



**FORM DQP 2.01-1
LEVEL 1 CHECK PRINT SIGN-OFF SHEET**

Client Name: Ohio Department of Transportation
 Job Title: Cleveland Innerbelt Design-Build Contract
 Job Number: CUY-90-14.90
 Document Title: KNEE BRACE STIFFENER AT FLANGE BENDS

Check Level (Mark One): 1A 100% Document Check
 1B 100% Input Check

Enter description below:

	Print Name	Signature	Date
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<input checked="" type="checkbox"/> Validater	<u>David Glastetter</u>	<u><i>D. Glastetter</i></u>	<u>10/6/11</u>

Insert an "X" in the box to indicate a required QC activity.

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SSL 10-5-11
 ✓ DSG 10/6/11

FLOOR BEAM TYPES A, B, C
 Stiffeners at Flange Bend Points

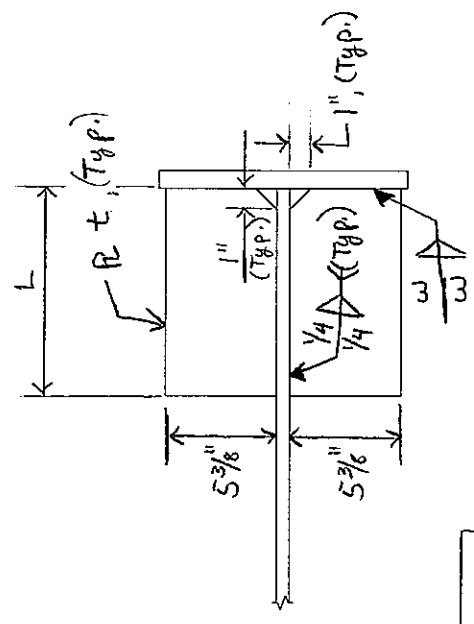
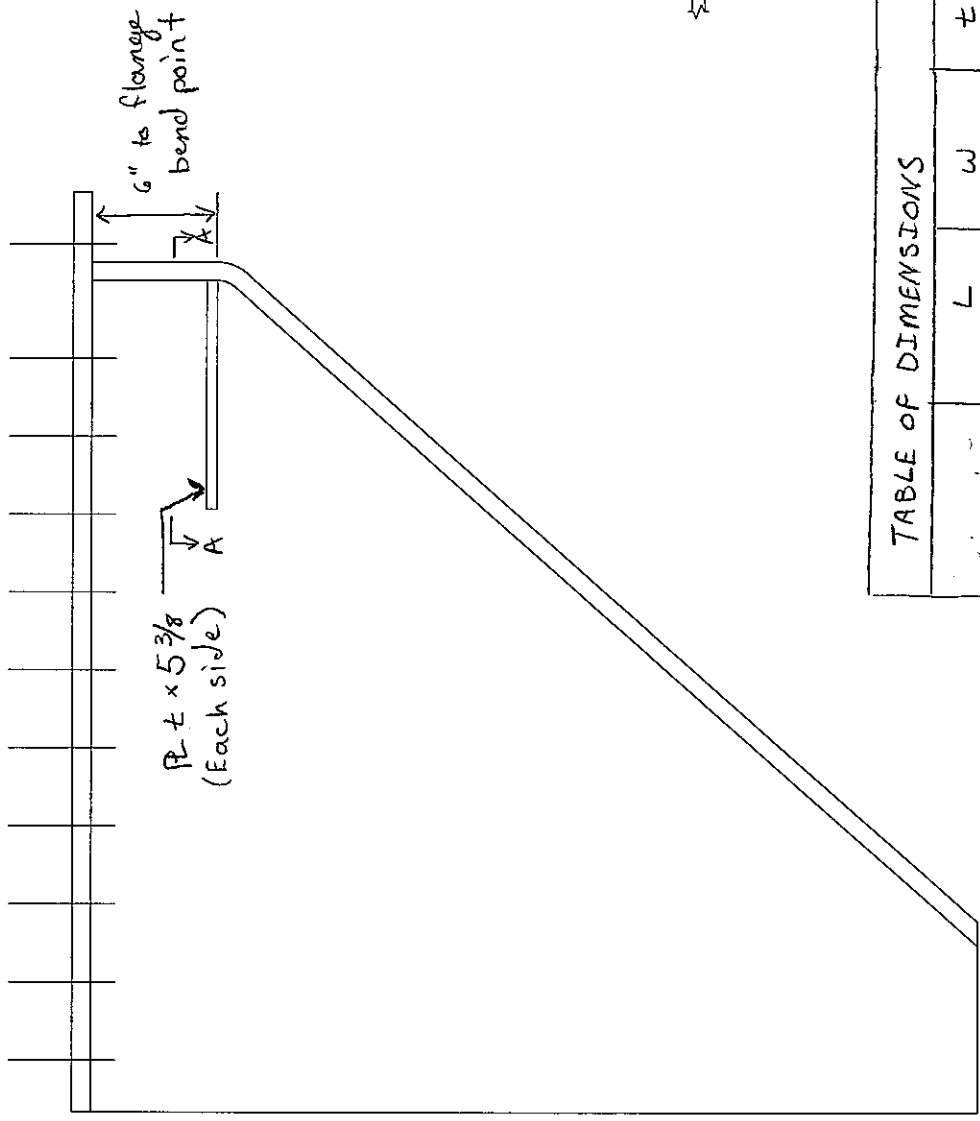
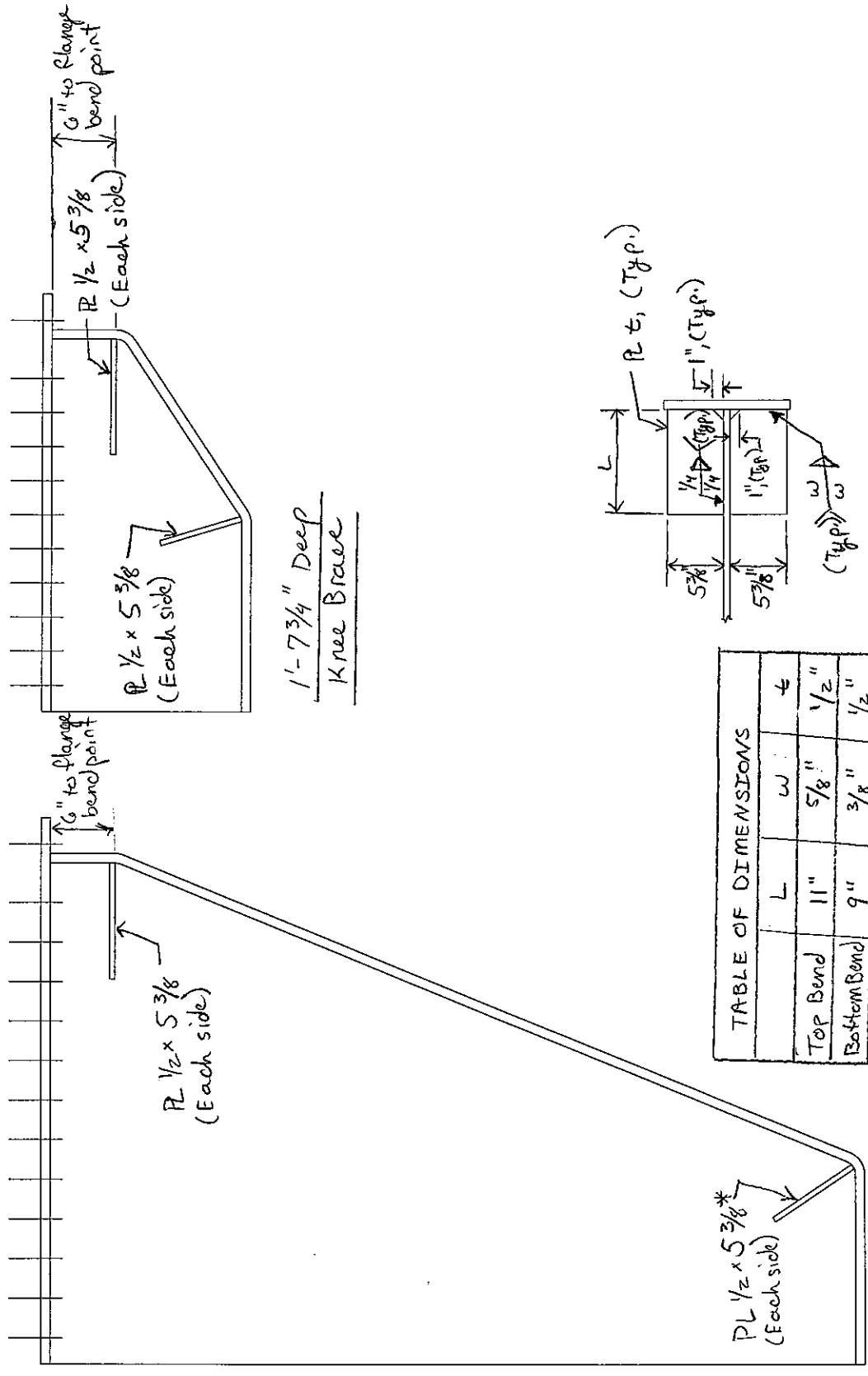


