

## RJ Watson, Inc - LRFD Masonry Plate Calculations - Model DB2650F Piers 6 & 7

$t_m := 2.50\text{in}$	as designed thickness of masonry plate
$t_{bp} := 2.20\text{in}$	<b>minimum masonry plate thickness required</b>
$MPL := 59\text{in}$	masonry plate length (longit)
$MPW := 60\text{in}$	masonry plate width (trans)
$LBP = 42.00\text{ in}$	lower bearing plate diameter

--> design masonry plate as a cantilever beam bending about the edge of lower bearing plate

$$A_1 := \frac{\pi \cdot (\min(MPL, MPW))^2}{4} \quad A_1 = 2734 \text{ in}^2 \quad \text{effective loaded area - assuming circular pressure distribution limited by smallest width of masonry plate}$$

$$A_p := \frac{\pi}{4} \cdot LBP^2 \quad A_p = 1385 \text{ in}^2 \quad \text{bearing area of lower bearing plate}$$

$$\text{Force} := \frac{P_u}{A_1} \cdot (A_1 - A_p) \quad \text{Force} = 1874 \text{ kips} \quad \text{effective bending force}$$

$$\text{Arm} := \frac{\min(MPL, MPW) - LBP}{4} \quad \text{Arm} = 4.25 \text{ in} \quad \text{moment arm}$$

$$M_u := \text{Force} \cdot \text{Arm} \quad M_u = 7966 \text{ kips} \cdot \text{in} \quad \text{factored bending moment}$$

$$Z := \pi \cdot LBP \cdot \frac{t_{bp}^2}{4} \quad Z = 159.7 \text{ in}^3 \quad \text{plastic section modulus}$$

$$\phi_f := 1.00 \quad \text{resistance factor for flexure at **strength** limit state (AASHTO LRFD 6.5.4.2)}$$

$$F_y := 50 \text{ ksi} \quad \text{yield strength of plate (ASTM A709 Gr. 50)}$$

$$M_n := Z \cdot F_y \quad M_n = 7983 \text{ kips} \cdot \text{in} \quad \text{nominal flexural resistance}$$

$$M_r := \phi_f \cdot M_n \quad M_r = 7983 \text{ kips} \cdot \text{in} \quad \text{factored flexural resistance}$$

$$M_r = 7983 \text{ kips} \cdot \text{in} \quad \geq \quad M_u = 7966 \text{ kips} \cdot \text{in} \quad \text{check flexural capacity of plate ..... OK}$$

**RJ Watson, Inc - LRFD Masonry Plate Calculations - Model DB2650F****Piers 6 & 7**Concrete Bearing Pressure ....

$$A1 := \frac{\pi \cdot LBP^2}{4}$$

$$A1 = 1385 \text{ in}^2$$

conservatively assume effective loaded area = lower bearing plate area

$$w := 78 \text{ in}$$

conservatively assume effective concrete supporting area is limited by minimum pedestal width

$$A2 := \frac{\pi \cdot w^2}{4}$$

$$A2 = 4778 \text{ in}^2$$

area as defined by AASHTO LRFD 5.7.5

$$m := \min\left(\sqrt{\frac{A2}{A1}}, 2.0\right)$$

$$m = 1.86$$

modification factor

$$f_c := 4.00 \text{ ksi}$$

concrete compressive strength

$$P_n := 0.85 \cdot f_c \cdot A1 \cdot m$$

$$P_n = 8748 \text{ kips}$$

nominal concrete bearing resistance (AASHTO LRFD 5.7.5-2)

$$\phi := 0.70$$

resistance factor for bearing on concrete (AASHTO LRFD 5.5.4.2.1)

$$P_r := \phi \cdot P_n$$

factored concrete bearing strength (AASHTO LRFD 5.7.5-1)

$$P_r = 6124 \text{ kips} \quad \geq$$

$$P_u = 3800 \text{ kips}$$

check bearing capacity of concrete ..... OK