

# *DeepEX 2022: Report Output*

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A program for the evaluation of deep excavations Deep Excavation LLC,  
New York, New York, [www.deepexcavation.com](http://www.deepexcavation.com)

Project: ODOT PID No. 108665; LAK-20-19.59 - WEST

Company: CT Consult  
Prepared by engineer:  
File number: CT PRO.  
Time: 7/6/2022 11:57:



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/isor  
its → engineers  
architects  
planners

## ANALYSIS AND CHECKING SUMMARY

The following tables summarize critical results for all design sections. These results may include wall moments, shears, displacements, stress checks, wall embedment safety factors, basal & slope stability safety factors, etc.

### Summary vs Design Section

Culvert at STA. 253	Wall Moment	Wall Shear	Wall Displace	Max Support	Critical Support	Embedment	Comments
0: AASHTO LRFD (201	(k-ft/ft)	(k/ft)	(in)	Reaction (k/ft)	Check	Wall FS	
Culvert at STA. 253	115.11	33.78	0	No supports	No supports	1.807	Calculation successful
0: AASHTO LRFD (201	115.11	33.78	0	No supports	No supports	1.807	Calculation successful
0: AASHTO LRFD (201	225.77	44.93	0	No supports	No supports	1.242	Calculation successful
0: AASHTO LRFD (201	225.77	44.93	0	No supports	No supports	1.242	Calculation successful
0: AASHTO LRFD (201	215.98	43.57	0	No supports	No supports	1.259	Calculation successful

### Extended Summary

Table: Extended summary for all design sections.

Design Section	Calculation Result	Wall Displacement	Settlement
Name		(in)	(in)
Culvert at STA. 253+86 Shoring (Se	Calculation successful	2.24	2.34
0: AASHTO LRFD (2010): Service I	Calculation successful	2.24	2.34
0: AASHTO LRFD (2010): Strength Ia	Calculation successful	5.64	2.39
0: AASHTO LRFD (2010): Strength Ib	Calculation successful	5.64	2.39
0: AASHTO LRFD (2010): Strength II	Calculation successful	5.29	2.36

Table: Extended summary for wall moments and shears for all design sections.

Design Section	Wall Moment	Wall Moment	Wall Shear	Wall Shear
Name	(k-ft/ft)	(k-ft)	(k/ft)	(k)
Culvert at STA. 253+86 Shoring (Serv	115.11	115.11	33.78	33.78
0: AASHTO LRFD (2010): Service I	115.11	115.11	33.78	33.78
0: AASHTO LRFD (2010): Strength Ia	225.77	225.77	44.93	44.93
0: AASHTO LRFD (2010): Strength Ib	225.77	225.77	44.93	44.93
0: AASHTO LRFD (2010): Strength II	215.98	215.98	43.57	43.57

Table: Extended summary for wall stress checks for all design sections.

Design Section	STR Combined	STR Moment	STR Shear	Wall Concrete Service
Name	Wall Ratio	Wall Ratio	Wall Ratio	Stress Ratio FIC
Culvert at STA. 253+86 Shoring (Serv	0.501	0.501	0.207	N/A
0: AASHTO LRFD (2010): Service I	0.501	0.501	0.207	N/A
0: AASHTO LRFD (2010): Strength Ia	0.982	0.982	0.275	N/A
0: AASHTO LRFD (2010): Strength Ib	0.982	0.982	0.275	N/A
0: AASHTO LRFD (2010): Strength II	0.94	0.94	0.267	N/A

Table notes:

STR Combined: Combined stress check, along eccentricity line considering axial load and moment (demand/capacity).

STR Moment : Moment stress check, assuming constant axial load on wall (demand/capacity).

STR Shear : Shear stress check (shear force demand/wall shear capacity).

Table: Extended summary for support results for all design sections

Design Section	Max Support	Max Support	Critical	STR Support	Support Geotech
Name	Reaction (k/ft)	Reaction (k)	Support Check	Ratio	Capacity Ratio (pull
Culvert at STA. 253+86 Shoring (Se	No supports	No supports	No supports	No supports	No supports
0: AASHTO LRFD (2010): Service I	No supports	No supports	No supports	No supports	No supports
0: AASHTO LRFD (2010): Strength Ia	No supports	No supports	No supports	No supports	No supports
0: AASHTO LRFD (2010): Strength Ib	No supports	No supports	No supports	No supports	No supports
0: AASHTO LRFD (2010): Strength II	No supports	No supports	No supports	No supports	No supports

Table notes:

STR Support ratio: Critical structural stress check for support (force demand/structural capacity).

Support geotech capacity ratio: Critical geotechnical capacity stress check (demand/geotechnical capacity).  
 Critical support check: Critical demand/design capacity ratio (structural or geotechnical).

Table: Summary for basal stability and wall embedment safety factors from conventional analyses.

Design Section	FS	Toe FS	Toe FS	Toe FS
Name	Basal	Passive	Rotation	Length
Culvert at STA. 253+86 Shoring (Serv	1000	21.622	2.535	1.807
0: AASHTO LRFD (2010): Service I	1000	21.622	2.535	1.807
0: AASHTO LRFD (2010): Strength Ia	1000	10.838	1.362	1.242
0: AASHTO LRFD (2010): Strength Ib	1000	10.838	1.362	1.242
0: AASHTO LRFD (2010): Strength II	1000	10.838	1.387	1.259

Table notes:

FSbasal : Critical basal stability safety factor (relevant only when soft clays are present beneath the excavation).  
 TOE FS Passive : Safety factor for wall embedment based on FS= Available horizontal thrust resistance/Driving hor. thrust.  
 TOE FS Rotation: Safety factor for wall embedment based on FS= Available resisting moment/Driving moment.  
 TOE FS Length : Safety factor for wall embedment based on FS= Available wall embedment/Required embedment for FS=1.0

Table: Summary for wall embedment safety factors from elastoplastic analyses.

Design Section	FS Mobilized	FS
Name	Passive	True/Active
Culvert at STA. 253+86 Shoring (Servi	N/A	N/A
0: AASHTO LRFD (2010): Service I	N/A	N/A
0: AASHTO LRFD (2010): Strength Ia	N/A	N/A
0: AASHTO LRFD (2010): Strength Ib	N/A	N/A
0: AASHTO LRFD (2010): Strength II	N/A	N/A

Table notes:

FS Mobilized Passive : Safety factor= Available horizontal passive resistance/Mobilized passive thrust.  
 FS True/Active : Soil thrust on retained wall side/Minimum theoretically horizontal active force thrust.

Table: Summary for hydraulic safety factors, water flow, and slope stability

Design Section	Hydraulic	Qflow	FSslope
Name	Heave FS	(ft <sup>3</sup> /hr)	
Culvert at STA. 253+86 Shoring (Servi	1.821	N/A	3.282
0: AASHTO LRFD (2010): Service I	1.821	N/A	3.282
0: AASHTO LRFD (2010): Strength Ia	1.821	N/A	3.243
0: AASHTO LRFD (2010): Strength Ib	1.821	N/A	3.243
0: AASHTO LRFD (2010): Strength II	1.821	N/A	3.266

### Critical Items

	Critical Value	Critical Design Sectio	Critical Stage	Critical Wall	Critical Item Index
Wall Moment Check	0.982	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	92
Wall Moment (k-ft/ft)	225.773	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	0
Wall Moment (k-ft)	225.773	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	0
Wall Moment Capacity (k-ft/ft)	229.875	4: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	91
Wall Shear (k/ft)	44.926	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	123
Wall Shear (k)	44.926	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	123
Wall Shear Check	0.275	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	123
Wall Shear Capacity (k/ft)	163.267	4: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	122
Wall Displacements (in)	5.639	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	N/A
Surface Settlements (in)	2.386	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	0
Toe FS Passive (Classic)	10.838	4: 0: AASHTO LRFD (	0: Stage 0	1: Wall 1	0
Toe FS Rotation (Classic)	1.362	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	1
Toe FS Length (Classic)	1.242	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	1
FS 1.0 Req. Embed (Classic) (ft)	25.37	3: 0: AASHTO LRFD (	1: Stage 1	1: Wall 1	1
Basal FS (Classic)	1000	4: 0: AASHTO LRFD (	0: Stage 0	1: Wall 1	0

### Support Results

	Critical Value	Critical Design Sectio	Critical Stage	Critical Wall	Critical Item Index
Results not available	Results not available	Results not available	Results not available	Results not available	Results not available

### Wall Results

	Critical Value	Critical Design Sectio	Critical Stage	Critical Wall	Critical Item Index
Wall Moment ABS (k-ft)	225.773	3: 0: AASHTO LRFD (2)	1: Stage 1	1: Wall 1	0
Wall Moment +M (k-ft)	0	4: 0: AASHTO LRFD (2)	0: Stage 0	1: Wall 1	0
Wall Moment -M (k-ft)	-225.773	3: 0: AASHTO LRFD (2)	1: Stage 1	1: Wall 1	0
Wall Moment Check	0.982	3: 0: AASHTO LRFD (2)	1: Stage 1	1: Wall 1	92
Wall Moment Capacity (k-ft/ft)	229.875	4: 0: AASHTO LRFD (2)	1: Stage 1	1: Wall 1	91
Wall Shear (k)	44.926	3: 0: AASHTO LRFD (2)	1: Stage 1	1: Wall 1	123
Wall Shear Check	0.275	3: 0: AASHTO LRFD (2)	1: Stage 1	1: Wall 1	123
Wall Shear Capacity (k/ft)	163.267	4: 0: AASHTO LRFD (2)	1: Stage 1	1: Wall 1	122

### Max. Moment vs Stage

	Base Model	DS: 1	DS: 2	DS: 3	DS: 4
M stg0 (k-ft/ft)	DS: 0	DS: 1	DS: 2	DS: 3	DS: 4
M stg1 (k-ft/ft)	-115.11	-115.11	-225.77	-225.77	-215.98

### Max. Shear vs Stage

	Base Model	DS: 1	DS: 2	DS: 3	DS: 4
V stg0 (k/ft)	DS: 0	DS: 1	DS: 2	DS: 3	DS: 4
V stg1 (k/ft)	-33.78	-33.78	-44.93	-44.93	-43.57

### Max. Support F vs Stage

	Base Model	DS: 1	DS: 2	DS: 3	DS: 4
Rmax Stage 0 (k/ft)	DS: 0	DS: 1	DS: 2	DS: 3	DS: 4
Rmax Stage 1 (k/ft)					

## STRUCTURAL MATERIALS DATA

### Steel

Name	Strength Fy (ksi)	Fu (ksi)	Elastic E (ksi)	Density g (kcf)
Fe360	34.1	52.2	29855.1	0.49
Fe510	51.5	73.9	29855.1	0.49
A36	36	58	29000	0.49
A50	50	72.5	29000	0.49
New steel 4	35	60	29855.1	0.49

### Concrete

Name	Strength Fc' (ksi)	Elastic E (ksi)	Density g (kcf)	Tension Strength Ft (% of Fc')
C20/25	2.9	4342.3	0.1591	10
C25/30	3.6	4561.7	0.1591	10
Fc 3ksi	3	3122	0.15	10

### Steel rebar

Name	Strength Fy (ksi)	Elastic E (ksi)

Grade 60	60	29000
Grade 75	75	29000
Grade 80	80	29000
Grade 150	150	29000
Strands 270 ksi	270	29000
S410	59.4	30434.8
S500	72.5	30434.8
B450C	65.2	30434.8

### Wood

Name	Ultimate Bending Strength Fbu	Ultimate Tensile Strength FtU	Ultimate Shear Strength Fvu	Density g	Elastic E
	(ksi)	(ksi)	(ksi)	(pcf)	(ksi)
Construction Timb	1.6	1.4	0.8	0.05	1000
Regular grade	1	1	0.6	0.05	800

### STEEL

Name=material name

$f_y=f_{yk}$ = characteristic resistance for steel (for all the codes)

$F_u=f_{uk}$ = ultimate resistance for steel (for all the codes)

Elastic E= Elastic modulus

Density g= specific weight

### CONCRETE

Name=material name

$f'_c=f_{ck}$ = cylindrical resistance for concrete (for all the codes)

Elastic E= Elastic modulus

Density g= specific weight

Tension strength= $f_t=f_{ctk}$ = characteristic tension resistance for concrete

### STEEL REBARS

Name=material name

$f_y=f_{yk}$ = characteristic resistance for steel (for all the codes)

$F_u=f_{uk}$ = ultimate resistance for steel (for all the codes)

Elastic E= Elastic modulus

Density g= specific weight

### WOOD

Name=material name

$F_b=f_{bk}$ = Ultimate bending strength

$F_{tu}=f_{tuk}$ = Ultimate tensile strength

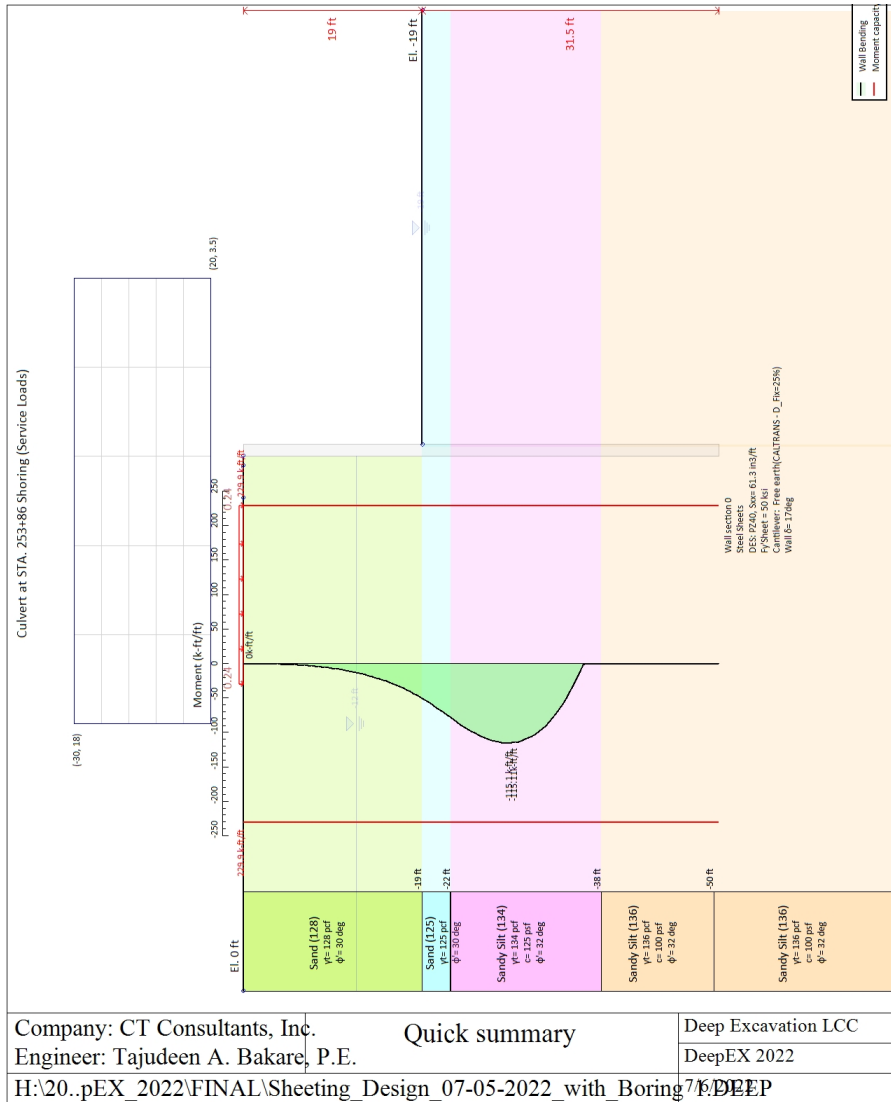
$F_{vu}=f_{vuk}$ = Ultimate shear strength

Density g= specific weight

Elastic E= Elastic modulus

***Project: ODOT PID No. 108665; LAK-20-19.59 - WEST  
Results for Design Section 0: Culvert at STA. 253+86  
Shoring (Service Loads)***

## ANALYSIS AND CHECKING SUMMARY



Company: CT Consultants, Inc.	Quick summary	Deep Excavation LCC
Engineer: Tajudeen A. Bakare, P.E.		DeepEX 2022
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### Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	115.11/229.88	21.622	2.535	1.807	-36.43	3.282

### Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.849	12.4	3.282	0.373	12.449	3.282

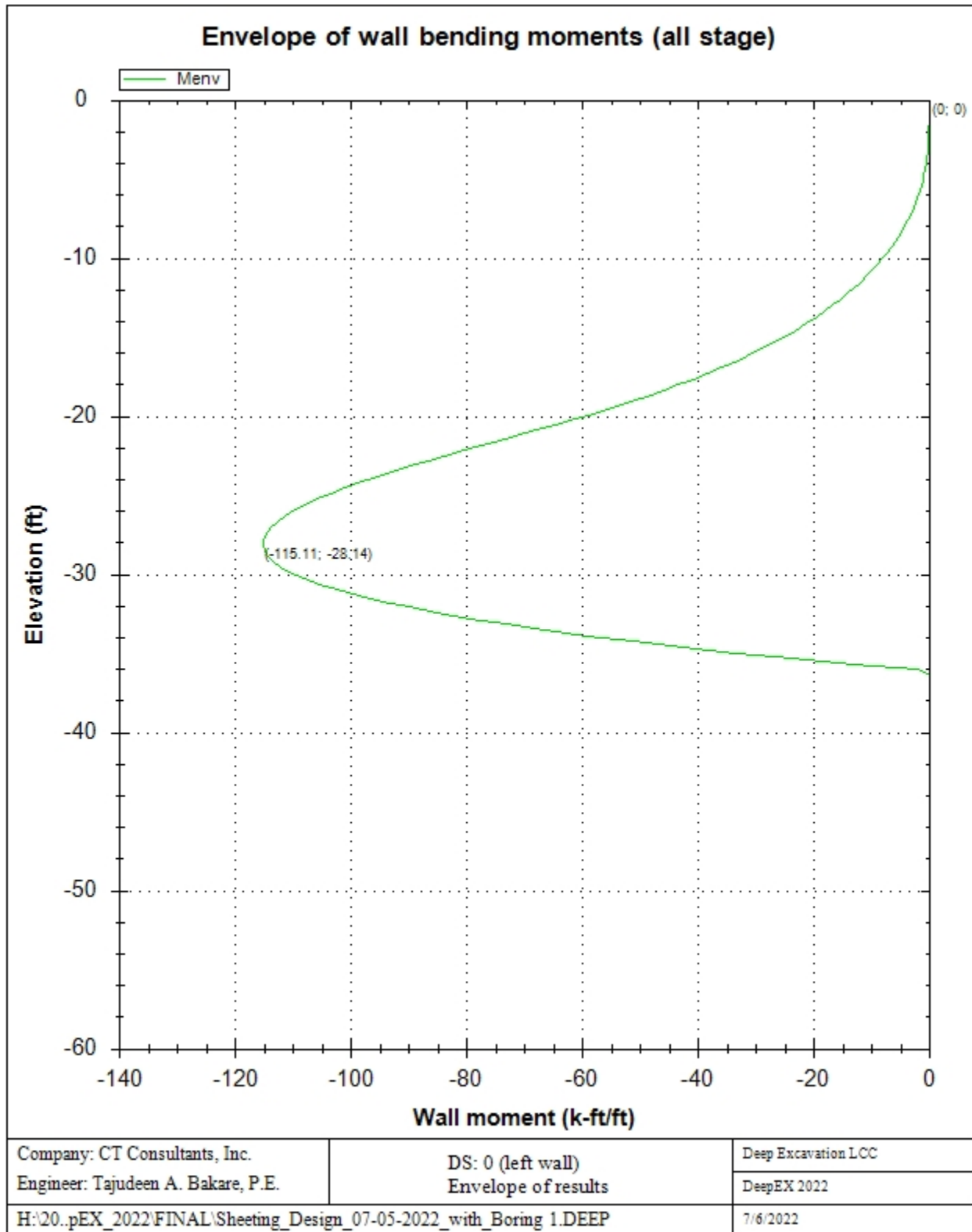
General assumptions for last stage: Stage 1

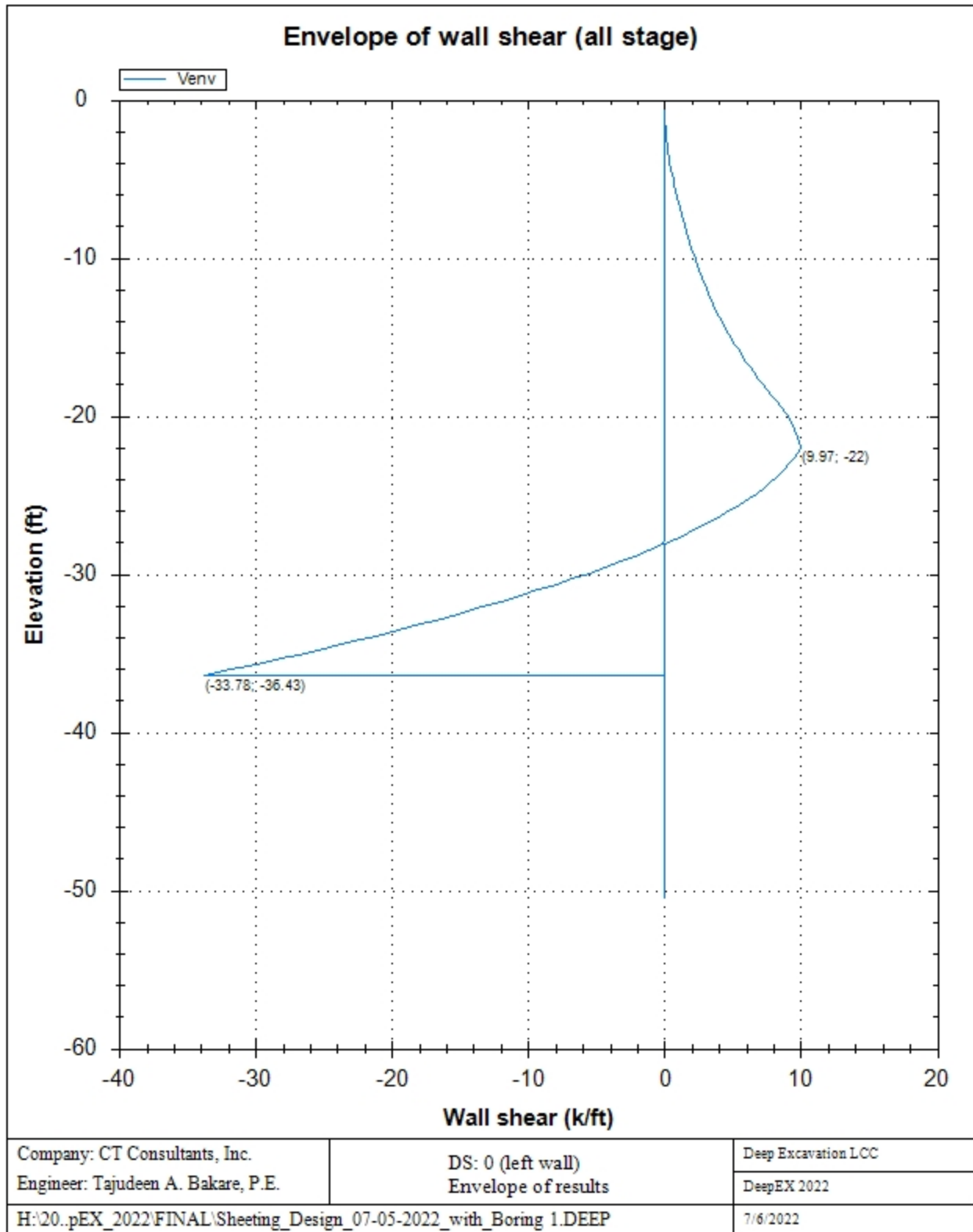


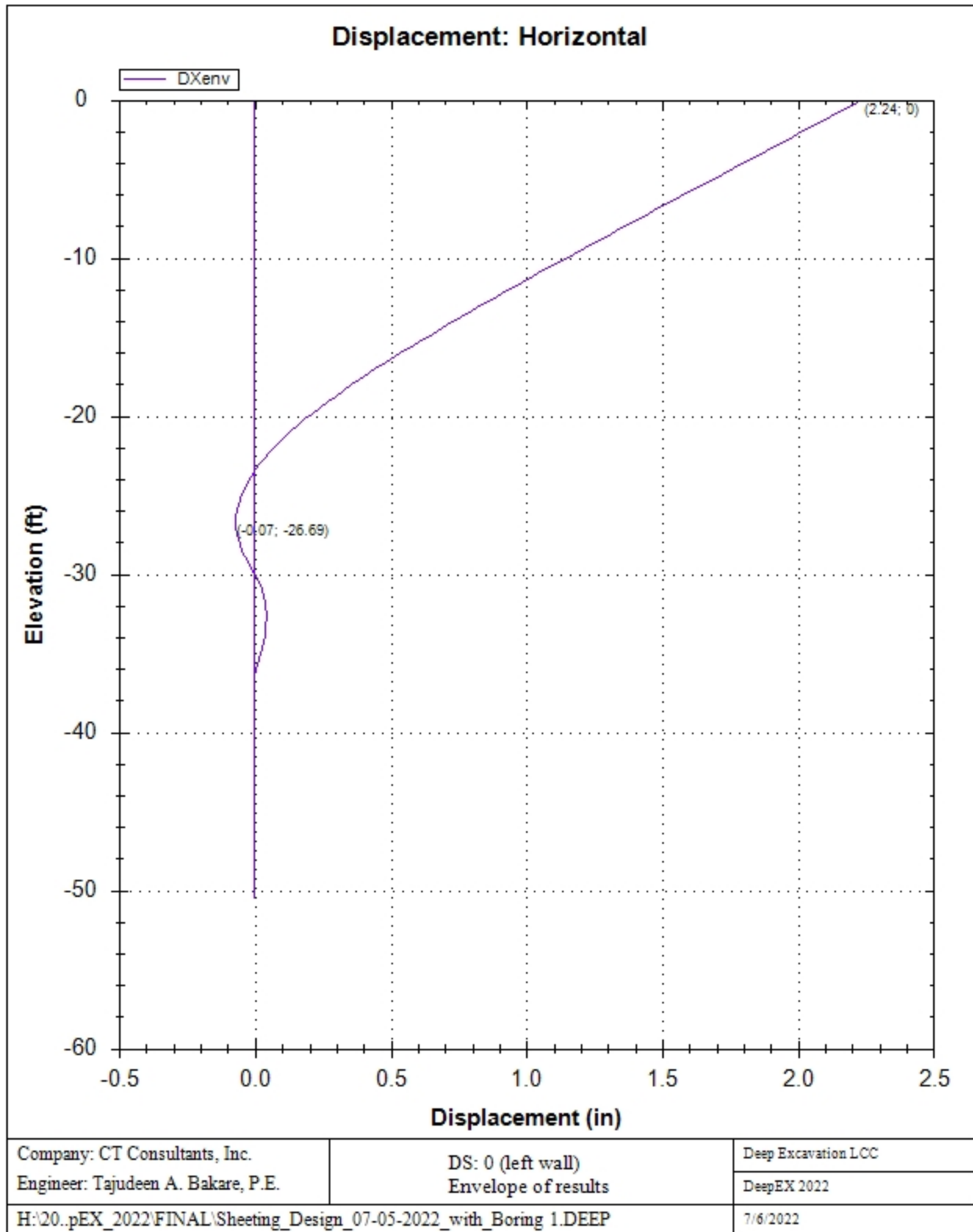
Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Caquot

### Envelope of results

A sequence of result diagrams for each excavation stage is reported







Extended vs Stage

	Calculation Result	Wall Displaceme (in)	Settlement (in)	Wall Moment (k-ft/ft)	Wall Moment (k-ft)
Stage 0	Calculated	0	N/A	0	0
Stage 1	Calculated	2.24	2.34	115.11	115.11

	Wall Shear (k/ft)	Wall Shear (k)	STR Combined Wall Ratio	STR Moment Wall Ratio	STR Shear Wall Ratio
Stage 0	0	0	0	0	0
Stage 1	33.78	33.78	0.501	0.501	0.207

Table notes:

STR Combined: Combined stress check, along eccentricity line considering axial load and moment (demand/capacity).

STR Moment : Moment stress check, assuming constant axial load on wall (demand/capacity).

STR Shear : Shear stress check (shear force demand/wall shear capacity).

	Max Support Reaction (k/ft)	Max Support Reaction (k)	Critical Support Check	STR Support Ratio	Support Geotech Capacity Ratio (pull out)
Stage 0	0	0	N/A	No supports	No supports
Stage 1	0	0	N/A	No supports	No supports

Table notes:

STR Support ratio: Critical structural stress check for support (force demand/structural capacity).

Support geotech capacity ratio: Critical geotechnical capacity stress check (demand/geotechnical capacity).

Critical support check: Critical demand/design capacity ratio (structural or geotechnical).

	FS Basal	Toe FS Passive	Toe FS Rotation	Toe FS Length	Zcut (nonlinear)	FS Mobilized Passive	FS True/Active
Stage 0	1000	21.622	20.213	140.278	N/A	N/A	N/A
Stage 1	N/A	N/A	2.535	1.807	N/A	N/A	N/A

	Hydraulic Heave FS	Qflow (ft3/hr)	FSslope
Stage 0	2.729	N/A	N/C
Stage 1	1.821	N/A	3.282

### Support Force/S vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

### Support Force vs Stage

### Support Force vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	20.213	21.622	20.213	140.278	N/A	N/A
0:Stage 0	1.807	N/A	2.535	1.807	N/A	N/A

Table notes:

FSbasal : Critical basal stability safety factor (relevant only when soft clays are present beneath the excavation).

Wall embedment safety factors from conventional analysis (limit-equilibrium):

FS1 Passive : Safety factor for wall embedment based on FS= Available horizontal thrust resistance/Driving hor. thrust.

FS2 Rotation: Safety factor for wall embedment based on FS= Available resisting moment/Driving moment.

FS3 Length : Safety factor for wall embedment based on FS= Available wall embedment/Required embedment for FS=1.0

Wall embedment safety factors from non-linear analysis:

FS4 Mobilized Passive : Safety factor= Available horizontal passive resistance/Mobilized passive thrust.

FS5 True/Active : Soil thrust on retained wall side/Minimum theoretically horizontal active force thrust.

Tables for stress checks follow: Support force/Design capacity

Support Check vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

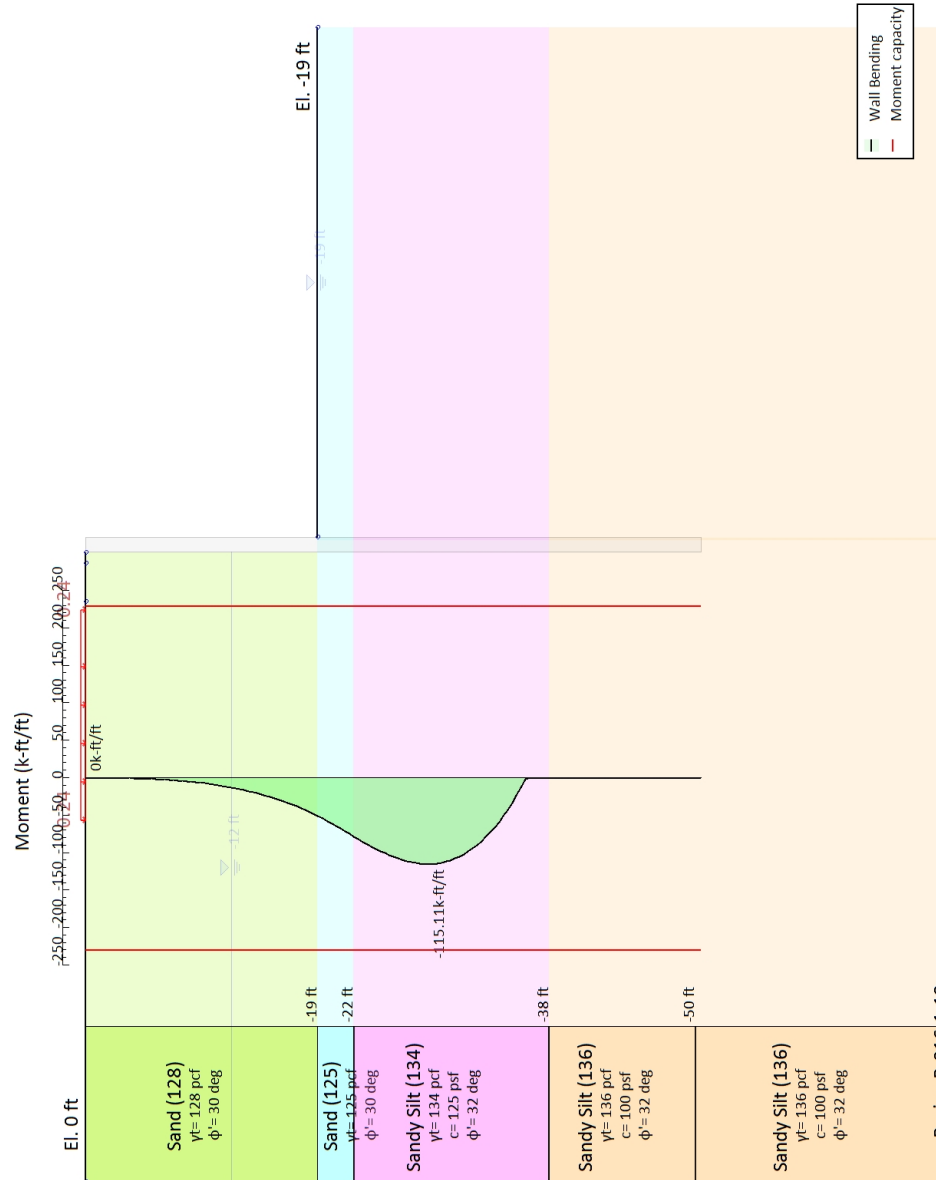
Forces (Res. F, M/Drive F, M)

	FS1 Passive (FxResist/FxDrive)	FS2 Rotation (Mresist/Mdrive)	FS3 Length (Embedment/ToeFS=1)	FS4 Mobilized Passive (FxPassive/FxPas_Mobili)	FS5 Actual Drive / Theory Active	Fh EQ Soil	Fh EQ Water
Stage 0	594.114/27.477	10534.52/521.19	50.5/0.36	N/A	N/A	N/A	N/A
Stage 1	N/A	1930.96/453.04	31.5/17.43	N/A	N/A	N/A	N/A

Reinforcement Requirements

	Parameter Description
Note:	Wall does not use steel reinforcement. Section does not apply.

Culvert at STA. 253+86 Shoring (Service Loads)



Company: CT Consultants, Inc.

Engineer: Tajudeen A. Bakare, P.E.

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Quick summary

Deep Excavation LCC

DeepEX 2022

7/6/2022

### Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	115.11/229.88	21.622	2.535	1.807	-36.43	3.282

### Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.849	12.4	3.282	0.373	12.449	3.282

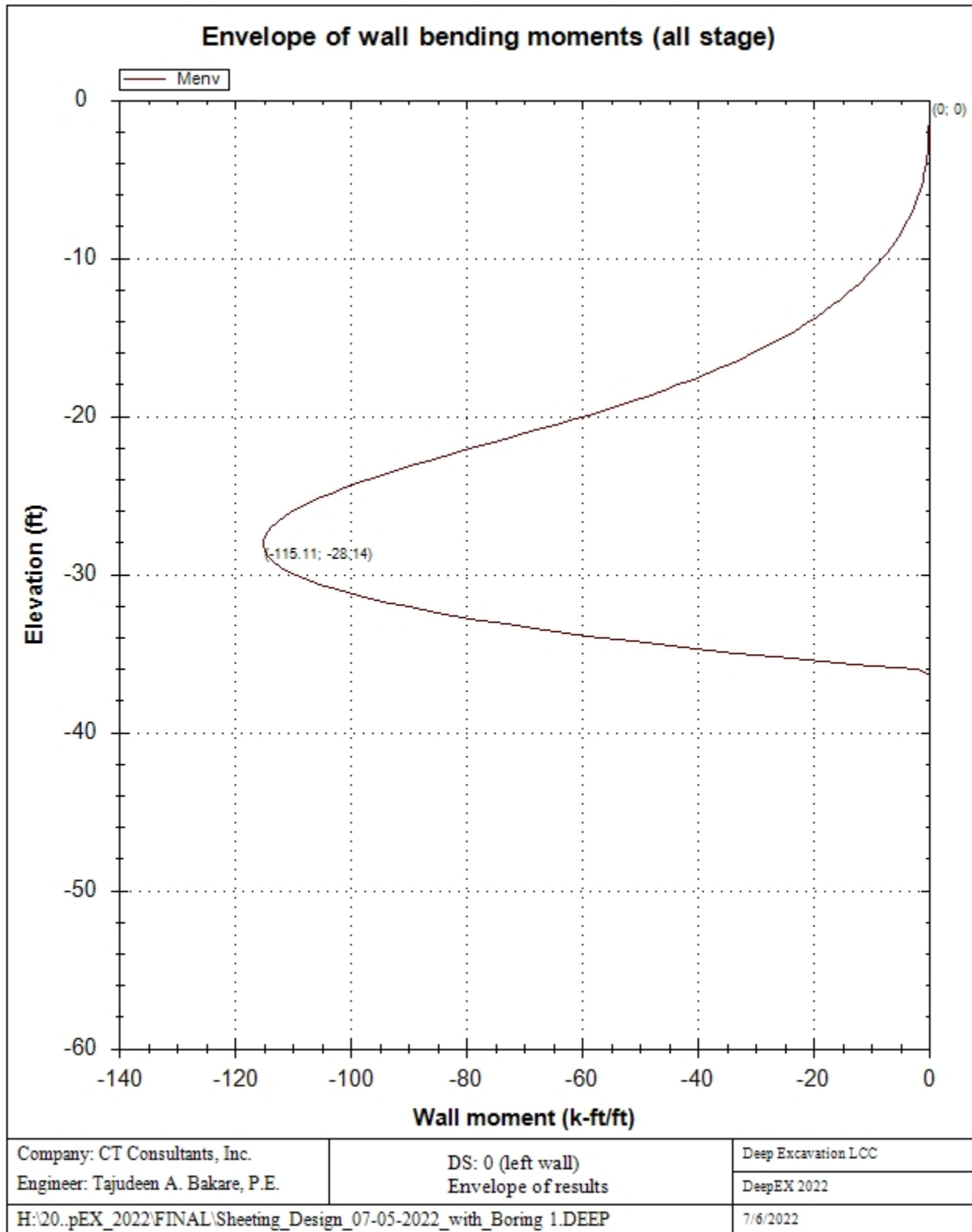
### General assumptions for last stage: Stage 1

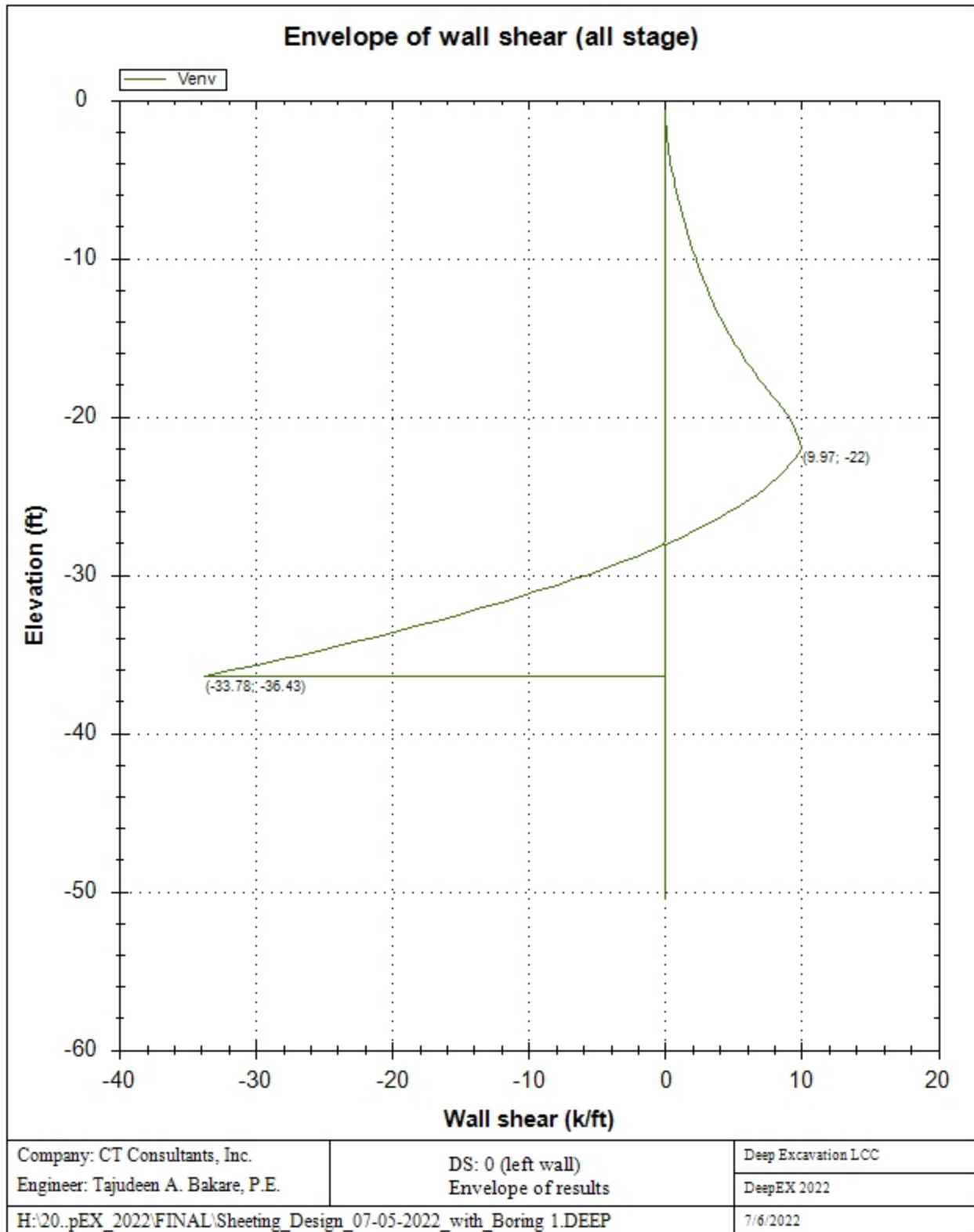
Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Coul

