HN1	r D	The HNTB Companies	Made	KDG	Date	10/19/2011	Job Number	49633
-AIN	ID	Engineers Architects Planners	Checked	DSB	Date	10/19/2011		
For	Cleveland Inn	erbelt	Backchk'd	KDG	Date	10/19/2011	Sheet No.	

RFI 00121

There is a conflict between the drip plates on the Delta Legs and the walk ways that run down the delta leg.

The WT 4x24 members that support the walk way on the Delta Leg were originally designed with a maximum spacing of 12.125', and a maximum space of 2" for the edge of the flange to the walk way.

The actual maximum spacing of the supports is 10.125', and to clear the drip plates the walk way will need to be 3.5" from the edge of the flange.

Wt. of Grip Strut. = 7 PLF

P_DL = =7 * 10.125= 70.875 LB

LL = 85 PSF

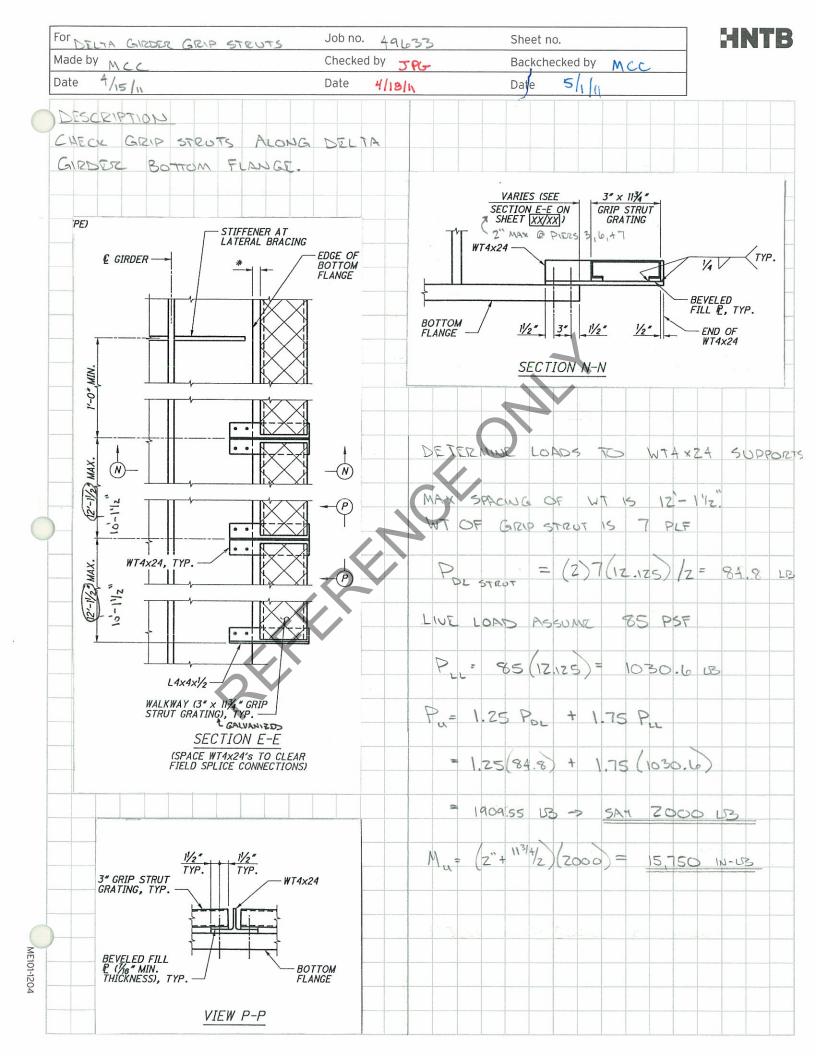
P_LL = =85 * 10.125= 860.625 LB

Pu = =1.25*P_DL+1.75* P_LL= 1594.688 LB

Mu = = (3.5"+11.75"/2)*Pu = 14950 in-lb

Mu Required = 14950 in-lb < Mu used in design = 15750 in-lb

Therefore it is OK to move the walk way along the Delta Leg to clear the drip plate.



FOR DELTA GIRDER GRIP STRUTS Job no. 49633 Sheet no.

