



SCI-823-0.00

PID No. 77366

S.R. 823 OVER WEBSTER STREET (S.R. 140)

PRELIMINARY DESIGN REPORT SUBMITTAL

Prepared for:

OHIO DEPARTMENT OF TRANSPORTATION

DISTRICT 9

650 EASTERN AVE.

CHILlicoTHE, OHIO 45601

JANUARY 14, 2008

Prepared by:

STRUCTURAL ENGINEERING

FEB 29 2008

RECEIVED





TranSystems

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January 14, 2008

Mr. Jawdat Siddiqi, PE
Office of Structural Engineering
Ohio Department of Transportation
1980 W. Broad Street
Columbus, Ohio 43223

**SUBJECT: Preliminary Design Report Submittal
SR 823 over Webster Street (SR 140)
SCI-823-0.00 Portsmouth Bypass
PID#77366**

Dear Mr. Siddiqi:

Submitted for review and comment is the Preliminary Design Report for SR 823 over Webster Street (SR 140). Included are The TS&L drawings and the Final Geotechnical Report by DLZ, Ohio, dated January 11, 2007. Please find below our disposition to the July 10, 2006 comments by Reza Zandi regarding the STS submittal.

Please verify the bridge limits stationing shown in the title block of site plan.

The limits have been revised in the attached plans.

Please don't hesitate to call me or Dr. Michael Lenett (513 621 1981) if there are any questions.

Sincerely,

Michael D. Weeks

Michael D. Weeks, P.E., P.S.
Project Manager

Cc: T. Barnitz, P.E.

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PRELIMINARY DESIGN REPORT

1. Introduction

TranSystems Corporation is providing engineering services to the Ohio Department of Transportation for the design of new left and right overpass structures that will carry the proposed S.R. 823 bypass over existing Webster Street (SR 140). As requested by the Scope of Services, a Preliminary Design Report is to be submitted as part of Step 8 of the Major PDP process. The purpose of this report is to summarize the structure type selected for final design. A revised Type Study was submitted on 5/12/06 to incorporate the updated roadway geometry. Comments were received from ODOT on 5/26/06. As a result of the comments a culvert was added in front of the MSE wall to convey the drainage under the bridge. The revised site plan and updated cost analysis were submitted on 6/2/06. Additional comments were received 6/15/06 and addressed on 6/27/06. Final comments on the Type Study were received July 10, 2006 and are incorporated into this submittal.

2. Design Criteria

The proposed structure will be designed according to the most current version of the Ohio Department of Transportation Bridge Design Manual and the 2002 AASHTO Standard Specifications for Highway Bridges, 17th Edition. Horizontal clearances (clear zone width and horizontal sight distance) are based on the Ohio Department of Transportation Location and Design Manual, Volume One – Roadway Design.

3. Subsurface Conditions and Foundation Recommendation

DLZ Ohio, Inc. performed the subsurface exploration for the proposed bridge and prepared the Final Bridge Foundation Recommendations dated January 11, 2007.

In summary, six test borings (B-15, B-16, B-17, TR-43, TR-44 and TR-45) were drilled and all encountered bedrock. The depth to bedrock varied across the site from 3' to 11' below existing ground. All borings encountered cohesive and granular soil deposits from stiff clay (A-7-6) to dense sandy silt (A-4a).

DLZ recommends spread footings, cast in place pile or drilled shafts to support the proposed abutments. The cast in place piles will be prebored 5' in to competent bedrock and grouted in place before the construction of the MSE walls. Driven H-piles are not recommended due to the depth of overburden/fill that needs to be placed on the existing rock cuts – the resulting depth of fill would provide insufficient lateral stability for driven H-piles.

The MSE walls were evaluated with respect to bearing capacity, sliding, overturning, global stability and settlement. The evaluations reveal that MSE walls can be used at the rear and forward abutment locations. At the rear abutment DLZ anticipates that the MSE wall will be founded on rock. At the forward abutment DLZ recommends the naturally occurring soils beneath the proposed MSE walls be overexcavated to top of rock and replaced with compacted, granular fill. MSE wall global stability safety factors are in excess of 1.5 therefore spread footings are acceptable at this location. As an alternative to undercutting the MSE walls the walls could be constructed in two stages up to 22'. DLZ's analysis indicates that a strap length of 0.95H was required to use the 22' stage height and maintain adequate stability factors for use with a spread footing.

4. Roadway

The purpose of this project is to construct a new bypass state route around the town of Portsmouth, Ohio. The proposed alignment will carry two lanes of traffic, 15 plus miles in either direction, from an interchange with US 52 just east of Portsmouth to another interchange with US 23, located north of Portsmouth in Valley Township.

The proposed structures are at the southern terminus of the proposed bypass, just north of the interchange with US 52. Due to their proximity to the terminus of the bypass, only a single ramp lane will cross over SR 140 in each direction. The section widens to 2~12'-0" lanes to the north, where the ramps for SR 140 join the mainline. The left and right structures are similar and will consist of a 16'-0" travel lane with 6'-0" median shoulders and 8'-0" outside shoulders. 1" opening centered about the centerline of construction and survey SR 823 will be positioned between the left and right bridges. A 4'-9" tall inside median barrier with a width of 1'-5 1/2" and a 1'-6" wide outside straight faced deflector parapet (standard drawing SBR-1-99) yield a deck width of 32'-11 1/2" out-to-out. This horizontal bridge layout maintains consistency with the proposed, and ODOT accepted roadway geometry and prevents alteration of the outside roadway edges. Horizontal and vertical sight distances, in accordance with the design standards, have been provided over the proposed bridge.

Vertical and Horizontal Clearances – Since the proposed vertical alignment for all overpass structures on this project was dictated by the overall design of the new bypass profile, vertical clearance was not a critical design issue for each alternative proposed herein. For this report, more than 17'-0" of preferred vertical clearance could be provided for each structure's alternatives considered. In accordance with the ODOT L&D manual, Volume 1, for the twin structures at Webster Street, a minimum horizontal clear zone width of 19'-0" from edge of traveled way to face of obstruction is required. The information input into Figure 600-1E is as follows:

1. the design speed is 45 mph;
 2. from June 2, 2005 OTS memo, the design ADT for SR 140 is 20600;
 3. maximum slopes of 6:1 foreslopes and 4:1 backslopes and maintain the drainage below the bridge on the left side of SR 140.
- wow!*

Alignment & Profile: The proposed mainline horizontal geometry is tangent along entire length of both the left and right structures. The cross section has a crown at the profile grade line with a break at the median shoulder in accordance with the BDM. The proposed mainline profile grade line is located on the inside edge of pavement for both bridges and is in a 1600' sag vertical curve, PVI= 66+50, El. 583.33, G1 = -0.5% and G2 = 5.0%. Embankment slopes will be a maximum of 2:1 in order to minimize right-of-way impacts.

The proposed alignment of SR 140 is tangent below the structures. East and west of the structures there are horizontal curves to the right however a normal crown is still able to be used. The proposed profile grade for SR 140 is in a 300' vertical curve, PVI= 11+00, El. 556.68, G1 = 0.42% and G2 = 3.12%. SR 140 will be widened to a three lane section with 10 foot shoulders on each side. The cross section will Guardrail along an existing ditch will be removed.

Pavement Drainage - The collection of storm water runoff will be addressed off of the bridge, thus scuppers will not be required. Pavement drainage systems have been designed and are shown in the accompanying site plans and general plan. Particular attention has been paid to the control of drainage around the MSE walls.

Utilities - No utilities will be placed on the bridge. However, lighting and ITS conduits will be provided as necessary. An existing waterline runs parallel to SR 140 approximately at the existing north edge of

pavement. A gas line also runs parallel to SR 140 on the north side, approximately 15'-0" off the existing edge of pavement. The gas line is approximately 10'-0" in front of the nearest MSE wall and under the proposed pavement. There is an existing aerial electric line also on the north side of SR 140 that will need to be relocated. There are no other utilities known at this point in time.

Maintenance of Traffic - While the new bridges are under construction, traffic will be maintained on existing Webster Street. It is anticipated that there will be limited closures during construction for beam setting.

5. Proposed Structure Configuration

Span Configuration: The proposed structure is comprised of a single span structure with span a length of 108'-0". The abutments are oriented parallel with the proposed tangent section of SR 140 giving a 21°35'48" right forward skew. Embankment slopes are supported by MSE walls approximately 20'-25' in height at both abutments. The forward MSE wall is set at the clear zone for SR 140 of 19'-0". The MSE wall at the rear abutment was set allow 2'-6" clearance to the 60" storm in front of the wall.

Substructure:

Abutments: The abutments will be semi-integral type supported on spread footings. The details of the abutments will follow ODOT Standard Construction drawings. Spread footing width was estimated from preliminary design reactions and used 4ksf as the allowable bearing pressure per BDM section 204.6.2.1. Drilled shaft and/or cast in place pile foundations were considered but eliminated as options due to the high construction costs. Driven piles were not recommended by the geotechnical engineer, as previously noted.

Superstructure:

The preliminary design of this alternative consists of are 4 - 72" AASHTO Type 4 Modified prestressed beams, spaced at 8'-8" with 3'-5 3/4" overhangs. The design loading applied was HS-25 with Alternate Military Loading and a future wearing surface of 60 psf. Details of the beams will follow ODOT standard construction drawings using standard 7000psi (final) concrete. Both the left and right bridge width will be 30'-0" from toe to toe of parapets with an overall bridge deck width of 33'-11 1/2". Deck thickness, including a 1" monolithic wearing surface, is 8 1/2".

