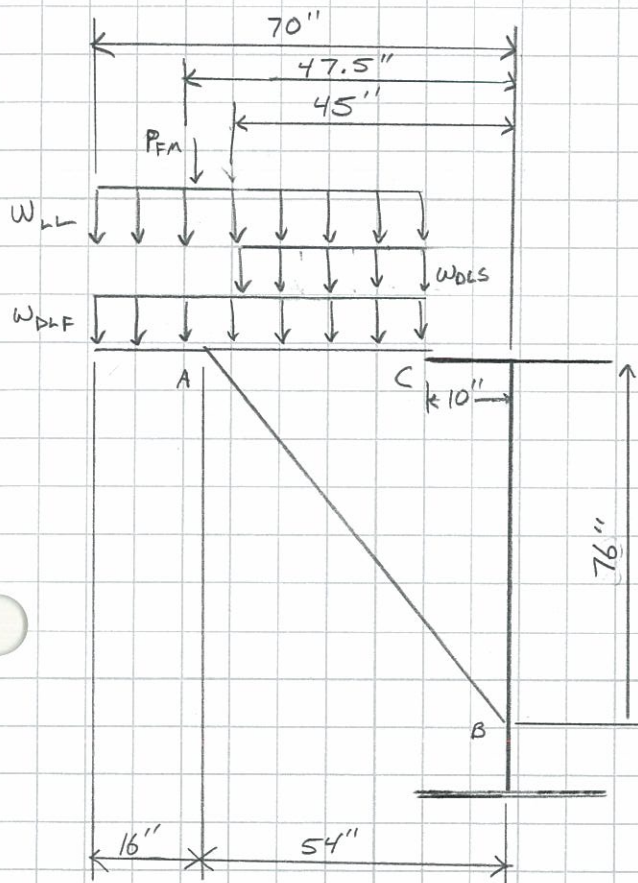


Oil canning check (ϕ_o)

Reaction from OH Bracket



Bracket Spacing = 32" = 2.67'

$$W_{DLF} = 10 \text{ psf} \times 2.67' = 26.7 \text{ \#/ft}$$

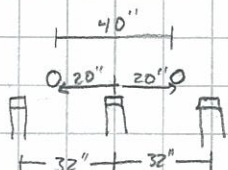
$$W_{DL5} = (14 \text{ \#/12}) \times 150 \times 2.67' = 467.25 \text{ \#/ft}$$

$$W_{LL} = 50 \text{ psf} \times 2.67' = 133.5 \text{ \#/ft}$$

$$P_F = 2.25^k$$

w/spacing 48"-40"-48"

conservatively say 1 wheel/bracket



$$\frac{12}{32} = 0.375$$

$$0.375 \times 2 = 0.75$$

∴ 1 wheel is conservative.

Reaction @ A

\sum Moments abt. C

$$A = \left[\left((W_{DLF} + W_{LL}) \times (70 - 10) \right) \left(\frac{70 - 10}{2} \right) + \right. \\ \left. (W_{DL5} \times (45 - 10)) \left(\frac{45 - 10}{2} \right) + \right. \\ \left. (P_{FA} \times (47.5 - 10)) \right] \div (54 - 10)$$

$$A = \left[\left((26.7 + 133.5) (5') (2.5') + \right. \right. \\ \left. \left. (467.25 \times 2.92) (1.46') + \right. \right. \\ \left. \left. (2250 \times (3.125)) \right] \div 3.67$$

$$A = 3.01^k \uparrow$$

$$B = (3.01^k \times 4.5 / 6.33) = 2.14^k \rightarrow$$

To estimate deflection in the web from the overhang bracket loading, assume the web acts as 96" x 32" plate with a 2.14" concentrated loading. The plate is simply supported on all sides. This will give a conservative estimate of the "oil-canning" effect.

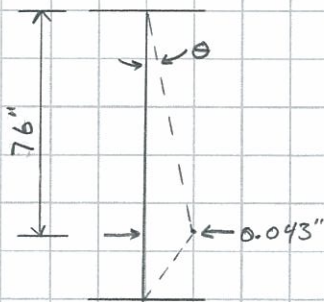
From Roark's Formulas for stress and strain. (Attached)

The max deflection of a simply supported plate with a concentrated load:

$$y_{max} = \frac{\alpha (2.14)(32^2)}{29000 (0.6875)^3}$$

$$a/b = 96/32 = 3 \quad \therefore \alpha = 0.1851$$

$$y_{max} = \frac{(0.1851)(2.14)(32^2)}{(29000)(0.6875)^3} = 0.043"$$



$$\theta = \tan^{-1} \left(\frac{0.043}{76} \right) = 0.032^\circ$$

Loss of Deck Thickness

$$\phi_o = 0.032^\circ$$

$$\phi_w = 0.104^\circ$$

$$\phi_{tot} = 0.136^\circ$$

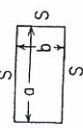

$$L_b = 47.5"$$

$$f = [\tan(0.136^\circ)] \times 47.5 =$$

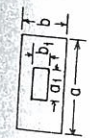
$$f = 0.11" < 0.5" \quad \underline{\underline{OK}}$$

TABLE 11.4 Formulas for flat plates with straight boundaries and constant thickness

NOTATION: The notation for Table 11.2 applies with the following modifications: a and b refer to plate dimensions, and when used as subscripts for stresses, they refer to the stresses in directions parallel to the sides a and b , respectively. σ is a bending stress which is positive when tensile on the bottom and compressive on the top if loadings are considered vertically downward. R is the reaction force per unit length normal to the plate surface exerted by the boundary support on the edge of the plate. r_0 is the equivalent radius of contact for a load concentrated on a very small area and is given by $r_0 = \sqrt{1.67t + t^2} - 0.675t$ if $r_0 < 0.5t$ and $r_0 = r_0$ if $r_0 \geq 0.5t$.