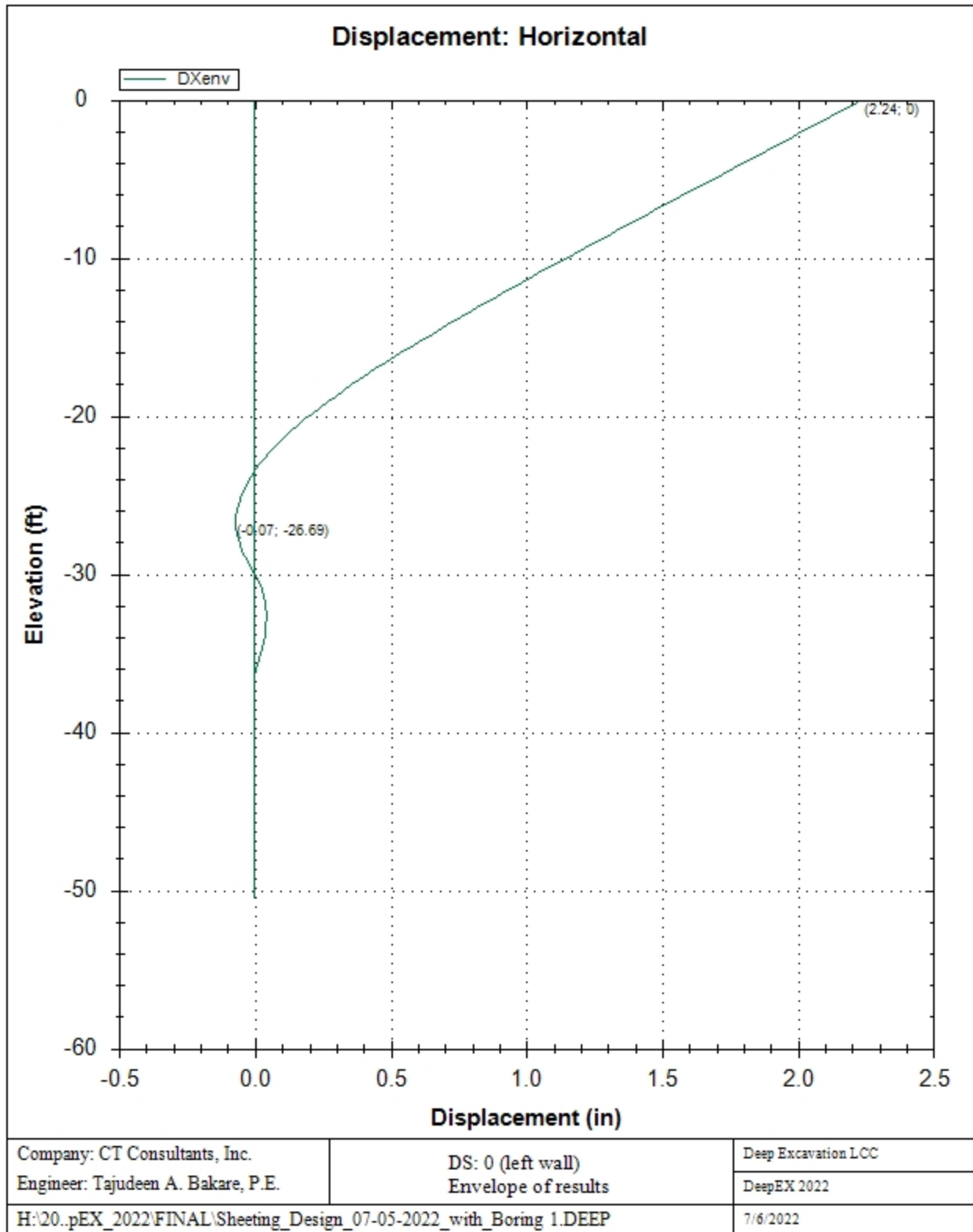


### Envelope of results

A sequence of result diagrams for each excavation stage is reported







**DESIGN APPROACHES AND COMBINATION FACTORS**

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

Ftan fr=mult factor for friction angle

F C'= safety factor on effective cohesion (Eurocode 7 methods)

F Su'= safety factof for undrained shear strength (Eurocode 7 methods)

F EQ= Load factor for seismic loads

F perm load= Load factor for permanent loads (dead load, etc)

F temp load= Load factor on live loads and other temporary loads

F perm supp= Reduction factor for resistance for pull out checking of permanent tiebacks

F temp supp= Reduction factor for resistance for pull out checking of temporary tiebacks

F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)

F earth stab= Safety factor for passive pressures, favorable (on excavation side)

F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable

F GWT stab (ground water)= Load factor for resisting water pressure, favorable

F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)

F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)

F UPL Dstab= Load factor for uplift check, unfavorable

F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan fr)	F (c')	F (Su)	F (EQ)	F(perm load)	F(temp load)	F(perm sup)	F(temp sup)	F Earth (Dstab)	F Earth (stab)	F GWT (Dstab)	F GWT (stab)	F HYD (Dstab)	F HYD (stab)	F UPL (Dstab)	F UPL (stab)
0	Default	Service Factors	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	Default	Service Factors	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1

## DESIGN APPROACHES AND COMBINATION FACTORS

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

Ftan fr=mult factor for friction angle

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F EQ= Load factor for seismic loads

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F temp load= Load factor on live loads and other temporary loads

F perm supp= Reduction factor for resistance for pull out checking of permanent tiebacks

F temp supp= Reduction factor for resistance for pull out checking of temporary tiebacks

F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)

F earth stab= Safety factor for passive pressures, favorable (on excavation side)

F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable

F GWT stab (ground water)= Load factor for resisting water pressure, favorable

F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)

F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)

F UPL Dstab= Load factor for uplift check, unfavorable

F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan fr)	F (c')	F (Su)	F (EQ)	F(perm load)	F(temp load)	F(perm sup)	F(temp sup)	F Earth (Dstab)	F Earth (stab)	F GWT (Dstab)	F GWT (stab)	F HYD (Dstab)	F HYD (stab)	F UPL (Dstab)	F UPL (stab)
0	Default	Service Factors	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
1	Default	Service Factors	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1

## SOIL DATA

Name	g tot (pcf)	g dry (pcf)	Frict (deg)	C' (psf)	Su (psf)	FRp (deg)	FRcv (deg)	Eload (ksf)	rEur (-)	kAp NL	kPp NL	kAcv NL	kPcv NL	Vary	Spring Model	Color
Sand (128)	128	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sand (125)	125	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sandy Silt (13)	134	134	32	125	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	
Sandy Silt (13)	136	136	32	100	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	

Name	Poisson	Min Ka	Min sh	ko.NC	nOCR	aH.EXP	aV.EXP	qSkin	qNails	kS.nails	PL
	v	(clays)	(clays)	-	-	(0 to 1)	(0 to 1)	(psi)	(psi)	(k/ft3)	(ksi)
Sand (128)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sand (125)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-

gtot = total soil specific weight

gdry = dry weight of the soil

Frict = friction angle

C' = effective cohesion

Su = Undrained shear strength (only for CLAY soils in undrained conditions, used as a cutoff strength in NL analysis)

Evc = Virgin compression elastic modulus

Eur = unloading/reloading elastic modulus

Kap = Peak active thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kpp = Peak passive thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kacv = Constant volume active thrust coeff (only for clays, initial value)

Kpcv = Constant volume passive thrust coeff (only for clays, initial value).

Spring models= spring model (LIN= constant E over the soil layer height , EXP=exponential , SIMC=simplified winkler)

LIN= Linear-Elastic-Perfectly Plastic,

EXP: Exponential, SUB: Modulus of Subgrade Reaction

SIMC= Simplified Clay mode

## **SOIL BORINGS**

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Top Elev= superior SOil level

Soil type= type of the soil (sand , clay , etc)

OCR= overconsolidation ratio

K0= at rest coefficient

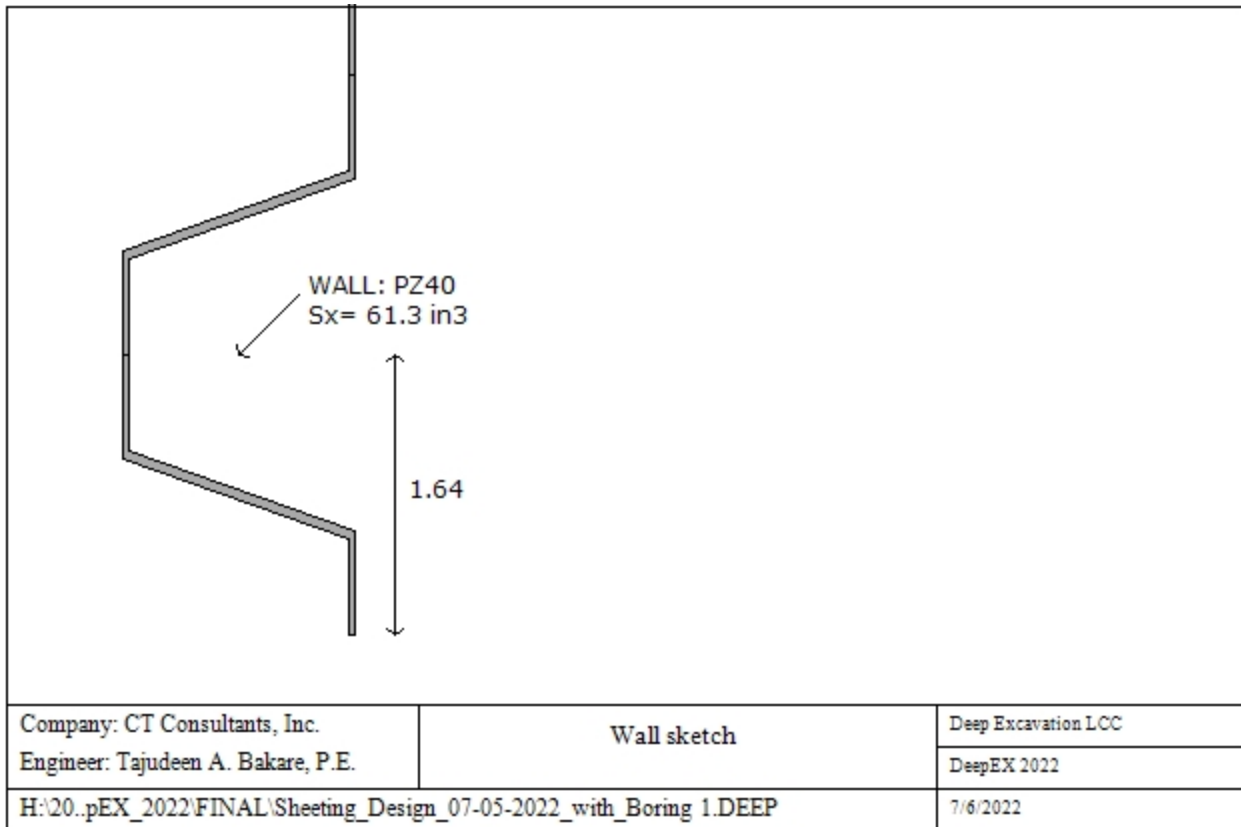
Name: Boring B-016-1-19, pos: (0, 0)

Top elev.	Soil type	OCR	Ko
0	Sand (128)	1	0.5
-19	Sand (125)	1	0.5
-22	Sandy Silt (134)	1	0.47
-38	Sandy Silt (136)	1	0.47
-50	Sandy Silt (136)	1	0.47

## **WALL DATA**

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Wall section 0: Wall section 0



Wall type: Steel sheet piling  
 Top wall El: 0 ft Bottom wall El: -50.5 ft  
 Hor. wall spacing: 1 ft Wall thickness = 1.37 ft  
 Passive width below exc: 1 ft Active width below exc: 1 ft Swater= 1 ft  
 Steel members fy = 50 ksi Esteel = 29000 ksi  
 Wall friction: Constant value = 17 degrees  
 Steel wall capacities are calculated with ANSI/AISC 360-10  
 Concrete capacities are calculated with ACI 318-19  
 Note: With ultimate capacities you may have to use a structural safety factor.  
 Steel sheet pile properties

Table: Steel Sheet Pile Cross Sectional Properties

DES	Shape	W	A	h	t	b	s	Ixx	Sxx
		(plf)	(in <sup>2</sup> /ft)	(in)	(in)	(in)	(in)	(in <sup>4</sup> /ft)	(in <sup>3</sup> /ft)
PZ40	Z	65.6	11.75	16.4	0.5	19.69	0.605	503	61.3

GENERAL WALL DATA

Hor wall spacing= Wall horizontal spacing  
 Passive width below exc= spacing for passive thrust pressure for classic analysis  
 f'c=fck= cylindrical concrete resistance  
 fyk=fyk= steel rebar characteristic resistance  
 Econc= Concrete Elastic modulus  
 fctk= characteristic Concrete tension  
 Esteel= steel elastic modulus  
 TABULAR DATA (principal parameters)  
 1) Diaphragm wall (rectangular cross section)  
 N/A= data not available  
 Fy=fyk

$F'c=f_{ck}$

$D$ =wall thickness

$B$ =wall width

2)Steel sheet pile

$DES$ =shape (Z or U)

$W$ =width per unit of length

$A$ =area

$h$ =height

$t$ =horizontal part thickness

$b$ =width of the single sheet pile part

$s$ =inclined part thickness

$I_{xx}$ =strong axis inertia (per unit of length)

$S_{xx}$ =strong axis section modulus (per unit of length)

3)Secant piles wall, Tangent piles wall, soldier piles, soldier piles and timber lagging

$W$ =weight per unit of length

$A$ =area

$D$ =diameter

$t_w$ =web thickness

$t_p$ = pipe thickness

$b_f$ =flange width

$t_f$ = flange thickness

$k$ = flange thickness+stem base height

$I_{xx}$ = strong axis inertia modulus (per unit of length)

$S_{xx}$ = strong axis section modulus (per unit of length)

$r_x$ =radius of gyration about X axis

$r_y$ =radius of gyration about Y axis

$I_{yy}$ =weak axis inertia modulus (per unit of length)

$S_{yy}$ =weak axis section modulus (per unit of length)

$r_T$ =radius of gyration for torsion

$C_w$ = warping constant

## **GENERAL ANALYSIS CRITERIA**

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### Summary of stage assumptions

Name	Analysis	Drive	ka-Mult	Htr T/B	Resist	Res	Contle
	Method	Press		(%)	Press	Mult	Method
Stage 0	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth
Stage 1	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth

Name	Support	Axial	Used	Min Toe	Toe	Toe
	Model	Incl	FSwall	FDtoe	FSrot	FSpas
Stage 0		N/A	1	20.213	20.213	21.622
Stage 1		N/A	1	1.807	2.535	N/A

Name=excavation stage name

Analysis method

springs = Elastoplastic spring analysis used

DR = Drained condition for CLAY model

U = Undrained condition for CLAY model for all the soils

Up = Undrained condition just for selected soil

Limit equilibrium analysis settings

Drive press:

Ka (Active pressure diagram), Ka-Trap = Trapezoid apparent diagram from active pressures x multiplier, FHWA= Federal Highway Administration apparent pressure diagrams.

Ko = At-rest lateral earth pressures.

Peck = Peck 1969 Apparent earth pressure diagrams.

2 Step rect = Two step rectangular apparent earth pressure diagram.

User def. = User defined apparent earth pressure diagram.

Ka+d (and so on) indicates that wall friction is applied

ka mult = multiplication factor for Ka when Ka-Trap is selected

Htr T/B (%) = trapezoidal pressure scheme, top and bottom triangular percentage of excavation depth H

Resit press = Kp (passive earth pressures)

Res Mult = Safety factor applied directly on resisting pressures (

COntle Method = cantilever analysis method for limit equilibrium analysis.

Support Model: Method for calculating support reactions in limit-equilibrium analysis.

Beam= support reactions beam analysis (uses Blum's method).

Trib= support reactions from tributary height calculations (Can be applied with apparent diagrams).

Axial Incl = Axial loads included for structural design

Used FS wall = Safety factor for axial+bending wall resistance to divide ultimate wall capacities.

Min FD Toe= embedded minimum safety factor (for limit equilibrium analysis)

Toe FS rot= rotation safety factor (classic for limit equilibrium analysis)

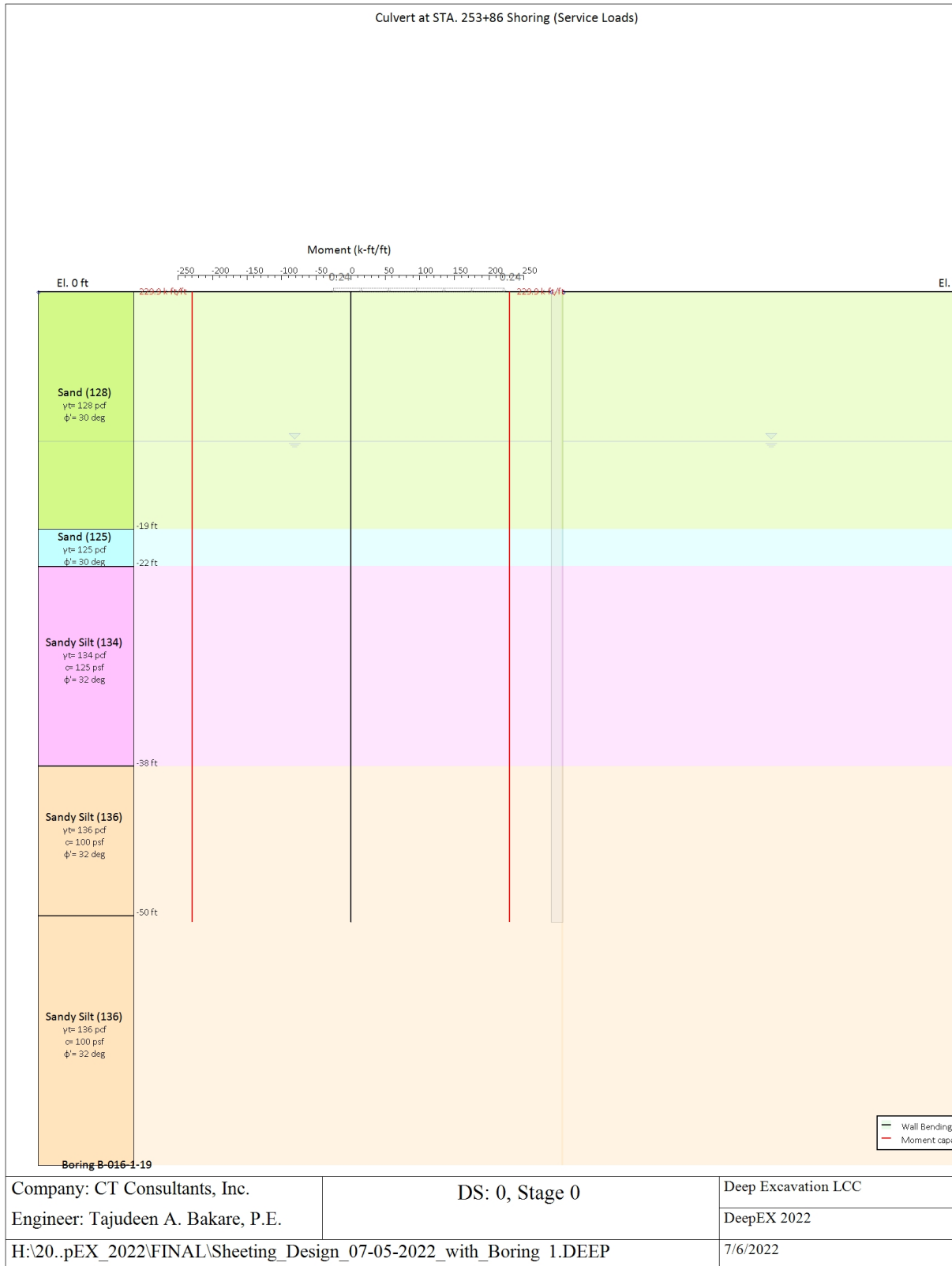
Toe FSpas= driving/resisting pressure safety factor (for limit equilibrium analysis)

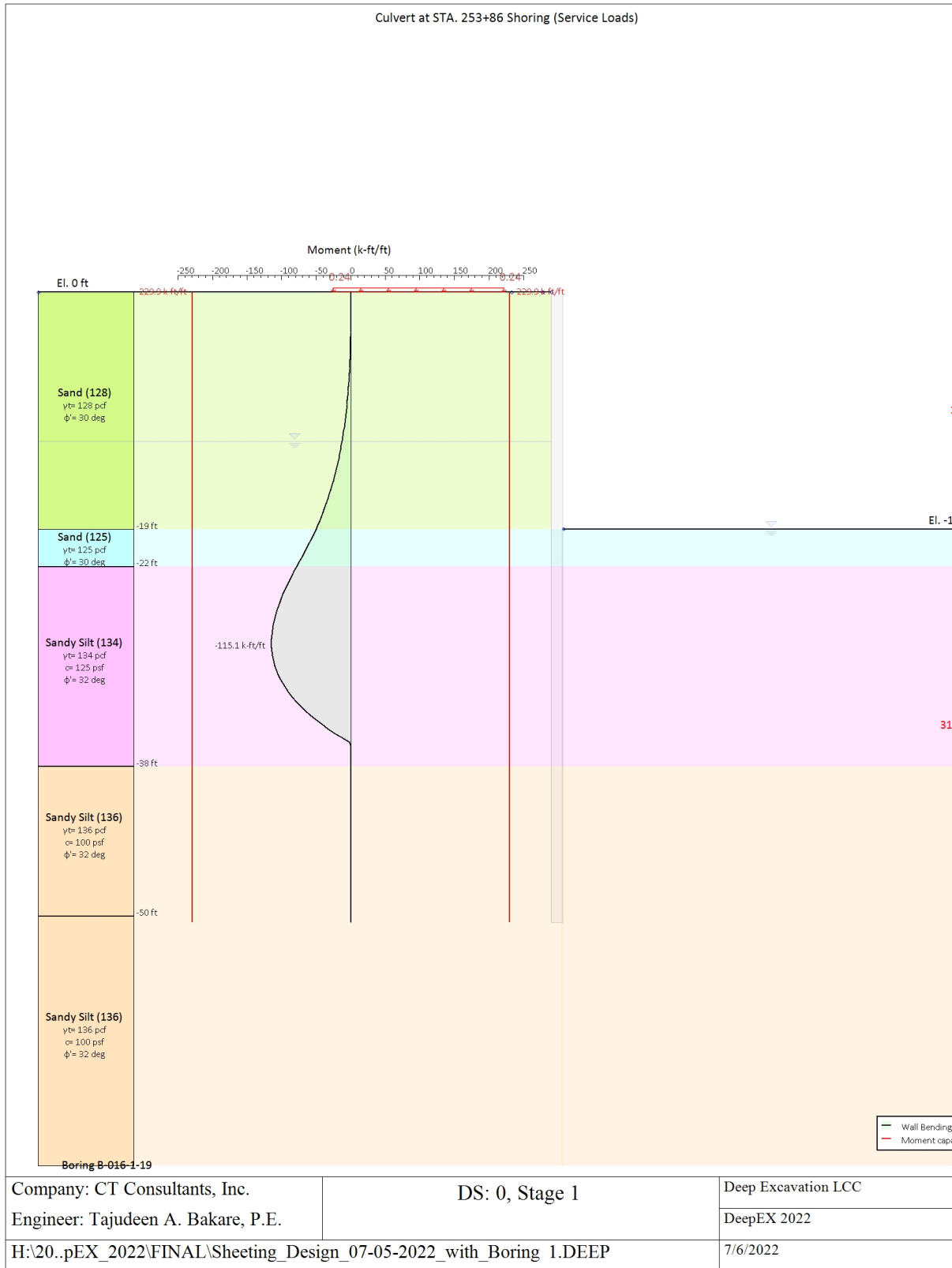
## **EXCAVATION STAGES SKETCHES**

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A sequence of figures for each excavation stage is reported







**Toe stability**

### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	20.213	21.622	20.213	140.278	N/A	N/A
Stage 1	1.807	N/A	2.535	1.807	N/A	N/A

Legend: Wall embedment safety factors (toe)

Min Toe FS= Minimum wall embedment safety factor (from all analysis methods)

Limit-equilibrium analysis methods: The following safety factors may not be applicable for all stages.

FS1 Passive: Horizontal force safety factor, FS1= Resisting/Driving force

FS2 Rotation: Rotational safety factor about lowest support, FS2= Resisting moment/Driving moment

FS3 Length (from FS1, FS2): Program determines maximum required wall embedment for safety factor of 1 for methods FS1 and FS2 (say length LFS1). Then FS length= Provided wall embedment/LFS1.

Non-linear elastoplastic analysis safety factors:

FS4 Mobilized Passive: Safety factor on mobilized passive resistance, FS4= Available passive soil resistance/Mobilized passive soil force on excavation side.

FS5 Active Drive Thrust/Theory Active: Ratio of soil thrust on retained side/ Active condition theoretical minimum thrust. This factor is not as critical, and indicates how close to active conditions the model is.

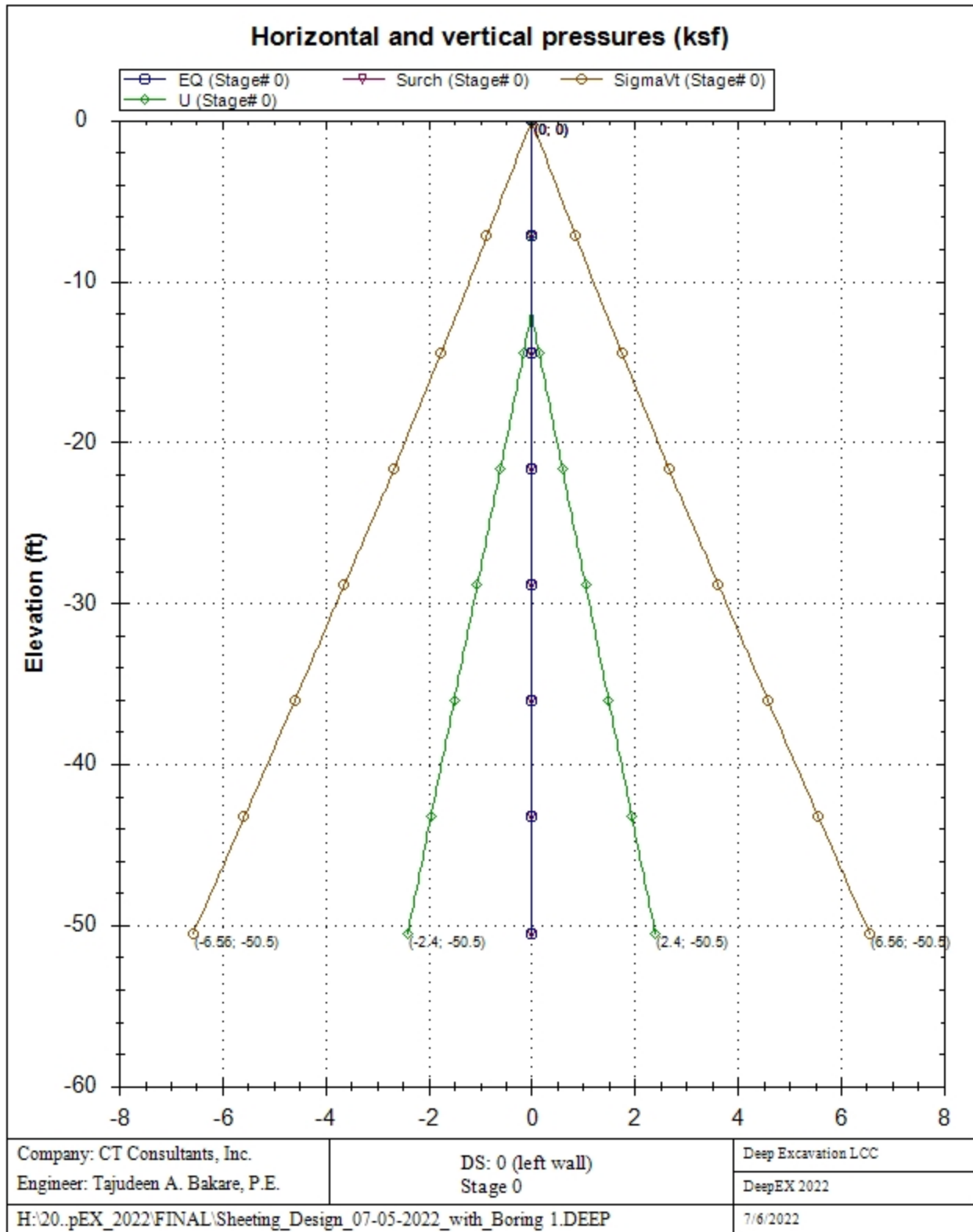
General recommendations on wall embedment (excluding FS5):

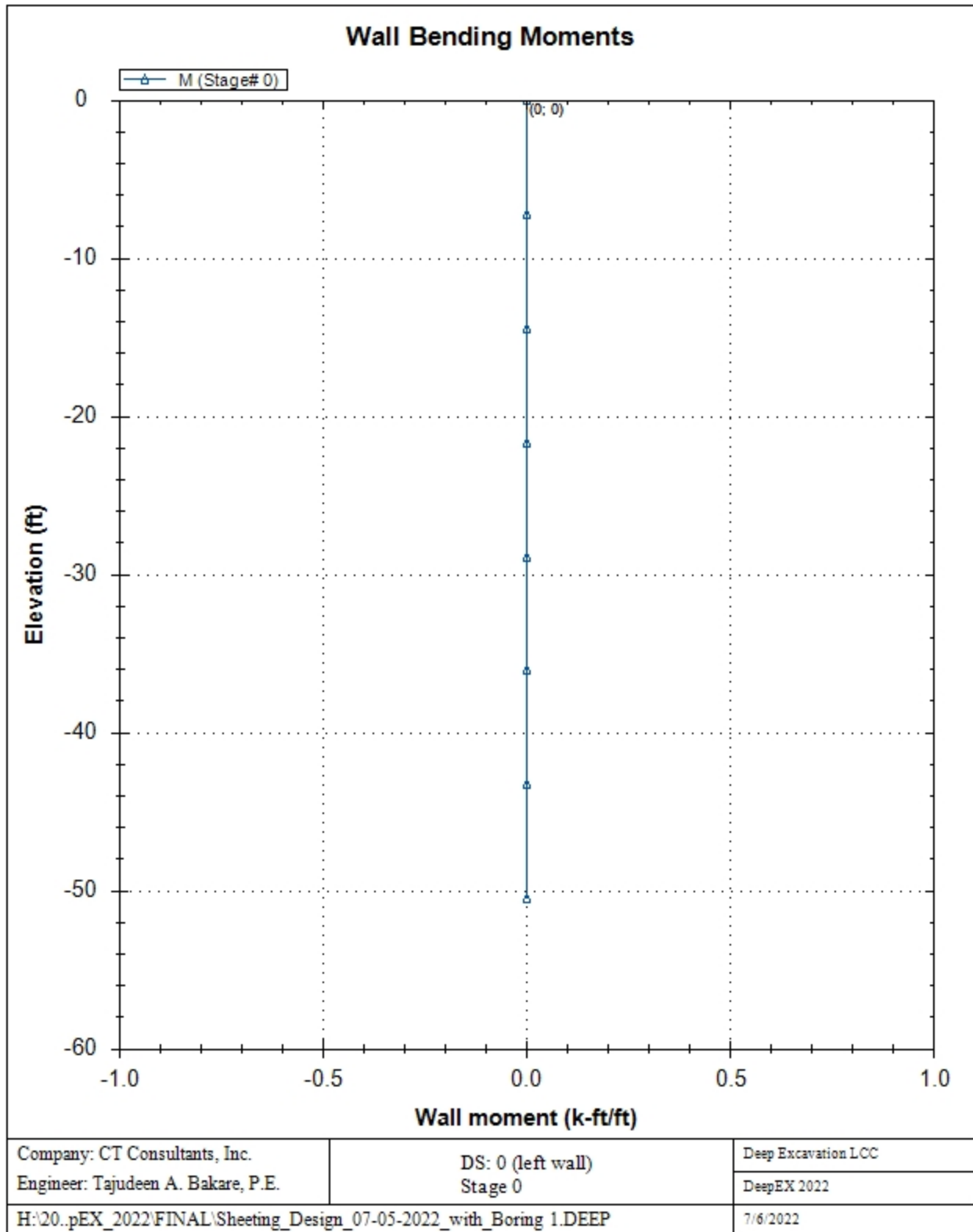
When the excavation is designed with allowable standards, engineers generally use minimum safety factors from 1.2 to 1.5 depending on the level of confidence. A minimum safety factor of 1.2 is generally applied on FS3.

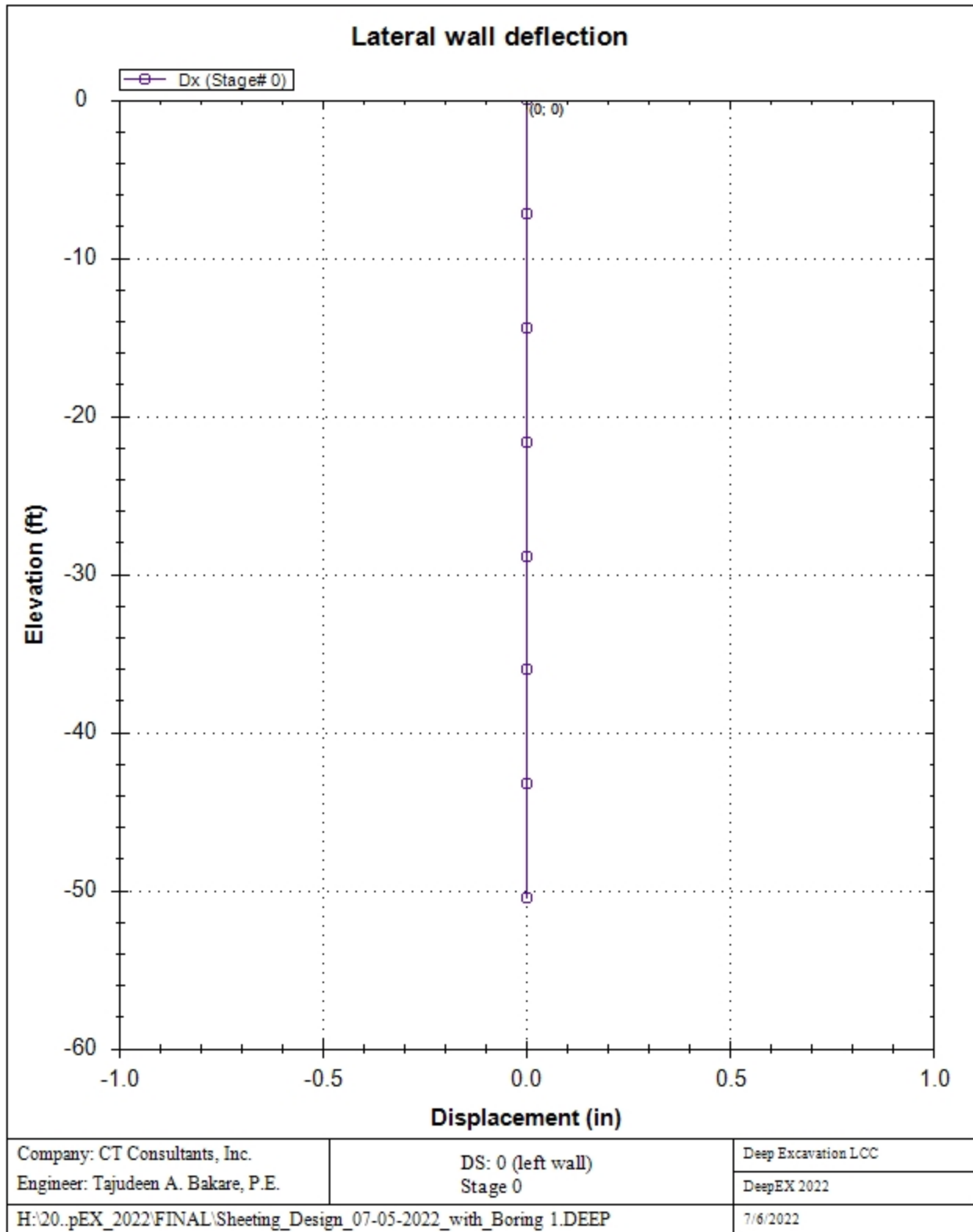
With ultimate limit state designs (such as Eurocode 7, and LRFD) the required safety factor must generally be greater than 1.0. In non-linear solutions it might be impossible to achieve exactly 1 on FS4 as this would likely trigger overall failure.

