

July 25, 2007

Michael D. Weeks, P.E., P.S. TranSystems Corporation 5747 Perimeter Drive, Suite 240 Dublin, OH 43017

Re: Bearing Capacity and Settlement Evaluation

(Culvert at STA. 364+36)

SCI-823-0.00 Portsmouth Bypass DLZ Job No.: 0121-3070.03

Document #0060

Dear Mr. Weeks:

This letter presents the findings of preliminary evaluations of the proposed culvert and embankment at Station 364+36 on the above-referenced project. The findings of other culvert and embankment evaluations will be submitted in separate documents at a later date.

It is our understanding that a new culvert will be constructed at Station 364+36 for the above referenced project. The culvert will be a 72-inch Type A conduit in accordance with ODOT Item 707.03 (Structural Plate Corrugated Steel Structures). Preliminary plans indicate the flow line of the culvert varies from approximately 0 to 8 feet below existing grade along its alignment. It is therefore anticipated that a portion of the embankment fill will need to be placed prior to excavating for construction of the culvert (ODOT CMS Item 603.05 Method B). The maximum cover over the culvert at this location is approximately 40 feet. The inlet and outlet of the culvert will be supported by headwalls flush with the face of the pipe at both ends. At the time of preparing this letter no further information was available regarding the proposed culvert.

It should be noted that this preliminary evaluation is based upon the findings of two culvert borings (C-5 and C-6) located along the proposed alignment of the culvert. The borings were advanced to depths ranging between 10.0 and 15.0 feet below the ground surface. Logs of the borings, a plan and profile drawing showing the approximate locations of the borings, a legend of the boring log terminology and general information regarding the drilling procedures are attached. The ground surface elevations at the boring locations were estimated from available topography maps and are reported on the logs.

## **Exploration Findings**

The borings generally encountered 3.0 to 4.0 feet of loose to very dense granular soil (A-4a) over sandstone bedrock. The bedrock was weathered and fractured to varying degrees but generally improved in quality with depth.



Michael D. Weeks, P.E., P.S. July 25, 2007 Page 2

## **General Recommendations**

Preliminary plans indicate that the invert elevations at the inlet and outlet of the culvert are 634.07 and 613.04, respectively. Based on this information and the shallow bedrock conditions encountered in the borings, it is likely that bedrock will be encountered at locations along the culvert alignment during construction. Bedrock in the conduit foundation should be removed at least 6 inches (150 mm) below the bottom of the bedding and replaced with structural backfill. Bedding should conform to the requirements of ODOT CMS Item 603.06.

# **Bearing Capacity and Settlement Evaluation**

Based on the results of the borings and the planned invert elevations at the culvert inlet and outlet, the headwall footings will bear in weathered, fractured sandstone bedrock. recommended that footings bearing in the weathered, broken sandstone be designed based on an allowable bearing capacity not greater than 10 tons per square foot (tsf). Post construction settlement of footings bearing in the rock is expected to be negligible. Since the conduit will be bedded on or near the bedrock surface, post construction settlement of the pipe is likewise anticipated to be negligible.

We appreciate having the opportunity to be of service to you on this project. Please do not hesitate to call if you have any questions concerning our preliminary findings.

Respectfully submitted,

DLZ OHIO, INC.

Wael Alkasawneh, P.E. Geotechnical Engineer

Bryan Wilson, P.E.

Krean a

Senior Geotechnical Engineer

Encl: As noted.

cc: J. Greg Brown, P.E. (TranSystems Corporation), File

# GENERAL INFORMATION DRILLING PROCEDURES AND LOGS OF BORINGS

Drilling and sampling were conducted in accordance with procedures generally recognized and accepted as standardized methods of investigation of subsurface conditions concerning geotechnical engineering considerations. Borings were drilled with either a truck-mounted or ATV-mounted drill rig.

Drive split-barrel sampling was performed in 1.5 foot increments at intervals not exceeding 5 feet. In the event the sampler encountered resistance to penetration of 6 inches or less after 50 blows of the drop hammer, the sampling increment was discontinued. Standard penetration data were recorded and one or more representative samples were preserved from each sampling increment.

In borings where rock was cored, NXM or NQ size diamond coring tools were used.

In the laboratory all samples were visually classified by a soils engineer. Moisture contents of representative fine-grained soil samples were determined. A limited number of samples, considered representative of foundation materials present, were selected for performance of grain-size analyses and plasticity characteristics tests. The results of these tests are shown on the boring logs.