Case no., shape, and supports	Case no., loading	Formulas and tabulated specific values																																										
1. Rectangular plate; all edges simply supported		(At center) $\sigma_{\max} = \sigma_y = \frac{\beta qb^2}{t^2}$ and $y_{\max} = \frac{-\alpha qb^4}{Et^3}$ (At center of long sides) $R_{\max} = \gamma qb$																																										
		<table border="1"> <tr> <td>a/b</td> <td>1.0</td> <td>1.2</td> <td>1.4</td> <td>1.6</td> <td>1.8</td> <td>2.0</td> <td>3.0</td> <td>4.0</td> <td>5.0</td> <td>∞</td> </tr> <tr> <td>β</td> <td>0.2874</td> <td>0.3762</td> <td>0.4530</td> <td>0.5172</td> <td>0.5688</td> <td>0.6102</td> <td>0.7134</td> <td>0.7410</td> <td>0.7476</td> <td>0.7500</td> </tr> <tr> <td>α</td> <td>0.0444</td> <td>0.0616</td> <td>0.0770</td> <td>0.0906</td> <td>0.1017</td> <td>0.1110</td> <td>0.1335</td> <td>0.1400</td> <td>0.1417</td> <td>0.1421</td> </tr> <tr> <td>γ</td> <td>0.420</td> <td>0.455</td> <td>0.478</td> <td>0.491</td> <td>0.499</td> <td>0.503</td> <td>0.505</td> <td>0.502</td> <td>0.501</td> <td>0.500</td> </tr> </table> (Ref. 21 for $\nu = 0.3$)	a/b	1.0	1.2	1.4	1.6	1.8	2.0	3.0	4.0	5.0	∞	β	0.2874	0.3762	0.4530	0.5172	0.5688	0.6102	0.7134	0.7410	0.7476	0.7500	α	0.0444	0.0616	0.0770	0.0906	0.1017	0.1110	0.1335	0.1400	0.1417	0.1421	γ	0.420	0.455	0.478	0.491	0.499	0.503	0.505	0.502
a/b	1.0	1.2	1.4	1.6	1.8	2.0	3.0	4.0	5.0	∞																																		
β	0.2874	0.3762	0.4530	0.5172	0.5688	0.6102	0.7134	0.7410	0.7476	0.7500																																		
α	0.0444	0.0616	0.0770	0.0906	0.1017	0.1110	0.1335	0.1400	0.1417	0.1421																																		
γ	0.420	0.455	0.478	0.491	0.499	0.503	0.505	0.502	0.501	0.500																																		
1b. Uniform over small concentric circle of radius r_0 (note definition of r_0)		$\sigma_{\max} = \frac{3W}{2\pi t^2} \left[(1 + \nu) \ln \frac{2b}{\pi r_0} + \beta \right]$ $y_{\max} = \frac{-\alpha W r_0^2}{Et^3}$																																										
		<table border="1"> <tr> <td>a/b</td> <td>1.0</td> <td>1.2</td> <td>1.4</td> <td>1.6</td> <td>1.8</td> <td>2.0</td> <td>∞</td> </tr> <tr> <td>β</td> <td>0.435</td> <td>0.650</td> <td>0.789</td> <td>0.875</td> <td>0.927</td> <td>0.958</td> <td>1.000</td> </tr> <tr> <td>α</td> <td>0.1267</td> <td>0.1478</td> <td>0.1621</td> <td>0.1715</td> <td>0.1770</td> <td>0.1806</td> <td>0.1851</td> </tr> </table> (Ref. 21 for $\nu = 0.3$)	a/b	1.0	1.2	1.4	1.6	1.8	2.0	∞	β	0.435	0.650	0.789	0.875	0.927	0.958	1.000	α	0.1267	0.1478	0.1621	0.1715	0.1770	0.1806	0.1851																		
a/b	1.0	1.2	1.4	1.6	1.8	2.0	∞																																					
β	0.435	0.650	0.789	0.875	0.927	0.958	1.000																																					
α	0.1267	0.1478	0.1621	0.1715	0.1770	0.1806	0.1851																																					

1c. Uniform over central rectangular area

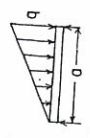


(At center) $\sigma_{\max} = \sigma_x = \frac{\beta W}{t^2}$ where $W = \alpha a b$

a/b	0	0.2	0.4	0.6	0.8	1.0	0	0.2	0.4	0.8	1.2	1.4	0	0.4	0.8	1.2	1.6	2.0
β	1.82	1.28	1.08	0.90	0.76	0.63	1.78	1.43	1.23	0.95	0.74	0.64	1.73	1.31	1.03	0.84	0.68	0.57
α	1.39	1.07	0.84	0.72	0.62	0.52	1.39	1.13	1.00	0.80	0.62	0.55	1.32	1.08	0.88	0.74	0.60	0.50
γ	0.92	0.76	0.62	0.51	0.42	0.36	0.90	0.76	0.68	0.53	0.47	0.40	0.87	0.76	0.63	0.54	0.44	0.38
	0.76	0.63	0.52	0.42	0.35	0.30	0.75	0.62	0.57	0.47	0.38	0.33	0.71	0.61	0.53	0.45	0.38	0.30

(Values from charts of Ref. 8; $\nu = 0.3$)

1d. Uniformly increasing along length



(Values from charts of Ref. 8; $\nu = 0.3$)

$\sigma_{\max} = \frac{\beta qb^2}{t^2}$ and $y_{\max} = \frac{-\alpha qb^4}{Et^3}$

a/b	1	1.5	2.0	2.5	3.0	3.5	4.0
β	0.16	0.26	0.34	0.38	0.43	0.47	0.49
α	0.022	0.043	0.060	0.070	0.078	0.086	0.091

(Values from charts of Ref. 8; $\nu = 0.3$)

1e. Uniformly increasing along width

$\sigma_{\max} = \frac{\beta qb^2}{t^2}$ and $y_{\max} = \frac{-\alpha qb^4}{Et^3}$

LJD 3/30/12
EDG 4-2-12
LJD 4/3/12



PROJECT INFORMATION

File Name..... Ramp A5_Overhang_RFI00282.prj
File Location..... N:\49633\Bridges\Design\Final Design\A5\TAEG\Ramp A5_Overhang_RFI00282.prj
Project Number..... 49633
Engineer..... LJD
Project Title..... Cleveland Innerbelt Ramp A5
Last Modified..... Friday, March 30, 2012
Created..... Friday, March 30, 2012
Units..... U.S. Customary
Notes.....

GIRDER DATA

Top Flange (Width x Thickness)..... 20 x 1 [in.]
Web (Height x Thickness)..... 96 x .6875 [in.]
Bottom Flange (Width x Thickness)..... 20 x 1 [in.]
Yield Stress, Fy..... 50 [ksi]
Modulus of Elasticity, E..... 29000 [ksi]

BRIDGE LATERAL DATA

Distance Between Lateral Supports..... 300 [in.]
Distance Between Adjacent Girders..... 131 [in.]
Number of Girders..... 5
Bridge Skew..... 0 - 20 [Degrees]
Continuous Girder..... YES
Length of Maximum Side Span..... 2662 [in.]
Length of Maximum Inner Span..... 2168 [in.]
Symmetric Loading ?..... YES
Continuous Diaphragms or Cross-Frames Full Width of Bridge ?..... YES
Continuous Timber Blocks Full Width of Bridge ?..... NO
Continuous Tie-Rods Full Width of Bridge ?..... NO

PERMANENT LATERAL SUPPORT DATA

Stiffener Width..... 12.5 [in.]
Stiffener Thickness..... .875 [in.]
Permanent Lateral Support Height..... 92 [in.]
Yield Stress, Fy..... 50 [ksi]
Modulus of Elasticity, E..... 29000 [ksi]
Top Offset..... 3 [in.]
Cross-Frames..... YES
Total Section Area of Chord Member..... 4.75 [in.^2]
Total Section Area of Web Member..... 4.75 [in.^2]

