



**FORM DQP 2.01-1
LEVEL 1 CHECK PRINT SIGN-OFF SHEET**

Client Name: Ohio Department of Transportation
 Job Title: Cleveland Innerbelt Design-Build Contract
 Job Number: CUY-90-14.90
 Document Title: RFI 167 Unit 1 End Diaphragm Oversized Holes

Check Level (Mark One): 1A 100% Document Check
 1B 100% Input Check

Enter description below:

	Print Name	Signature	Date
<input checked="" type="checkbox"/> Originator	<u>Kolbe Gravatt</u>	<u>[Signature]</u>	<u>Dec. 14, 2011</u>
<input checked="" type="checkbox"/> Checker	<u>Larry Rolwes</u>	<u>[Signature]</u>	<u>12/15/11</u>
<input checked="" type="checkbox"/> Backchecker	<u>Kolbe Gravatt</u>	<u>[Signature]</u>	<u>12-15-11</u>
<input checked="" type="checkbox"/> Updater	<u>Kolbe Gravatt</u>	<u>[Signature]</u>	<u>12-15-11</u>
<input checked="" type="checkbox"/> Validater	<u>Larry Rolwes</u>	<u>[Signature]</u>	<u>12/16/11</u>

Insert an "X" in the box to indicate a required QC activity.

For **Cleveland Innerbelt**

RFI 00167

The RFI requests the use of oversized holes for all of the connections of the Unit 1, Girder 4 and Girder 5 End Diaphragms. *(and Girder 6)*

From BDGS at the ends of Girders 4 and 5 connected to the end diaphragm

Girder 4

	V (k)	M (k*ft)
DC	173.9 ✓	2 ✓
DW	61.6 ✓	5 ✓
LL truck	72.2 ✓	9 ✓
LL lane	42.6 ✓	7 ✓

Importance Factor = 1.05

Service 2

$$V_u = 1.05 * [1.0 * (173.9 + 61.6) + 1.3 * (1.33 * (72.2) + 42.6)]$$

$$V_u = 436 \text{ kips}$$

$$M_u = 1.05 * [1.0 * (2 + 5) + 1.3 * (1.33 * (9) + 7)]$$

$$M_u = 33.2 \text{ k*ft}$$

Girder 5

	V (k)	M (k*ft)
DC	437.8 ✓	1 ✓
DW	140.3 ✓	2 ✓
LL truck	37.5 ✓	1 ✓
LL lane	68.1 ✓	2 ✓

Importance Factor = 1.05

Service 2

$$V_u = 1.05 * [1.0 * (437.8 + 140.3) + 1.3 * (1.33 * (37.5) + 68.1)]$$

$$V_u = 768 \text{ kips}$$

$$M_u = 1.05 * [1.0 * (1 + 2) + 1.3 * (1.33 * (1) + 2)]$$

$$M_u = 7.7 \text{ k*ft}$$

Girder 5 Shear Controls

and Girder 4 Moment Controls

S_{min} = 3.5" 3.25" ✓

S_{edge} = 2.0" ✓

S_{max} = (4 + 4t) $\frac{309}{40} < 7.0$
= 4 + 4(0.75) = 7" ✓ OK

V_u = 307 k ✓
*M_u = 37.5 k*ft ✓*

Girder 6

	V(k)	M(k*ft)
DC	86.4 ✓	2 ✓
DW	35.7 ✓	6 ✓
LLT	69.2 ✓	10 ✓
LL L	38.9 ✓	8 ✓

RFI 00167 (Cont.)

These calculations are to revise the Bolt slip Resistance to include oversized holes

All other checks from the original design are still valid.

At the End of the Stub Girder

$$R_n = K_h \cdot K_s \cdot N_s \cdot P_t \quad (6.13.2.8-1)$$

$$R_n = (0.85)(0.33)(2)(51) = 28.61 \text{ k/bolt}$$

$$P_t = 51 \text{ k (1" bolt table 6.13.2.8-1)}$$

$$\phi_s = 0.80 \rightarrow 1.0$$

There are 50 bolts in the end of the Stub Girder

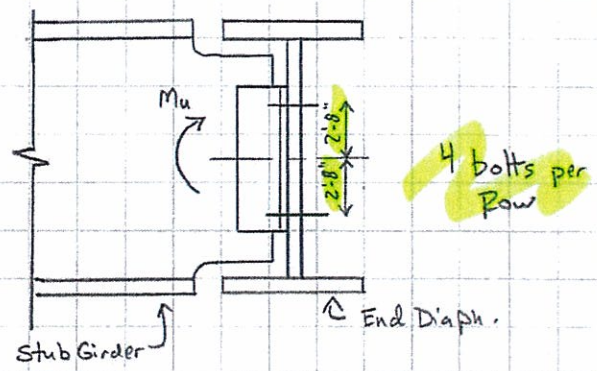
$$\phi R_n = 0.80(28.61)(50) = 1144 \text{ k}$$

$$1430.5 - 1144 > 286.5$$

∴ Oversized holes are OK

Connection to End Diaphragm Web - 4

Find Axial Tension in Bolts



$$M_u = 33.2 \text{ k-ft} \rightarrow 37.5 \text{ or } 33.2 \text{ k-ft}$$

$$T_u = 33.2 \text{ k-ft} \div 2.66 \text{ ft} \div 4 \text{ bolts} = 3.11 \text{ k/bolt}$$

Reduction in Slip Resistance for Combine Shear and Axial

$$1 - \frac{1.70(3.11)}{51} = 0.94 \rightarrow 0.97 \quad (6.13.2.11-3)$$

$$R_n = 0.97(K_h \cdot K_s \cdot N_s \cdot P_t) = 13.88 \text{ k/bolt}$$

$$R_n = 0.97(0.85)(0.33)(1)(51) = 13.45 \text{ k/bolt}$$

There are 68 bolts connecting to the web of the end Diaphragm

$$\phi R_n = 0.80(13.88)(68) = 944 \text{ k}$$

$$944 - 436 = 508 \text{ k} \rightarrow \text{Conservative } \therefore \text{all checks should be OK}$$

∴ oversized holes are OK for Connection to End Diaphragm web on Girder + End Diaphragm

RFI 00167 (cont.)

Connection to End Diaph. Web - G5

$$M_u = 7.7 \text{ k-ft}$$

$$T_u = 7.7 \div 2.667 \div 4 = 0.72 \text{ k/bolt}$$

Reduction Factor

$$1 - \frac{0.72}{51} = 0.99$$

$$R_n = 0.99 (0.85) (0.33) (1) (51) = 14.16 \text{ k/bolt}$$

$$\phi R_n = 0.80 (14.16) (68 \text{ bolts}) = 770 \text{ k}$$

$$\frac{963}{770} > 768$$

∴ Oversized holes are OK
for connection to End Diaph.
web on Girder 5 End Diaph.

Check on previous page
covers All Girders this is
no longer needed

Connection of End Diaphragm
to Adjacent Girder Stiffener

Oversized holes were included
in the Original Design
No additional calculations need
to be provided.

BDGS Output – Unit 1 G4

----- CAMBER DATA -----

*** GIRDER 11 DEAD LOAD CAMBER VALUES: (Positive Values Upward) ***

Note: Displacements due to removable forms are not included.

SPAN, LOC FRAC	A-DC DEAD LOAD					B-DC DEAD LOAD			DW DEAD LOAD		
	STEEL GIRDER (in)	USER STEEL (in)	CONCRETE SLAB (in)	USER CONC (in)	USER ADD. (in)	BARR (in)	SDWALK (in)	USER ADD. (in)	INTEGRAL WEARING SURFACE (in)	FUTURE WEARING SURFACE (in)	UTILS (in)
1.031	0.106	0.000	0.214	0.001	0.000	0.011	0.000	0.000	0.000	0.066	0.000
1.050	0.169	0.000	0.343	0.001	0.000	0.017	0.000	0.000	0.000	0.105	0.000
1.052	0.176	0.000	0.358	0.001	0.000	0.018	0.000	0.000	0.000	0.110	0.000
1.100	0.336	0.000	0.681	0.002	0.000	0.034	0.000	0.000	0.000	0.210	0.000
1.104	0.350	0.000	0.710	0.002	0.000	0.035	0.000	0.000	0.000	0.218	0.000
1.150	0.497	0.000	1.008	0.003	0.000	0.050	0.000	0.000	0.000	0.311	0.000
1.200	0.653	0.000	1.322	0.004	0.000	0.066	0.000	0.000	0.000	0.408	0.000
1.216	0.701	0.000	1.420	0.004	0.000	0.071	0.000	0.000	0.000	0.439	0.000
1.250	0.799	0.000	1.617	0.005	0.000	0.080	0.000	0.000	0.000	0.501	0.000
1.300	0.936	0.000	1.891	0.005	0.000	0.094	0.000	0.000	0.000	0.587	0.000
1.328	1.008	0.000	2.036	0.006	0.000	0.101	0.000	0.000	0.000	0.633	0.000
1.350	1.061	0.000	2.141	0.006	0.000	0.107	0.000	0.000	0.000	0.666	0.000
1.400	1.172	0.000	2.363	0.007	0.000	0.118	0.000	0.000	0.000	0.738	0.000
1.440	1.253	0.000	2.522	0.007	0.000	0.126	0.000	0.000	0.000	0.790	0.000
1.445	1.262	0.000	2.541	0.007	0.000	0.127	0.000	0.000	0.000	0.796	0.000
1.450	1.271	0.000	2.558	0.007	0.000	0.127	0.000	0.000	0.000	0.801	0.000
1.500	1.355	0.000	2.724	0.008	0.000	0.136	0.000	0.000	0.000	0.856	0.000
1.550	1.427	0.000	2.865	0.008	0.000	0.143	0.000	0.000	0.000	0.902	0.000
1.552	1.430	0.000	2.870	0.008	0.000	0.143	0.000	0.000	0.000	0.904	0.000
1.567	1.448	0.000	2.905	0.009	0.000	0.145	0.000	0.000	0.000	0.916	0.000
1.595	1.479	0.000	2.966	0.009	0.000	0.148	0.000	0.000	0.000	0.936	0.000
1.597	1.482	0.000	2.970	0.009	0.000	0.148	0.000	0.000	0.000	0.938	0.000
1.600	1.484	0.000	2.975	0.009	0.000	0.148	0.000	0.000	0.000	0.940	0.000
1.600	1.485	0.000	2.976	0.009	0.000	0.148	0.000	0.000	0.000	0.940	0.000
1.601	1.485	0.000	2.977	0.009	0.000	0.148	0.000	0.000	0.000	0.940	0.000
1.650	1.529	0.000	3.060	0.009	0.000	0.152	0.000	0.000	0.000	0.969	0.000
1.664	1.539	0.000	3.079	0.009	0.000	0.153	0.000	0.000	0.000	0.976	0.000
1.700	1.560	0.000	3.118	0.009	0.000	0.155	0.000	0.000	0.000	0.989	0.000
1.750	1.578	0.000	3.151	0.010	0.000	0.156	0.000	0.000	0.000	1.001	0.000
1.776	1.583	0.000	3.159	0.010	0.000	0.156	0.000	0.000	0.000	1.004	0.000
1.800	1.583	0.000	3.158	0.010	0.000	0.156	0.000	0.000	0.000	1.005	0.000
1.850	1.576	0.000	3.141	0.010	0.000	0.155	0.000	0.000	0.000	1.001	0.000
1.900	1.561	0.000	3.107	0.010	0.000	0.153	0.000	0.000	0.000	0.991	0.000
1.950	1.540	0.000	3.063	0.011	0.000	0.150	0.000	0.000	0.000	0.977	0.000
2.000	1.516	0.000	3.013	0.011	0.000	0.147	0.000	0.000	0.000	0.961	0.000

HNTB BRIDGE DESIGN PROGRAM BDGS
 RUN TIME: 05/03/2011 13:25:17.893
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRF\G4.OUT

VERSION 2.9.1.0

PAGE 38

----- UNFACTORED MOMENT SUMMARY -----

*** GIRDER 11, UNFACTORED MOMENT SUMMARY (Based on Input Section) ***

Notes: values do not include impact, except for COMBINED TRUCK+LANE.

MIN COMBINED TRUCK+LANE is the larger of: (1.33×TRK+LANE) and 0.9×(1.33×DTRK+LANE)

SPAN, LOC FRAC	DEAD LOAD		HL93 TRUCK	HL93 LANE	DOUBLE TRUCK	COMBINED TRUCK+LANE		FATIGUE TRUCK	
	A-DC MOMENT (ft-k)	B-DC MOMENT (ft-k)				MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)
0.000	0	0	2	2	-2	4	-3	1	-1
0.110	0	0	2	2	-1	4	-3	1	-1
0.736	-1	0	2	2	-6	4	-10	1	-5
0.890	-2	0	2	2	-41	5	-56	1	-34
1.000	-3	0	2	2	-49	5	-68	1	-41
					-56	5	-76	1	-46
1.000	-3	0	-2	1	-55	1	-76	0	-46
1.000	0	0	-1	1	-55	1	-75	0	-46
1.002	30	1	8	14	-55	7	-74	8	-45
1.010	123	6	37	53	-53	27	-74	29	-44
1.025	322	17	99	141	-50	71	-74	76	-42
1.031	396	21	122	165	-49	86	-73	86	-41
1.050	628	33	194	262	-45	136	-73	138	-37
1.052	655	34	202	268	-44	137	-72	140	-37
1.100	1216	63	373	448	-40	251	-78	230	-29
1.104	1265	66	388	464	-39	257	-79	237	-28
1.150	1733	91	536	586	-40	353	-92	294	-23
1.200	2207	116	683	694	-45	441	-112	349	-22
1.216	2353	124	728	744	-49	466	-121	373	-24
1.250	2639	139	814	791	-57	515	-142	395	-28
1.300	3032	158	929	852	-69	574	-171	418	-34
1.328	3238	168	988	884	-76	601	-188	430	-38
1.350	3342	175	1030	908	-82	627	-202	445	-41
1.400	3557	190	1115	961	-95	677	-233	472	-47
1.440	3703	199	1172	989	-105	708	-257	489	-52
1.445	3719	200	1178	990	-106	711	-260	489	-53
1.445	3719	200	1178	990	-106	711	-260	489	-53
1.450	3734	201	1185	988	-108	714	-264	485	-54
1.500	3874	209	1238	1006	-120	740	-294	488	-60
1.550	3976	214	1275	1015	-132	756	-324	491	-66
1.552	3980	214	1276	1018	-133	756	-325	493	-66
1.567	3963	213	1279	1023	-135	761	-330	498	-67
1.595	3923	212	1282	1024	-138	767	-339	494	-69
1.597	3918	212	1282	1023	-139	768	-340	492	-69
1.600	3914	212	1282	1022	-139	768	-340	491	-69
1.600	3914	212	1283	1017	-140	769	-342	488	-70
1.601	3913	212	1282	1017	-140	769	-342	488	-70
1.650	3809	208	1274	1021	-146	773	-357	490	-73
1.664	3772	206	1268	1036	-147	772	-360	504	-73
1.700	3668	201	1249	1016	-150	765	-369	487	-75
1.750	3492	193	1207	984	-153	745	-376	461	-76
1.776	3385	187	1176	971	-153	726	-376	462	-75
1.800	3058	171	1077	921	-142	677	-350	442	-70
1.850	2344	134	848	773	-116	550	-285	372	-57
1.900	1596	93	594	586	-84	398	-208	287	-42

BDGS Output - Unit 1 G4

1.950	815	49	313	332	-47	213	-53	0	655	-115	164	-23
2.000	1	1	5	9	-3	7	-4	0	18	-8	4	-2

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0 PAGE 39
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G4.OUT

UNFACTORED SHEAR SUMMARY

*** GIRDER 11, UNFACTORED SHEAR SUMMARY (Based on Input Section) ***

Note: values do not include impact, except for COMBINED TRUCK+LANE.