APPENDIX A
Structure Plans




FIRST GUARDRAIL POST OFF BRIDGE LOCATIONS	
LOCATION	STATION
REAR ABUT. (NB)	61+39.47
REAR ABUT. (SB)	61+14.43
FWD. ABUT. (NB)	63+18.02
FWD. ABUT. (SB)	62+92.98

BENCHMARK 1	BENCHMARK 2
(TO BE PROVIDED LATER)	(TO BE PROVIDED LATER)

TRAFFIC DATA	
(S.R. 823)	
CURRENT YEAR ADT (2010)	- 13,400
DESIGN YEAR ADT (2030)	- 21,000
CURRENT YEAR ADTT (2010)	- 1,876
DESIGN YEAR ADTT (2030)	- 2,940

NOTES:

- ALL SHEETS WITH PLAN DIMENSIONS ARE SHOWN HORIZONTAL.
- EARTHWORK LIMITS SHOWN ARE APPROXIMATE. ACTUAL SLOPES SHALL CONFORM TO PLAN CROSS SECTIONS.
- THE PROPOSED PROFILE GRADE IS WITHIN BRIDGE LIMITS. SEE ROADWAY PLANS FOR PAVEMENT ELEVATIONS BEYOND BRIDGE LIMITS.
- FOR CULVERT DETAILS SEE SHEET .

LEGEND

- BTA-1 - BRIDGE TERMINAL ASSEMBLY TYPE 1
- BTA-2 - BRIDGE TERMINAL ASSEMBLY TYPE 2
-  - BORING LOCATION

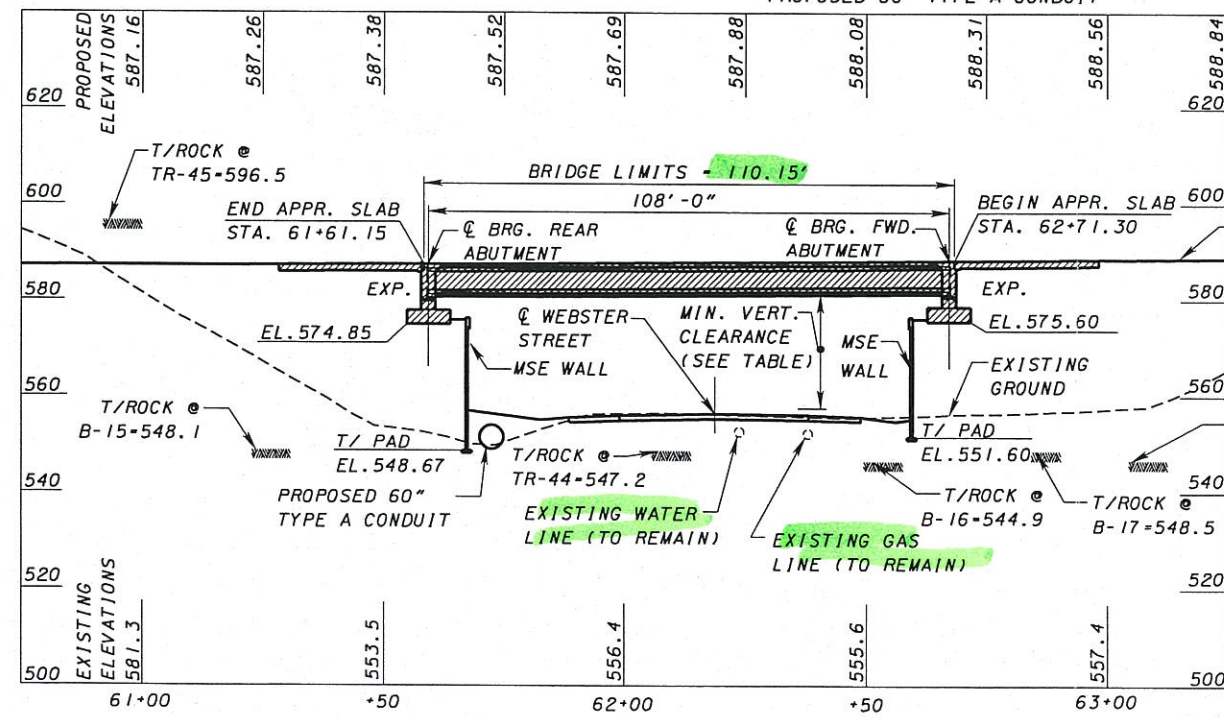
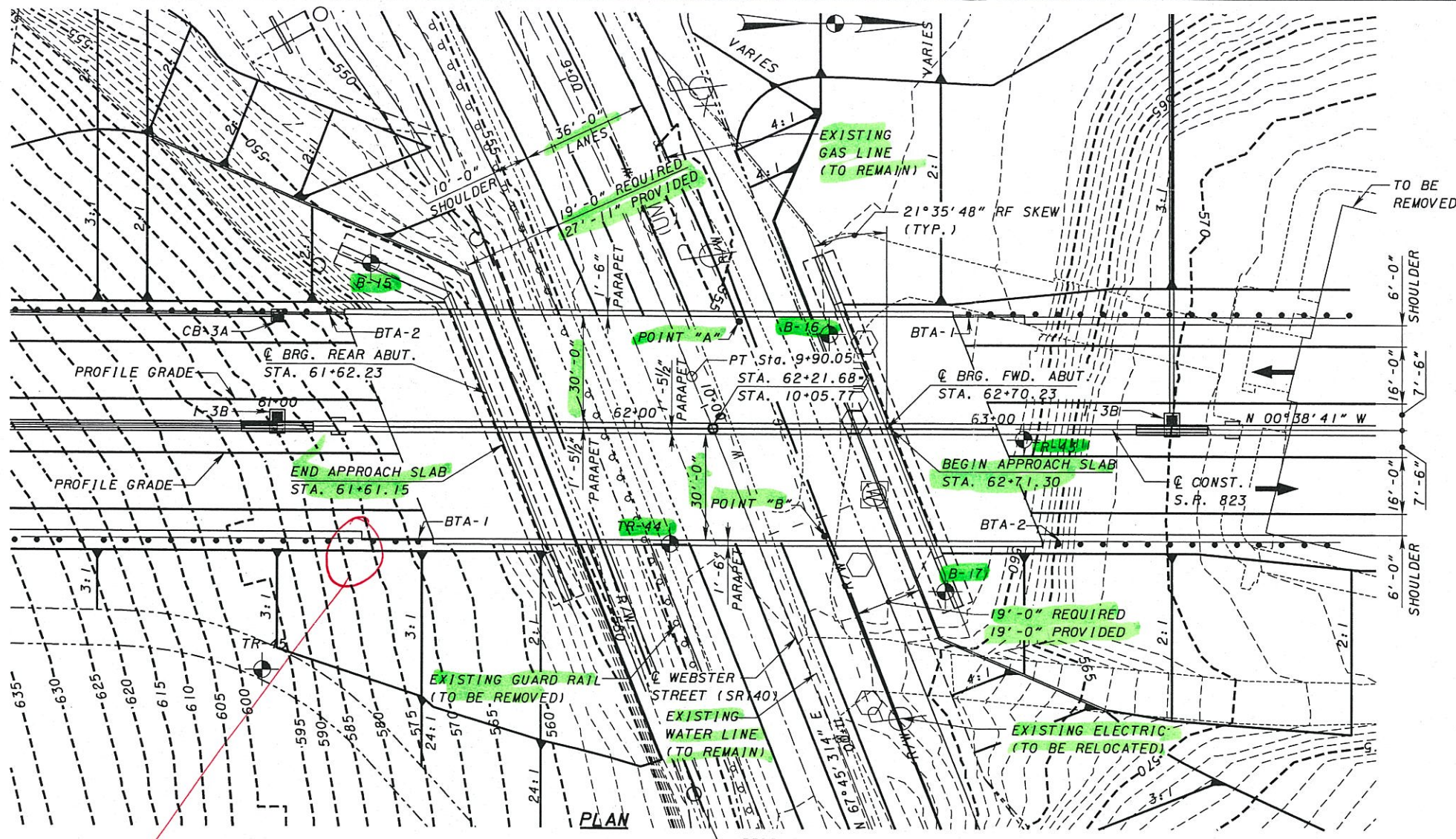


TABLE OF VERTICAL CLEARANCES		
LOCATION	"A"	"B"
PROPOSED	24.09'	23.66'
PREFERRED	17.0'	17.0'