TEMPORARY LATERAL SUPPORT DATA

Number of Tie-Rods..... NONE
Number of Timber Blocks..... NONE

BRACKET DATA

Bracket Dimension A..... 70 [in.]
Walkway Width (B)..... 15 [in.]
Bracket Dimension C..... 45 [in.]
Bracket Dimension D..... 5 [in.]
Bracket Dimension E..... 5 [in.]
Bracket Dimension F..... 52.4 [Degrees]
Bracket Dimension G..... 80 [in.]
Bracket Spacing..... 32 [in.]
Bracket Weight..... 50 [lbs]

LOAD DATA

CALCULATED LATERAL SUPPORT RESPONSE

Lateral Support Reaction of the Top Flange (Ft).....	10.26 [kips]
Lateral Support Reaction of the Bottom Flange (Fb).....	10.26 [kips]
Resulting Moment Acting on the Permanent Support (M).....	82.93 [kip-ft.]

ULTIMATE STRENGTH CHECK

Check for Ultimate Strength Using Eq. (10-155) AASHTO : 0.043 < 1 !

FROM BDGS

stlwood\pmwork\jobs\49633\Techprod\Bridges\Design\BDGS\steelDsh_Run_Mod-FI

Girder 1. out. \$ Girder 5. out

Max stress from BDGS:

$$44.64 \text{ ksi (Girder 5 @ 1.355)}$$

conservatively, add max lateral stress from TAEG to max BDGS stress.

$$44.64 \text{ ksi} + 4.34 \text{ ksi} \times 1.5 \times \frac{1}{3} = 46.81 \text{ ksi}$$

Add in wind load stresses calculated by LER:

(see attached page from 2011-08-01_Ramp A5_Superstructure Calculations_Conformance,

$$46.81 \text{ ksi} + 1.54 \text{ ksi} / 3 = 47.3 \text{ ksi}$$

REFERENCE ONLY

For Cleveland - Ramp A5	Job no. 491233	Sheet no.
Made by LER	Checked by DHE	Backchecked by
Date 3/2/11	Date 03/09/2011	Date

Results:

Case No	f_2 (ksi)	
	TF	BF
1 ✓	1.7 ✓	1.7 ✓
2 ✓	2.4 ✓	1.7 ✓

The stresses at the top and bottom flanges for Case 1 are consistent with those estimated using AASHTO's approximate method. The same can be said for the bottom flange of case 2. The lateral flange stresses due to OH dead loads are combined with the stress due to wind load when checking the capacity of the flanges. Accounting for the larger flange size at the top flange of case 2, the stress due to wind load is:

$$S = \frac{1}{16} (22)^2 (1.25) = 101 \text{ in}^3 \checkmark$$

$$f_w = \frac{13 \text{ kft} \times 12}{101} = 1.54 \text{ ksi} \checkmark$$

Conservatively using the flange stress shown above, which includes live load, to calculate the Str IV construction case design stress gives ✓

$$f_{2u} = 1.25(2.4) + 1.4(1.54) = 5.2 \text{ ksi} \checkmark$$

Subsequent calculations estimate a factored Str IV (const) lateral flange stress of 5.9 ksi using stresses from the approximate AASHTO method. The later is therefore considered sufficient for design. ✓

CALCULATED LATERAL SUPPORT RESPONSE

Lateral Support Reaction of the Top Flange (Ft).....	6.64 [kips]
Lateral Support Reaction of the Bottom Flange (Fb).....	6.64 [kips]
Resulting Moment Acting on the Permanent Support (M).....	53.61 [kip-ft.]

ULTIMATE STRENGTH CHECK

Check for Ultimate Strength Using Eq. (10-155) AASHTO : $0.02 < 1$!

CALCULATED LATERAL SUPPORT RESPONSE

Lateral Support Reaction of the Top Flange (Ft).....	10.23 [kips]
Lateral Support Reaction of the Bottom Flange (Fb).....	10.25 [kips]
Resulting Moment Acting on the Permanent Support (M).....	83.06 [kip-ft.]

ULTIMATE STRENGTH CHECK

Check for Ultimate Strength Using Eq. (10-155) AASHTO : $0.028 < 1$!

HMTB BRIDGE DESIGN PROGRAM BDSGS VERSION 2.9.1.0 OUTPUT File Name: M:\Jobs\A9633\Techprcd\Bridges\Bump As\Design\BDSGs\SteelBridg..._m_Mod_Final\CL Girder 5.0UT ...

A-DEAD LOADS MINOR LIVE LOADS INTEGRAL WEARING SURFACE FUTURE WEARING SURFACE FUTURE WEARING SURFACE FUTURE WEARING SURFACE ...

BDGS RUN FOR RAMP A5 COMPLETED ON 5/13/2011

SPAN,LOC TOP FLANGE BOT FLANGE ... SHEAR (kips) TOP REIN MOMENT (in-kips) ...

IMPACT INCLUDED STRESSES IN (ksi) ** LRFD STRESS SUMMARY (Based on Input Section) ...

SPAN,LOC TOP FLANGE BOT FLANGE ... SHEAR (kips) TOP REIN MOMENT (in-kips) ...

IMPACT INCLUDED STRESSES IN (ksi) ** LRFD STRESS SUMMARY (Based on Input Section) ...

SPAN,LOC TOP FLANGE BOT FLANGE ... SHEAR (kips) TOP REIN MOMENT (in-kips) ...

IMPACT INCLUDED STRESSES IN (ksi) ** LRFD STRESS SUMMARY (Based on Input Section) ...

SPAN,LOC TOP FLANGE BOT FLANGE ... SHEAR (kips) TOP REIN MOMENT (in-kips) ...

IMPACT INCLUDED STRESSES IN (ksi) ** LRFD STRESS SUMMARY (Based on Input Section) ...

HMTB BRIDGE DESIGN PROGRAM BDSGS VERSION 2.9.1.0 OUTPUT File Name: M:\Jobs\A9633\Techprcd\Bridges\Bump As\Design\BDSGs\SteelBridg..._m_Mod_Final\CL Girder 5.0UT ...

A-DEAD LOADS MINOR LIVE LOADS INTEGRAL WEARING SURFACE FUTURE WEARING SURFACE FUTURE WEARING SURFACE ...

SPAN,LOC TOP FLANGE BOT FLANGE ... SHEAR (kips) TOP REIN MOMENT (in-kips) ...

IMPACT INCLUDED STRESSES IN (ksi) ** LRFD STRESS SUMMARY (Based on Input Section) ...

SPAN,LOC TOP FLANGE BOT FLANGE ... SHEAR (kips) TOP REIN MOMENT (in-kips) ...

