

August 14, 2007

Michael D. Weeks, P.E., P.S. TranSystems Corporation 5747 Perimeter Drive, Suite 240 Dublin, OH 43017

Re: Bearing Capacity and Settlement Evaluation

(Culvert at STA. 868+91)

SCI-823-0.00 Portsmouth Bypass DLZ Job No.: 0121-3070.03

Document #0074

Dear Mr. Weeks:

This letter includes the findings of the preliminary evaluation of the proposed culvert at Station 868+91 on the above-referenced project. The findings of other culvert evaluations will be submitted in separate documents.

It is our understanding that a new culvert will be constructed at Station 868+91 for the above referenced project. The culvert will be a 42-inch Type A conduit in accordance with ODOT Item 707.01 (Metallic Coated Corrugated Steel Conduits and Underdrains). The culvert will be installed using cut and fill construction procedures then an embankment up to approximately 23 ft high will be built over the culvert. The inlet and outlet of the culvert will be supported by headwalls flush with the face of the pipe at both ends. At the time of preparing this letter no further information was available regarding the proposed culvert.

It should be noted that the results of this evaluation are based upon the findings of three borings (C-64 through C-66) located along the proposed alignment of the culvert. The borings were advanced to depths ranging between 14 and 27.5 feet below the ground surface. Logs of the borings, a plan and profile drawing showing the approximate locations of the borings, a legend of the boring log terminology and general information regarding the drilling procedures are attached. The surveyed ground elevations at the boring locations are reported on the logs.

Exploration Findings

The borings generally encountered 3.0 feet of soil overlying decomposed sandstone and shale bedrock. The overburden soil consisted of very soft to stiff, wet silt (A-4b). The decomposed rock extended to depths of 9.0 to 22.5 feet where more competent sandstone and shale was encountered. The bedrock at depth was generally medium hard, slightly weathered and slightly fractured to unfractured.



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General Recommendations

Preliminary plans indicate that the invert elevations at the inlet and outlet of the culvert are 650.23 and 631.40, respectively. Based on this information and the shallow bedrock conditions encountered in the borings, it is possible that weathered/decomposed bedrock could be encountered at locations along the culvert alignment during construction. Bedrock in the conduit foundation should be removed at least 6 inches (150 mm) below the bottom of the bedding and replaced with structural backfill. Bedding should conform to the requirements of ODOT CMS Item 603.06.

Bearing Capacity Evaluation

The bottoms of the headwall footings were assumed to be 4 feet below the invert elevations to place them below the frost zone and prevent scour of the headwall (Ohio BDM Section 200). Based on the results of the borings and the proposed invert elevations, footings at these elevations will bear in decomposed bedrock. Footings bearing in the decomposed bedrock may be designed based on an allowable bearing capacity not greater than 5 tons per square foot (tsf).

The surficial wet silts are unsuitable for support of construction traffic/fill operations and will therefore need to be stripped prior to placing embankment fill. Since the conduit will be bedded in decomposed bedrock, settlement of the culvert is anticipated to be small and to occur during construction of the embankment.

We appreciate having the opportunity to be of service to you on this project. Please do not hesitate to call if you have any questions concerning our preliminary findings.

Respectfully submitted,

DLZ OHIO, INC.

Wael Alkasawneh, P.E. Geotechnical Engineer

Bryan Wilson, P.E.

Senior Geotechnical Engineer

Encl: As noted.

cc: J. Greg Brown, P.E. (TranSystems Corporation), File

GENERAL INFORMATION DRILLING PROCEDURES AND LOGS OF BORINGS

Drilling and sampling were conducted in accordance with procedures generally recognized and accepted as standardized methods of investigation of subsurface conditions concerning geotechnical engineering considerations. Borings were drilled with either a truck-mounted or ATV-mounted drill rig.

Drive split-barrel sampling was performed in 1.5 foot increments at intervals not exceeding 5 feet. In the event the sampler encountered resistance to penetration of 6 inches or less after 50 blows of the drop hammer, the sampling increment was discontinued. Standard penetration data were recorded and one or more representative samples were preserved from each sampling increment.

In borings where rock was cored, NXM or NQ size diamond coring tools were used.