SPAN_Loc	A-DC	DEAD LOAD		HL93 TRUCK		HL93 LANE		COMBINED TRUCK+LANE		FATIGUE TRUCK		
		FRAC	SHEAR (kips)	B-DC SHEAR (kips)	DW SHEAR (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	
0.000	0.0	0.0	0.0	0.0	0.2	-24.1	0.2	-0.2	0.4	-32.2	0.1	-20.1
0.110	-0.1	0.0	-0.2	0.2	0.2	-24.2	0.2	-0.6	0.4	-32.8	0.1	-20.2
0.736	-1.8	-0.2	-1.0	0.2	0.2	-24.2	0.2	-0.6	0.4	-32.8	0.1	-20.2
0.890	-2.4	-0.2	-1.2	0.2	0.2	-24.2	0.2	-0.6	0.4	-32.8	0.1	-20.2
1.000	-2.8	-0.3	-1.3	0.2	0.2	-34.3	0.2	-1.0	0.4	-46.7	0.1	-22.9
1.000	129.2	6.8	40.1	59.1	-2.2	28.7	-2.5	107.3	-5.4	32.2	-1.1	31.9
1.000	129.2	6.8	40.1	58.6	-2.2	28.6	-2.5	106.5	-5.4	31.9	-1.1	31.9
1.002	128.8	6.8	40.0	59.0	-2.2	28.6	-2.5	107.1	-5.4	31.9	-1.1	31.9
1.010	127.6	6.7	39.5	55.3	-2.2	27.8	-2.5	101.3	-5.4	29.7	-1.1	29.7
1.025	124.8	6.6	38.6	55.4	-2.2	27.8	-2.5	101.4	-5.4	29.7	-1.1	29.7
1.031	123.8	6.5	38.3	55.7	-3.3	26.2	-2.5	94.9	-6.9	27.4	-1.1	27.4
1.050	120.6	6.3	37.1	52.0	-3.3	26.2	-2.5	95.3	-6.9	27.4	-1.1	27.4
1.052	120.2	6.3	37.0	51.6	-4.7	25.4	-2.6	94.0	-8.8	27.2	-1.1	27.2
1.100	112.1	5.8	34.1	41.0	-8.7	22.9	-3.0	82.8	-14.6	23.3	-1.1	23.3
1.104	111.4	5.7	33.8	46.8	-10.1	23.3	-3.2	85.4	-16.5	25.5	-1.1	25.5
1.150	97.7	5.3	30.7	40.6	-8.2	23.0	-3.4	75.0	-14.4	21.8	-1.1	21.8
1.200	89.6	4.7	27.6	36.1	-11.5	18.9	-4.2	67.0	-19.5	19.3	-1.1	19.3
1.216	87.0	4.5	26.4	32.9	-14.8	17.1	-5.2	60.8	-24.9	17.5	-1.1	17.5
1.250	81.7	4.2	24.5	33.3	-14.8	17.2	-5.2	61.4	-24.9	17.4	-1.1	17.4
1.300	73.9	3.6	21.4	30.0	-17.4	15.6	-6.2	55.5	-29.3	15.5	-1.1	15.5
1.328	69.6	3.3	19.8	33.9	-21.9	16.0	-7.6	61.1	-36.8	19.8	-1.1	19.8
1.350	46.2	3.1	18.5	32.7	-16.3	15.3	-6.4	58.8	-28.0	19.0	-1.1	19.0
1.400	38.7	2.5	15.4	28.2	-19.6	13.3	-7.4	50.9	-33.4	16.2	-1.1	16.2
1.440	32.8	2.0	12.8	26.6	-21.3	12.4	-8.1	47.7	-36.5	14.9	-1.1	14.9
1.445	32.1	2.0	12.5	26.9	-21.5	11.4	-8.5	43.3	-37.1	12.8	-1.1	12.8
1.445	32.1	2.0	12.5	23.9	-21.5	11.4	-8.5	43.3	-37.1	12.8	-1.1	12.8
1.450	31.4	1.9	12.2	24.3	-21.5	11.5	-8.5	43.8	-37.1	12.3	-1.1	12.3
1.500	23.9	1.3	9.0	22.6	-24.1	10.5	-9.4	40.6	-41.4	12.3	-1.1	12.3
1.550	16.6	0.6	5.9	21.7	-26.1	9.8	-10.2	38.7	-44.9	11.8	-1.1	11.8
1.552	16.2	0.5	5.6	25.6	-26.3	9.8	-10.1	43.8	-45.0	16.2	-1.1	16.2
1.567	-12.4	-0.4	1.7	24.7	-20.8	9.4	-7.6	42.2	-35.2	13.4	-1.1	13.4
1.595	-16.5	-0.6	0.1	21.5	-21.7	8.1	-8.1	36.9	-37.0	13.0	-1.1	13.0
1.597	-16.8	-0.6	0.0	21.5	-21.7	8.1	-8.1	36.9	-37.0	13.0	-1.1	13.0
1.600	-17.2	-0.6	-0.2	21.5	-21.7	8.1	-8.1	36.9	-37.0	13.0	-1.1	13.0
1.600	-17.2	-0.7	-0.5	22.4	-21.4	8.3	-8.1	38.0	-36.6	13.5	-1.1	13.5
1.601	-17.3	-0.7	-0.5	22.4	-20.5	8.3	-7.7	38.0	-35.0	13.5	-1.1	13.5
1.650	-24.4	-1.1	-3.8	19.3	-23.6	7.1	-8.8	32.7	-40.3	11.6	-1.1	11.6
1.664	-26.4	-1.2	-4.5	18.5	-24.7	6.5	-9.0	31.1	-41.9	11.0	-1.1	11.0
1.700	-31.4	-1.6	-7.3	17.0	-25.3	6.9	-9.5	28.5	-43.1	9.6	-1.1	9.6
1.750	-38.3	-2.1	-11.1	15.2	-27.7	4.3	-10.3	21.9	-47.2	7.4	-1.1	7.4
1.776	-134.7	-6.8	-41.0	11.3	-38.2	2.2	-22.5	21.2	-73.3	6.8	-1.1	6.8
1.800	-137.9	-7.2	-44.0	6.8	-41.6	2.2	-25.5	15.7	-80.8	3.1	-1.1	3.1
1.850	-144.7	-7.9	-48.9	6.2	-45.3	7.3	-29.4	15.6	-89.6	3.6	-1.1	3.6
1.900	-151.3	-8.6	-54.1	6.3	-55.8	8.3	-35.3	18.1	-109.5	4.0	-1.1	4.0
1.950	-157.9	-9.2	-58.9	8.1	-60.8	8.3	-39.8	20.2	-120.7	4.0	-1.1	4.0
2.000	-164.3	-9.6	-61.6	8.1	-72.2	9.3	-42.6	20.2	-138.6	4.0	-1.1	4.0

LOAD COMBINATION TABLES

COMBINATION TABLE: 1 LRFD2009 (Default)

#	NAME	CATEGORY	A-DL	B-DL	DW-DL	LL	NU	IMPACT TRK	FACT-LN	ENVELOPE-MOM	SHR
1	DC CONSTRUCTIBILITY	STRENGTH-IV	1.500	0.000	0.000	0.000	1.050	0.000	0.000	NONE	
2	DC+DW CONSTRUCTIBILITY	STRENGTH-IV	1.500	1.500	1.500	0.000	1.050	0.000	0.000	NONE	
3	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	MOM-MAX	
4	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	MOM-MIN	

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0 PAGE 40
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G4.OUT

LOAD COMBINATION TABLES

COMBINATION TABLE: 1 LRFD2009 (Default) (CONTD)

#	NAME	CATEGORY	A-DL	B-DL	DW-DL	LL	NU	IMPACT TRK	FACT-LN	ENVELOPE-MOM	SHR
5	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	SHR-MAX	
6	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	SHR-MIN	
7	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	MOM-MAX	
8	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	MOM-MIN	
9	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	SHR-MAX	
10	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	SHR-MIN	
11	SERVICE-II	SERVICE-II	1.000	1.000	1.000	1.300	1.000	1.330	1.000	MOM-MAX	
12	SERVICE-II	SERVICE-II	1.000	1.000	1.000	1.300	1.000	1.330	1.000	MOM-MIN	
13	SERVICE-II	SERVICE-II	1.000	1.000	1.000	1.300	1.000	1.330	1.000	SHR-MAX	
14	SERVICE-II	SERVICE-II	1.000	1.000	1.000	1.300	1.000	1.330	1.000	SHR-MIN	
15	FATIGUE I	FATIGUE-I LL M	1.000	1.000	1.000	1.500	1.000	1.150	1.000	MOM-MAX	
16	FATIGUE I	FATIGUE-I LL M	1.000	1.000	1.000	1.500	1.000	1.150	1.000	MOM-MIN	
17	FATIGUE I	FATIGUE-I LL V	1.000	1.000	1.000	1.500	1.000	1.150	1.000	SHR-MAX	
18	FATIGUE I	FATIGUE-I LL V	1.000	1.000	1.000	1.500	1.000	1.150	1.000	SHR-MIN	
19	FATIGUE WEB	FATIGUE-LL V WEB	1.000	1.000	1.000	1.500	1.000	1.150	1.000	SHR-MAX	
20	FATIGUE WEB	FATIGUE-LL V WEB	1.000	1.000	1.000	1.500	1.000	1.150	1.000	SHR-MIN	
21	FATIGUE II	FATIGUE-II LL M	1.000	1.000	1.000	0.750	1.000	1.150	1.000	MOM-MAX	
22	FATIGUE II	FATIGUE-II LL M	1.000	1.000	1.000	0.750	1.000	1.150	1.000	MOM-MIN	
23	FATIGUE II	FATIGUE-II LL V	1.000	1.000	1.000	0.750	1.000	1.150	1.000	SHR-MAX	
24	FATIGUE II	FATIGUE-II LL V	1.000	1.000	1.000	0.750	1.000	1.150	1.000	SHR-MIN	

BDGS Output - Unit 1 G5

1.767	0.743	0.000	1.433	-0.009	0.000	0.067	0.000	0.000	0.000	0.464	0.000
1.790	0.648	0.000	1.245	-0.008	0.000	0.057	0.000	0.000	0.000	0.401	0.000
1.796	0.623	0.000	1.196	-0.008	0.000	0.055	0.000	0.000	0.000	0.385	0.000
1.800	0.609	0.000	1.168	-0.008	0.000	0.054	0.000	0.000	0.000	0.376	0.000
1.809	0.575	0.000	1.102	-0.008	0.000	0.051	0.000	0.000	0.000	0.354	0.000
1.814	0.557	0.000	1.065	-0.008	0.000	0.049	0.000	0.000	0.000	0.341	0.000
1.826	0.508	0.000	0.971	-0.007	0.000	0.044	0.000	0.000	0.000	0.310	0.000
1.837	0.468	0.000	0.893	-0.007	0.000	0.040	0.000	0.000	0.000	0.284	0.000
1.850	0.420	0.000	0.798	-0.006	0.000	0.036	0.000	0.000	0.000	0.252	0.000
1.856	0.399	0.000	0.757	-0.006	0.000	0.034	0.000	0.000	0.000	0.238	0.000
1.860	0.384	0.000	0.722	-0.006	0.000	0.032	0.000	0.000	0.000	0.229	0.000
1.883	0.303	0.000	0.572	-0.005	0.000	0.025	0.000	0.000	0.000	0.177	0.000
1.886	0.296	0.000	0.558	-0.005	0.000	0.024	0.000	0.000	0.000	0.172	0.000
1.900	0.249	0.000	0.468	-0.005	0.000	0.020	0.000	0.000	0.000	0.143	0.000
1.907	0.228	0.000	0.428	-0.004	0.000	0.018	0.000	0.000	0.000	0.130	0.000
1.915	0.201	0.000	0.378	-0.004	0.000	0.016	0.000	0.000	0.000	0.113	0.000
1.930	0.158	0.000	0.296	-0.003	0.000	0.012	0.000	0.000	0.000	0.087	0.000
1.945	0.118	0.000	0.220	-0.003	0.000	0.009	0.000	0.000	0.000	0.063	0.000
1.950	0.105	0.000	0.196	-0.003	0.000	0.008	0.000	0.000	0.000	0.056	0.000
1.953	0.097	0.000	0.180	-0.002	0.000	0.007	0.000	0.000	0.000	0.051	0.000
1.973	0.052	0.000	0.097	-0.001	0.000	0.004	0.000	0.000	0.000	0.026	0.000
1.977	0.043	0.000	0.081	-0.001	0.000	0.003	0.000	0.000	0.000	0.021	0.000
1.999	0.002	0.000	0.004	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.000
2.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2.011	-0.001	0.000	-0.002	0.000	0.000	0.000	0.000	0.000	0.000	-0.001	0.000
2.050	-0.005	0.000	-0.010	0.000	0.000	-0.001	0.000	0.000	0.000	-0.004	0.000
2.100	-0.010	0.000	-0.019	0.001	0.000	-0.001	0.000	0.000	0.000	-0.008	0.000
2.150	-0.013	0.000	-0.027	0.001	0.000	-0.001	0.000	0.000	0.000	-0.011	0.000
2.200	-0.017	0.000	-0.033	0.002	0.000	-0.002	0.000	0.000	0.000	-0.013	0.000
2.250	-0.019	0.000	-0.038	0.002	0.000	-0.002	0.000	0.000	0.000	-0.015	0.000
2.259	-0.019	0.000	-0.039	0.002	0.000	-0.002	0.000	0.000	0.000	-0.016	0.000
2.300	-0.021	0.000	-0.042	0.002	0.000	-0.002	0.000	0.000	0.000	-0.017	0.000
2.350	-0.022	0.000	-0.045	0.003	0.000	-0.002	0.000	0.000	0.000	-0.018	0.000
2.400	-0.023	0.000	-0.047	0.003	0.000	-0.002	0.000	0.000	0.000	-0.018	0.000
2.450	-0.024	0.000	-0.049	0.004	0.000	-0.002	0.000	0.000	0.000	-0.018	0.000
2.500	-0.024	0.000	-0.049	0.004	0.000	-0.002	0.000	0.000	0.000	-0.018	0.000
2.518	-0.024	0.000	-0.049	0.004	0.000	-0.002	0.000	0.000	0.000	-0.018	0.000
2.550	-0.023	0.000	-0.048	0.004	0.000	-0.002	0.000	0.000	0.000	-0.018	0.000

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0 PAGE 42
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G5.OUT

----- CAMBER DATA -----

*** GIRDER 12 DEAD LOAD CAMBER VALUES: (Positive Values Upward) ***

Note: Displacements due to removable forms are not included.

SPAN, LOC FRAC	A-DC DEAD LOAD					B-DC DEAD LOAD			INTEGRAL	DW DEAD	LOAD
	STEEL GIRDER (in)	USER STEEL (in)	CONCRETE SLAB (in)	USER CONC (in)	USER ADD. (in)	BARR (in)	SDWALK (in)	USER ADD. (in)	WEARING SURFACE (in)	WEARING SURFACE (in)	UTILS (in)
2.600	-0.022	0.000	-0.045	0.005	0.000	-0.002	0.000	0.000	0.000	-0.017	0.000
2.650	-0.020	0.000	-0.042	0.005	0.000	-0.002	0.000	0.000	0.000	-0.016	0.000
2.700	-0.018	0.000	-0.039	0.006	0.000	-0.001	0.000	0.000	0.000	-0.014	0.000
2.750	-0.016	0.000	-0.035	0.006	0.000	-0.001	0.000	0.000	0.000	-0.013	0.000
2.800	-0.014	0.000	-0.030	0.007	0.000	-0.001	0.000	0.000	0.000	-0.011	0.000
2.850	-0.012	0.000	-0.026	0.007	0.000	0.000	0.000	0.000	0.000	-0.009	0.000
2.900	-0.009	0.000	-0.021	0.008	0.000	0.000	0.000	0.000	0.000	-0.007	0.000
2.950	-0.006	0.000	-0.016	0.008	0.000	0.000	0.000	0.000	0.000	-0.005	0.000
3.000	-0.004	0.000	-0.011	0.009	0.000	0.001	0.000	0.000	0.000	-0.003	0.000

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0 PAGE 43
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G5.OUT

----- UNFACTORED MOMENT SUMMARY -----

*** GIRDER 12, UNFACTORED MOMENT SUMMARY (Based on Input Section) ***

Notes: Values do not include impact, except for COMBINED TRUCK+LANE.

MIN COMBINED TRUCK+LANE is the larger of: (1.33*TRK+LANE) and 0.9*(1.33*DTRK+LANE)

SPAN, LOC FRAC	A-DC MOMENT (ft-k)	DEAD LOAD B-DC MOMENT (ft-k)	DW MOMENT (ft-k)	HL93 TRUCK		HL93 LANE		DOUBLE TRUCK	COMBINED TRUCK+LANE		FATIGUE TRUCK	
				MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)
0.000	0	0	0	0	0	0	0	0	0	0	0	0
0.109	0	0	0	0	-6	0	0	-6	0	-8	0	-5
0.891	-2	0	-1	0	-51	0	-1	-51	0	-69	0	-42
0.914	-2	0	-1	0	-52	0	-1	-52	0	-70	0	-43
1.000	-3	0	-2	0	-57	0	-1	-57	0	-77	0	-47
1.000	-3	0	-1	2	-57	2	-2	-57	5	-78	1	-47
1.000	0	0	0	3	-57	2	-2	0	6	-78	1	-47
1.010	227	12	75	107	-53	50	-5	0	192	-76	57	-44
1.020	459	25	152	203	-49	100	-10	0	370	-75	107	-41
1.027	599	32	199	267	-46	131	-13	0	486	-74	140	-39
1.031	684	37	227	287	-44	144	-14	0	526	-73	146	-37
1.034	753	41	250	314	-43	158	-16	0	575	-73	161	-36
1.034	767	42	254	320	-43	161	-16	0	587	-73	164	-36
1.050	1088	59	361	439	-41	227	-23	0	810	-77	223	-31
1.053	1156	62	383	462	-40	240	-25	0	855	-78	234	-30
1.068	1435	77	475	542	-39	291	-31	0	1013	-83	270	-25
1.080	1657	90	551	600	-39	338	-37	0	1136	-88	295	-23
1.100	1995	108	665	699	-39	404	-45	0	1334	-98	346	-20
1.107	2104	114	702	712	-42	424	-48	0	1371	-104	346	-21
1.126	2398	130	801	791	-49	478	-56	0	1530	-122	393	-24
1.133	2506	135	838	799	-52	497	-60	0	1559	-129	386	-26
1.150	2734	147	914	850	-58	534	-67	0	1665	-144	416	-29
1.160	2865	154	958	855	-62	554	-71	0	1691	-154	408	-31
1.184	3152	169	1053	912	-71	596	-81	0	1808	-176	439	-35
1.187	3177	170	1061	913	-72	601	-82	0	1815	-178	437	-36

BDGS Output - Unit 1 G5

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0
RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G5.OUT

UNFACTORED MOMENT SUMMARY

*** GIRDER 12, UNFACTORED MOMENT SUMMARY (Based on Input Section) ***

Notes: values do not include impact, except for COMBINED TRUCK+LANE.

MIN COMBINED TRUCK+LANE is the larger of: (1.33*TRK+LANE) and 0.9*(1.33*DTRK+LANE)

Table with 14 columns: SPAN, LOC, A-DC, B-DC, DW, HL93 TRUCK, HL93 LANE, DOUBLE TRUCK, COMBINED TRUCK+LANE, FATIGUE TRUCK. Rows show moment values in ft-k for various span lengths from 2.450 to 3.000.

UNFACTORED SHEAR SUMMARY

*** GIRDER 12, UNFACTORED SHEAR SUMMARY (Based on Input Section) ***

Note: values do not include impact, except for COMBINED TRUCK+LANE.

Table with 14 columns: SPAN, LOC, A-DC, B-DC, DW, HL93 TRUCK, HL93 LANE, COMBINED TRUCK+LANE, FATIGUE TRUCK. Rows show shear values in kips for various span lengths from 0.000 to 1.267.

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0
RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G5.OUT

UNFACTORED SHEAR SUMMARY

*** GIRDER 12, UNFACTORED SHEAR SUMMARY (Based on Input Section) ***

Note: values do not include impact, except for COMBINED TRUCK+LANE.