IMPACT INCLUDED STRESSES IN (ksi) ** LRFD STRESS SUMMARY (Based on Input Section) ...

SPAN,LOC TOP FLANGE BOT FLANGE ... SHEAR (kips) TOP REIN MOMENT (in-kips) ...

IMPACT INCLUDED STRESSES IN (ksi) ** LRFD STRESS SUMMARY (Based on Input Section) ...

SPAN,LOC TOP FLANGE BOT FLANGE ... SHEAR (kips) TOP REIN MOMENT (in-kips) ...

IMPACT INCLUDED STRESSES IN (ksi) ** LRFD STRESS SUMMARY (Based on Input Section) ...

HNTB BRIDGE DESIGN PROGRAM BDS
VERSION 2.9.1.0 CURTUP
RUN TIME: 05/13/2011 17:46:26.149
Filename: M:\Jobs\49633\Techpro\Bridges\SteelDen_Run_Mod_Final\CL Girder 5.OUT

Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

*** LRFD STRESS SUMMARY (Based on Input Section) ***

Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

*** LRFD STRESS SUMMARY (Based on Input Section) ***

Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

*** LRFD STRESS SUMMARY (Based on Input Section) ***

Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

*** LRFD STRESS SUMMARY (Based on Input Section) ***

Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

HNTB BRIDGE DESIGN PROGRAM BDS
VERSION 2.9.1.0 CURTUP
RUN TIME: 05/13/2011 17:46:26.149
Filename: M:\Jobs\49633\Techpro\Bridges\SteelDen_Run_Mod_Final\CL Girder 5.OUT

Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

*** LRFD STRESS SUMMARY (Based on Input Section) ***

Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

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Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

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*** LRFD STRESS SUMMARY (Based on Input Section) ***

Table with columns: SPAN, LOC, TOP FLANGE, BOT FLANGE, TOP REIN, MOMENT, SHEAR, IMPACT INCLUDED, STRESS IN (ksi)

VERSION 2.9.1.0

HNTB BRIDGE DESIGN PROGRAM BDGS
 RUN TIME: 05/13/2011 17:46:26.149
 Filename: M:\Jobs\496313\Techprod\Bridges\Hamp A3\Design\BDGS\SteelDen_Run_Modal_VCL Girder 5.OUT

*** LRFD STRESS SUMMARY (Based on Input Section) ***
 STRESSES IN (ksi)

SPAN, LOC	TOP FLANGE	BOT FLANGE	IMPACT INCLUDED	TOP REINF	MOMENT (in-kips)	SHEAR (kips)
4.724	31.80226371	-24.38122640	0.00000000	0.00000000	125216.82483569	-75.66088712
4.750	30.24107895	-23.22267562	0.00000000	0.00000000	119466.75294371	-91.16921517
4.750	30.24107895	-23.22267562	0.00000000	0.00000000	119466.75294371	-91.16921517
4.773	28.71007730	-22.01059966	0.00000000	0.00000000	113041.78705255	-106.44731709
4.773	28.71007730	-22.01059966	0.00000000	0.00000000	113041.78705255	-106.44731709
4.781	30.24330356	-24.04731432	0.00000000	0.00000000	110687.15540706	-111.88231870
4.781	30.24330356	-24.04731432	0.00000000	0.00000000	110687.15540706	-111.88231870
4.800	28.57614223	-22.70671613	0.00000000	0.00000000	104516.20341070	-124.16251406
4.800	28.57614223	-22.70671613	0.00000000	0.00000000	104516.20341070	-124.16251406
4.822	26.37323140	-20.95627447	0.00000000	0.00000000	96459.13569858	-140.92870967
4.822	26.37323140	-20.95627447	0.00000000	0.00000000	96459.13569858	-140.92870967
4.850	23.27218371	-18.49216966	0.00000000	0.00000000	85117.24105722	-158.96755709
4.850	23.27218371	-18.49216966	0.00000000	0.00000000	85117.24105722	-158.96755709
4.850	23.27218371	-18.49216966	0.00000000	0.00000000	85117.24105722	-158.96755709
4.900	16.70989429	-13.27774653	0.00000000	0.00000000	6116.49709854	-193.12043972
4.900	16.70989429	-13.27774653	0.00000000	0.00000000	6116.49709854	-193.12043972
4.921	13.28067599	-10.63412451	0.00000000	0.00000000	61115.82264856	-191.62042979
4.921	13.28067599	-10.63412451	0.00000000	0.00000000	61115.82264856	-191.62042979
4.950	8.76106870	-7.01516919	0.00000000	0.00000000	49634.30164278	-204.16199600
4.950	8.76106870	-7.01516919	0.00000000	0.00000000	49634.30164278	-204.16199600
4.950	8.76106870	-7.01516919	0.00000000	0.00000000	49634.30164278	-204.16199600
4.960	7.11528074	-5.69736719	0.00000000	0.00000000	32742.99218606	-223.02191791
4.960	7.11528074	-5.69736719	0.00000000	0.00000000	32742.99218606	-223.02191791
4.961	7.00874191	-5.61205124	0.00000000	0.00000000	2743.02622148	-223.02191791
4.965	6.24823192	-5.00109604	0.00000000	0.00000000	2582.2011532	-229.50497544
4.965	6.24823192	-5.00109604	0.00000000	0.00000000	2582.2011532	-229.50497544
4.979	3.90471494	-3.12658970	0.00000000	0.00000000	26193.99872660	-229.91330140
4.979	3.90471494	-3.12658970	0.00000000	0.00000000	26193.99872660	-229.91330140
4.982	1.45856010	-1.15798032	0.00000000	0.00000000	23351.72751625	-232.84790224
4.982	1.45856010	-1.15798032	0.00000000	0.00000000	23351.72751625	-232.84790224
4.992	1.45855239	-1.16789445	0.00000000	0.00000000	14593.21791488	-241.65200036
4.992	1.45855239	-1.16789445	0.00000000	0.00000000	14593.21791488	-241.65200036
5.000	0.00000000	0.00000000	0.00000000	0.00000000	5451.0921658	-250.51184047
5.000	0.00000000	0.00000000	0.00000000	0.00000000	5451.0921658	-250.51184047
5.000	0.00000000	0.00000000	0.00000000	0.00000000	-0.00000169	-255.52188502
5.000	0.00000000	0.00000000	0.00000000	0.00000000	-27.19033419	-255.54599838

← Point 11

*** LRFD STRESS SUMMARY (Based on Input Section) ***
 STRESSES IN (ksi)

SPAN, LOC	TOP FLANGE	BOT FLANGE	IMPACT INCLUDED	TOP REINF	MOMENT (in-kips)	SHEAR (kips)
5.000	-0.00352900	0.00286598	0.00000000	0.00000000	-13.71437278	2.02658831
5.191	-0.00217766	0.00176853	0.00000000	0.00000000	-8.46281330	1.49507678
6.000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000

Table with columns: SPAN, I, TOP FLANGE, BOT FLANGE, TOP REINF, MOMENT, SHEAR, etc. Includes sub-sections for SPAN 1.000, SPAN 1.000, SPAN 1.000, and SPAN 1.000.