TABLE OF DIMENSIONS

	L	w	t
Type A, C	9"	1/2"	1/2"
Type B	11"	5/8"	1/2"

FLOOR BEAM TYPES D, E, F
Stiffeners at Flange Bend Points



Note: Intermediate Knee Brace sizes not shown. Stiffeners at flange bend points are similar.
* Bottom Bend stiffener is placed radially in flange bend.

TABLE OF DIMENSIONS

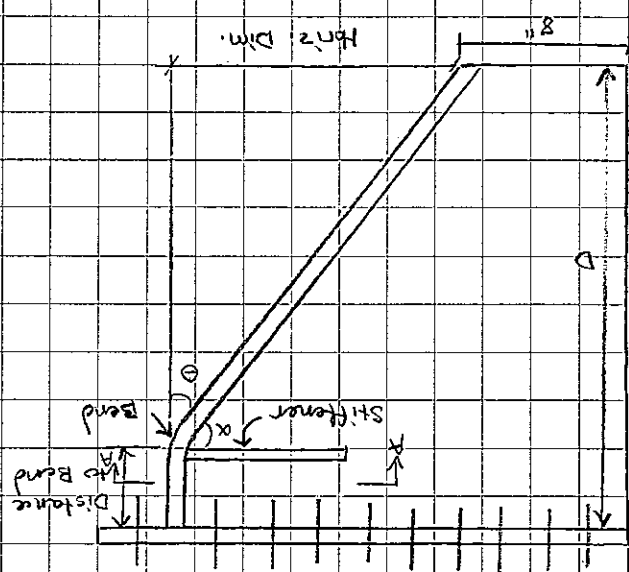
	L	W	t
Top Bend	11"	5 3/8"	1/2"
Bottom Bend	9"	3 1/8"	1/2"

6'-6" Deep
Knee Brace

UNIT 2 - DIAPHRAGMS

KNEE BRACE

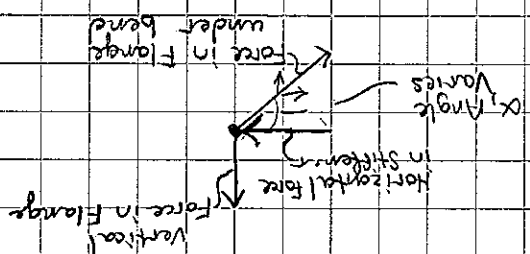
Per RFI, change kneebrace flange
to have a bend to allow for a girth
weld between knee brace top
and side flanges. Add stiffener
at flange bend.



Weld Capacity:
 $Capacity = \phi_w (0.6) F_{EXX} A_e (0.707)$
 $\phi_w = 0.80$
 $F_{EXX} = 70 \text{ ksi}$

$$\sum F_y = 0 = +(\text{Vert Flange } F) - (\text{Flange under Bend } F)(\sin \alpha)$$

$$\sum F_x = 0 = +(\text{Horiz. Stiff. } F) - (\text{Flange under Bend } F)(\cos \alpha)$$



→ Determine component of horizontal force to be resisted by stiffener.

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UNIT 2 - DIAPHRAGMS

KNEE BRACE

→ Distance to Bend for Bolt clearance

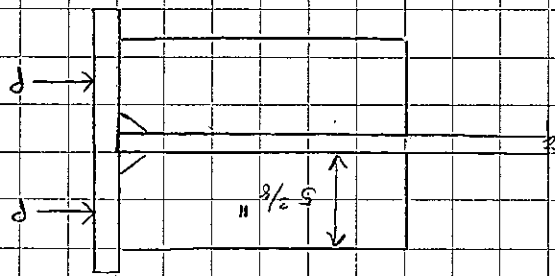
Bolt Length:

$$L = \frac{7}{8}'' + 1.5'' + 0.177'' + \frac{13}{4}'' + \frac{39}{64}''$$

bolt head

$$L = 4.91''$$

→ Use 6'' between bend point



SECTION A-A

→ Design stiffener as a Non-slimmer member (AASHTO G.9.4.2)

