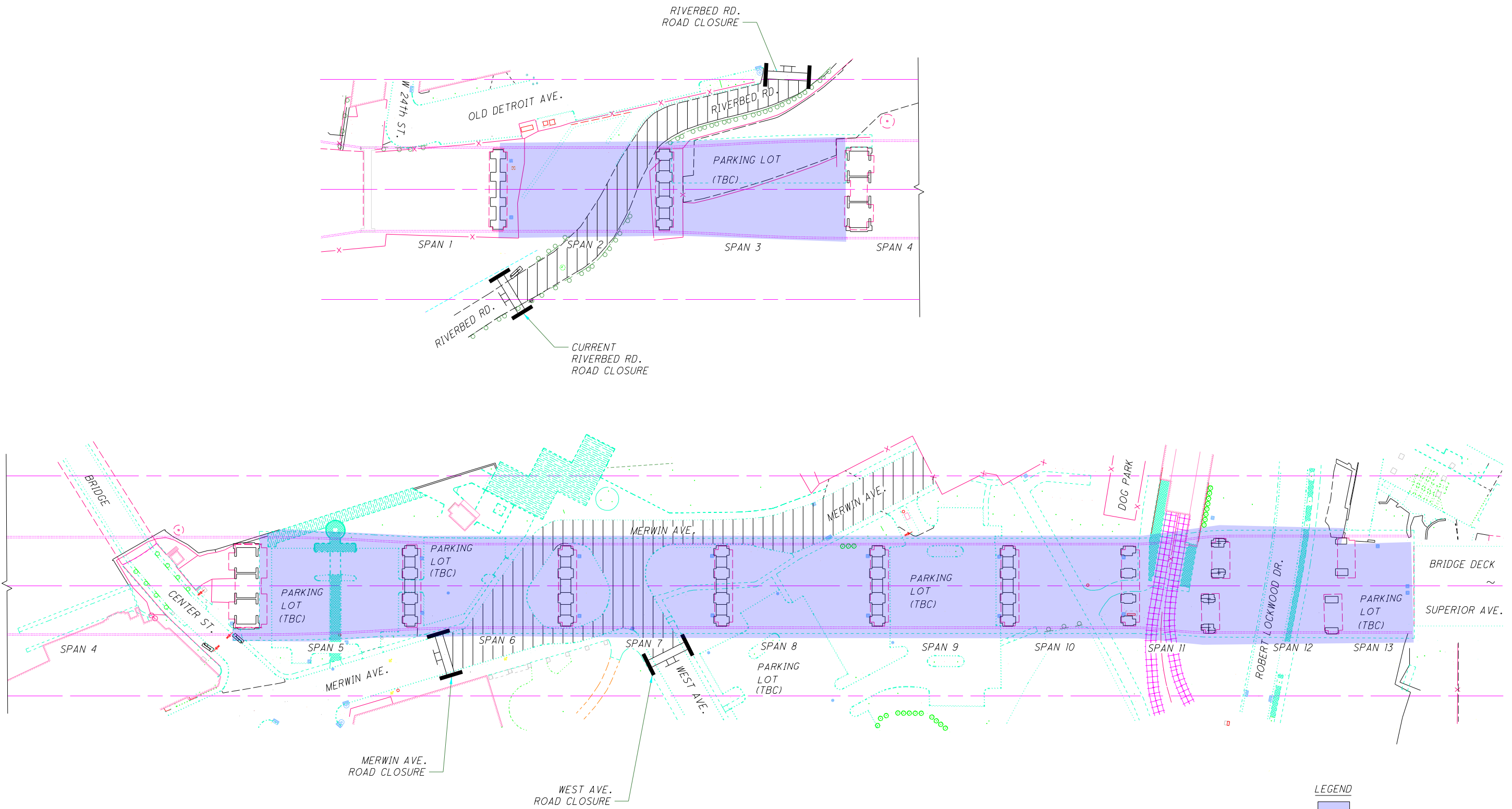
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MAINTENANCE OF TRAFFIC PHASE 3





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LEGEND

-  - PUBLIC AREAS
-  - ROAD CLOSED
-  - ROAD CLOSURE BARRIER AND ROAD CLOSED SIGN
-  - TO BE CLOSED, WHEN REQUIRED



MAINTENANCE OF TRAFFIC
PUBLIC AREAS AND CLOSURES

CUY-6-14.56