1600' VERT. CURVE DATA
P.V.I. STA. - 66+50.00
P.V.I. EL. - 583.33
G₁ - -0.50%
G₂ - 5.00%

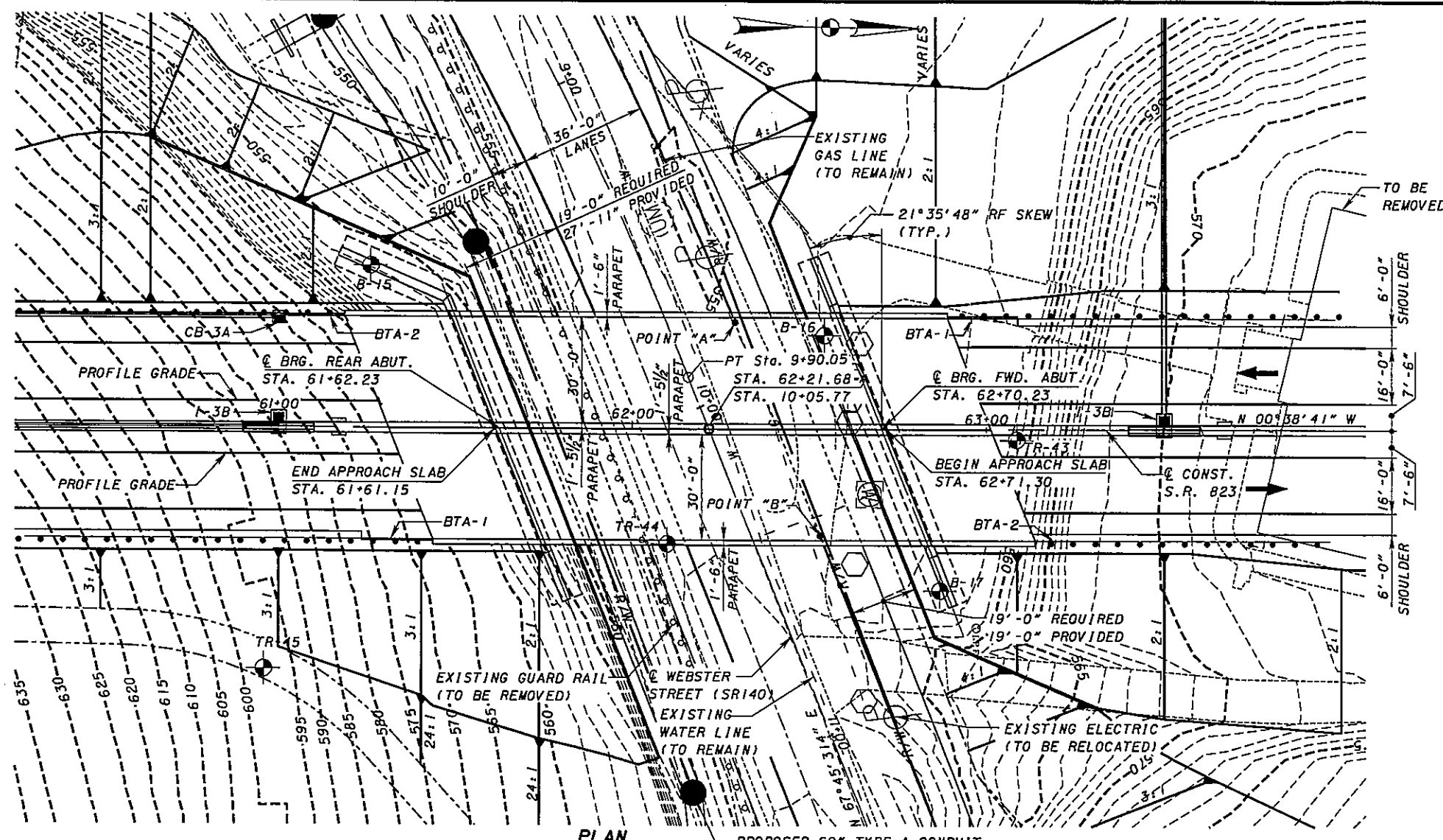
PROPOSED STRUCTURE

TYPE: SINGLE SPAN 72" MODIFIED AASHTO TYPE 4 PRESTRESSED CONCRETE I-BEAMS WITH COMPOSITE REINFORCED CONCRETE DECK ON SEMI-INTEGRAL ABUTMENTS AND MSE WALL SUPPORTED EMBANKMENTS.

SPANS: 108'-0" C/C BEARING
ROADWAY: 2 - 30'-0" T/T PARAPETS
LOADING: HS-25 AND ALTERNATE MILITARY LOADING, FWS-60 PSF
SKEW: 21°35'48" RF
CROWN: 0.016 FT/FT
ALIGNMENT: TANGENT
WEARING SURFACE: MONOLITHIC CONCRETE
APPROACH SLABS: AS-1-81 (30'-0" LONG)
LATITUDE: 82° 52' 23" N
LONGITUDE: 38° 45' 14" W

PROFILE ALONG PROFILE GRADE S.R. 823 LEFT BRIDGE

Drainage



FIRST GUARDRAIL POST OFF BRIDGE LOCATIONS	
LOCATION	STATION
REAR ABUT. (NB)	61+39.48
REAR ABUT. (SB)	61+14.43
FWD. ABUT. (NB)	63+18.02
FWD. ABUT. (SB)	62+92.98

BENCHMARK 1	BENCHMARK 2
(TO BE PROVIDED LATER)	(TO BE PROVIDED LATER)

TRAFFIC DATA	
(S.R. 823)	
CURRENT YEAR ADT (2010)	- 13,400
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CURRENT YEAR ADTT (2010)	- 1,876
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 - FOR CULVERT DETAILS SEE SHEET []