The boring logs included in the Appendix have been prepared on the basis of the field record of drilling and sampling, and the results of the laboratory examination and testing of samples. Stratification lines on the boring logs indicating changes in soil stratigraphy represent depths of changes approximated by the driller, by sampling effort and recovery, and by laboratory test results. Actual depths to changes may differ somewhat from the estimated depths, or transitions may occur gradually and not be sharply defined. The boring logs presented in this report therefore contain both factual and interpretative information and are not an exact copy of the field log.

Although it is considered that the borings have disclosed information generally representative of site conditions, it should be expected that between borings conditions may occur which are not precisely represented by any one of the borings. Soil deposition processes and natural geologic forces are such that soil and rock types and conditions may change in short vertical intervals and horizontal distances.

Soil/rock samples will be stored at our laboratory for a period of six months. After this period of time, they will be discarded, unless notified to the contrary by the client.

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#### **LEGEND - BORING LOG TERMINOLOGY**

## Explanation of each column, progressing from left to right

- Depth (in feet) refers to distance below the ground surface.
- Elevation (in feet) is referenced to mean sea level, unless otherwise noted.
- Standard Penetration (N) the number of blows required to drive a 2-inch O.D., 1-3/8 inch I.D., split-barrel sampler, using a 140-pound hammer with a 30-inch free fall. The blows are recorded in 6-inch drive increments. Standard penetration resistance is determined from the total number of blows required for one foot of penetration by summing the second and third 6-inch increments of an 18-inch drive.

50/n - indicates number of blows (50) to drive a split-barrel sampler a certain number of inches (n) other than the normal 6-inch increment.

- The length of the sampler drive is indicated graphically by horizontal lines across the "Standard Penetration" and "Recovery" columns.
- Sample recovery from each drive is indicated numerically in the column headed "Recovery".
- The drive sample location is designated by the heavy vertical bar in the "Sample No., Drive" column.
- The length of hydraulically pressed "Undisturbed" samples is indicated graphically by horizontal lines across the "Press" column.
- 8. Sample numbers are designated consecutively, increasing in depth.
- 9. Soil Description
  - a. The following terms are used to describe the relative compactness and consistency of soils:

#### Granular Soils - Compactness

<u>Terms</u>	Blows/Foot Standard <u>Penetration</u>
Very Loose	0 - 4
Loose	4 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	over 50

#### Cohesive Soils - Consistency

<u>Term</u>	Unconfined Compression tons/sq.ft.	Blows/Foot Standard Penetration	Hand <u>Manipulation</u>
Very Soft less that	n 0.25	below 2	Easily penetrated by fist
Soft	0.25 - 0.50	2 - 4	Easily penetrated by thumb
Medium Stiff	0.50 - 1.00	4 - 8	Penetrated by thumb w/ moderate effort
Stiff	1.0 - 2.0	8 - 15	Readily indented by thumb but not penetrated
Very Stiff	2.0 - 4.0	15 - 30	Readily indented by thumb nail
Hard	over 4.0	over 30	Indented with difficulty by thumb nail

- b. Color If a soil is a uniform color throughout, the term is single, modified by such adjective as light and dark. If the predominant color is shaded by a secondary color, the secondary color precedes the primary color. If two major and distinct colors are swirled throughout the soil, the colors are modified by the term "mottled".
- c. Texture is based on the ODOT Classification System. Soil particle size definitions are as follows:

<u>Size</u>	Description	<u>Size</u>
Larger than 8"	Sand-Coarse	2.00 mm. to 0.42 mm.
8" to 3"	-Fine	0.42 mm. to 0.074 mm.
3" to 3/4"	Silt	0.074 mm. to 0.005 mm.
3/4" to 2.00" mm.	Clay	Smaller than 0.005 mm.
	Larger than 8" 8" to 3" 3" to 3/4"	Larger than 8" Sand-Coarse 8" to 3" -Fine 3" to 3/4" Silt

d. The main soil component is listed first. The minor components are listed in order of decreasing percentage of particle size.

e. Modifiers to main soil descriptions are indicated as a percentage by weight of particle sizes.

trace - 0 to 10% little - 10 to 20% some - 20 to 35% "and" - 35 to 50%

f. The moisture content of cohesive soils (silts and clays) is expressed relative to plastic properties.