If member satisfies b/ϵ ratio

for non-slimmer members,

yielding will control over

local buckling (AASHTO G.9.4.2.1)

$$\frac{b}{\epsilon} \leq k \sqrt{\frac{F_y}{E}}$$

$$k = 0.95$$

$$\Rightarrow \epsilon \geq b = (5.375'')^2$$

$$k \sqrt{\frac{F_y}{E}} = (0.95) \sqrt{\frac{(29000 \text{ ksi})}{(50 \text{ ksi})}}$$

$$\epsilon \geq 0.5''$$

→ Check yielding

$$\phi P_n = \phi F_y A_g = (0.9)(50 \text{ ksi})(5.375'')(\frac{1}{2}'')$$

$$\phi P_n = 121 \text{ k}$$

Max Force to both stiffeners = 225k

→ Force to 1 stiffener = 225k = 113k = P_u

2

$$\phi P_n = 121 \text{ k} > 113 \text{ k} = P_u \Rightarrow \text{OK}$$

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UNIT 2 - DIAPHRAGMS

KNEE BRACE

→ Check for Flexure: (AASHTO 6.12.2.2.7)

$$Lbd \leq 0.08E \frac{F_y}{z}$$

$$(5.375)(8) \leq (0.08)(29000 \text{ ksi}) \frac{F_y}{z}$$

$$172 \leq 46.4 \frac{F_y}{z}$$

→ Flexural yielding is N/A

Lateral Torsional Buckling

$$0.08E \leq Lbd \leq 1.9F_y z$$

$$46.4 \leq 172 \leq 1102$$

$$M_n = C_b \left[1.52 - 0.274 \left(\frac{Lbd}{F_y} \right) \left(\frac{z}{E} \right) \right] M_y \leq M_p$$

$$M_n = (1) \left[1.52 - (0.274) \left(\frac{383}{5.375} \right) \left(\frac{8}{8} \right) \right] (50 \text{ ksi}) \left(\frac{1}{2} \right)^2 \left(\frac{29000 \text{ ksi}}{2} \right)$$

$$M_n = (50 \text{ ksi}) \left(\frac{1}{6} \right) \left(\frac{1}{2} \right) \left(\frac{1}{8} \right)^2 \leq M_p$$

$$M_n = 383.7 \text{ k.in} \leq M_p$$

$$M_p = (50 \text{ ksi}) \left(\frac{1}{4} \right) \left(\frac{1}{2} \right) \left(\frac{1}{8} \right)^2$$

$$M_p = 400 \text{ k.in}$$

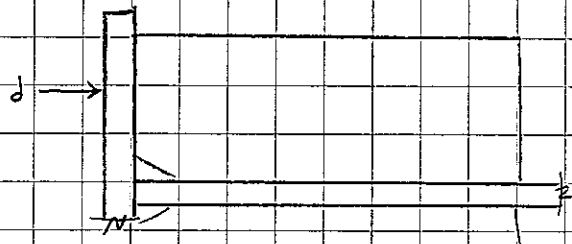
$$\phi = 1.0$$

$$\phi M_n = 383 \text{ k.in}$$

$$M_u = PL = (113 \text{ k})(2.6875) = 304 \text{ k.in}$$

Assume P is centered at half of flange

$$L = \frac{12 \text{ in}}{2} - \left(\frac{5 \text{ in}}{2} \right) = 2.6875 \text{ in}$$



$$\phi M_n = 383 \text{ k.in} > 304 \text{ k.in} = M_u \Rightarrow \text{OK}$$

→ Check Shear: (AASHTO 6.10.9.2)

$$V_r = \phi V_n \quad V_n = C V_p$$

$$L = 510$$

$$\frac{D}{l} \leq 1.12 \sqrt{\frac{F_y}{E}}$$

$$\frac{8 \text{ in}}{510} \leq (1.12) \sqrt{\frac{(50 \text{ ksi})}{(29000 \text{ ksi})}}$$

$$10 \leq 60.3 \Rightarrow C = 1.0$$

$$V_p = 0.58 F_y D \leq (0.58)(50 \text{ ksi})(8 \text{ in}) \left(\frac{1}{2} \right)$$

$$V_p = 116 \text{ k}$$

$$V_r = (1)(1)(116 \text{ k})$$

$$V_r = 116 \text{ k} > P_u = 113 \text{ k} \Rightarrow \text{OK}$$

→ Use a 5.375" x 1/2" stiffener at knee brace flange points

Cleveland Innerbelt - Unit 2		Made	SJL	Date	10/4/2011	Job Number	49633
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For K:\49633\Bridges\Design\Drawings\Diaphragm\final\cross\lateral\Bracing\Revision\RFI\calcs\Diaphragm_connections.xlsx KB band stiffener