Table with 14 columns: SPAN, LOC, A-DC, B-DC, DW, HL93 TRUCK, HL93 LANE, COMBINED TRUCK+LANE, FATIGUE TRUCK. Rows show shear values in kips for various span lengths from 1.294 to 1.480.

BDGS Output - Unit 1 G5

1.500	0.6	0.4	3.2	28.0	-20.7	11.6	-14.6	48.9	-42.2	13.0	-12.6
1.502	0.0	0.4	2.9	28.0	-20.7	11.6	-14.6	48.9	-42.2	13.0	-12.6
1.507	-1.4	0.5	3.7	31.2	-20.7	13.1	-14.6	54.7	-42.2	14.0	-12.6
1.533	-8.3	0.1	1.1	28.5	-22.5	12.6	-15.4	50.6	-45.3	13.7	-14.4
1.534	-78.5	-4.0	-24.2	38.6	-25.8	12.6	-15.7	56.0	-50.1	19.5	-15.2
1.550	-83.9	-4.2	-26.0	28.8	-27.4	9.3	-14.3	47.5	-50.7	16.9	-13.8
1.557	-86.2	-4.3	-26.8	27.3	-28.5	9.7	-14.9	45.0	-52.8	16.0	-14.7
1.580	-93.9	-4.6	-29.3	24.6	-30.4	7.5	-15.9	40.2	-56.4	14.2	-16.2
1.592	-97.7	-4.8	-30.5	22.9	-31.3	6.9	-16.5	37.3	-58.1	13.1	-16.9
1.600	-100.3	-4.9	-31.3	22.9	-31.3	6.9	-16.5	37.3	-58.1	13.1	-16.9
1.604	-101.5	-4.9	-31.8	21.2	-32.7	6.3	-17.3	34.6	-60.8	12.1	-18.1
1.627	-109.0	-5.3	-34.3	17.5	-35.1	5.1	-19.0	28.3	-65.6	9.6	-19.9
1.650	-116.2	-5.6	-36.7	17.4	-37.6	4.9	-20.0	28.0	-70.1	9.5	-21.7
1.650	-116.3	-5.6	-36.7	22.7	-37.7	6.2	-20.1	36.5	-70.2	14.3	-21.8
1.650	-110.7	-5.3	-35.1	20.8	-31.4	4.8	-18.6	35.4	-60.3	13.2	-16.3
1.674	-118.0	-5.6	-37.5	16.8	-33.6	4.5	-20.1	26.9	-64.7	10.7	-17.8
1.697	-125.2	-6.0	-40.0	16.2	-35.9	4.2	-21.2	25.8	-68.9	10.5	-19.4
1.700	-126.1	-6.0	-40.3	16.4	-35.3	4.2	-21.1	26.1	-68.0	10.5	-18.9
1.709	-128.7	-6.1	-41.2	16.0	-36.8	3.8	-21.9	23.8	-70.8	9.6	-20.1
1.716	-130.9	-6.2	-42.0	14.3	-37.5	3.6	-22.3	22.6	-72.2	9.1	-20.7
1.716	-130.9	-6.2	-42.0	14.3	-37.5	3.6	-22.3	22.6	-72.2	9.1	-20.7
1.720	-132.3	-6.3	-42.5	12.4	-38.1	3.0	-23.1	19.5	-73.7	7.6	-22.2
1.723	-132.2	-6.3	-42.7	12.4	-37.4	3.0	-22.9	19.5	-72.7	7.6	-20.6
1.744	-139.6	-6.6	-44.9	11.2	-40.0	3.0	-24.5	17.4	-77.8	6.6	-22.8
1.750	-141.5	-6.7	-45.6	11.2	-39.4	2.5	-24.4	17.4	-76.8	6.6	-22.3
1.767	-146.6	-6.9	-47.3	11.6	-42.1	2.5	-25.7	24.2	-81.7	9.9	-22.7
1.767	-144.1	-6.8	-46.5	13.1	-36.0	2.9	-24.2	20.2	-72.1	8.3	-19.4
1.790	-151.2	-7.1	-49.0	12.6	-38.0	2.6	-25.2	19.3	-75.8	8.0	-20.8
1.796	-153.0	-7.2	-49.6	11.1	-38.4	2.3	-25.7	17.0	-76.7	7.1	-21.0
1.800	-154.1	-7.2	-50.0	11.1	-38.4	2.3	-25.7	17.0	-76.7	7.1	-21.0
1.809	-156.7	-7.4	-50.9	10.5	-39.6	2.1	-26.3	16.0	-79.0	6.8	-22.0
1.814	-158.4	-7.4	-51.4	9.3	-40.1	1.8	-26.9	14.1	-80.2	6.0	-22.4
1.826	-162.8	-7.8	-53.8	13.4	-41.1	1.7	-27.4	20.5	-82.1	8.7	-22.2
1.837	-164.6	-7.9	-55.0	10.1	-37.9	1.8	-27.5	15.3	-77.9	6.6	-20.4
1.850	-169.2	-8.1	-56.4	10.1	-37.5	1.8	-27.4	15.3	-77.3	6.6	-20.0
1.856	-171.2	-8.2	-57.0	9.7	-39.8	1.8	-28.4	14.6	-81.3	6.3	-21.8
1.860	-172.7	-8.3	-57.5	7.4	-40.0	1.5	-29.1	11.9	-82.3	4.3	-22.0
1.883	-180.6	-8.6	-60.1	7.2	-41.9	1.5	-30.3	11.1	-86.0	4.7	-23.8
1.886	-181.4	-9.3	-64.6	9.1	-42.1	1.7	-31.1	13.8	-87.1	6.2	-23.9
1.900	-184.1	-9.5	-66.1	8.0	-40.2	1.7	-31.5	12.3	-84.9	5.1	-21.5

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0 PAGE 47
 RUN TIME: 05/03/2011 13:25:17.893
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G5.OUT

UNFACTORED SHEAR SUMMARY

*** GIRDER 12, UNFACTORED SHEAR SUMMARY (Based on Input Section) ***

Note: values do not include impact, except for COMBINED TRUCK+LANE.

SPAN, LOC FRAC	A-DC SHEAR (kips)	DEAD LOAD B-DC SHEAR (kips)	DW SHEAR (kips)	HL93 TRUCK		HL93 LANE		COMBINED TRUCK+LANE		FATIGUE TRUCK	
				MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)
1.907	-186.4	-9	-67.0	6.6	-42.4	1.7	-32.8	10.1	-89.1	4.3	-23.1
1.915	-189.3	-9.8	-67.9	5.0	-43.4	1.7	-33.6	8.4	-91.4	3.4	-23.9
1.930	-194.2	-10.0	-69.6	3.4	-44.8	1.8	-34.9	6.3	-94.4	2.3	-25.0
1.945	-199.1	-11.1	-77.3	4.1	-46.7	2.0	-37.6	7.4	-99.7	2.8	-26.2
1.950	-199.5	-11.2	-77.8	4.1	-47.1	2.0	-38.0	7.5	-100.7	2.5	-26.0
1.953	-200.6	-11.3	-78.4	2.9	-47.3	2.0	-39.0	5.9	-101.9	2.5	-26.1
1.973	-206.9	-11.5	-80.4	2.7	-49.2	2.0	-40.0	5.6	-105.4	1.6	-27.8
1.977	-208.2	-11.6	-81.0	2.0	-49.5	2.1	-41.2	4.7	-107.0	1.4	-28.0
1.999	-215.3	-11.9	-83.3	2.0	-51.7	2.1	-42.3	4.7	-111.1	1.1	-29.8
2.000	-215.8	-12.0	-83.4	2.0	-51.8	2.1	-42.4	4.7	-111.4	1.1	-29.9
2.000	370.2	18.3	124.5	40.1	-3.2	62.4	-2.6	115.8	-6.8	25.8	-1.5
2.011	369.8	18.3	124.4	40.0	-3.2	62.4	-2.6	115.6	-6.8	25.7	-1.5
2.050	368.2	18.2	123.9	38.9	-3.2	61.9	-2.6	113.7	-6.8	24.9	-1.5
2.100	366.3	18.1	123.3	37.1	-3.2	61.5	-2.6	110.8	-6.8	23.5	-1.5
2.150	364.3	18.0	122.8	35.9	-3.2	61.0	-2.6	108.7	-6.8	22.5	-1.5
2.200	362.4	18.0	122.3	34.6	-3.2	60.7	-2.6	106.7	-6.8	21.6	-2.0
2.250	360.4	17.9	121.8	33.7	-3.3	60.3	-2.6	105.1	-7.0	20.8	-2.7
2.259	360.1	17.9	121.7	33.7	-3.3	60.3	-2.6	105.1	-7.0	20.8	-2.7
2.300	358.5	17.8	121.3	32.9	-4.1	60.1	-2.6	103.9	-8.0	19.9	-3.2
2.350	356.6	17.8	120.9	32.2	-5.2	59.9	-2.6	102.7	-9.5	19.0	-3.8
2.400	354.7	17.7	120.5	31.4	-6.3	59.7	-2.6	101.5	-11.0	18.1	-4.4
2.450	352.8	17.7	120.2	30.7	-7.4	59.6	-2.6	100.5	-12.5	17.2	-5.0
2.500	350.8	17.6	119.8	30.3	-8.6	59.7	-2.7	100.0	-14.1	16.6	-5.6
2.518	435.2	21.1	143.6	35.5	-10.9	67.1	-3.3	114.3	-17.8	18.2	-6.4
2.550	434.0	21.1	143.5	35.7	-11.5	67.1	-3.3	114.6	-18.6	18.3	-6.7
2.600	432.1	21.1	143.2	36.0	-13.0	67.2	-3.3	115.0	-20.6	18.4	-7.5
2.650	430.2	21.1	143.0	36.2	-14.5	67.3	-3.4	115.5	-22.7	18.6	-8.4
2.700	428.3	21.0	142.7	36.5	-16.0	67.4	-3.4	116.0	-24.7	18.8	-9.4
2.750	426.4	21.0	142.4	36.8	-17.6	67.7	-3.4	116.6	-26.8	18.9	-10.5
2.800	424.5	20.9	142.2	37.0	-19.2	67.8	-3.4	117.0	-28.9	19.0	-11.6
2.850	422.7	20.9	141.8	37.2	-20.8	67.9	-3.5	117.4	-31.1	19.1	-12.6
2.900	420.8	20.8	141.4	37.4	-22.4	68.1	-3.6	117.8	-33.5	19.2	-13.6
2.950	418.9	20.8	140.9	37.5	-24.1	68.1	-4.1	117.9	-36.1	19.2	-14.6
3.000	417.1	20.7	140.3	37.5	-25.7	68.1	-4.4	117.9	-38.6	19.2	-15.6

LOAD COMBINATION TABLES

COMBINATION TABLE: 1 LRFD2009 (Default)

#	NAME	CATEGORY	LOAD FACTORS					-IMPACT TRK	FACT- LN	ENVELOPE	
			A-DL	B-DL	DW-DL	LL	NU			MOM	SHR
1	DC CONSTRUCTIBILITY	STRENGTH-IV	1.500	0.000	0.000	0.000	1.050	0.000	0.000	NONE	
2	DC+DW CONSTRUCTIBILITY	STRENGTH-IV	1.500	1.500	1.500	0.000	1.050	0.000	0.000	NONE	
3	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	MOM-MAX	
4	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	MOM-MIN	
5	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	SHR-MAX	
6	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	SHR-MIN	
7	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	MOM-MAX	
8	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	MOM-MIN	
9	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	SHR-MAX	
10	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	SHR-MIN	
11	SERVICE-II	SERVICE-II	1.000	1.000	1.000	1.300	1.000	1.330	1.000	MOM-MAX	

BDGS Output - Unit 1 G6

1.386	4313	203	1439	1087	-153	795	-175	0	2241	-379	520	-76
1.400	4307	202	1438	1087	-161	795	-183	0	2241	-397	519	-79
1.405	4302	202	1436	1079	-163	794	-186	0	2229	-402	510	-80
1.425	4268	200	1426	1075	-173	789	-197	0	2218	-427	509	-85
1.432	4243	199	1419	1070	-177	792	-201	0	2215	-436	502	-87
1.450	4166	196	1398	1079	-186	798	-212	0	2234	-460	509	-92
1.459	4123	194	1386	1076	-191	800	-218	0	2231	-472	502	-94
1.482	3984	188	1344	1087	-204	803	-232	0	2248	-504	519	-101
1.486	3960	187	1337	1078	-206	802	-235	0	2236	-508	514	-102
1.500	3856	182	1304	1066	-214	798	-243	0	2217	-528	503	-106
1.513	3756	177	1272	1070	-221	794	-251	0	2217	-545	505	-110
1.538	3523	166	1195	1047	-235	780	-268	0	2172	-581	491	-117

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G6.OUT

----- UNFACTORED MOMENT SUMMARY -----

*** GIRDER 13, UNFACTORED MOMENT SUMMARY (Based on Input Section) ***

Notes: values do not include impact, except for COMBINED TRUCK+LANE.

MIN COMBINED TRUCK+LANE is the larger of: (1.33*TRK+LANE) and 0.9*(1.33*DTRK+LANE)

SPAN. LOC FRAC	A-DC MOMENT (ft-k)	DEAD LOAD B-DC MOMENT (ft-k)	DW MOMENT (ft-k)	HL93 TRUCK		HL93 LANE		DOUBLE TRUCK MIN (ft-k)	COMBINED TRUCK+LANE		FATIGUE TRUCK	
				MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)		MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)
1.540	3509	166	1190	1048	-236	779	-268	0	2172	-582	492	-118
1.550	3364	159	1147	1030	-241	763	-274	0	2152	-594	485	-120
1.563	3181	151	1091	1015	-246	743	-280	0	2093	-608	484	-123
1.586	2823	135	981	977	-257	700	-292	0	1999	-633	469	-128
1.597	2635	126	922	957	-262	677	-298	0	1950	-646	460	-131
1.600	2584	124	906	941	-263	670	-300	0	1921	-650	450	-131
1.609	2436	117	859	931	-267	652	-304	0	1890	-660	447	-133
1.632	2019	97	725	880	-278	599	-317	0	1769	-687	417	-139
1.650	1665	81	610	832	-287	552	-327	0	1659	-710	389	-144
1.654	1577	76	582	825	-289	541	-330	0	1638	-715	388	-145
1.655	1572	76	580	825	-290	542	-330	0	1640	-716	388	-145
1.678	1064	54	428	790	-304	498	-346	0	1548	-750	375	-152
1.700	543	31	269	753	-318	447	-362	0	1448	-784	358	-159
1.701	527	30	264	750	-318	447	-363	0	1445	-786	357	-160
1.712	257	18	180	734	-325	420	-371	0	1397	-804	349	-163
1.719	74	10	124	714	-330	402	-377	0	1351	-816	338	-165
1.719	74	10	124	714	-330	402	-377	0	1351	-816	338	-165
1.722	0	7	101	712	-332	395	-380	-541	1342	-990	337	-166
1.724	-39	5	89	705	-333	392	-382	-543	1329	-993	333	-167
1.747	-634	-22	-98	653	-348	337	-408	-567	1205	-1046	304	-175
1.750	-721	-26	-125	639	-350	328	-412	-571	1178	-1054	293	-176
1.769	-1244	-49	-291	600	-363	283	-443	-593	1081	-1108	273	-183
1.770	-1259	-50	-295	599	-364	283	-444	-593	1079	-1110	273	-183
1.793	-1930	-80	-504	547	-380	239	-490	-620	967	-1184	246	-192
1.799	-2103	-87	-558	538	-384	228	-502	-627	944	-1203	243	-194
1.800	-2146	-89	-572	532	-385	225	-506	-629	933	-1208	238	-194
1.811	-2485	-105	-678	504	-393	204	-533	-641	874	-1247	223	-199
1.816	-2630	-111	-724	491	-396	196	-546	-647	849	-1266	216	-201
1.828	-3010	-128	-844	463	-405	175	-579	-660	791	-1312	201	-204
1.839	-3368	-144	-952	432	-413	158	-611	-673	732	-1356	186	-209
1.850	-3740	-160	-1065	398	-421	140	-645	-688	669	-1404	169	-214
1.857	-3984	-170	-1139	386	-426	130	-669	-696	643	-1435	173	-216
1.862	-4144	-177	-1188	368	-430	123	-684	-702	613	-1457	165	-219
1.885	-4955	-212	-1434	303	-447	91	-767	-743	494	-1580	143	-228
1.887	-5014	-215	-1452	299	-448	88	-772	-747	487	-1589	144	-229
1.900	-5510	-234	-1592	260	-457	80	-823	-789	427	-1686	128	-234
1.908	-5807	-246	-1676	239	-463	79	-855	-816	397	-1747	120	-237
1.916	-6108	-258	-1760	222	-469	76	-887	-843	371	-1807	116	-240
1.931	-6693	-282	-1926	178	-480	74	-954	-898	310	-1933	91	-247
1.945	-7257	-304	-2085	141	-490	71	-1020	-950	259	-2055	78	-253
1.950	-7454	-311	-2136	127	-493	71	-1043	-968	240	-2097	72	-255
1.954	-7616	-317	-2178	123	-499	71	-1062	-982	235	-2132	63	-256
1.973	-8390	-345	-2378	126	-543	70	-1158	-1052	236	-2301	63	-282
1.977	-8576	-352	-2426	126	-558	69	-1182	-1070	237	-2344	63	-288
1.999	-9513	-386	-2669	129	-632	69	-1309	-1160	240	-2566	65	-330
2.000	-9569	-388	-2684	129	-637	69	-1317	-1165	241	-2580	65	-332
2.000	-9569	-388	-2683	129	-636	68	-1316	-1165	240	-2578	65	-331
2.002	-9532	-387	-2673	127	-635	67	-1309	-1160	237	-2566	64	-330
2.010	-9395	-381	-2638	123	-630	64	-1284	-1142	227	-2523	62	-328
2.021	-9223	-375	-2593	116	-624	60	-1253	-1120	214	-2469	58	-324
2.031	-9054	-369	-2549	110	-617	55	-1223	-1099	201	-2417	55	-320
2.041	-8886	-363	-2505	103	-611	53	-1195	-1079	191	-2367	52	-316
2.050	-8742	-357	-2468	98	-606	53	-1171	-1062	183	-2325	49	-313
2.051	-8721	-356	-2463	97	-605	53	-1167	-1060	182	-2319	49	-313
2.053	-8695	-355	-2456	96	-604	52	-1163	-1056	180	-2311	48	-312
2.062	-8558	-350	-2421	91	-600	52	-1141	-1041	173	-2273	51	-309
2.072	-8397	-345	-2380	103	-594	51	-1116	-1023	188	-2229	59	-306

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G6.OUT

----- UNFACTORED MOMENT SUMMARY -----

*** GIRDER 13, UNFACTORED MOMENT SUMMARY (Based on Input Section) ***

Notes: values do not include impact, except for COMBINED TRUCK+LANE.