In the laboratory all samples were visually classified by a soils engineer. Moisture contents of representative fine-grained soil samples were determined. A limited number of samples, considered representative of foundation materials present, were selected for performance of grain-size analyses and plasticity characteristics tests. The results of these tests are shown on the boring logs.

The boring logs included in the Appendix have been prepared on the basis of the field record of drilling and sampling, and the results of the laboratory examination and testing of samples. Stratification lines on the boring logs indicating changes in soil stratigraphy represent depths of changes approximated by the driller, by sampling effort and recovery, and by laboratory test results. Actual depths to changes may differ somewhat from the estimated depths, or transitions may occur gradually and not be sharply defined. The boring logs presented in this report therefore contain both factual and interpretative information and are not an exact copy of the field log.

Although it is considered that the borings have disclosed information generally representative of site conditions, it should be expected that between borings conditions may occur which are not precisely represented by any one of the borings. Soil deposition processes and natural geologic forces are such that soil and rock types and conditions may change in short vertical intervals and horizontal distances.

Soil/rock samples will be stored at our laboratory for a period of six months. After this period of time, they will be discarded, unless notified to the contrary by the client.

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LEGEND - BORING LOG TERMINOLOGY

Explanation of each column, progressing from left to right

- Depth (in feet) refers to distance below the ground surface.
- 2. Elevation (in feet) is referenced to mean sea level, unless otherwise noted.
- 3. Standard Penetration (N) the number of blows required to drive a 2-inch O.D., 1-3/8 inch I.D., split-barrel sampler, using a 140-pound hammer with a 30-inch free fall. The blows are recorded in 6-inch drive increments. Standard penetration resistance is determined from the total number of blows required for one foot of penetration by summing the second and third 6-inch increments of an 18-inch drive.

50/n - indicates number of blows (50) to drive a split-barrel sampler a certain number of inches (n) other than the normal 6-inch increment.

- 4. The length of the sampler drive is indicated graphically by horizontal lines across the "Standard Penetration" and "Recovery" columns.
- 5. Sample recovery from each drive is indicated numerically in the column headed "Recovery".
- 6. The drive sample location is designated by the heavy vertical bar in the "Sample No., Drive" column.
- 7. The length of hydraulically pressed "Undisturbed" samples is indicated graphically by horizontal lines across the "Press" column.
- 8. Sample numbers are designated consecutively, increasing in depth.
- 9. Soil Description
 - a. The following terms are used to describe the relative compactness and consistency of soils:

Granular Soils - Compactness

<u>Terms</u>	Blows/Foo Standard <u>Penetratio</u>
Very Loose	0 - 4
Loose	4 - 10
Medium Dense	10 - 30
Dense	30 - 50
Very Dense	over 50

Cohesive Soils - Consistency

<u>Term</u>	Unconfined Compression tons/sq.ft.	Blows/Foot Standard Penetration	Hand <u>Manipulation</u>
Very Soft less th	an 0.25	below 2	Easily penetrated by fist
Soft	0.25 - 0.50	2 - 4	Easily penetrated by thumb
Medium Stiff	0.50 - 1.00	4 - 8	Penetrated by thumb w/ moderate effort
Stiff	1.0 - 2.0	8 - 15	Readily indented by thumb but not penetrated
Very Stiff	2.0 - 4.0	15 - 30	Readily indented by thumb nail
Hard	over 4.0	over 30	Indented with difficulty by thumb nail

- b. Color If a soil is a uniform color throughout, the term is single, modified by such adjective as light and dark. If the predominant color is shaded by a secondary color, the secondary color precedes the primary color. If two major and distinct colors are swirled throughout the soil, the colors are modified by the term "mottled".
- c. Texture is based on the ODOT Classification System. Soil particle size definitions are as follows:

Description	<u>Size</u>	<u>Description</u>	<u>Size</u>
Boulders	Larger than 8"	Sand-Coarse	2.00 mm. to 0.42 mm.
Cobbles	8" to 3"	-Fine	0.42 mm. to 0.074 mm.
Gravel-Coarse	3" to 3/4"	Silt	0.074 mm. to 0.005 mm.
-Fine	3/4" to 2.00" mm.	Clay	Smaller than 0.005 mm.

d. The main soil component is tisted first. The minor components are listed in order of decreasing percentage of particle size.

e. Modifiers to main soil descriptions are indicated as a percentage by weight of particle sizes.

trace - 0 to 10% little - 10 to 20% some - 20 to 35% "and" - 35 to 50%

f. The moisture content of cohesive soils (silts and clays) is expressed relative to plastic properties.