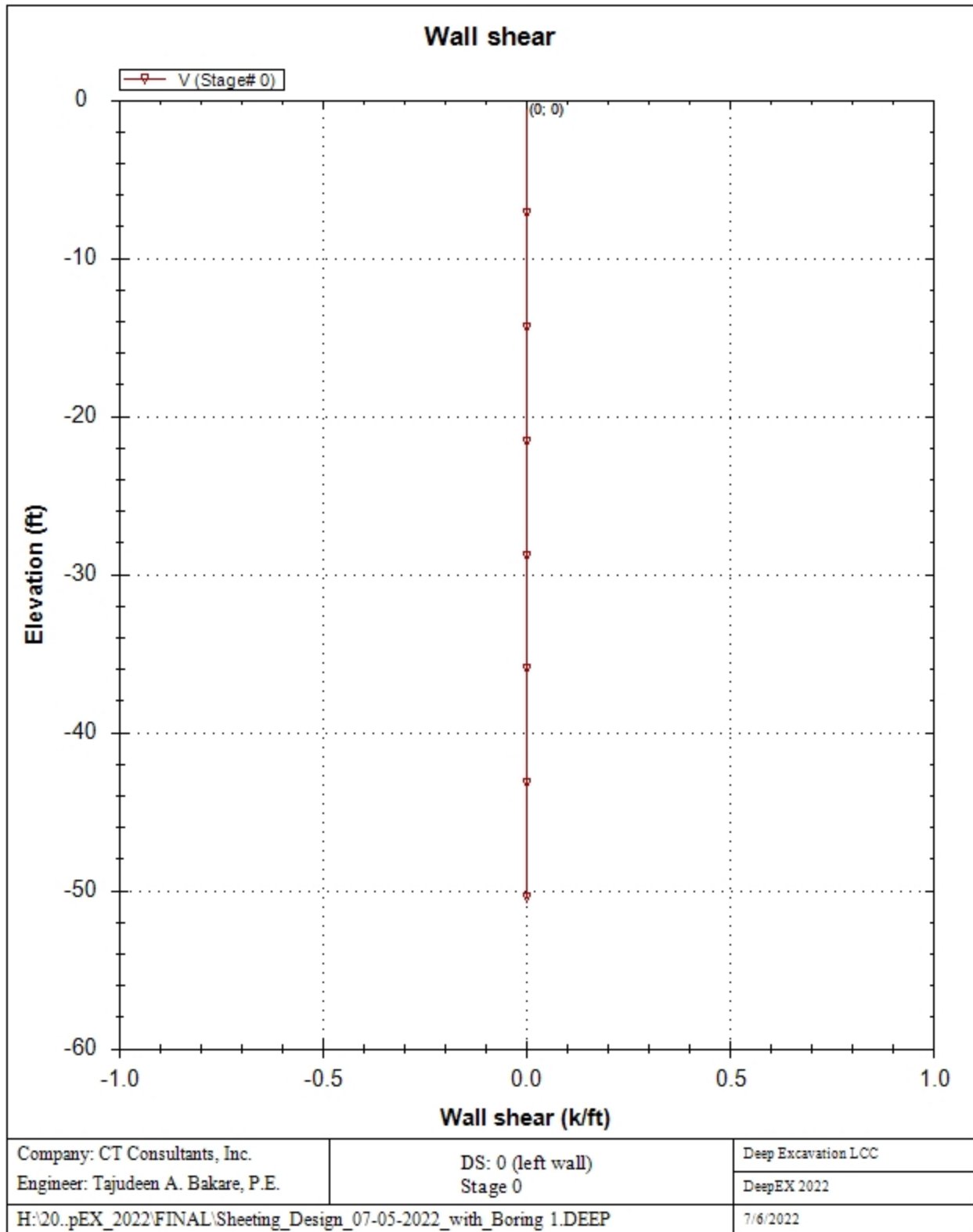
### **Result diagrams (for walls)**

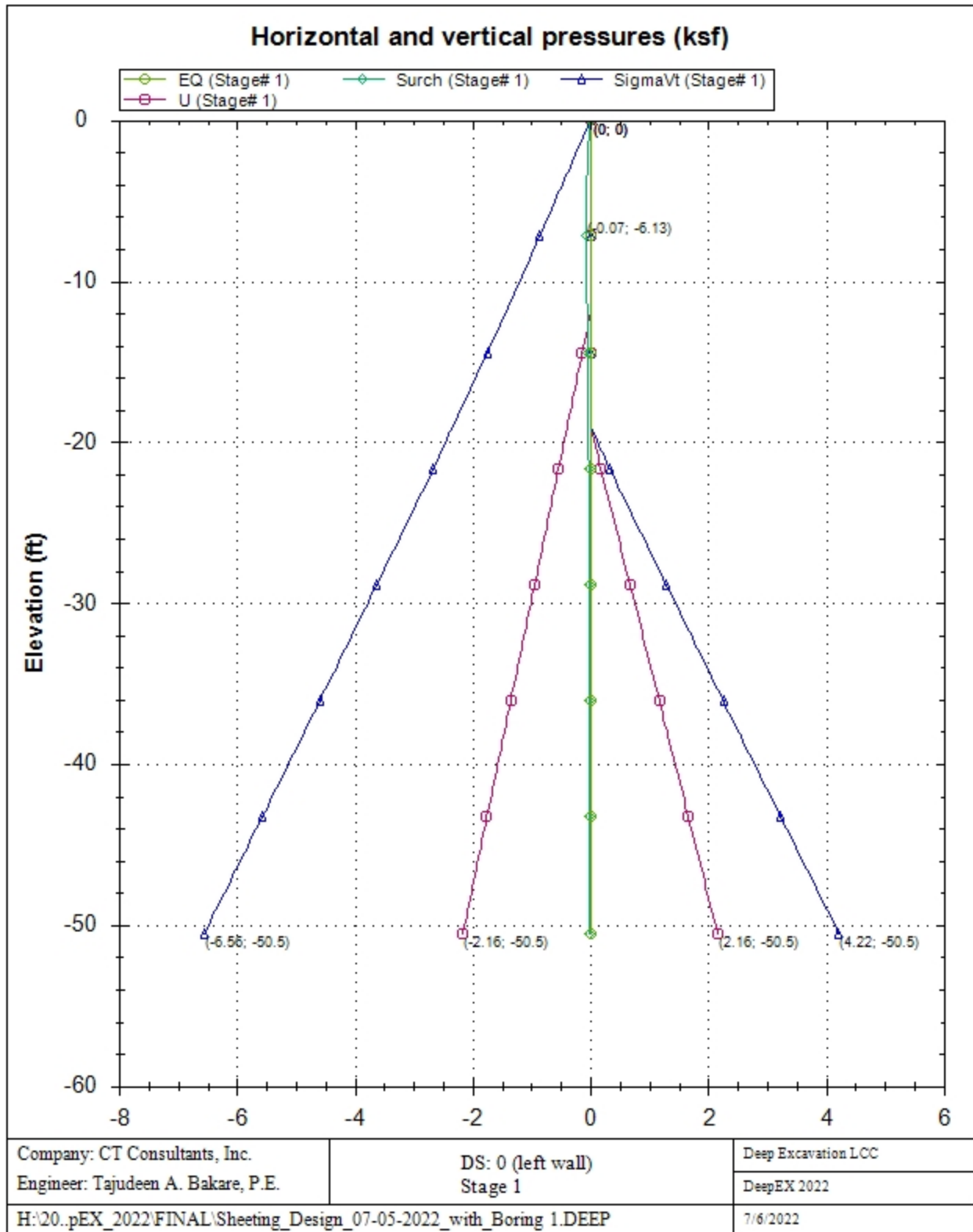
A sequence of result diagrams for each excavation stage is reported



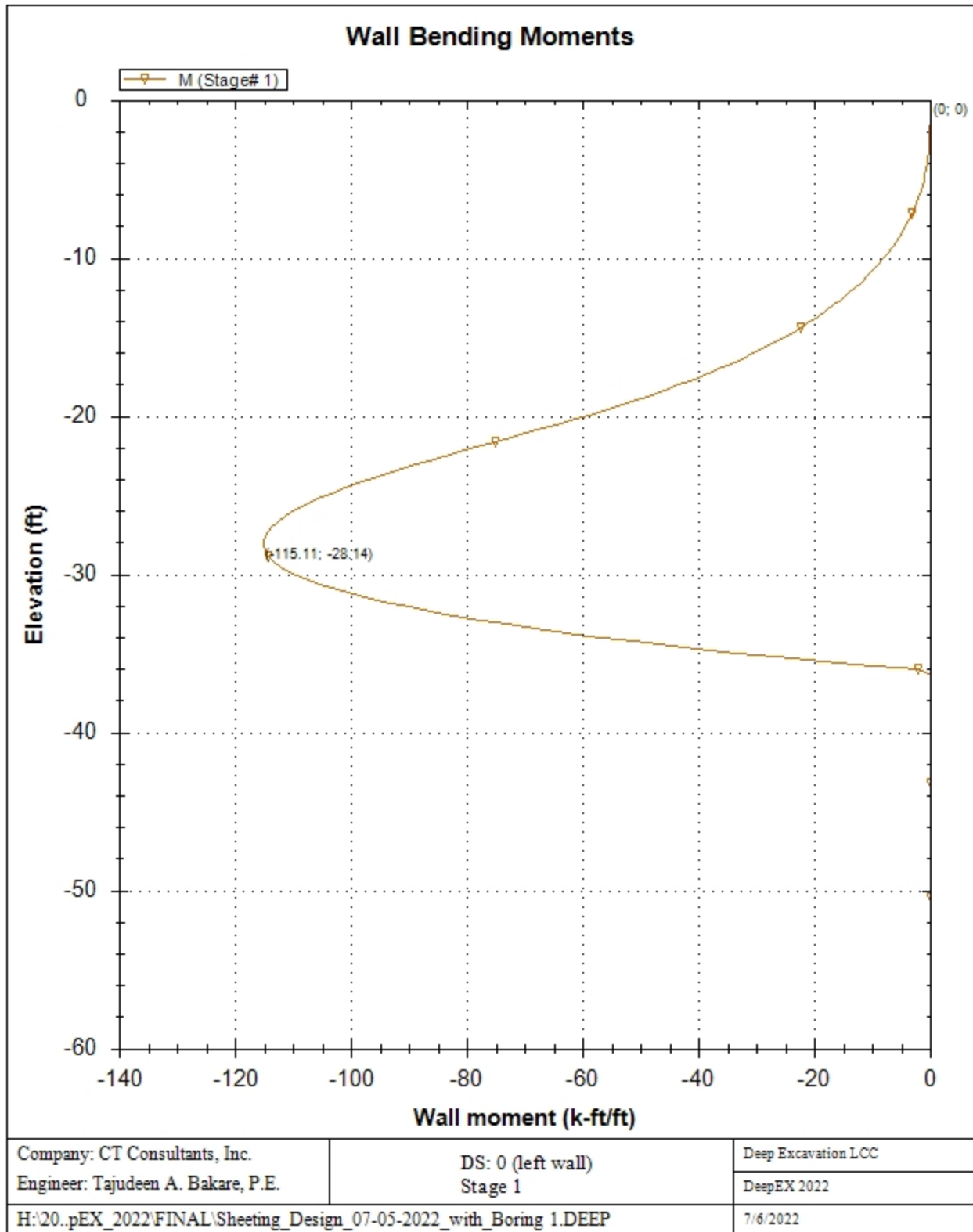


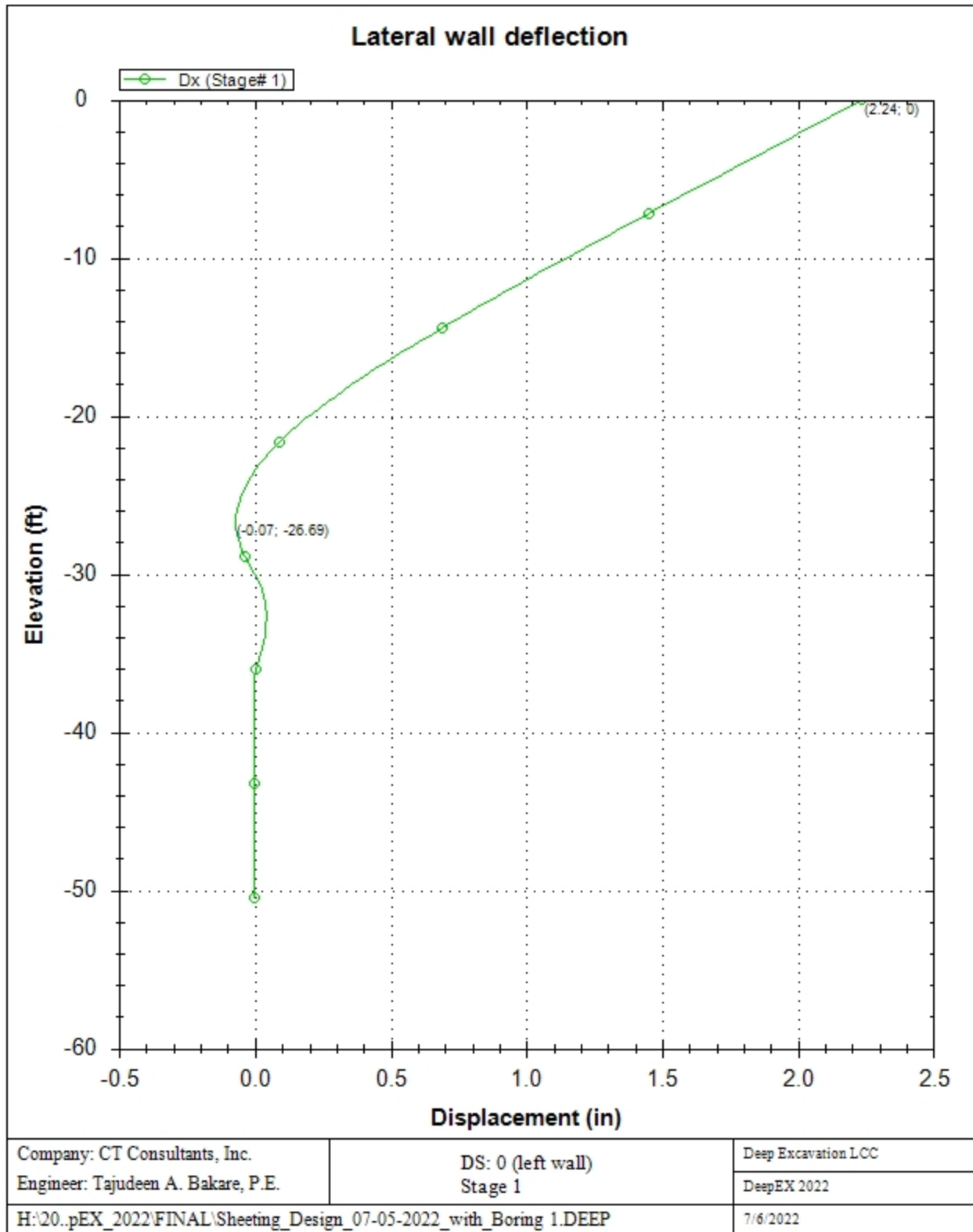


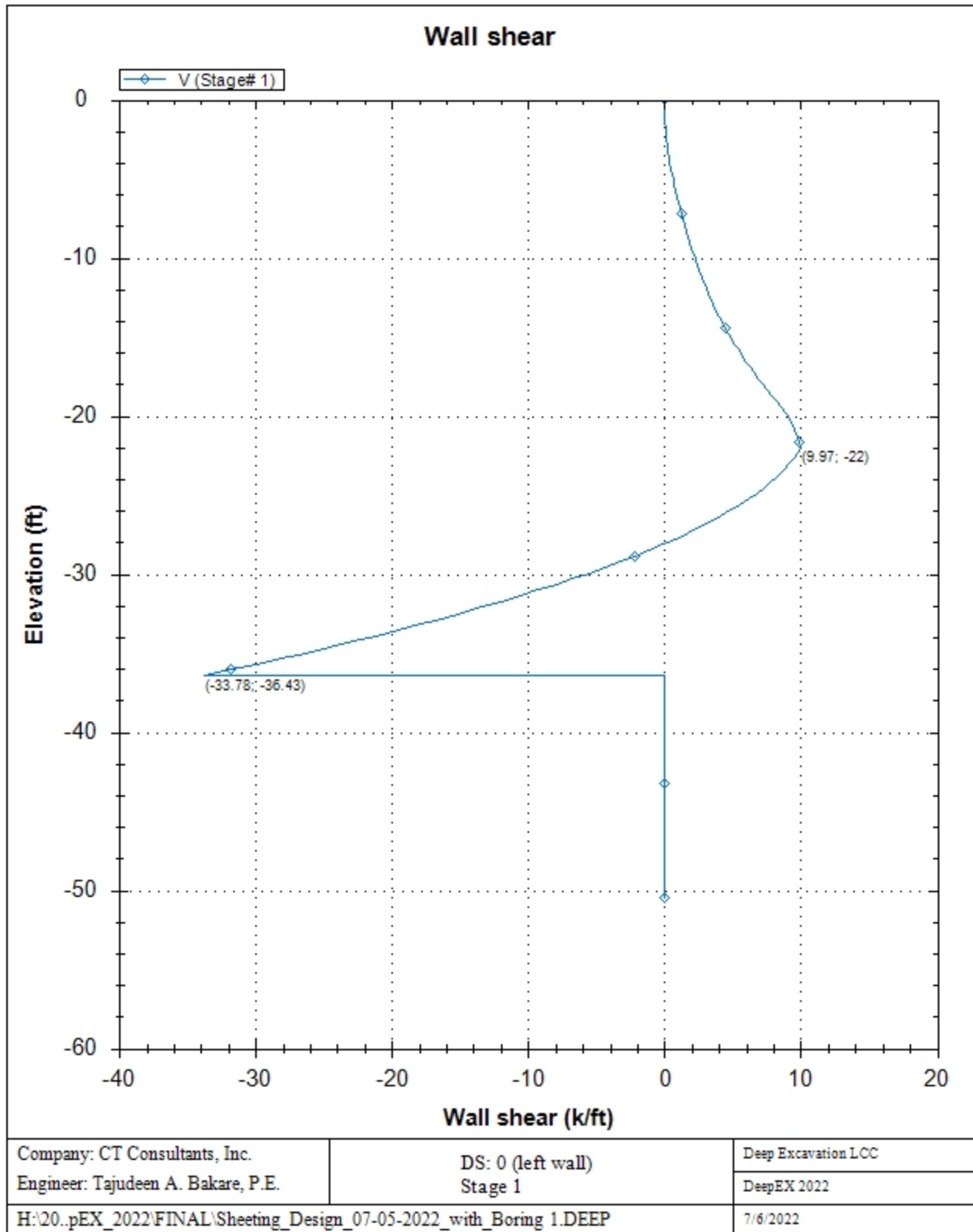












**WALL RESULTS TABLE**

## Wall 1 Stage: 0

Wall Node	EL (ft)	Sht L (ksf)	Sht R (ksf)	Shs L (ksf)	Shs R (ksf)	q (ksf)	U L (ksf)	U R (ksf)	M (k-ft/ft)	V (klf)	dx (in)	Mcap L (k-ft/ft)	Mcap R (k-ft/ft)	VcapL (klf)	VcapR (klf)
0	0	0	0	0	0	0	0	0	0	0	0	229.88	229.88	163.27	163.27
2	-0.72	0.025	0.405	0.025	0.405	0	0	0	0	0	0	229.88	229.88	163.27	163.27
4	-1.44	0.05	0.809	0.05	0.809	0	0	0	0	0	0	229.88	229.88	163.27	163.27
6	-2.16	0.074	1.214	0.074	1.214	0	0	0	0	0	0	229.88	229.88	163.27	163.27
8	-2.89	0.099	1.618	0.099	1.618	0	0	0	0	0	0	229.88	229.88	163.27	163.27
10	-3.61	0.124	2.023	0.124	2.023	0	0	0	0	0	0	229.88	229.88	163.27	163.27
12	-4.33	0.149	2.427	0.149	2.427	0	0	0	0	0	0	229.88	229.88	163.27	163.27
14	-5.05	0.174	2.832	0.174	2.832	0	0	0	0	0	0	229.88	229.88	163.27	163.27
16	-5.77	0.198	3.236	0.198	3.236	0	0	0	0	0	0	229.88	229.88	163.27	163.27
18	-6.49	0.223	3.641	0.223	3.641	0	0	0	0	0	0	229.88	229.88	163.27	163.27
20	-7.21	0.248	4.046	0.248	4.046	0	0	0	0	0	0	229.88	229.88	163.27	163.27
22	-7.94	0.273	4.45	0.273	4.45	0	0	0	0	0	0	229.88	229.88	163.27	163.27
24	-8.66	0.297	4.855	0.297	4.855	0	0	0	0	0	0	229.88	229.88	163.27	163.27
26	-9.38	0.322	5.259	0.322	5.259	0	0	0	0	0	0	229.88	229.88	163.27	163.27
28	-10.1	0.347	5.664	0.347	5.664	0	0	0	0	0	0	229.88	229.88	163.27	163.27
30	-10.82	0.372	6.068	0.372	6.068	0	0	0	0	0	0	229.88	229.88	163.27	163.27
32	-11.54	0.397	6.473	0.397	6.473	0	0	0	0	0	0	229.88	229.88	163.27	163.27
34	-12.26	0.434	6.83	0.418	6.814	0	0.016	0.016	0	0	0	229.88	229.88	163.27	163.27
36	-12.99	0.493	7.097	0.431	7.035	0	0.062	0.062	0	0	0	229.88	229.88	163.27	163.27
38	-13.71	0.551	7.363	0.445	7.256	0	0.107	0.107	0	0	0	229.88	229.88	163.27	163.27
40	-14.43	0.61	7.629	0.458	7.477	0	0.152	0.152	0	0	0	229.88	229.88	163.27	163.27
42	-15.15	0.668	7.895	0.472	7.699	0	0.197	0.197	0	0	0	229.88	229.88	163.27	163.27
44	-15.87	0.727	8.161	0.485	7.92	0	0.242	0.242	0	0	0	229.88	229.88	163.27	163.27
46	-16.59	0.785	8.428	0.499	8.141	0	0.287	0.287	0	0	0	229.88	229.88	163.27	163.27
48	-17.31	0.844	8.694	0.512	8.362	0	0.332	0.332	0	0	0	229.88	229.88	163.27	163.27
50	-18.04	0.903	8.96	0.526	8.583	0	0.377	0.377	0	0	0	229.88	229.88	163.27	163.27
52	-18.76	0.961	9.226	0.54	8.804	0	0.422	0.422	0	0	0	229.88	229.88	163.27	163.27
54	-19.48	1.019	9.486	0.553	9.019	0	0.467	0.467	0	0	0	229.88	229.88	163.27	163.27
56	-20.2	1.077	9.742	0.566	9.23	0	0.512	0.512	0	0	0	229.88	229.88	163.27	163.27
58	-20.92	1.135	9.998	0.579	9.441	0	0.557	0.557	0	0	0	229.88	229.88	163.27	163.27
60	-21.64	1.193	10.254	0.591	9.652	0	0.602	0.602	0	0	0	229.88	229.88	163.27	163.27
62	-22.36	1.079	12.219	0.432	11.573	0	0.647	0.647	0	0	0	229.88	229.88	163.27	163.27
64	-23.09	1.137	12.533	0.446	11.841	0	0.692	0.692	0	0	0	229.88	229.88	163.27	163.27
66	-23.81	1.196	12.847	0.459	12.11	0	0.737	0.737	0	0	0	229.88	229.88	163.27	163.27
68	-24.53	1.255	13.161	0.473	12.379	0	0.782	0.782	0	0	0	229.88	229.88	163.27	163.27
70	-25.25	1.314	13.475	0.487	12.648	0	0.827	0.827	0	0	0	229.88	229.88	163.27	163.27
72	-25.97	1.372	13.789	0.5	12.917	0	0.872	0.872	0	0	0	229.88	229.88	163.27	163.27
74	-26.69	1.431	14.103	0.514	13.186	0	0.917	0.917	0	0	0	229.88	229.88	163.27	163.27
76	-27.41	1.49	14.416	0.528	13.455	0	0.962	0.962	0	0	0	229.88	229.88	163.27	163.27
78	-28.14	1.548	14.73	0.542	13.723	0	1.007	1.007	0	0	0	229.88	229.88	163.27	163.27
80	-28.86	1.607	15.044	0.555	13.992	0	1.052	1.052	0	0	0	229.88	229.88	163.27	163.27
82	-29.58	1.666	15.358	0.569	14.261	0	1.097	1.097	0	0	0	229.88	229.88	163.27	163.27
84	-30.3	1.725	15.672	0.583	14.53	0	1.142	1.142	0	0	0	229.88	229.88	163.27	163.27
86	-31.02	1.783	15.986	0.596	14.799	0	1.187	1.187	0	0	0	229.88	229.88	163.27	163.27
88	-31.74	1.842	16.3	0.61	15.068	0	1.232	1.232	0	0	0	229.88	229.88	163.27	163.27
90	-32.46	1.901	16.613	0.624	15.336	0	1.277	1.277	0	0	0	229.88	229.88	163.27	163.27
92	-33.19	1.959	16.927	0.637	15.605	0	1.322	1.322	0	0	0	229.88	229.88	163.27	163.27
94	-33.91	2.018	17.241	0.651	15.874	0	1.367	1.367	0	0	0	229.88	229.88	163.27	163.27

96	-34.63	2.077	17.555	0.665	16.143	0	1.412	1.412	0	0	0	229.88	229.88	163.27	163.27
98	-35.35	2.136	17.869	0.679	16.412	0	1.457	1.457	0	0	0	229.88	229.88	163.27	163.27
100	-36.07	2.194	18.183	0.692	16.681	0	1.502	1.502	0	0	0	229.88	229.88	163.27	163.27
102	-36.79	2.253	18.497	0.706	16.95	0	1.547	1.547	0	0	0	229.88	229.88	163.27	163.27
104	-37.51	2.312	18.811	0.72	17.218	0	1.592	1.592	0	0	0	229.88	229.88	163.27	163.27
106	-38.24	2.396	19.013	0.759	17.376	0	1.637	1.637	0	0	0	229.88	229.88	163.27	163.27
108	-38.96	2.455	19.334	0.773	17.652	0	1.682	1.682	0	0	0	229.88	229.88	163.27	163.27
110	-39.68	2.514	19.656	0.787	17.928	0	1.727	1.727	0	0	0	229.88	229.88	163.27	163.27
112	-40.4	2.574	19.977	0.801	18.205	0	1.772	1.772	0	0	0	229.88	229.88	163.27	163.27
114	-41.12	2.633	20.298	0.816	18.481	0	1.817	1.817	0	0	0	229.88	229.88	163.27	163.27
116	-41.84	2.692	20.62	0.83	18.758	0	1.862	1.862	0	0	0	229.88	229.88	163.27	163.27
118	-42.56	2.751	20.941	0.844	19.034	0	1.907	1.907	0	0	0	229.88	229.88	163.27	163.27
120	-43.29	2.81	21.262	0.858	19.31	0	1.952	1.952	0	0	0	229.88	229.88	163.27	163.27
122	-44.01	2.869	21.584	0.872	19.587	0	1.997	1.997	0	0	0	229.88	229.88	163.27	163.27
124	-44.73	2.928	21.905	0.886	19.863	0	2.042	2.042	0	0	0	229.88	229.88	163.27	163.27
126	-45.45	2.987	22.227	0.9	20.139	0	2.087	2.087	0	0	0	229.88	229.88	163.27	163.27
128	-46.17	3.046	22.548	0.914	20.416	0	2.132	2.132	0	0	0	229.88	229.88	163.27	163.27
130	-46.89	3.105	22.869	0.928	20.692	0	2.177	2.177	0	0	0	229.88	229.88	163.27	163.27
132	-47.61	3.165	23.191	0.942	20.968	0	2.222	2.222	0	0	0	229.88	229.88	163.27	163.27
134	-48.34	3.224	23.512	0.956	21.245	0	2.267	2.267	0	0	0	229.88	229.88	163.27	163.27
136	-49.06	3.283	23.834	0.97	21.521	0	2.312	2.312	0	0	0	229.88	229.88	163.27	163.27
138	-49.78	3.342	24.155	0.985	21.798	0	2.357	2.357	0	0	0	229.88	229.88	163.27	163.27
140	-50.5	3.401	24.476	0.999	22.074	0	2.402	2.402	0	0	0	229.88	229.88	163.27	163.27

Wall 1 Stage: 1

Wall Node	EL (ft)	Sht L (ksf)	Sht R (ksf)	Shs L (ksf)	Shs R (ksf)	q (ksf)	U L (ksf)	U R (ksf)	M (k-ft/ft)	V (klf)	dx (in)	Mcap L (k-ft/ft)	Mcap R (k-ft/ft)	VcapL (klf)	VcapR (klf)
0	0	0	0	0	0	0	0	0	0	0	2.24	229.88	229.88	163.27	163.27
2	-0.72	0.025	0	0.025	0	0.015	0	0	0	0.01	2.16	229.88	229.88	163.27	163.27
4	-1.44	0.05	0	0.05	0	0.03	0	0	0.03	0.06	2.08	229.88	229.88	163.27	163.27
6	-2.16	0.074	0	0.074	0	0.042	0	0	0.09	0.13	2	229.88	229.88	163.27	163.27
8	-2.89	0.099	0	0.099	0	0.051	0	0	0.22	0.22	1.92	229.88	229.88	163.27	163.27
10	-3.61	0.124	0	0.124	0	0.058	0	0	0.42	0.34	1.84	229.88	229.88	163.27	163.27
12	-4.33	0.149	0	0.149	0	0.063	0	0	0.72	0.49	1.76	229.88	229.88	163.27	163.27
14	-5.05	0.174	0	0.174	0	0.065	0	0	1.13	0.65	1.69	229.88	229.88	163.27	163.27
16	-5.77	0.198	0	0.198	0	0.067	0	0	1.66	0.83	1.61	229.88	229.88	163.27	163.27
18	-6.49	0.223	0	0.223	0	0.067	0	0	2.33	1.03	1.53	229.88	229.88	163.27	163.27
20	-7.21	0.248	0	0.248	0	0.066	0	0	3.15	1.25	1.45	229.88	229.88	163.27	163.27
22	-7.94	0.273	0	0.273	0	0.065	0	0	4.14	1.48	1.37	229.88	229.88	163.27	163.27
24	-8.66	0.297	0	0.297	0	0.063	0	0	5.3	1.74	1.29	229.88	229.88	163.27	163.27
26	-9.38	0.322	0	0.322	0	0.061	0	0	6.65	2	1.22	229.88	229.88	163.27	163.27
28	-10.1	0.347	0	0.347	0	0.059	0	0	8.19	2.29	1.14	229.88	229.88	163.27	163.27
30	-10.82	0.372	0	0.372	0	0.057	0	0	9.95	2.59	1.06	229.88	229.88	163.27	163.27
32	-11.54	0.397	0	0.397	0	0.055	0	0	11.94	2.91	0.98	229.88	229.88	163.27	163.27
34	-12.26	0.433	0	0.418	0	0.052	0.015	0	14.15	3.24	0.91	229.88	229.88	163.27	163.27
36	-12.99	0.488	0	0.433	0	0.05	0.055	0	16.62	3.61	0.84	229.88	229.88	163.27	163.27
38	-13.71	0.544	0	0.448	0	0.048	0.096	0	19.37	4.02	0.76	229.88	229.88	163.27	163.27
40	-14.43	0.599	0	0.463	0	0.046	0.136	0	22.43	4.47	0.69	229.88	229.88	163.27	163.27
42	-15.15	0.654	0	0.477	0	0.043	0.177	0	25.82	4.95	0.62	229.88	229.88	163.27	163.27
44	-15.87	0.71	0	0.492	0	0.041	0.217	0	29.58	5.47	0.55	229.88	229.88	163.27	163.27
46	-16.59	0.765	0	0.507	0	0.039	0.258	0	33.73	6.03	0.48	229.88	229.88	163.27	163.27
48	-17.31	0.82	0	0.522	0	0.037	0.298	0	38.29	6.63	0.42	229.88	229.88	163.27	163.27

50	-18.04	0.876	0	0.537	0	0.036	0.339	0	43.31	7.27	0.36	229.88	229.88	163.27	163.27
52	-18.76	0.931	0	0.552	0	0.034	0.379	0	48.79	7.95	0.3	229.88	229.88	163.27	163.27
54	-19.48	0.986	0.159	0.566	0.126	0.032	0.42	0.033	54.78	8.62	0.24	229.88	229.88	163.27	163.27
56	-20.2	1.041	0.398	0.58	0.316	0.031	0.461	0.082	61.21	9.18	0.19	229.88	229.88	163.27	163.27
58	-20.92	1.095	0.638	0.594	0.506	0.029	0.501	0.132	67.99	9.6	0.14	229.88	229.88	163.27	163.27
60	-21.64	1.15	0.877	0.609	0.696	0.028	0.542	0.181	75.02	9.88	0.09	229.88	229.88	163.27	163.27
62	-22.36	1.031	1.805	0.449	1.574	0.026	0.582	0.231	82.15	9.72	0.05	229.88	229.88	163.27	163.27
64	-23.09	1.087	2.1	0.464	1.82	0.025	0.623	0.28	88.95	9.09	0.02	229.88	229.88	163.27	163.27
66	-23.81	1.142	2.395	0.479	2.065	0.024	0.663	0.33	95.23	8.29	-0.01	229.88	229.88	163.27	163.27
68	-24.53	1.197	2.69	0.494	2.311	0.023	0.704	0.379	100.88	7.32	-0.04	229.88	229.88	163.27	163.27
70	-25.25	1.253	2.985	0.509	2.556	0.022	0.744	0.429	105.75	6.17	-0.05	229.88	229.88	163.27	163.27
72	-25.97	1.308	3.28	0.524	2.801	0.021	0.785	0.479	109.74	4.85	-0.07	229.88	229.88	163.27	163.27
74	-26.69	1.364	3.575	0.538	3.047	0.02	0.825	0.528	112.71	3.36	-0.07	229.88	229.88	163.27	163.27
76	-27.41	1.419	3.87	0.553	3.292	0.019	0.866	0.578	114.55	1.69	-0.07	229.88	229.88	163.27	163.27
78	-28.14	1.474	4.165	0.568	3.538	0.018	0.906	0.627	115.11	-0.15	-0.06	229.88	229.88	163.27	163.27
80	-28.86	1.53	4.46	0.583	3.783	0.017	0.947	0.677	114.29	-2.17	-0.04	229.88	229.88	163.27	163.27
82	-29.58	1.585	4.755	0.598	4.028	0.016	0.987	0.726	111.95	-4.35	-0.01	229.88	229.88	163.27	163.27
84	-30.3	1.641	5.05	0.613	4.274	0.016	1.028	0.776	107.96	-6.71	0.01	229.88	229.88	163.27	163.27
86	-31.02	1.696	5.344	0.628	4.519	0.015	1.068	0.825	102.22	-9.25	0.03	229.88	229.88	163.27	163.27
88	-31.74	1.751	5.639	0.643	4.765	0.014	1.109	0.875	94.58	-11.96	0.04	229.88	229.88	163.27	163.27
90	-32.46	1.807	5.934	0.658	5.01	0.014	1.149	0.924	84.92	-14.84	0.04	229.88	229.88	163.27	163.27
92	-33.19	1.862	6.229	0.672	5.256	0.013	1.19	0.974	73.12	-17.89	0.04	229.88	229.88	163.27	163.27
94	-33.91	1.918	6.524	0.687	5.501	0.012	1.23	1.023	59.06	-21.12	0.04	229.88	229.88	163.27	163.27
96	-34.63	1.973	6.819	0.702	5.746	0.012	1.271	1.073	42.61	-24.52	0.03	229.88	229.88	163.27	163.27
98	-35.35	2.028	7.114	0.717	5.992	0.011	1.311	1.122	23.64	-28.1	0.02	229.88	229.88	163.27	163.27
100	-36.07	2.084	7.409	0.732	6.237	0.011	1.352	1.172	2.03	-31.84	0.01	229.88	229.88	163.27	163.27
102	-36.79	2.139	7.704	0.747	6.483	0.01	1.392	1.221	0	0	0	229.88	229.88	163.27	163.27
104	-37.51	2.195	7.999	0.762	6.728	0.01	1.433	1.271	0	0	0	229.88	229.88	163.27	163.27
106	-38.24	2.276	8.182	0.803	6.862	0.01	1.473	1.32	0	0	0	229.88	229.88	163.27	163.27
108	-38.96	2.332	8.485	0.818	7.115	0.009	1.514	1.37	0	0	0	229.88	229.88	163.27	163.27
110	-39.68	2.388	8.787	0.833	7.368	0.009	1.554	1.419	0	0	0	229.88	229.88	163.27	163.27
112	-40.4	2.443	9.09	0.848	7.621	0.008	1.595	1.469	0	0	0	229.88	229.88	163.27	163.27
114	-41.12	2.499	9.392	0.864	7.874	0.008	1.635	1.518	0	0	0	229.88	229.88	163.27	163.27
116	-41.84	2.555	9.695	0.879	8.127	0.008	1.676	1.568	0	0	0	229.88	229.88	163.27	163.27
118	-42.56	2.611	9.997	0.894	8.38	0.007	1.716	1.617	0	0	0	229.88	229.88	163.27	163.27
120	-43.29	2.667	10.299	0.91	8.632	0.007	1.757	1.667	0	0	0	229.88	229.88	163.27	163.27
122	-44.01	2.722	10.602	0.925	8.885	0.007	1.798	1.716	0	0	0	229.88	229.88	163.27	163.27
124	-44.73	2.778	10.904	0.94	9.138	0.007	1.838	1.766	0	0	0	229.88	229.88	163.27	163.27
126	-45.45	2.834	11.207	0.955	9.391	0.006	1.879	1.816	0	0	0	229.88	229.88	163.27	163.27
128	-46.17	2.89	11.509	0.971	9.644	0.006	1.919	1.865	0	0	0	229.88	229.88	163.27	163.27
130	-46.89	2.946	11.812	0.986	9.897	0.006	1.96	1.915	0	0	0	229.88	229.88	163.27	163.27
132	-47.61	3.001	12.114	1.001	10.15	0.006	2	1.964	0	0	0	229.88	229.88	163.27	163.27
134	-48.34	3.057	12.417	1.016	10.403	0.005	2.041	2.014	0	0	0	229.88	229.88	163.27	163.27
136	-49.06	3.113	12.719	1.032	10.656	0.005	2.081	2.063	0	0	0	229.88	229.88	163.27	163.27
138	-49.78	3.169	13.021	1.047	10.909	0.005	2.122	2.113	0	0	0	229.88	229.88	163.27	163.27
140	-50.5	3.224	13.324	1.062	11.162	0.005	2.162	2.162	0	0	0	229.88	229.88	163.27	163.27

## LEGEND

Wall node=number of the node (0 at top)

EL= Node elevation

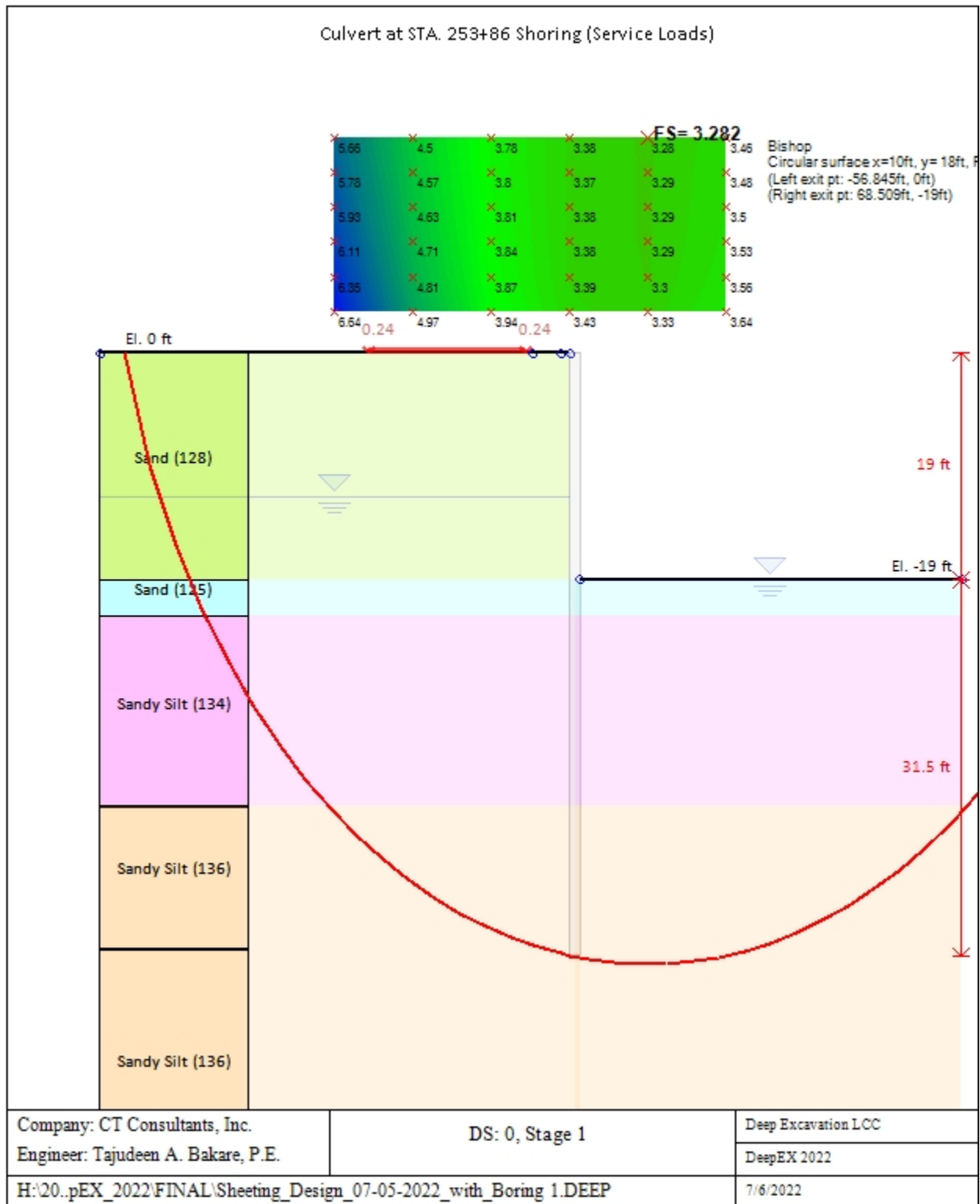
Sht L=Total horizontal soil pressure (on the left side of the wall)

Sht R=Total horizontal soil pressure (on the right side of the wall)

Shs L=Effective horizontal soil pressure (on the left side of the wall)  
Shs R=Effective horizontal soil pressure (on the right side of the wall)  
q=pressure given by the surcharge  
U L= Water pressure (on the left side of the wall)  
U R= Water pressure (on the right side of the wall)  
M=bending moment (per unit length)  
V=shear (per unit length)  
dx=wall deflection  
McapL=Ultimate bending moment (on the left side of the wall)  
McapR=Ultimate bending moment (on the right side of the wall)  
VcapL=Ultimate resistance shear (on the left side of the wall)  
VcapR=Ultimate resistance shear (on the right side of the wall)

## EXCAVATION STAGES AND SLOPE STABILITY

Reports a sequence of figures for each stage with slope stability results.





## SLOPE STABILITY ANALYSIS: SLICE RESULTS ALL STAGES

Slope stability analysis design section: Culvert at STA. 253+86 Shoring (Service Loads)

### Slope stability analysis Stage: 0

Slope stability not analyzed for this stage.

### Slope stability analysis Stage: 1

Slope stability calculated for this stage.