Term Relative Moisture or Appearance

Dry Powdery

Damp Moisture content slightly below plastic limit

Wet Moisture content above liquid limit

Moisture content of cohesionless soils (sands and gravels) is described as follows:

Term Relative Moisture or Appearance

Dry No moisture present

Damp Internal moisture, but none to little surface moisture

Moist Free water on surface
Wet Voids filled with free water

Rock hardness and rock quality description.

a. The following terms are used to describe the relative hardness of the bedrock.

<u>Term</u> <u>Description</u>

Very Soft Difficult to indent with thumb nails; resembles hard soil but has rock structure

Soft Resists indentation with thumb nail but can be abraded and pierced to a shallow depth by a pencil point.

Medium Hard Resists pencil point, but can be scratched with a knife blade.

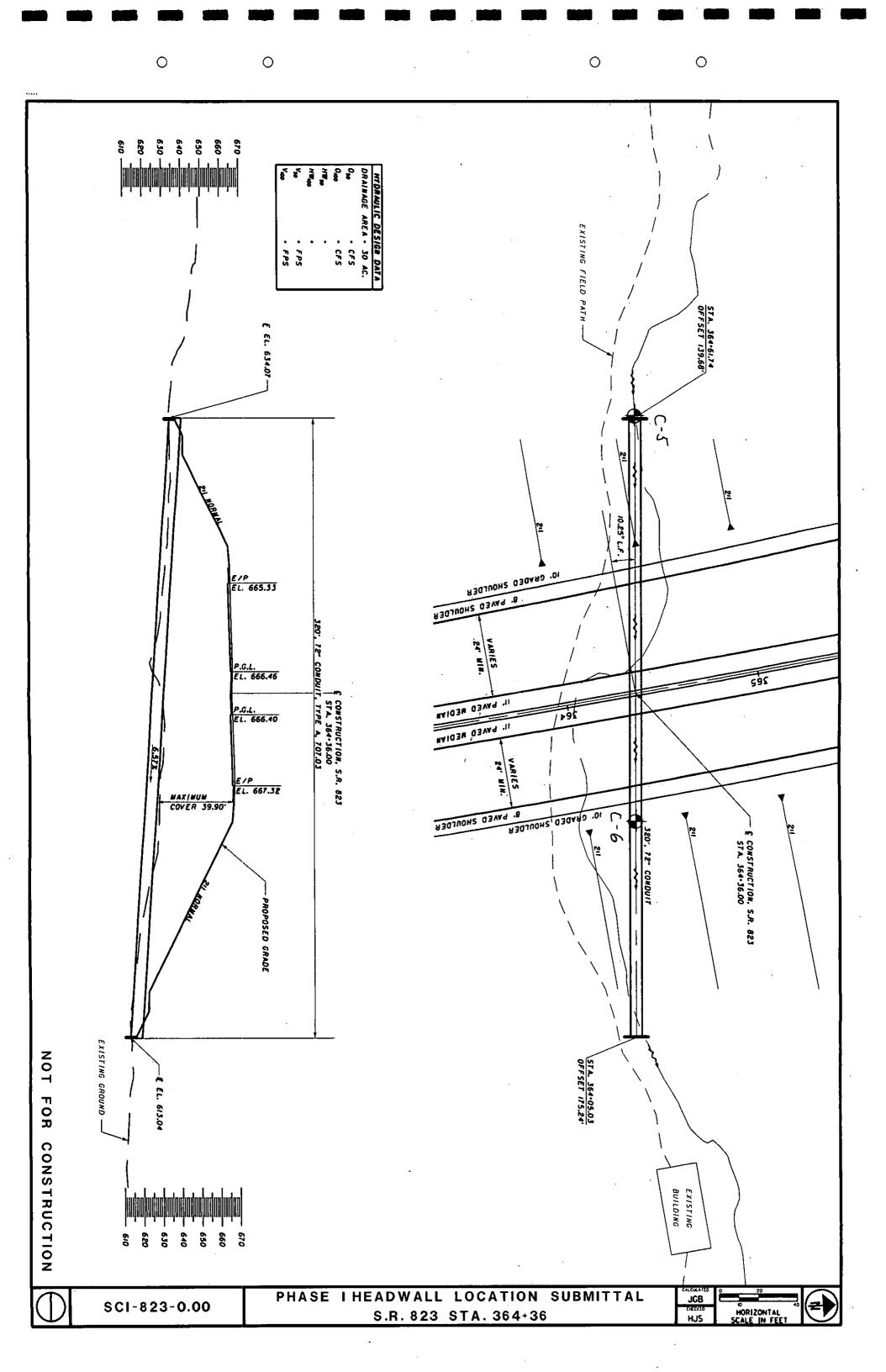
Hard Can be deformed or broken by light to moderate hammer blows.