MIN COMBINED TRUCK+LANE is the larger of: (1.33*TRK+LANE) and 0.9*(1.33*DTRK+LANE)

SPAN. LOC FRAC	A-DC MOMENT (ft-k)	DEAD LOAD B-DC MOMENT (ft-k)	DW MOMENT (ft-k)	HL93 TRUCK		HL93 LANE		DOUBLE TRUCK MIN (ft-k)	COMBINED TRUCK+LANE		FATIGUE TRUCK	
				MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)		MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)
2.082	-8239	-339	-2340	121	-589	50	-1093	-1006	211	-2187	66	-303
2.092	-8083	-333	-2301	139	-583	49	-1071	-989	234	-2147	74	-299
2.100	-7967	-329	-2272	152	-579	49	-1055	-977	252	-2119	82	-297
2.103	-7929	-328	-2263	156	-578	49	-1050	-973	256	-2109	82	-296

BDGS Output - Unit 1 G6

2.106	-7881	-326	-2251	162	-576	49	-1043	-968	264	-2098	86	-295
2.113	-7826	-325	-2241	174	-577	48	-1035	-963	280	-2084	90	-294
2.123	-7747	-323	-2226	193	-578	48	-1024	-956	305	-2065	98	-294
2.133	-7671	-321	-2212	212	-579	48	-1014	-949	330	-2049	106	-295
2.144	-7598	-319	-2200	231	-581	55	-1005	-946	362	-2037	114	-295
2.150	-7553	-318	-2193	239	-582	60	-1000	-948	378	-2034	117	-295
2.154	-7526	-317	-2188	250	-583	62	-997	-949	395	-2033	121	-295
2.155	-7515	-317	-2187	253	-583	64	-996	-949	400	-2033	123	-295
2.164	-7456	-316	-2178	271	-585	70	-991	-953	430	-2032	128	-295
2.174	-7389	-315	-2169	290	-588	78	-986	-957	464	-2032	138	-295
2.185	-7324	-314	-2161	310	-591	85	-981	-960	497	-2033	148	-296
2.195	-7261	-313	-2154	328	-594	93	-978	-964	529	-2034	158	-298
2.200	-7231	-312	-2151	337	-596	97	-976	-966	545	-2035	161	-299
2.205	-7203	-312	-2148	348	-598	100	-975	-969	564	-2037	168	-300
2.205	-7201	-312	-2148	349	-598	101	-976	-969	565	-2039	169	-300
2.245	-6260	-269	-1853	422	-559	137	-852	-902	698	-1847	194	-280
2.250	-6142	-263	-1815	426	-553	141	-837	-893	707	-1823	192	-277
2.255	-6031	-258	-1781	439	-548	146	-823	-886	730	-1801	199	-274
2.285	-5358	-227	-1570	488	-520	175	-743	-840	824	-1674	215	-259
2.300	-5020	-212	-1464	503	-504	190	-705	-815	859	-1610	219	-251
2.305	-4921	-207	-1433	516	-500	195	-694	-809	880	-1592	227	-249
2.322	-4565	-190	-1320	539	-485	214	-655	-785	932	-1529	239	-242
2.324	-4525	-189	-1307	545	-484	217	-651	-781	941	-1520	243	-241
2.350	-4028	-165	-1149	575	-462	244	-600	-745	1009	-1431	256	-230
2.354	-3947	-162	-1123	586	-459	250	-592	-739	1028	-1418	263	-228
2.364	-3759	-153	-1064	597	-451	261	-574	-726	1056	-1386	269	-224
2.400	-3095	-122	-855	631	-421	301	-515	-679	1141	-1277	286	-209
2.404	-3025	-119	-833	640	-418	306	-509	-674	1157	-1266	293	-208
2.444	-2382	-88	-626	690	-392	359	-460	-632	1276	-1170	324	-194
2.450	-2282	-84	-593	690	-387	366	-453	-625	1284	-1155	322	-192
2.479	-1834	-62	-450	724	-369	405	-423	-594	1368	-1092	343	-183
2.479	-1834	-62	-450	724	-369	405	-423	-594	1368	-1092	343	-183
2.483	-1771	-59	-431	733	-366	410	-419	-589	1383	-1083	351	-181
2.500	-1525	-48	-352	749	-356	431	-405	-571	1427	-1048	359	-176
2.503	-1477	-46	-337	753	-354	435	-402	-568	1436	-1042	361	-175
2.523	-1191	-32	-247	769	-341	460	-387	-548	1482	-1004	369	-169
2.550	-814	-15	-130	777	-325	490	-368	-521	1523	-955	363	-160
2.563	-639	-7	-76	796	-317	505	-359	-509	1563	-933	381	-157
2.600	-151	15	72	812	-295	540	-335	-474	1619	-869	387	-145
2.603	-117	16	83	818	-294	542	-333	-472	1630	-865	390	-145
2.614	0	22	122	819	-288	553	-326	-460	1642	-860	388	-142
2.642	266	35	212	850	-274	578	-311	-445	1708	-808	409	-135
2.650	337	39	235	849	-270	584	-307	-438	1713	-806	406	-133
2.682	621	53	328	873	-255	607	-289	-415	1767	-769	423	-125
2.700	772	60	375	877	-246	617	-280	-408	1783	-760	425	-121
2.702	789	60	380	881	-246	618	-279	-407	1790	-760	427	-121
2.722	949	68	430	887	-237	628	-269	-400	1808	-753	429	-116
2.750	1164	77	494	886	-223	636	-253	-393	1814	-750	425	-110
2.762	1248	81	519	892	-218	640	-248	-388	1826	-748	429	-107
2.800	1511	91	589	880	-199	638	-226	-368	1808	-726	420	-98
2.801	1520	92	592	884	-200	641	-227	-369	1816	-727	422	-98
2.841	1269	80	518	800	-166	558	-188	-300	1622	-609	384	-81
2.850	1209	77	498	760	-157	534	-179	-291	1545	-588	365	-77
2.881	991	66	424	677	-130	456	-147	-216	1356	-320	331	-64

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0 PAGE 48
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G6.OUT

----- UNFACTORED MOMENT SUMMARY -----

*** GIRDER 13, UNFACTORED MOMENT SUMMARY (Based on Input Section) ***

Notes: values do not include impact, except for COMBINED TRUCK+LANE.

MIN COMBINED TRUCK+LANE is the larger of: (1.33*TRK+LANE) and 0.9*(1.33*DTRK+LANE)

SPAN, LOC FRAC	A-DC MOMENT (ft-k)	DEAD LOAD B-DC MOMENT (ft-k)	DW MOMENT (ft-k)	HL93 TRUCK		HL93 LANE		DOUBLE TRUCK MIN	COMBINED TRUCK+LANE		FATIGUE TRUCK	
				MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)		MAX (ft-k)	MIN (ft-k)	MAX (ft-k)	MIN (ft-k)
2.900	848	57	369	602	-110	395	-125	0	1195	-272	296	-54
2.921	687	48	308	516	-90	330	-103	0	1016	-222	256	-44
2.950	445	32	205	341	-58	217	-66	0	670	-143	165	-28
2.960	357	26	168	294	-47	178	-53	0	569	-116	148	-23
3.000	1	1	6	10	-3	8	-3	0	21	-7	5	-2

----- UNFACTORED SHEAR SUMMARY -----

*** GIRDER 13, UNFACTORED SHEAR SUMMARY (Based on Input Section) ***

Note: values do not include impact, except for COMBINED TRUCK+LANE.

SPAN, LOC FRAC	A-DC SHEAR (kips)	DEAD LOAD B-DC SHEAR (kips)	DW SHEAR (kips)	HL93 TRUCK		HL93 LANE		COMBINED TRUCK+LANE MAX	COMBINED TRUCK+LANE MIN	FATIGUE TRUCK	
				MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)			MAX (kips)	MIN (kips)
0.000	0.0	0.0	0.0	0.2	-29.8	0.2	-0.3	0.4	-39.8	0.1	-20.8
0.108	0.1	0.0	-0.1	0.2	-29.8	0.2	-0.4	0.4	-39.9	0.1	-20.9
0.892	-2.4	-0.3	-1.2	0.2	-29.9	0.2	-0.8	0.4	-40.6	0.1	-22.5
1.000	-2.9	-0.3	-1.4	0.2	-34.0	0.2	-1.2	0.4	-46.5	0.1	-22.6
1.000	120.3	6.5	40.2	59.0	-2.0	26.9	-2.3	105.4	-4.9	32.1	-1.0
1.000	120.3	6.5	40.2	58.9	-2.0	26.8	-2.3	105.2	-4.9	31.9	-1.0
1.012	116.4	6.2	38.8	55.5	-2.0	26.0	-2.3	99.8	-4.9	29.8	-1.0
1.024	112.4	6.0	37.5	52.1	-3.1	24.4	-2.3	93.7	-6.4	27.4	-2.1
1.027	111.3	5.9	37.1	51.6	-4.5	23.7	-2.3	92.4	-8.4	27.1	-2.1
1.025	108.6	5.7	36.2	48.8	-4.8	22.9	-2.4	87.7	-8.8	25.3	-3.7
1.040	107.0	5.6	35.6	48.5	-7.2	22.3	-2.6	86.8	-12.1	25.0	-5.0
1.046	104.9	5.5	34.9	45.8	-7.5	21.6	-2.6	82.6	-12.6	23.3	-5.2
1.050	103.7	5.4	34.5	45.8	-7.5	21.6	-2.6	82.6	-12.6	23.3	-5.2
1.050	103.5	5.4	34.4	45.8	-7.5	21.6	-2.6	82.6	-12.6	23.3	-5.2
1.054	102.3	5.3	34.0	45.5	-10.2	21.1	-2.9	81.6	-16.5	23.1	-6.6
1.080	93.8	4.8	31.0	44.3	-15.0	20.1	-3.8	79.1	-23.8	23.7	-9.3
1.081	90.8	4.7	30.7	43.0	-10.3	19.8	-3.2	76.9	-16.9	23.0	-6.1
1.100	84.6	4.4	28.5	38.7	-11.2	18.2	-3.5	69.7	-18.4	20.4	-6.6
1.108	82.0	4.2	27.5	38.3	-11.2	18.4	-3.5	70.7	-18.4	20.9	-6.6
1.135	75.3	3.7	24.4	35.6	-13.9	16.7	-4.3	64.0	-22.9	18.7	-8.4
1.137	72.5	3.6	24.1	32.0	-16.9	15.0	-5.3	57.7	-27.8	16.4	-10.2

BDGS Output - Unit 1 G6

1.150	68.5	3.3	22.7	32.0	-16.9	15.0	-5.3	57.7	-27.8	16.4	-10.2
1.162	64.7	3.1	21.4	29.1	-20.7	13.7	-6.5	52.4	-34.1	14.6	-12.1
1.189	56.2	2.6	18.3	28.3	-23.9	13.1	-7.5	50.7	-39.3	14.1	-13.6
1.195	55.1	2.5	18.7	37.1	-25.2	16.0	-7.9	65.4	-41.4	20.8	-14.4
1.200	53.5	2.4	18.1	37.8	-17.0	15.5	-6.0	63.1	-28.7	19.9	-8.3
1.216	48.5	2.1	16.4	32.6	-18.6	14.3	-6.6	57.7	-31.4	17.7	-9.4
1.230	44.2	1.8	14.8	32.6	-17.8	14.3	-6.4	57.7	-30.2	17.7	-8.8
1.230	44.2	1.8	14.8	32.6	-17.8	14.3	-6.4	57.7	-30.2	17.7	-8.8
1.243	40.0	1.6	13.4	30.7	-22.6	13.0	-7.9	53.9	-37.9	16.5	-12.0
1.250	37.7	1.4	12.6	30.4	-23.0	12.8	-8.1	53.2	-38.7	16.3	-12.3
1.252	37.0	1.4	12.3	30.2	-23.3	12.6	-8.2	52.8	-39.2	16.1	-12.5
1.270	31.4	1.0	10.4	27.8	-23.6	11.9	-8.6	48.9	-39.9	14.6	-12.7
1.297	22.9	0.5	7.2	25.5	-28.4	10.7	-10.5	44.7	-48.2	13.3	-16.2
1.300	21.9	0.4	7.2	25.5	-27.4	10.7	-10.2	44.7	-46.7	13.3	-15.5
1.310	23.4	0.6	8.5	31.9	-29.2	13.1	-10.9	55.6	-49.7	18.5	-16.9
1.324	19.0	0.4	7.0	30.6	-22.0	12.6	-9.3	53.4	-38.6	17.7	-11.4
1.336	16.6	0.3	6.2	28.2	-22.0	11.7	-9.6	49.1	-38.8	16.0	-11.3
1.336	15.2	0.3	5.7	28.2	-22.0	11.7	-9.6	49.1	-38.8	16.0	-11.3
1.341	13.8	0.3	5.2	28.2	-22.0	11.7	-9.6	49.1	-38.8	16.0	-11.3
1.342	13.3	0.2	5.0	28.2	-22.0	11.7	-9.6	49.1	-38.8	16.0	-11.3

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G6.OUT

----- UNFACTORED SHEAR SUMMARY -----

*** GIRDER 13, UNFACTORED SHEAR SUMMARY (Based on Input Section) ***

Note: values do not include impact, except for COMBINED TRUCK+LANE.