Critical point at x= 10 z= 18 FS= 3.282

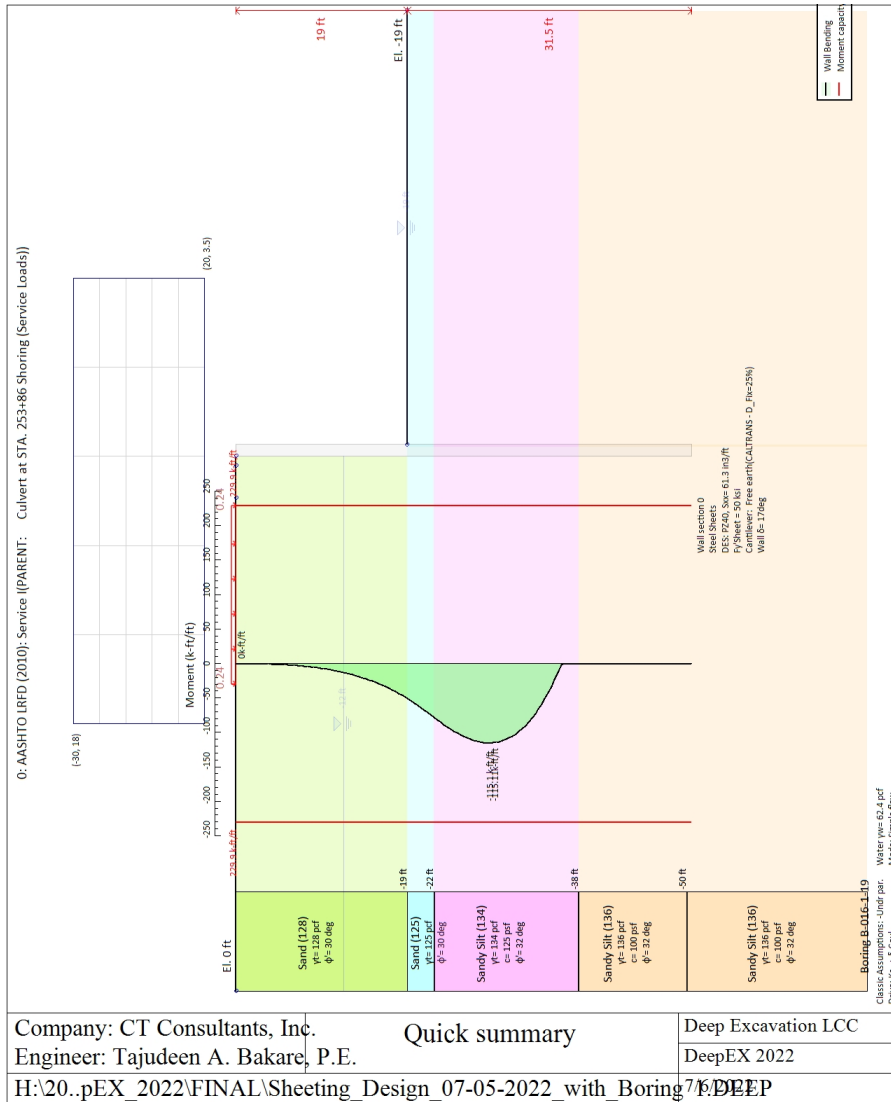
Slice No.	x1 ft	ZsL ft	ZtL ft	x2 ft	ZsR ft	ZtR ft	DL ft	an deg	Fr deg	c ksf	Wn k/ft	ubL ksf	ubR ksf	tBase k/ft	Nr k/ft	EiL k/ft	EiR k/ft	TL k/ft	TR k/ft	UbF k/ft
0	-56.84	0	0	-53.55	-9.46	0	10.02	70.78	30	0	1.9	0	0	0.7	3.8	0	0	0	0	0
1	-53.55	-9.46	0	-50.25	-16.1	0	7.41	63.56	30	0	5.1	0	0.3	1.4	8	0	0	0	0	0.6
2	-50.25	-16.1	0	-46.95	-21.36	0	6.21	57.92	30	0	7.6	0.3	0.6	1.6	9.1	0	0	0	0	2.6
3	-46.95	-21.36	0	-43.65	-25.75	0	5.49	53.08	31	0.06	9.6	0.6	0.9	1.9	9.6	0	0	0	0	4
4	-43.65	-25.75	0	-40.35	-29.51	0	5	48.73	32	0.12	11.4	0.9	1.1	2.1	10.1	0	0	0	0	4.9
5	-40.35	-29.51	0	-37.05	-32.78	0	4.64	44.74	32	0.12	13	1.1	1.3	2.2	10.6	0	0	0	0	5.5
6	-37.05	-32.78	0	-33.75	-35.65	0	4.37	41.01	32	0.12	14.3	1.3	1.5	2.3	11	0	0	0	0	6.1
7	-33.75	-35.65	0	-30.45	-38.18	0	4.16	37.48	32	0.11	15.5	1.5	1.6	2.3	11.3	0	0	0	0	6.5
8	-30.45	-38.18	0	-27.16	-40.41	0	3.98	34.11	32	0.1	16.6	1.6	1.8	2.3	11.7	0	0	0	0	6.8
9	-27.16	-40.41	0	-23.86	-42.38	0	3.84	30.87	32	0.1	17.5	1.8	1.9	2.5	12.4	0	0	0	0	7
10	-23.86	-42.38	0	-20.56	-44.12	0	3.73	27.74	32	0.1	18.4	1.9	2	2.6	13	0	0	0	0	7.3
11	-20.56	-44.12	0	-17.26	-45.63	0	3.63	24.69	32	0.1	19.1	2	2.1	2.6	13.2	0	0	0	0	7.4
12	-17.26	-45.63	0	-13.96	-46.95	0	3.55	21.72	32	0.1	19.7	2.1	2.2	2.7	13.4	0	0	0	0	7.6
13	-13.96	-46.95	0	-10.66	-48.07	0	3.48	18.81	32	0.1	20.3	2.2	2.3	2.7	13.6	0	0	0	0	7.7
14	-10.66	-48.07	0	-7.36	-49.01	0	3.43	15.95	32	0.1	20.7	2.3	2.3	2.7	13.8	0	0	0	0	7.8
15	-7.36	-49.01	0	-4.66	-49.66	0	2.78	13.38	32	0.1	17.3	2.3	2.3	2.2	11.2	0	0	0	0	6.5
16	-4.66	-49.66	0	-1	-50.35	0	3.72	10.68	32	0.1	23.7	2.3	2.4	2.9	14.8	0	0	0	0	8.8
17	-1	-50.35	0	0	-50.5	0	1.01	8.72	32	0.1	6.5	2.4	2.4	0.8	4.1	0	0	0	0	2.4
18	0	-50.5	0	1.37	-50.69	0	1.38	7.73	32	0.1	9	2.4	2	1.2	5.9	0	0	0	0	3
19	1.37	-50.69	-19	2.53	-50.82	-19	1.17	6.68	32	0.1	4.9	2	2	0.5	2.6	0	0	0	0	2.3
20	2.53	-50.82	-19	5.83	-51.1	-19	3.31	4.82	32	0.1	14.1	2	2	1.5	7.4	0	0	0	0	6.6
21	5.83	-51.1	-19	9.13	-51.22	-19	3.3	2.09	32	0.1	14.2	2	2	1.5	7.5	0	0	0	0	6.6
22	9.13	-51.22	-19	12.43	-51.18	-19	3.3	-0.65	32	0.1	14.2	2	2	1.6	7.6	0	0	0	0	6.6
23	12.43	-51.18	-19	15.73	-50.99	-19	3.3	-3.38	32	0.1	14.2	2	2	1.6	7.7	0	0	0	0	6.6
24	15.73	-50.99	-19	19.03	-50.64	-19	3.32	-6.12	32	0.1	14.1	2	2	1.6	7.7	0	0	0	0	6.6
25	19.03	-50.64	-19	22.33	-50.12	-19	3.34	-8.87	32	0.1	13.9	2	1.9	1.6	7.7	0	0	0	0	6.5
26	22.33	-50.12	-19	25.62	-49.44	-19	3.37	-11.65	32	0.1	13.6	1.9	1.9	1.6	7.7	0	0	0	0	6.5
27	25.62	-49.44	-19	28.92	-48.59	-19	3.41	-14.45	32	0.1	13.3	1.9	1.8	1.6	7.7	0	0	0	0	6.4
28	28.92	-48.59	-19	32.22	-47.56	-19	3.45	-17.29	32	0.1	12.8	1.8	1.8	1.6	7.7	0	0	0	0	6.3
29	32.22	-47.56	-19	35.52	-46.35	-19	3.51	-20.18	32	0.1	12.3	1.8	1.7	1.5	7.6	0	0	0	0	6.1
30	35.52	-46.35	-19	38.82	-44.94	-19	3.59	-23.12	32	0.1	11.7	1.7	1.6	1.5	7.5	0	0	0	0	6
31	38.82	-44.94	-19	42.12	-43.32	-19	3.67	-26.12	32	0.1	11.1	1.6	1.5	1.5	7.3	0	0	0	0	5.8
32	42.12	-43.32	-19	45.42	-41.48	-19	3.78	-29.21	32	0.1	10.3	1.5	1.4	1.5	7.1	0	0	0	0	5.5
33	45.42	-41.48	-19	48.72	-39.39	-19	3.91	-32.39	32	0.1	9.4	1.4	1.3	1.4	6.8	0	0	0	0	5.2
34	48.72	-39.39	-19	52.01	-37.02	-19	4.06	-35.69	32	0.11	8.4	1.3	1.1	1.4	6.5	0	0	0	0	4.9
35	52.01	-37.02	-19	55.31	-34.33	-19	4.25	-39.13	32	0.12	7.3	1.1	1	1.3	6	0	0	0	0	4.4
36	55.31	-34.33	-19	58.61	-31.29	-19	4.49	-42.75	32	0.12	6	1	0.8	1.2	5.4	0	0	0	0	3.9
37	58.61	-31.29	-19	61.91	-27.8	-19	4.8	-46.59	32	0.12	4.6	0.8	0.5	1.1	4.6	0	0	0	0	3.2
38	61.91	-27.8	-19	65.21	-23.76	-19	5.21	-50.74	32	0.12	2.9	0.5	0.3	0.9	3.4	0	0	0	0	2.2
39	65.21	-23.76	-19	68.51	-19	-19	5.79	-55.29	31	0.06	1	0.3	0	0.4	1.5	0	0	0	0	0.9

LEGEND

x1 = Left x coordinate  
ZsL= Left slice bottom elevation  
ZtL= Left top elevation  
x2 = Right x coordinate  
ZsR= Right slice bottom elevation  
ZtR= Right top elevation  
DL = Slice base width  
an = Base angle  
Fr = Average friction angle at base  
c = Average cohesion at base (may include undrained clay strengths)  
Wn = Total slice weight  
ubL= Water pressure at left bottom point  
ubR= Water pressure at right bottom point  
tBase= Base shear resistance  
Nr = Effective normal reaction at bottom of slice  
EiL= Lateral interslice force on left face  
EiR= Lateral interslice force on right face  
TL = Vertical interslice shear on left vertical face  
TR = Vertical interslice shear on right vertical face  
UbF= Normal water force at slice base

***Project: ODOT PID No. 108665; LAK-20-19.59 - WEST  
Results for Design Section 1: 0: AASHTO LRFD (2010):  
Service I***

## ANALYSIS AND CHECKING SUMMARY



### Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	115.11/229.88	21.622	2.535	1.807	-36.43	3.282

### Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

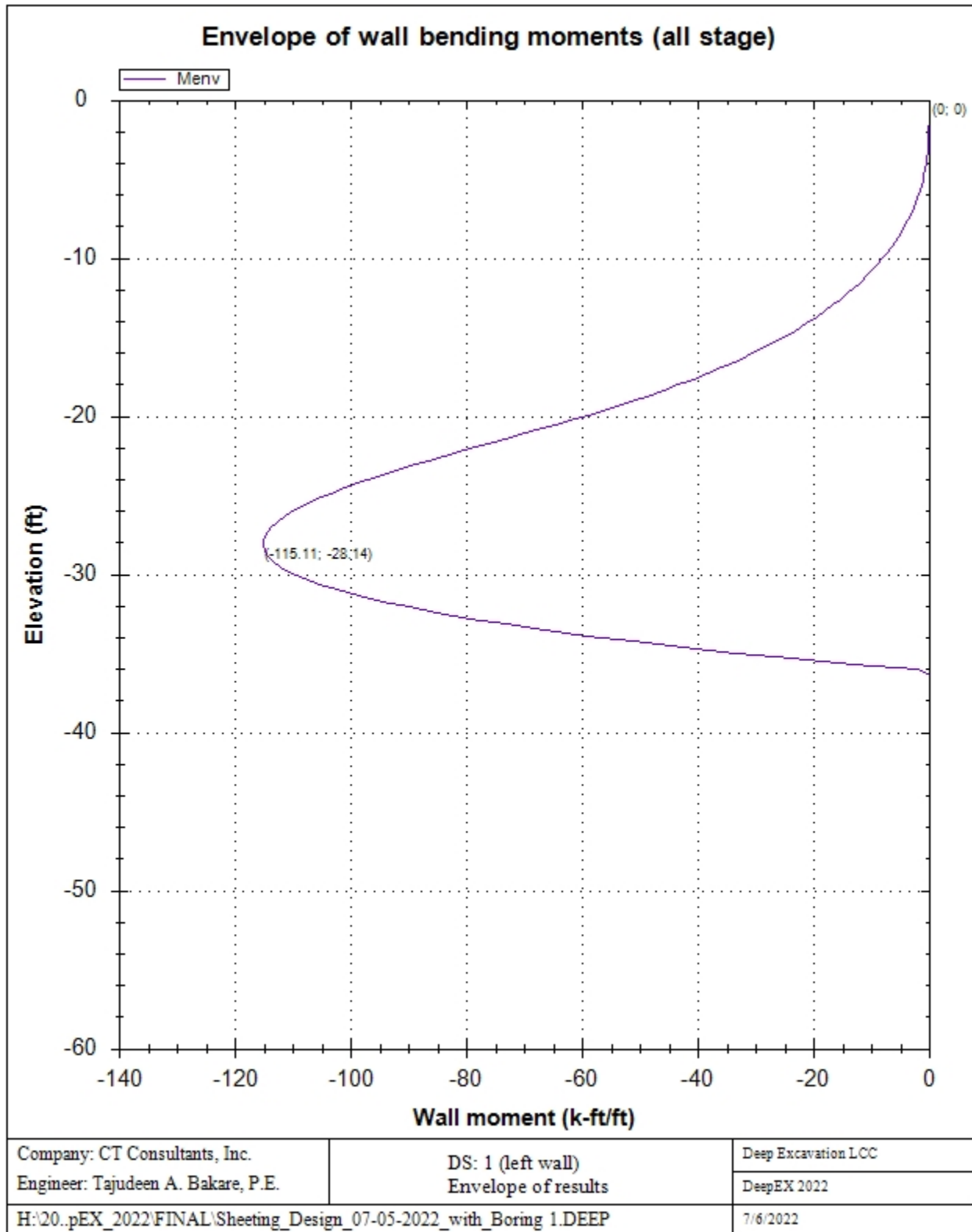
1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.849	12.4	3.282	0.373	12.449	3.282

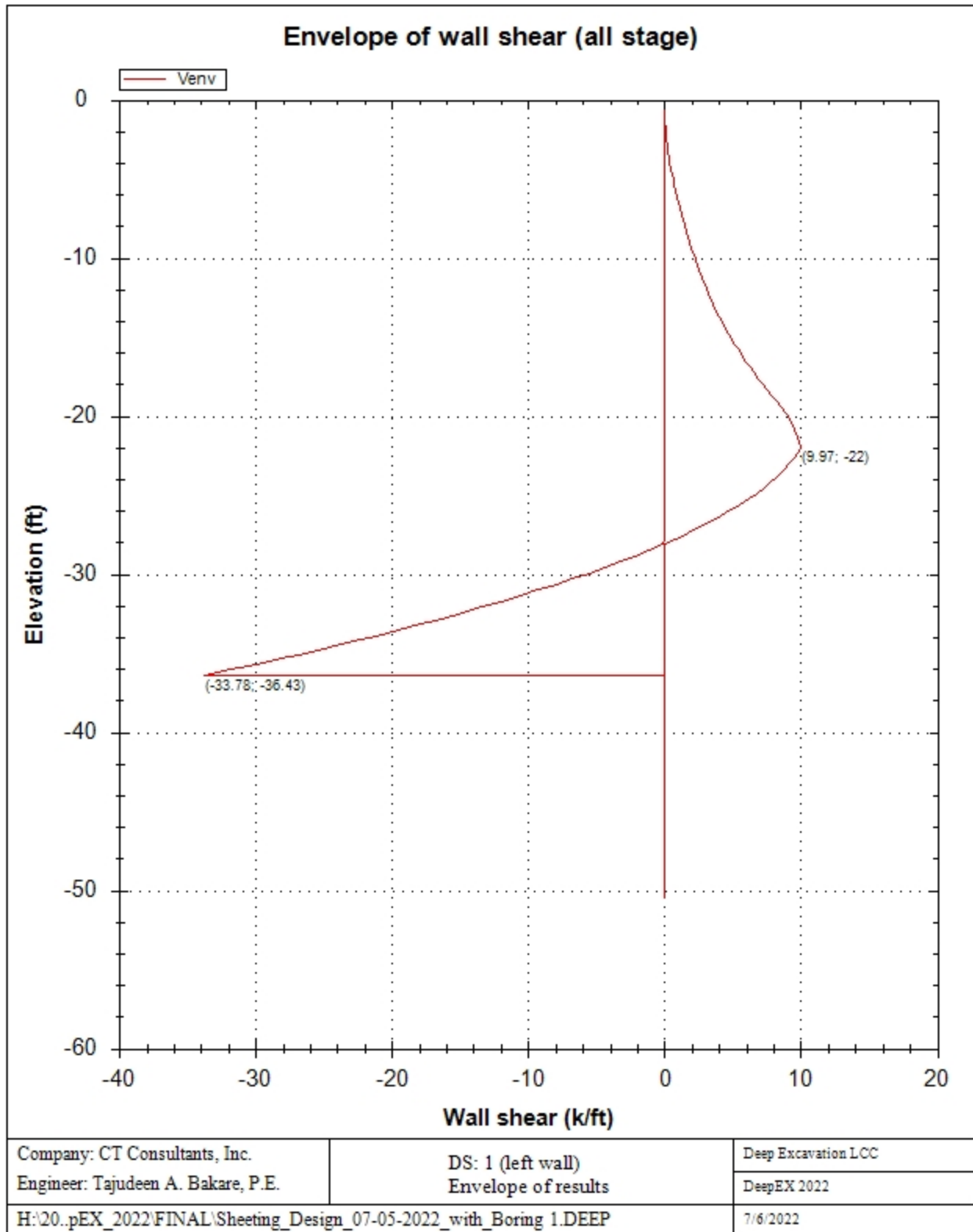
General assumptions for last stage: Stage 1

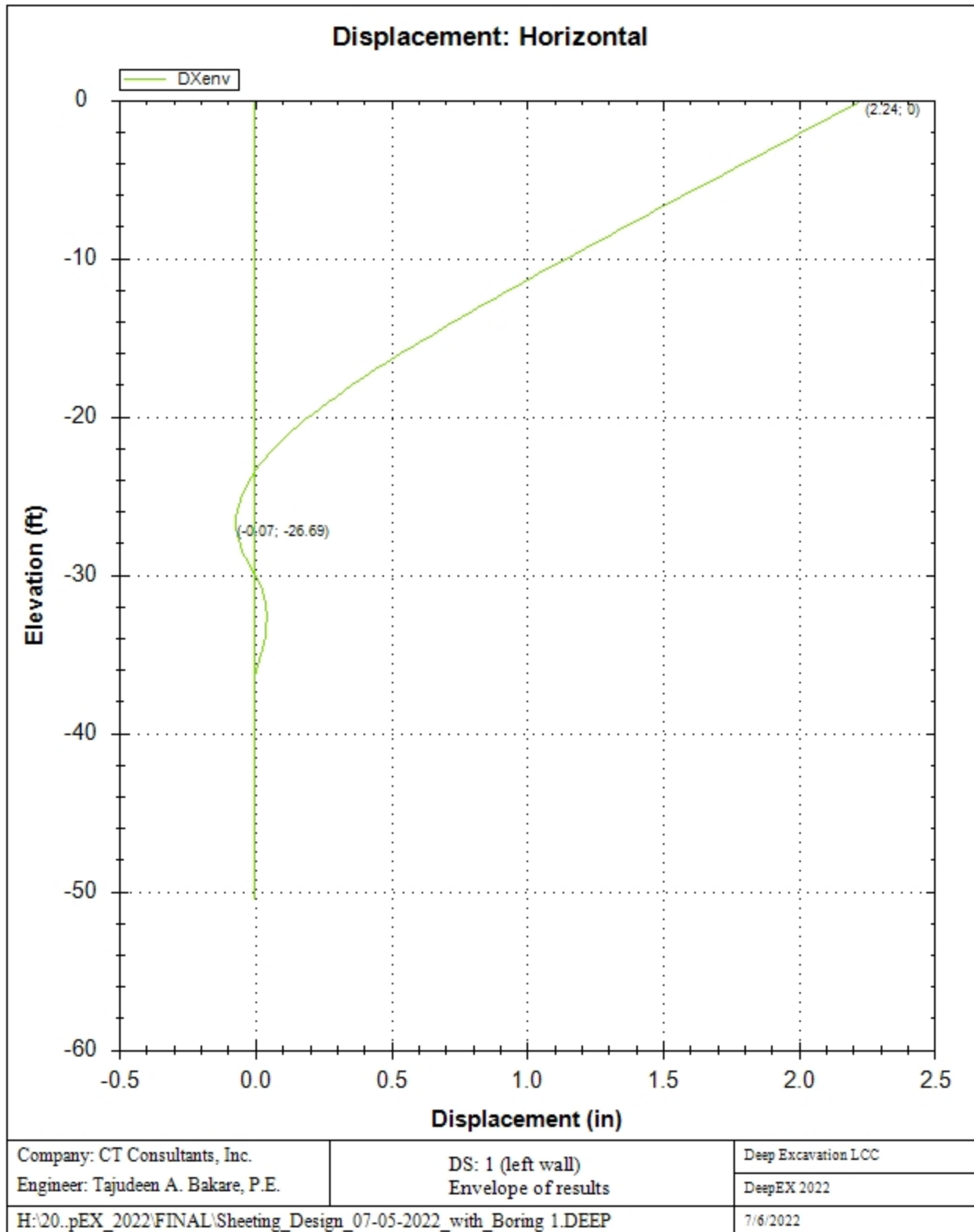
Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Caquot

### Envelope of results

A sequence of result diagrams for each excavation stage is reported







Extended vs Stage



	Calculation Result	Wall Displaceme (in)	Settlement (in)	Wall Moment (k-ft/ft)	Wall Moment (k-ft)
Stage 0	Calculated	0	N/A	0	0
Stage 1	Calculated	2.24	2.34	115.11	115.11

	Wall Shear (k/ft)	Wall Shear (k)	STR Combined Wall Ratio	STR Moment Wall Ratio	STR Shear Wall Ratio
Stage 0	0	0	0	0	0
Stage 1	33.78	33.78	0.501	0.501	0.207

Table notes:

STR Combined: Combined stress check, along eccentricity line considering axial load and moment (demand/capacity).

STR Moment : Moment stress check, assuming constant axial load on wall (demand/capacity).

STR Shear : Shear stress check (shear force demand/wall shear capacity).

	Max Support Reaction (k/ft)	Max Support Reaction (k)	Critical Support Check	STR Support Ratio	Support Geotech Capacity Ratio (pull out)
Stage 0	0	0	N/A	No supports	No supports
Stage 1	0	0	N/A	No supports	No supports

Table notes:

STR Support ratio: Critical structural stress check for support (force demand/structural capacity).

Support geotech capacity ratio: Critical geotechnical capacity stress check (demand/geotechnical capacity).

Critical support check: Critical demand/design capacity ratio (structural or geotechnical).

	FS Basal	Toe FS Passive	Toe FS Rotation	Toe FS Length	Zcut (nonlinear)	FS Mobilized Passive	FS True/Active
Stage 0	1000	21.622	20.213	140.278	N/A	N/A	N/A
Stage 1	N/A	N/A	2.535	1.807	N/A	N/A	N/A

	Hydraulic Heave FS	Qflow (ft3/hr)	FSslope
Stage 0	2.729	N/A	N/C
Stage 1	1.821	N/A	3.282

### Support Force/S vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

### Support Force vs Stage

### Support Force vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	20.213	21.622	20.213	140.278	N/A	N/A
0:Stage 0	1.807	N/A	2.535	1.807	N/A	N/A

Table notes:

FSbasal : Critical basal stability safety factor (relevant only when soft clays are present beneath the excavation).

Wall embedment safety factors from conventional analysis (limit-equilibrium):

FS1 Passive : Safety factor for wall embedment based on FS= Available horizontal thrust resistance/Driving hor. thrust.

FS2 Rotation: Safety factor for wall embedment based on FS= Available resisting moment/Driving moment.

FS3 Length : Safety factor for wall embedment based on FS= Available wall embedment/Required embedment for FS=1.0

Wall embedment safety factors from non-linear analysis:

FS4 Mobilized Passive : Safety factor= Available horizontal passive resistance/Mobilized passive thrust.

FS5 True/Active : Soil thrust on retained wall side/Minimum theoretically horizontal active force thrust.

Tables for stress checks follow: Support force/Design capacity

### Support Check vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

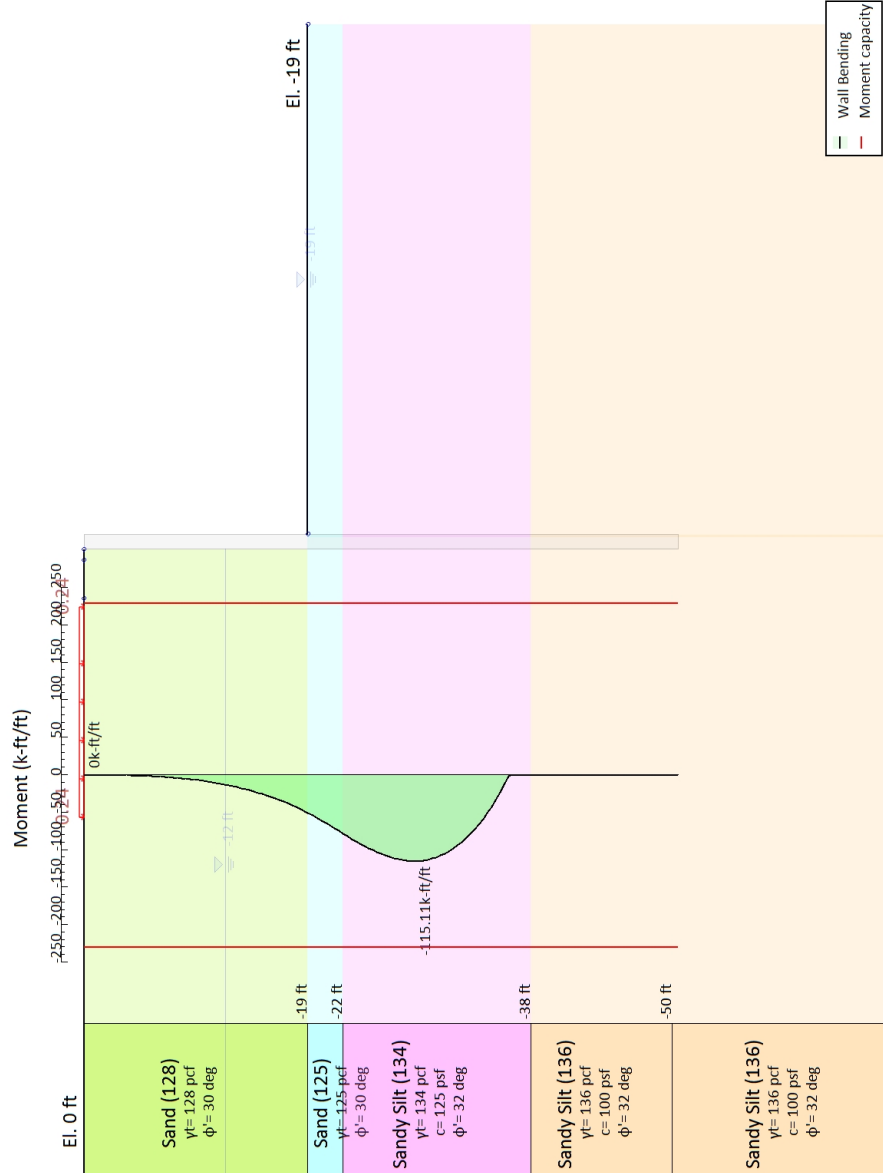
### Forces (Res. F, M/Drive F, M)

	FS1 Passive (FxResist/FxDrive)	FS2 Rotation (Mresist/Mdrive)	FS3 Length (Embedment/ToeFS=1)	FS4 Mobilized Passive (FxPassive/FxPas_Mobili)	FS5 Actual Drive / Theory Active	Fh EQ Soil	Fh EQ Water
Stage 0	594.114/27.477	10534.52/521.19	50.5/0.36	N/A	N/A	N/A	N/A
Stage 1	N/A	1930.96/453.04	31.5/17.43	N/A	N/A	N/A	N/A

### Reinforcement Requirements

	Parameter Description
Note:	Wall does not use steel reinforcement. Section does not apply.

0: AASHTO LRFD (2010): Service ((PARENT: Culvert at STA. 253+86 Shoring (Service Loads))



O LRFD 8 (2018), Case: Service I  
 FS(tanFR)= 1, FS c= 1, FS Su= 1  
 1, gDStab= 1, FSres= 1, FSdriveE= 1  
 s'A: Temp= 1, Perm= 1, EQ= 0  
 FS\_Drive= 1, FS\_Rev= 1, HYDgDStab = 1, HYDgStab = 1  
 fs'R: Temp= 1, Perm= 1

Company: CT Consultants, Inc.  
 Engineer: Tajudeen A. Bakare, P.E.

Quick summary

Deep Excavation LCC

DeepEX 2022

H:\20..pEX\_2022\FINAL\Sheeting\_Design\_07-05-2022\_with\_Boring 1.DEEP

7/6/2022

## Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	115.11/229.88	21.622	2.535	1.807	-36.43	3.282

## Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

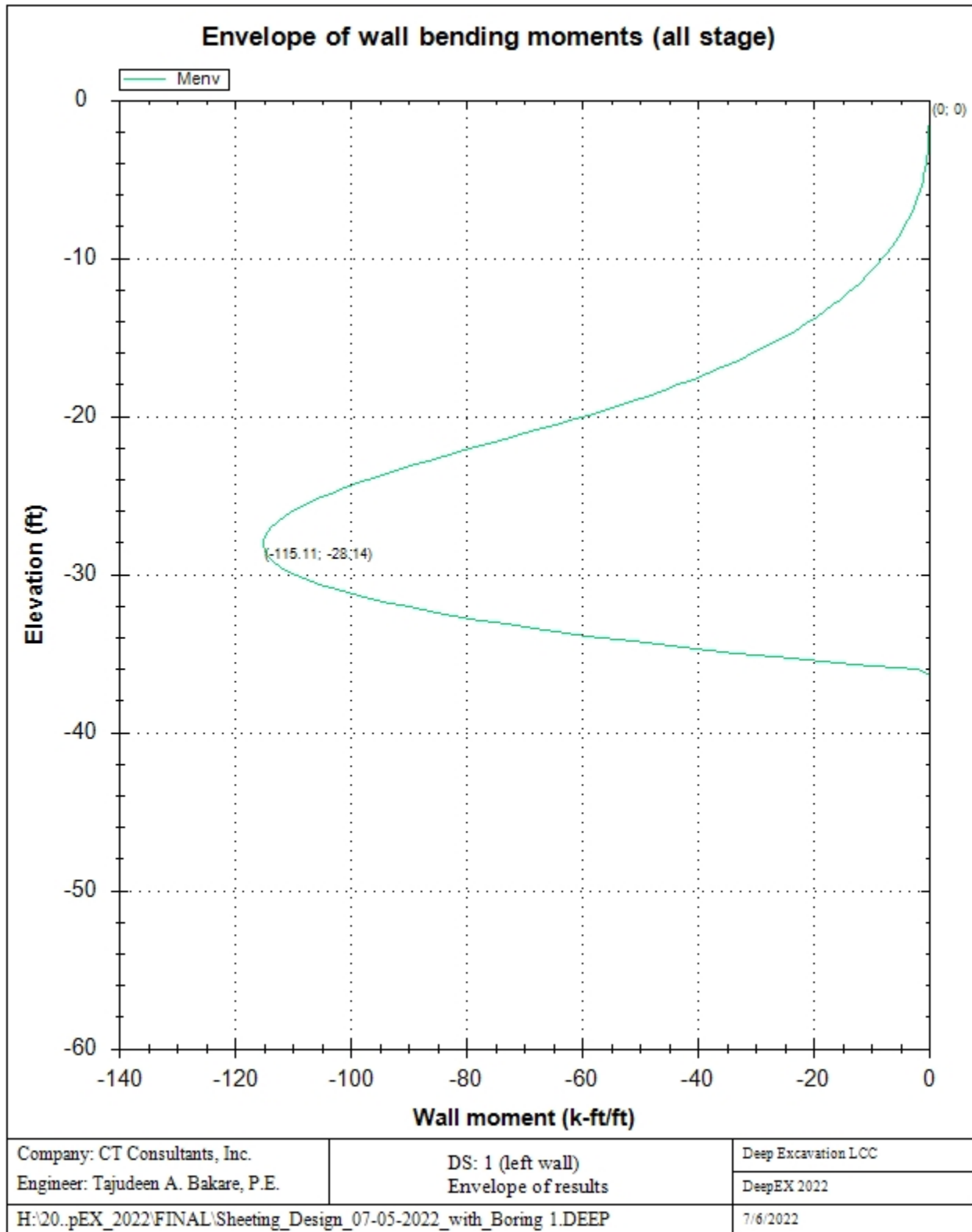
1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.849	12.4	3.282	0.373	12.449	3.282

## General assumptions for last stage: Stage 1

Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Coul

### Envelope of results

A sequence of result diagrams for each excavation stage is reported



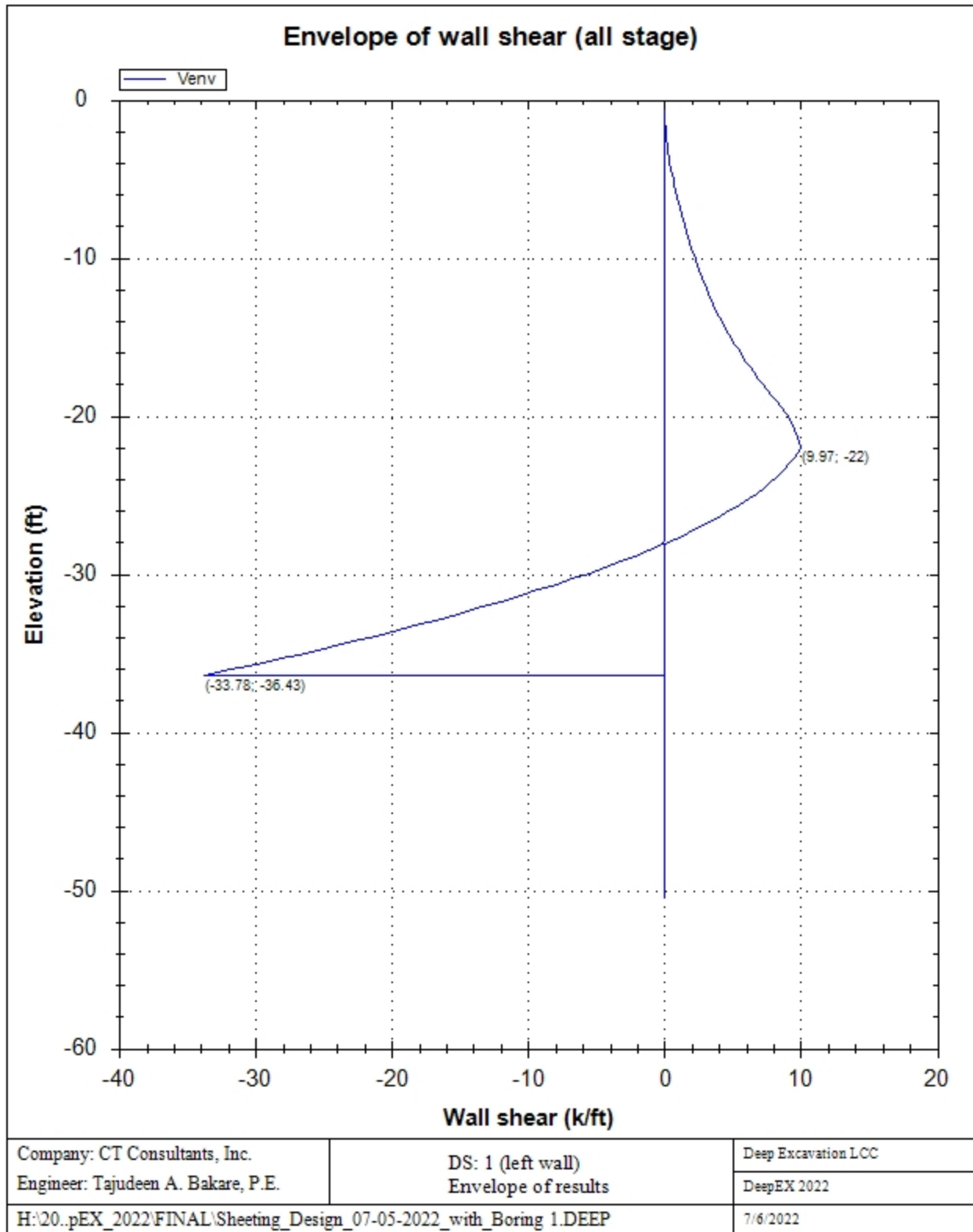
Company: CT Consultants, Inc.  
 Engineer: Tajudeen A. Bakare, P.E.

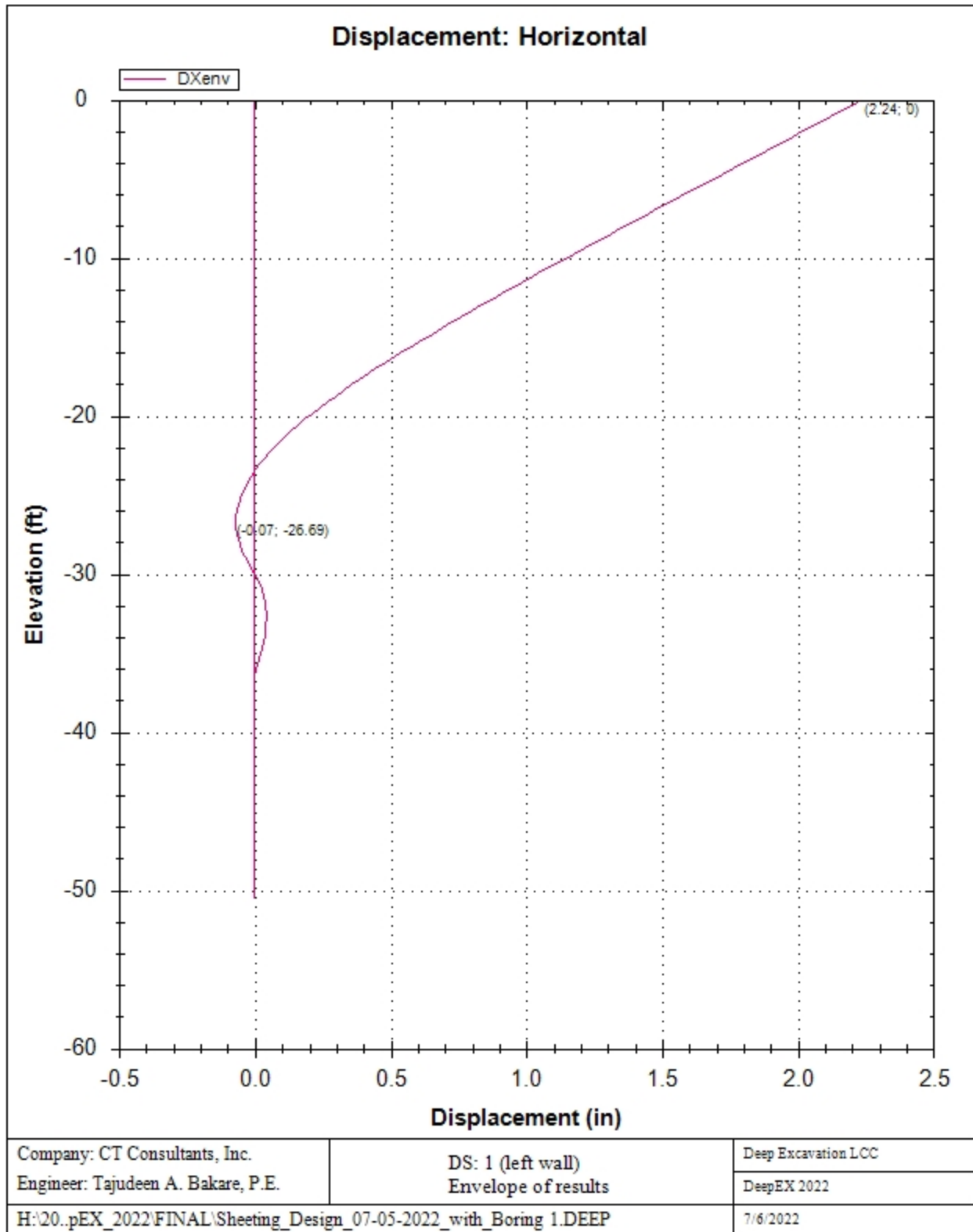
DS: 1 (left wall)  
 Envelope of results

Deep Excavation LCC  
 DeepEX 2022

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7/6/2022





**DESIGN APPROACHES AND COMBINATION FACTORS**

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

Ftan fr=mult factor for friction angle

F C'= safety factor on effective cohesion (Eurocode 7 methods)

F Su'= safety factof for undrained shear strength (Eurocode 7 methods)

F EQ= Load factor for seismic loads

F perm load= Load factor for permanent loads (dead load, etc)

F temp load= Load factor on live loads and other temporary loads

F perm supp= Reduction factor for resistance for pull out checking of permanent tiebacks

F temp supp= Reduction factor for resistance for pull out checking of temporary tiebacks

F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)

F earth stab= Safety factor for passive pressures, favorable (on excavation side)

F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable

F GWT stab (ground water)= Load factor for resisting water pressure, favorable

F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)

F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)

F UPL Dstab= Load factor for uplift check, unfavorable

F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan fr)	F (c')	F (Su)	F (EQ)	F(perm load)	F(temp load)	F(perm sup)	F(temp sup)	F Earth (Dstab)	F Earth (stab)	F GWT (Dstab)	F GWT (stab)	F HYD (Dstab)	F HYD (stab)	F UPL (Dstab)	F UPL (stab)
0	AASHTO LRFD	Service I	1	1	1	0	1	1	1	1	1	1	1	1	1	1	1	1
1	AASHTO LRFD	Service I	1	1	1	0	1	1	1	1	1	1	1	1	1	1	1	1

## DESIGN APPROACHES AND COMBINATION FACTORS

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

Ftan fr=mult factor for friction angle

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F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)

F earth stab= Safety factor for passive pressures, favorable (on excavation side)

F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable

F GWT stab (ground water)= Load factor for resisting water pressure, favorable

F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)

F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)

F UPL Dstab= Load factor for uplift check, unfavorable

F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan fr)	F (c')	F (Su)	F (EQ)	F(perm load)	F(temp load)	F(perm sup)	F(temp sup)	F Earth (Dstab)	F Earth (stab)	F GWT (Dstab)	F GWT (stab)	F HYD (Dstab)	F HYD (stab)	F UPL (Dstab)	F UPL (stab)
0	AASHTO LRFD	Service I	1	1	1	0	1	1	1	1	1	1	1	1	1	1	1	1
1	AASHTO LRFD	Service I	1	1	1	0	1	1	1	1	1	1	1	1	1	1	1	1

## SOIL DATA

Name	g tot (pcf)	g dry (pcf)	Frict (deg)	C' (psf)	Su (psf)	FRp (deg)	FRcv (deg)	Eload (ksf)	rEur (-)	kAp NL	kPp NL	kAcv NL	kPcv NL	Vary	Spring Model	Color
Sand (128)	128	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sand (125)	125	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sandy Silt (13)	134	134	32	125	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	
Sandy Silt (13)	136	136	32	100	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	



Name	Poisson	Min Ka	Min sh	ko.NC	nOCR	aH.EXP	aV.EXP	qSkin	qNails	kS.nails	PL
	v	(clays)	(clays)	-	-	(0 to 1)	(0 to 1)	(psi)	(psi)	(k/ft3)	(ksi)
Sand (128)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sand (125)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-

gtot = total soil specific weight

gdry = dry weight of the soil

Frict = friction angle

C' = effective cohesion

Su = Undrained shear strength (only for CLAY soils in undrained conditions, used as a cutoff strength in NL analysis)

Evc = Virgin compression elastic modulus

Eur = unloading/reloading elastic modulus

Kap = Peak active thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kpp = Peak passive thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kacv = Constant volume active thrust coeff (only for clays, initial value)

Kpcv = Constant volume passive thrust coeff (only for clays, initial value).

