

**DISKTRON BEARING CALCULATIONS**

**FOR**

**WALSH CONSTRUCTION**

**PIER 6 MASONRY PLATE MODIFICATIONS**

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**MAIN SPAN – UNIT 2**

**INNERBELT BRIDGE**

**I-90WB, BRIDGE NO. CUY-90-1566**

**CLEVELAND, OHIO**

**CUY-90-14.90**

**PID NO. 77332/85531**

2687A

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Prepared By:

**R.J. Watson, Inc.**

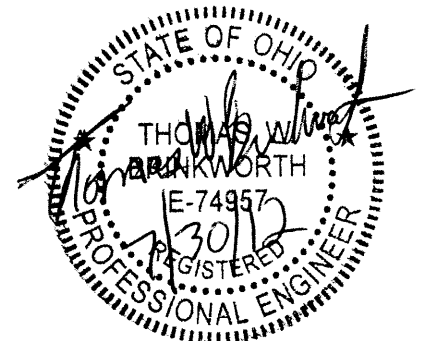
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**RJ Watson, Inc - LRFD Masonry Plate Calculations - Model DB2650F****Pier 6 G2-4**

$t_{bp} := 2.50\text{in}$	<i>new masonry plate thickness</i>
$MPL := 59\text{in}$	<i>new masonry plate length (longit)</i>
$MPW := 68\text{in}$	<i>new masonry plate width (trans)</i>
$LBP = 42.00\text{in}$	<i>lower bearing plate diameter</i>
$off := 6.50\text{in}$	<i>maximum lower bearing plate <b>offset</b> on masonry plate (trans)</i>

$$M_{min} := \min\left[\frac{MPL}{2}, \left(\frac{MPW}{2} - off\right)\right] \quad \text{minimum distance from centerline of lower bearing plate to edge of masonry plate}$$

$$M_{min} = 27.5\text{ in}$$

--> design masonry plate as a cantilever beam bending about the edge of lower bearing plate

$$A_1 := \pi \cdot (M_{min})^2 \quad A_1 = 2376\text{ in}^2 \quad \text{effective loaded area - assuming circular pressure distribution limited by closest edge of masonry plate}$$

$$A_p := \frac{\pi}{4} \cdot LBP^2 \quad A_p = 1385\text{ in}^2 \quad \text{bearing area of lower bearing plate}$$

$$\text{Force} := \frac{P_u}{A_1} \cdot (A_1 - A_p) \quad \text{Force} = 1584\text{ kips} \quad \text{effective bending force}$$

$$\text{Arm} := \frac{M_{min} - \frac{LBP}{2}}{2} \quad \text{Arm} = 3.25\text{ in} \quad \text{moment arm}$$

$$M_u := \text{Force} \cdot \text{Arm} \quad M_u = 5148\text{ kips}\cdot\text{in} \quad \text{factored bending moment}$$

$$Z := \pi \cdot LBP \cdot \frac{t_{bp}^2}{4} \quad Z = 206.2\text{ in}^3 \quad \text{plastic section modulus}$$

$$\phi_f := 1.00 \quad \text{resistance factor for flexure at **strength** limit state (AASHTO LRFD 6.5.4.2)}$$

$$F_y := 50\text{ksi} \quad \text{yield strength of plate (ASTM A709 Gr. 50)}$$

$$M_n := Z \cdot F_y \quad M_n = 10308\text{ kips}\cdot\text{in} \quad \text{nominal flexural resistance}$$

$$M_r := \phi_f \cdot M_n \quad M_r = 10308\text{ kips}\cdot\text{in} \quad \text{factored flexural resistance}$$

$$M_r = 10308\text{ kips}\cdot\text{in} \quad \geq \quad M_u = 5148\text{ kips}\cdot\text{in} \quad \text{check flexural capacity of plate ..... OK}$$

**RJ Watson, Inc - LRFD Masonry Plate Calculations - Model DB2650F****Pier 6 G2-4**Concrete Bearing Pressure ....

$$A1 := \frac{\pi \cdot LBP^2}{4}$$

$$A1 = 1385 \text{ in}^2$$

conservatively assume effective loaded area = lower bearing plate area

$$w := 78 \text{ in}$$

conservatively assume effective concrete supporting area is limited by minimum pedestal width

$$A2 := \frac{\pi \cdot w^2}{4}$$

$$A2 = 4778 \text{ in}^2$$

area as defined by AASHTO LRFD 5.7.5

$$m := \min\left(\sqrt{\frac{A2}{A1}}, 2.0\right)$$

$$m = 1.86$$

modification factor

$$f_c := 4.00 \text{ ksi}$$

concrete compressive strength

$$P_n := 0.85 \cdot f_c \cdot A1 \cdot m$$

$$P_n = 8748 \text{ kips}$$

nominal concrete bearing resistance (AASHTO LRFD 5.7.5-2)

$$\phi := 0.70$$

resistance factor for bearing on concrete (AASHTO LRFD 5.5.4.2.1)

$$P_r := \phi \cdot P_n$$

factored concrete bearing strength (AASHTO LRFD 5.7.5-1)

$$P_r = 6124 \text{ kips} \quad \geq$$

$$P_u = 3800 \text{ kips}$$

check bearing capacity of concrete ..... OK

## RJ Watson, Inc - LRFD Masonry Plate Calculations - Model DB2650F      Piers 6 & 7

$t_m := 2.50\text{in}$       as designed thickness of masonry plate

$t_{bp} := 2.20\text{in}$       **minimum masonry plate thickness required**

$MPL := 59\text{in}$       masonry plate length (longit)

$MPW := 60\text{in}$       masonry plate width (trans)

$LBP = 42.00\text{in}$       lower bearing plate diameter

--> design masonry plate as a cantilever beam bending about the edge of lower bearing plate

$A_1 := \frac{\pi \cdot (\min(MPL, MPW))^2}{4}$        $A_1 = 2734\text{in}^2$       effective loaded area - assuming circular pressure distribution limited by smallest width of masonry plate

$A_p := \frac{\pi}{4} \cdot LBP^2$        $A_p = 1385\text{in}^2$       bearing area of lower bearing plate

$\text{Force} := \frac{P_u}{A_1} \cdot (A_1 - A_p)$        $\text{Force} = 1874\text{kips}$       effective bending force

$\text{Arm} := \frac{\min(MPL, MPW) - LBP}{4}$        $\text{Arm} = 4.25\text{in}$       moment arm

$M_u := \text{Force} \cdot \text{Arm}$        $M_u = 7966\text{kips}\cdot\text{in}$       factored bending moment

$Z := \pi \cdot LBP \cdot \frac{t_{bp}^2}{4}$        $Z = 159.7\text{in}^3$       plastic section modulus

$\phi_f := 1.00$       resistance factor for flexure at **strength** limit state (AASHTO LRFD 6.5.4.2)

$F_y := 50\text{ksi}$       yield strength of plate (ASTM A709 Gr. 50)

$M_n := Z \cdot F_y$        $M_n = 7983\text{kips}\cdot\text{in}$       nominal flexural resistance

$M_r := \phi_f \cdot M_n$        $M_r = 7983\text{kips}\cdot\text{in}$       factored flexural resistance

$M_r = 7983\text{kips}\cdot\text{in} \geq M_u = 7966\text{kips}\cdot\text{in}$       check flexural capacity of plate ..... OK