SPAN. LOC FRAC	A-DC SHEAR (kips)	DEAD LOAD B-DC SHEAR (kips)	DW SHEAR (kips)	HL93 TRUCK		HL93 LANE		COMBINED TRUCK+LANE		FATIGUE TRUCK	
				MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)
1.350	10.9	0.2	4.2	25.0	-24.8	10.7	-10.8	43.8	-43.8	13.7	-13.4
1.351	10.7	0.2	4.1	26.0	-24.8	10.7	-10.8	43.8	-43.8	14.5	-13.4
1.367	5.6	0.1	2.4	26.3	-25.8	10.2	-11.3	43.8	-45.6	14.0	-14.3
1.378	2.4	0.0	1.3	24.3	-26.5	9.9	-11.7	42.2	-46.9	13.3	-14.9
1.386	0.0	-0.1	0.4	24.3	-25.4	9.9	-11.4	42.2	-45.2	13.3	-14.0
1.400	-4.4	-0.3	-1.1	20.9	-28.1	8.5	-12.9	36.3	-50.3	10.8	-16.3
1.405	-5.8	-0.3	-1.6	21.9	-28.1	8.8	-12.9	38.0	-50.3	11.5	-16.3
1.425	-16.6	-0.7	-4.1	30.2	-30.5	11.7	-13.3	51.8	-54.3	17.8	-18.1
1.425	-18.7	-0.8	-4.9	29.6	-22.3	11.6	-11.2	51.0	-40.9	17.4	-17.7
1.450	-24.2	-1.1	-6.8	25.6	-23.7	10.0	-12.0	44.0	-43.4	14.5	-15.5
1.459	-26.8	-1.2	-7.9	26.6	-23.7	10.3	-12.0	45.6	-43.4	15.3	-15.5
1.482	-33.8	-1.5	-10.4	24.7	-27.3	9.2	-13.2	42.1	-49.6	13.9	-15.1
1.486	-34.8	-1.6	-10.9	24.5	-27.4	9.2	-13.4	41.7	-49.9	13.8	-15.1
1.500	-39.0	-1.8	-12.5	22.6	-27.5	8.5	-13.8	36.9	-50.4	11.7	-15.2
1.513	-42.7	-2.0	-14.0	22.3	-27.5	8.5	-13.8	37.9	-50.4	12.3	-15.2
1.538	-50.2	-2.3	-16.6	19.6	-31.0	7.2	-15.4	33.3	-56.7	10.3	-17.7
1.540	-69.4	-3.1	-20.6	21.5	-32.2	7.2	-16.0	35.8	-58.7	10.4	-18.6
1.550	-72.4	-3.3	-21.8	19.8	-28.7	6.0	-16.1	32.3	-54.3	12.3	-14.6
1.563	-76.0	-3.5	-23.2	17.6	-31.0	5.7	-17.3	28.6	-58.6	10.8	-16.5
1.586	-82.6	-3.8	-25.8	16.1	-32.6	4.7	-18.3	24.1	-61.6	9.7	-17.8
1.597	-85.9	-4.0	-27.1	14.8	-32.7	4.3	-18.6	24.0	-62.1	8.9	-18.0
1.600	-86.8	-4.0	-27.4	14.8	-32.7	4.3	-18.6	24.0	-62.1	8.9	-18.0
1.609	-89.2	-4.1	-28.4	14.1	-33.9	4.0	-19.3	22.8	-64.4	8.4	-19.0
1.632	-95.7	-4.5	-30.9	12.0	-35.1	3.4	-20.5	19.3	-67.2	6.8	-20.2
1.650	-100.9	-4.7	-32.9	12.2	-34.0	3.4	-20.0	19.5	-65.3	6.8	-19.4
1.654	-109.4	-4.8	-35.4	18.5	-36.5	3.0	-21.0	29.6	-69.6	11.8	-21.5
1.655	-109.4	-4.8	-35.4	17.4	-28.7	4.8	-18.3	27.9	-56.5	11.1	-15.1
1.678	-115.9	-5.1	-38.1	17.7	-30.0	3.9	-19.3	23.4	-59.2	9.2	-15.1
1.700	-122.1	-5.4	-41.5	13.9	-31.6	3.5	-20.0	22.0	-62.1	8.6	-17.3
1.701	-122.3	-5.4	-41.7	14.7	-31.6	3.7	-20.0	23.2	-62.1	9.1	-17.3
1.712	-122.3	-5.6	-38.8	13.7	-32.1	3.3	-20.4	21.5	-63.1	8.4	-17.6
1.719	-127.4	-5.7	-39.6	13.0	-32.8	3.1	-20.8	20.4	-64.3	7.9	-18.1
1.719	-127.4	-5.7	-39.6	13.0	-32.8	3.1	-20.8	20.4	-64.3	7.9	-18.1
1.722	-128.2	-5.7	-39.9	13.0	-32.8	3.1	-20.8	20.5	-64.3	7.9	-18.1
1.724	-128.6	-5.8	-40.1	11.4	-33.2	2.7	-21.4	17.9	-65.6	6.7	-18.5
1.747	-135.1	-6.1	-42.6	10.4	-34.9	2.3	-22.4	16.1	-68.9	5.9	-19.7
1.747	-136.1	-6.1	-42.9	10.4	-34.2	2.3	-22.2	16.1	-67.8	5.9	-19.2
1.769	-145.5	-6.5	-45.0	13.7	-36.8	3.2	-23.4	21.4	-72.3	8.6	-21.1
1.770	-145.6	-6.5	-45.1	11.5	-32.5	3.7	-22.9	18.0	-66.1	7.2	-17.2
1.793	-152.7	-6.8	-47.6	11.2	-34.0	2.5	-23.7	17.3	-69.0	7.0	-18.4
1.799	-153.7	-6.9	-48.2	9.9	-34.2	2.1	-24.1	15.3	-69.6	6.3	-18.6
1.800	-154.1	-6.9	-48.3	9.9	-34.2	2.1	-24.1	15.3	-69.6	6.3	-18.6
1.811	-157.1	-7.1	-49.5	9.4	-35.2	1.9	-24.6	14.4	-71.5	6.0	-19.5
1.816	-159.7	-7.1	-50.0	8.3	-35.6	1.7	-25.1	12.8	-72.5	5.7	-19.8
1.828	-162.7	-7.3	-51.2	12.0	-36.3	2.6	-25.5	18.5	-74.0	7.7	-20.5
1.839	-168.3	-7.3	-51.1	9.1	-34.3	1.8	-25.6	14.0	-71.2	5.9	-18.2
1.850	-172.0	-7.4	-52.2	9.1	-33.6	1.8	-25.5	14.0	-70.2	5.9	-17.9
1.857	-174.4	-7.5	-53.0	8.8	-35.8	1.6	-26.3	13.3	-73.9	5.7	-19.4
1.862	-175.9	-7.6	-53.5	6.9	-35.9	1.3	-26.9	10.5	-74.7	4.5	-19.5
1.885	-183.4	-7.9	-55.8	6.8	-37.6	1.3	-27.7	10.4	-77.7	4.4	-21.0
1.887	-183.4	-7.9	-55.9	8.8	-37.7	1.6	-27.8	13.3	-77.9	5.7	-21.0
1.900	-190.2	-7.6	-53.7	6.6	-35.6	1.3	-27.0	11.5	-74.4	4.9	-18.8
1.908	-192.8	-7.7	-54.6	6.5	-37.3	1.3	-28.0	10.0	-77.6	4.2	-20.2
1.916	-195.4	-7.8	-55.2	6.2	-38.0	1.3	-28.5	8.2	-79.1	3.3	-20.8
1.931	-200.2	-8.0	-56.8	6.6	-39.1	1.3	-29.4	6.2	-81.4	2.5	-21.8
1.945	-206.4	-8.2	-58.0	4.1	-40.6	1.5	-29.9	7.0	-83.9	3.1	-21.0
1.950	-207.9	-8.5	-53.7	4.3	-40.1	1.5	-28.9	7.2	-82.3	2.8	-22.4
1.954	-209.2	-7.6	-54.1	2.6	-40.2	1.5	-29.6	5.0	-83.0	1.6	-22.5
1.973	-215.1	-7.8	-55.8	2.4	-42.2	1.5	-30.2	4.8	-86.4	1.4	-24.1
1.977	-216.6	-7.9	-56.3	2.3	-42.6	1.6	-31.1	4.7	-87.7	1.0	-24.4

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G6.OUT

----- UNFACTORED SHEAR SUMMARY -----

*** GIRDER 13, UNFACTORED SHEAR SUMMARY (Based on Input Section) ***

Note: values do not include impact, except for COMBINED TRUCK+LANE.

SPAN. LOC	A-DC	DEAD LOAD B-DC	DW	HL93 TRUCK		HL93 LANE		COMBINED TRUCK+LANE		FATIGUE TRUCK	
				MAX	MIN	MAX	MIN	MAX	MIN	MAX	MIN
N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\Girder design doc\BDGS_G6_output_singpage.doc											

BDGS Output - Unit 1 G6

FRAC	SHEAR (kips)	SHEAR (kips)	SHEAR (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)
1.999	-223.9	-8.2	-58.4	2.3	-45.3	1.6	-32.2	4.7	-92.3	1.0	-26.5
2.000	-223.9	-8.2	-58.5	2.3	-45.4	1.6	-32.2	4.7	-92.5	1.0	-26.5
2.000	148.9	5.6	38.9	44.5	-7.0	28.0	-5.6	87.2	-14.9	25.6	-3.3
2.002	148.4	5.5	38.7	44.3	-7.0	27.9	-5.6	86.9	-14.9	25.5	-3.3
2.010	146.9	5.5	38.2	43.8	-7.0	27.6	-5.6	85.8	-14.9	25.0	-3.3
2.021	145.0	5.4	37.6	42.7	-7.0	27.1	-5.6	83.9	-14.9	24.1	-3.3
2.031	143.1	5.3	36.9	42.0	-7.0	26.6	-5.7	82.4	-14.9	23.5	-3.3
2.041	141.2	5.2	36.3	41.2	-7.0	26.1	-5.7	80.9	-15.0	22.9	-3.3
2.050	139.6	5.1	35.7	40.5	-7.0	25.5	-5.7	79.4	-15.0	22.2	-3.3
2.051	139.3	5.1	35.6	40.6	-7.0	25.5	-5.7	79.5	-15.0	22.2	-3.3
2.053	139.0	5.1	35.4	40.6	-7.0	25.4	-5.7	79.4	-15.0	22.2	-3.3
2.062	137.4	5.0	34.9	39.9	-7.0	25.1	-5.7	78.2	-15.1	21.6	-3.3
2.072	135.5	4.9	34.1	39.3	-7.1	24.5	-5.8	76.8	-15.2	21.0	-3.3
2.082	133.7	4.8	33.4	38.5	-7.1	24.0	-5.8	75.3	-15.3	20.5	-3.3
2.092	131.8	4.7	32.6	37.8	-7.2	23.4	-5.9	73.7	-15.4	19.9	-3.3
2.100	130.4	4.6	31.9	37.3	-7.2	23.0	-5.9	72.6	-15.4	19.5	-3.3
2.103	129.9	4.6	31.8	37.4	-7.2	23.0	-6.0	72.7	-15.6	19.6	-3.3
2.106	129.3	4.5	31.4	40.3	-9.2	22.7	-9.1	76.2	-21.4	20.6	-4.6
2.113	67.4	1.8	12.8	39.1	-9.4	18.3	-9.2	70.3	-21.7	19.9	-4.6
2.123	65.6	1.6	11.9	38.4	-9.4	17.8	-9.4	68.9	-22.0	19.4	-4.7
2.133	63.7	1.5	11.1	37.7	-9.5	17.4	-9.6	67.6	-22.3	18.8	-4.8
2.144	61.8	1.4	10.2	37.1	-9.6	16.9	-9.8	66.3	-22.6	18.4	-4.8
2.150	60.6	1.3	9.5	37.2	-9.6	16.9	-9.8	66.4	-22.6	18.4	-4.8
2.154	59.9	1.3	9.3	37.0	-9.7	16.7	-10.0	66.0	-23.0	18.4	-4.9
2.155	59.6	1.2	9.0	36.5	-9.7	16.4	-10.0	65.0	-23.0	18.1	-4.9
2.164	58.1	1.1	8.4	36.9	-9.8	16.1	-10.3	63.9	-23.3	17.9	-5.0
2.174	56.2	1.0	7.6	35.4	-9.9	15.8	-10.5	62.9	-23.3	17.7	-5.0
2.185	54.3	0.9	6.7	35.0	-10.0	15.4	-10.7	61.9	-24.0	17.6	-5.1
2.195	52.5	0.8	5.9	34.6	-10.1	15.1	-10.8	61.1	-24.3	17.5	-5.2
2.200	51.5	0.7	5.4	34.6	-10.1	15.1	-10.8	61.1	-24.3	17.5	-5.2
2.205	50.7	0.7	5.2	34.6	-10.1	15.1	-10.8	61.1	-24.3	17.5	-5.2
2.205	210.7	9.7	66.1	46.4	-10.1	37.2	-10.8	98.8	-24.3	27.0	-5.6
2.245	202.1	9.3	63.5	42.8	-11.6	35.2	-11.8	92.1	-17.2	24.6	-7.6
2.250	201.0	9.2	62.9	42.1	-11.1	34.7	-11.8	90.7	-16.6	24.0	-7.3
2.255	200.0	9.2	62.5	39.4	-11.8	33.7	-2.0	86.1	-17.7	22.0	-7.7
2.285	193.6	8.9	60.6	38.2	-14.4	32.8	-2.6	83.5	-21.8	21.1	-9.3
2.300	190.3	8.7	59.4	38.2	-13.8	32.5	-2.5	83.3	-20.9	21.1	-8.9
2.305	189.3	8.7	59.1	41.0	-15.7	32.3	-2.9	86.6	-23.8	24.2	-10.0
2.322	171.9	8.1	54.8	39.2	-11.5	30.2	-2.2	82.2	-17.7	22.9	-7.5
2.324	171.5	8.0	54.7	38.9	-12.3	29.9	-2.2	81.6	-18.7	22.8	-7.9
2.350	167.0	7.8	52.9	36.9	-12.2	29.0	-2.3	78.7	-18.7	21.3	-7.9
2.354	166.2	7.7	52.6	36.0	-14.3	28.5	-2.4	76.4	-21.9	20.6	-9.1
2.364	164.5	7.6	52.0	35.3	-15.2	27.4	-3.2	71.6	-23.4	18.6	-9.6
2.400	158.2	7.3	49.5	33.3	-14.4	27.2	-3.0	71.5	-22.2	18.6	-9.1
2.404	157.5	7.3	49.3	38.9	-18.2	26.8	-3.8	75.5	-28.0	23.6	-11.3
2.444	137.4	6.5	44.1	33.6	-14.1	23.8	-3.4	68.5	-22.1	19.8	-8.5
2.450	136.3	6.4	43.6	33.6	-13.4	23.6	-3.4	68.5	-21.1	19.8	-8.5
2.479	131.3	6.2	41.7	32.5	-15.2	23.2	-3.7	66.4	-23.9	19.0	-9.2
2.479	131.3	6.2	41.7	32.5	-15.2	23.2	-3.7	66.4	-23.9	19.0	-9.2
2.483	130.6	6.1	41.4	31.9	-16.1	22.6	-4.0	65.0	-25.4	18.6	-9.9
2.500	127.9	6.0	40.3	31.9	-15.3	22.6	-3.8	65.0	-24.2	18.6	-9.2
2.503	127.3	5.9	40.1	30.0	-16.7	21.9	-4.2	61.8	-26.5	17.2	-10.2
2.523	124.1	5.7	38.8	30.8	-18.1	21.7	-4.6	62.6	-28.7	17.8	-11.3
2.540	119.7	5.5	37.0	28.0	-17.3	20.8	-4.6	58.0	-27.6	15.6	-10.6
2.563	117.6	5.3	36.2	27.3	-20.3	20.0	-5.4	56.3	-32.1	15.1	-12.5
2.600	111.7	5.0	33.7	27.3	-20.7	19.5	-5.7	54.4	-35.2	14.2	-12.9
2.603	111.3	5.0	33.5	31.0	-21.9	19.4	-6.0	60.6	-35.1	19.2	-13.7
2.614	85.4	4.2	28.6	27.7	-15.1	17.5	-4.5	54.3	-24.6	16.7	-8.1
2.642	81.0	4.0	26.9	26.3	-17.3	16.5	-5.2	51.5	-28.3	15.7	-9.8

HNTB BRIDGE DESIGN PROGRAM BDGS VERSION 2.9.1.0 PAGE 51
 RUN TIME: 05/03/2011 13:25:17.893 OUTPUT
 Filename: N:\49633\Bridges\Design\Final Design\Unit 1\BDGS\Revised041411\Clean\2010 LRFD\G6.OUT

UNFACTORED SHEAR SUMMARY

*** GIRDER 13, UNFACTORED SHEAR SUMMARY (Based on Input Section) ***

Note: Values do not include impact, except for COMBINED TRUCK+LANE.

SPAN LOC	A-DC SHEAR (kips)	DEAD LOAD B-DC SHEAR (kips)	DW SHEAR (kips)	HL93 TRUCK		HL93 LANE		COMBINED TRUCK+LANE		FATIGUE TRUCK	
				MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)	MAX (kips)	MIN (kips)
2.650	79.3	3.9	26.1	26.3	-16.5	16.4	-5.0	51.4	-27.0	15.7	-9.1
2.682	74.8	3.6	24.1	24.3	-18.9	15.5	-5.8	47.8	-30.9	14.3	-10.8
2.700	72.0	3.3	22.5	24.3	-18.1	15.3	-5.6	47.6	-29.7	14.3	-10.1
2.702	71.7	3.3	22.4	23.0	-19.3	14.7	-6.1	45.4	-31.7	13.2	-11.0
2.722	68.7	3.1	21.1	21.0	-20.5	14.0	-6.6	42.1	-33.9	11.8	-11.9
2.750	64.4	2.8	18.7	21.0	-19.8	13.6	-6.4	41.6	-32.7	11.8	-11.3
2.762	62.6	2.7	18.0	18.4	-22.2	12.7	-7.5	37.2	-37.0	9.8	-13.1
2.800	56.8	2.2	14.6	17.5	-22.0	12.0	-7.5	35.3	-36.8	9.6	-12.7
2.801	56.6	2.2	15.1	17.5	-33.9	11.8	-19.2	35.1	-64.3	9.6	-16.0
2.841	57.9	-2.4	-19.4	8.2	-39.3	9.6	-23.4	20.4	-75.7	4.0	-18.8
2.850	-59.3	-3.1	-19.9	8.2	-39.3	9.6	-23.4	20.4	-75.7	4.0	-18.8
2.881	-63.8	-3.8	-24.1	8.8	-46.2	10.1	-27.7	21.9	-89.1	4.3	-22.9
2.900	-66.6	-3.9	-25.3	8.8	-46.2	10.1	-27.7	21.9	-89.1	4.3	-22.9
2.921	-69.5	-4.5	-29.0	9.6	-54.5	10.9	-32.6	23.6	-105.1	4.7	-27.3
2.950	-73.8	-4.8	-30.8	9.6	-54.9	10.9	-33.4	23.6	-106.4	4.7	-27.5
2.960	-75.2	-5.1	-33.3	10.2	-63.3	11.6	-38.1	25.2	-122.3	5.0	-32.1
3.000	-80.9	-5.5	-35.7	10.2	-69.2	11.6	-38.9	25.2	-131.0	5.0	-36.1

LOAD COMBINATION TABLES

COMBINATION TABLE: 1 LRFD2009 (Default)

#	NAME	CATEGORY	LOAD FACTORS					-IMPACT TRK	FACT-LN	-ENVELOPE-MOM	SHR
			A-DL	B-DL	DW-DL	LL	NU				
1	DC CONSTRUCTIBILITY	STRENGTH-IV	1.500	0.000	0.000	0.000	1.050	0.000	0.000	NONE	
2	DC+DW CONSTRUCTIBILITY	STRENGTH-IV	1.500	1.500	1.500	0.000	1.050	0.000	0.000	NONE	
3	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	MOM-MAX	
4	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	MOM-MIN	
5	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	SHR-MAX	
6	STRENGTH-I MAX-LF	STRENGTH-I	1.250	1.250	1.500	1.750	1.050	1.330	1.000	SHR-MIN	
7	STRENGTH-I MIN-LF	STRENGTH-I	0.900	0.900	0.650	1.750	0.952	1.330	1.000	MOM-MAX	

Made	DSB	Date	5/22/2011	Job Number	49633
Checked	MPM	Date	5/27/2011		
Backchk'd	DSB	Date	5/27/2011	Sheet No.	

For **Cleveland Innerbelt**

End Diaphragm Design G4 Unit 1

The end diaphragm at the end of stub girder will be an I-section and will be designed as a simple span beam in between the adjacent girders. Design as a non-composite section.