- LEGEND**
- BTA-1 - BRIDGE TERMINAL ASSEMBLY TYPE 1
 - BTA-2 - BRIDGE TERMINAL ASSEMBLY TYPE 2
 - ⊙ - BORING LOCATION

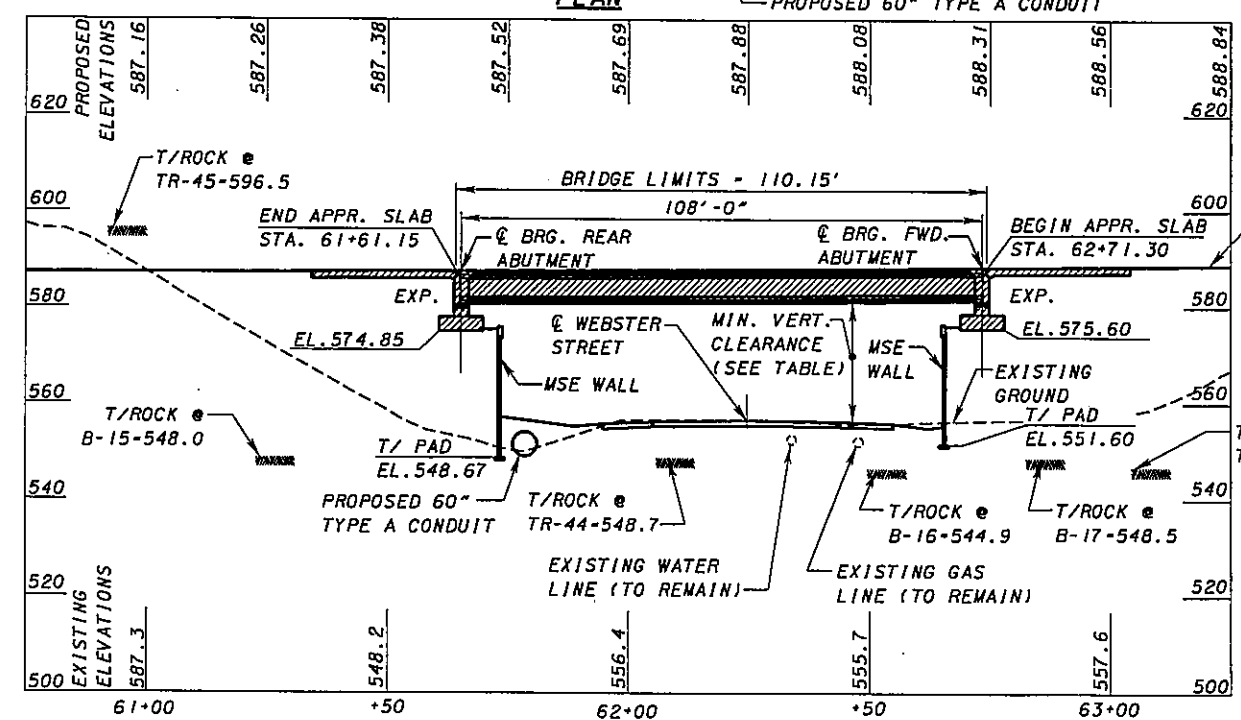


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1600' VERT. CURVE DATA

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P.V.I. EL. - 583.33

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SPANS: 108'-0" C/C BEARING

ROADWAY: 2 - 30'-0" T/T PARAPETS

LOADING: HS-25 AND ALTERNATE MILITARY LOADING, FWS-60 PSF

SKREW: 21°35'48" RF

CROWN: NORMAL, 0.016 FT/FT

ALIGNMENT: TANGENT

WEARING SURFACE: MONOLITHIC CONCRETE

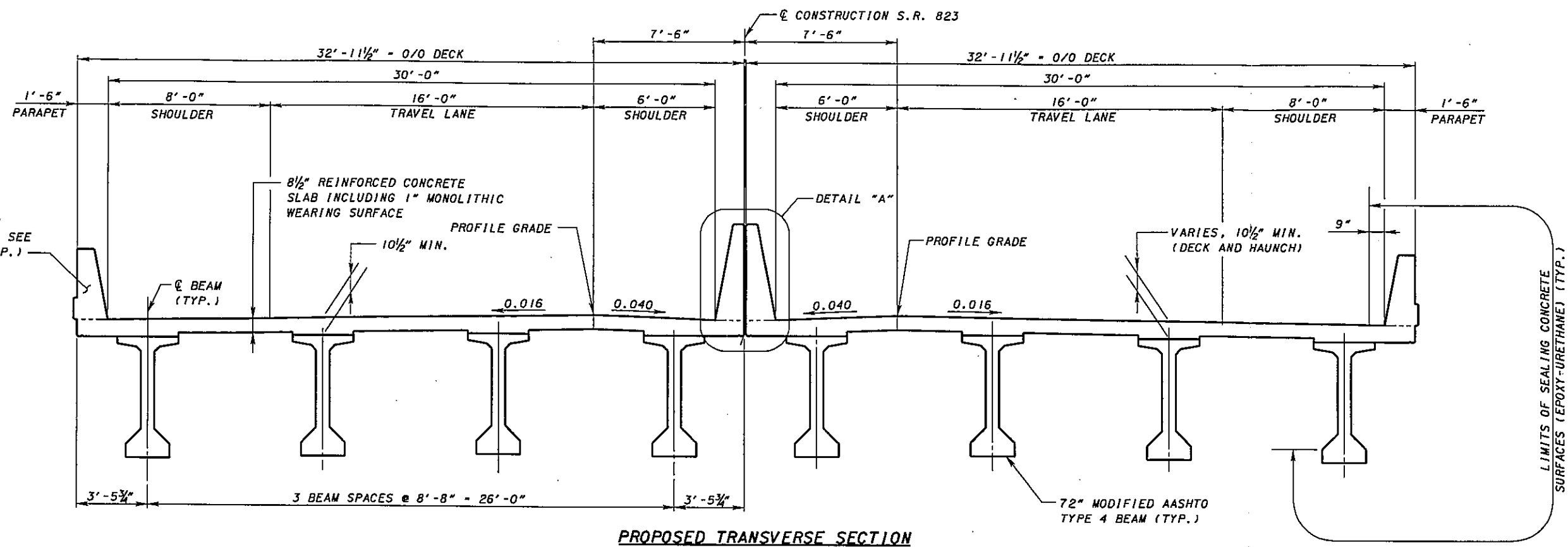
APPROACH SLABS: AS-1-81 (30'-0" LONG)

LATITUDE: 82° 52' 23" N

LONGITUDE: 38° 45' 14" W

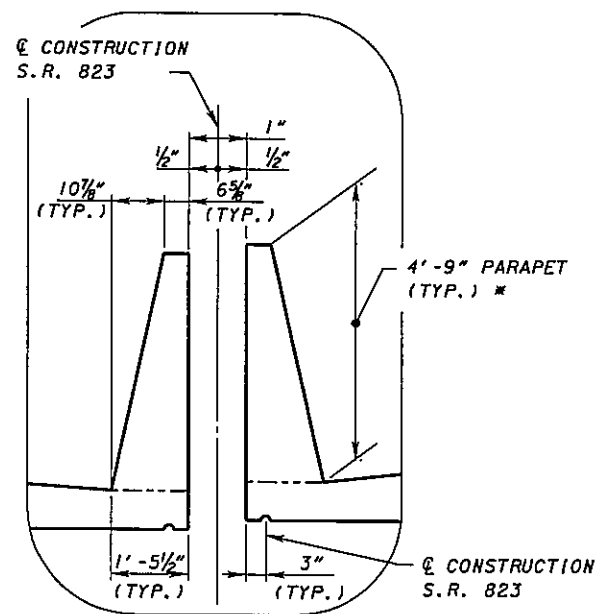
DESIGN AGENCY: **TranSystems**
 DATE: 6/11/07
 REVISION: MSL
 STRUCTURE FILE NUMBER: 730631B
 DRAWN: CAS
 CHECKED: MTN
 DESIGNED: PJP
 MSL
 SCIOTO COUNTY STA. 61+61.15 STA. 62+71.30
 BRIDGE NO. SCI-823-017 R
 S.R. 823 OVER WEBSTER STREET (SR 140)
 SCI-823-0.00
 PID 77366
 2/7
 814
 847

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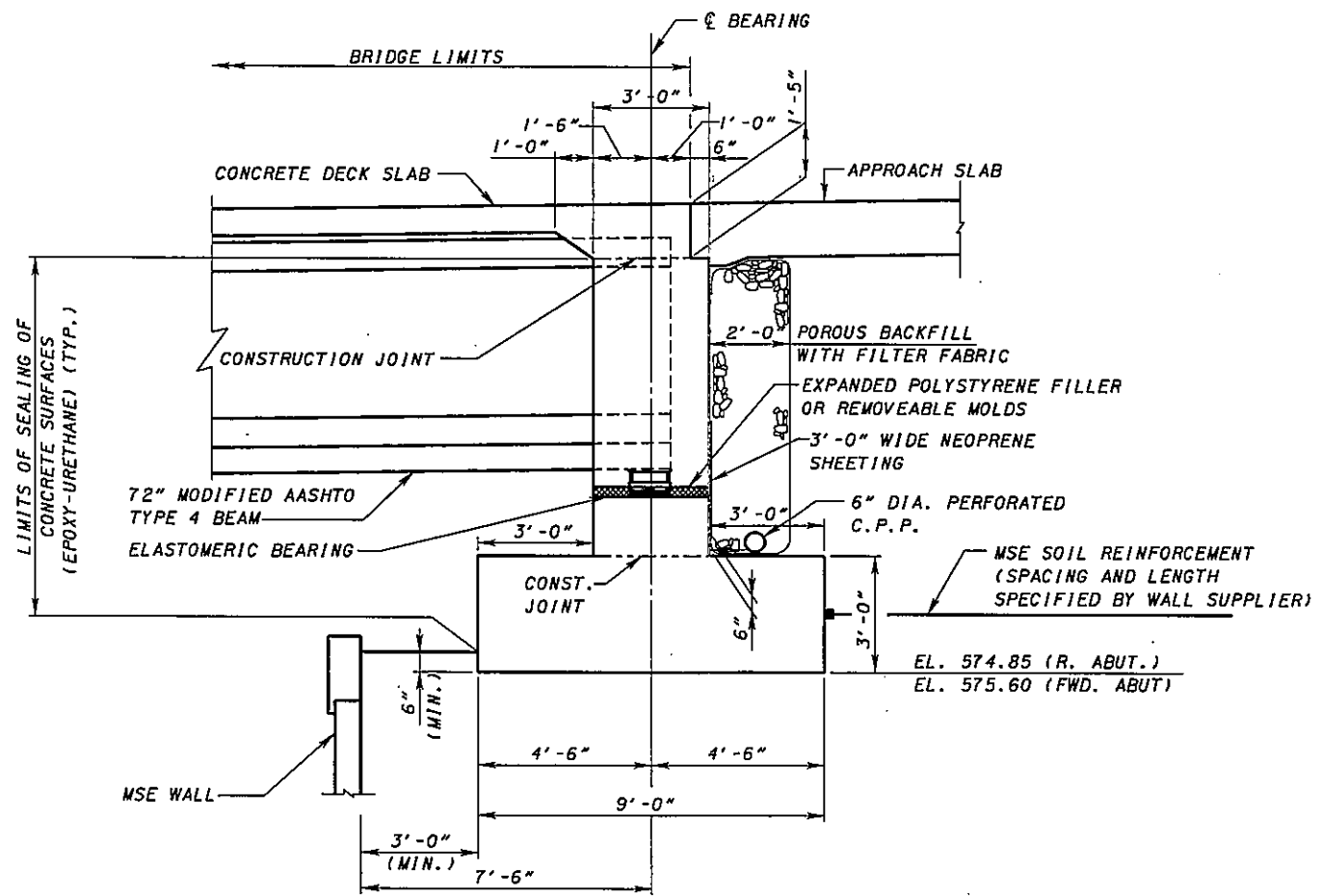
PROPOSED TRANSVERSE SECTION

SUPERSTRUCTURE DEPTH	
ITEM	72" MODIFIED AASHTO TYPE 4 I-BEAM
SLAB (INCLUDING WEARING SURFACE)	8 1/2"
HAUNCH (BOTTOM OF SLAB TO TOP OF FLANGE)	2"
GIRDER DEPTH	72"
TOP OF WEARING SURFACE TO BOTTOM OF GIRDER FLANGE (INCH)	82.5"
TOP OF WEARING SURFACE TO BOTTOM OF GIRDER FLANGE (FEET)	6.875'



DETAIL "A"
 (NOT SHOWN TO SCALE)

