

GEOTECHNICAL CALCULATION COVER SHEET



400 N 34th St, Suite 100; Seattle, WA 98103

PROJECT: Cleveland Innerbelt CCG1

CLIENT: HNTB / Walsh

CALC. NO: _____

JOB NO: 21-1-21361-611

SHEETS: 4 (not including cover)

SUBMITTAL NO.: _____ 0

TITLE:

Required Rock Socket Length Based on O-Cell Test

PURPOSE AND OBJECTIVE:

Revise rock socket length based on unit side and base resistances determined from the results of the O-Cell test as reported by LoadTest in their revised report dated May 4, 2012.

SUMMARY AND CONCLUSIONS:

Required rock socket length is 8.3 feet and is controlled by minimum depth stipulated in the RFP of 1.5D (where D is the diameter of the shaft). Estimated shaft settlements under Service limit loads is approximately 1/2 to 1 inch.

SIGN OFF

| REV. NO. | ORIGINATOR Name/Date | TECHNICAL REVIEW Name/Date | PRINCIPAL REVIEW Name/Date |
|----------|---------------------------|-------------------------------|-------------------------------|
| 1 | Gerard Buechel / 5-9-2012 | David Vara / 5-9-2012 | Bill Perkins / 5-10-2012 |
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| Rev. No | Revision Description | Revision Date |
|---------|----------------------|---------------|
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Strength Limit - 6905 kips ✓; Service Limit - 5270 kips ✓

Design - grade - 17 ksf; 170 ksf tip \rightarrow 22' ✓

April 10 LT values - 17 ksf; 220 ksf tip \rightarrow 18' ✓

May 4 LT - 17 ksf; 370 ksf tip \rightarrow 2.25' (construction) (1.5 ϕ) ✓

Rock Socket - 5.5' ϕ ✓

RF = 0.7 per AASHTO for Strength. ✓

Load Test Results

Transducer A - 3.8 inches

Transducer B+C - 5.3 to 5.5 inches

Plate ϕ - 42 inches \rightarrow 5% = 2.1 inches ✓

Shaft ϕ - 66 inches ✓

Plate ϕ + 2V:1H = 42 + 8 = 50 \times 0.05 = 2.5 inches ✓

shear $\approx \sqrt{f'_c} \Rightarrow$ 18 ksf

Average $\phi = 42 + 4 = 46'' \rightarrow \pi(46) = 12.0$ ft

Shear surface = 12 ft \times $\frac{8}{12} = 8$ ft²

shear = $18 \times 8 = 144$ kips

FOR A HEMISPHERICAL SHEAR SURFACE: per Dave Uava



$R_2 = 21''$
 $R_1 = 29''$

$A = \pi(R_1 + R_2) \sqrt{(R_1 - R_2)^2 + h^2}$
 $A = \pi(29'' + 21'') \sqrt{(29'' - 21'')^2 + 8^2} = 1,777 \text{ in}^2 = 12.3 \text{ ft}^2$

$12.3(18) = 221$ kips

Conclusion - At nominal loads, concrete sheared ^{o-cell}



Strength Limit Design

$$6905 / 0.7 = 9864 \text{ kips} \rightarrow \text{Required Nominal Resist.} \checkmark$$

Base @ 2.5" deflection = 370 ksf \checkmark

End Bearing Creep Limit \rightarrow O.C. - 4300 k @ 1.95" displacement
(Figure D-1 pg 56/82)
Side Shear Creep Limit \rightarrow O.C. - 3900 k @ 0.33" displacement
(Figure D-2 pg 57/82) \checkmark

Side Resistance = 17 ksf. \checkmark

5.5' ϕ \rightarrow Area Perimeter
23.7 ft² \checkmark 17.3 ft \checkmark

Base Resistance = 23.7(370) = 8769 kips \checkmark

Required Nominal = 8769 - 9864 = 1095 kips \checkmark

Required Embedment = 1095 / (17 ksf * 17.3 ft)
= 3.7 ft \checkmark

Required min Embed = 1.5(5.5) = 8.25' \checkmark

Mobilized Base Resistance =

Side Resist = 8.25' (17.3') (17 ksf) = 2426 kips \checkmark

9864 - 2426 kips = 7438 kips = 314 ksf \checkmark

At 314 ksf, Settlement is 1.9 inch \checkmark
314 * π (2.5')² / 144 = 4300 O.C Force is 4300 k \checkmark

- Note Load transferred in soil that is ignored:
per Design Criteria - 2,400 k Figure 5 of 8

- Recheck mobilized Base:

9864 - 2426 - 2400 = 5038 kips = 212 ksf \checkmark
(Figure 7 of 8) 23.7 about 1/2" deflection



Check Service Limit State

Service Limit is 5270 kips ✓

With maximum embed - $8.25' (17.3') \times 17 \text{ ksf}$
= 2426 kips ✓

Mobilized Base = $5270 - 2426$
= 2844 kips = 120 ksf ✓
23.7 ft²

Settlement at 120 ksf \Rightarrow 0.75 inch
(Note this is requiring soil contribution) ✓

Force in O-cell $\Rightarrow 120 \frac{\text{k}}{\text{ft}^2} \times \pi (25\text{-m})^2 \times \frac{\text{ft}^2}{144 \text{m}^2}$
 \Rightarrow 1635 kips. ✓

Also see Fig 1 of 8 at 0.75 - Force in O.C. \approx 1600 k ✓

At this force, side resistance mobilized in soil is about 800 kips (Figure 5 of 8). ✓

True Base Resistance:

$5270 - 2426 \text{ k} - 800 \text{ k} = 2044 \text{ k}$ ✓

$2044 / 23.7 \text{ k} = 86 \text{ ksf}$ Settlement is about 0.5 inch ✓

| | Excluding soil | With soil |
|--------|-------------------------|------------------------|
| Side - | 2426 k ✓ | 3226 k ✓ |
| Base - | <u>2844 k</u> (120 ksf) | <u>2044 k</u> (86 ksf) |
| | 5270 k ✓ | 5270 k ✓ |

Both Forces in Base + Side are less than the creep limits see page 2. ✓



Conclusions

- OK to use minimum Embedment - 9.3' ✓
- Nominal Required shaft Resistance - 9864k ✓
- Service Limit State Resistance - 5270k ✓

Shaft Design

| | (kips) Excluding Soil | (kips) Including Soil |
|----------------------|-----------------------------|-----------------------------|
| <u>Strength</u> | | |
| side | ✓ 2426 (17kSF) | ✓ 4826 (17kSF+soil) |
| Base | ✓ 7438 (314kSF) | ✓ 5038 (212kSF) |
| | ✓ 9864 ✓ | ✓ 9864 ✓ |
| Estimated Settlement | ✓ 2.0 inch | ✓ 1.2 inch |

Service

| | | |
|----------------------|-----------------|------------------|
| side | ✓ 2426 (17kSF) | ✓ 3226 (17+soil) |
| Base | ✓ 2844 (120kSF) | ✓ 2044 (86kSF) |
| | ✓ 5270 ✓ | ✓ 5270 ✓ |
| Estimated Settlement | ✓ 0.7 inch | ✓ 0.5 inch |

- Service Limit Settlement less than Creep Limit shaft will not creep. ✓

Check Settlement Using Old version of Report -
Figure 7 of 8 For Service Limit
Base Resistance

120kSF

86kSF

1.4 inch ✓

0.9 inch

Tell HWTB Service Limit Settlement 0.7 to 1.0 inch