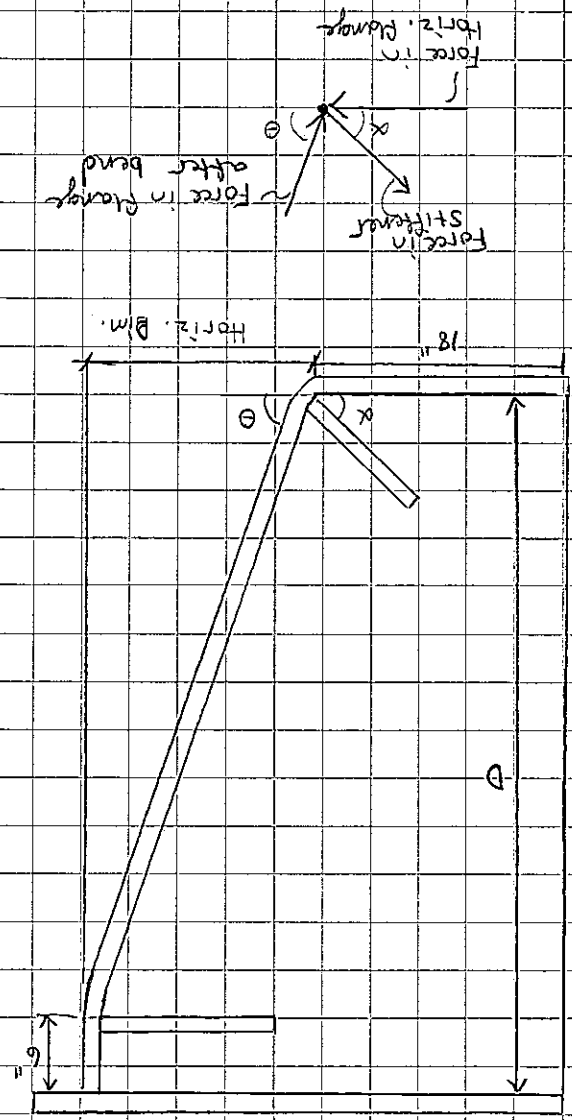
Knee Brace Stiffener at Flange Bend

$R_r = \Phi * 0.6 * F_{tmax} = 33.6 \text{ ksi}$

Type	Flange Stress (ksi)	Flange Area (in ²)	Knee Brace Web Depth (in)	Distance to Bend Point (in)	Horiz. Flange Dimension (in)	Vertical Force in Flange (k)	Angle θ (deg.)	Angle α (deg.)	Force in Flange Under Bend (k)	Horiz. Force to Stiffeners (k)	Weld length for Stiff. to side Flange (in)	Req'd Weld Size, Stiff. to side Flange (in)	Weld length for Stiff. to KB web (in)	Req'd Weld Size, Stiff. to KB web (in)
Type A														
A-S Min M	-18.4	10.5	42.625	6	32	-193.2	41.1	48.9	-256.6	-168.8	7.75	0.458	8	0.222
A-S Max M	19.5	10.5	42.625	6	32	204.8	41.1	48.9	271.9	178.9	7.75	0.486	8	0.235
A-T Min M	-20.8	10.5	71.125	6	32	-218.4	26.2	63.8	-243.3	-107.3	7.75	0.291	8	0.141
A-T Max M	22.2	10.5	71.125	6	32	233.1	26.2	63.8	259.7	114.5	7.75	0.311	8	0.151
Type B														
B-S Min M	-15.8	10.5	35.125	6	39.5	-165.9	53.6	36.4	-279.5	-225.0	7.75	0.611	10	0.237
B-S Max M	11.4	10.5	35.125	6	39.5	119.7	53.6	36.4	201.7	162.3	7.75	0.441	10	0.171
B-T Min M	-29.3	10.5	77.125	6	39.5	-307.7	29.0	61.0	-351.9	-170.9	7.75	0.464	10	0.180
B-T Max M	22.5	10.5	77.125	6	39.5	236.3	29.0	61.0	270.2	131.2	7.75	0.356	10	0.138
Type C														
C-S Min M	-15.1	10.5	34.125	6	26.25	-158.6	43.0	47.0	-216.9	-148.0	7.75	0.402	8	0.195
C-S Max M	18.2	10.5	34.125	6	26.25	191.1	43.0	47.0	261.4	178.4	7.75	0.484	8	0.235
C-T Min M	-20.6	10.5	47.125	6	26.25	-216.3	32.6	57.4	-256.6	-138.1	7.75	0.375	8	0.182
C-T Max M	24.6	10.5	47.125	6	26.25	258.3	32.6	57.4	306.4	164.9	7.75	0.448	8	0.217
Type D, E, F														
D Bot Min M	-14.7	10.5	18	6	17.5	-154.4	55.6	34.4	-272.9	-225.1	7.75	0.611	10	0.237
D Bot Max M	10.3	10.5	18	6	17.5	108.2	55.6	34.4	191.2	157.7	7.75	0.428	10	0.166
D Top Min M	13	10.5	18	6	17.5	136.5	55.6	34.4	241.4	199.1	7.75	0.541	10	0.209
D Top Max M	-11.3	10.5	18	6	17.5	-118.7	55.6	34.4	-209.8	-173.0	7.75	0.470	10	0.182
D-M Min M	-24.6	10.5	27.75	6	17.5	-258.3	38.8	51.2	-331.5	-207.8	7.75	0.564	10	0.219
D-M Max M	17.8	10.5	27.75	6	17.5	186.9	38.8	51.2	239.9	150.4	7.75	0.408	10	0.158
D-T Min M	-30.2	10.5	76.25	6	29.5	-317.1	22.8	67.2	-343.9	-133.2	7.75	0.362	10	0.140
D-T Max M	23.7	10.5	76.25	6	29.5	248.9	22.8	67.2	269.9	104.5	7.75	0.284	10	0.110