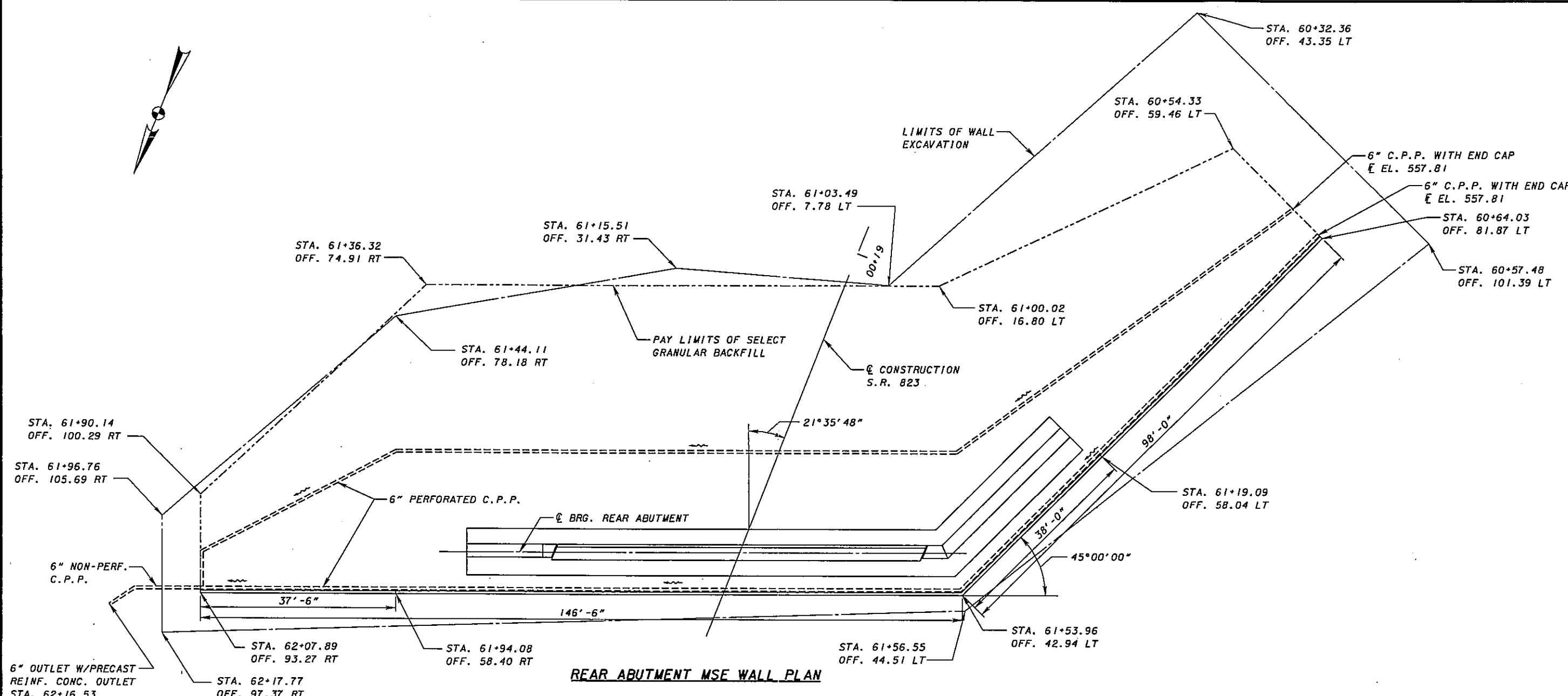
* PARAPETS ARE SIMILAR TO ROADWAY CONCRETE MEDIAN BARRIER



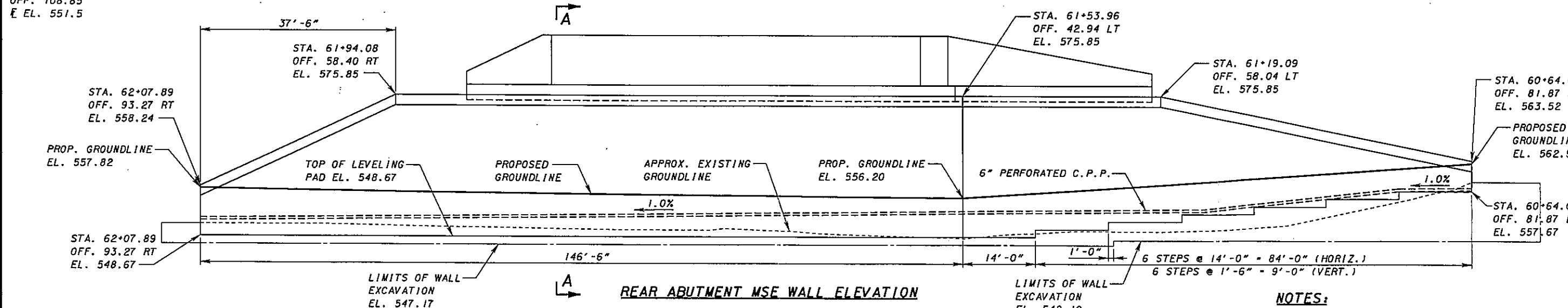
PROPOSED ABUTMENT SECTION



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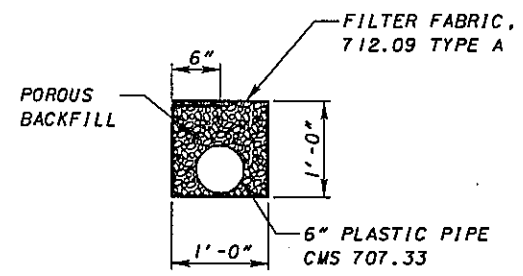
REAR ABUTMENT MSE WALL PLAN



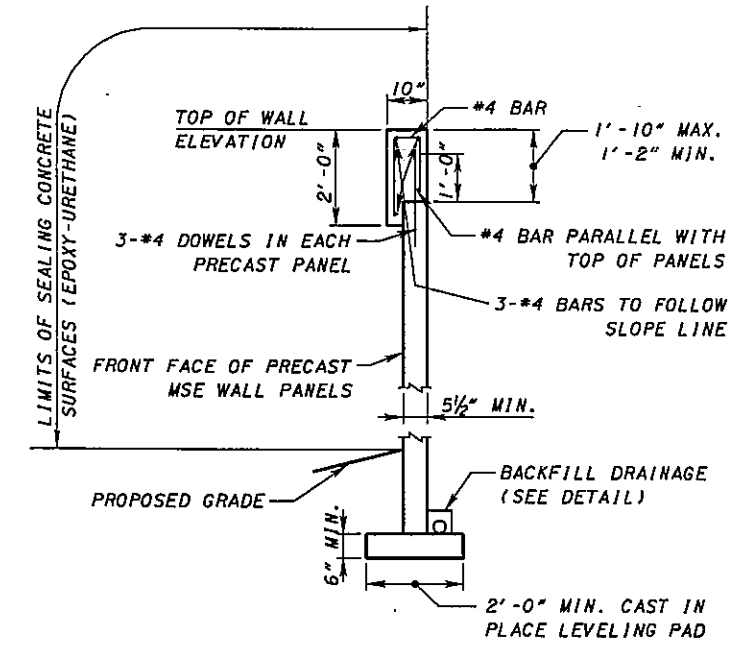
REAR ABUTMENT MSE WALL ELEVATION

- NOTES:**
1. WALL LOCATIONS GIVEN TO FRONT FACE OF MSE WALL PANELS.
 2. WALL ELEVATIONS GIVEN TO TOP OF LEVELING PAD AND TOP OF MSE WALL COPING.
 3. SEE SHEET FOR SECTION A-A.

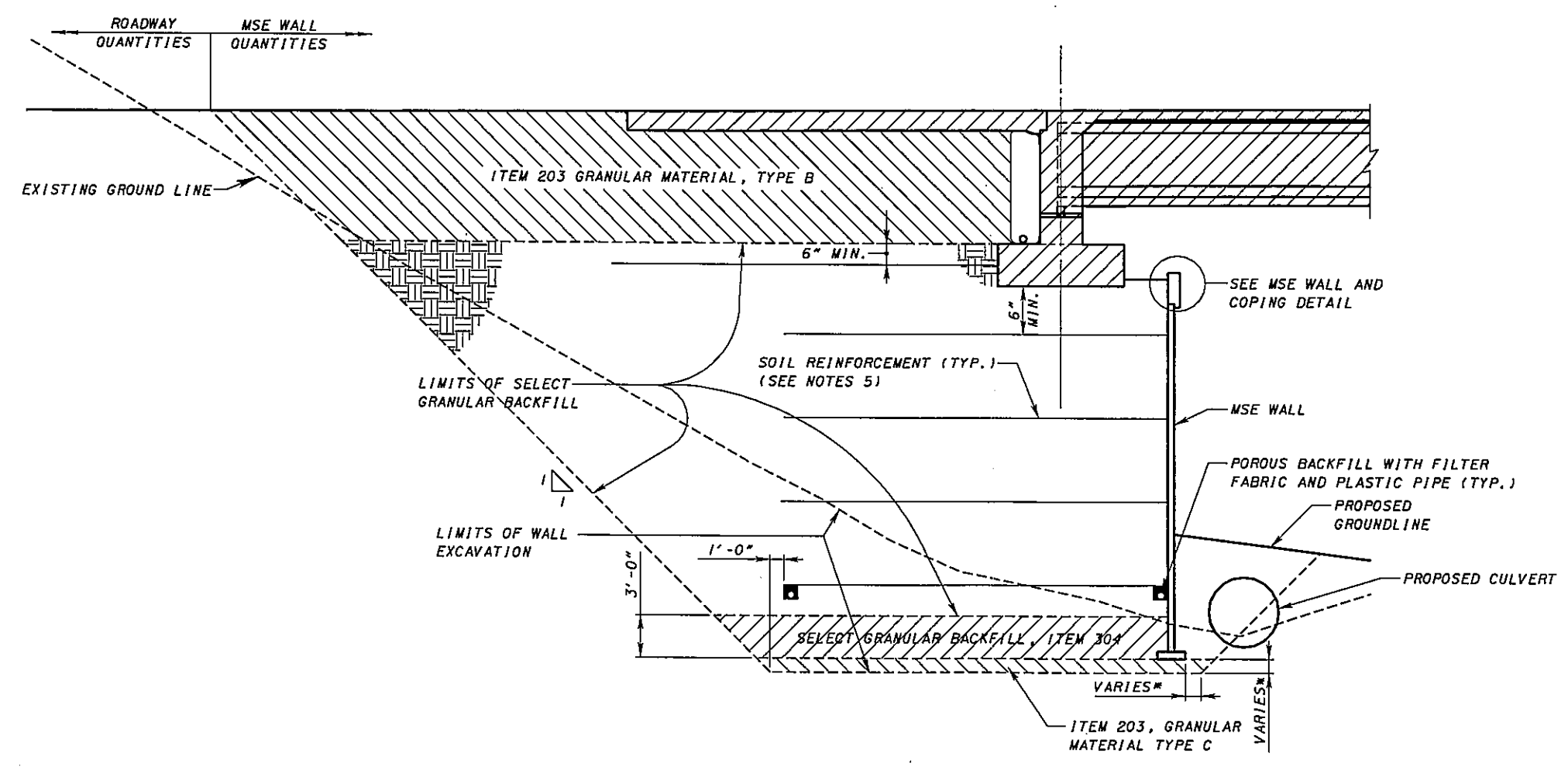
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			S.R. 823 OVER WEBSTER STREET (SR 140)
SC1-823-0.00 PID 77366		REAR ABUT. MSE WALL PLAN & ELEVATION	
4 / 7 			