Term Relative Moisture or Appearance

Dry Powdery

Damp Moisture content slightly below plastic limit

Moist Moisture content above plastic limit, but below liquid limit

Wet Moisture content above liquid limit

g. Moisture content of cohesionless soils (sands and gravels) is described as follows:

Term Relative Moisture or Appearance

Ory No moisture present

Damp Internal moisture, but none to little surface moisture

Moist Free water on surface
Wet Voids filled with free water

- Rock hardness and rock quality description.
 - The following terms are used to describe the relative hardness of the bedrock.

<u>Term</u> <u>Description</u>

Very Soft Difficult to indent with thumb nails; resembles hard soil but has rock structure

Soft Resists indentation with thumb nail but can be abraded and pierced to a shallow depth by a pencil point.

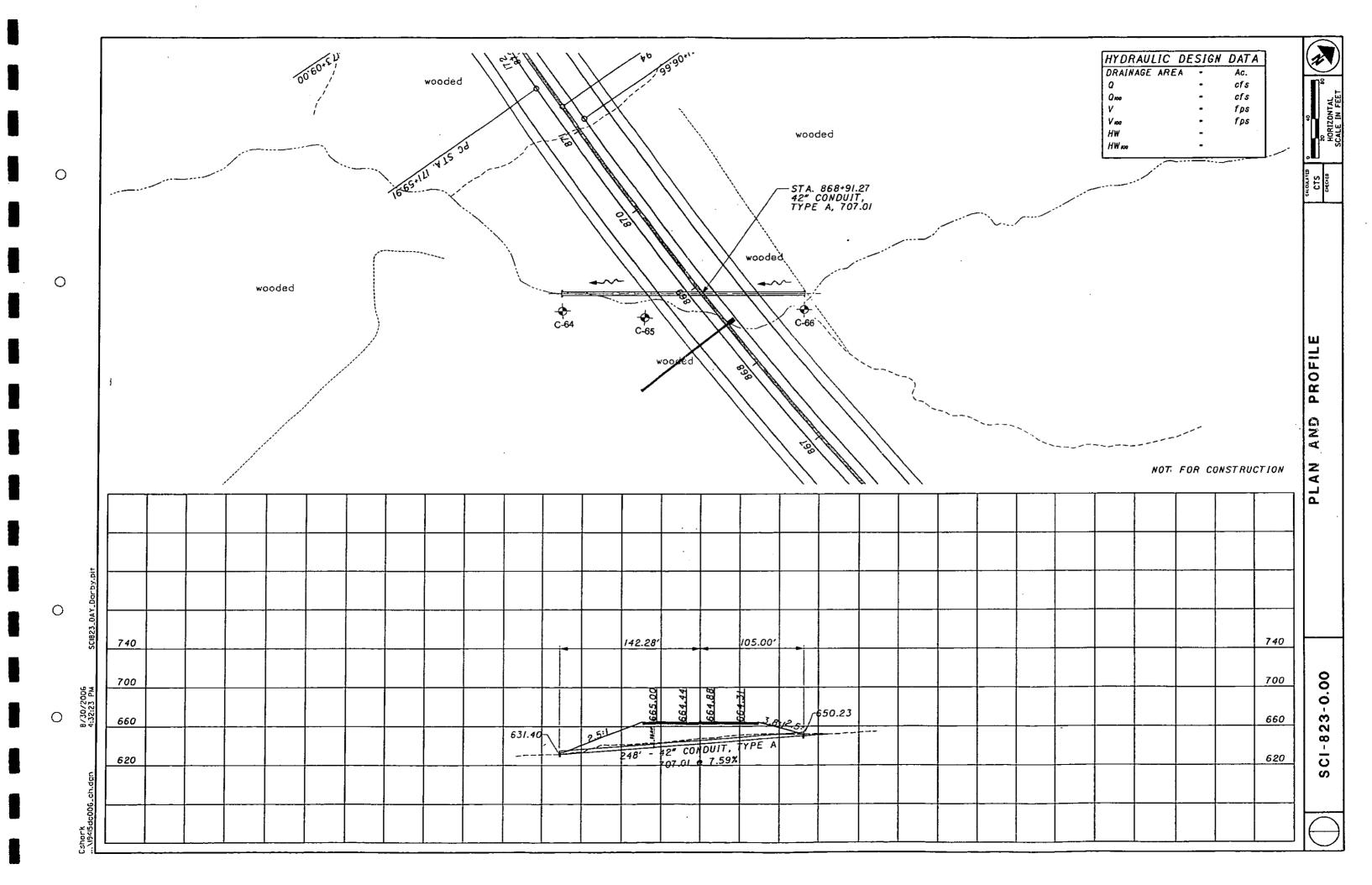
Medium Hard Resists pencil point, but can be scratched with a knife blade.