Spring models= spring model (LIN= constant E over the soil layer height , EXP=exponential , SIMC=simplified winkler)

LIN= Linear-Elastic-Perfectly Plastic,

EXP: Exponential, SUB: Modulus of Subgrade Reaction

SIMC= Simplified Clay mode

## **SOIL BORINGS**

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Top Elev= superior SOil level

Soil type= type of the soil (sand , clay , etc)

OCR= overconsolidation ratio

K0= at rest coefficient

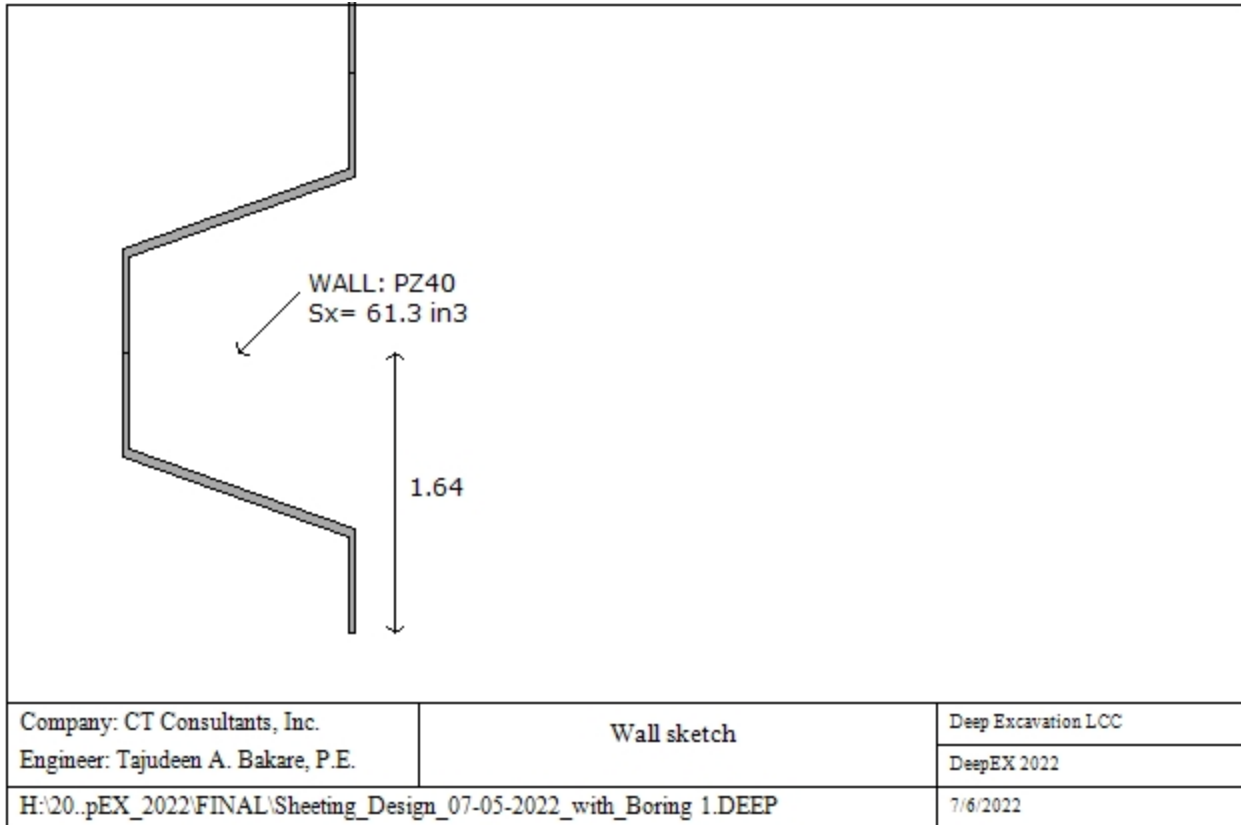
Name: Boring B-016-1-19, pos: (0, 0)

Top elev.	Soil type	OCR	Ko
0	Sand (128)	1	0.5
-19	Sand (125)	1	0.5
-22	Sandy Silt (134)	1	0.47
-38	Sandy Silt (136)	1	0.47
-50	Sandy Silt (136)	1	0.47

## **WALL DATA**

---

Wall section 0: Wall section 0



Wall type: Steel sheet piling  
 Top wall El: 0 ft Bottom wall El: -50.5 ft  
 Hor. wall spacing: 1 ft Wall thickness = 1.37 ft  
 Passive width below exc: 1 ft Active width below exc: 1 ft Swater= 1 ft  
 Steel members fy = 50 ksi Esteel = 29000 ksi  
 Wall friction: Constant value = 17 degrees  
 Steel wall capacities are calculated with ANSI/AISC 360-10  
 Concrete capacities are calculated with ACI 318-19  
 Note: With ultimate capacities you may have to use a structural safety factor.  
 Steel sheet pile properties

Table: Steel Sheet Pile Cross Sectional Properties

DES	Shape	W	A	h	t	b	s	Ixx	Sxx
		(plf)	(in <sup>2</sup> /ft)	(in)	(in)	(in)	(in)	(in <sup>4</sup> /ft)	(in <sup>3</sup> /ft)
PZ40	Z	65.6	11.75	16.4	0.5	19.69	0.605	503	61.3

GENERAL WALL DATA

Hor wall spacing= Wall horizontal spacing  
 Passive width below exc= spacing for passive thrust pressure for classic analysis  
 f'c=fck= cylindrical concrete resistance  
 fyk=fyk= steel rebar characteristic resistance  
 Econc= Concrete Elastic modulus  
 fctk= characteristic Concrete tension  
 Esteel= steel elastic modulus  
 TABULAR DATA (principal parameters)  
 1) Diaphragm wall (rectangular cross section)  
 N/A= data not available  
 Fy=fyk

$F'c=f_{ck}$

$D$ =wall thickness

$B$ =wall width

2)Steel sheet pile

$DES$ =shape (Z or U)

$W$ =width per unit of length

$A$ =area

$h$ =height

$t$ =horizontal part thickness

$b$ =width of the single sheet pile part

$s$ =inclined part thickness

$I_{xx}$ =strong axis inertia (per unit of length)

$S_{xx}$ =strong axis section modulus (per unit of length)

3)Secant piles wall, Tangent piles wall, soldier piles, soldier piles and timber lagging

$W$ =weight per unit of length

$A$ =area

$D$ =diameter

$t_w$ =web thickness

$t_p$ = pipe thickness

$b_f$ =flange width

$t_f$ = flange thickness

$k$ = flange thickness+stem base height

$I_{xx}$ = strong axis inertia modulus (per unit of length)

$S_{xx}$ = strong axis section modulus (per unit of length)

$r_x$ =radius of gyration about X axis

$r_y$ =radius of gyration about Y axis

$I_{yy}$ =weak axis inertia modulus (per unit of length)

$S_{yy}$ =weak axis section modulus (per unit of length)

$r_T$ =radius of gyration for torsion

$C_w$ = warping constant

## **GENERAL ANALYSIS CRITERIA**

### Summary of stage assumptions

Name	Analysis	Drive	ka-Mult	Htr T/B	Resist	Res	Contle
	Method	Press		(%)	Press	Mult	Method
Stage 0	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth
Stage 1	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth

Name	Support	Axial	Used	Min Toe	Toe	Toe
	Model	Incl	FSwall	FDtoe	FSrot	FSpas
Stage 0		N/A	1	20.213	20.213	21.622
Stage 1		N/A	1	1.807	2.535	N/A

Name=excavation stage name

Analysis method

springs = Elastoplastic spring analysis used

DR = Drained condition for CLAY model

U = Undrained condition for CLAY model for all the soils

Up = Undrained condition just for selected soil

Limit equilibrium analysis settings

Drive press:

Ka (Active pressure diagram), Ka-Trap = Trapezoid apparent diagram from active pressures x multiplier, FHWA= Federal Highway Administration apparent pressure diagrams.

Ko = At-rest lateral earth pressures.

Peck = Peck 1969 Apparent earth pressure diagrams.

2 Step rect = Two step rectangular apparent earth pressure diagram.

User def. = User defined apparent earth pressure diagram.

Ka+d (and so on) indicates that wall friction is applied

ka mult = multiplication factor for Ka when Ka-Trap is selected

Htr T/B (%) = trapezoidal pressure scheme, top and bottom triangular percentage of excavation depth H

Resit press = Kp (passive earth pressures)

Res Mult = Safety factor applied directly on resisting pressures (

COntle Method = cantilever analysis method for limit equilibrium analysis.

Support Model: Method for calculating support reactions in limit-equilibrium analysis.

Beam= support reactions beam analysis (uses Blum's method).

Trib= support reactions from tributary height calculations (Can be applied with apparent diagrams).

Axial Incl = Axial loads included for structural design

Used FS wall = Safety factor for axial+bending wall resistance to divide ultimate wall capacities.

Min FD Toe= embedded minimum safety factor (for limit equilibrium analysis)

Toe FS rot= rotation safety factor (classic for limit equilibrium analysis)

Toe FSpas= driving/resisting pressure safety factor (for limit equilibrium analysis)

## **EXCAVATION STAGES SKETCHES**

A sequence of figures for each excavation stage is reported

### **Toe stability**

#### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	20.213	21.622	20.213	140.278	N/A	N/A
Stage 1	1.807	N/A	2.535	1.807	N/A	N/A

Legend: Wall embedment safety factors (toe)

Min Toe FS= Minimum wall embedment safety factor (from all analysis methods)

Limit-equilibrium analysis methods: The following safety factors may not be applicable for all stages.

FS1 Passive: Horizontal force safety factor, FS1= Resisting/Driving force

FS2 Rotation: Rotational safety factor about lowest support, FS2= Resisting moment/Driving moment

FS3 Length (from FS1, FS2): Program determines maximum required wall embedment for safety factor of 1 for methods FS1 and FS2 (say length LFS1). Then FS length= Provided wall embedment/LFS1.

Non-linear elastoplastic analysis safety factors:

FS4 Mobilized Passive: Safety factor on mobilized passive resistance, FS4= Available passive soil resistance/Mobilized passive soil force on excavation side.

FS5 Active Drive Thrust/Theory Active: Ratio of soil thrust on retained side/ Active condition theoretical minimum thrust. This factor is not as critical, and indicates how close to active conditions the model is.

General recommendations on wall embedment (excluding FS5):

When then excavation is designed with allowable standards, engineers generally use minimum safety factors from 1.2 to 1.5 depending on the level of confidence. A minimum safety factor of 1.2 is generally applied on FS3.

With ultimate limit state designs (such as Eurocode 7, and LRFD) the required safety factor must generally be greater than 1.0. In non-linear solutions it might be impossible to achieve exactly 1 on FS4 as this would likely trigger overall failure.

## **Result diagrams (for walls)**

A sequence of result diagrams for each excavation stage is reported

## **WALL RESULTS TABLE**

LEGEND

Wall node=number of the node (0 at top)

EL= Node elevation

Sht L=Total horizontal soil pressure (on the left side of the wall)

Sht R=Total horizontal soil pressure (on the right side of the wall)

Shs L=Effective horizontal soil pressure (on the left side of the wall)

Shs R=Effective horizontal soil pressure (on the right side of the wall)

q=pressure given by the surcharge

U L= Water pressure (on the left side of the wall)

U R= Water pressure (on the right side of the wall)

M=bending moment (per unit length)

V=shear (per unit length)

dx=wall deflection

McapL=Ultimate bending moment (on the left side of the wall)

McapR=Ultimate bending moment (on the right side of the wall)

VcapL=Ultimate resistance shear (on the left side of the wall)

VcapR=Ultimate resistance shear (on the right side of the wall)

## **EXCAVATION STAGES AND SLOPE STABILITY**

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Reports a sequence of figures for each stage with slope stability results.

## **SLOPE STABILITY ANALYSIS: SLICE RESULTS ALL STAGES**

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Slope stability analysis design section: 0: AASHTO LRFD (2010): Service I

### LEGEND

x1 = Left x coordinate

ZsL= Left slice bottom elevation

ZtL= Left top elevation

x2 = Right x coordinate

ZsR= Right slice bottom elevation

ZtR= Right top elevation

DL = Slice base width

an = Base angle

Fr = Average friction angle at base

c = Average cohesion at base (may include undrained clay strengths)

Wn = Total slice weight

ubL= Water pressure at left bottom point

ubR= Water pressure at right bottom point

tBase= Base shear resistance

Nr = Effective normal reaction at bottom of slice

EiL= Lateral interslice force on left face

EiR= Lateral interslice force on right face

TL = Vertical interslice shear on left vertical face

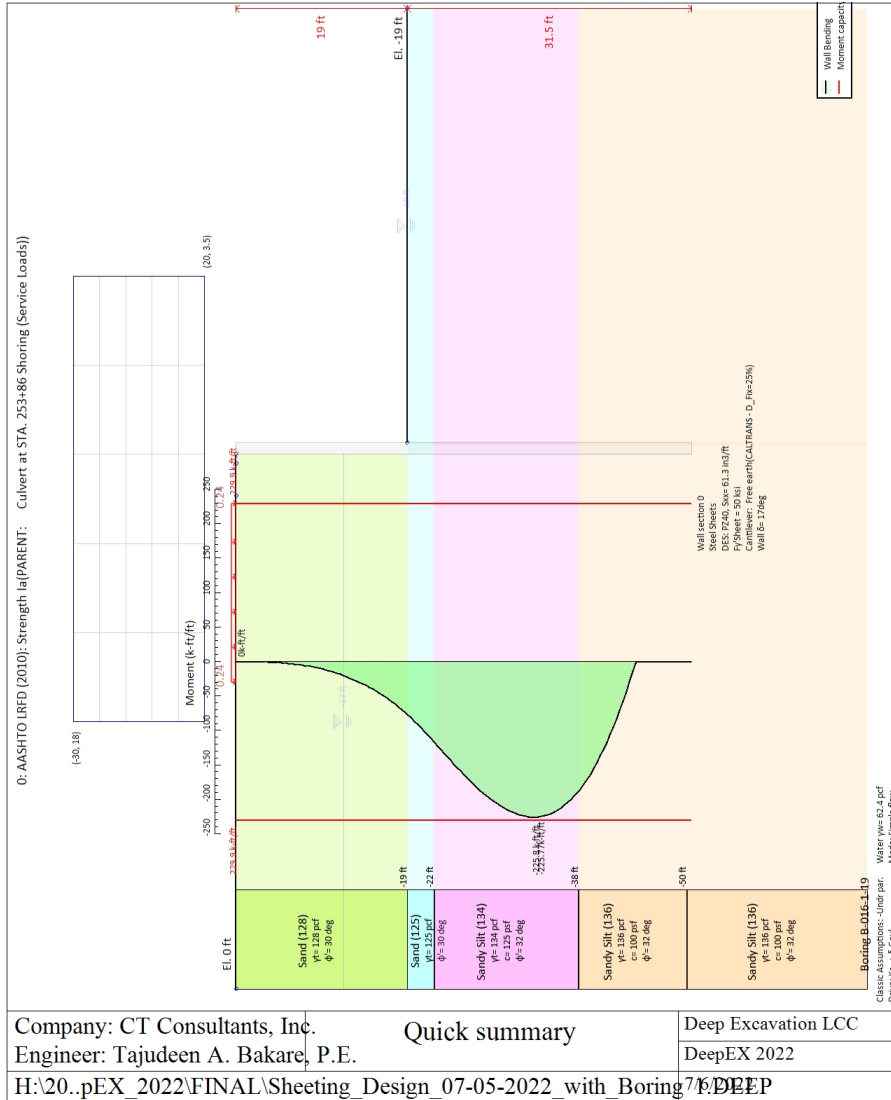
TR = Vertical interslice shear on right vertical face

UbF= Normal water force at slice base

***Project: ODOT PID No. 108665; LAK-20-19.59 - WEST  
Results for Design Section 2: 0: AASHTO LRFD (2010):  
Strength Ia***



## ANALYSIS AND CHECKING SUMMARY



Company: CT Consultants, Inc. Quick summary Deep Excavation LCC  
 Engineer: Tajudeen A. Bakare, P.E. DeepEX 2022  
 H:\20.pEX\_2022\FINAL\Sheeting\_Design\_07-05-2022\_with Boring 7/1/2022

### Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	225.77/229.88	10.838	1.362	1.242	-44.37	3.243

### Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

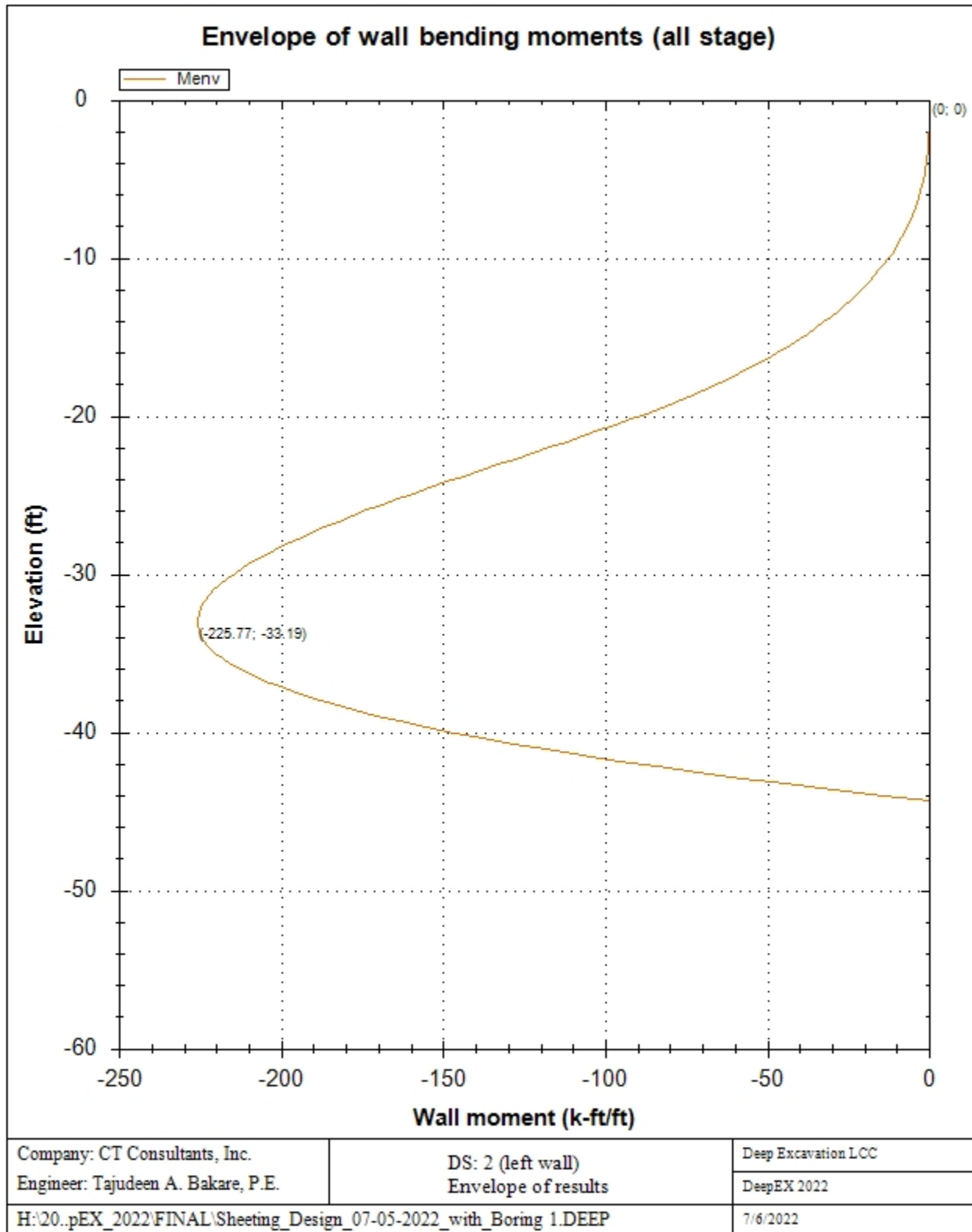
1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.867	12.4	3.243	0.38	12.449	3.243

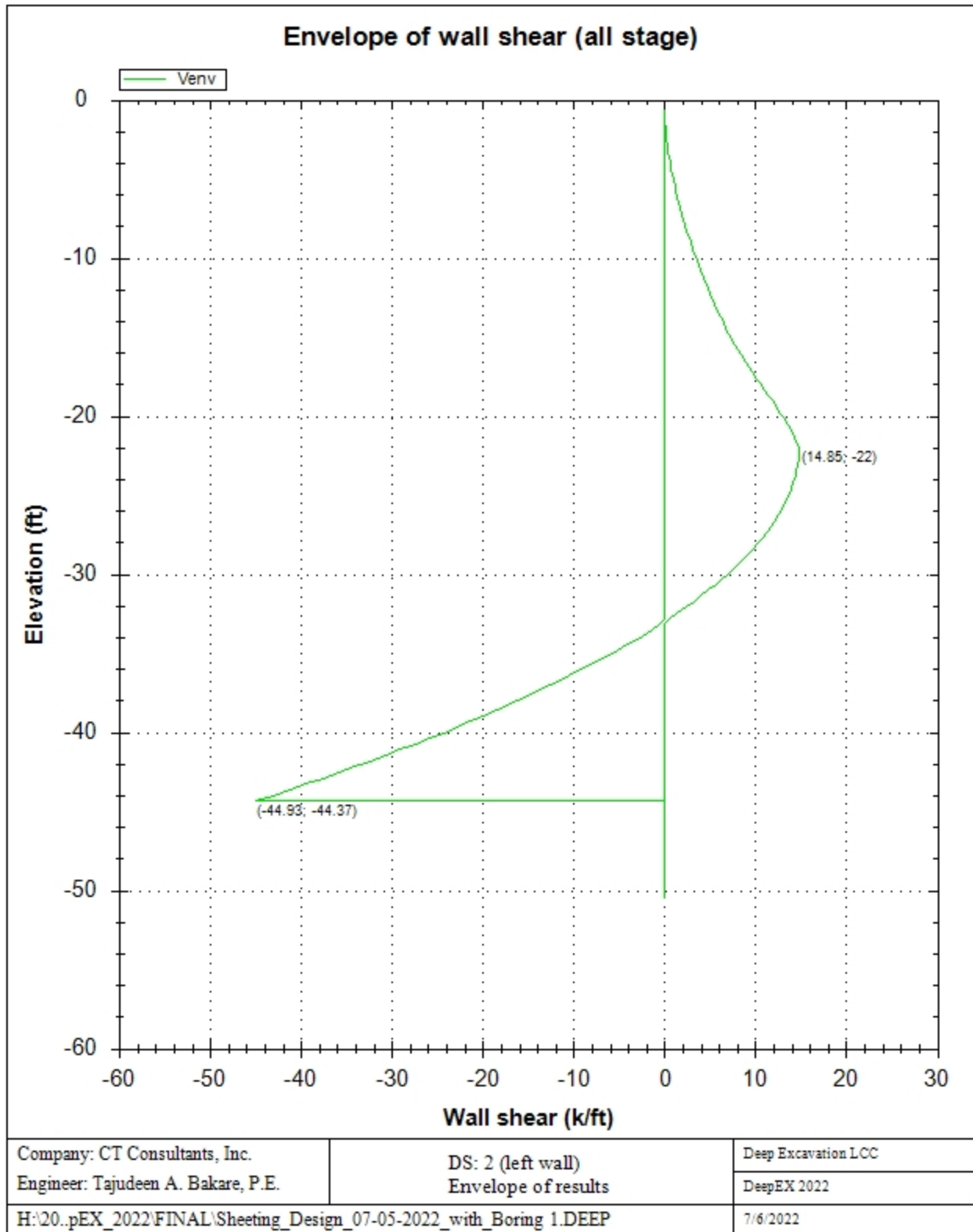
General assumptions for last stage: Stage 1

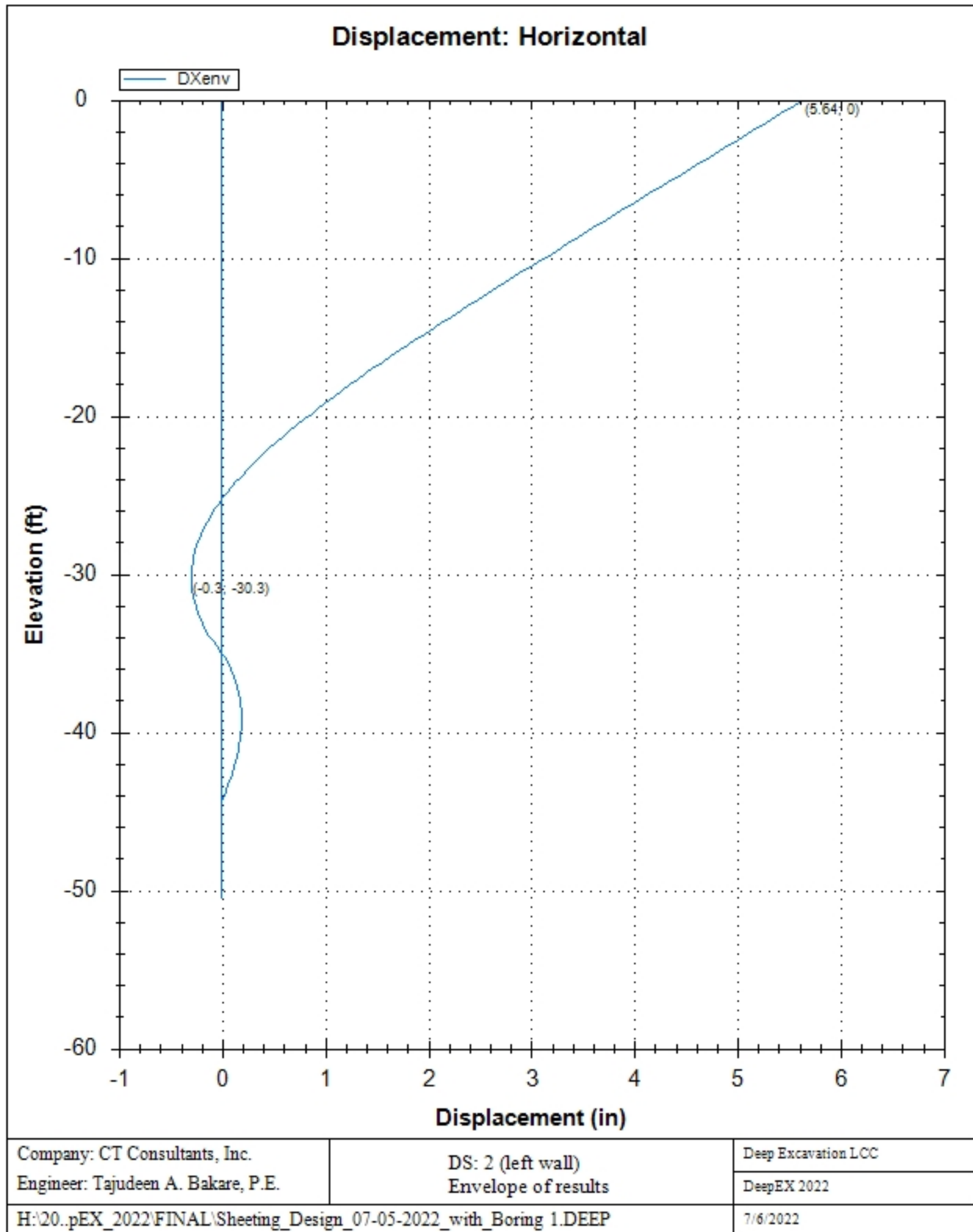
Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Caquot

### Envelope of results

A sequence of result diagrams for each excavation stage is reported







Extended vs Stage

	Calculation Result	Wall Displaceme (in)	Settlement (in)	Wall Moment (k-ft/ft)	Wall Moment (k-ft)
Stage 0	Calculated	0	N/A	0	0
Stage 1	Calculated	5.64	2.39	225.77	225.77

	Wall Shear (k/ft)	Wall Shear (k)	STR Combined Wall Ratio	STR Moment Wall Ratio	STR Shear Wall Ratio
Stage 0	0	0	0	0	0
Stage 1	44.93	44.93	0.982	0.982	0.275

Table notes:

STR Combined: Combined stress check, along eccentricity line considering axial load and moment (demand/capacity).

STR Moment : Moment stress check, assuming constant axial load on wall (demand/capacity).

STR Shear : Shear stress check (shear force demand/wall shear capacity).

	Max Support Reaction (k/ft)	Max Support Reaction (k)	Critical Support Check	STR Support Ratio	Support Geotech Capacity Ratio (pull out)
Stage 0	0	0	N/A	No supports	No supports
Stage 1	0	0	N/A	No supports	No supports

Table notes:

STR Support ratio: Critical structural stress check for support (force demand/structural capacity).

Support geotech capacity ratio: Critical geotechnical capacity stress check (demand/geotechnical capacity).

Critical support check: Critical demand/design capacity ratio (structural or geotechnical).

	FS Basal	Toe FS Passive	Toe FS Rotation	Toe FS Length	Zcut (nonlinear)	FS Mobilized Passive	FS True/Active
Stage 0	1000	10.838	10.132	140.278	N/A	N/A	N/A
Stage 1	N/A	N/A	1.362	1.242	N/A	N/A	N/A

	Hydraulic Heave FS	Qflow (ft3/hr)	FSslope
Stage 0	2.729	N/A	N/C
Stage 1	1.821	N/A	3.243

### Support Force/S vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

### Support Force vs Stage

### Support Force vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	10.132	10.838	10.132	140.278	N/A	N/A
0:Stage 0	1.242	N/A	1.362	1.242	N/A	N/A

Table notes:

FSbasal : Critical basal stability safety factor (relevant only when soft clays are present beneath the excavation).

Wall embedment safety factors from conventional analysis (limit-equilibrium):

FS1 Passive : Safety factor for wall embedment based on FS= Available horizontal thrust resistance/Driving hor. thrust.

FS2 Rotation: Safety factor for wall embedment based on FS= Available resisting moment/Driving moment.

FS3 Length : Safety factor for wall embedment based on FS= Available wall embedment/Required embedment for FS=1.0

Wall embedment safety factors from non-linear analysis:

FS4 Mobilized Passive : Safety factor= Available horizontal passive resistance/Mobilized passive thrust.

FS5 True/Active : Soil thrust on retained wall side/Minimum theoretically horizontal active force thrust.

Tables for stress checks follow: Support force/Design capacity

### Support Check vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

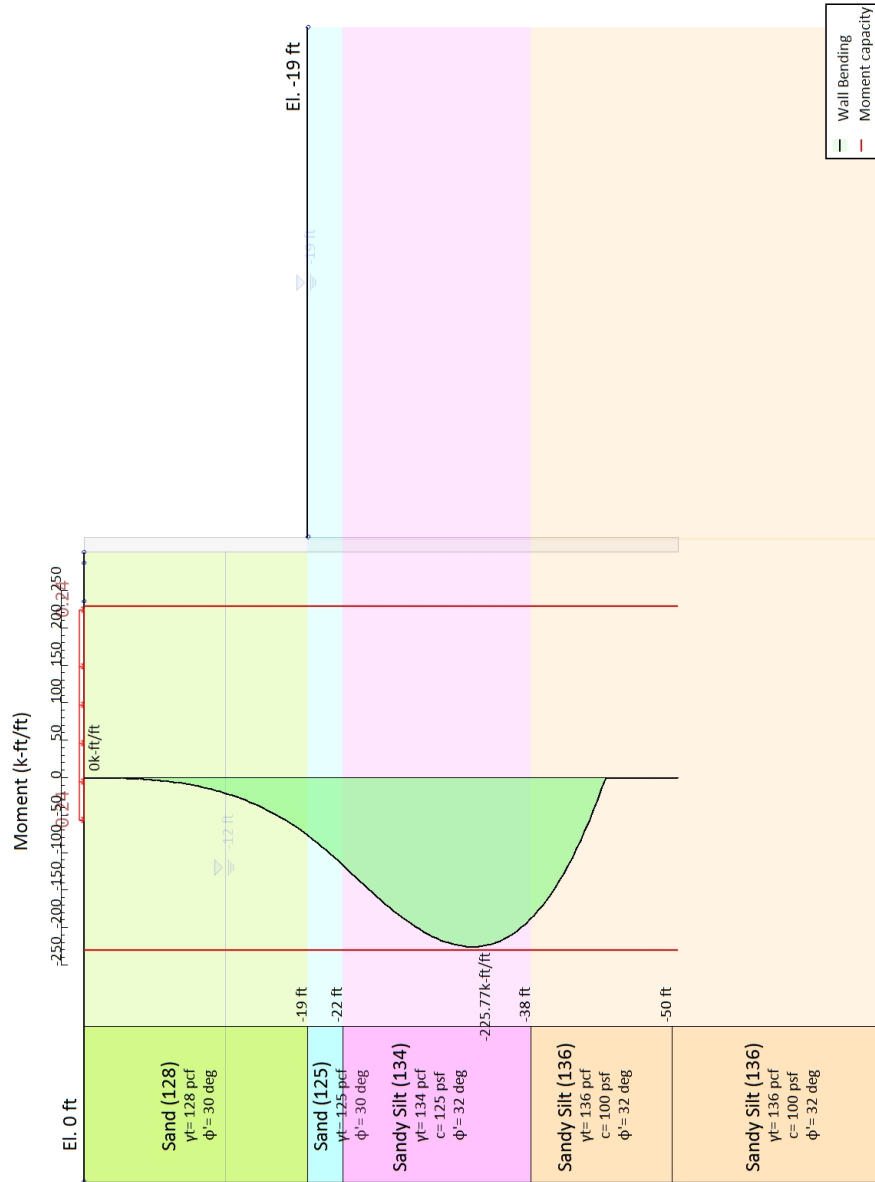
### Forces (Res. F, M/Drive F, M)

	FS1 Passive (FxResist/FxDrive)	FS2 Rotation (Mresist/Mdrive)	FS3 Length (Embedment/ToeFS=1)	FS4 Mobilized Passive (FxPassive/FxPas_Mobili)	FS5 Actual Drive / Theory Active	Fh EQ Soil	Fh EQ Water
Stage 0	446.702/41.215	7920.69/781.78	50.5/0.36	N/A	N/A	N/A	N/A
Stage 1	N/A	1451.85/616.83	31.5/25.37	N/A	N/A	N/A	N/A

### Reinforcement Requirements

	Parameter Description
Note:	Wall does not use steel reinforcement. Section does not apply.

O: AASHTO LRFD (2010): Strength Ia(PARENT): Culvert at STA. 253+86 Shoring (Service Loads)



O LRFD 8 (2018), Case: Strength Ia  
 FS(tanFR)= 1, FS c'= 1, FS Su= 1  
 1, gDStab= 1, FSres= 1.33, FSdriveE= 1.35  
 s'A: Temp= 1.75, Perm= 1, EQ= 0  
 FS\_Drive= 1, FS\_Res= 1, HYDgDStab = 1, HYDgStab = 1  
 fs'R: Temp= 1, Perm= 1.11

Company: CT Consultants, Inc.

Engineer: Tajudeen A. Bakare, P.E.