HMB BRIDGE DESIGN PROGRAM BDSG VERSION 2.9.1.0 CUTPUT

Run Time: 05/13/2011 17:46:26.149

Filename: M:\Jobs\A9633\Techprod\Bridges\A5\Design\BDSG\SteelBridg..._MOD_Final\CL Girder 1.0UT

Table with columns: SPAN, I, TOP FLANGE, BOT FLANGE, TOP REINF, MOMENT, SHEAR, etc. Includes sub-sections for SPAN 1.000, SPAN 1.000, SPAN 1.000, and SPAN 1.000.

HMB BRIDGE DESIGN PROGRAM BDSG VERSION 2.9.1.0 CUTPUT

Run Time: 05/13/2011 17:46:26.149

Filename: M:\Jobs\A9633\Techprod\Bridges\A5\Design\BDSG\SteelBridg..._MOD_Final\CL Girder 1.0UT

Table with columns: SPAN, I, TOP FLANGE, BOT FLANGE, TOP REINF, MOMENT, SHEAR, etc. Includes sub-sections for SPAN 1.000, SPAN 1.000, SPAN 1.000, and SPAN 1.000.

HMTB BRIDGE DESIGN PROGRAM BUGS
VERSION 2.9.1.0
RUN TIME: 05/13/2011 17:46:26.149
File name: M:\Jobs\4963\Techproj\Bridges\Steel\Mod Final\CL Girder 1.0UT

Table with 10 columns: SPAN, I/O, TOP FLANGE, BOT FLANGE, TOP REINF, BOT REINF, MOMENT (in-kips), SHEAR (kips), TOP OF SLAB, IMPACT INCLUDED, STRESSES IN (ksi). Contains stress data for span 3.000.

HMTB BRIDGE DESIGN PROGRAM BUGS
VERSION 2.9.1.0
RUN TIME: 05/13/2011 17:46:26.149
File name: M:\Jobs\4963\Techproj\Bridges\Steel\Mod Final\CL Girder 1.0UT

Table with 10 columns: SPAN, I/O, TOP FLANGE, BOT FLANGE, TOP REINF, BOT REINF, MOMENT (in-kips), SHEAR (kips), TOP OF SLAB, IMPACT INCLUDED, STRESSES IN (ksi). Contains stress data for span 3.000.

HMTB BRIDGE DESIGN PROGRAM BUGS
VERSION 2.9.1.0
RUN TIME: 05/13/2011 17:46:26.149
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Table with 10 columns: SPAN, I/O, TOP FLANGE, BOT FLANGE, TOP REINF, BOT REINF, MOMENT (in-kips), SHEAR (kips), TOP OF SLAB, IMPACT INCLUDED, STRESSES IN (ksi). Contains stress data for span 3.000.

HMTB BRIDGE DESIGN PROGRAM BUGS
VERSION 2.9.1.0
RUN TIME: 05/13/2011 17:46:26.149
File name: M:\Jobs\4963\Techproj\Bridges\Steel\Mod Final\CL Girder 1.0UT

Table with 10 columns: SPAN, I/O, TOP FLANGE, BOT FLANGE, TOP REINF, BOT REINF, MOMENT (in-kips), SHEAR (kips), TOP OF SLAB, IMPACT INCLUDED, STRESSES IN (ksi). Contains stress data for span 3.000.

HMTB BRIDGE DESIGN PROGRAM BUGS
VERSION 2.9.1.0
RUN TIME: 05/13/2011 17:46:26.149
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Table with 10 columns: SPAN, I/O, TOP FLANGE, BOT FLANGE, TOP REINF, BOT REINF, MOMENT (in-kips), SHEAR (kips), TOP OF SLAB, IMPACT INCLUDED, STRESSES IN (ksi). Contains stress data for span 3.000.

HMTB BRIDGE DESIGN PROGRAM BUGS
VERSION 2.9.1.0
RUN TIME: 05/13/2011 17:46:26.149
File name: M:\Jobs\4963\Techproj\Bridges\Steel\Mod Final\CL Girder 1.0UT

Table with 10 columns: SPAN, I/O, TOP FLANGE, BOT FLANGE, TOP REINF, BOT REINF, MOMENT (in-kips), SHEAR (kips), TOP OF SLAB, IMPACT INCLUDED, STRESSES IN (ksi). Contains stress data for span 3.000.

4.500 31.25952590 -24.25055402 0.00000000 0.00000000 158871.54724105 96.53139505
 4.500 31.25935749 -24.25042371 0.00000000 0.00000000 158870.69355351 96.53139505
 HWPB BRIDGE DESIGN PROGRAM BDCS
 VERSION 2.9.1.0 OUTPUT
 RUN TIME: 05/13/2011 17:46:26.149
 Filename: M:\jobs\49633\Techprod\Bridges\AmpAS\Design\BDCS\Steel\MOD_Final\GL Girder 1.OUT
 *** LRFD STRESS SUMMARY (Based on Input Section) ***
 STRESSES IN (ksi)