Hard Can be deformed or broken by light to moderate hammer blows.

Very Hard Can be broken only by heavy blows, and in some rocks, by repeated hammer blows.

- b. Rock Quality Designation, RQD This value is expressed in percent and is an indirect measure of rock soundness. It is obtained by summing the total length of all core pieces which are at least four inches long, and then dividing this sum by the total length of the core run.
- 11. Gradation when tests are performed, the percentage of each particle size is listed in the appropriate column (defined in Item 9c).
- 12. When a test is performed to determine the natural moisture content, liquid limit moisture content, or plastic limit moisture content, the moisture content is indicated graphically.
- 13. The standard penetration (N) value in blows per foot is indicated graphically.

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Client:	ranSv	stems.	Inc.				Project: SCI-823-0.00							Job No. 0121-3070.03
LOG C				•] L	ocation: Sta	i. 869+55.5, 124.8 ft. LT of SR 823 CL Date Drilled: 10	/10.	/06					
				Samp No		Hand	WATER OBSERVATIONS: Water seepage at: None	\vdash	GF	RAD.	ATIC	NC 		-
Depth	Elev.	per 6"	ry (in)		Core	Penetro- meter	Water level at completion: 8.9'	egate	Sand	Sand	Sand	1		STANDARD PENETRATION (N) Natural Moisture Content, % -
(ft)	(ft) 640.9	Blows p	Recovery	Drive	Press / Core	(tsf)	DESCRIPTION	% Aggregate	% C. S.		% F. S.	% Sitt	% Clay	PL
—o.3=	-640.5						Topsoil - 4"							
-		1 1	18	1		<u></u>	Very soft brown SILT (A-4b) trace fine to coarse sand trace gravel; contains organic material; moist to wet.	3	2	-	3	70	22	
3.0	637.9	3 6 6	18	2			Stiff brown SILT AND CLAY (A-6a), trace to little fine to coarse sand, trace gravel; damp.(Decomposed SHALE).	1	i					
—5.5—	635.4-	6		3			Medium dense brown GRAVEL WITH SAND (A-1-b), some silty clay; damp. (Decomposed SANDSTONE).	52	8		15	2	5	
-		12	18				clay, damp. (Decomposed OANDOTONE).						Ĭ	
10 —	† 	6 7	18_	4			.							
-		6 10 18	18	5										
15 —	627.4	12 12	18	6			Very stiff brown SILT (A-4b), little fine to coarse sand, trace gravel; damp.	4	8	-	9	56	23	
	624.9	6 17 21	18	7			Medium dense brown GRAVEL WITH SAND (A-1-b), some silty clay; damp. (Decomposed SANDSTONE).	7						
20 —	-	2 15 30	18	8	ļ									δ
22 5	- 610 4	6 15 50/3	15	9] .						50+1
25 —	 6 18.4-	Core 60"	Rec 60"	RQD 98%	R1		Medium hard gray SHALE; slightly to moderately weathered, micaceous, thinly laminated, slightly fractured.							30°C
25 — —27.5—	613.4				-		Bottom of Boring - 27.5'	1						
30							201.011 01 201.11,g 21 1.0							1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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Client: T	ranSys	stems,	Inc.				Project: SCI-823-0.00								Job No.	121-307	0.03
LOG O	F: Bo	ring (C-65		L	ocation: Sta	. 869+10.9, 17.0 ft. LT of SR 823 CL Date Drilled: 10	/10/	_					,			
Depth	Elev.	er 6*	ry (in)	Samp No.		Hand Penetro- meter	WATER OBSERVATIONS: Water seepage at, None Water level at completion: 2.2'	egate	Sand	Sand	Sand	ON.		Natu	ANDARD P	Content,	% - •
(ft)	<i>(ft)</i> 646.1	Blows per 6	Recovery	Drive	Press / Core	(tsf)	DESCRIPTION	% Aggregat	ن		% F. S.	% Sit	% Clay	<i>P</i>	PL	foot - 30	LL) <u>40</u>
-		WOH 1	6	1			Topsoil - 2" Very soft to soft brown SILT (A-4b), trace fine to coarse sand; contains organic material; wet.	0	2	-	3	75	20	Q.		· · · · · · · · · · · · · · · · · · ·	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
3.0 5	-6 43.1 -	4 5 11	18	2			Very stiff brown SANDY SILT (A-4a), little to some fine to coarse sand, trace to little gravel; damp. (Decomposed SHALE).									1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
- - 8.0	638.1-	8 12 13	18	3		-		12	10	_	8	48	22	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		<u></u>	
10 —		8 9 50/3	15	4		4.5+	Hard brown and gray SILT AND CLAY (A-6a), trace to little fine to coarse sand, trace gravel; damp.(Decomposed SHALE).							5 1 7 1 6 1 6 1 5 1 6 1 7 1 7 1	1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		50+
11.0 11.5	-635.1 - 634.6-	50/5_	3	_ 5			Severely weathered brown SANDSTONE.	1									50+
 15		Core 60"	Rec 60"	RQD 96%	R1		Medium hard gray SANDSTONE; very fine to fine grained, slightly weathered, micaceous, laminated to thinly bedded, slightly fractured. @ 11.5'-11.9',12.9'-13.2',14.7' clay seams.							7 1 1 1 1 1 1 1 1 1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	629.6						Bottom of Boring - 16.5'									1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
-															1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
25 								ļ								() ; () ; ()) () () ()) () ()	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
- 30														1 1 4 1	11111	()) () ()) () ()) () (