H:\20..pEX\_2022\FINAL\Sheeting\_Design\_07-05-2022\_with\_Boring 1.DEEP

Quick summary

Deep Excavation LCC

DeepEX 2022

7/6/2022



## Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	225.77/229.88	10.838	1.362	1.242	-44.37	3.243

## Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

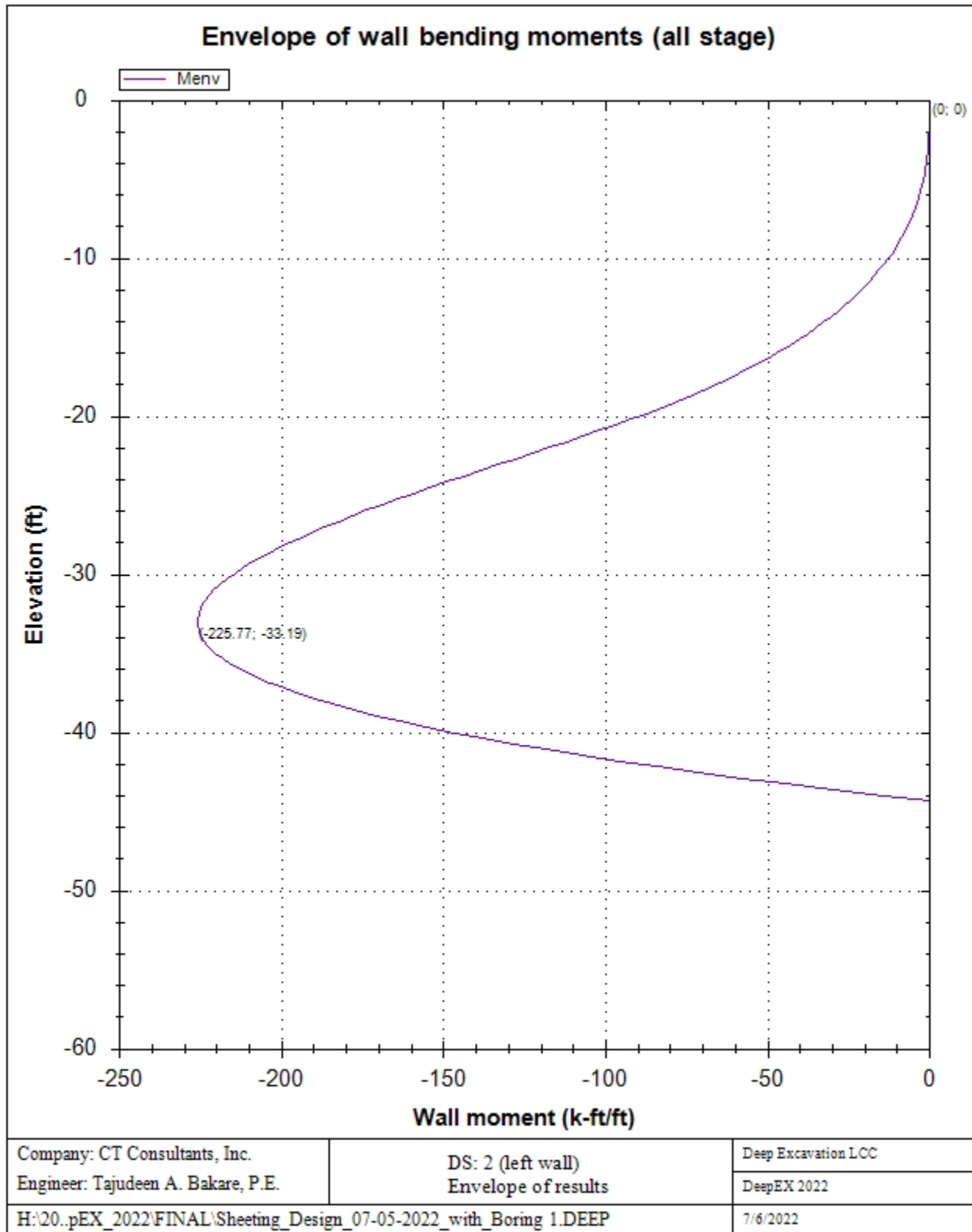
1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.867	12.4	3.243	0.38	12.449	3.243

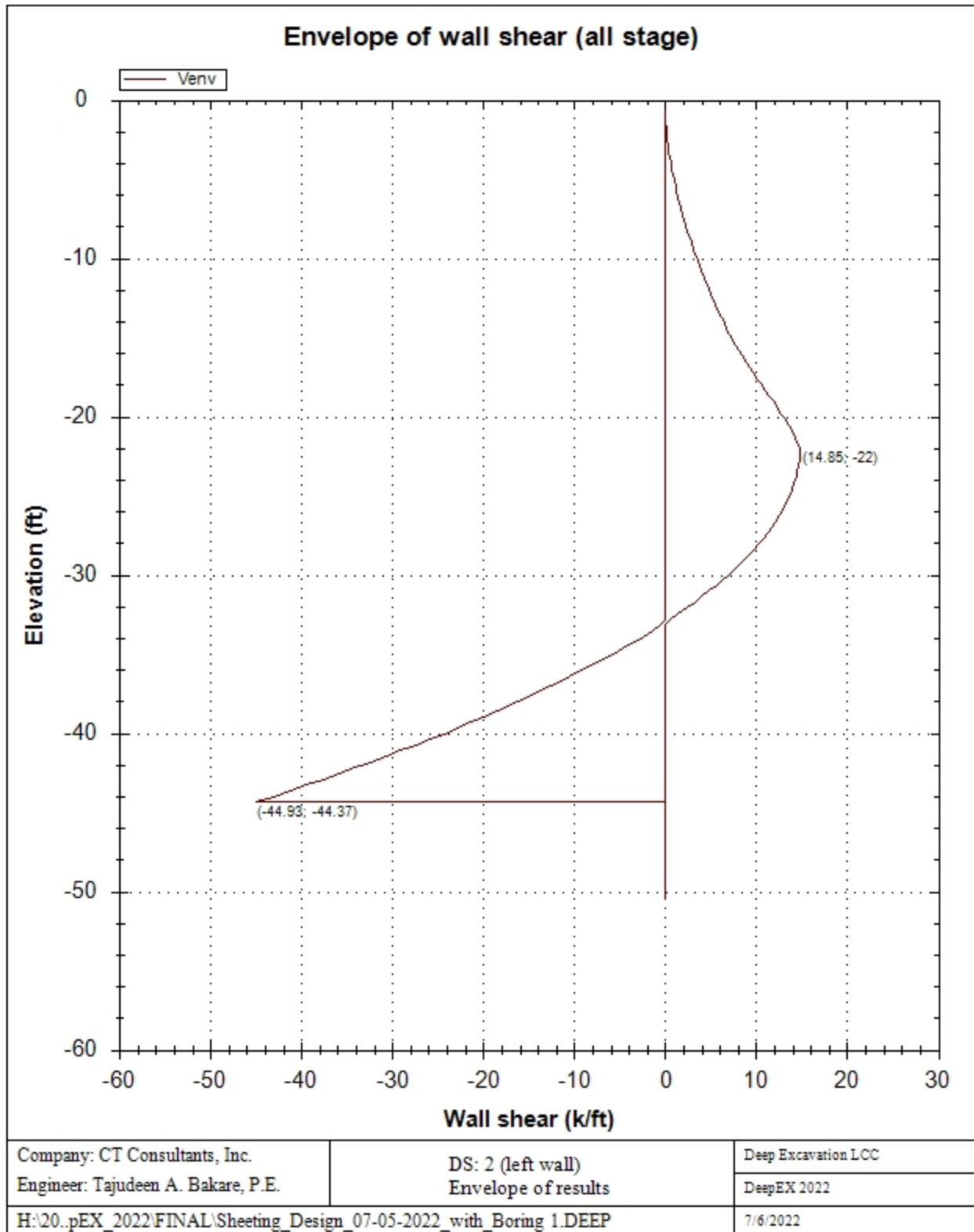
## General assumptions for last stage: Stage 1

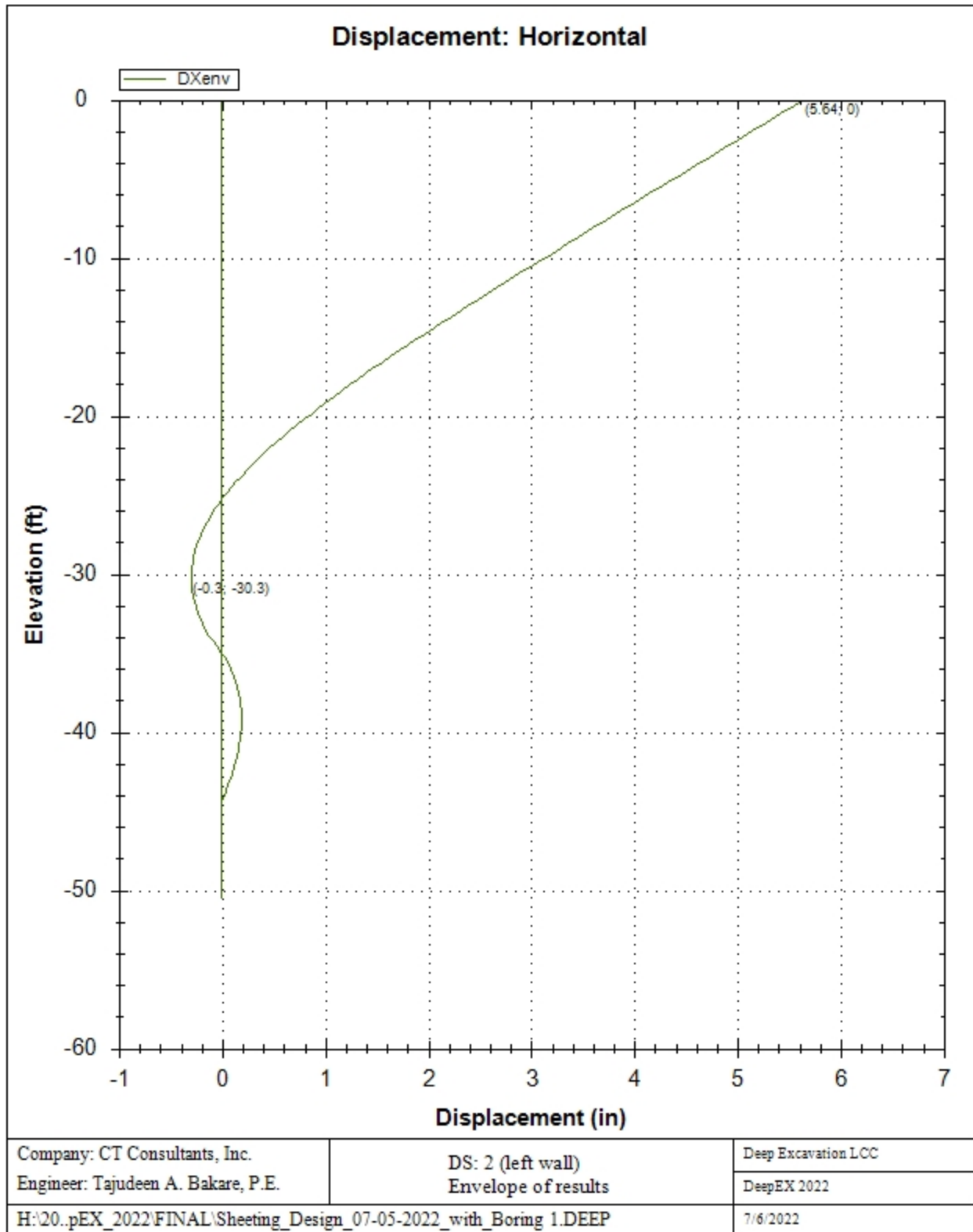
Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Coul

### Envelope of results

A sequence of result diagrams for each excavation stage is reported







**DESIGN APPROACHES AND COMBINATION FACTORS**

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

Ftan fr=mult factor for friction angle

F C'= safety factor on effective cohesion (Eurocode 7 methods)

F Su'= safety factof for undrained shear strength (Eurocode 7 methods)

F EQ= Load factor for seismic loads

F perm load= Load factor for permanent loads (dead load, etc)

F temp load= Load factor on live loads and other temporary loads

F perm supp= Reduction factor for resistance for pull out checking of permanent tiebacks

F temp supp= Reduction factor for resistance for pull out checking of temporary tiebacks

F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)

F earth stab= Safety factor for passive pressures, favorable (on excavation side)

F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable

F GWT stab (ground water)= Load factor for resisting water pressure, favorable

F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)

F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)

F UPL Dstab= Load factor for uplift check, unfavorable

F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan fr)	F (c')	F (Su)	F (EQ)	F(perm load)	F(temp load)	F(perm sup)	F(temp sup)	F Earth (Dstab)	F Earth (stab)	F GWT (Dstab)	F GWT (stab)	F HYD (Dstab)	F HYD (stab)	F UPL (Dstab)	F UPL (stab)
0	AASHTO LRFD	Strength Ia	1	1	1	0	1	1.75	1.11	1	1.35	1.33	1	1	1	1	1	1
1	AASHTO LRFD	Strength Ia	1	1	1	0	1	1.75	1.11	1	1.35	1.33	1	1	1	1	1	1

## DESIGN APPROACHES AND COMBINATION FACTORS

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

Ftan fr=mult factor for friction angle

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F GWT stab (ground water)= Load factor for resisting water pressure, favorable

F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)

F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)

F UPL Dstab= Load factor for uplift check, unfavorable

F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan fr)	F (c')	F (Su)	F (EQ)	F(perm load)	F(temp load)	F(perm sup)	F(temp sup)	F Earth (Dstab)	F Earth (stab)	F GWT (Dstab)	F GWT (stab)	F HYD (Dstab)	F HYD (stab)	F UPL (Dstab)	F UPL (stab)
0	AASHTO LRFD	Strength Ia	1	1	1	0	1	1.75	1.11	1	1.35	1.33	1	1	1	1	1	1
1	AASHTO LRFD	Strength Ia	1	1	1	0	1	1.75	1.11	1	1.35	1.33	1	1	1	1	1	1

## SOIL DATA

Name	g tot (pcf)	g dry (pcf)	Frict (deg)	C' (psf)	Su (psf)	FRp (deg)	FRcv (deg)	Eload (ksf)	rEur (-)	kAp NL	kPp NL	kAcv NL	kPcv NL	Vary	Spring Model	Color
Sand (128)	128	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sand (125)	125	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sandy Silt (13)	134	134	32	125	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	
Sandy Silt (13)	136	136	32	100	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	

Name	Poisson	Min Ka	Min sh	ko.NC	nOCR	aH.EXP	aV.EXP	qSkin	qNails	kS.nails	PL
	v	(clays)	(clays)	-	-	(0 to 1)	(0 to 1)	(psi)	(psi)	(k/ft3)	(ksi)
Sand (128)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sand (125)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-

gtot = total soil specific weight

gdry = dry weight of the soil

Frict = friction angle

C' = effective cohesion

Su = Undrained shear strength (only for CLAY soils in undrained conditions, used as a cutoff strength in NL analysis)

Evc = Virgin compression elastic modulus

Eur = unloading/reloading elastic modulus

Kap = Peak active thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kpp = Peak passive thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kacv = Constant volume active thrust coeff (only for clays, initial value)

Kpcv = Constant volume passive thrust coeff (only for clays, initial value).

Spring models= spring model (LIN= constant E over the soil layer height , EXP=exponential , SIMC=simplified winkler)

LIN= Linear-Elastic-Perfectly Plastic,

EXP: Exponential, SUB: Modulus of Subgrade Reaction

SIMC= Simplified Clay mode

## **SOIL BORINGS**

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Top Elev= superior SOil level

Soil type= type of the soil (sand , clay , etc)

OCR= overconsolidation ratio

K0= at rest coefficient

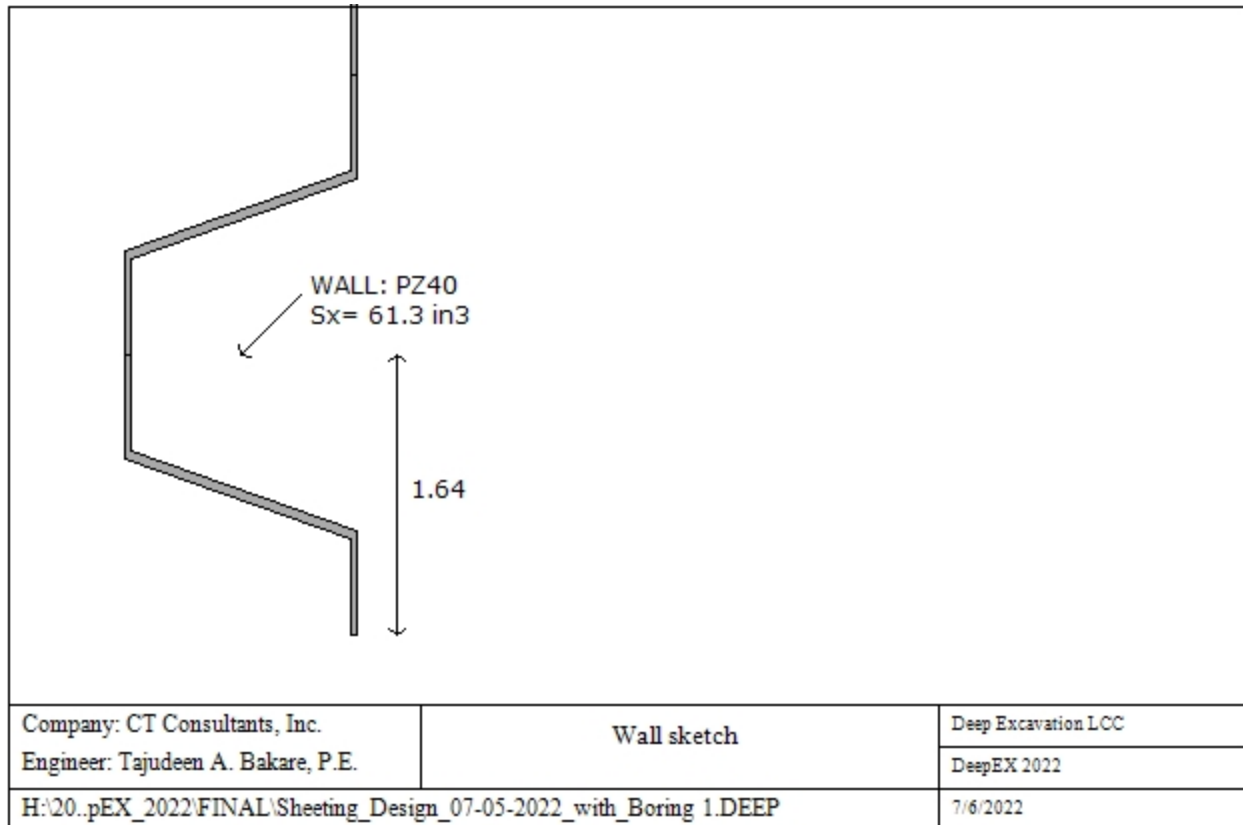
Name: Boring B-016-1-19, pos: (0, 0)

Top elev.	Soil type	OCR	Ko
0	Sand (128)	1	0.5
-19	Sand (125)	1	0.5
-22	Sandy Silt (134)	1	0.47
-38	Sandy Silt (136)	1	0.47
-50	Sandy Silt (136)	1	0.47

## **WALL DATA**

---

Wall section 0: Wall section 0



Wall type: Steel sheet piling

Top wall El: 0 ft Bottom wall El: -50.5 ft

Hor. wall spacing: 1 ft Wall thickness = 1.37 ft

Passive width below exc: 1 ft Active width below exc: 1 ft Swater= 1 ft

Steel members  $f_y = 50$  ksi Esteel = 29000 ksi

Wall friction: Constant value = 17 degrees

Steel wall capacities are calculated with ANSI/AISC 360-10

Concrete capacities are calculated with ACI 318-19

Note: With ultimate capacities you may have to use a structural safety factor.

Steel sheet pile properties

Table: Steel Sheet Pile Cross Sectional Properties

DES	Shape	W	A	h	t	b	s	Ixx	Sxx
		(plf)	(in <sup>2</sup> /ft)	(in)	(in)	(in)	(in)	(in <sup>4</sup> /ft)	(in <sup>3</sup> /ft)
PZ40	Z	65.6	11.75	16.4	0.5	19.69	0.605	503	61.3

#### GENERAL WALL DATA

Hor wall spacing= Wall horizontal spacing

Passive width below exc= spacing for passive thrust pressure for classic analysis

$f'_c=f_{ck}$ = cylindrical concrete resistance

$f_y=f_{yk}$ = steel rebar characteristic resistance

E<sub>con</sub>= Concrete Elastic modulus

$f_{ctk}$ = characteristic Concrete tension

E<sub>steel</sub>= steel elastic modulus

TABULAR DATA (principal parameters)

1) Diaphragm wall (rectangular cross section)

N/A= data not available

$F_y=f_{yk}$

$F'c=fck$

$D$ =wall thickness

$B$ =wall width

2)Steel sheet pile

$DES$ =shape (Z or U)

$W$ =width per unit of length

$A$ =area

$h$ =height

$t$ =horizontal part thickness

$b$ =width of the single sheet pile part

$s$ =inclined part thickness

$I_{xx}$ =strong axis inertia (per unit of length)

$S_{xx}$ =strong axis section modulus (per unit of length)

3)Secant piles wall, Tangent piles wall, soldier piles, soldier piles and timber lagging

$W$ =weight per unit of length

$A$ =area

$D$ =diameter

$t_w$ =web thickness

$t_p$ = pipe thickness

$b_f$ =flange width

$t_f$ = flange thickness

$k$ = flange thickness+stem base height

$I_{xx}$ = strong axis inertia modulus (per unit of length)

$S_{xx}$ = strong axis section modulus (per unit of length)

$r_x$ =radius of gyration about X axis

$r_y$ =radius of gyration about Y axis

$I_{yy}$ =weak axis inertia modulus (per unit of length)

$S_{yy}$ =weak axis section modulus (per unit of length)

$r_T$ =radius of gyration for torsion

$C_w$ = warping constant



## GENERAL ANALYSIS CRITERIA

### Summary of stage assumptions

Name	Analysis	Drive	ka-Mult	Htr T/B	Resist	Res	Contle
	Method	Press		(%)	Press	Mult	Method
Stage 0	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth
Stage 1	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth

Name	Support	Axial	Used	Min Toe	Toe	Toe
	Model	Incl	FSwall	FDtoe	FSrot	FSpas
Stage 0		N/A	1	10.132	10.132	10.838
Stage 1		N/A	1	1.242	1.362	N/A

Name=excavation stage name

Analysis method

springs = Elastoplastic spring analysis used

DR = Drained condition for CLAY model

U = Undrained condition for CLAY model for all the soils

Up = Undrained condition just for selected soil

Limit equilibrium analysis settings

Drive press:

Ka (Active pressure diagram), Ka-Trap = Trapezoid apparent diagram from active pressures x multiplier, FHWA= Federal Highway Administration apparent pressure diagrams.

Ko = At-rest lateral earth pressures.

Peck = Peck 1969 Apparent earth pressure diagrams.

2 Step rect = Two step rectangular apparent earth pressure diagram.

User def. = User defined apparent earth pressure diagram.

Ka+d (and so on) indicates that wall friction is applied

ka mult = multiplication factor for Ka when Ka-Trap is selected

Htr T/B (%) = trapezoidal pressure scheme, top and bottom triangular percentage of excavation depth H

Resit press = Kp (passive earth pressures)

Res Mult = Safety factor applied directly on resisting pressures (

COntle Method = cantilever analysis method for limit equilibrium analysis.

Support Model: Method for calculating support reactions in limit-equilibrium analysis.

Beam= support reactions beam analysis (uses Blum's method).

Trib= support reactions from tributary height calculations (Can be applied with apparent diagrams).

Axial Incl = Axial loads included for structural design

Used FS wall = Safety factor for axial+bending wall resistance to divide ultimate wall capacities.

Min FD Toe= embedded minimum safety factor (for limit equilibrium analysis)

Toe FS rot= rotation safety factor (classic for limit equilibrium analysis)

Toe FSpas= driving/resisting pressure safety factor (for limit equilibrium analysis)

## EXCAVATION STAGES SKETCHES

A sequence of figures for each excavation stage is reported

### Toe stability

#### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	10.132	10.838	10.132	140.278	N/A	N/A
Stage 1	1.242	N/A	1.362	1.242	N/A	N/A

Legend: Wall embedment safety factors (toe)

Min Toe FS= Minimum wall embedment safety factor (from all analysis methods)

Limit-equilibrium analysis methods: The following safety factors may not be applicable for all stages.

FS1 Passive: Horizontal force safety factor, FS1= Resisting/Driving force

FS2 Rotation: Rotational safety factor about lowest support, FS2= Resisting moment/Driving moment

FS3 Length (from FS1, FS2): Program determines maximum required wall embedment for safety factor of 1 for methods

FS1 and FS2 (say length LFS1). Then FS length= Provided wall embedment/LFS1.

Non-linear elastoplastic analysis safety factors:

FS4 Mobilized Passive: Safety factor on mobilized passive resistance, FS4= Available passive soil resistance/Mobilized passive soil force on excavation side.

FS5 Active Drive Thrust/Theory Active: Ratio of soil thrust on retained side/ Active condition theoretical minimum thrust.

This factor is not as critical, and indicates how close to active conditions the model is.

General recommendations on wall embedment (excluding FS5):

When the excavation is designed with allowable standards, engineers generally use minimum safety factors from 1.2 to 1.5 depending on the level of confidence. A minimum safety factor of 1.2 is generally applied on FS3.

With ultimate limit state designs (such as Eurocode 7, and LRFD) the required safety factor must generally be greater than 1.0. In non-linear solutions it might be impossible to achieve exactly 1 on FS4 as this would likely trigger overall failure.

## **Result diagrams (for walls)**

A sequence of result diagrams for each excavation stage is reported

## **WALL RESULTS TABLE**

LEGEND

Wall node=number of the node (0 at top)

EL= Node elevation

Sht L=Total horizontal soil pressure (on the left side of the wall)

Sht R=Total horizontal soil pressure (on the right side of the wall)

Shs L=Effective horizontal soil pressure (on the left side of the wall)

Shs R=Effective horizontal soil pressure (on the right side of the wall)

q=pressure given by the surcharge

U L= Water pressure (on the left side of the wall)

U R= Water pressure (on the right side of the wall)

M=bending moment (per unit length)

V=shear (per unit length)

dx=wall deflection

McapL=Ultimate bending moment (on the left side of the wall)

McapR=Ultimate bending moment (on the right side of the wall)

VcapL=Ultimate resistance shear (on the left side of the wall)

VcapR=Ultimate resistance shear (on the right side of the wall)

## **EXCAVATION STAGES AND SLOPE STABILITY**

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Reports a sequence of figures for each stage with slope stability results.

**SLOPE STABILITY ANALYSIS: SLICE RESULTS ALL STAGES**

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Slope stability analysis design section: 0: AASHTO LRFD (2010): Strength Ia

**LEGEND**

x1 = Left x coordinate

ZsL= Left slice bottom elevation

ZtL= Left top elevation

x2 = Right x coordinate

ZsR= Right slice bottom elevation

ZtR= Right top elevation

DL = Slice base width

an = Base angle

Fr = Average friction angle at base

c = Average cohesion at base (may include undrained clay strengths)

Wn = Total slice weight

ubL= Water pressure at left bottom point

ubR= Water pressure at right bottom point

tBase= Base shear resistance

Nr = Effective normal reaction at bottom of slice

EiL= Lateral interslice force on left face

EiR= Lateral interslice force on right face

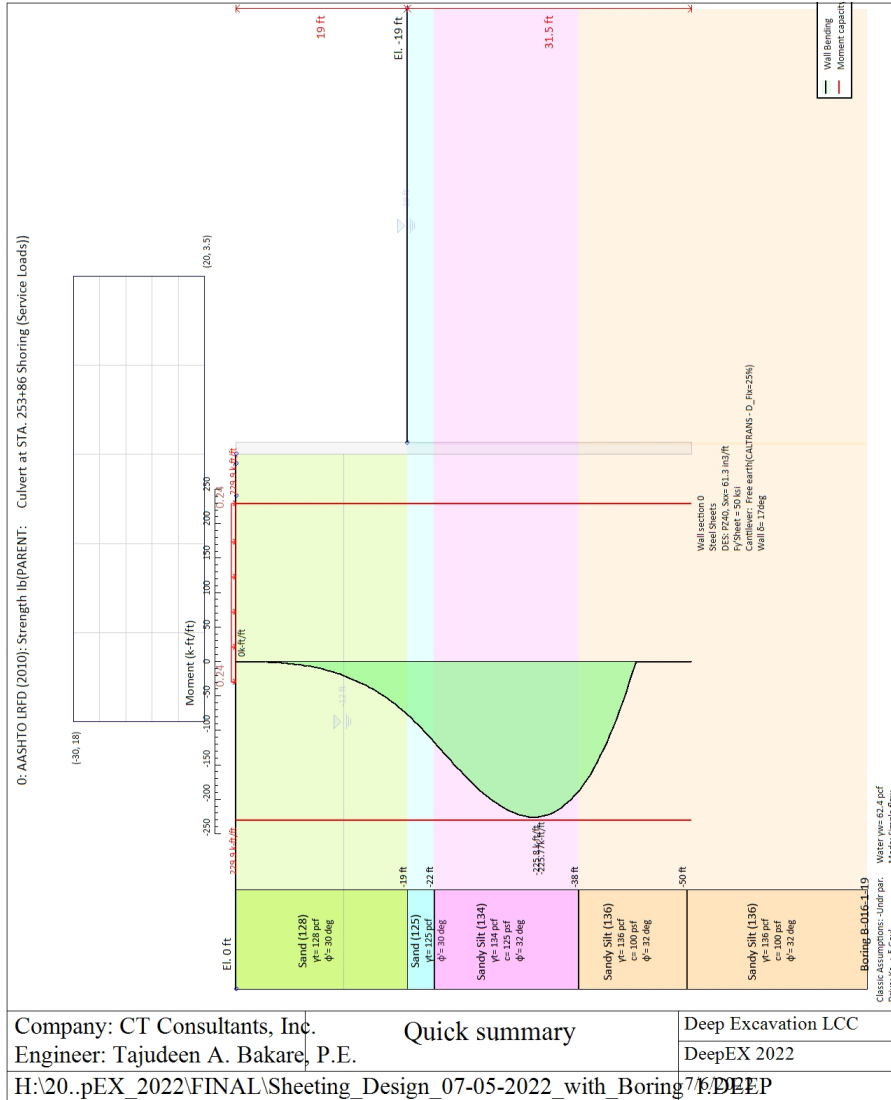
TL = Vertical interslice shear on left vertical face

TR = Vertical interslice shear on right vertical face

UbF= Normal water force at slice base

***Project: ODOT PID No. 108665; LAK-20-19.59 - WEST  
Results for Design Section 3: 0: AASHTO LRFD (2010):  
Strength Ib***

# ANALYSIS AND CHECKING SUMMARY



Company: CT Consultants, Inc. Quick summary Deep Excavation LCC  
 Engineer: Tajudeen A. Bakare, P.E. DeepEX 2022  
 H:\20.pEX\_2022\FINAL\Sheeting\_Design\_07-05-2022\_with Boring 7\DEEP

## Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	225.77/229.88	10.838	1.362	1.242	-44.37	3.243

## Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

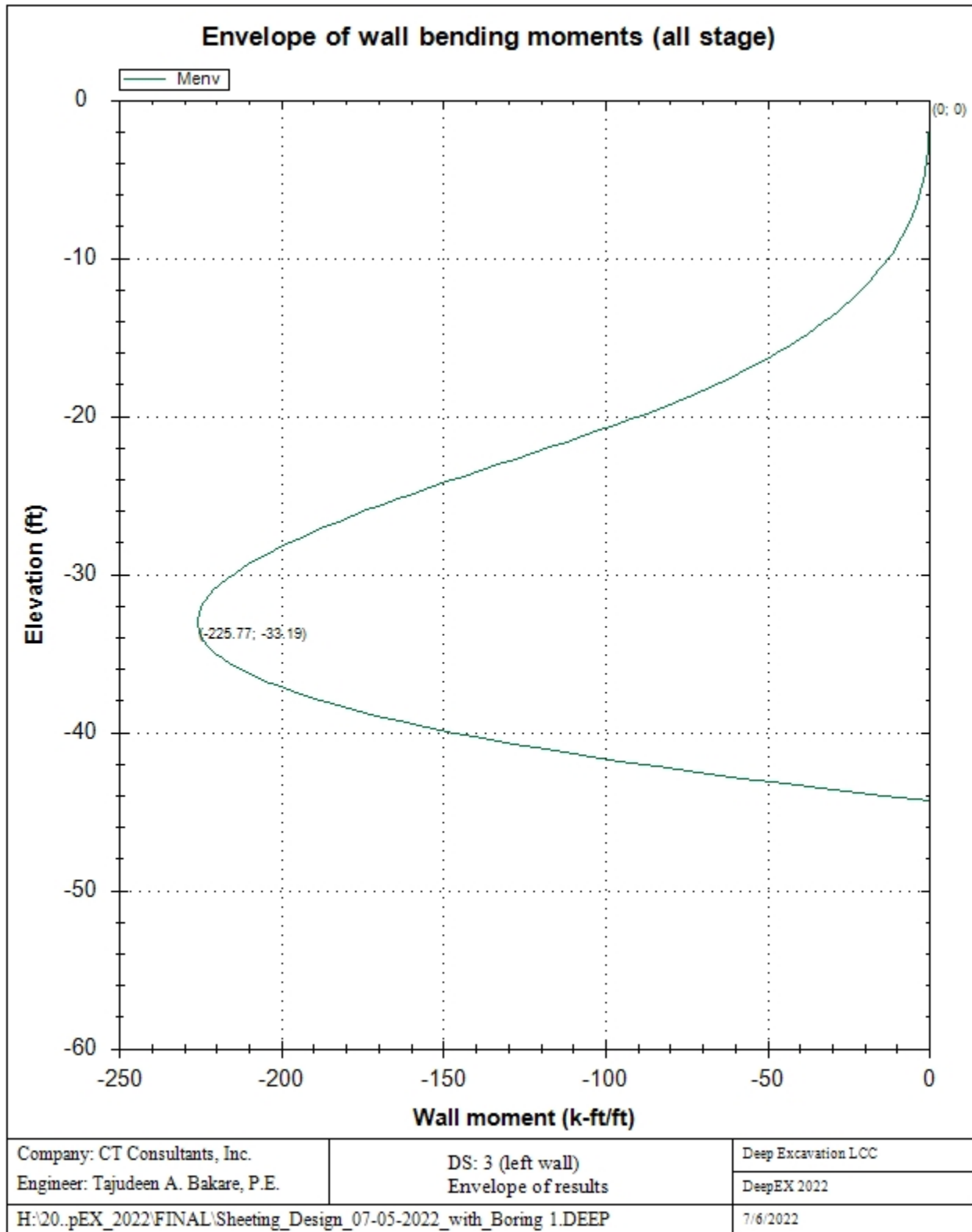
1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.867	12.4	3.243	0.38	12.449	3.243

General assumptions for last stage: Stage 1

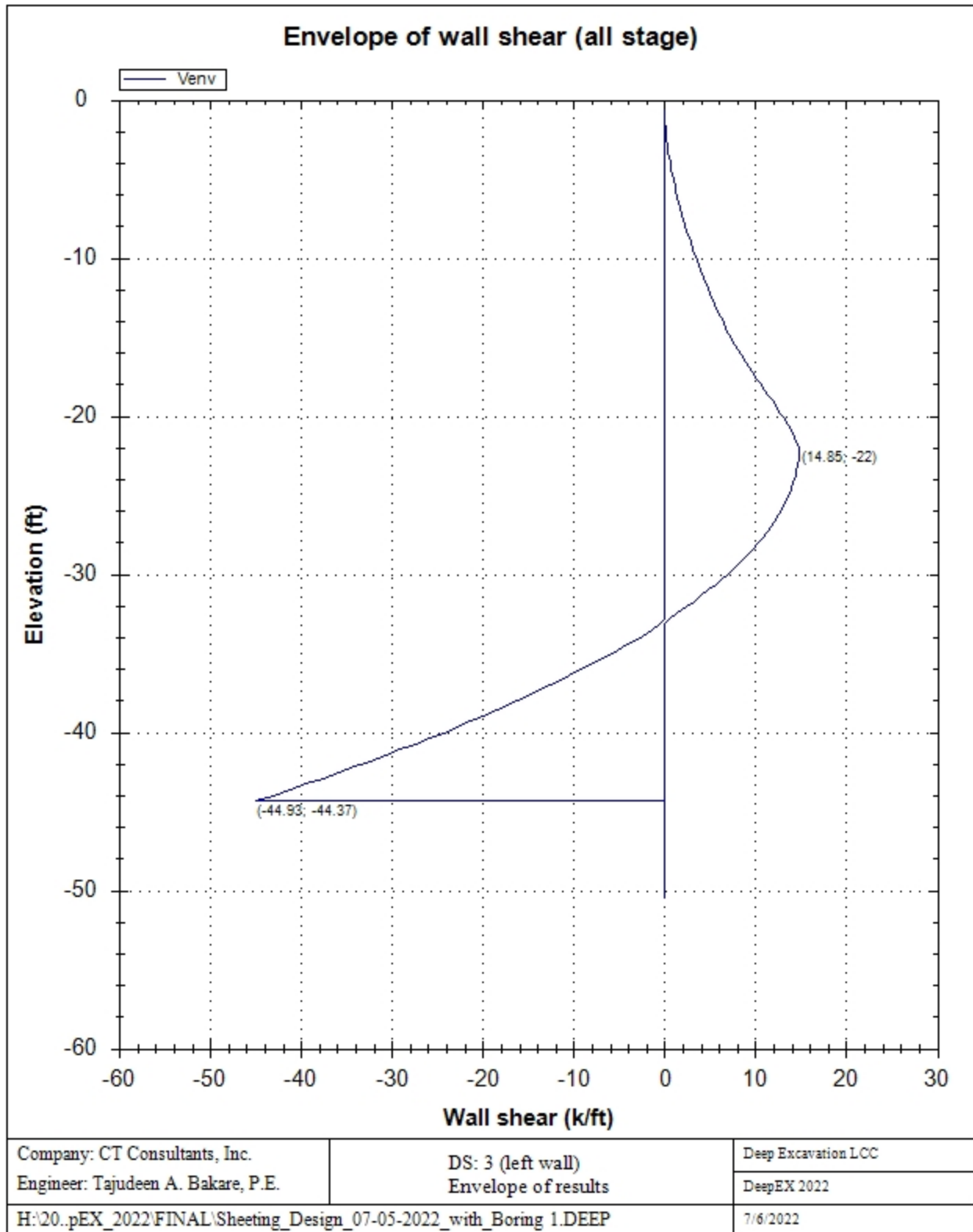
Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Caquot

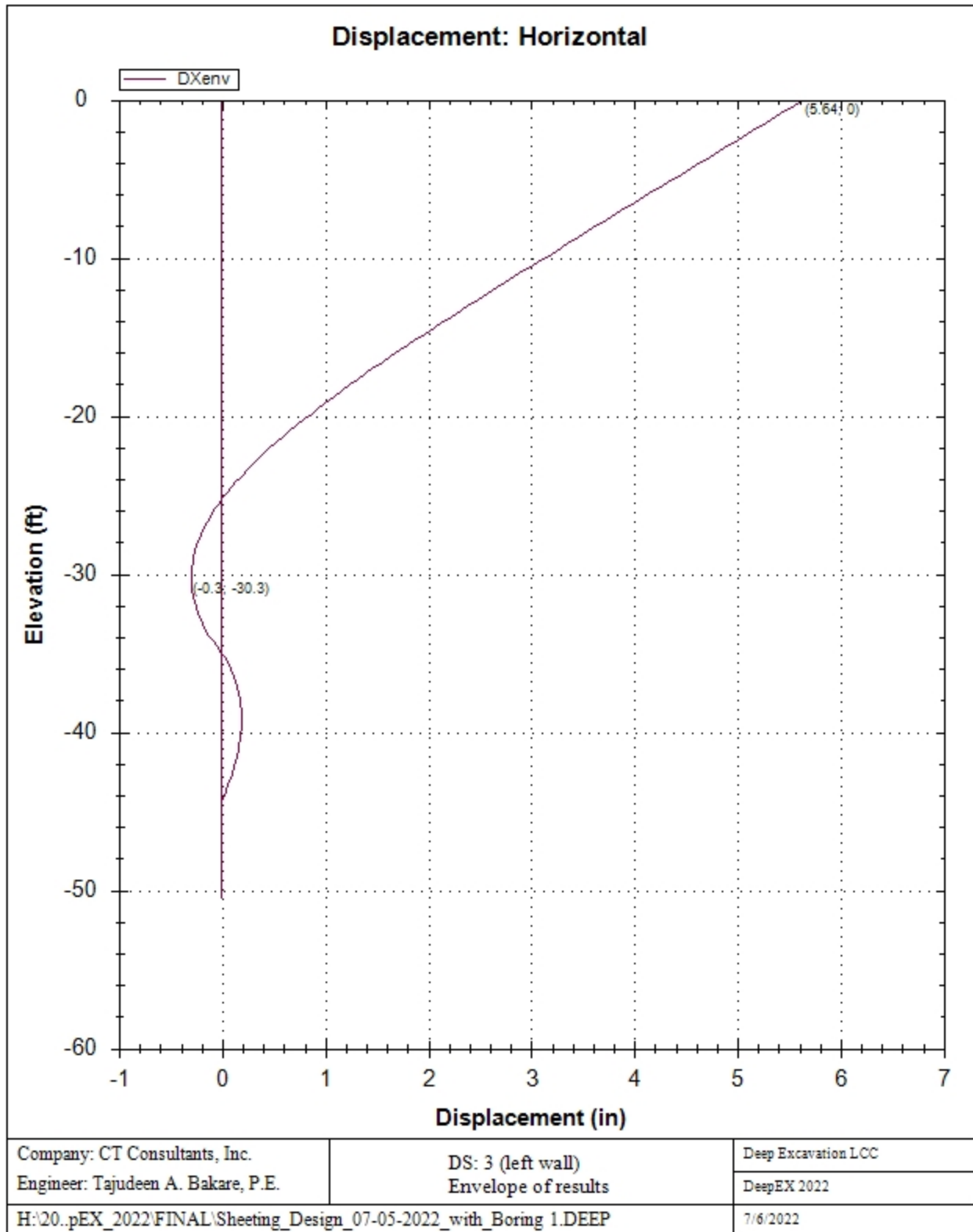
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Extended vs Stage

	Calculation Result	Wall Displaceme (in)	Settlement (in)	Wall Moment (k-ft/ft)	Wall Moment (k-ft)
Stage 0	Calculated	0	N/A	0	0
Stage 1	Calculated	5.64	2.39	225.77	225.77

	Wall Shear (k/ft)	Wall Shear (k)	STR Combined Wall Ratio	STR Moment Wall Ratio	STR Shear Wall Ratio
Stage 0	0	0	0	0	0
Stage 1	44.93	44.93	0.982	0.982	0.275

Table notes:

STR Combined: Combined stress check, along eccentricity line considering axial load and moment (demand/capacity).

STR Moment : Moment stress check, assuming constant axial load on wall (demand/capacity).

STR Shear : Shear stress check (shear force demand/wall shear capacity).

	Max Support Reaction (k/ft)	Max Support Reaction (k)	Critical Support Check	STR Support Ratio	Support Geotech Capacity Ratio (pull out)
Stage 0	0	0	N/A	No supports	No supports
Stage 1	0	0	N/A	No supports	No supports

Table notes:

STR Support ratio: Critical structural stress check for support (force demand/structural capacity).

Support geotech capacity ratio: Critical geotechnical capacity stress check (demand/geotechnical capacity).

Critical support check: Critical demand/design capacity ratio (structural or geotechnical).

	FS Basal	Toe FS Passive	Toe FS Rotation	Toe FS Length	Zcut (nonlinear)	FS Mobilized Passive	FS True/Active
Stage 0	1000	10.838	10.132	140.278	N/A	N/A	N/A
Stage 1	N/A	N/A	1.362	1.242	N/A	N/A	N/A

	Hydraulic Heave FS	Qflow (ft3/hr)	FSslope
Stage 0	2.729	N/A	N/C
Stage 1	1.821	N/A	3.243

**Support Force/S vs Stage**

	No Supports
0:Stage 0	No support
1:Stage 1	

**Support Force vs Stage**

**Support Force vs Stage**

	No Supports
0:Stage 0	No support
1:Stage 1	

**Embedment FS vs Stage**

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	10.132	10.838	10.132	140.278	N/A	N/A
0:Stage 0	1.242	N/A	1.362	1.242	N/A	N/A

Table notes:

FSbasal : Critical basal stability safety factor (relevant only when soft clays are present beneath the excavation).

Wall embedment safety factors from conventional analysis (limit-equilibrium):

FS1 Passive : Safety factor for wall embedment based on FS= Available horizontal thrust resistance/Driving hor. thrust.

FS2 Rotation: Safety factor for wall embedment based on FS= Available resisting moment/Driving moment.

FS3 Length : Safety factor for wall embedment based on FS= Available wall embedment/Required embedment for FS=1.0

Wall embedment safety factors from non-linear analysis:

FS4 Mobilized Passive : Safety factor= Available horizontal passive resistance/Mobilized passive thrust.

FS5 True/Active : Soil thrust on retained wall side/Minimum theoretically horizontal active force thrust.

Tables for stress checks follow: Support force/Design capacity

Support Check vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

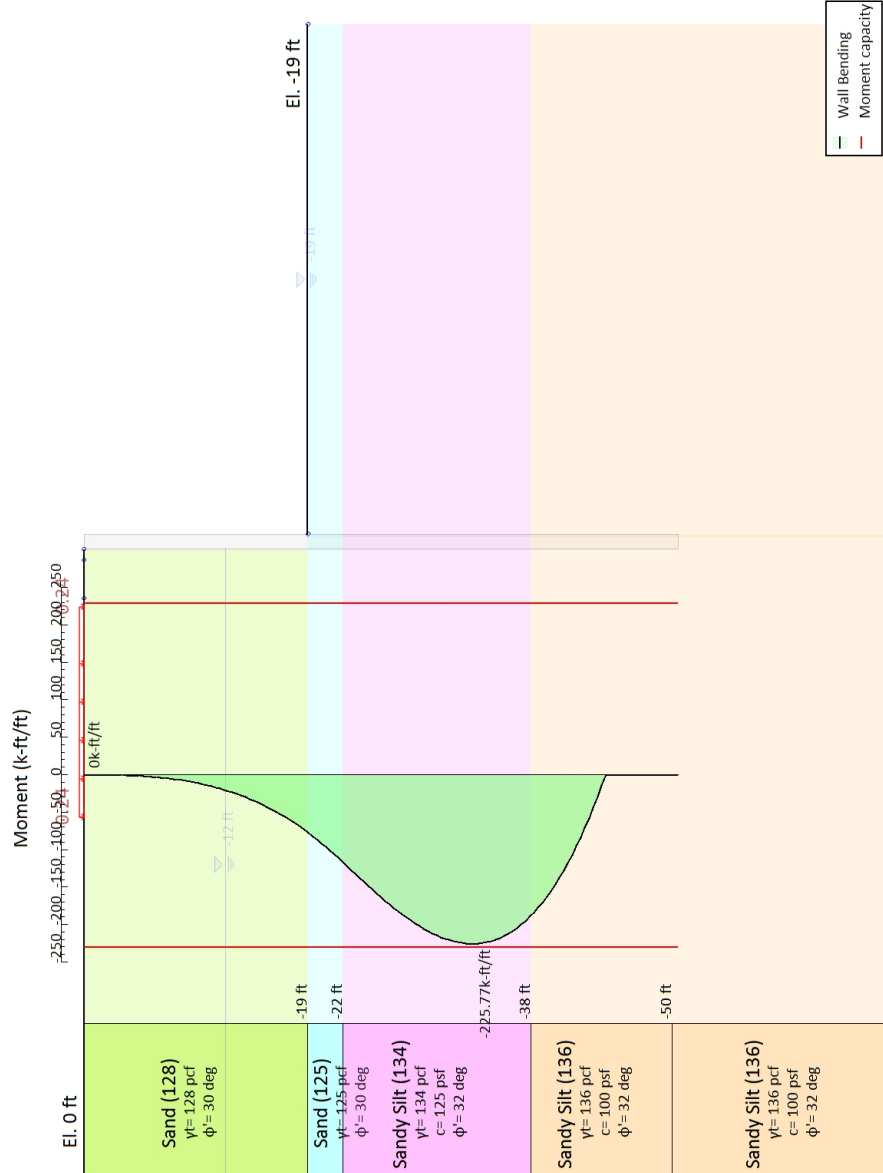
Forces (Res. F, M/Drive F, M)

	FS1 Passive (FxResist/FxDrive)	FS2 Rotation (Mresist/Mdrive)	FS3 Length (Embedment/ToeFS=1)	FS4 Mobilized Passive (FxPassive/FxPas_Mobili)	FS5 Actual Drive / Theory Active	Fh EQ Soil	Fh EQ Water
Stage 0	446.702/41.215	7920.69/781.78	50.5/0.36	N/A	N/A	N/A	N/A
Stage 1	N/A	1451.85/616.83	31.5/25.37	N/A	N/A	N/A	N/A

Reinforcement Requirements

	Parameter Description
Note:	Wall does not use steel reinforcement. Section does not apply.