SPAN, LOC	TOP FLANGE	BOT FLANGE	IMPACT INCLUDED	TOP REINF	MOMENT (in-klips)	TOP REINF	MOMENT (in-klips)	SHEAR (klips)
4.548	33.28487687	-25.82179394	0.00000000	0.00000000	169165.07151521	0.00000000	0.00000000	44.40143131
4.550	33.32055987	-25.84945694	0.00000000	0.00000000	169346.42465521	0.00000000	0.00000000	43.34849398
4.550	33.32057359	-25.84947649	0.00000000	0.00000000	169346.42465521	0.00000000	0.00000000	43.34849398
4.600	34.01023850	-26.38450559	0.00000000	0.00000000	172851.60617010	0.00000000	0.00000000	9.64895810
4.600	34.01024094	-26.38487987	0.00000000	0.00000000	172854.05811406	0.00000000	0.00000000	9.58400618
4.600	33.70459456	-26.41220626	0.00000000	0.00000000	173933.07960857	0.00000000	0.00000000	0.00000000
4.614	33.82013584	-26.23370752	0.00000000	0.00000000	171885.43977901	0.00000000	0.00000000	-24.18048168
4.650	33.81991886	-26.23685919	0.00000000	0.00000000	171884.33701547	0.00000000	0.00000000	-24.18048168
4.651	33.80237099	-26.22324292	0.00000000	0.00000000	171795.13430065	0.00000000	0.00000000	-44.98399335
4.700	32.24730999	-25.01485902	0.00000000	0.00000000	163978.69481005	0.00000000	0.00000000	-77.82344578
4.700	32.24731207	-25.01485902	0.00000000	0.00000000	163978.69481005	0.00000000	0.00000000	-77.82344578
4.703	32.12818207	-24.92441156	0.00000000	0.00000000	163286.35225849	0.00000000	0.00000000	-79.73146144
4.750	29.77452596	-23.09851693	0.00000000	0.00000000	151324.25555564	0.00000000	0.00000000	-111.58993375
4.750	29.77424951	-23.09830479	0.00000000	0.00000000	151322.86979851	0.00000000	0.00000000	-111.58993375
4.754	29.52113378	-22.90194231	0.00000000	0.00000000	150036.44865126	0.00000000	0.00000000	-135.09178725
4.774	28.09287606	-21.79190971	0.00000000	0.00000000	142764.34272127	0.00000000	0.00000000	-148.16224497
4.774	28.09287606	-21.79190971	0.00000000	0.00000000	142764.34272127	0.00000000	0.00000000	-148.16224497
4.800	25.9377436	-20.11816091	0.00000000	0.00000000	131799.18742104	0.00000000	0.00000000	-165.94727744
4.800	25.93772332	-20.11812073	0.00000000	0.00000000	131798.92545894	0.00000000	0.00000000	-165.94727744
4.806	25.42852420	-19.72697250	0.00000000	0.00000000	129236.41139593	0.00000000	0.00000000	-169.83425977
4.850	21.16444964	-16.41898338	0.00000000	0.00000000	107564.93888850	0.00000000	0.00000000	-199.7176557
4.850	21.16423659	-16.41891906	0.00000000	0.00000000	107563.85283270	0.00000000	0.00000000	-199.7176557
4.900	15.09275498	-11.70867629	0.00000000	0.00000000	76706.51618806	0.00000000	0.00000000	-252.42328125
4.900	15.09275143	-11.70867369	0.00000000	0.00000000	76706.49915749	0.00000000	0.00000000	-252.42328125
4.909	13.93632167	-10.81153716	0.00000000	0.00000000	70829.12956244	0.00000000	0.00000000	-258.28623286
4.950	8.06930660	-6.26001682	0.00000000	0.00000000	41010.96228310	0.00000000	0.00000000	-286.18776954
4.950	8.06222770	-6.25995561	0.00000000	0.00000000	41010.56227953	0.00000000	0.00000000	-286.18776954
4.980	5.22608116	-3.53391918	0.00000000	0.00000000	17012.13331207	0.00000000	0.00000000	-313.58835597
5.000	0.01732224	-0.01360572	0.00000000	0.00000000	91.34556481	0.00000000	0.00000000	-327.04513401

← Pict 11

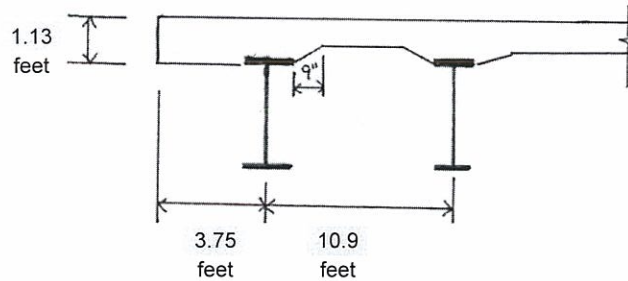
*** LRFD STRESS SUMMARY (Based on Input Section) ***
 STRESSES IN (ksi)

SPAN, LOC	TOP FLANGE	BOT FLANGE	IMPACT INCLUDED	TOP REINF	MOMENT (in-klips)	TOP REINF	MOMENT (in-klips)	SHEAR (klips)
5.000	-0.00317130	0.00249642	0.00000000	0.00000000	-16.63236687	0.00000000	0.00000000	2.50156264
5.100	-0.00247931	0.00195169	0.00000000	0.00000000	-13.15945428	0.00000000	0.00000000	2.14833347
5.100	-0.00247931	0.00195169	0.00000000	0.00000000	-13.15945428	0.00000000	0.00000000	2.14833347
5.191	-0.00194536	0.00153137	0.00000000	0.00000000	-10.32339304	0.00000000	0.00000000	1.84620005
6.000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000	0.00000000

Global Superstructure Distortion (ϕ_g)

Girder twist due to superstructure deformation can be neglected when the tributary deck load carrier by the fascia girder does not exceed 110% carried by the interior member.

Span 1 Right Overhang G1 & G2



- Slab thickness = 9.25 inches
- G1 Top Flange W = 20 inches
- G1 Top Flange t = 0.88 inches
- G2 Top Flange W = 20 inches
- G2 Top Flange t = 0.88 inches
- Top of deck to top of Web = 14 inches

Interior

- Slab = 1262 #/ft
- Haunch = 80.7 #/ft
- 9" wedge = 44.5 #/ft
- SIP (16psf) = 148 #/ft
- Total = 1536 #/ft

Exterior

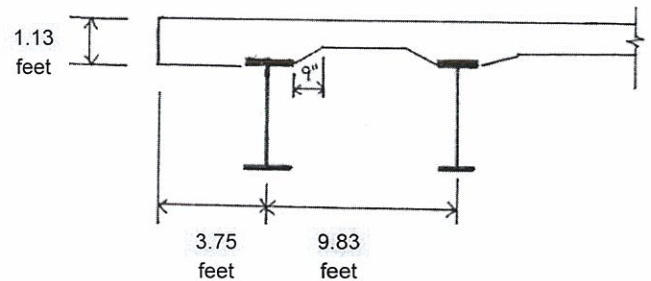
- Half Interior = 768 #/ft
- Overhang = 492 #/ft
- Conc. on Flange = 137 #/ft
- Total = 1397 #/ft

Ratio Exterior to Interior = 0.91 < 1.1

OK - Neglect Distortion

DONE PREVIOUSLY, NOTHING ON THIS WORKSHEET WILL CHANGE. LEAVE AS IS
 LJD 3/30/12
 EDG 4-2-12
 LJD 4/3/12

Span 1 Leftt Overhang G5 & G4



- Slab thickness = 9.25 inches
- G5 Top Flange W = 28 inches
- G5 Top Flange t = 1.63 inches
- G4 Top Flange W = 20 inches
- G4 Top Flange t = 1.38 inches
- Top of deck to top of Web = 14 inches

Interior

- Slab = 1137 #/ft
- Haunch = 70.3 #/ft
- 9" wedge = 44.5 #/ft
- SIP (16psf) = 131 #/ft
- Total = 1382 #/ft