UNIT 2 - DIAPHRAGMS
KNEE BRACE

→ Determine Force in Type D, E, F
bottom bend stiffener



$$\sum F_x = + (F_{horz.f.}) - (F_{a.b.})(\cos \theta)$$

$$- (F_{stiff.})(\cos \alpha) = 0$$

$$(F_{horz.f.}) = + \int (F_{stiff.})(\sin \alpha) \left[(\cos \theta) + (F_{stiff.})(\cos \alpha) \right]$$

$$(F_{horz.f.}) = (F_{stiff.}) \left[(\sin \alpha)(\cos \theta) + (\cos \alpha) \right]$$

$$\sum F_y = 0 = - (F_{a.b.})(\sin \theta) + (F_{stiff.})(\sin \alpha)$$

$$F_{a.b.} = (F_{stiff.}) \left(\frac{\sin \theta}{\sin \alpha} \right)$$

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Checked	DJR	Date	9/6/11	Sheet No.	
Backcheck		Date			

Type D, Bottom Bend	Flange Stress (ksi)	Flange Area (in ²)	Web Depth (in)	Distance to Bend Point (in)	Horiz. Flange Dimension (in)	Horiz. Force in Flange (k)	Angle θ (deg.)	Angle α (deg.)	Force in Flange after Bend (k)	Force to Stiffeners (k)	Weld length for Stiff. to side Flange (in)	Req'd Weld Size, Stiff. to side Flange (in)	Weld length for Stiff. to KB web (in)	Req'd Weld Size, Stiff. to KB web (in)
D Bot Min M	-15.4	10.5	18	6	17.5	-161.7	34.4	72.8	161.7	95.7	7.75	0.260	8	0.126
D Bot Max M	10.5	10.5	18	6	17.5	110.3	34.4	72.8	110.3	65.3	7.75	0.177	8	0.086
D Top Min M	13	10.5	18	6	17.5	136.5	34.4	72.8	136.5	80.8	7.75	0.219	8	0.106
D Top Max M	-11.9	10.5	18	6	17.5	-125.0	34.4	72.8	125.0	74.0	7.75	0.201	8	0.097
D-M Min M	-13.1	10.5	27.75	6	17.5	-137.6	51.2	64.4	137.6	118.8	7.75	0.323	8	0.156
D-M Max M	8.7	10.5	27.75	6	17.5	91.4	51.2	64.4	91.4	78.9	7.75	0.214	8	0.104
D-T Min M	-4.8	10.5	76.25	6	29.25	-50.4	67.4	56.3	50.4	55.9	7.75	0.152	8	0.074
D-T Max M	1.6	10.5	76.25	6	29.25	16.8	67.4	56.3	16.8	18.6	7.75	0.051	8	0.025