O: AASHTO LRFD (2010): Strength lb(PARENT): Culvert at STA. 253+86 Shoring (Service Loads)



Boring B-016-1-19  
 O LRFD 8 (2018), Case: Strength lb  
 γ: FS(tanFR)= 1, FS c= 1, FS Su= 1  
 1, gDStab= 1, FSres= 1.33, FSdriveE= 1.35  
 s'A: Temp= 1.75, Perm= 1.35, EQ= 0  
 FS\_Drive= 1, FS\_Res= 1, HYDgDStab = 1, HYDgStab = 1  
 fs'R: Temp= 1, Perm= 1.11

Company: CT Consultants, Inc.

Engineer: Tajudeen A. Bakare, P.E.

H:\20..pEX\_2022\FINAL\Sheeting\_Design\_07-05-2022\_with\_Boring 1.DEEP

Quick summary

Deep Excavation LCC

DeepEX 2022

7/6/2022

### Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	225.77/229.88	10.838	1.362	1.242	-44.37	3.243

### Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

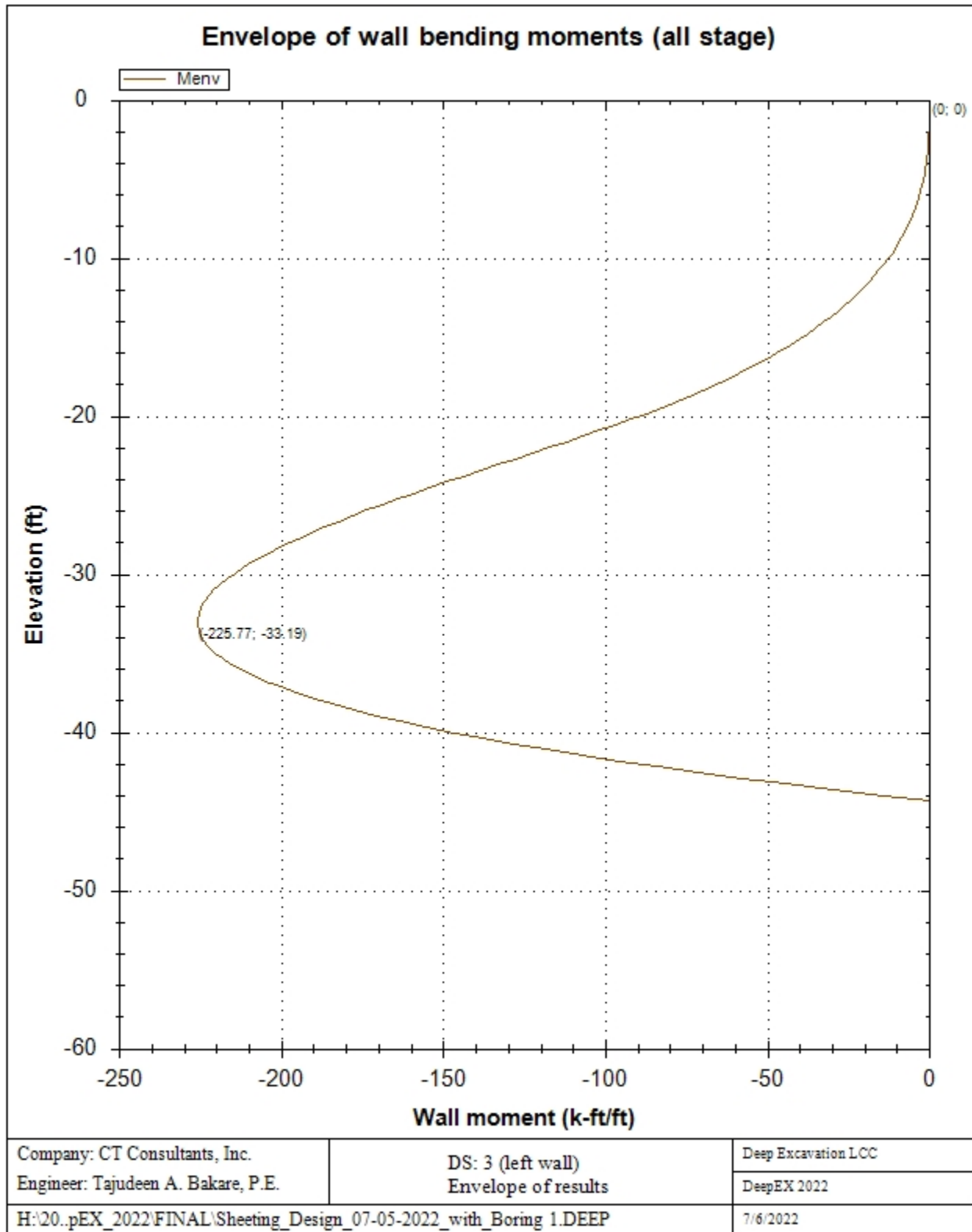
1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.867	12.4	3.243	0.38	12.449	3.243

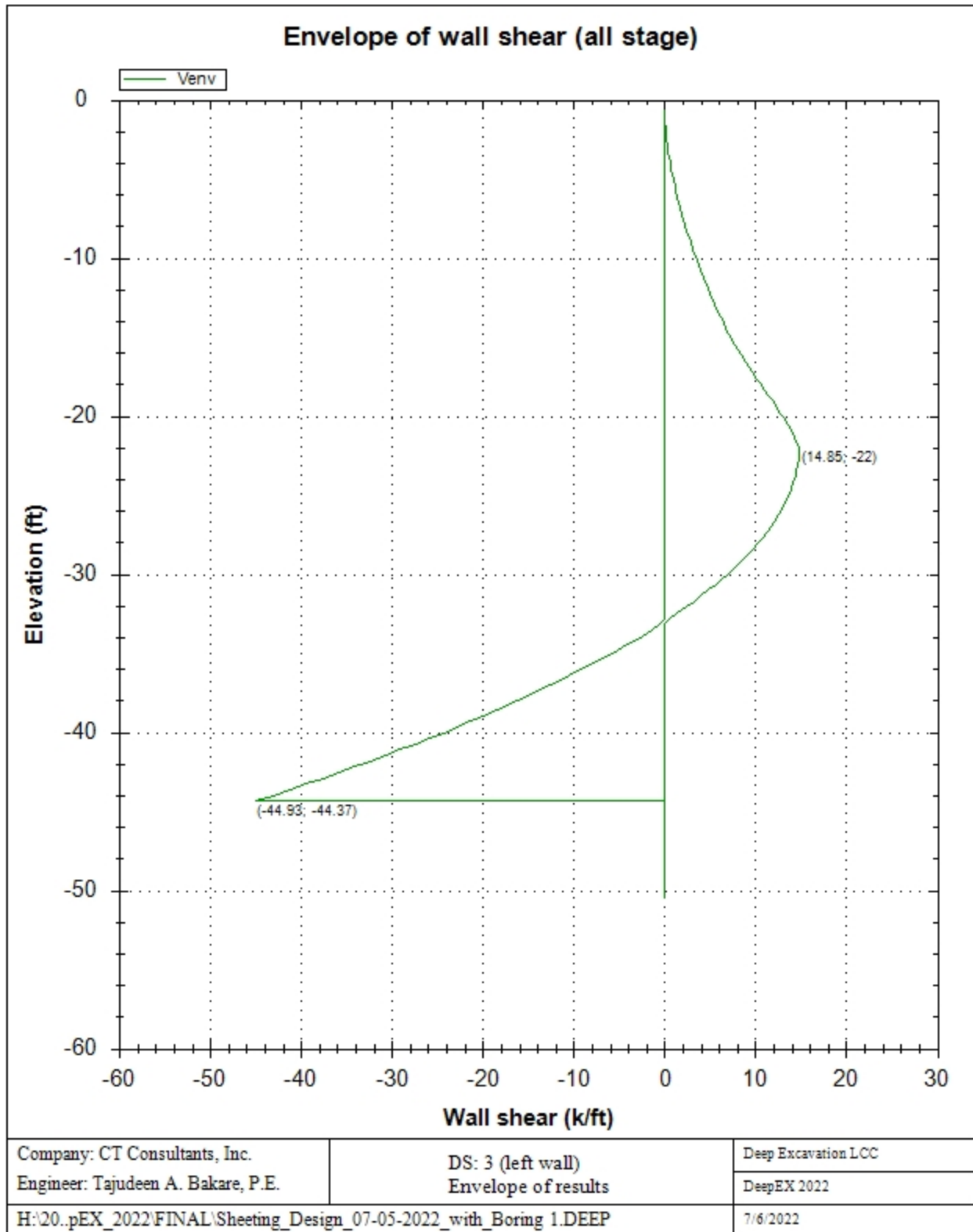
### General assumptions for last stage: Stage 1

Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Coul

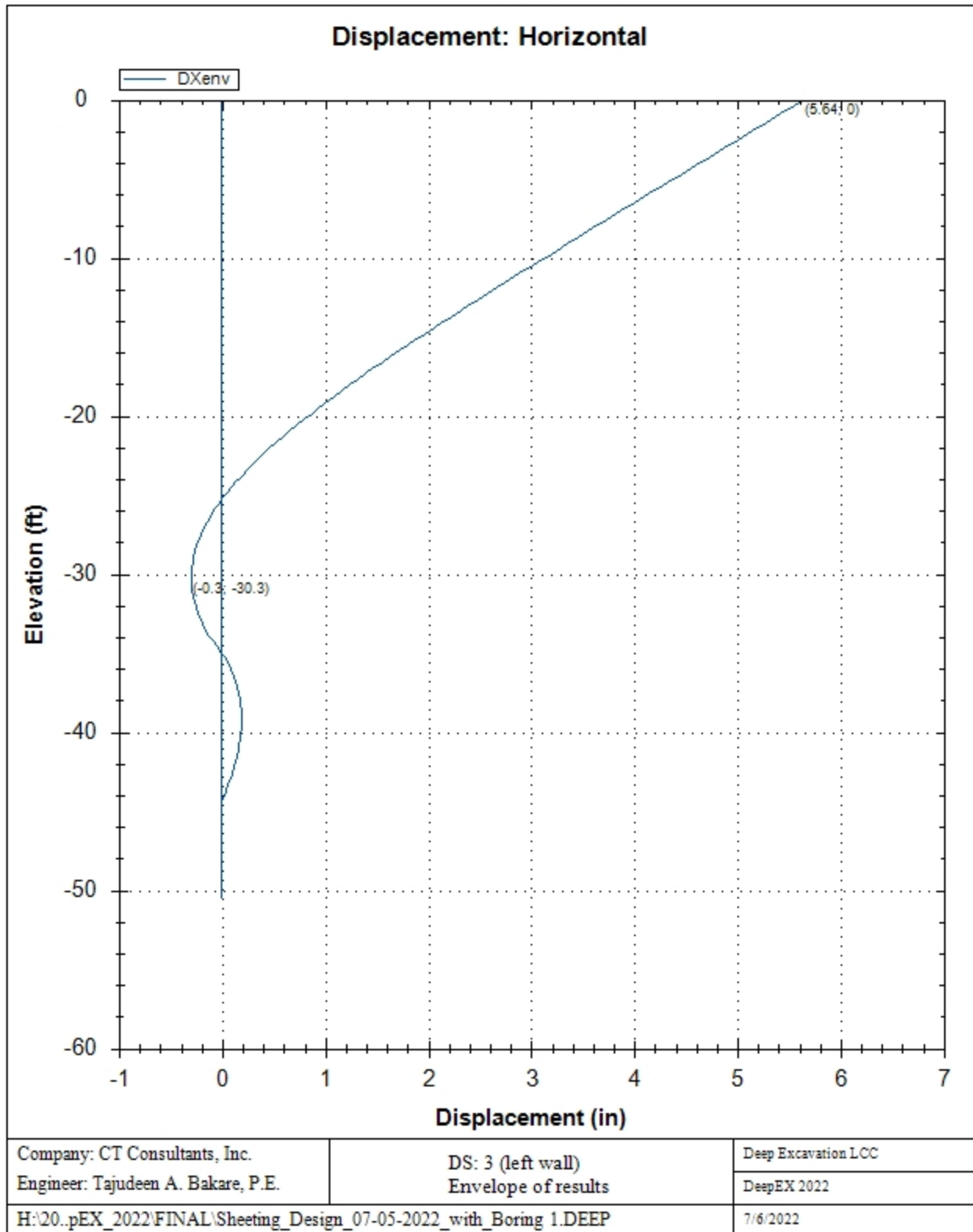
### Envelope of results

A sequence of result diagrams for each excavation stage is reported









**DESIGN APPROACHES AND COMBINATION FACTORS**

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

Ftan fr=mult factor for friction angle

F C'= safety factor on effective cohesion (Eurocode 7 methods)

F Su'= safety factof for undrained shear strength (Eurocode 7 methods)

F EQ= Load factor for seismic loads

F perm load= Load factor for permanent loads (dead load, etc)

F temp load= Load factor on live loads and other temporary loads

F perm supp= Reduction factor for resistance for pull out checking of permanent tiebacks

F temp supp= Reduction factor for resistance for pull out checking of temporary tiebacks

F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)

F earth stab= Safety factor for passive pressures, favorable (on excavation side)

F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable

F GWT stab (ground water)= Load factor for resisting water pressure, favorable

F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)

F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)

F UPL Dstab= Load factor for uplift check, unfavorable

F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan fr)	F (c')	F (Su)	F (EQ)	F(perm load)	F(temp load)	F(perm sup)	F(temp sup)	F Earth (Dstab)	F Earth (stab)	F GWT (Dstab)	F GWT (stab)	F HYD (Dstab)	F HYD (stab)	F UPL (Dstab)	F UPL (stab)
0	AASHTO LRFD	Strength Ib	1	1	1	0	1.35	1.75	1.11	1	1.35	1.33	1	1	1	1	1	1
1	AASHTO LRFD	Strength Ib	1	1	1	0	1.35	1.75	1.11	1	1.35	1.33	1	1	1	1	1	1

## DESIGN APPROACHES AND COMBINATION FACTORS

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

Ftan fr=mult factor for friction angle

F C'= safety factor on effective cohesion (Eurocode 7 methods)

F Su'= safety factof for undrained shear strength (Eurocode 7 methods)

F EQ= Load factor for seismic loads

F perm load= Load factor for permanent loads (dead load, etc)

F temp load= Load factor on live loads and other temporary loads

F perm supp= Reduction factor for resistance for pull out checking of permanent tiebacks

F temp supp= Reduction factor for resistance for pull out checking of temporary tiebacks

F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)

F earth stab= Safety factor for passive pressures, favorable (on excavation side)

F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable

F GWT stab (ground water)= Load factor for resisting water pressure, favorable

F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)

F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)

F UPL Dstab= Load factor for uplift check, unfavorable

F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan fr)	F (c')	F (Su)	F (EQ)	F(perm load)	F(temp load)	F(perm sup)	F(temp sup)	F Earth (Dstab)	F Earth (stab)	F GWT (Dstab)	F GWT (stab)	F HYD (Dstab)	F HYD (stab)	F UPL (Dstab)	F UPL (stab)
0	AASHTO LRFD	Strength Ib	1	1	1	0	1.35	1.75	1.11	1	1.35	1.33	1	1	1	1	1	1
1	AASHTO LRFD	Strength Ib	1	1	1	0	1.35	1.75	1.11	1	1.35	1.33	1	1	1	1	1	1

## SOIL DATA

Name	g tot (pcf)	g dry (pcf)	Frict (deg)	C' (psf)	Su (psf)	FRp (deg)	FRcv (deg)	Eload (ksf)	rEur (-)	kAp NL	kPp NL	kAcv NL	kPcv NL	Vary	Spring Model	Color
Sand (128)	128	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sand (125)	125	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sandy Silt (13)	134	134	32	125	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	
Sandy Silt (13)	136	136	32	100	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	

Name	Poisson	Min Ka	Min sh	ko.NC	nOCR	aH.EXP	aV.EXP	qSkin	qNails	kS.nails	PL
	v	(clays)	(clays)	-	-	(0 to 1)	(0 to 1)	(psi)	(psi)	(k/ft3)	(ksi)
Sand (128)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sand (125)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-

gtot = total soil specific weight

gdry = dry weight of the soil

Frict = friction angle

C' = effective cohesion

Su = Undrained shear strength (only for CLAY soils in undrained conditions, used as a cutoff strength in NL analysis)

Evc = Virgin compression elastic modulus

Eur = unloading/reloading elastic modulus

Kap = Peak active thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kpp = Peak passive thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kacv = Constant volume active thrust coeff (only for clays, initial value)

Kpcv = Constant volume passive thrust coeff (only for clays, initial value).

Spring models= spring model (LIN= constant E over the soil layer height , EXP=exponential , SIMC=simplified winkler)

LIN= Linear-Elastic-Perfectly Plastic,

EXP: Exponential, SUB: Modulus of Subgrade Reaction

SIMC= Simplified Clay mode

## **SOIL BORINGS**

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Top Elev= superior SOil level

Soil type= type of the soil (sand , clay , etc)

OCR= overconsolidation ratio

K0= at rest coefficient

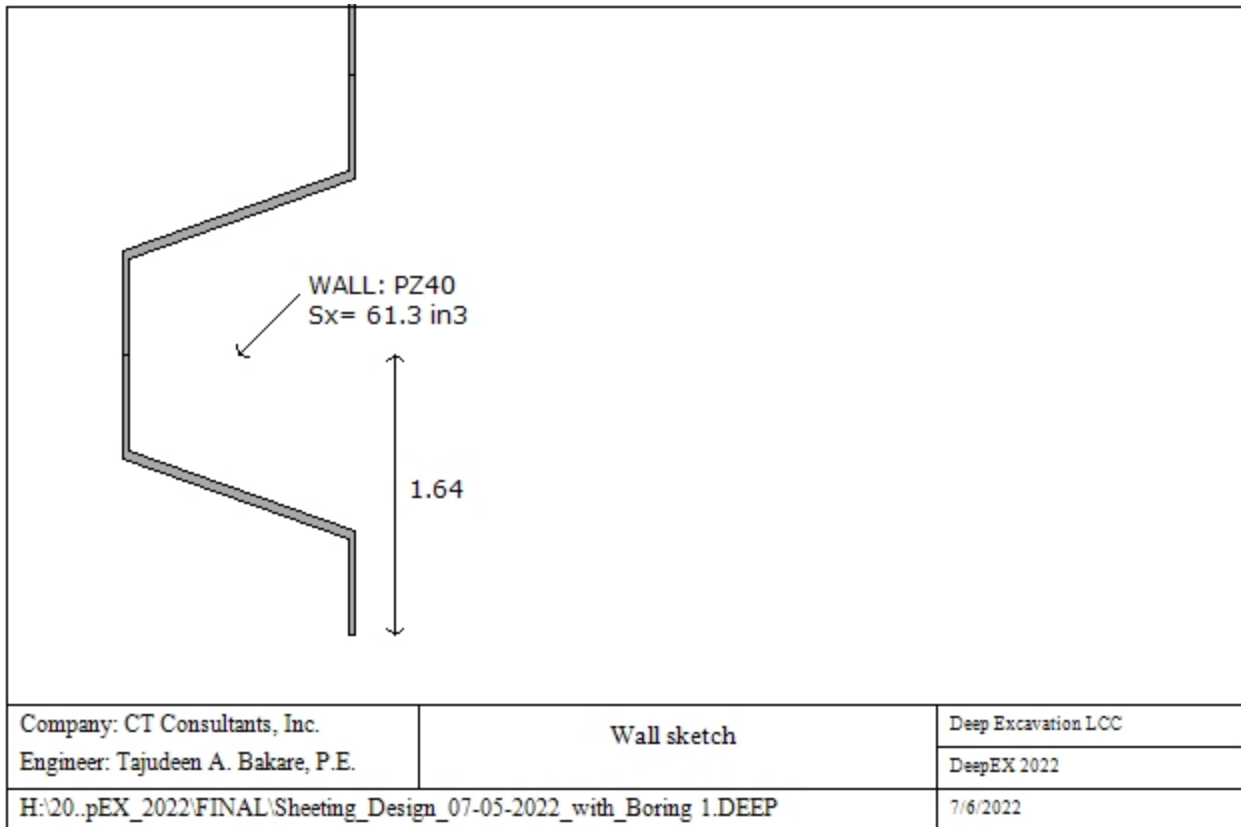
Name: Boring B-016-1-19, pos: (0, 0)

Top elev.	Soil type	OCR	Ko
0	Sand (128)	1	0.5
-19	Sand (125)	1	0.5
-22	Sandy Silt (134)	1	0.47
-38	Sandy Silt (136)	1	0.47
-50	Sandy Silt (136)	1	0.47

## **WALL DATA**

---

Wall section 0: Wall section 0



Wall type: Steel sheet piling  
 Top wall El: 0 ft Bottom wall El: -50.5 ft  
 Hor. wall spacing: 1 ft Wall thickness = 1.37 ft  
 Passive width below exc: 1 ft Active width below exc: 1 ft Swater= 1 ft  
 Steel members fy = 50 ksi Esteel = 29000 ksi  
 Wall friction: Constant value = 17 degrees  
 Steel wall capacities are calculated with ANSI/AISC 360-10  
 Concrete capacities are calculated with ACI 318-19  
 Note: With ultimate capacities you may have to use a structural safety factor.  
 Steel sheet pile properties

Table: Steel Sheet Pile Cross Sectional Properties

DES	Shape	W	A	h	t	b	s	Ixx	Sxx
		(plf)	(in <sup>2</sup> /ft)	(in)	(in)	(in)	(in)	(in <sup>4</sup> /ft)	(in <sup>3</sup> /ft)
PZ40	Z	65.6	11.75	16.4	0.5	19.69	0.605	503	61.3

GENERAL WALL DATA

Hor wall spacing= Wall horizontal spacing  
 Passive width below exc= spacing for passive thrust pressure for classic analysis  
 f'c=fck= cylindrical concrete resistance  
 fyk=fyk= steel rebar characteristic resistance  
 Econc= Concrete Elastic modulus  
 fctk= characteristic Concrete tension  
 Esteel= steel elastic modulus  
 TABULAR DATA (principal parameters)  
 1) Diaphragm wall (rectangular cross section)  
 N/A= data not available  
 Fy=fyk

$F'c=fck$

D=wall thickness

B=wall width

2)Steel sheet pile

DES=shape (Z or U)

W=width per unit of length

A=area

h=height

t=horizontal part thickness

b=width of the single sheet pile part

s=inclined part thickness

$I_{xx}$ =strong axis inertia (per unit of length)

$S_{xx}$ =strong axis section modulus (per unit of length)

3)Secant piles wall, Tangent piles wall, soldier piles, soldier piles and timber lagging

W=weight per unit of length

A=area

D=diameter

$t_w$ =web thickness

$t_p$ = pipe thickness

$b_f$ =flange width

$t_f$ = flange thickness

$k$ = flange thickness+stem base height

$I_{xx}$ = strong axis inertia modulus (per unit of length)

$S_{xx}$ = strong axis section modulus (per unit of length)

$r_x$ =radius of gyration about X axis

$r_y$ =radius of gyration about Y axis

$I_{yy}$ =weak axis inertia modulus (per unit of length)

$S_{yy}$ =weak axis section modulus (per unit of length)

$r_T$ =radius of gyration for torsion

$C_w$ = warping constant

## GENERAL ANALYSIS CRITERIA

### Summary of stage assumptions

Name	Analysis	Drive	ka-Mult	Htr T/B	Resist	Res	Contle
	Method	Press		(%)	Press	Mult	Method
Stage 0	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth
Stage 1	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth

Name	Support	Axial	Used	Min Toe	Toe	Toe
	Model	Incl	FSwall	FDtoe	FSrot	FSpas
Stage 0		N/A	1	10.132	10.132	10.838
Stage 1		N/A	1	1.242	1.362	N/A

Name=excavation stage name

Analysis method

springs = Elastoplastic spring analysis used

DR = Drained condition for CLAY model

U = Undrained condition for CLAY model for all the soils

Up = Undrained condition just for selected soil

Limit equilibrium analysis settings

Drive press:

Ka (Active pressure diagram), Ka-Trap = Trapezoid apparent diagram from active pressures x multiplier, FHWA= Federal Highway Administration apparent pressure diagrams.

Ko = At-rest lateral earth pressures.

Peck = Peck 1969 Apparent earth pressure diagrams.

2 Step rect = Two step rectangular apparent earth pressure diagram.

User def. = User defined apparent earth pressure diagram.

Ka+d (and so on) indicates that wall friction is applied

ka mult = multiplication factor for Ka when Ka-Trap is selected

Htr T/B (%) = trapezoidal pressure scheme, top and bottom triangular percentage of excavation depth H

Resit press = Kp (passive earth pressures)

Res Mult = Safety factor applied directly on resisting pressures (

COntle Method = cantilever analysis method for limit equilibrium analysis.

Support Model: Method for calculating support reactions in limit-equilibrium analysis.

Beam= support reactions beam analysis (uses Blum's method).

Trib= support reactions from tributary height calculations (Can be applied with apparent diagrams).

Axial Incl = Axial loads included for structural design

Used FS wall = Safety factor for axial+bending wall resistance to divide ultimate wall capacities.

Min FD Toe= embedded minimum safety factor (for limit equilibrium analysis)

Toe FS rot= rotation safety factor (classic for limit equilibrium analysis)

Toe FSpas= driving/resisting pressure safety factor (for limit equilibrium analysis)

## EXCAVATION STAGES SKETCHES

A sequence of figures for each excavation stage is reported

### Toe stability

#### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	10.132	10.838	10.132	140.278	N/A	N/A
Stage 1	1.242	N/A	1.362	1.242	N/A	N/A

Legend: Wall embedment safety factors (toe)

Min Toe FS= Minimum wall embedment safety factor (from all analysis methods)

Limit-equilibrium analysis methods: The following safety factors may not be applicable for all stages.

FS1 Passive: Horizontal force safety factor, FS1= Resisting/Driving force

FS2 Rotation: Rotational safety factor about lowest support, FS2= Resisting moment/Driving moment

FS3 Length (from FS1, FS2): Program determines maximum required wall embedment for safety factor of 1 for methods

FS1 and FS2 (say length LFS1). Then FS length= Provided wall embedment/LFS1.

Non-linear elastoplastic analysis safety factors:

FS4 Mobilized Passive: Safety factor on mobilized passive resistance, FS4= Available passive soil resistance/Mobilized passive soil force on excavation side.

FS5 Active Drive Thrust/Theory Active: Ratio of soil thrust on retained side/ Active condition theoretical minimum thrust.

This factor is not as critical, and indicates how close to active conditions the model is.

General recommendations on wall embedment (excluding FS5):

When the excavation is designed with allowable standards, engineers generally use minimum safety factors from 1.2 to 1.5 depending on the level of confidence. A minimum safety factor of 1.2 is generally applied on FS3.

With ultimate limit state designs (such as Eurocode 7, and LRFD) the required safety factor must generally be greater than 1.0. In non-linear solutions it might be impossible to achieve exactly 1 on FS4 as this would likely trigger overall failure.

## **Result diagrams (for walls)**

A sequence of result diagrams for each excavation stage is reported

## **WALL RESULTS TABLE**

LEGEND

Wall node=number of the node (0 at top)

EL= Node elevation

Sht L=Total horizontal soil pressure (on the left side of the wall)

Sht R=Total horizontal soil pressure (on the right side of the wall)

Shs L=Effective horizontal soil pressure (on the left side of the wall)

Shs R=Effective horizontal soil pressure (on the right side of the wall)

q=pressure given by the surcharge

U L= Water pressure (on the left side of the wall)

U R= Water pressure (on the right side of the wall)

M=bending moment (per unit length)

V=shear (per unit length)

dx=wall deflection

McapL=Ultimate bending moment (on the left side of the wall)

McapR=Ultimate bending moment (on the right side of the wall)

VcapL=Ultimate resistance shear (on the left side of the wall)

VcapR=Ultimate resistance shear (on the right side of the wall)

## **EXCAVATION STAGES AND SLOPE STABILITY**

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Reports a sequence of figures for each stage with slope stability results.



**SLOPE STABILITY ANALYSIS: SLICE RESULTS ALL STAGES**

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Slope stability analysis design section: 0: AASHTO LRFD (2010): Strength Ib

**LEGEND**

x1 = Left x coordinate

ZsL= Left slice bottom elevation

ZtL= Left top elevation

x2 = Right x coordinate

ZsR= Right slice bottom elevation

ZtR= Right top elevation

DL = Slice base width

an = Base angle

Fr = Average friction angle at base

c = Average cohesion at base (may include undrained clay strengths)

Wn = Total slice weight

ubL= Water pressure at left bottom point

ubR= Water pressure at right bottom point

tBase= Base shear resistance

Nr = Effective normal reaction at bottom of slice

EiL= Lateral interslice force on left face

EiR= Lateral interslice force on right face

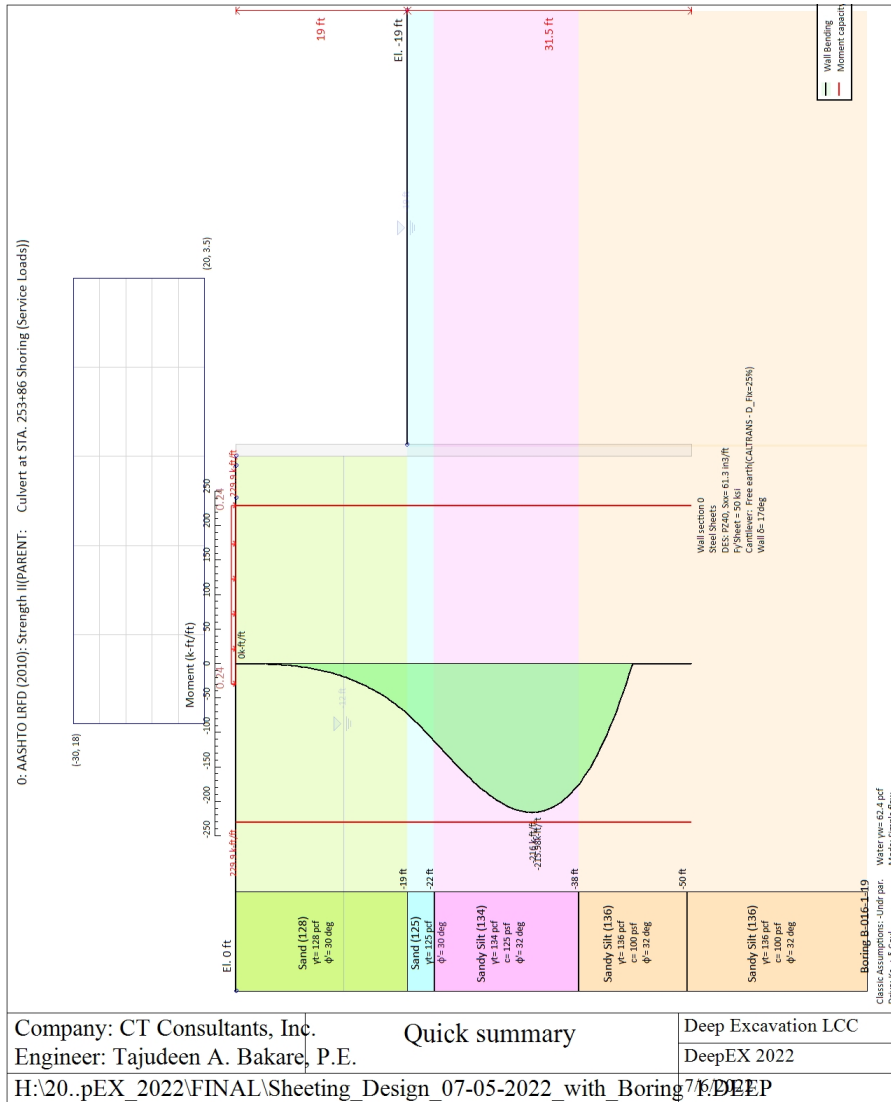
TL = Vertical interslice shear on left vertical face

TR = Vertical interslice shear on right vertical face

UbF= Normal water force at slice base

***Project: ODOT PID No. 108665; LAK-20-19.59 - WEST  
Results for Design Section 4: 0: AASHTO LRFD (2010):  
Strength II***

# ANALYSIS AND CHECKING SUMMARY



Company: CT Consultants, Inc. Quick summary Deep Excavation LCC  
 Engineer: Tajudeen A. Bakare, P.E. DeepEX 2022  
 H:\20.pEX\_2022\FINAL\Sheeting\_Design\_07-05-2022\_with Boring 7/1/2022

## Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	215.98/229.88	10.838	1.387	1.259	-44.01	3.266

## Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

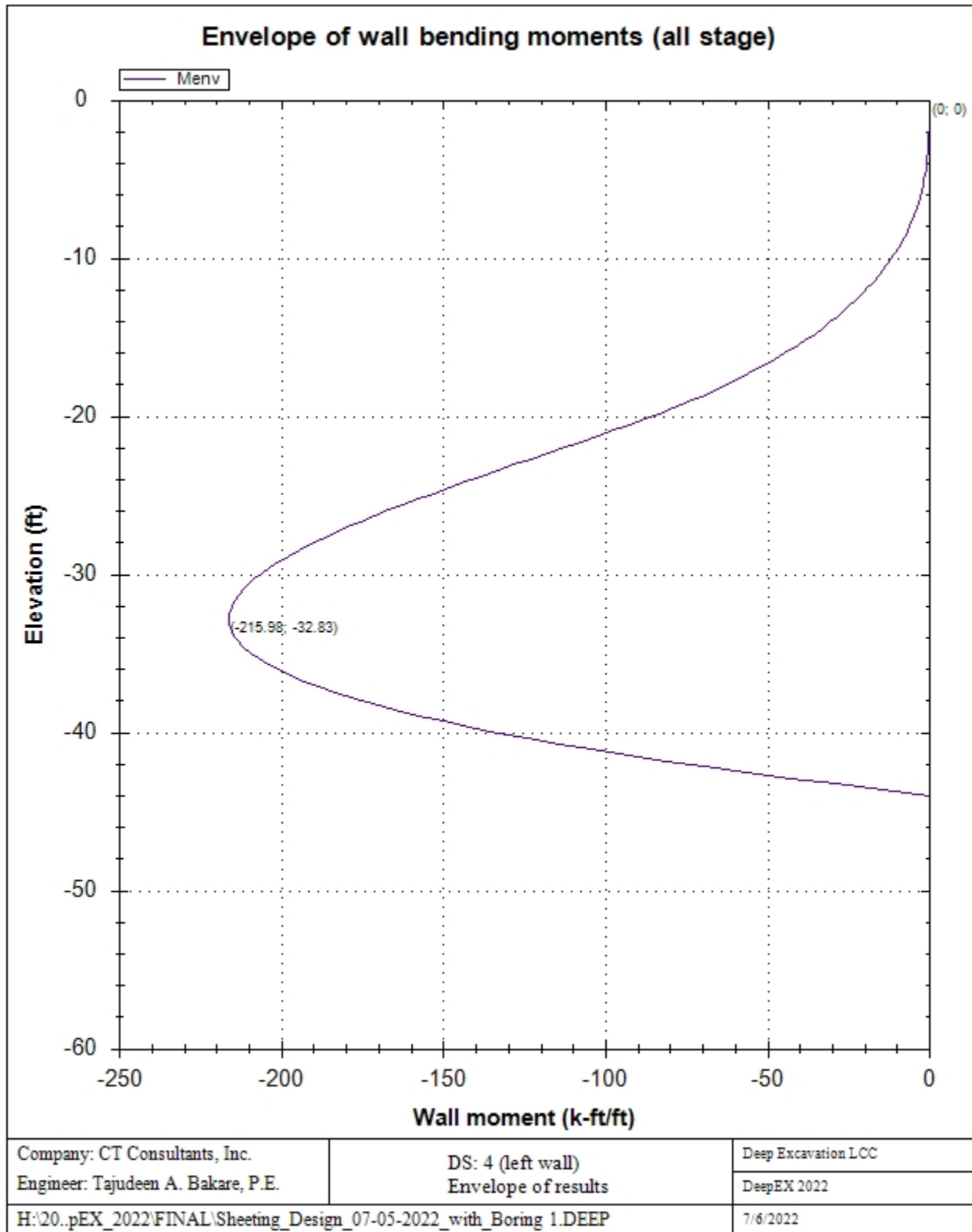
1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.857	12.4	3.266	0.376	12.449	3.266

General assumptions for last stage: Stage 1

Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Caquot

### Envelope of results

A sequence of result diagrams for each excavation stage is reported



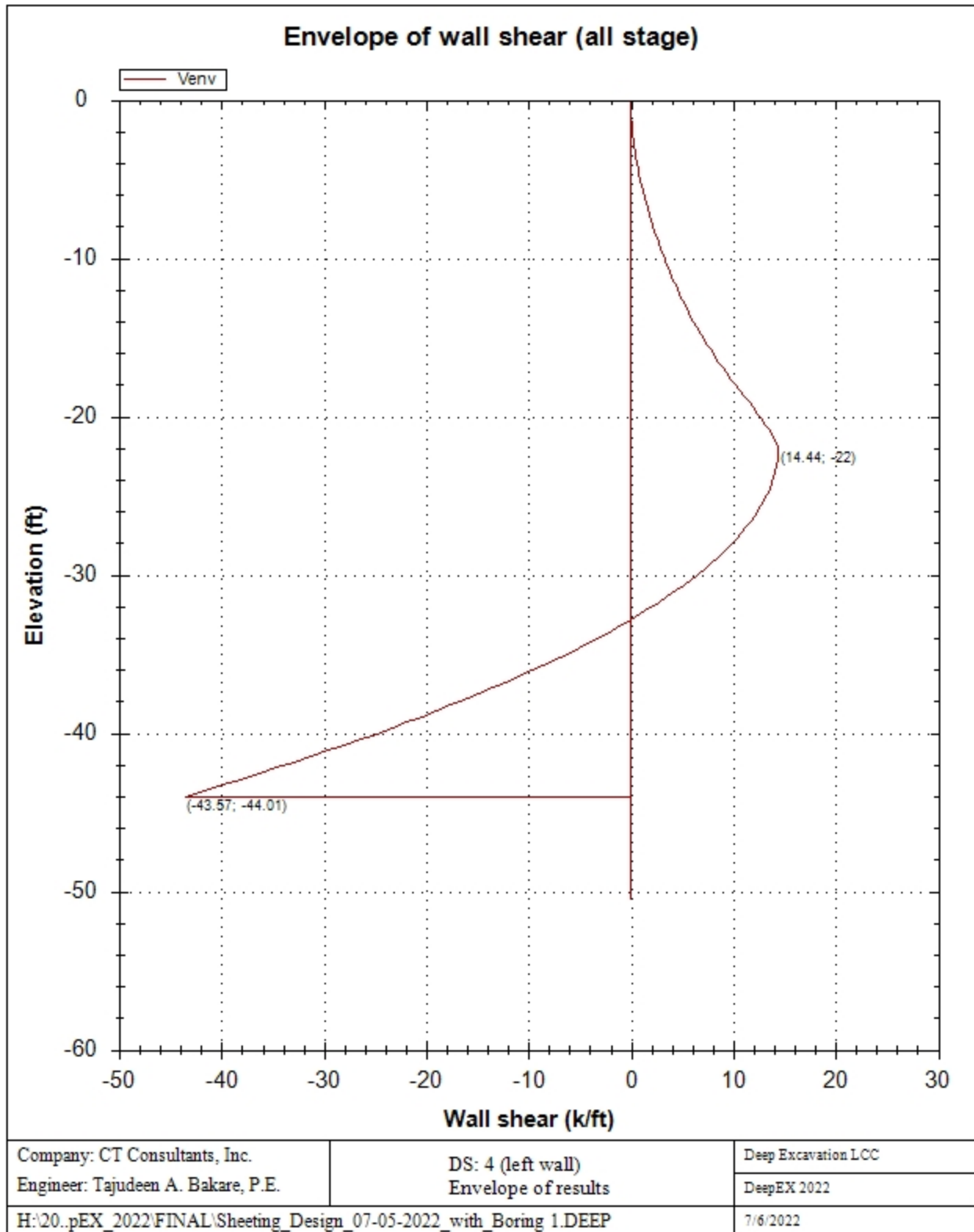
Company: CT Consultants, Inc.  
 Engineer: Tajudeen A. Bakare, P.E.