BACKFILL DRAINAGE DETAIL



MSE WALL AND COPING DETAIL



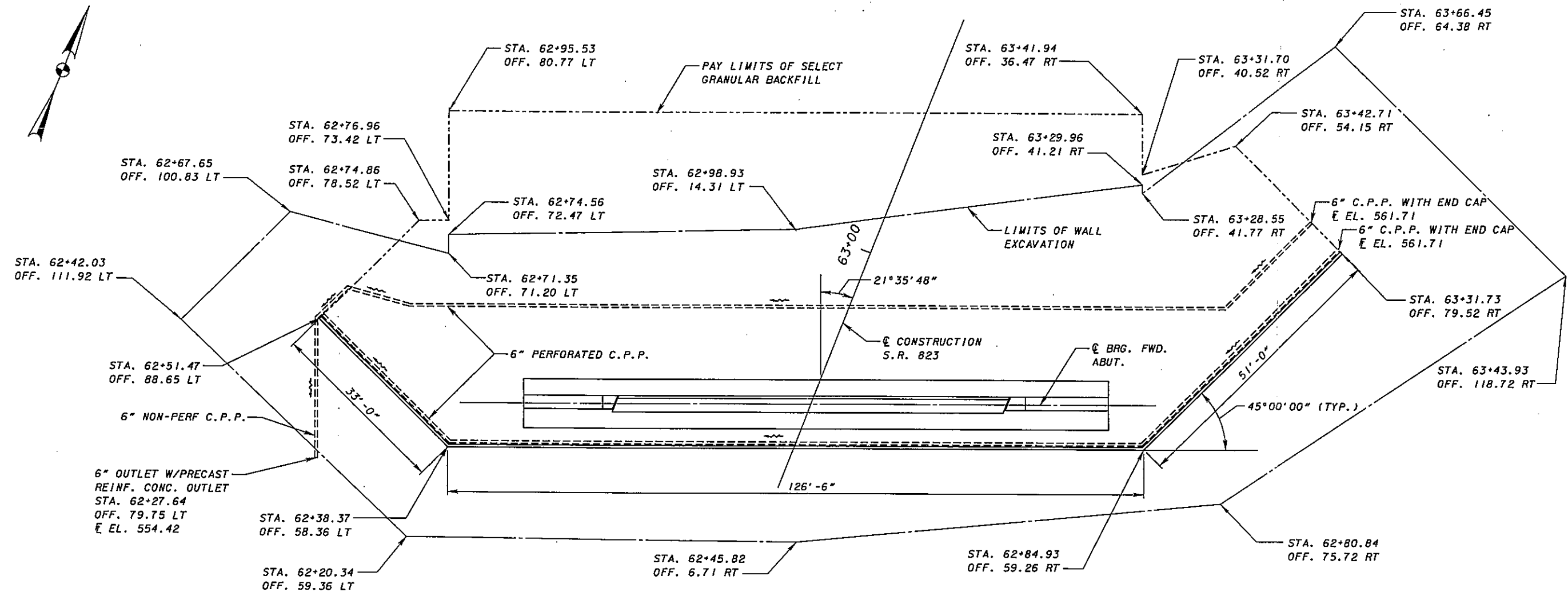
SECTION A-A

* SEE MSE WALL ELEVATION FOR ELEVATION OF EXCAVATION LIMIT

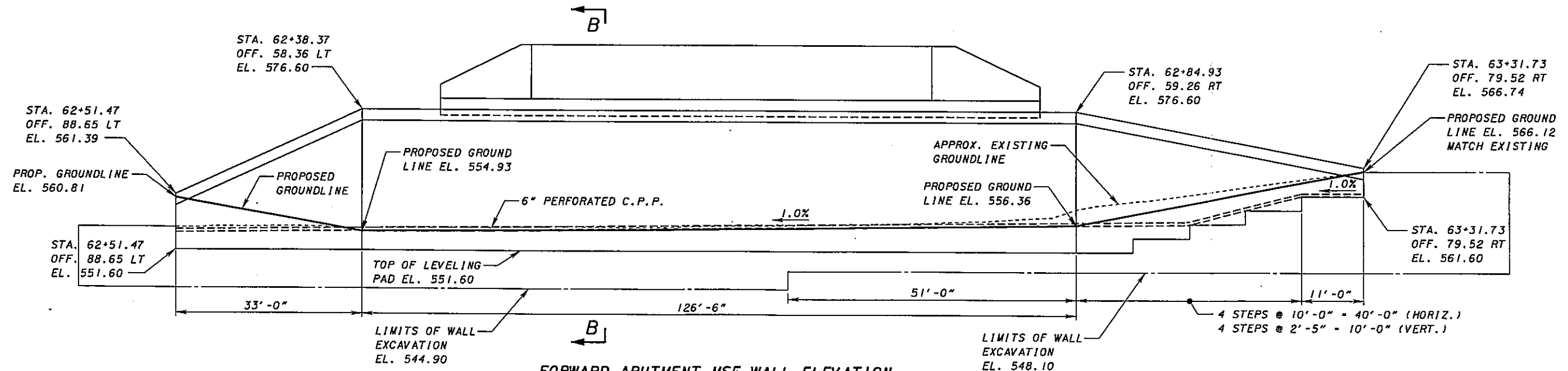
NOTES:

1. SEE SITE PLAN DRAWING FOR BORING LOCATIONS AND APPROX. TOP OF ROCK ELEVATIONS.
2. THE SLOPING LINE WHICH DEFINES THE LIMIT OF THE SELECT GRANULAR BACKFILL IS NOT AN ALLOWABLE SLOPE FOR EXCAVATION. CUT THE SIDES OF ALL EXCAVATIONS TO PREVENT CAVING OR PROTECT THE EXCAVATIONS FROM CAVING.
3. ALL REINFORCING STEEL TO BE EPOXY COATED.
4. WALL EXCAVATION SHALL EXTEND TO A LEVEL BEDROCK SURFACE. THE DEPARTMENT WILL APPROVE WALL EXCAVATION PRIOR TO FOUNDATION PREPARATION.
5. PROPRIETARY RETAINING WALL DATA: THE PROPRIETARY WALL SUPPLIER SHALL DESIGN THE INTERNAL STABILITY OF A MECHANICALLY STABILIZED EARTH (MSE) WALL IN ACCORDANCE WITH THE SPECIAL PROVISIONS TO SUPPORT THE ABUTMENT. THE DESIGN FOR INTERNAL STABILITY SHALL INCLUDE AN UNFACTORED HORIZONTAL STRIP LOAD FROM THE SUPERSTRUCTURE OF _____ K/FT APPLIED PERPENDICULAR TO THE FACE OF WALL AT THE BASE OF THE CONCRETE FOOTING.

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FORWARD ABUTMENT MSE WALL PLAN



FORWARD ABUTMENT MSE WALL ELEVATION

- NOTES:**
1. WALL LOCATIONS GIVEN TO FRONT FACE OF MSE WALL PANELS.
 2. WALL ELEVATIONS GIVEN TO TOP OF LEVELING PAD AND TOP OF MSE WALL COPING.
 3. SEE SHEET [] FOR SECTION B-B.