Made by MCC Checked by JPG Backchecked by MCC

WT4×Z4 PROP	UZTIRS	M	=	TT /Z9	000 (30,5	11165)	0.97	6.87	7+114	6.827	1
A= 7.05 w2	Ix= 6.85 w+					8						-1
d= 4.25 m	5 = 1.97 w3											
tw= 0.400 w	1x = 0,986 in		=	520	1 488	+	197	<i>t.</i>	USR	М.	Mo=	10
b= 8.11 w	Z= 3.94 103									V1	W .	
tg= 0.685 W			M	= C	5 M	17		_				
FLANGE b = 8.1	1 0,400 Z = 3.855	5.63		= 1	.00	197						
F	0.685											
) - 0.30 E/- 0	$\frac{29000}{50} = 9.15$			=	197							
1 p = 0.58/F, = 0	.50 50	The second secon	M	_=	9711	K	> M		15.7	5	1.	0
swee 1/2 = Ap	FLANGE IS COMP	ACT	American					14				and the same of th
AASHTO 6.12.2.2	4	6	HES	3	(,	0.17,1	2 2					
					10	0.12 1	16.5	/				
$M_1 = M_0 = \overline{T}_1$	Z = 50(3.94)= 19	77.11-4	V,	p=0	.58	FAM	>t w	/				
						(50)	(4.2	5/0	,400)			-
LTB		24		+	49.	3 K						
M= T/EI,G	B+11+B2 =	No.	D		.25		10.	625				
		1	tw	(3.40	2						
I,= 30,5 12			\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	FX		17	zann	E	= 60	~ ~ ~		
	.385 (BACCO)= 11165	5 KG1		VF4		1 1	50		- 60	٠. ر	\	
				1	N	V						
D = 0.977 W Lb = USE Z" + 11314 Z	\$ 8"				10,6	75	460	.31	->	C	= \.(5
B= = = 23 d	I											
Lb			V	= 1	100=	CV	p= 1	.6(49.3)= 4	9.3	
	TRE IS IN TENS	1010,	V	-= ¢	N.	= 1.0	49,2)=	49.7	5 K		4
USE (+) 5	ددع		V-1		10		, ,					
B = + 7 - 2 4 - 2	5 30.5 - 6.82	27	1	r=	14.3	K	- 1	u= 7	2.0	14 .	·OK	=
7 (2,5)	5 \0.977											
	70,111											+

Job no. 49633 FOR DELTA GIRDER GRIP STRUTS Sheet no. Made by MCC Checked by 396 Backchecked by Mcc
Date 5/1/4

Data 4/	Cliecked by 365	Backchecked by MCC
Date 4/16/11	Date 4/18/11	Date 5/1/N
BOLTS	1,55	
	USE 1	MINIMUM GAGR PER AISC OF 512."
ASSUME WSIDE BELTS RESI	ST TUTIER I	
MONOUT.		100
		IP STRUT, TRY 5 DIAMOND PLAN
	1\3/4 \h	NIDE, USE 12 GA. STEEL.
Tb	57.00	A
		MCNICHOLS PRODUCT LOAD TABLE, T
	to 27.	A UNIFORMLY DISTRIBUTED LOAD (
	P	17 725.
4.5 MN 8"	2277	37 85 PSF PEDESTRIAN LOAD
T = 8"(P) = 8" (24/2 BOUT) 4.5" 4.5"	5)	Ok .
4,5" 4.5"		
		2 GA. 5 DIAMOND PLANK 113
= 1.8 K/BOC	T (T) wide.	SEE MCNICHOLS CUT SHEET F
		, THIS PRODUCT COMES IN
		COTITS, SO SPACWG OF WY
TRY USWG 518" A325 FO		TS MUST ACCOMODATE THIS,
CONVECTION TO GIRDER BO		C 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
TENSILE EXSISTANCE (6.13.20		IL: MILL- GALV. ASTM ASZ5
		F : 2405301210
Tn= 0.76 Ab		2.0350.20
= 0.76 (0.31) (120)		
= 27.98 ×		
T= 0 Tn= 0.8 (27.98)	: 27.4 K/BOLT	
7 22 1 4 5 - 2		
Tr= 22.4 k > Tu= 2.	LIOK	
USE 5/8" A325		
UDL 18 A325		
	District Control of the Control of t	