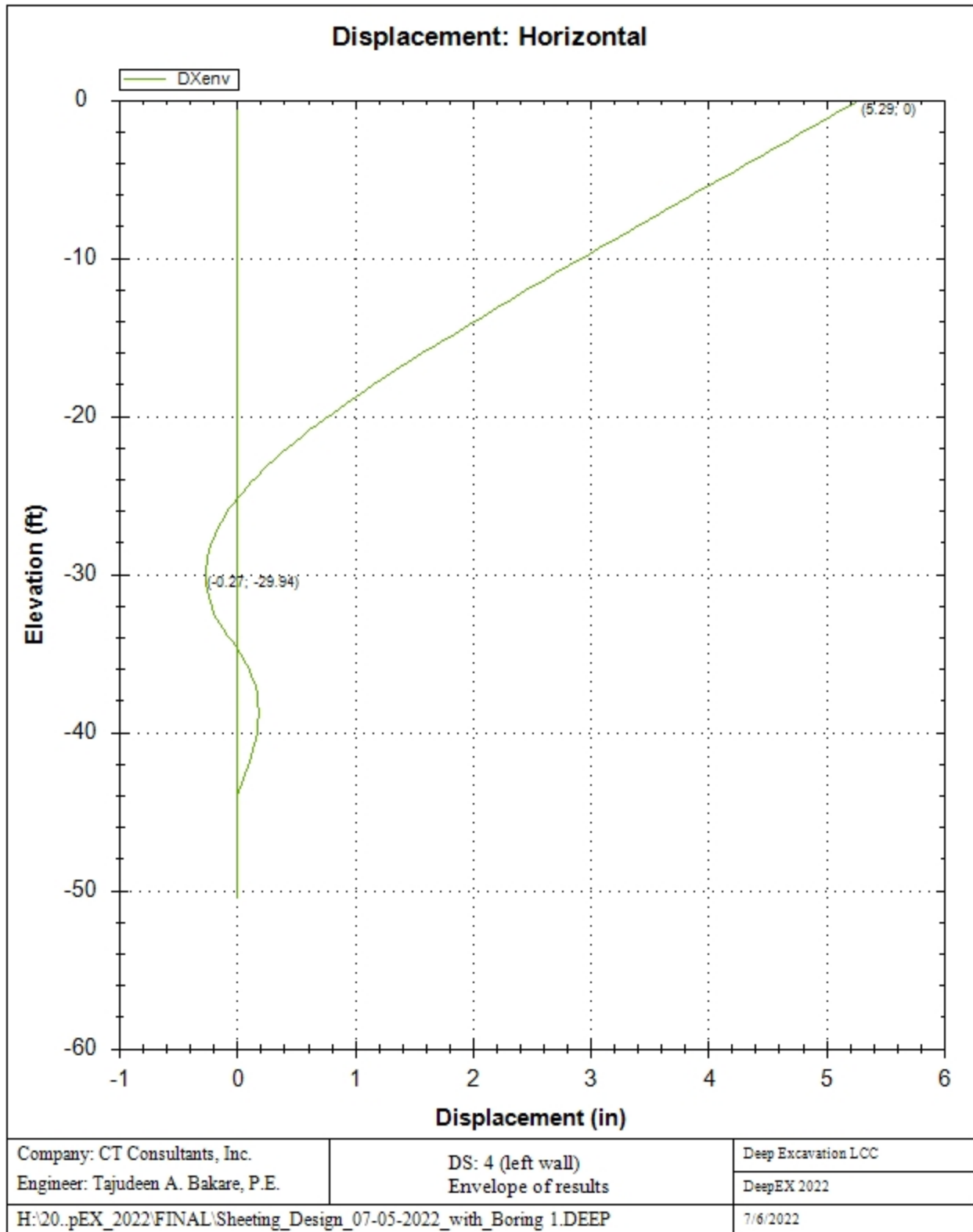
DS: 4 (left wall)  
 Envelope of results

Deep Excavation LCC  
 DeepEX 2022

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7/6/2022





Extended vs Stage

	Calculation Result	Wall Displaceme (in)	Settlement (in)	Wall Moment (k-ft/ft)	Wall Moment (k-ft)
Stage 0	Calculated	0	N/A	0	0
Stage 1	Calculated	5.29	2.36	215.98	215.98

	Wall Shear (k/ft)	Wall Shear (k)	STR Combined Wall Ratio	STR Moment Wall Ratio	STR Shear Wall Ratio
Stage 0	0	0	0	0	0
Stage 1	43.57	43.57	0.94	0.94	0.267

Table notes:

STR Combined: Combined stress check, along eccentricity line considering axial load and moment (demand/capacity).

STR Moment : Moment stress check, assuming constant axial load on wall (demand/capacity).

STR Shear : Shear stress check (shear force demand/wall shear capacity).

	Max Support Reaction (k/ft)	Max Support Reaction (k)	Critical Support Check	STR Support Ratio	Support Geotech Capacity Ratio (pull out)
Stage 0	0	0	N/A	No supports	No supports
Stage 1	0	0	N/A	No supports	No supports

Table notes:

STR Support ratio: Critical structural stress check for support (force demand/structural capacity).

Support geotech capacity ratio: Critical geotechnical capacity stress check (demand/geotechnical capacity).

Critical support check: Critical demand/design capacity ratio (structural or geotechnical).

	FS Basal	Toe FS Passive	Toe FS Rotation	Toe FS Length	Zcut (nonlinear)	FS Mobilized Passive	FS True/Active
Stage 0	1000	10.838	10.132	140.278	N/A	N/A	N/A
Stage 1	N/A	N/A	1.387	1.259	N/A	N/A	N/A

	Hydraulic Heave FS	Qflow (ft3/hr)	FSslope
Stage 0	2.729	N/A	N/C
Stage 1	1.821	N/A	3.266

#### Support Force/S vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

#### Support Force vs Stage

#### Support Force vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

#### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	10.132	10.838	10.132	140.278	N/A	N/A
0:Stage 0	1.259	N/A	1.387	1.259	N/A	N/A

Table notes:

FSbasal : Critical basal stability safety factor (relevant only when soft clays are present beneath the excavation).

Wall embedment safety factors from conventional analysis (limit-equilibrium):

FS1 Passive : Safety factor for wall embedment based on FS= Available horizontal thrust resistance/Driving hor. thrust.

FS2 Rotation: Safety factor for wall embedment based on FS= Available resisting moment/Driving moment.

FS3 Length : Safety factor for wall embedment based on FS= Available wall embedment/Required embedment for FS=1.0

Wall embedment safety factors from non-linear analysis:

FS4 Mobilized Passive : Safety factor= Available horizontal passive resistance/Mobilized passive thrust.



FS5 True/Active : Soil thrust on retained wall side/Minimum theoretically horizontal active force thrust.

Tables for stress checks follow: Support force/Design capacity

Support Check vs Stage

	No Supports
0:Stage 0	No support
1:Stage 1	

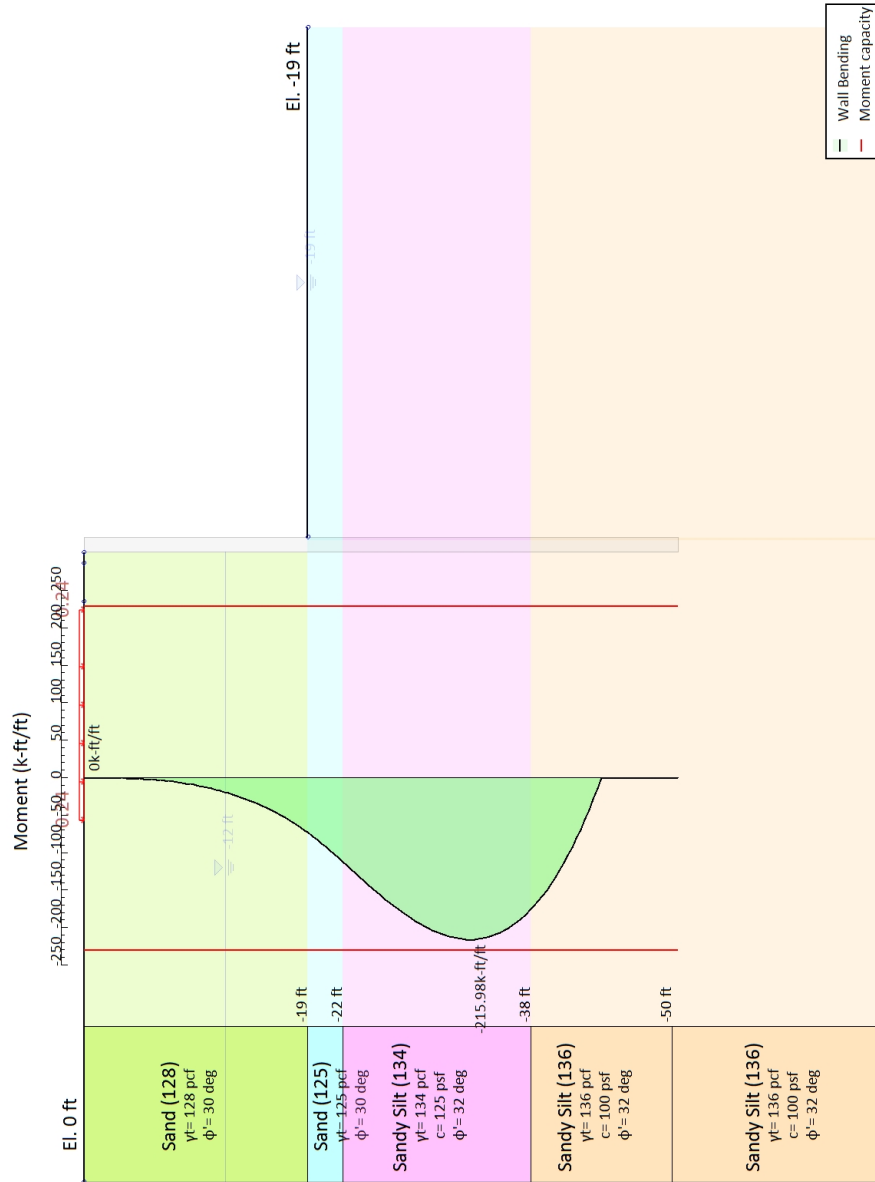
Forces (Res. F, M/Drive F, M)

	FS1 Passive (FxResist/FxDrive)	FS2 Rotation (Mresist/Mdrive)	FS3 Length (Embedment/ToeFS=1)	FS4 Mobilized Passive (FxPassive/FxPas_Mobili)	FS5 Actual Drive / Theory Active	Fh EQ Soil	Fh EQ Water
Stage 0	446.702/41.215	7920.69/781.78	50.5/0.36	N/A	N/A	N/A	N/A
Stage 1	N/A	1451.85/613.17	31.5/25.01	N/A	N/A	N/A	N/A

Reinforcement Requirements

	Parameter Description
Note:	Wall does not use steel reinforcement. Section does not apply.

O: AASHTO LRFD (2010): Strength II(PARENT: Culvert at STA. 253+86 Shoring (Service Loads))



O LRFD 8 (2018), Case: Strength II  
 FS(tanFR)= 1, FS c= 1, FS Su= 1  
 1, gDStab= 1, FSres= 1.33, FSdriveE= 1.35  
 s'A: Temp= 1.35, Perm= 1.35, EQ= 0  
 FS\_Drive= 1, FS\_Res= 1, HYDgDStab = 1, HYDgStab = 1  
 fs'R: Temp= 1, Perm= 1.11

Company: CT Consultants, Inc.

Engineer: Tajudeen A. Bakare, P.E.

H:\20..pEX\_2022\FINAL\Sheeting\_Design\_07-05-2022\_with\_Boring 1.DEEP

Quick summary

Deep Excavation LCC

DeepEX 2022

7/6/2022

## Summary of Wall Moments and Toe Requirements

Top Wall (ft)	Wall Section	L-Wall (ft)	H-Exc. (ft)	Max+M/Cap (k-ft/ft)	Max-M/Cap (k-ft/ft)	FS Toe Passive	FS Toe Rotation	FS Toe Embedment	FS 1 Toe EL. (ft)	Slope Stab. FS
0	Wall section	50.5	19	0/229.88	215.98/229.88	10.838	1.387	1.259	-44.01	3.266

## Summary of Basal Stability and Predicted Wall Movements According to Clough 1989 Method Wall: W

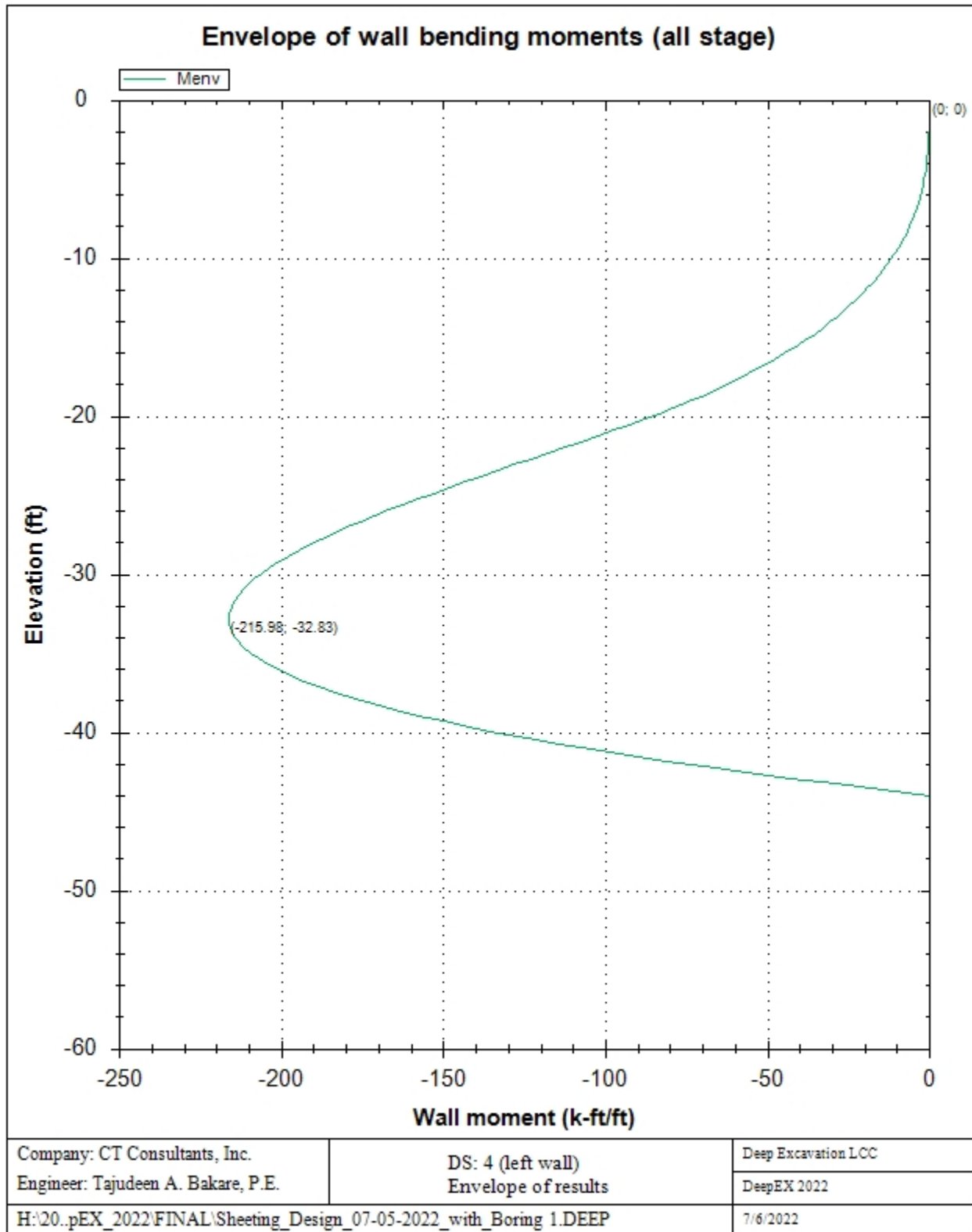
1. FSmin @ stage 0	2. DxMax (in) @ stage 1	2. Stiffness @ DxMax	2. FSbasal @ DxMax	3. Dx/H (%) @ stage 1	3. Stiffness @ Dx/H max	3. FSbasal @ Dx/H max
1000	0.857	12.4	3.266	0.376	12.449	3.266

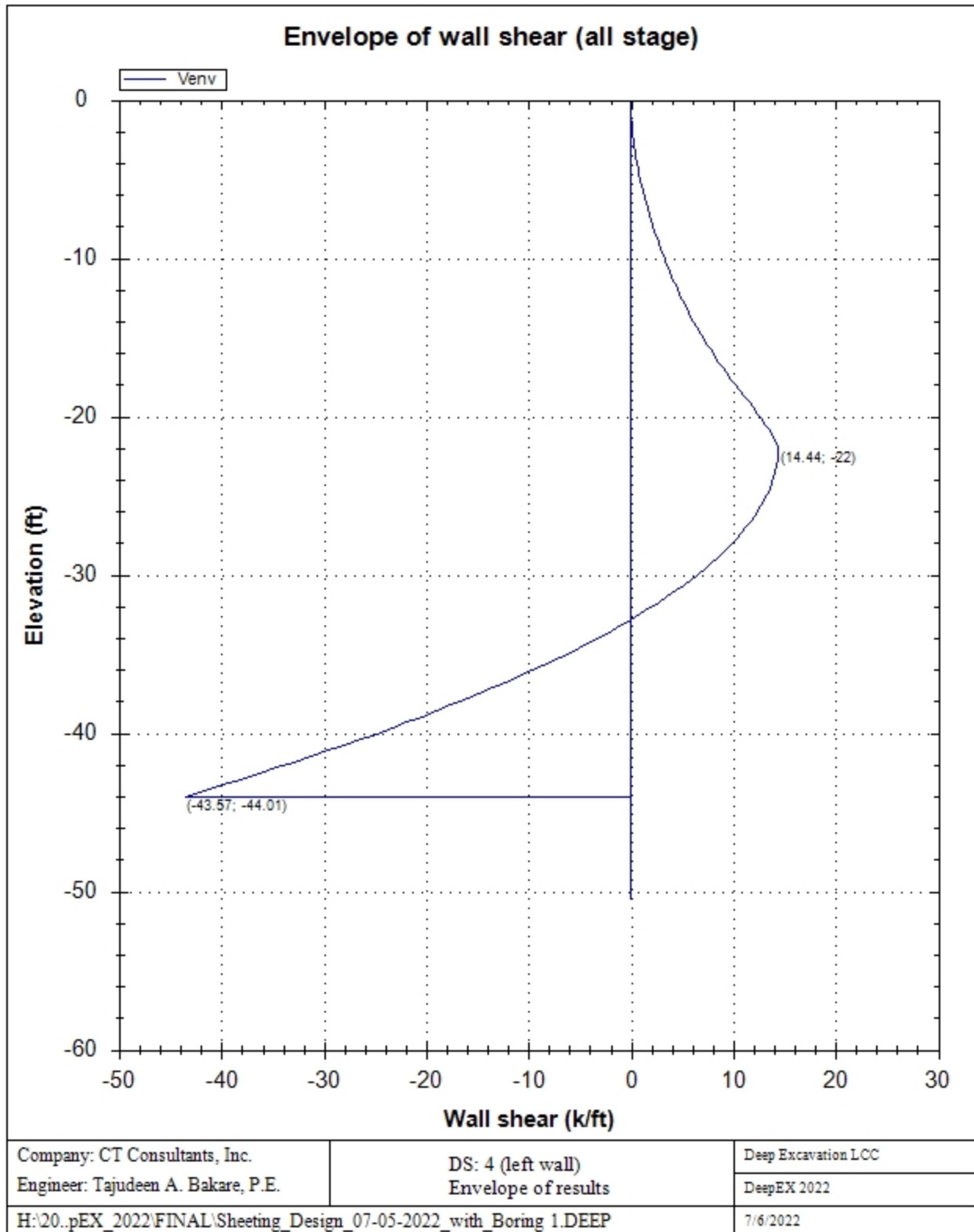
## General assumptions for last stage: Stage 1

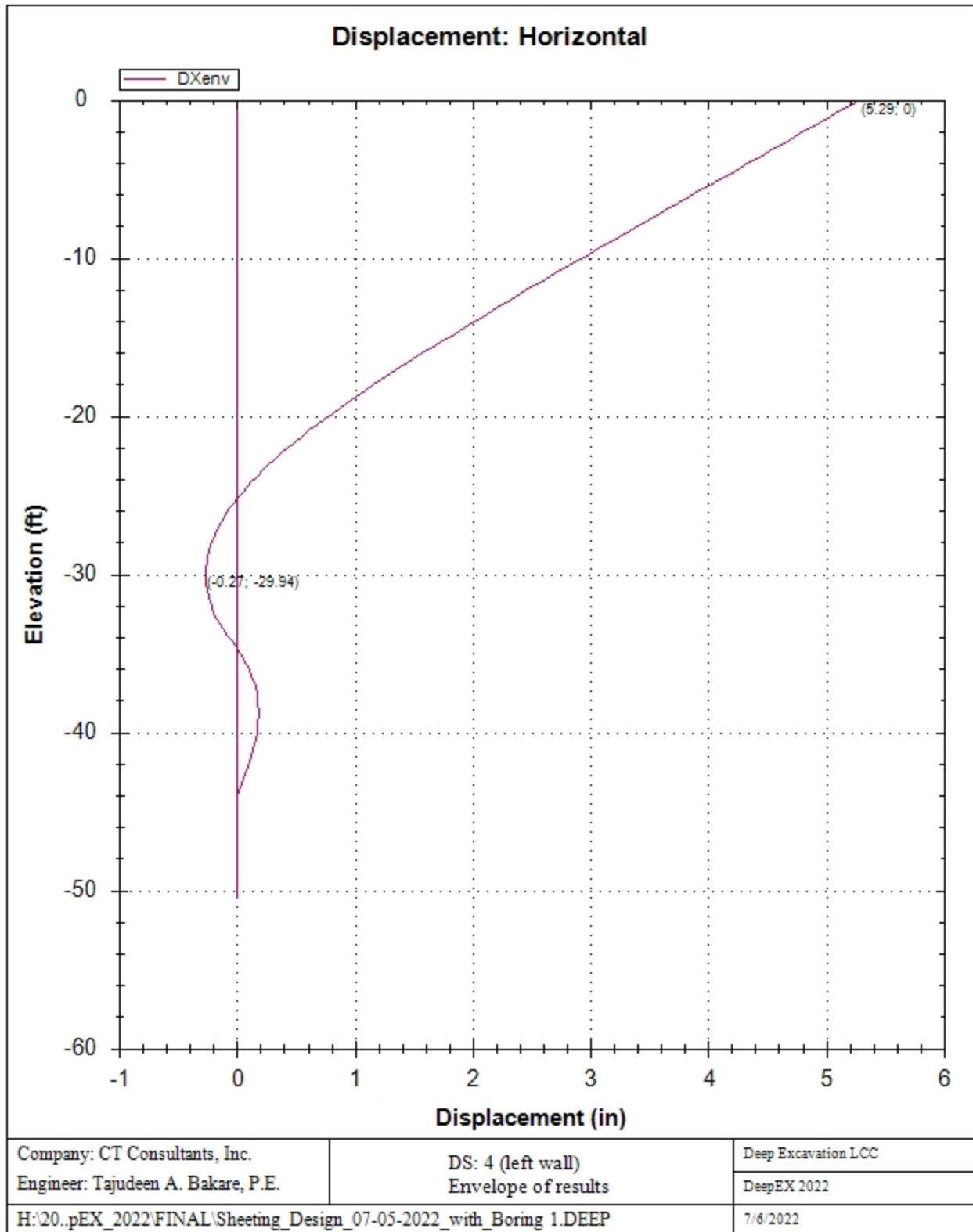
Concrete Code:	ACI 318-19
Steel Code:	ANSI/AISC 360-10
1st Wall Limit Equilibrium	California Shoring Manual-11
Negative moment	20%:
Drain State Clays	Default
Water $\gamma = 62.4$ pcf	Simple flow
Drive	$K_a, + \delta$ -Coul
Resist	$K_p, + \delta$ -Coul

### Envelope of results

A sequence of result diagrams for each excavation stage is reported







**DESIGN APPROACHES AND COMBINATION FACTORS**

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

- Ftan fr=mult factor for friction angle
- F C'= safety factor on effective cohesion (Eurocode 7 methods)
- F Su'= safety factof for undrained shear strength (Eurocode 7 methods)
- F EQ= Load factor for seismic loads
- F perm load= Load factor for permanent loads (dead load, etc)
- F temp load= Load factor on live loads and other temporary loads
- F perm supp= Reduction factor for resistance for pull out checking of permanent tiebacks
- F temp supp= Reduction factor for resistance for pull out checking of temporary tiebacks
- F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)
- F earth stab= Safety factor for passive pressures, favorable (on excavation side)
- F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable
- F GWT stab (ground water)= Load factor for resisting water pressure, favorable
- F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)
- F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)
- F UPL Dstab= Load factor for uplift check, unfavorable
- F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan	F	F	F	F(perm	F(temp	F(perm	F(temp	F Earth	F Earth	F GWT	F GWT	F HYD	F HYD	F UPL	F UPL
	Name		fr)	(c')	(Su)	(EQ)	load)	load)	sup)	sup)	(Dstab)	(stab)	(Dstab)	(stab)	(Dstab)	(stab)	(Dstab)	(stab)
0	AASHTO LRFD	Strength II	1	1	1	0	1.35	1.35	1.11	1	1.35	1.33	1	1	1	1	1	1
1	AASHTO LRFD	Strength II	1	1	1	0	1.35	1.35	1.11	1	1.35	1.33	1	1	1	1	1	1

## DESIGN APPROACHES AND COMBINATION FACTORS

The Design Approaches (from Codes or Customized by the user) and related safety factors are the following:

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- F C'= safety factor on effective cohesion (Eurocode 7 methods)
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- F EQ= Load factor for seismic loads
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- F temp load= Load factor on live loads and other temporary loads
- F perm supp= Reduction factor for resistance for pull out checking of permanent tiebacks
- F temp supp= Reduction factor for resistance for pull out checking of temporary tiebacks
- F earth Dstab= Load factor for driving earth pressures, unfavorable (on retained side)
- F earth stab= Safety factor for passive pressures, favorable (on excavation side)
- F GWT Dstab (ground water)= Load factor for driving water pressures, unfavorable
- F GWT stab (ground water)= Load factor for resisting water pressure, favorable
- F HYD Dstab= Load factor for hydraulic heave, unfavorable (hydraulic checking)
- F HYD stab= Resistance factor for hydraulic heave, favorable (hydraulic checking)
- F UPL Dstab= Load factor for uplift check, unfavorable
- F UPL stab= Resistance factor for uplift check, favorable

Stage	Design Code	Design Case	F(tan	F	F	F	F(perm	F(temp	F(perm	F(temp	F Earth	F Earth	F GWT	F GWT	F HYD	F HYD	F UPL	F UPL
	Name		fr)	(c')	(Su)	(EQ)	load)	load)	sup)	sup)	(Dstab)	(stab)	(Dstab)	(stab)	(Dstab)	(stab)	(Dstab)	(stab)
0	AASHTO LRFD	Strength II	1	1	1	0	1.35	1.35	1.11	1	1.35	1.33	1	1	1	1	1	1
1	AASHTO LRFD	Strength II	1	1	1	0	1.35	1.35	1.11	1	1.35	1.33	1	1	1	1	1	1

## SOIL DATA

Name	g tot	g dry	Frict	C'	Su	FRp	FRcv	Eload	rEur	kAp	kPp	kAcv	kPcv	Vary	Spring	Color
	(pcf)	(pcf)	(deg)	(psf)	(psf)	(deg)	(deg)	(ksf)	(-)	NL	NL	NL	NL		Model	
Sand (128)	128	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sand (125)	125	120	30	0	N/A	N/A	N/A	300	3	0.33	3	N/A	N/A	True	Linear	
Sandy Silt (13)	134	134	32	125	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	
Sandy Silt (13)	136	136	32	100	N/A	N/A	N/A	400	3	0.31	3.26	N/A	N/A	True	Linear	

Name	Poisson	Min Ka	Min sh	ko.NC	nOCR	aH.EXP	aV.EXP	qSkin	qNails	kS.nails	PL
	v	(clays)	(clays)	-	-	(0 to 1)	(0 to 1)	(psi)	(psi)	(k/ft3)	(ksi)
Sand (128)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sand (125)	0.35	-	-	0.5	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-
Sandy Silt (13)	0.4	-	-	0.47	0.8	-	-	0	0	0	-

gtot = total soil specific weight

gdry = dry weight of the soil

Frict = friction angle

C' = effective cohesion

Su = Undrained shear strength (only for CLAY soils in undrained conditions, used as a cutoff strength in NL analysis)

Evc = Virgin compression elastic modulus

Eur = unloading/reloading elastic modulus

Kap = Peak active thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kpp = Peak passive thrust coefficient (initial value, may be modified on each stage according to analysis settings).

Kacv = Constant volume active thrust coeff (only for clays, initial value)

Kpcv = Constant volume passive thrust coeff (only for clays, initial value).

Spring models= spring model (LIN= constant E over the soil layer height , EXP=exponential , SIMC=simplified winkler)

LIN= Linear-Elastic-Perfectly Plastic,

EXP: Exponential, SUB: Modulus of Subgrade Reaction

SIMC= Simplified Clay mode

## **SOIL BORINGS**

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Top Elev= superior SOil level

Soil type= type of the soil (sand , clay , etc)

OCR= overconsolidation ratio

K0= at rest coefficient

Name: Boring B-016-1-19, pos: (0, 0)

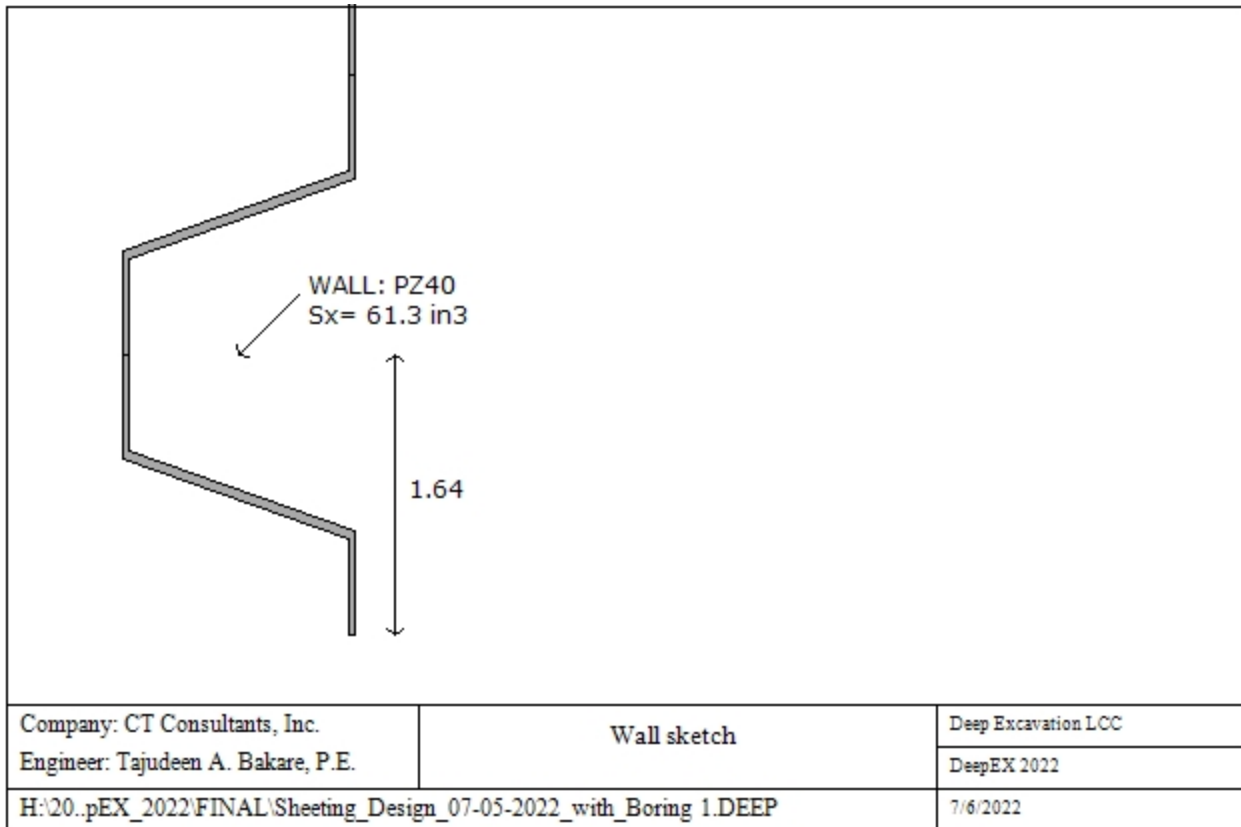
Top elev.	Soil type	OCR	Ko
0	Sand (128)	1	0.5
-19	Sand (125)	1	0.5
-22	Sandy Silt (134)	1	0.47
-38	Sandy Silt (136)	1	0.47
-50	Sandy Silt (136)	1	0.47

## **WALL DATA**

---

Wall section 0: Wall section 0





Wall type: Steel sheet piling  
 Top wall El: 0 ft Bottom wall El: -50.5 ft  
 Hor. wall spacing: 1 ft Wall thickness = 1.37 ft  
 Passive width below exc: 1 ft Active width below exc: 1 ft Swater= 1 ft  
 Steel members fy = 50 ksi Esteel = 29000 ksi  
 Wall friction: Constant value = 17 degrees  
 Steel wall capacities are calculated with ANSI/AISC 360-10  
 Concrete capacities are calculated with ACI 318-19  
 Note: With ultimate capacities you may have to use a structural safety factor.  
 Steel sheet pile properties

Table: Steel Sheet Pile Cross Sectional Properties

DES	Shape	W	A	h	t	b	s	Ixx	Sxx
		(plf)	(in <sup>2</sup> /ft)	(in)	(in)	(in)	(in)	(in <sup>4</sup> /ft)	(in <sup>3</sup> /ft)
PZ40	Z	65.6	11.75	16.4	0.5	19.69	0.605	503	61.3

GENERAL WALL DATA

Hor wall spacing= Wall horizontal spacing  
 Passive width below exc= spacing for passive thrust pressure for classic analysis  
 f'c=fck= cylindrical concrete resistance  
 fyk=fyk= steel rebar characteristic resistance  
 Econc= Concrete Elastic modulus  
 fctk= characteristic Concrete tension  
 Esteel= steel elastic modulus  
 TABULAR DATA (principal parameters)  
 1) Diaphragm wall (rectangular cross section)  
 N/A= data not available  
 Fy=fyk

$F'c=fck$

$D$ =wall thickness

$B$ =wall width

2)Steel sheet pile

$DES$ =shape (Z or U)

$W$ =width per unit of length

$A$ =area

$h$ =height

$t$ =horizontal part thickness

$b$ =width of the single sheet pile part

$s$ =inclined part thickness

$I_{xx}$ =strong axis inertia (per unit of length)

$S_{xx}$ =strong axis section modulus (per unit of length)

3)Secant piles wall, Tangent piles wall, soldier piles, soldier piles and timber lagging

$W$ =weight per unit of length

$A$ =area

$D$ =diameter

$t_w$ =web thickness

$t_p$ = pipe thickness

$b_f$ =flange width

$t_f$ = flange thickness

$k$ = flange thickness+stem base height

$I_{xx}$ = strong axis inertia modulus (per unit of length)

$S_{xx}$ = strong axis section modulus (per unit of length)

$r_x$ =radius of gyration about X axis

$r_y$ =radius of gyration about Y axis

$I_{yy}$ =weak axis inertia modulus (per unit of length)

$S_{yy}$ =weak axis section modulus (per unit of length)

$r_T$ =radius of gyration for torsion

$C_w$ = warping constant

## GENERAL ANALYSIS CRITERIA

### Summary of stage assumptions

Name	Analysis	Drive	ka-Mult	Htr T/B	Resist	Res	Contle
	Method	Press		(%)	Press	Mult	Method
Stage 0	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth
Stage 1	Conventional	Ka+ $\delta$	N/A	N/A	Kp+ d	N/A	Free Earth

Name	Support	Axial	Used	Min Toe	Toe	Toe
	Model	Incl	FSwall	FDtoe	FSrot	FSpas
Stage 0		N/A	1	10.132	10.132	10.838
Stage 1		N/A	1	1.259	1.387	N/A

Name=excavation stage name

Analysis method

springs = Elastoplastic spring analysis used

DR = Drained condition for CLAY model

U = Undrained condition for CLAY model for all the soils

Up = Undrained condition just for selected soil

Limit equilibrium analysis settings

Drive press:

Ka (Active pressure diagram), Ka-Trap = Trapezoid apparent diagram from active pressures x multiplier, FHWA= Federal Highway Administration apparent pressure diagrams.

Ko = At-rest lateral earth pressures.

Peck = Peck 1969 Apparent earth pressure diagrams.

2 Step rect = Two step rectangular apparent earth pressure diagram.

User def. = User defined apparent earth pressure diagram.

Ka+d (and so on) indicates that wall friction is applied

ka mult = multiplication factor for Ka when Ka-Trap is selected

Htr T/B (%) = trapezoidal pressure scheme, top and bottom triangular percentage of excavation depth H

Resit press = Kp (passive earth pressures)

Res Mult = Safety factor applied directly on resisting pressures (

COntle Method = cantilever analysis method for limit equilibrium analysis.

Support Model: Method for calculating support reactions in limit-equilibrium analysis.

Beam= support reactions beam analysis (uses Blum's method).

Trib= support reactions from tributary height calculations (Can be applied with apparent diagrams).

Axial Incl = Axial loads included for structural design

Used FS wall = Safety factor for axial+bending wall resistance to divide ultimate wall capacities.

Min FD Toe= embedded minimum safety factor (for limit equilibrium analysis)

Toe FS rot= rotation safety factor (classic for limit equilibrium analysis)

Toe FSpas= driving/resisting pressure safety factor (for limit equilibrium analysis)

## EXCAVATION STAGES SKETCHES

A sequence of figures for each excavation stage is reported

### Toe stability

#### Embedment FS vs Stage

	Min Toe FS	FS1 Passive	FS2 Rotation	FS3 Length (from FS1, FS2)	FS4 Mobilized Passive	FS5 Actual Drive Thrust / Theory
Stage 0	10.132	10.838	10.132	140.278	N/A	N/A
Stage 1	1.259	N/A	1.387	1.259	N/A	N/A

Legend: Wall embedment safety factors (toe)

Min Toe FS= Minimum wall embedment safety factor (from all analysis methods)

Limit-equilibrium analysis methods: The following safety factors may not be applicable for all stages.

FS1 Passive: Horizontal force safety factor, FS1= Resisting/Driving force

FS2 Rotation: Rotational safety factor about lowest support, FS2= Resisting moment/Driving moment

FS3 Length (from FS1, FS2): Program determines maximum required wall embedment for safety factor of 1 for methods

FS1 and FS2 (say length LFS1). Then FS length= Provided wall embedment/LFS1.

Non-linear elastoplastic analysis safety factors:

FS4 Mobilized Passive: Safety factor on mobilized passive resistance, FS4= Available passive soil resistance/Mobilized passive soil force on excavation side.

FS5 Active Drive Thrust/Theory Active: Ratio of soil thrust on retained side/ Active condition theoretical minimum thrust.

This factor is not as critical, and indicates how close to active conditions the model is.

General recommendations on wall embedment (excluding FS5):

When then excavation is designed with allowable standards, engineers generally use minimum safety factors from 1.2 to 1.5 depending on the level of confidence. A minimum safety factor of 1.2 is generally applied on FS3.

With ultimate limit state designs (such as Eurocode 7, and LRFD) the required safety factor must generally be greater than 1.0. In non-linear solutions it might be impossible to achieve exactly 1 on FS4 as this would likely trigger overall failure.

## **Result diagrams (for walls)**

A sequence of result diagrams for each excavation stage is reported

## **WALL RESULTS TABLE**

LEGEND

Wall node=number of the node (0 at top)

EL= Node elevation

Sht L=Total horizontal soil pressure (on the left side of the wall)

Sht R=Total horizontal soil pressure (on the right side of the wall)

Shs L=Effective horizontal soil pressure (on the left side of the wall)

Shs R=Effective horizontal soil pressure (on the right side of the wall)

q=pressure given by the surcharge

U L= Water pressure (on the left side of the wall)

U R= Water pressure (on the right side of the wall)

M=bending moment (per unit length)

V=shear (per unit length)

dx=wall deflection

McapL=Ultimate bending moment (on the left side of the wall)

McapR=Ultimate bending moment (on the right side of the wall)

VcapL=Ultimate resistance shear (on the left side of the wall)

VcapR=Ultimate resistance shear (on the right side of the wall)

## **EXCAVATION STAGES AND SLOPE STABILITY**

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Reports a sequence of figures for each stage with slope stability results.

**SLOPE STABILITY ANALYSIS: SLICE RESULTS ALL STAGES**

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Slope stability analysis design section: 0: AASHTO LRFD (2010): Strength II

**LEGEND**

x1 = Left x coordinate

ZsL= Left slice bottom elevation

ZtL= Left top elevation

x2 = Right x coordinate

ZsR= Right slice bottom elevation

ZtR= Right top elevation

DL = Slice base width

an = Base angle

Fr = Average friction angle at base

c = Average cohesion at base (may include undrained clay strengths)

Wn = Total slice weight

ubL= Water pressure at left bottom point

ubR= Water pressure at right bottom point

tBase= Base shear resistance

Nr = Effective normal reaction at bottom of slice

EiL= Lateral interslice force on left face

EiR= Lateral interslice force on right face

TL = Vertical interslice shear on left vertical face

TR = Vertical interslice shear on right vertical face

UbF= Normal water force at slice base