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Client:	ranSy:	stems	Inc.			· · · · · · · · · · · · · · · · · · ·	DLZ OHIO INC. * 6121 HUNTLEY ROAD, COLUMBUS, OHIO 43229 * (614)88 Project: SCI-823-0.00								Job No. 0121	-3070.03
LOG O	F: Bo	ring ⁻	C-66		_	ocation: Sta	a. 868+30.1, 84.4 ft. RT of SR 823 CL Date Drilled: 10)/10.	_					-		
Depth (ft)	Elev. (ft) 652.5	Blows per 6*	Recovery (in)	Sam No No		Hand Penetro- meter (tsf)	WATER OBSERVATIONS: Water seepage at: None Water level at completion: 3.3' DESCRIPTION	% Aggregate	C. Sand	% M. Sand	% F. Sand	Sitt	% Clay	Natur P	NDARD PENET ral Moisture Con line Blows per foot 0 20 3	itent, % - ● —— I LL
-0.2	-652.3 -649.5	WOH WOH 1	18	1		1.75	Topsoil - 2" Stiff brown SILT (A-4b), little clay, trace gravel; moist to wet. Very stiff to hard brown SILT AND CLAY (A-6a), trace fine to	6	9		6	62	17)		
5 -6.0	-6 46.5 -	10 10	6	2			coarse sand, trace gravel; damp.(Decomposed SHALE). Very dense brown and gray GRAVEL WITH SAND AND SILT	80	5		4	1	1			7
	-6 43. 5-	50/5	3	44			(A-2-4); damp. (Decomposed SANDSTONE). Hard gray SANDSTONE; fine grained, unweathered to slightly									50
10 		Core 60"	Rec 60"	RQD 100%	R1		weathered, micaceous, thinly bedded, unfractured.							1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6		
-14.0 15 - - - 20	638.5						Bottom of Boring - 14.0'							1		
25 —														# 1 # 1		