Very Hard Can be broken only by heavy blows, and in some rocks, by repeated hammer blows.

b. Rock Quality Designation, RQD - This value is expressed in percent and is an indirect measure of rock soundness. It is obtained by summing the total length of all core pieces which are at least four inches long, and then dividing this sum by the total length of the core

- 11. Gradation when tests are performed, the percentage of each particle size is listed in the appropriate column (defined in Item 9c).
- 12. When a test is performed to determine the natural moisture content, liquid limit moisture content, or plastic limit moisture content, the moisture content is indicated graphically.
- 13. The standard penetration (N) value in blows per foot is indicated graphically.

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lient:	FranSys	stems,	Inc.				Project: SCI-823-0.00		040					Job No	. 0121-3070.03
.og o	F: Bo	ring (	2-5		_		. 364+58.5, 138.8 ft. LT of SR 823 CL Date Drilled: 0	6/09			ATIO	761			<u> </u>
Depth (ft)	Elev. (ft) 635.7	Blows per 6"	Recovery (in)	Samp No.			WATER OBSERVATIONS: Water seepage at: Not reported Water level at completion: None  DESCRIPTION	% Aggregate		M. Sand	nd	% Silt	% Clay	Natural Mois PL ⊢— Blows	D PENETRATION (N ture Content, % - LL per foot - 20 30 40
-0.2 <del></del> - - -3.0	635.5 632.7	2 7 21		1		-	Topsoil - 2" Loose to medium dense brown SANDY SILT (A-4a), some to "and" gravel, trace clay; contains sandstone fragments; damp.  Severely weathered brown SANDSTONE. (augered through								0
-5.0 <del></del>	630.7						rock)	-							
		Core 60"	Rec 57*	RQD 88%	R-1		Medium hard gray SANDSTONE; fine grained, slightly weathered, laminated to thinly bedded, moderately fractured.								
·10.0 - - -	-625.7-						Bottom of Boring - 10.0'								
15 —											:				
20 <del></del> 													-		
- 25 — - -	-														

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Client;	TranSy	stems,	Inc.				Project: SCI-823-0.00								Job No.	0121	3070.	03
	F: Bo				L	ocation: Sta	. 364+25.7, 61.6 ft. RT of SR 823 CL Date Drilled: 06	3/08	/06									
Sample No.						Hand	WATER OBSERVATIONS: Water seepage at: Not reported	_	GI	RAD	ATIC	ON						
Depth (ft)	Elev. (ft)	Blows per 6"	Recovery (in)	9,	Press / Core	Perietro- meter (tsf)	Water level at completion: 3.0'	Aggregate	C. Sand	M. Sand	Sand	Silt	Clay	Natu	ANDARD : iral Moistu PL 1 Blows pe	ıre Cont	ent, %	- •
٥	631.4	Blo	Rec	Drive	Pre		DESCRIPTION	1%	%	%	% F.	%	%		10 20			0
0.3  	631.1-	9 5 50/2	7	1			Topsoil - 4"  Very dense brown SANDY SILT (A-4a), trace clay, trace gravel; contains roots; moist.	5	22		19	46	8		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	Ņon	-Plastig
4.0 5 -	627.4-						Medium hard brown and gray SANDSTONE; very fine to fine grained, moderately weathered, argillaceous, thinly laminated to thinly bedded, highly fractured.	- } 				:			1 1 4 7 1 1 4 7 1 1 5 1 1 1 1 5 1 1 1 1 1 1 1 2 5 1 5 1 2 5 1 1 1	1 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1		2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
8.0— 10—	623.4	Core 120"	Rec 113"	RQD 66%	R-1		Medium hard to hard gray SANDSTONE; very fine to fine grained, unweathered to slightly weathered, argillaceous, thinly laminated to medium bedded, moderately fractured.  @ 11.6'-12.1', highly fractured.							1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		
- - 15.0	616.4-	Core 12"	Rec 12"	RQD 75%,	R-2		Bottom of Boring - 15.0'											
- - 20 —														1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1				
- - 25 —	- - - -					·									1000		1111	1 1 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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