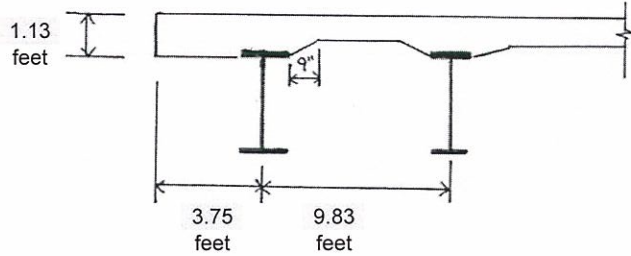
Exterior

- Half Interior = 691 #/ft
- Overhang = 436 #/ft
- Conc. on Flange = 180 #/ft
- Total = 1308 #/ft

Ratio Exterior to Interior = 0.95 < 1.1

OK - Neglect Distortion

Span 4 Right Overhang G1 & G3



Slab thickness = 9.25 inches
 G1 Top Flange W = 28 inches
 G1 Top Flange t = 1.5 inches
 G3 Top Flange W = 22 inches
 G3 Top Flange t = 1 inches
 Top of deck to top of Web = 14 inches

Interior

Slab = 1137 #/ft
 Haunch = 85.9 #/ft
 9" wedge = 44.5 #/ft
 SIP (16psf) = 128 #/ft
Total = 1395 #/ft

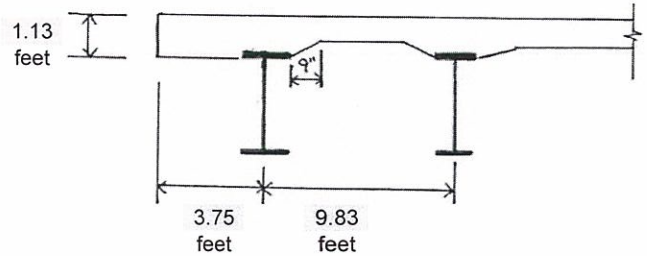
Exterior

Half Interior = 698 #/ft
 Overhang = 436 #/ft
 Conc. on Flange = 182 #/ft
Total = 1316 #/ft

Ratio Exterior to Interior = 0.94 < 1.1

OK - Neglect Distortion

Span 5 Leftt Overhang G5 & G4



Slab thickness = 9.25 inches
 G5 Top Flange W = 24 inches
 G5 Top Flange t = 1.25 inches
 G4 Top Flange W = 22 inches
 G4 Top Flange t = 1 inches
 Top of deck to top of Web = 14 inches

Interior

Slab = 1137 #/ft
 Haunch = 85.9 #/ft
 9" wedge = 44.5 #/ft
 SIP (16psf) = 128 #/ft
Total = 1395 #/ft

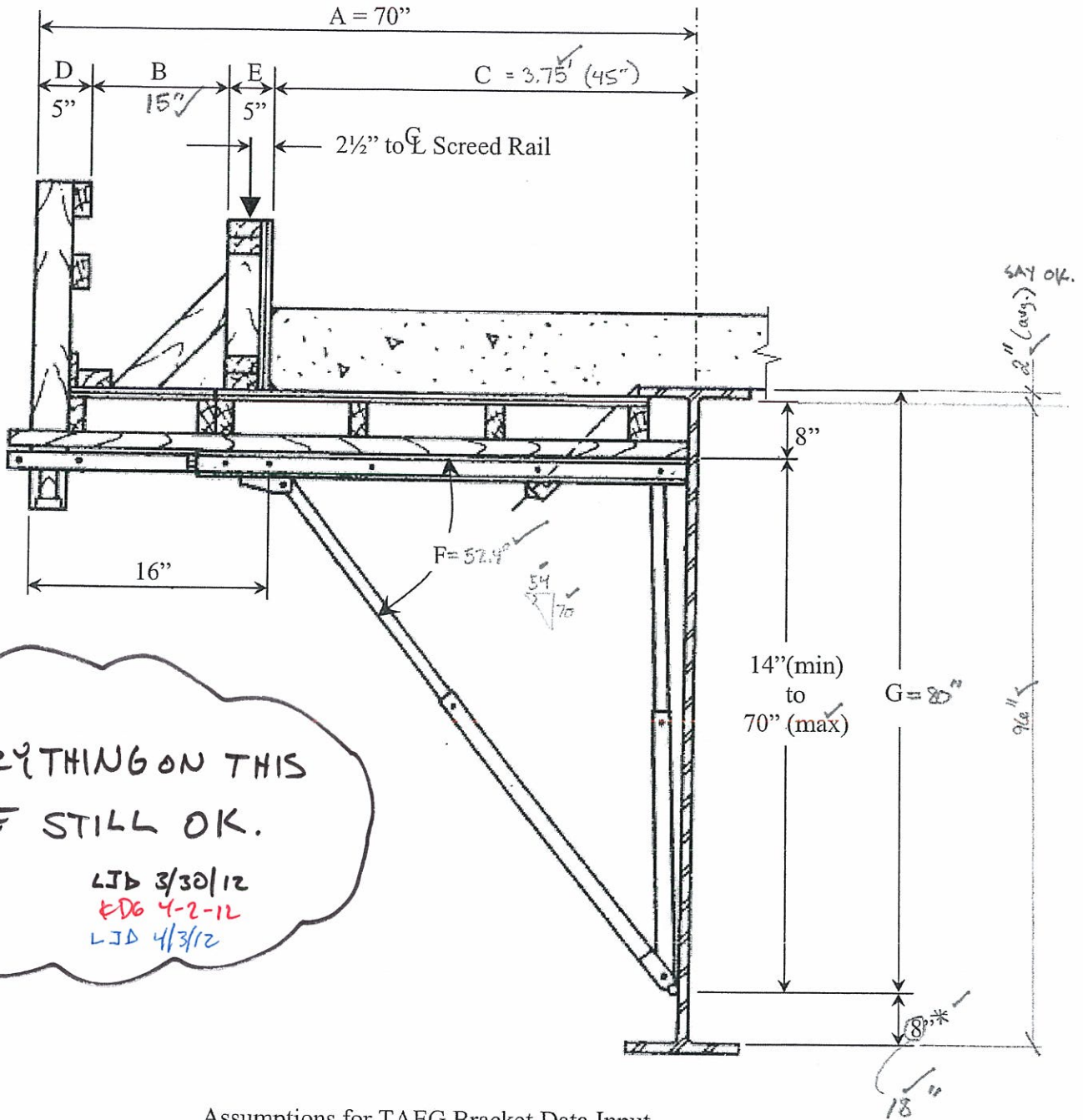
Exterior

Half Interior = 698 #/ft
 Overhang = 464 #/ft
 Conc. on Flange = 159 #/ft
Total = 1321 #/ft

Ratio Exterior to Interior = 0.95 < 1.1

OK - Neglect Distortion

CHK: DHE 02/18/2011
 BV: LER 3/8/11



Assumptions for TAEG Bracket Data Input

*Per CMS 508, bracket lower contact point must be within 8" of bottom of web. Since web depth > 86" this requirement cannot be met due to max. bracket height of 70". Provide note on plans removing requirement of CMS 508 such that the bracket location will be 3-79.9" per plan. (See BDM Sec. 300)