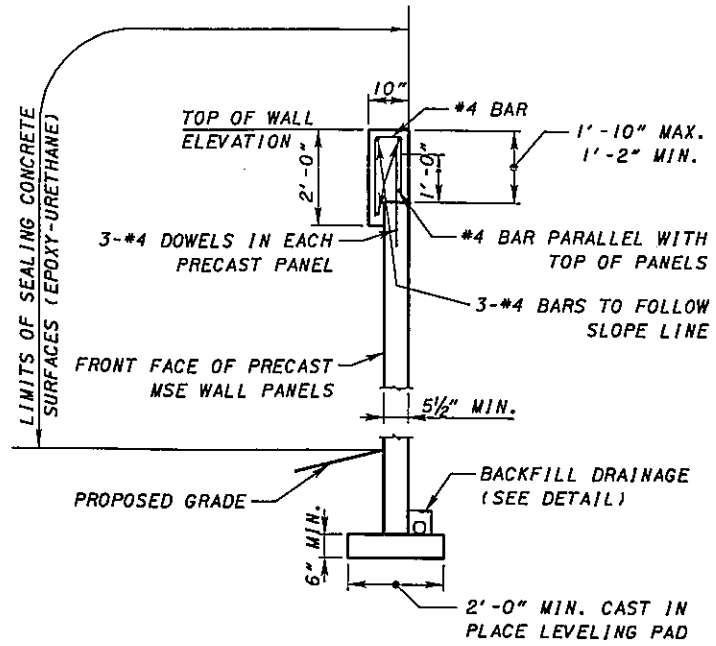
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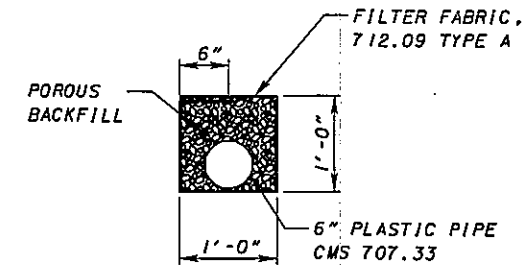
DESIGNED	MTN	CHECKED	PJP
DRAWN	MTN	REVISED	
REVIEWED	MSL	DATE	6/11/07
STRUCTURE FILE NUMBER	7306296L, 7306316R		

FORWARD ABUT. MSE WALL PLAN & ELEVATION
 BRIDGE NO. SCI-823-017 L&R
 S.R. 823 OVER WEBSTER STREET (SR 140)

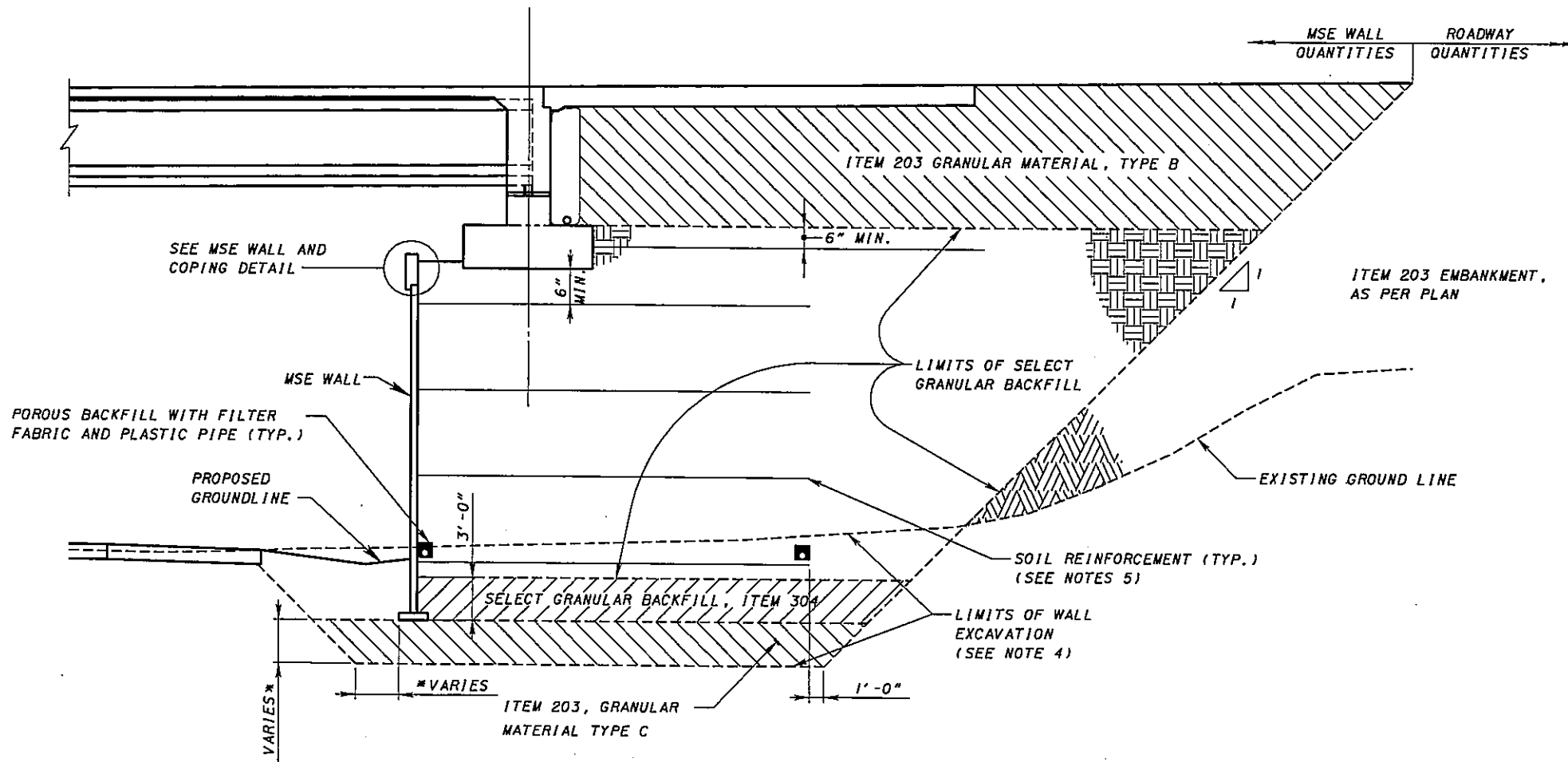
SCI-823-0.00
 PID 77366



MSE WALL AND COPING DETAIL



BACKFILL DRAINAGE DETAIL



SECTION B-B

* SEE MSE WALL ELEVATION FOR ELEVATION OF EXCAVATION LIMIT

NOTES:

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5/8/2008 9:50:03 AM 0064\bridge\cn\brs\04-rl\40\webster\1\ts&l\823_017\msefw\02.dgn

DESIGNED	DATE	REVIEWED	DATE
MTN	6/11/07	MSL	6/11/07
CHECKED	FILE NUMBER	STRUCTURE	FILE NUMBER
PJP		73062961	73063188

FORWARD ABUT. MSE WALL DETAILS
 BRIDGE NO. SCI-823-017 L&R
 S.R. 823 OVER WEBSTER STREET (SR 140)

SCI-823-0.00
 PID 77366

APPENDIX B
Structure Cost Estimate



SCI-823-0.00 - PORTSMOUTH BYPASS

S.R. 823 over Webster Street (S.R. 140) L&R

STRUCTURE TYPE STUDY

By: PJP
Checked: MSL

Date: 6/11/2007
Date:

ALTERNATIVE COST SUMMARY

Alternative No.	Span Arrangement		Total Span Length (ft.)	Framing Alternative	Proposed Stringer Section	Subtotal Superstructure Cost	Subtotal Substructure Cost	Structure Incidental Cost (16%)	Structure Contingency Cost (20%)	Total Alternative Const. Cost	Life Cycle Maintenance Cost	Total Relative Ownership Cost
	No. Spans	Lengths										
1	1	108'-0"	108.00	4 Prestressed Concrete Girders /per BRIDGE	AASHTO Type 4 Modified (72")	\$707,000	\$858,000	\$250,400	\$0	\$1,820,000	\$0	\$1,820,000

NOTES:

- Structure incidental cost allowance includes provision for structure excavation, porous backfill, sealing of concrete surfaces, bearings, and crushed aggregate slope protection costs.
- Estimated construction cost does not include existing structure removal (if any), which should be quantified seperately, if required.

SCI-823-0.00 - PORTSMOUTH BYPASS
S.R. 823 over Webster Street (S.R. 140) L&R

STRUCTURE TYPE STUDY - PRESTRESSED CONCRETE GIRDER ALTERNATIVE 1 - SUPERSTRUCTURE

By: PJP
 Checked: MSL

Date: 6/11/2007
 Date: 1/0/1900

SUPERSTRUCTURE

Alternative No.	Span Arrangement No. Spans	Lengths	Total Span Length (ft.)	Deck Length (ft.)	Deck Volume (cu. yd.)	Deck Concrete Cost	Deck Reinforcing Cost	Approach Slab Cost	Approach Roadway Cost	Framing Alternative	Proposed Girder Section	Prestressed Concrete Cost	Subtotal Superstructure Cost
1	1	108'-0"	108.00	110.00	379	\$204,300	\$96,200	\$86,200	\$0	4 Prestressed Concrete Girders /per BRIDGE	AASHTO Type 4 Modified (72")	\$320,280	\$707,000

COST SUPPORT CALCULATIONS

Deck Cross-Sectional Area:

Parapets:		No.	Individual Area (sq. ft.)	Parapet Area (sq. ft.)	Slab:			
Parapets	1	4.77	4.77	T (ft.)	W (ft.)	Slab Area	Haunch & Overhang Area	Total Concrete Area (sq. ft.)
Parapets	1	4.26	4.26	0.71	33.00	23.4	2.3	34.7
				0.71	33.00	23.4	2.3	34.7

Note: Deck width is out to out
 10% of deck area allowed for haunches and overhangs.