Stub Girder End Shear

DC =	173.9	kip
DW =	61.6	kip
LL truck (no impact) =	72.2	kip
LL truck range (no impact) =	41.3	kip
LL lane =	42.6	kip
Importance Factor =	1.05	
V_u =	580.0	kip (Strength I)
V_u =	436.5	kip (Service II)
V_u =	74.8	kip (Fatigue I)

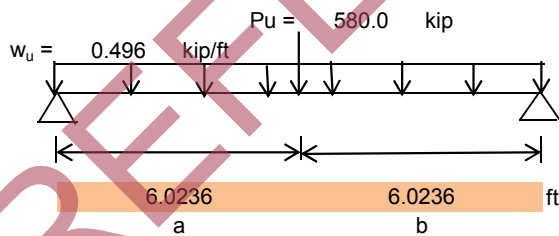
End Diaphragm Section Properties

	b (in)	t (in)	A (in ²)	y (in)	Ay (in ³)
Top	24.0	1.00	24.00	85.50	2052.0
Web	0.750	84	63.00	43.00	2709.0
Bottom	24.0	1.00	24.00	0.50	12.0

	d (in)	lo (in ⁴)	A*d ² (in ⁴)
Top	42.50	2.0	43350.0
Web	0.00	37044.0	0.0
Bottom	-42.50	2.0	43350.0

A =	111.00	in ²
y _{bot} =	43.00	in
I =	123748	in ⁴
S _{bot} =	2877.9	in ³
S _{top} =	2877.9	in ³
w =	0.378	k/ft

Design Moment and Stress



$M_{ii} = P_u * a * b / (a+b) + w_{ii} * (a+b)^2 / 8 =$	1755.8	kip-ft
$f_{bu \text{ top}} =$	7.32	ksi (compression)
$f_{bu \text{ bot}} =$	7.32	ksi (tension)
$V_{u \text{ max}} =$	293.0	kip (Strength I)
$V_{u \text{ max}} =$	220.6	kip (Service II)
$V_{u \text{ max}} =$	37.4	kip (Fatigue I)

Material Properties

$F_y =$	50	ksi
$E =$	29000	ksi
$F_u =$	65	ksi

(6.4.1-1)

Tension Flange Flexural Resistance (6.10.8.1.2, 6.10.8.3)

$$F_{nt} = R_h * F_{yt}$$

$$R_h = 1.0 \quad (6.10.1.10)$$

$$F_{nt} = 50.0 \text{ ksi}$$

$$\phi_f = 1.00 \quad (6.5.4.2)$$

$$\phi_f F_{nt} = 50.0 \text{ ksi}$$

$$f_{bu} + 1/3 * f_t = 7.32 \text{ ksi}$$

Factored Stress < Capacity, OK

Compression Flange Flexural Resistance (6.10.8.1.1, 6.10.8.2)

Local Buckling Resistance (10.8.2.2)

$$\lambda_{nf} = 0.38 * (E/F_{vc})^{0.5} = 9.15 \quad (6.10.8.2.2-4)$$

$$\lambda_{rf} = 0.56 * (E/F_{vc})^{0.5} = 13.49 \quad (6.10.8.2.2-5)$$

$$\lambda_f = b_{fc} / (2t_{fc}) = 12.0 \quad (6.10.8.2.2-3)$$

If $\lambda_f \leq \lambda_{pf}$

$$F_{nc} = R_b * R_h * F_{yc} \quad (6.10.8.2.2-1)$$

Otherwise

$$F_{nc} = [1 - (1 - F_{yr} / (R_h * F_{yc})) * (\lambda_f - \lambda_{pf}) / (\lambda_{rf} - \lambda_{pf})] * R_b * R_h * F_{yc} \quad (6.10.8.2.2-2)$$

$$R_b = 1.0 \quad (6.10.1.10)$$

$$F_{yr} = 0.7 * F_{yc} = 35.0 \text{ ksi}$$

$$F_{nc} = 40.14 \text{ ksi}$$

Lateral Torsional Buckling Resistance (10.8.2.3)

$$D_c = 42.00 \text{ in}$$

$$r_t = b_{fc} / ((12 * (1 + 1/3 * D_c * t_w / (b_{fc} * t_{fc})))^{0.5}) = 5.78 \text{ in} \quad (6.10.8.2.3-9)$$

$$L_n = 1.0 * r_t * (E/F_{vc})^{0.5} = 139.2 \text{ in} \quad (6.10.8.2.3-4)$$

$$L_r = \pi * r_t * (E/F_{vc})^{0.5} = 437.2 \text{ in} \quad (6.10.8.2.3-5)$$

$$L_b = 72.3 \text{ in}$$

If $L_b \leq L_p$

$$F_{nc} = R_b * R_h * F_{yc} \quad (6.10.8.2.3-1)$$

If $L_p < L_b \leq L_r$

$$F_{nc} = C_b * [1 - (1 - F_{yr} / (R_h * F_{yc})) * (L_b - L_p) / (L_r - L_p)] * R_b * R_h * F_{yc} \quad (6.10.8.2.3-2)$$

$$\leq R_b * R_h * F_{yc}$$

If $L_b > L_r$

$$F_{nc} = F_{cr} \leq R_b * R_h * F_{yc} \quad (6.10.8.2.3-3)$$

$$C_b = 1.0 \quad (\text{conservative assumption})$$

$$F_{cr} = C_b * R_b * \pi^2 * E / (L_b / r_t)^2 = 1829.2 \text{ ksi} \quad (6.10.8.2.3-8)$$

$$F_{nc} = 50.0 \text{ ksi}$$

HNTB	The HNTB Companies Engineers Architects Planners	Made	DSB	Date	5/22/2011	Job Number	49633
		Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backch'kd	DSB	Date	5/27/2011	Sheet No.	

**End Diaphragm Design G4
Unit 1**

Controlling Compressive Resistance

$$F_{nc} = 40.14 \text{ ksi}$$

$$\phi_r = 1.00 \quad (6.5.4.2)$$

$$\phi_r F_{nc} = 40.1 \text{ ksi}$$

$$f_{bu} + 1/3 * f_t = 7.32 \text{ ksi}$$

Factored Stress < Capacity, OK

CONNECTION DESIGN

Stub Girder End

Design Force (6.13.1)

$$\phi_v = 1.00 \quad (6.5.4.2)$$

$$\text{Stub girder } t_w = 0.69 \text{ in}$$

$$\text{Stub girder } D = 84.0 \text{ in}$$

$$\text{Stiffener spacing, } d_o = 90.5 \text{ in}$$

$$k = 9.31$$

$$D/t_w = 122.2$$

$$1.12 * (E * k / F_{vw})^{0.5} = 82.3$$

$$1.40 * (E * k / F_{vw})^{0.5} = 102.9$$

$$C = 0.568$$

$$V_p = 0.58 * F_{yw} * D * t_w = 1674.8 \text{ kip} \quad (6.10.9.2-2)$$

$$V_n = C * V_p = 950.8 \text{ kip} \quad (6.10.9.2-1)$$

$$\phi V_n = 950.8 \text{ kip}$$

Strength I Case Only

If $V_u < 0.75 \phi_v V_n$

$$V_{uw} = 0.75 * \phi_v V_n \quad (6.13.6.1.4b-1)$$

Otherwise

$$V_{uw} = (V_u + \phi_v V_n) / 2 \quad (6.13.6.1.4b-2)$$

$$V_{uw} = 713.1 \text{ kip (Strength I)}$$

$$V_{uw} = 436.5 \text{ kip (Service II)}$$

$$V_{uw} = 74.8 \text{ kip (Fatigue I)}$$

Bolt Properties

$$\text{A325 Bolt diameter, } D_b = 1.00 \text{ in}$$

$$\text{Hole diameter} = 1.125 \text{ in}$$

$$\text{A325 Bolt area, } A_b = 0.79 \text{ in}^2$$

$$F_{ub} = 120.00 \text{ ksi}$$

Girder Web Connection

$$n_{col} = 5$$

$$n_{row} = 10$$

$$d_{edge} = 2.00 \text{ in}$$

$$spa_{col} = 4.00 \text{ in}$$

$$spa_{row} = 7.00 \text{ in}$$

$$\text{Connecting angle thickness} = 0.75 \text{ in}$$

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

Angles on either side of the connection gives 2 shear planes.

$$R_n = 0.38 * A_b * F_{ub} * N_s \quad (6.13.2.7-2)$$

$$N_s = 2$$

$$R_n \text{ (per bolt)} = 71.63 \text{ kip}$$

$$\text{Number of bolts} = 50$$

$$R_n \text{ (entire connection)} = 3581.4 \text{ kip}$$

$$\phi_s = 0.80 \quad (6.5.4.2)$$

$$\phi_s R_n = 2865.1 \text{ kip}$$

$$R_u = 713.12 \text{ kip}$$

Factored Load < Capacity, OK

Bolt Slip Resistance (6.13.2.8)

Assume standard holes and Class B surface.

$$R_n = K_h * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$$K_h = 1.00 \quad (\text{Table 6.13.2.8-2})$$

$$K_s = 0.50 \quad (\text{Table 6.13.2.8-3})$$

$$N_s = 2$$

$$P_t = 51 \text{ kip} \quad (\text{Table 6.13.2.8-1})$$

$$R_n \text{ (per bolt)} = 51.00 \text{ kip}$$

$$\text{Number of bolts} = 50.00$$

$$R_n \text{ (entire connection)} = 2550.00 \text{ kip}$$

$$\phi_s = 0.80 \quad (6.5.4.2)$$

$$\phi_s R_n = 2040.0 \text{ kip}$$

$$R_u = 436.50 \text{ kip}$$

Factored Load < Capacity, OK

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

Conservatively designed per 6.13.6.1.4b rather than actual loads.

ksi (Table 6.6.1.2.5-3)

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0$$

$$A_b = 0.79 \text{ in}^2$$

$$\text{Number of bolts} = 50.00$$

$$N_s = 2$$

$$R_u = 74.8 \text{ kip}$$

$$v(\Delta f) = 0.95 \text{ ksi}$$

Factored Load < Capacity, OK

HNTB	The HNTB Companies Engineers Architects Planners	Made	DSB	Date	5/22/2011	Job Number	49633
		Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backchk'd	DSB	Date	5/27/2011	Sheet No.	

End Diaphragm Design G4
Unit 1

Bolt Bearing Resistance (6.13.2.9)

-With bolts spaced at a clear distance between holes not less than 2.0d and with a clear end distance not less than 2.0d:

$$R_n = 2.4 \cdot d \cdot t \cdot F_u \quad (6.13.2.9-1)$$

-With either the clear distance between holes is less than 2.0d, or the clear end distance is less than 2.0d:

$$R_n = 1.2 \cdot L_c \cdot t \cdot F_u \quad (6.13.2.9-2)$$

$$L_{c \text{ int}} = 5.875 \text{ in } \geq 2.0d$$

$$L_{c \text{ end}} = 1.438 \text{ in } < 2.0d$$

Equation to use: 6.13.2.9-2

Controlling thickness, t = 0.688 in (web)

$$R_n = 5211.68 \text{ kip}$$

$$\phi_{bb} = 0.80 \quad (6.5.4.2)$$

$$\phi_{bb} R_n = 4169.3 \text{ kip}$$

$$R_u = 713.12 \text{ kip}$$

Factored Load < Capacity, OK

Connecting Angle Shear (6.13.5.3)

Shear Yielding

$$R_r = \phi_v \cdot 0.58 \cdot F_y \cdot A_g \quad (6.13.5.3-1)$$

$$\text{Length} = 67.0 \text{ in}$$

$$A_g \text{ (2 angles)} = 100.5 \text{ in}^2$$

$$\phi_v = 1.00 \quad (6.5.4.2)$$

$$R_r = 2914.5 \text{ kip}$$

$$R_u = 713.12 \text{ kip}$$

Factored Load < Capacity, OK

Shear Rupture

$$R_r = \phi_{vu} \cdot 0.58 \cdot R_p \cdot F_u \cdot A_{vn} \quad (6.13.5.3-2)$$

$$R_p = 0.90 \text{ Assume punched full sized}$$

$$A_{vn} = 83.6 \text{ in}^2$$

$$\phi_{vu} = 0.80 \quad (6.5.4.2)$$

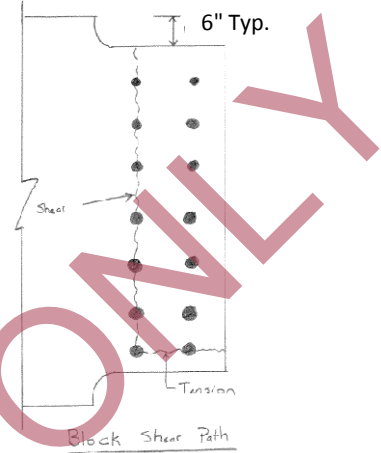
$$R_r = 2269.9 \text{ kip}$$

$$R_u = 713.12 \text{ kip}$$

Factored Load < Capacity, OK

Coped Beam End Block Shear (6.13.4)

Consider beam end and connecting plates



$$R_r = \phi_{bs} \cdot R_p \cdot (0.58 \cdot F_u \cdot A_{vn} + U_{bs} \cdot F_u \cdot A_{tn})$$

$$\leq \phi_{bs} \cdot R_p \cdot (0.58 \cdot F_y \cdot A_{vg} + U_{bs} \cdot F_u \cdot A_{tn}) \quad (6.13.4-1)$$

$$A_{vg} = 46.41 \text{ in}^2$$

$$A_{vn} = 39.06 \text{ in}^2$$

$$A_{tn} = 8.89 \text{ in}^2$$

$$U_{bs} = 0.5$$

$$\phi_{bs} = 0.80 \quad (6.5.4.2)$$

$$\phi_{bs} \cdot R_p \cdot (0.58 \cdot F_u \cdot A_{vn} + U_{bs} \cdot F_u \cdot A_{tn}) = 1268.3 \text{ kip}$$

$$\phi_{bs} \cdot R_p \cdot (0.58 \cdot F_y \cdot A_{vg} + U_{bs} \cdot F_u \cdot A_{tn}) = 1177.1 \text{ kip}$$

$$R_r = 1177.1 \text{ kip}$$

$$R_u = 713.12 \text{ kip}$$

Factored Load < Capacity, OK

Diaphragm Web Connection

Determine number of bolts required based on bolt shear resistance. Each connection will take 1/2 of the design force. Detail bolts in 2 rows. The row closest to the stub girder web will have no bolts in the outside thirds of the connecting angles to allow flexibility in the joint.

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

$$R_n = 0.38 \cdot A_b \cdot F_{ub} \cdot N_s \quad (6.13.2.7-2)$$

$$N_s = 1$$

$$R_n \text{ (per bolt)} = 35.81 \text{ kip}$$

$$\phi_s = 0.80 \quad (6.5.4.2)$$

$$\phi_s R_n \text{ (per bolt)} = 28.7 \text{ kip}$$

$$R_u = 356.6 \text{ kip}$$

Min. Number of bolts required = 13

HNTB The HNTB Companies For Cleveland Innerbelt	Made DSB	Date 5/22/2011	Job Number 49633
	Checked MPM	Date 5/27/2011	
	Backch'k'd DSB	Date 5/27/2011	Sheet No.

End Diaphragm Design G4
Unit 1

Bolt Slip Resistance (6.13.2.8)

$$R_n = K_n * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$K_n = 1.00$ (Table 6.13.2.8-2)
 $K_s = 0.50$ (Table 6.13.2.8-3)
 $N_s = 1$
 $P_t = 51$ kip (Table 6.13.2.8-1)
 R_n (per bolt) = 25.50 kip
 $\phi_s = 0.80$
 $\phi_s R_n$ (per bolt) = 20.40 kip
 $R_u = 218.2$ kip
 Min. Number of bolts required = 11

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0 \text{ ksi (Table 6.6.1.2.5-3)}$$

$$A_b = 0.79 \text{ in}^2$$

$$R_u = 37.4 \text{ kip}$$

Min. Number of bolts required = 3

Stub girder span length, $L = 101.10$ ft
 Required gage = $(L * t/8)^{0.5} = 10.66$ in

End Diaphragm Connection to Girder Web

Design Force (6.13.1)

$$\phi_v = 1.00 \quad (6.5.4.2)$$

Diaphragm $t_w = 0.75$ in
 Diaphragm $D = 84.0$ in
 $k = 5.0$ (assume unstiffened web)
 $D/t_w = 112.0$

$$1.12 * (E * k / F_{vw})^{0.5} = 60.3$$

$$1.40 * (E * k / F_{vw})^{0.5} = 75.4$$

$C = 0.363$
 $V_p = 0.58 * F_{yw} * D * t_w = 1827.0$ kip (6.10.9.2-2)
 $V_n = C * V_p = 663.1$ kip (6.10.9.2-1)
 $\phi V_n = 663.1$ kip

Strength I Case Only

If $V_u < 0.75 \phi_v V_n$
 $V_{uw} = 0.75 * \phi_v V_n$ (6.13.6.1.4b-1)

Otherwise
 $V_{uw} = (V_u + \phi_v V_n) / 2$ (6.13.6.1.4b-2)

$V_{uw} = 497.3$ kip (Strength I)
 $V_{uw} = 220.6$ kip (Strength I)
 $V_{uw} = 37.4$ kip (Fatigue I)

Determine number of bolts based on bolt shear resistance

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

$$R_n = 0.38 * A_b * F_{ub} * N_s \quad (6.13.2.7-2)$$

$N_s = 1$
 R_n (per bolt) = 35.81 kip
 $\phi_s = 0.80$ (6.5.4.2)
 $\phi_s R_n$ (per bolt) = 28.7 kip
 $R_u = 497.3$ kip
 Min. Number of bolts required = 18

Bolt Slip Resistance (6.13.2.8)

Assume oversized holes and Class B surface.

$$R_n = K_n * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$K_n = 0.85$ (Table 6.13.2.8-2)
 $K_s = 0.50$ (Table 6.13.2.8-3)
 $N_s = 1$
 $P_t = 51$ kip (Table 6.13.2.8-1)
 R_n (per bolt) = 21.68 kip
 $\phi_s = 0.80$
 $\phi_s R_n$ (per bolt) = 17.34 kip
 $R_u = 220.6$ kip

Min. Number of bolts required = 13

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0 \text{ ksi (Table 6.6.1.2.5-3)}$$

$$A_b = 0.79 \text{ in}^2$$

Min. number of bolts required = 3

Made	DSB	Date	5/22/2011	Job Number	49633
Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backchk'd	DSB	Date	5/27/2011
				Sheet No.	

End Diaphragm Design G5 Unit 1

The end diaphragm at the end of stub girder will be an I-section and will be designed as a simple span beam in between the adjacent girders. Design as a non-composite section.