C. Permanent Lateral Support Data: *< Use X-Frame w/ Strut Top & Foot >*

The default crossframe type assumed by the TAEG software consists of a stiffener and diagonal x-bracing with top and bottom horizontal chords. In order to analyze the structure with a standard ODOT crossframe, designers should input stiffener dimensions and select the "Diaphragms (Inputted Ix)" option. For ODOT Type 1 crossframes, designers should assume a fictitious stiffener of dimensions: 5" x 3/8". Determine the diaphragm moment of inertia for all standard ODOT crossframes as follows:

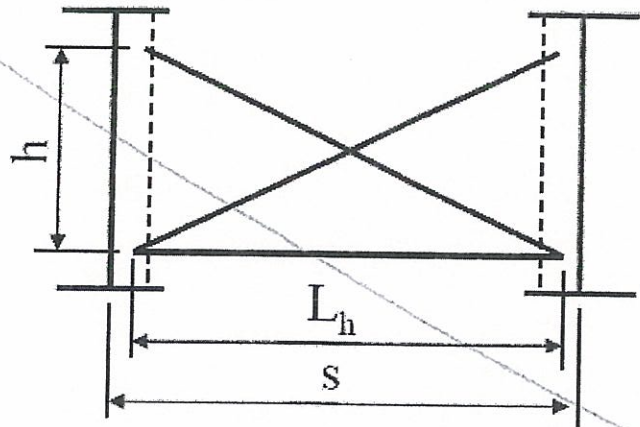
$$I_x = \frac{h^2 s}{4L_d^3 \left(\frac{1}{A_d L_h^2} + \frac{L_h}{A_h L_d^3 + A_d L_h^3} \right)}$$

Where:

A_d = Area of the diagonal member (in²)

A_h = Area of the horizontal member (in²)

$L_d = \sqrt{L_h^2 + h^2}$



D. Temporary Lateral Support Data: *< None >*

Designers should generally avoid utilizing temporary tie rods and timber blocks; however, if required these should be detailed in the contract plans.

E. Load Data:

1. Live Load on Walkway.....50 lb/ft²
2. Live Load on Slab.....50 lb/ft²
3. Dead Load of Formwork.....10 lb/ft²
4. Dead Load of Concrete 150(t_{avg}) lb/ft² = 175
 (t_{avg} = Average thickness [ft.] of deck slab overhang) *$t_{OH} = 1\frac{1}{4}$*
5. Wheel Spacing [1-2-3]..... *36" - 31" - 36"*
6. Maximum Wheel Load: *(See Calc on next sheet)*..... *48" - 40" - 48"*

To estimate the total finishing machine length required for placement along the skew, add the rail-to-rail length and the extra end length from the following table using the plan specified skew rounded to the nearest 5 degrees. W is the rail-to-rail length as measured perpendicular to the centerline of the bridge.

WHEEL SPACING
 CHANGED.

 LJD 3/30/12
 DDG 4-2-11
 LJD 4/3/11

CHK: DHE 02/18/2011
 B V: LER 3/18/11

Skew Angle	Rail-to-Rail Length, ft.	Extra End Length, ft.
0	1.00 W	0.0
15	1.04 W	5.0
20	1.06 W	5.5
25	1.10 W	6.5
30	1.15 W	7.0
35	1.22 W	8.0
40	1.31 W	9.0
45	1.41 W	10.5
50	1.56 W	11.5
55	1.74 W	13.5

For total machine lengths of 36 ft. and less, assume a total machine weight of 7.6 kip. Add 0.09 kip for each additional foot of machine length required above 36 ft. The maximum total machine length shall not exceed 120 ft. If greater lengths are required, consult the Office of Structural Engineering for recommendations.

To determine the maximum wheel load, divide the total machine weight by 8.0.

F. Bracket Data:

1. Refer to the following figure to determine TAEG dimensions A, B, C, D, E, F and G.
2. Designers may assume a center-to-center bracket spacing of 48.0 in.
3. Designers may assume a bracket weight of 50 lbs.

Max. Wheel Load

Case 1: Deck width = 49' ✓
 $W = 49 - 5'' \rightarrow$ assume 25° skew ∴ add 6.5' + 1.10 (49.4167) = 60.9' ✓
 $F_m = 7.6 \text{ k} + 0.09 (60.9 - 36)$
 $= 9.8 \text{ k} ✓$
 $F_w = 9.8 / 8 = 1.23 \text{ k/wheel} \Rightarrow$ Say 1.25 k ✓

Case 2: Deck width = 37' ✓
 $W = 37 - 5'' \rightarrow$ assume 20° skew ∴ add 5.5' + 1.06 (37.4167) = 45.8' ✓
 $F_m = 7.6 \text{ k} + 0.09 (45.8 - 36)$
 $= 8.4 \text{ k} ✓$
 $F_w = 8.4 / 8 = 1.1 \text{ k/wheel} ✓$

LTD 3/30/12
 CDB 4-2-12
 LJD 4/3/12

WHEEL LOAD NOW
2.25 k PER WALSH
RFI #00287.



The Walsh Group National Heavy / Civil

Project CLEVELAND INNERBELT BRIDGE

Date 4-8-2011

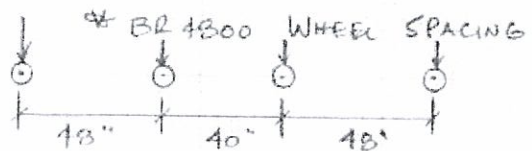
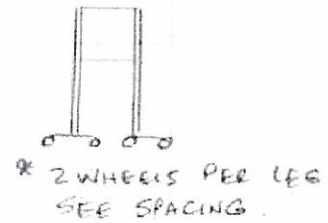
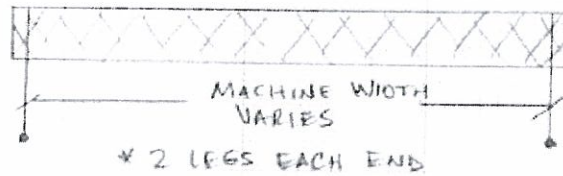
Name J. HALTERMAN

Subject BRIDGE MACHINE LOADS

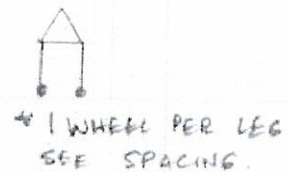
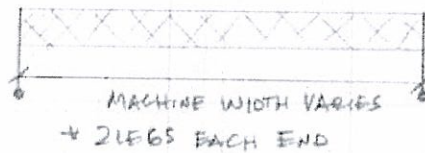
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Scale N/A

BIDWELL 4800 :



RAZORBACK 12 HED :



* 12 HED WHEEL SPACING