QC/QA Concrete, Class QSC2

Unit Cost (\$/cu. yd.):

	Year 2005	Annual Escalation	Year 2007
Deck	\$525.00	5.0%	\$579.00
Parapets	\$385.00	5.0%	\$424.00
Weighted Average =			\$539.00

Based on parapet and slab percentages of total concrete area

Epoxy Coated Reinforcing Steel

Unit Cost (\$/lb):
 Assume 285 lbs of reinforcing steel per cubic yard of deck concrete

	Year 2005	Annual Escalation	Year 2007
Deck Reinforcing	\$0.81	5.0%	\$0.89

Prestressed Concrete Girders

Unit Costs:

	Year 2005	Annual Escalation	Year 2007	No. Required	
AASHTO Type IV Beams					
Pier Diaphragms	\$1,800 ea.	5.0%	\$1,980 ea.	0	\$0
Abutment Diaphragms	\$1,200 ea.	5.0%	\$1,320 ea.	0	\$0
Intermediate Diaphragms	\$905 ea.	5.0%	\$1,000 ea.	18	\$18,000
Modified Type 4 I-Beams (72")	\$300 per ft.	5.0%	\$330 ea.	916	\$302,280
					\$320,280

Construction Complexity Factor

Percent of Superstructure = 0% Due to Deck forming, Screed and Varying Girder Spaces

Reinforced Concrete Approach Slabs (T=17")

Unit Cost (\$/sq. yd.):
 Length = 30 ft. Width = 66 ft.
 Area = 440 sq. yd.

	Year 2005	Annual Escalation	Year 2007
Approach Slabs	\$178.00	5.0%	\$196.00

Approach Roadway

	Year 2005	Annual Escalation	Year 2007	
Embankment fill	0.00 cu.yd.	\$4.00	5.0%	\$4.41
Roadway incl. base	0.00 sq.yd.	\$26.00	5.0%	\$28.67
Barrier (single faced)	0 ft.	\$50.00	5.0%	\$55.13
Barrier (dbl faced)	0 ft.	\$80.00	5.0%	\$88.20

SCI-823-0.00 - PORTSMOUTH BYPASS
S.R. 823 over Webster Street (S.R. 140) L&R

STRUCTURE TYPE STUDY - PRESTRESSED CONCRETE GIRDER ALTERNATIVE 1 - SUBSTRUCTURE

By: PJP
 Checked: MSL

Date: 6/11/2007
 Date: 1/0/1900

SUBSTRUCTURE

Alternative No.	Span Arrangement No. Spans Lengths	Framing Alternative	Proposed Stringer Section	Pier Concrete Cost	Pier Reinforcing Cost	Abutment Concrete Cost	Abutment Reinforcing Cost	Pile Foundation Cost	MSE Wall Cost	Additional Crane Cost	Subtotal Substructure Cost
1	1 108'-0"	4 Steel Girders /per BRIDGE	AASHTO Type 4 Modified (72")	\$0	\$0	\$143,100	\$24,800	\$0	\$614,900	\$75,000	\$858,000

COST SUPPORT CALCULATIONS

Pier QC/QA Concrete, Class QSC1 Cost: (Spread Footing)

Component	Volume (cu. yd.)	Year 2005	Annual Escalation	Year 2007	Total Cost
Cap	0	\$575.00	5.0%	\$634.00	\$0
Stem	0	\$575.00	5.0%	\$634.00	\$0
Footings	0	\$300.00	5.0%	\$331.00	\$0
Total	0				\$0

Pile Foundation Unit Cost (\$/ft.):

HP 12X53 Piles, Furnished & Driven

Number of Piles	Total Pile Length
0	0

SEE QUANTITY CALCULATIONS

Pile Foundation Unit Cost (\$/ft.):

2005 Unit Cost	Annual Escalation	Year 2007
\$26.47	5.0%	\$29.20
\$9.62	5.0%	\$10.60
Total		\$39.80

Shaft Foundation Unit Cost (\$/ft.):

36" Drilled Shaft

Furnished	Driven	Total	Number of Shafts	Total Shaft Length
			0	0

SEE QUANTITY CALCULATIONS

Shaft Foundation Unit Cost (\$/ft.):

Unit Cost	Escalation	2007
\$125.00	5.0%	\$145.00

Cost of Shafts: \$ -

Temporary Shoring and Support

Unit Costs (\$/sq. ft.):

Temp. Shoring Area (sq. ft.)	Temp. Girder Support (lump sum)
Alt. 1 0	\$ -

MSE Abutment Unit Cost (\$/sq. ft.):

Total Area (sq. ft.)	Year 2005 Unit Cost	Annual Escalation	Year 2007
Alt. 1 10,005	\$50.00	5.0%	\$55.10

Epoxy Coated Reinforcing Steel

Unit Cost (\$/lb):

Assume 125 lbs of reinforcing steel per cubic yard of pier concrete.
 Assume 90 lbs of reinforcing steel per cubic yard of abutment concrete.

Year 2005	Annual Escalation	Year 2007	MSE Abutment Undercut Cost: Alternative No.	Total Area (sq. ft.)	Depth (ft.)	Volume (cu. yd.)	Year 2005 Unit Cost	Annual Escalation	Year 2007	Additional Crane Cost
\$0.81	5.0%	\$0.89	1	8,764	3.25	1050	\$55.00	5.0%	\$60.60	\$ 75,000

**SCI-823-0.00 - PORTSMOUTH BYPASS
S.R. 823 over Webster Street (S.R. 140) L&R**

STRUCTURE TYPE STUDY - PRESTRESSED CONCRETE GIRDER ALTERNATIVE 1 - QUANTITY CALCULATIONS

By: PJP
Checked: MSL

Date: 6/11/2007
Date: 1/0/1900

Pier Quantities														
Pier Location	Length	Cap				Stem				Footing				Total Volume
		Width	Depth	Area	Volume	Width	Height	Length	Volume	Width	Depth	Length	Volume	
Pier 1 (Spr Ftg)	0	0	0	0.00	0	0	0	0.00	0	0	0	0.00	0	0
Pier 2														0
Pier 3														0
Pier 4														0
Pier 5														0
Pier 6														0
Pier 7														0
Total (Cu.Ft.)					0				0					0
Total (Cu.Yd.)					0				0					0
		Qty x 2 (L/R)				0			0					0

Pile Quantities													
Location	Load/girder (Kips)	# Girders	Total Girder Load	Subst Wt (kips)	Pile Cap.(Kips)	No. Piles	Increase Factor	Total Piles	Top Elev.	Bot Elev.	Pile Length	Total Pile Length (Feet)	
Rear Abut.	0	0	0	0	140	0	1	0	575.3	550.0	25.0	0	
Pier 1	0	0	0	0	140	0	1	0	0	0	0.0	0	
Pier 2	0	0	0	0	140	0	1	0	0	0	0.0	0	
Pier 3	0	0	0	0	140	0	1	0	0	0	0.0	0	
Pier 4	0	0	0	0	140	0	1	0	0	0	0.0	0	
Pier 5	0	0	0	0	140	0	1	0	0	0	0.0	0	
Pier 6	0	0	0	0	140	0	1	0	0	0	0.0	0	
Pier 7	0	0	0	0	140	0	1	0	0	0	0.0	0	
Fwd. Abut.	0	0	0	0	140	0	1	0	576.1	550	30.0	0	
Total								0				0	
								Qty x 2 (L/R)				0	

Abutment Quantities *														
Abut Location	Length (feet)	Backwall				Beam Seat				Footing				Total Volume
		Width	Depth	Area	Volume	Width	Height	Area	Volume	Width	Depth	Area	# Footitl Volume	
Rear Abut	0	0	0	0.00	0	0	1.5	0.00	0	0	3	0	1	0
Fwd. Abut	0	0	0	0.00	0	0	1.5	0.00	0	0	3	0	1	0
Total (Cu.Ft.)					0				0				0	0
Total (Cu.Yd.)					0				0				0	0
		Qty x 2 (L/R)				0			0					0

* Includes Wingwalls

MSE Abutment Wall Quantities				
Abut Location	Wall			
	Height	Length	Area	Volume
Rear Abut	0	0	0	0
RA Wing (L)	0	0	0	0
RA Wing (R)	0	0	0	0
Fwd Abut	0	0	0	0
FA Wing (L)	0	0	0	0
FA Wing (R)	0	0	0	0
Total (Sq.Ft.)			10005	

36" Drilled Shafts													
Location	Load/girder (Kips)	# Girders	Total Load	Subst Wt (kips)	Pile Cap.(Kips)	No. Piles	Increase Factor	Total Shafts	Top Elev.	Bot Elev.	Pile Length	Total Shaft Length (Feet)	
Rear Abut.	0	0	0	0	0	0	1	0	0	0	0.0	0	
Pier 1	0	0	0	0	0	0	1	0	0	0	0.0	0	
Pier 2	0	0	0	0	0	0	1	0	0	0	0.0	0	
Pier 3	0	0	0	0	0	0	1	0	0	0	0.0	0	
Pier 4	0	0	0	0	0	0	1	0	0	0	0.0	0	
Pier 5	0	0	0	0	0	0	1	0	0	0	0.0	0	
Pier 6	0	0	0	0	0	0	1	0	0	0	0.0	0	
Pier 7	0	0	0	0	0	0	1	0	0	0	0.0	0	
Fwd. Abut.	0	10	0	0	0	0	1	0	0	0	0.0	0	
Total								0				0	

Superstructure P/S Concrete Quantities					Spacing Int. diaphragm	No. of Int in span	Number of Int Diap. 1 location	Total No. in Span
Location	Type of girder	# Girders	Span Length	Total				
Span 1	MOD TYPE 4 72	8	108.0	864	27.00	6	3	18
Span 2		0	0.0	0	0.00			0
Span 3		0	0.0	0	0.00			0
Span 4		0	0.0	0	0.00			0
Span 5		0	0.0	0	0.00			0
Span 6		0	0.0	0	0.00			0
Span 7		0	0.0	0	0.00			0
Span 8		0	0.0	0	0.00			0
Span 9		0	0.0	0	0.00			0
Total	MOD TYPE 4 72	8		880	Total			18