Stub Girder End Shear

DC =	437.8	kip
DW =	140.3	kip
LL truck (no impact) =	37.5	kip
LL truck range (no impact) =	34.8	kip
LL lane =	68.1	kip
Importance Factor =	1.05	
V_u =	1012.4	kip (Strength I)
V_u =	768.0	kip (Service II)
V_u =	63.0	kip (Fatigue I)

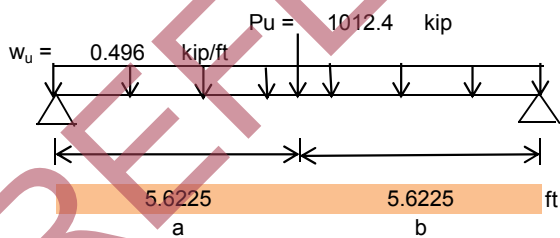
End Diaphragm Section Properties

	b (in)	t (in)	A (in ²)	y (in)	Ay (in ³)
Top	24.0	1.00	24.00	85.50	2052.0
Web	0.750	84	63.00	43.00	2709.0
Bottom	24.0	1.00	24.00	0.50	12.0

	d (in)	lo (in ⁴)	A*d ² (in ⁴)
Top	42.50	2.0	43350.0
Web	0.00	37044.0	0.0
Bottom	-42.50	2.0	43350.0

A =	111.00	in ²
y _{bot} =	43.00	in
I =	123748	in ⁴
S _{bot} =	2877.9	in ³
S _{top} =	2877.9	in ³
w =	0.378	k/ft

Design Moment and Stress



$M_{ii} = P_u * a * b / (a+b) + w_{ii} * (a+b)^2 / 8 =$	2853.8	kip-ft
$f_{bu \text{ top}} =$	11.90	ksi (compression)
$f_{bu \text{ bot}} =$	11.90	ksi (tension)
$V_{u \text{ max}} =$	509.0	kip (Strength I)
$V_{u \text{ max}} =$	386.3	kip (Service II)
$V_{u \text{ max}} =$	31.5	kip (Fatigue I)

Material Properties

$F_y =$	50	ksi
$E =$	29000	ksi
$F_u =$	65	ksi

(6.4.1-1)

Tension Flange Flexural Resistance (6.10.8.1.2, 6.10.8.3)

$$F_{nt} = R_h * F_{yt}$$

$$R_h = 1.0 \quad (6.10.1.10)$$

$$F_{nt} = 50.0 \text{ ksi}$$

$$\phi_f = 1.00 \quad (6.5.4.2)$$

$$\phi_f F_{nt} = 50.0 \text{ ksi}$$

$$f_{bu} + 1/3 * f_t = 11.90 \text{ ksi}$$

Factored Stress < Capacity, OK

Compression Flange Flexural Resistance (6.10.8.1.1, 6.10.8.2)

Local Buckling Resistance (10.8.2.2)

$$\lambda_{nf} = 0.38 * (E/F_{vc})^{0.5} = 9.15 \quad (6.10.8.2.2-4)$$

$$\lambda_{rf} = 0.56 * (E/F_{vc})^{0.5} = 13.49 \quad (6.10.8.2.2-5)$$

$$\lambda_f = b_{fc} / (2t_{fc}) = 12.0 \quad (6.10.8.2.2-3)$$

If $\lambda_f \leq \lambda_{pf}$

$$F_{nc} = R_b * R_h * F_{yc} \quad (6.10.8.2.2-1)$$

Otherwise

$$F_{nc} = [1 - (1 - F_{yr} / (R_h * F_{yc})) * (\lambda_f - \lambda_{pf}) / (\lambda_{rf} - \lambda_{pf})] * R_b * R_h * F_{yc} \quad (6.10.8.2.2-2)$$

$$R_b = 1.0 \quad (6.10.1.10)$$

$$F_{yr} = 0.7 * F_{yc} = 35.0 \text{ ksi}$$

$$F_{nc} = 40.14 \text{ ksi}$$

Lateral Torsional Buckling Resistance (10.8.2.3)

$$D_c = 42.00 \text{ in}$$

$$r_t = b_{fc} / ((12 * (1 + 1/3 * D_c * t_w / (b_{fc} * t_{fc})))^{0.5}) = 5.78 \text{ in} \quad (6.10.8.2.3-9)$$

$$L_n = 1.0 * r_t * (E/F_{vc})^{0.5} = 139.2 \text{ in} \quad (6.10.8.2.3-4)$$

$$L_r = \pi * r_t * (E/F_{vc})^{0.5} = 437.2 \text{ in} \quad (6.10.8.2.3-5)$$

$$L_b = 67.5 \text{ in}$$

If $L_b \leq L_p$

$$F_{nc} = R_b * R_h * F_{yc} \quad (6.10.8.2.3-1)$$

If $L_p < L_b \leq L_r$

$$F_{nc} = C_b * [1 - (1 - F_{yr} / (R_h * F_{yc})) * (L_b - L_p) / (L_r - L_p)] * R_b * R_h * F_{yc} \quad (6.10.8.2.3-2)$$

$$\leq R_b * R_h * F_{yc}$$

If $L_b > L_r$

$$F_{nc} = F_{cr} \leq R_b * R_h * F_{yc} \quad (6.10.8.2.3-3)$$

$$C_b = 1.0 \quad (\text{conservative assumption})$$

$$F_{cr} = C_b * R_b * \pi^2 * E / (L_b / r_t)^2 = 2099.5 \text{ ksi} \quad (6.10.8.2.3-8)$$

$$F_{nc} = 50.0 \text{ ksi}$$

HNTB	The HNTB Companies Engineers Architects Planners	Made	DSB	Date	5/22/2011	Job Number	49633
		Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backch'kd	DSB	Date	5/27/2011	Sheet No.	

End Diaphragm Design G5
Unit 1

Controlling Compressive Resistance

$$F_{nc} = 40.14 \text{ ksi}$$

$$\phi_r = 1.00 \quad (6.5.4.2)$$

$$\phi_r F_{nc} = 40.1 \text{ ksi}$$

$$f_{bu} + 1/3 * f_i = 11.90 \text{ ksi}$$

Factored Stress < Capacity, OK

CONNECTION DESIGN

Stub Girder End

Design Force (6.13.1)

$$\phi_v = 1.00 \quad (6.5.4.2)$$

$$\text{Stub girder } t_w = 0.69 \text{ in}$$

$$\text{Stub girder } D = 84.0 \text{ in}$$

$$\text{Stiffener spacing, } d_o = 68.5 \text{ in}$$

$$k = 12.52$$

$$D/t_w = 122.2$$

$$1.12 * (E * k / F_{vw})^{0.5} = 95.4$$

$$1.40 * (E * k / F_{vw})^{0.5} = 119.3$$

$$C = 0.764$$

$$V_p = 0.58 * F_{yw} * D * t_w = 1674.8 \text{ kip} \quad (6.10.9.2-2)$$

$$V_n = C * V_p = 1278.9 \text{ kip} \quad (6.10.9.2-1)$$

$$\phi V_n = 1278.9 \text{ kip}$$

Strength I Case Only

If $V_u < 0.75 \phi_v V_n$

$$V_{uw} = 0.75 * \phi_v V_n \quad (6.13.6.1.4b-1)$$

Otherwise

$$V_{uw} = (V_u + \phi_v V_n) / 2 \quad (6.13.6.1.4b-2)$$

$$V_{uw} = 1145.6 \text{ kip (Strength I)}$$

$$V_{uw} = 768.0 \text{ kip (Service II)}$$

$$V_{uw} = 63.0 \text{ kip (Fatigue I)}$$

Bolt Properties

$$\text{A325 Bolt diameter, } D_b = 1.00 \text{ in}$$

$$\text{Hole diameter} = 1.125 \text{ in}$$

$$\text{A325 Bolt area, } A_b = 0.79 \text{ in}^2$$

$$F_{ub} = 120.00 \text{ ksi}$$

Girder Web Connection

$$n_{col} = 5$$

$$n_{row} = 10$$

$$d_{edge} = 2.00 \text{ in}$$

$$spa_{col} = 4.00 \text{ in}$$

$$spa_{row} = 7.00 \text{ in}$$

$$\text{Connecting angle thickness} = 0.75 \text{ in}$$

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

Angles on either side of the connection gives 2 shear planes.

$$R_n = 0.38 * A_b * F_{ub} * N_s \quad (6.13.2.7-2)$$

$$N_s = 2$$

$$R_n \text{ (per bolt)} = 71.63 \text{ kip}$$

$$\text{Number of bolts} = 50$$

$$R_n \text{ (entire connection)} = 3581.4 \text{ kip}$$

$$\phi_s = 0.80 \quad (6.5.4.2)$$

$$\phi_s R_n = 2865.1 \text{ kip}$$

$$R_u = 1145.62 \text{ kip}$$

Factored Load < Capacity, OK

Bolt Slip Resistance (6.13.2.8)

Assume standard holes and Class B surface.

$$R_n = K_h * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$$K_h = 1.00 \quad (\text{Table 6.13.2.8-2})$$

$$K_s = 0.50 \quad (\text{Table 6.13.2.8-3})$$

$$N_s = 2$$

$$P_t = 51 \text{ kip} \quad (\text{Table 6.13.2.8-1})$$

$$R_n \text{ (per bolt)} = 51.00 \text{ kip}$$

$$\text{Number of bolts} = 50.00$$

$$R_n \text{ (entire connection)} = 2550.00 \text{ kip}$$

$$\phi_s = 0.80 \quad (6.5.4.2)$$

$$\phi_s R_n = 2040.0 \text{ kip}$$

$$R_u = 768.04 \text{ kip}$$

Factored Load < Capacity, OK

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

Conservatively designed per 6.13.6.1.4b rather than actual loads.

ksi (Table 6.6.1.2.5-3)

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0$$

$$A_b = 0.79 \text{ in}^2$$

$$\text{Number of bolts} = 50.00$$

$$N_s = 2$$

$$R_u = 63.0 \text{ kip}$$

$$v(\Delta f) = 0.80 \text{ ksi}$$

Factored Load < Capacity, OK

HNTB	The HNTB Companies Engineers Architects Planners	Made	DSB	Date	5/22/2011	Job Number	49633
		Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backchk'd	DSB	Date	5/27/2011	Sheet No.	

End Diaphragm Design G5
Unit 1

Bolt Bearing Resistance (6.13.2.9)

-With bolts spaced at a clear distance between holes not less than 2.0d and with a clear end distance not less than 2.0d:

$$R_n = 2.4*d*t*F_u \quad (6.13.2.9-1)$$

-With either the clear distance between holes is less than 2.0d, or the clear end distance is less than 2.0d:

$$R_n = 1.2*L_c*t*F_u \quad (6.13.2.9-2)$$

$$L_{c\text{int}} = 5.875 \text{ in } \geq 2.0d$$

$$L_{c\text{end}} = 1.438 \text{ in } < 2.0d$$

Equation to use: 6.13.2.9-2

Controlling thickness, t = 0.688 in (web)

$$R_n = 5211.68 \text{ kip}$$

$$\phi_{bb} = 0.80 \quad (6.5.4.2)$$

$$\phi_{bb}R_n = 4169.3 \text{ kip}$$

$$R_u = 1145.62 \text{ kip}$$

Factored Load < Capacity, OK

Connecting Angle Shear (6.13.5.3)

Shear Yielding

$$R_r = \phi_v*0.58*F_y*A_g \quad (6.13.5.3-1)$$

$$\text{Length} = 67.0 \text{ in}$$

$$A_g \text{ (2 angles)} = 100.5 \text{ in}^2$$

$$\phi_v = 1.00 \quad (6.5.4.2)$$

$$R_r = 2914.5 \text{ kip}$$

$$R_u = 1145.62 \text{ kip}$$

Factored Load < Capacity, OK

Shear Rupture

$$R_r = \phi_{vu}*0.58*R_p*F_u*A_{vn} \quad (6.13.5.3-2)$$

$$R_p = 0.90 \text{ Assume punched full sized}$$

$$A_{vn} = 83.6 \text{ in}^2$$

$$\phi_{vu} = 0.80 \quad (6.5.4.2)$$

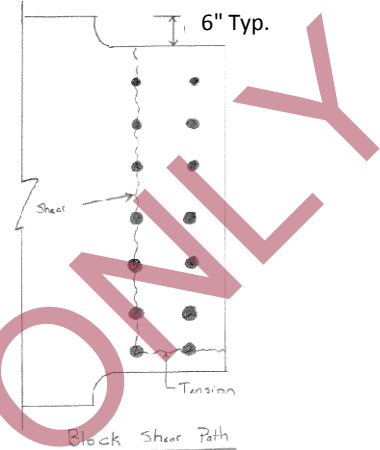
$$R_r = 2269.9 \text{ kip}$$

$$R_u = 1145.62 \text{ kip}$$

Factored Load < Capacity, OK

Coped Beam End Block Shear (6.13.4)

Consider beam end and connecting plates



$$R_r = \phi_{bs}*R_p*(0.58*F_u*A_{vn} + U_{bs}*F_u*A_{tn})$$

$$\leq \phi_{bs}*R_p*(0.58*F_y*A_{vg} + U_{bs}*F_u*A_{tn}) \quad (6.13.4-1)$$

$$A_{vg} = 46.41 \text{ in}^2$$

$$A_{vn} = 39.06 \text{ in}^2$$

$$A_{tn} = 8.89 \text{ in}^2$$

$$U_{bs} = 0.5$$

$$\phi_{bs} = 0.80 \quad (6.5.4.2)$$

$$\phi_{bs}*R_p*(0.58*F_u*A_{vn} + U_{bs}*F_u*A_{tn}) = 1268.3 \text{ kip}$$

$$\phi_{bs}*R_p*(0.58*F_y*A_{vg} + U_{bs}*F_u*A_{tn}) = 1177.1 \text{ kip}$$

$$R_r = 1177.1 \text{ kip}$$

$$R_u = 1145.62 \text{ kip}$$

Factored Load < Capacity, OK

Diaphragm Web Connection

Determine number of bolts required based on bolt shear resistance. Each connection will take 1/2 of the design force. Detail bolts in 2 rows. The row closest to the stub girder web will have no bolts in the outside thirds of the connecting angles to allow flexibility in the joint.

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

$$R_n = 0.38*A_b*F_{ub}*N_s \quad (6.13.2.7-2)$$

$$N_s = 1$$

$$R_n \text{ (per bolt)} = 35.81 \text{ kip}$$

$$\phi_s = 0.80 \quad (6.5.4.2)$$

$$\phi_s R_n \text{ (per bolt)} = 28.7 \text{ kip}$$

$$R_u = 572.8 \text{ kip}$$

Min. Number of bolts required = 20

HNTB	The HNTB Companies	Made	DSB	Date	5/22/2011	Job Number	49633
		Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backch'k'd	DSB	Date	5/27/2011	Sheet No.	

End Diaphragm Design G5
Unit 1

Bolt Slip Resistance (6.13.2.8)

$$R_n = K_n * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$K_n = 1.00$ (Table 6.13.2.8-2)
 $K_s = 0.50$ (Table 6.13.2.8-3)
 $N_s = 1$
 $P_t = 51$ kip (Table 6.13.2.8-1)
 R_n (per bolt) = 25.50 kip
 $\phi_s = 0.80$
 $\phi_s R_n$ (per bolt) = 20.40 kip
 $R_u = 384.0$ kip
 Min. Number of bolts required = 19

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0 \text{ ksi (Table 6.6.1.2.5-3)}$$

$$A_b = 0.79 \text{ in}^2$$

$$R_u = 31.5 \text{ kip}$$

Min. Number of bolts required = 3

Stub girder span length, $L = 23.69$ ft
 Required gage = $(L * t/8)^{0.5} = 5.16$ in

End Diaphragm Connection to Girder Web

Design Force (6.13.1)

$$\phi_v = 1.00 \quad (6.5.4.2)$$

Diaphragm $t_w = 0.75$ in
 Diaphragm $D = 84.0$ in
 $k = 5.0$ (assume unstiffened web)
 $D/t_w = 112.0$

$$1.12 * (E * k / F_{vw})^{0.5} = 60.3$$

$$1.40 * (E * k / F_{vw})^{0.5} = 75.4$$

$C = 0.363$
 $V_p = 0.58 * F_{yw} * D * t_w = 1827.0$ kip (6.10.9.2-2)
 $V_n = C * V_p = 663.1$ kip (6.10.9.2-1)
 $\phi V_n = 663.1$ kip

Strength I Case Only

If $V_u < 0.75 \phi_v V_n$

$$V_{uw} = 0.75 * \phi_v V_n \quad (6.13.6.1.4b-1)$$

Otherwise

$$V_{uw} = (V_u + \phi_v V_n) / 2 \quad (6.13.6.1.4b-2)$$

$V_{uw} = 586.1$ kip (Strength I)
 $V_{uw} = 386.3$ kip (Strength I)
 $V_{uw} = 31.5$ kip (Fatigue I)

Determine number of bolts based on bolt shear resistance

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

$$R_n = 0.38 * A_b * F_{ub} * N_s \quad (6.13.2.7-2)$$

$N_s = 1$
 R_n (per bolt) = 35.81 kip
 $\phi_s = 0.80$ (6.5.4.2)
 $\phi_s R_n$ (per bolt) = 28.7 kip
 $R_u = 586.1$ kip
 Min. Number of bolts required = 21

Bolt Slip Resistance (6.13.2.8)

Assume oversized holes and Class B surface.

$$R_n = K_n * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$K_n = 0.85$ (Table 6.13.2.8-2)
 $K_s = 0.50$ (Table 6.13.2.8-3)
 $N_s = 1$
 $P_t = 51$ kip (Table 6.13.2.8-1)
 R_n (per bolt) = 21.68 kip
 $\phi_s = 0.80$
 $\phi_s R_n$ (per bolt) = 17.34 kip
 $R_u = 386.3$ kip

Min. Number of bolts required = 23

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0 \text{ ksi (Table 6.6.1.2.5-3)}$$

$$A_b = 0.79 \text{ in}^2$$

Min. number of bolts required = 3

Made	DSB	Date	5/22/2011	Job Number	49633
Checked	MPM	Date	5/27/2011		
Backchk'd	DSB	Date	5/27/2011	Sheet No.	

For **Cleveland Innerbelt**

End Diaphragm Design G6 Unit 1

The end diaphragm at the end of stub girder will be an I-section and will be designed as a simple span beam in between the adjacent girders. Design as a non-composite section.

Stub Girder End Shear

DC =	86.4	kip
DW =	35.7	kip
LL truck (no impact) =	69.2	kip
LL truck range (no impact) =	41.1	kip
LL lane =	38.9	kip
Importance Factor =	1.05	
V _u =	410.2	kip (Strength I)
V _u =	306.9	kip (Service II)
V _u =	74.4	kip (Fatigue I)

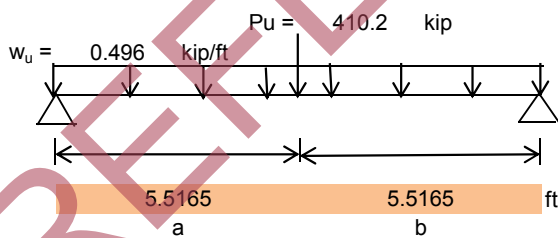
End Diaphragm Section Properties

	b (in)	t (in)	A (in ²)	y (in)	Ay (in ³)
Top	24.0	1.00	24.00	85.50	2052.0
Web	0.750	84	63.00	43.00	2709.0
Bottom	24.0	1.00	24.00	0.50	12.0

	d (in)	I _o (in ⁴)	A*d ² (in ⁴)
Top	42.50	2.0	43350.0
Web	0.00	37044.0	0.0
Bottom	-42.50	2.0	43350.0

A =	111.00	in ²
y _{bot} =	43.00	in
I =	123748	in ⁴
S _{bot} =	2877.9	in ³
S _{top} =	2877.9	in ³
w =	0.378	k/ft

Design Moment and Stress



M _u = P _u *a*b/(a+b) + w _u *(a+b) ² /8 =	1139.0	kip-ft
f _{bu top} =	4.75	ksi (compression)
f _{bu bot} =	4.75	ksi (tension)
V _{u max} =	207.8	kip (Strength I)
V _{u max} =	155.7	kip (Service II)
V _{u max} =	37.2	kip (Fatigue I)

Material Properties

F _y =	50	ksi
E =	29000	ksi
F _u =	65	ksi

(6.4.1-1)

Tension Flange Flexural Resistance (6.10.8.1.2, 6.10.8.3)

$$F_{nt} = R_h * F_{yt}$$

$$R_h = 1.0 \quad (6.10.1.10)$$

$$F_{nt} = 50.0 \text{ ksi}$$

$$\phi_f = 1.00 \quad (6.5.4.2)$$

$$\phi_f F_{nt} = 50.0 \text{ ksi}$$

$$f_{bu} + 1/3 * f_t = 4.75 \text{ ksi}$$

Factored Stress < Capacity, OK

Compression Flange Flexural Resistance (6.10.8.1.1, 6.10.8.2)

Local Buckling Resistance (10.8.2.2)

$$\lambda_{nf} = 0.38 * (E/F_{vc})^{0.5} = 9.15 \quad (6.10.8.2.2-4)$$

$$\lambda_{rf} = 0.56 * (E/F_{vc})^{0.5} = 13.49 \quad (6.10.8.2.2-5)$$

$$\lambda_f = b_{fc} / (2t_{fc}) = 12.0 \quad (6.10.8.2.2-3)$$

If $\lambda_f \leq \lambda_{pf}$

$$F_{nc} = R_b * R_h * F_{yc} \quad (6.10.8.2.2-1)$$

Otherwise

$$F_{nc} = [1 - (1 - F_{yr} / (R_h * F_{yc})) * (\lambda_f - \lambda_{pf}) / (\lambda_{rf} - \lambda_{pf})] * R_b * R_h * F_{yc} \quad (6.10.8.2.2-2)$$

$$R_b = 1.0 \quad (6.10.1.10)$$

$$F_{yr} = 0.7 * F_{yc} = 35.0 \text{ ksi}$$

$$F_{nc} = 40.14 \text{ ksi}$$

Lateral Torsional Buckling Resistance (10.8.2.3)

$$D_c = 42.00 \text{ in}$$

$$r_t = b_{fc} / ((12 * (1 + 1/3 * D_c * t_w / (b_{fc} * t_{fc})))^{0.5}) = 5.78 \text{ in} \quad (6.10.8.2.3-9)$$

$$L_n = 1.0 * r_t * (E/F_{vc})^{0.5} = 139.2 \text{ in} \quad (6.10.8.2.3-4)$$

$$L_r = \pi * r_t * (E/F_{vc})^{0.5} = 437.2 \text{ in} \quad (6.10.8.2.3-5)$$

$$L_b = 66.2 \text{ in}$$

If $L_b \leq L_p$

$$F_{nc} = R_b * R_h * F_{yc} \quad (6.10.8.2.3-1)$$

If $L_p < L_b \leq L_r$

$$F_{nc} = C_b * [1 - (1 - F_{yr} / (R_h * F_{yc})) * (L_b - L_p) / (L_r - L_p)] * R_b * R_h * F_{yc} \leq R_b * R_h * F_{yc} \quad (6.10.8.2.3-2)$$

If $L_b > L_r$

$$F_{nc} = F_{cr} \leq R_b * R_h * F_{yc} \quad (6.10.8.2.3-3)$$

$$C_b = 1.0 \quad (\text{conservative assumption})$$

$$F_{cr} = C_b * R_b * \pi^2 * E / (L_b / r_t)^2 = 2180.9 \text{ ksi} \quad (6.10.8.2.3-8)$$

$$F_{nc} = 50.0 \text{ ksi}$$

HNTB The HNTB Companies Engineers Architects Planners	Made	DSB	Date	5/22/2011	Job Number	49633
	Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backch'kd	DSB	Date	5/27/2011	Sheet No.

End Diaphragm Design G6
Unit 1

Controlling Compressive Resistance

$$F_{nc} = 40.14 \text{ ksi}$$

$$\phi_r = 1.00 \quad (6.5.4.2)$$

$$\phi_r F_{nc} = 40.1 \text{ ksi}$$

$$f_{bu} + 1/3 * f_i = 4.75 \text{ ksi}$$

Factored Stress < Capacity, OK

CONNECTION DESIGN

Stub Girder End

Design Force (6.13.1)

$$\phi_v = 1.00 \quad (6.5.4.2)$$

$$\text{Stub girder } t_w = 0.69 \text{ in}$$

$$\text{Stub girder } D = 84.0 \text{ in}$$

$$\text{Stiffener spacing, } d_o = 273.6 \text{ in}$$

$$k = 5.00 \text{ (Unstiffened web)}$$

$$D/t_w = 122.2$$

$$1.12 * (E * k / F_{vw})^{0.5} = 60.3$$

$$1.40 * (E * k / F_{vw})^{0.5} = 75.4$$

$$C = 0.305$$

$$V_p = 0.58 * F_{yw} * D * t_w = 1674.8 \text{ kip} \quad (6.10.9.2-2)$$

$$V_n = C * V_p = 510.8 \text{ kip} \quad (6.10.9.2-1)$$

$$\phi V_n = 510.8 \text{ kip}$$

Strength I Case Only

If $V_u < 0.75 \phi_v V_n$

$$V_{uw} = 0.75 * \phi_v V_n \quad (6.13.6.1.4b-1)$$

Otherwise

$$V_{uw} = (V_u + \phi_v V_n) / 2 \quad (6.13.6.1.4b-2)$$

$$V_{uw} = 460.5 \text{ kip (Strength I)}$$

$$V_{uw} = 306.9 \text{ kip (Service II)}$$

$$V_{uw} = 74.4 \text{ kip (Fatigue I)}$$

Bolt Properties

$$\text{A325 Bolt diameter, } D_b = 1.00 \text{ in}$$

$$\text{Hole diameter} = 1.125 \text{ in}$$

$$\text{A325 Bolt area, } A_b = 0.79 \text{ in}^2$$

$$F_{ub} = 120.00 \text{ ksi}$$

Girder Web Connection

$$n_{col} = 5$$

$$n_{row} = 10$$

$$d_{edge} = 2.00 \text{ in}$$

$$spa_{col} = 4.00 \text{ in}$$

$$spa_{row} = 7.00 \text{ in}$$

$$\text{Connecting angle thickness} = 0.75 \text{ in}$$

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

Angles on either side of the connection gives 2 shear planes.

$$R_n = 0.38 * A_b * F_{ub} * N_s \quad (6.13.2.7-2)$$

$$N_s = 2$$

$$R_n \text{ (per bolt)} = 71.63 \text{ kip}$$

$$\text{Number of bolts} = 50$$

$$R_n \text{ (entire connection)} = 3581.4 \text{ kip}$$

$$\phi_s = 0.80 \quad (6.5.4.2)$$

$$\phi_s R_n = 2865.1 \text{ kip}$$

$$R_u = 460.50 \text{ kip}$$

Factored Load < Capacity, OK

Bolt Slip Resistance (6.13.2.8)

Assume standard holes and Class B surface.

$$R_n = K_h * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$$K_h = 1.00 \quad (\text{Table 6.13.2.8-2})$$

$$K_s = 0.50 \quad (\text{Table 6.13.2.8-3})$$

$$N_s = 2$$

$$P_t = 51 \text{ kip} \quad (\text{Table 6.13.2.8-1})$$

$$R_n \text{ (per bolt)} = 51.00 \text{ kip}$$

$$\text{Number of bolts} = 50.00$$

$$R_n \text{ (entire connection)} = 2550.00 \text{ kip}$$

$$\phi_s = 0.80 \quad (6.5.4.2)$$

$$\phi_s R_n = 2040.0 \text{ kip}$$

$$R_u = 306.93 \text{ kip}$$

Factored Load < Capacity, OK

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

Conservatively designed per 6.13.6.1.4b rather than actual loads.

ksi (Table 6.6.1.2.5-3)

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0$$

$$A_b = 0.79 \text{ in}^2$$

$$\text{Number of bolts} = 50.00$$

$$N_s = 2$$

$$R_u = 74.4 \text{ kip}$$

$$v(\Delta f) = 0.95 \text{ ksi}$$

Factored Load < Capacity, OK

HNTB	The HNTB Companies Engineers Architects Planners	Made	DSB	Date	5/22/2011	Job Number	49633
		Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backchk'd	DSB	Date	5/27/2011	Sheet No.	

End Diaphragm Design G6
Unit 1

Bolt Bearing Resistance (6.13.2.9)

-With bolts spaced at a clear distance between holes not less than 2.0d and with a clear end distance not less than 2.0d:

$$R_n = 2.4*d*t*F_u \quad (6.13.2.9-1)$$

-With either the clear distance between holes is less than 2.0d, or the clear end distance is less than 2.0d:

$$R_n = 1.2*L_c*t*F_u \quad (6.13.2.9-2)$$

$$L_{c\text{int}} = 5.875 \text{ in } \geq 2.0d$$

$$L_{c\text{end}} = 1.438 \text{ in } < 2.0d$$

Equation to use: 6.13.2.9-2

Controlling thickness, t = 0.688 in (web)

$$R_n = 5211.68 \text{ kip}$$

$$\phi_{bb} = 0.80 \quad (6.5.4.2)$$

$$\phi_{bb}R_n = 4169.3 \text{ kip}$$

$$R_u = 460.50 \text{ kip}$$

Factored Load < Capacity, OK

Connecting Angle Shear (6.13.5.3)

Shear Yielding

$$R_r = \phi_v*0.58*F_y*A_g \quad (6.13.5.3-1)$$

$$\text{Length} = 67.0 \text{ in}$$

$$A_g \text{ (2 angles)} = 100.5 \text{ in}^2$$

$$\phi_v = 1.00 \quad (6.5.4.2)$$

$$R_r = 2914.5 \text{ kip}$$

$$R_u = 460.50 \text{ kip}$$

Factored Load < Capacity, OK

Shear Rupture

$$R_r = \phi_{vu}*0.58*R_p*F_u*A_{vn} \quad (6.13.5.3-2)$$

$$R_p = 0.90 \text{ Assume punched full sized}$$

$$A_{vn} = 83.6 \text{ in}^2$$

$$\phi_{vu} = 0.80 \quad (6.5.4.2)$$

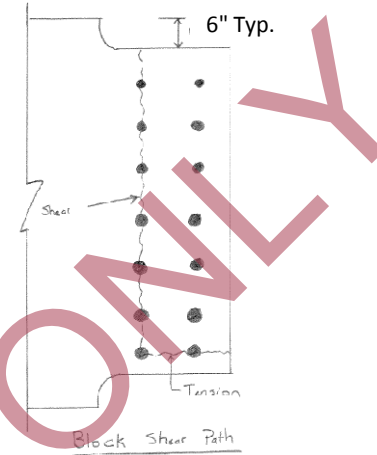
$$R_r = 2269.9 \text{ kip}$$

$$R_u = 460.50 \text{ kip}$$

Factored Load < Capacity, OK

Coped Beam End Block Shear (6.13.4)

Consider beam end and connecting plates



$$R_r = \phi_{bs}*R_p*(0.58*F_u*A_{vn} + U_{bs}*F_u*A_{tn})$$

$$\leq \phi_{bs}*R_p*(0.58*F_y*A_{vg} + U_{bs}*F_u*A_{tn}) \quad (6.13.4-1)$$

$$A_{vg} = 46.41 \text{ in}^2$$

$$A_{vn} = 39.06 \text{ in}^2$$

$$A_{tn} = 8.89 \text{ in}^2$$

$$U_{bs} = 0.5$$

$$\phi_{bs} = 0.80 \quad (6.5.4.2)$$

$$\phi_{bs}*R_p*(0.58*F_u*A_{vn} + U_{bs}*F_u*A_{tn}) = 1268.3 \text{ kip}$$

$$\phi_{bs}*R_p*(0.58*F_y*A_{vg} + U_{bs}*F_u*A_{tn}) = 1177.1 \text{ kip}$$

$$R_r = 1177.1 \text{ kip}$$

$$R_u = 460.50 \text{ kip}$$

Factored Load < Capacity, OK

Diaphragm Web Connection

Determine number of bolts required based on bolt shear resistance. Each connection will take 1/2 of the design force. Detail bolts in 2 rows. The row closest to the stub girder web will have no bolts in the outside thirds of the connecting angles to allow flexibility in the joint.

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

$$R_n = 0.38*A_b*F_{ub}*N_s \quad (6.13.2.7-2)$$

$$N_s = 1$$

$$R_n \text{ (per bolt)} = 35.81 \text{ kip} \quad (6.5.4.2)$$

$$\phi_s = 0.80$$

$$\phi_s R_n \text{ (per bolt)} = 28.7 \text{ kip}$$

$$R_u = 230.3 \text{ kip}$$

Min. Number of bolts required = 9

HNTB	The HNTB Companies	Made	DSB	Date	5/22/2011	Job Number	49633
		Checked	MPM	Date	5/27/2011		
For	Cleveland Innerbelt	Backch'k'd	DSB	Date	5/27/2011	Sheet No.	

End Diaphragm Design G6
Unit 1

Bolt Slip Resistance (6.13.2.8)

$$R_n = K_n * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$K_n = 1.00$ (Table 6.13.2.8-2)
 $K_s = 0.50$ (Table 6.13.2.8-3)
 $N_s = 1$
 $P_t = 51$ kip (Table 6.13.2.8-1)
 R_n (per bolt) = 25.50 kip
 $\phi_s = 0.80$
 $\phi_s R_n$ (per bolt) = 20.40 kip
 $R_u = 153.5$ kip
 Min. Number of bolts required = 8

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0 \text{ ksi (Table 6.6.1.2.5-3)}$$

$$A_b = 0.79 \text{ in}^2$$

$$R_u = 37.2 \text{ kip}$$

Min. Number of bolts required = 3

Stub girder span length, $L = 114.76$ ft
 Required gage = $(L * t/8)^{0.5} = 11.36$ in

End Diaphragm Connection to Girder Web

Design Force (6.13.1)

$$\phi_v = 1.00 \quad (6.5.4.2)$$

Diaphragm $t_w = 0.75$ in
 Diaphragm $D = 84.0$ in
 $k = 5.0$ (assume unstiffened web)
 $D/t_w = 112.0$

$$1.12 * (E * k / F_{vw})^{0.5} = 60.3$$

$$1.40 * (E * k / F_{vw})^{0.5} = 75.4$$

$C = 0.363$
 $V_p = 0.58 * F_{yw} * D * t_w = 1827.0$ kip (6.10.9.2-2)
 $V_n = C * V_p = 663.1$ kip (6.10.9.2-1)
 $\phi V_n = 663.1$ kip

Strength I Case Only

If $V_u < 0.75 \phi_v V_n$
 $V_{uw} = 0.75 * \phi_v V_n$ (6.13.6.1.4b-1)

Otherwise
 $V_{uw} = (V_u + \phi_v V_n) / 2$ (6.13.6.1.4b-2)

$V_{uw} = 497.3$ kip (Strength I)
 $V_{uw} = 155.7$ kip (Strength I)
 $V_{uw} = 37.2$ kip (Fatigue I)

Determine number of bolts based on bolt shear resistance

Bolt Shear Resistance (6.13.2.7)

Assume threads are included in the shear plane

$$R_n = 0.38 * A_b * F_{ub} * N_s \quad (6.13.2.7-2)$$

$N_s = 1$
 R_n (per bolt) = 35.81 kip
 $\phi_s = 0.80$ (6.5.4.2)
 $\phi_s R_n$ (per bolt) = 28.7 kip
 $R_u = 497.3$ kip
 Min. Number of bolts required = 18

Bolt Slip Resistance (6.13.2.8)

Assume oversized holes and Class B surface.

$$R_n = K_n * K_s * N_s * P_t \quad (6.13.2.8-1)$$

$K_n = 0.85$ (Table 6.13.2.8-2)
 $K_s = 0.50$ (Table 6.13.2.8-3)
 $N_s = 1$
 $P_t = 51$ kip (Table 6.13.2.8-1)
 R_n (per bolt) = 21.68 kip
 $\phi_s = 0.80$
 $\phi_s R_n$ (per bolt) = 17.34 kip
 $R_u = 155.7$ kip

Min. Number of bolts required = 9

Fatigue Resistance (6.6.1.2.2)

Bolted connections are a Class B fatigue detail. Fatigue I loading.

$$(\Delta F)_n = (\Delta F)_{TH} = 16.0 \text{ ksi (Table 6.6.1.2.5-3)}$$

$$A_b = 0.79 \text{ in}^2$$

Min. number of bolts required = 3